### DEPARTMENT OF ENVIRONMENTAL REGULATION



ı	APPLICATION TO OPERATE/CONSTRUCT AIR POLLUTION SOURCES
S	SOURCE TYPE: <u>Fossil Fuel Steam Generator</u> [ ] New <sup>1</sup> [X] Existing <sup>1</sup>
A	APPLICATION TYPE: [ ] Construction [ ] Operation [X] Amendment to existing Operation
C	COMPANY NAME: Florida Power & Light Company Permit  COUNTY: Volusia
I	dentify the specific emission point source(s) addressed in this application (i.e., Lime
K	Kiln No. 4 with Venturi Scrubber; Peaking Unit No. 2, Gas Fired) <u>Sanford Unit 4</u>
S	SOURCE LOCATION: Street Lake Monroe off Highway 17-92 City Sanford
1	UTM: East 17-468.3 North 3190.3
ı	Latitude <u>28</u> ° <u>50</u> ′ <u>31</u> "N Longitude <u>81</u> ° <u>19</u> ′ <u>32</u> "W
A	APPLICANT NAME AND TITLE: Charles D. Henderson, P.E., Manager of Air & Water Permitting and
A	APPLICANT ADDRESS: P.O. Box 078768, West Palm Beach, FL 33407-0768
	SECTION I: STATEMENTS BY APPLICANT AND ENGINEER
A	A. APPLICANT
	I am the undersigned owner or authorized representative* of <u>Florida Power &amp; Light</u>
	amendment to existing
ı	I certify that the statements made in this application for an <u>Operation Permit</u> permit are true, correct and complete to the best of my knowledge and belief. Further,
	I agree to maintain and operate the pollution control source and pollution control
	facilities in such a manner as to comply with the provision of Chapter 403, Florida
	Statutes, and all the rules and regulations of the department and revisions thereof. I
l	also understand that a permit, if granted by the department, will be non-transferable
	and I will promptly notify the department upon sale or legal transfer of the permitted establishment.
1 *	
	Attach letter of authorization Signed: C. D. Henderson, P.E.,
	Mgr of Air & Water Permitting and Programs
İ	Name and Title (Please Type)
	Date: 5/13/9Z Telephone No. (407) 697-6960
١,	B. PROFESSIONAL ENGINEER REGISTERED IN FLORIDA (where required by Chapter 471, F.S.)
	This is to certify that the engineering features of this pollution control project have
	been designed/examined by me and found to be in conformity with modern engineering
	principles applicable to the treatment and disposal of pollutants characterized in the
-	permit application. There is reasonable assurance, in my professional judgement, that
1	See Florida Administration Code Rule 17-2.100(57) and (104)

DER Form 17-1.202(1) Effective October 31, 1982

	the pollution control facilities, when properly maintained and operated, will discharge an effluent that complies with all applicable statutes of the State of Florida and the rules and regulations of the department. It is also agreed that the undersigned will furnish, if authorized by the owner, the applicant a set of instructions for the proper maintenance and operation of the pollution control facilities and, in applicable, pollution sources.
	Signed Numore 70/2 mg 5
	Kennard F. Kosky
	Name (Please Type)), (Please Type),
	Company Name (Please Type)
	1034 N.W. 57th Street, Gainesville, FL 32605  Mailing Address (Please Type)
Flo	rida Registration No. 14996 Date: 5/8/92 Telephone No. (904) 331-9000
	SECTION II: GENERAL PROJECT INFORMATION
Α.	Describe the nature and extent of the project. Refer to pollution control equipment, and expected improvements in source performance as a result of installation. State whether the project will result in full compliance. Attach additional sheet if necessary.
	Co-firing of Orimulsion with natural gas and residual oil.
	The amount of Orimulsion fired with natural gas will be controlled to meet proposed
	emission limits of 1.6 lb SO <sub>2</sub> /10 <sup>6</sup> Btu heat input and 0.1 lb particulate/10 <sup>6</sup> Btu heat
•	input (plus an allowance for soot blowing). See Attachment A for further description.
В.	Schedule of project covered in this application (Construction Permit Application Only)
	Start of Construction NA (SEE NOTE BELOW) Completion of Construction NA (SEE NOTE BELOW)
С.	Costs of pollution control system(s): (Note: Show breakdown of estimated costs only for individual components/units of the project serving pollution control purposes. Information on actual costs shall be furnished with the application for operation permit.)
2	No change in the existing pollution control equipment, i.e. cyclones (see Section
	III D).
D.	Indicate any previous DER permits, orders and notices associated with the emission point, including permit issuance and expiration dates.
	A064-132055 Issued 12/16/87 Expires 10/17/92
	AC64-180842 Issued 10/2/90 (test burn permit) Expires 6/30/92 or upon consumption of
	90 full-power burn days.
	Note: The proposed co-firing natural gas and Orimulsion does not require any physical changes to the unit or fuel system.

F	Requested permitted equipment operating time: hrs/day <u>24</u> ; days/wk <u>7</u> ; wks/yr <u>52</u>
]	f power plant, hrs/yr <u>8,760</u> ; if seasonal, describe:
_	<u> </u>
_	
	If this is a new source or major modification, answer the following questions.  (Yes or No) Not Applicable
]	. Is this source in a non-attainment area for a particular pollutant?
]	If yes, has "offset" been applied?
	b. If yes, has "Lowest Achievable Emission Rate" been applied?
	c. If yes, list non-attainment pollutants.
2	2. Does best available control technology (BACT) apply to this source?  If yes, see Section VI.
3	3. Does the State "Prevention of Significant Deterioration" (PSD) requirement apply to this source? If yes, see Sections VI and VII.
4	4. Do "Standards of Performance for New Stationary Sources" (NSPS) apply to this source?
	5. Do "National Emission Standards for Hazardous Air Pollutants" (NESHAP) apply to this source?
1	Do "Reasonably Available Control Technology" (RACT) requirements apply to this source?
	a. If yes, for what pollutants?
	b. If yes, in addition to the information required in this form, any information requested in Rule 17-2.650 must be submitted.
	Attach all supportive information related to any answer of "Yes". Attach any

### SECTION III: AIR POLLUTION SOURCES & CONTROL DEVICES (Other than Incinerators)

Α.	Raw Materials	and Chemicals	Used in your	Process,	if a	applicable:	No change condition	from	existing
		Contar	ninants						

	Contamir	nants	Utilization	Relate to Flow Diagram
Description	Туре	% Wt	Rate - 1bs/hr	Refute to 110W Blugium

- B. Process Rate, if applicable: (See Section V, Item 1)
  - 1. Total Process Input Rate (lbs/hr): N/A
  - 2. Product Weight (lbs/hr): N/A
- C. Airborne Contaminants Emitted: (Information in this table must be submitted for each emission point, use additional sheets as necessary)

(SEE ATTACHMENT A, TABLE A-1)

Name of Contaminant	Emis	sion <sup>1</sup>	Allowed <sup>2</sup> Emission Rate per	Allowable <sup>3</sup> Emission	Potent Emiss		Relate to Flow
Concaminant	Maximum lbs/hr	Actual T/yr	Rule 17-2	lbs/hr	lbs/hr	T/yr	Diagram
	_						
		_					
						· · · · · ·	-

<sup>1</sup>See Section V, Item 2.

<sup>2</sup>Reference applicable emission standards and units (e.g. Rule 17-2.600(5)(b)2. Table II, E. (1) - 0.1 pounds per million BTU heat input)

<sup>3</sup>Calculated from operating rate and applicable standard.

<sup>4</sup>Emission, if source operated with<del>out</del> control (See Section V, Item 3).

DER Form 17-1.202(1) Effective October 31, 1982 D. Control Devices: (See Section V, Item 4)

Name and Type (Model & Serial No.)	Contaminant	Efficiencyª	Range of Particles Size Collected (in microns) (If applicable)	Basis for Efficiency (Section V Item 5)
Multicyclones	Particulate	30.3%	0-5 µm	Manufacturer
		66.2%	5-10 ш	Manufacturer
		86.6%	10-20 шш	Manufacturer
		99.1%	20-45 ш	Manufacturer
		99.5%	> 45 µm	Manufacturer

<sup>&</sup>lt;sup>a</sup> Actual efficiency expected to be lower for fossil fuel combustion products.

E. Fuels (Maximum Orimulsion contribution during co-firing with a corresponding amount of natural gas; see Attachment A)

Type (Be Specific)	Consump	Maximum Heat Input (MMBTU/hr)	
Type (Be specific)	avg/hr max./hr		
Orimulsion	NA	136,615 1b/hr	1,776
Natural gas	NA	2.54ª MMCF	2,538
Total		264,927 1b/hr	4,314

\*Units: Natural Gas--MMCF/hr; Fuel Oils--gallons/hr; Coal, wood, refuse, others--lbs/hr.

\*\*Batural gas heating value = 1,000 Btu/scf and 19,780 Btu/lb; NA = not applicable.

Fuel Analysis: (TYPICAL UNLESS OTHERWISE NOTED)

Percent Sulfur: 1 grain per 100 CF-gas/2	2.8 Orimulsion	Percent Ash: 0.21 for Orimulsion
Density: <u>8.4 for Orimulsion</u>	lbs/gal Typical	Percent Nitrogen: 0.5 for Orimulsion
Heat Capacity: <u>19,780 gas/13,000 Orimul</u>	sion BTU/lb	BTU/gal
Other Fuel Contaminants (which may cause	e air pollution):	see Tables A-1, A-2, and A-3.

F. If applicable, indicate the percent of fuel used for spa	pace heating.
---	---------------

G. Indicate liquid or solid wastes generated and method of disposal.

No change from disposal methods currently approved by the Department.

Maximum

Annual Average <u>N/A</u>

İ	•	•			•	a for each s er:	tack): ft.
Gas Flow	Rate: <u>~1.60</u>	<u>0,000</u> A	CFM <u>~840,</u>	000 DS	SCFM Gas Exi	t Temperatur	e: <u>~375-400</u> °F.
Water Vap	or Content:	<del>~17</del>		<i>x</i>	/elocity: <u>~9</u>	2	FPS
Note: N	latural gas	and Orimuls	sion co-fii	ring flow ch	naracteristi	cs were deve	loped from co-
f	iring tests	•					
		SEC	CTION IV:	INCINERATOR	R INFORMATIO	N	
			N	ot Applicab	le		
Type of Waste	Type O (Plastics)	Type II (Rubbish)	Type III (Refuse)	Type IV (Garbage)	Type IV (Pathologi cal)	Type V (Liq. & Gas By-prod.)	Type VI (Solid By-prod.)
Actual lb/hr Inciner- ated							
Uncon- trolled (lbs/hr)		-	gr <sup>e</sup>			_	
Dogorinti	ion of Waste				1		
							-
		•					/yr
	rer			_	day/wk	w.s	/ 91
					Model No		
							<u>-</u>
						h1	
		Volume		t Release		uel	Temperature
		(ft) <sup>3</sup>		BTU/hr)	Туре	BTU/hr	(°F)
Prima	ry Chamber						
Second	ary Chamber						
_			I		<u> </u>		<u> </u>
Stack Hei	ight:	ft	. Stack D	iameter:		Stack Tem	p
Gas Flow	Rate:		ACFM		DSCF	M* Velocity:	FPS
	more tons dard cubic f					ns rate in g	rains per
Type of p	pollution co	ntrol devi	ces: [ ] C	yclone [ ]	Wet Scrubbe	r [ ] After	burner
			[]0	ther (speci	fy)		

DER Form 17-1.202(1) Effective October 31, 1982

					_					
ltimate disposal	of any	effluent	other	than	that	emitted	from	the	stack	(scrubber wate

NOTE: Items 2, 3, 4, 6, 7, 8, and 10 in Section V must be included where applicable.

### SECTION V: SUPPLEMENTAL REQUIREMENTS

Please provide the following supplements where required for this application.

- Total process input rate and product weight -- show derivation [Rule 17-2.100(127)]
   Not Applicable
- 2. To a construction application, attach basis of emission estimate (e.g., design calculations, design drawings, pertinent manufacturer's test data, etc.) and attach proposed methods (e.g., FR Part 60 Methods, 1, 2, 3, 4, 5) to show proof of compliance with applicable standards. To an operation application, attach test results or methods used to show proof of compliance. Information provided when applying for an operation permit from a construction permit shall be indicative of the time at which the test was made.

See Attachment A; Table A-1; Table A-3

- Attach basis of potential discharge (e.g., emission factor, that is, AP42 test).
   See Attachment A; Table A-1
- 4. With construction permit application, include design details for all air pollution control systems (e.g., for baghouse include cloth to air ratio; for scrubber include cross-section sketch, design pressure drop, etc.)

Not Applicable

- 5. With construction permit application, attach derivation of control device(s) efficiency. Include test or design data. Items 2, 3 and 5 should be consistent: actual emissions = potential (1-efficiency). Not Applicable
- 6. An 8 ½" x 11" flow diagram which will, without revealing trade secrets, identify the individual operations and/or processes. Indicate where raw materials enter, where solid and liquid waste exit, where gaseous emissions and/or airborne particles are evolved and where finished products are obtained. See Attachment A; Figure A-3
- 7. An 8 ½" x 11" plot plan showing the location of the establishment, and points of airborne emissions, in relation to the surrounding area, residences and other permanent structures and roadways (Examples: Copy of relevant portion of USGS topographic map).

  See Attachment A; Figure A-1
- 8. An 8 ½" x 11" plot plan of facility showing the location of manufacturing processes and outlets for airborne emissions. Relate all flows to the flow diagram.

  See Attachment A; Figure A-2

9.		accordance with Rule 17-4.05. The check should be Environmental Regulation. Applicable fee enclosed
10.		permit, attach a Certificate of Completion of ource was constructed as shown in the construction
	SECTION VI: BEST	F AVAILABLE CONTROL TECHNOLOGY
		Not Applicable
Α.	Are standards of performance for new applicable to the source?	stationary sources pursuant to 40 C.F.R. Part 60
	[ ] Yes [ ] No	
	Contaminant	Rate or Concentration
	-	· -
В.	yes, attach copy)	control technology for this class of sources (If
	[ ] Yes [ ] No	
	Contaminant	Rate or Concentration
C.	What emission levels do you propose	as best available control technology?
	Contaminant	Rate or Concentration
;		<u> </u>
	-	
D.	Describe the existing control and to	reatment technology (if any).
	1. Control Device/System:	2. Operating Principles:
	3. Efficiency:*	4. Capital Costs:
	-	
*Ex	plain method of determining	

DER Form 17-1.202(1) Effective October 31, 1982

	5.	Useful Life:		6.	Operating Costs:	
	7.	Energy:		8.	Maintenance Cost:	
	9.	Emissions:				
		Contaminant			Rate or Concentr	ation
	10.	Stack Parameters	3			
	a.	Height:	ft.	Ъ.	Diameter	ft.
	с.	Flow Rate:	ACFM	d.	Temperature:	°F.
	е.	Velocity:	FPS	•		
Ε.		cribe the control and additional pages if		ology av	vailable (As many t	ypes as applicable,
	1.					_
	a.	Control Devices:		ь.	Operating Princip	oles:
	c.	Efficiency: 1		d.	Capital Cost:	
	e.	Useful Life:		f.	Operating Cost:	
	g.	Energy: <sup>2</sup>		h.	Maintenance Cost:	
	i.	Availability of cons		-	rocess chemicals:	
	j.	Applicability to man	• •			
	k.	Ability to construct within proposed level		vice, ir	nstall in available	e space, and operate
	2.					
	a.	Control Device:		b.	Operating Princip	oles:
	c.	Efficiency:1		d.	Capital Cost:	
	e.	Useful Life:		f.	Operating Cost:	
	g.	Energy: <sup>2</sup>		h.	Maintenance Cost:	:
	i.	Availability of con	struction materia	ls and p	process chemicals:	
	_	n method of determing to be reported in u	_	l power	- KWH design rate.	

- j. Applicability to manufacturing processes: k. Ability to construct with control device, install in available space, and operate within proposed levels: 3. Control Device: b. Operating Principles: a. c. Efficiency:1 d. Capital Cost: Useful Life: f. Operating Cost: е. Maintenance Cost: Energy:2 h. g. i. Availability of construction materials and process chemicals: j. Applicability to manufacturing processes: Ability to construct with control device, install in available space, and operate k. within proposed levels: 4. Control Device: b. Operating Principles: c. Efficiency:1 d. Capital Cost: Useful Life: f. Operating Cost: е. Energy:2 Maintenance Cost: h. i. Availability of construction materials and process chemicals: j. Applicability to manufacturing processes: k. Ability to construct with control device, install in available space, and operate within proposed levels: Describe the control technology selected: 1. Control Device: 2. Efficiency: 1 4. Useful Life: 3. Capital Cost:
- - 5. Operating Cost:

6. Energy:<sup>2</sup>

7. Maintenance Cost:

- Manufacturer:
- 9. Other locations where employed on similar processes:
- a. (1) Company:
- (2) Mailing Address:
- (3) City:

(4) State:

Explain method of determining efficiency.  $^2$ Energy to be reported in units of electrical power - KWH design rate.

(6)		
	Telephone No.:	
(7)	Emissions:1	
	Contaminant	Rate or Concentration
		· · · · · · · · · · · · · · · · · · ·
(8)	Process Rate:1	
Ъ.	(1) Company:	
(2)	Mailing Address:	
(3)	City:	(4) State:
(5)	Environmental Manager:	
(6)	Telephone No.:	
(7)	Emissions:1	
	Contaminant	Rate or Concentration
(8)	Process Rate:1	· · · · · · · · · · · · · · · · · · ·
	Reason for selection and	description of systems:
10.		
Applica vailab	le, applicant must state th	rmation when available. Should this information not be he reason(s) why.  PREVENTION OF SIGNIFICANT DETERIORATION  Not Applicable
Applica vailab	le, applicant must state th SECTION VII - pany Monitored Data	he reason(s) why.  PREVENTION OF SIGNIFICANT DETERIORATION  Not Applicable
Applica vailab . Comp	le, applicant must state th SECTION VII - pany Monitored Data	he reason(s) why.  PREVENTION OF SIGNIFICANT DETERIORATION  Not Applicable  TSP () SO <sup>2*</sup> Wind spd/dir  to /
Applica vailab Comp	le, applicant must state th  SECTION VII -  pany Monitored Data  no. sites	he reason(s) why.  PREVENTION OF SIGNIFICANT DETERIORATION  Not Applicable
Applica vailab . Comp l Per	le, applicant must state the SECTION VII - pany Monitored Data no. sites iod of Monitoring	he reason(s) why.  PREVENTION OF SIGNIFICANT DETERIORATION  Not Applicable  TSP () SO <sup>2*</sup> Wind spd/dir  to /
Applica availab . Comp l Per:	le, applicant must state the SECTION VII - pany Monitored Data no. sites iod of Monitoring er data recorded	he reason(s) why.  PREVENTION OF SIGNIFICANT DETERIORATION  Not Applicable  TSP () SO <sup>2*</sup> Wind spd/dir  month day year month day year
Applica availab . Comp l Per:	le, applicant must state the SECTION VII - pany Monitored Data no. sites iod of Monitoring er data recorded	he reason(s) why.  PREVENTION OF SIGNIFICANT DETERIORATION  Not Applicable  TSP () SO <sup>2*</sup> Wind spd/dir  / to /  month day year month day year
Applicativailab	le, applicant must state the SECTION VII - pany Monitored Data no. sites iod of Monitoring er data recorded	he reason(s) why.  PREVENTION OF SIGNIFICANT DETERIORATION  Not Applicable  TSP () SO <sup>2*</sup> Wind spd/dir  month day year month day year  1 summaries to this application.

	a. Was instrumentation EPA referenced	or its eq	uivalent?	[ ] Yes [	] No	
	b. Was instrumentation calibrated in a	accordance	with Depar	tment proce	dures?	
	[ ] Yes [ ] No [ ] Unknown					
В.	Meteorological Data Used for Air Qualis	ty Modelin	ıg			
	1 Year(s) of data from month		t	o	/_/	<u>,                                      </u>
	month	day	year	month	day	year
	2. Surface data obtained from (location	on)	<u></u>			
	3. Upper air (mixing height) data obta	ained from	(location)			
	4. Stability wind rose (STAR) data ob	tained fro	om (location	)		
C.	Computer Models Used					
	1	-	Modified?	If ves. at	tach de	escription.
			_	-		-
	2.		_ Modified?	lf yes, at	tach de	escription.
	3		Modified?	If yes, at	tach de	escription.
	4		Modified?	If yes, at	tach de	escription.
	Attach copies of all final model runs	showing ir	nput data, r	eceptor loc	ations,	and
	principle output tables.					
D.	Applicants Maximum Allowable Emission	Data				
	Pollutant Emission	Rate				
	TSP		gram	s/sec		
	S0 <sup>2</sup>		gram	s/sec		
E.	Emission Data Used in Modeling					
	Attach list of emission sources. Emis point source (on NEDS point number), U and normal operating time.					
	. 0					
F.	Attach all other information supportiv	re to the 1	PSD review.			
G.	Discuss the social and economic impact applicable technologies (i.e, jobs, pa assessment of the environmental impact	yroll, pro	oduction, ta			
Н.	Attach scientific, engineering, and te	chnical ma	aterial, rep	orts, publ	ication	s, journals,

2. Instrumentation, Field and Laboratory

requested best available control technology.

and other competent relevant information describing the theory and application of the

### **ATTACHMENT A**

### 1.0 BACKGROUND

The Florida Power & Light Company (FPL) Sanford Plant is located in Volusia County adjacent to Lake Monroe (see Figure A-1). The Sanford Plant comprises three fossil-fuel-fired steam electric generating units, designated as Units No. 3, 4, and 5 (see Figure A-2). Unit No. 3 is a 160-megawatt (MW) class unit placed in service in 1959, and Units No. 4 and 5 are 400-MW class units placed in service in 1972 and 1973, respectively.

Sanford Unit No. 4 includes a Foster-Wheeler steam generator originally designed to fire a variety of fossil fuels and has been typically fired with liquid fossil fuels and natural gas, as currently authorized under Florida Department of Environmental Regulation (FDER) air permit No. A064-132055. The unit is classified as an "existing fossil fuel steam generator" and is subject to the emission-limiting standards set forth in Florida Administrative Code (FAC) Rule 17-2.600(5)(a).

Orimulsion is a heavy hydrocarbon fuel consisting of an emulsion of a heavy bitumen in water. On October 4, 1990, FPL received authorization (FDER permit number AC64-180842; PSD-FL-150; Research and Testing Order) to test burn Orimulsion in Unit 4. The results of this test indicated that Orimulsion could effectively be burned in Unit 4 as an alternative fuel either by itself or in conjunction with natural gas.

In January 1992, FPL requested an amendment to its air operation permit for Sanford Unit No. 4 (A064-132055) to co-fire natural gas and the Orimulsion remaining at the Sanford plant and at the Port of Jacksonville. On February 12, 1992, the air operation permit for Unit No. 4 was amended to allow FPL to co-fire approximately 200,000 barrels of Orimulsion with natural gas through June 30, 1992. The remaining Orimulsion was co-fired with natural gas under the terms of the permit, as amended, concluding on April 17, 1992.

### 2.0 PROJECT DESCRIPTION

Sanford Unit 4 currently has the full capability of burning residual oil, natural gas, and Orimulsion. No additional equipment or modifications to

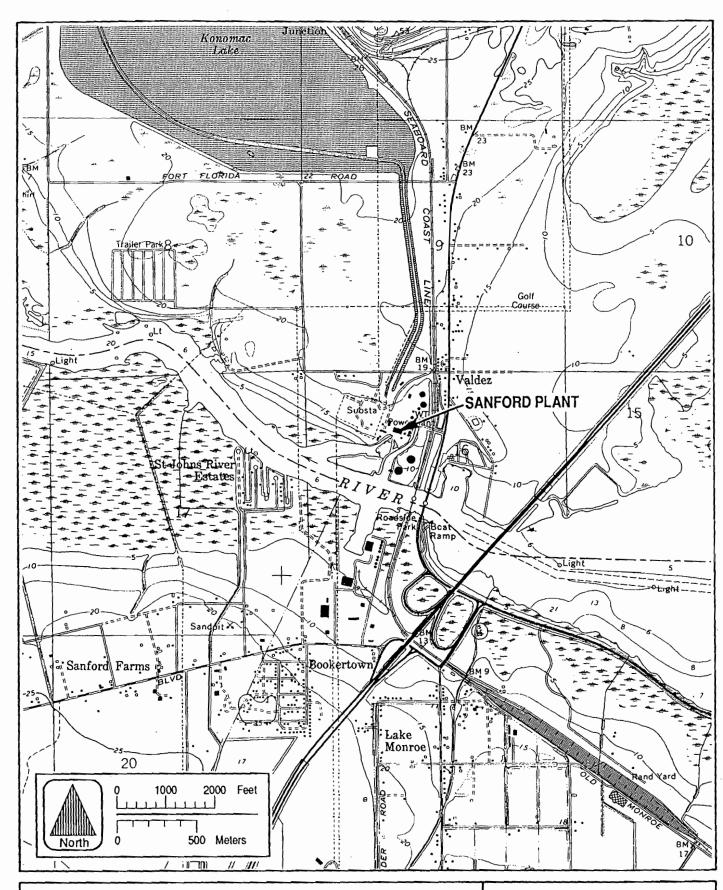


Figure A-1 SANFORD PLANT LOCATION MAP



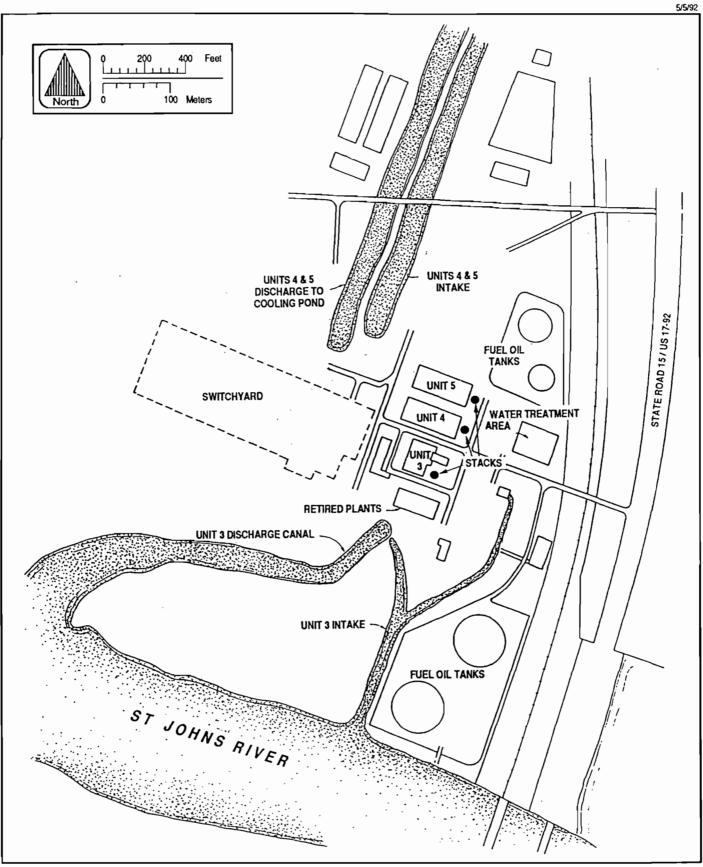


Figure A-2 PLOT PLAN OF FPL SANFORD PLANT



existing equipment will be required for co-firing. A flow diagram of Unit No. 4 is provided in Figure A-3. FPL proposes to co-fire a mixture of natural gas and Orimulsion. The maximum amount of Orimulsion that will be co-fired with natural gas will be consistent with the proposed emission limits. The proposed emission limits are at or below those currently authorized for Unit 4.

Because the cost of Orimulsion is lower than residual oil or natural gas, this project will allow FPL's customers to directly benefit from co-firing.

During certain operating conditions, Orimulsion, natural gas, and residual oil will be co-fired. Under these conditions, the amount of Orimulsion and natural gas co-fired will be reduced, but in proportion to meet the proposed emission limits. Residual oil will be used to make up any difference between the load with Orimulsion/natural gas co-firing and full load. For example, if natural gas and Orimulsion make up 50 percent of full load, the ratio will be approximately 30:20 with the remaining 50 percent load made up by firing residual oil. The amount of Orimulsion and residual oil used during co-firing will meet the proposed emission limits.

### 3.0 REGULATED POLLUTANT EMISSIONS

Maximum potential air emissions from Unit No. 4 when burning either No. 6 oil, natural gas, or natural gas and Orimulsion are presented in Table A-1. The maximum allowable emissions when burning No. 6 (i.e., residual) oil, based upon limitations in Rule 17-2.600 (5)(a) Florida Administrative Code (FAC) and the current operating permit, are as follows:

Particulate matter - 0.1 lb/million (MM) Btu (steady state)

- 0.3 lb/MM Btu, maximum 3-hours (soot blowing/load changes)

Sulfur dioxide - 2.75 lb/MM Btu

Visible Emissions - 40 percent opacity (steady state)

- 60 percent opacity (soot blowing/load changes)

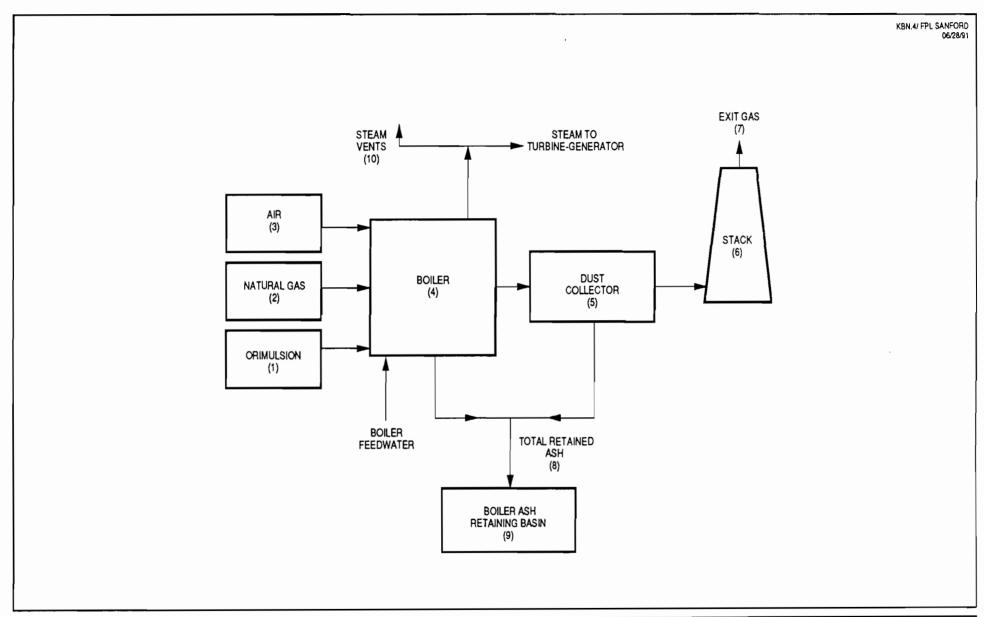


Figure A-3 FLOW DIAGRAM, SANFORD UNIT 4



Table A-1. Maximum Estimated Emissions for Residual Oil, Natural Gas and Natural Gas/Orimulsion Firing at FPL Sanford Unit 4 (Page 1 of 2)

Data	Residual Oil	Natural Gas	Natural Gas and Orimulsion
eat Input (10° Btu/hr)	4,050	4,230	4,314
uel Flow (lb/hr)	221,311	213,852	264,927
ulfur Dioxide			
Emissions Basis	Permit	See Note b	See Note o
Emissions Basis (lb/106 Btu)	2.75	0.00286	1.60
Emissions (lb/hour) Emissions (tons/year)	11,138 48,782	12 53	6,902 30,233
lambi laba Mabban			
articulate Matter Emissions Basis	Permit <sup>e</sup>	AP-42	Permit
Emissions Basis (lb/106 Btu)	0.125	0.0050	0.12
Emissions (1b/hour)	506	21	539
Emissions (tons/year)d	2,217	93	2,26
articulate Matter (PM10)			
Emissions Basis	Permit*	AP-42	Permit
Emissions Basis (lb/106 Btu)	0.125	0.0050	0.12
Emissions (lb/hour)	506	21	539
Emissions (tons/year)d	2,217	93	2,36
itrogen Oxides			m
Emissions Basis	AP-42f	AP-42	Test Result
Emissions Basis (1b/10° Btu)	0.70 2.834	0.55 2,327	2,42
Emissions (lb/hour) Emissions (tons/year)d	12,412	10,190	10,62
arbon Monoxide			
Emissions Basis	AP-42	AP-42	AP-4
Emissions Basis (1b/106 Btu)	0.03	0.04	0.0
Emissions (lb/hour)	135	169	16
Emissions (tons/year)	591	741	70
Volatile Organic Compounds			
Emissions Basis	AP-42	AP-42	Test Result
Emissions Basis (lb/106 Btu)	0.005	0.0014	0.003
Emissions (1b/hour)	20.5	5.9 25.9	13. 59.
Emissions (tons/year)d	89.8	25.9	J <del>9</del> .
ead	ED4 (1000)		Took Booule
Emissions Basis Emissions Basis (lb/106 Btu)	EPA(1989) 2.80E-05	neg.	Test Result N
Emissions (lb/hour)	0.11	0.00	N.
Emissions (tons/year)	0.50	0	N
Sulfuric Acid Mist			
Emissions Basis	AP-42	AP-42	Test Result
Emissions Basis (1b/106 Btu)	0.048	2.86E-05	0.003
Emissions (lb/hour)	196	0.12	12.
Emissions (tons/year)	857	1	5
otal Fluorides			
Emissions Basis	EPA (1981)	EPA (1981)	a sa= -
Emissions Basis (1b/106 Btu)	6.29E-06	neg.	2.59E-0
Emissions (lb/hour) Emissions (tons/year)d	2.55E-02 1.12E-01	0.00 0	1.12E-0 4.89E-0
dercury			
Emissions Basis	EPA (1989)	KBN (1992)	Test Result
Emissions Basis (1b/106 Btu)	3,20E-06	2.70E-08	1.02E-0
Emissions (lb/hour)	1.30E-02	1.14E-04	4.41E-0
Emissions (tons/year)d	5.68E-02	5.00E-04	1.93E-0

Table A-1. Maximum Estimated Emissions for Residual Oil, Natural Gas and Natural Gas/Orimulsion Firing at FPL Sanford Unit 4 (Page 2 of 2)

Data	Residual Oil	Natural Gas	Natural Gas and Orimulsion <sup>a</sup>
Beryllium			
Emissions Basis	EPA (1989)	Test Results	
Emissions Basis (lb/106 Btu)	4.20E-06	neg.	2.53E-08
Emissions (lb/hour)	1.70E-02	0.00	1.09E-04
Emissions (tons/year)d	7.45E-02	0	4.78E-04
Arsenic			
Emissions Basis	EPA (1989)	Test Results	
Emissions Basis (lb/106 Btu)	1.90E-05	neg.	1.01E-06
Emissions (lb/hour)	7.70E-02	0.00	4.35E-03
Emissions (tons/year)d	3.37E-01	0	1.91E-02

Based on 60% full load with natural gas(2,538 10° Btu/hr) and 40% full load on Orimulsion (1,776 10° Btu/hr).

### Sources:

Environmental Protection Agency (EPA). 1989. Estimating Air Toxics Emissions from Coal and Oil Combustion Sources. EPA-450/2-89-001

KBN. 1992. Mercury Emission Inventory for Florida.

Environmental Protection Agency (EPA). 1981. Emissions Assessment of Conventional Stationary Systems: Volume III. External Combustion Sources of Electricity Generation. EPA-600/7-81-003a.

<sup>1</sup> grain sulfur/100 scf from Florida Gas Transmission data.

c Amount of Orimulsion will be adjusted to meet proposed emission limit (see Table A-2).

d assumes 8,760 hours per year operation.

based on an average of 0.1 lb/10° Btu for 21 hours and excess emissions of 0.3 lb/10° Btu for 3 hours.

f based on vertical fired boilers, could be as high as 1 lb/106 Btu due to low excess air burners.

The proposed maximum emission limitations and opacity limits during any period that Orimulsion is co-fired in Unit 4 are:

Particulate matter - 0.1 lb/MM Btu (steady state)

- 0.3 lb/MM Btu, maximum 3-hours (soot

blowing/load changes)

Sulfur dioxide - 1.6 lb/MM Btu

Visible Emissions - 35 percent opacity (steady state)

- 60 percent opacity (soot blowing/load changes)

The maximum emissions of particulate matter will be no higher than the present limitations for residual oil. During the Orimulsion test burn, particulate matter testing was conducted on May 28 and 29, 1991, with Unit 4 co-firing natural gas and Orimulsion at a ratio of 60 and 40 percent of total heat input, respectively. Results of this testing indicated an emission rate of 0.09 lb/MMBtu and 0.15 lb/MMBtu during steady-state and soot blowing conditions, respectively. (These tests results for co-firing were transmitted to the FDER central district office on June 12, 1991.) Opacity during the co-firing particulate test, as measured by the continuous opacity measurement instrument, averaged 18 percent under steady-state conditions and 28.5 percent under soot-blowing conditions. Compliance with the proposed sulfur dioxide limit will be assured by limiting the maximum percentage of Orimulsion in the co-firing mixture to meet the proposed limit.

As shown in Table A-1, co-firing a mixture with the maximum component of Orimulsion with natural gas will result in emission rates, for virtually all regulated pollutants, that are lower than burning No. 6 fuel oil.

### 4.0 NONREGULATED POLLUTANT EMISSIONS

Nonregulated pollutant emissions from co-firing of natural gas and Orimulsion were estimated using test results taken by Entropy Environmentalists Inc. in April 1991 with Unit 4 operating on 100 percent Orimulsion. A copy of these test results has been submitted to FDER as part of the Orimulsion test burn program (May 1991). Table A-2 presents a comparison of nonregulated pollutant emissions for residual oil, natural

Table A-2. Maximum Estimated Emissions for Residual Oil, Natural Gas and Natural Gas/Orimulsion Firing at FPL Sanford Unit 4 (Non-regulated Pollutants) (Page 1 of 2)

	Data	Residual Oil	Natural Gas	Natural Gas and Orimulsion <sup>a</sup>
Antimony				
Emissions	Basis	EPA (1981)		Test Results
Emissions	Basis $(1b/10^6 \text{ Btu})$	2.33E-05	neg.	1.08E-06
	(lb/hour)	9.44E-02	0.00	4.65E-03
Emissions	(tons/year) <sup>b</sup>	0.41	0	0.020
Barium				
Emissions	Basis	EPA (1981)		Test Results
Emissions	Basis ( $1b/10^6$ Btu)	6.71E-05	neg.	1.72E-06
	(lb/hour)	2.72E-01	0.00	7.41E-03
Emissions	(tons/year) <sup>b</sup>	1.19	0	0.032
Cadmium				
Emissions		EPA (1989)		Test Results
Emissions	Basis (lb/10 <sup>6</sup> Btu)	1.57E-05	neg.	2.34E-06
Emissions	(lb/hour)	6.36E-02	0.00	1.01E-02
Emissions	(tons/year) <sup>b</sup>	0.28	0	0.044
Chromium				
Emissions	Basis	EPA (1989)		Test Results
	Basis $(1b/10^6 \text{ Btu})$	2.10E-05	neg.	8.07E-06
	(lb/hour)	8.51E-02	0.00	3.48E-02
Emissions	(tons/year) <sup>b</sup>	0.37	0	0.152
Copper				
Emissions		EPA (1989)		Test Results
	Basis $(1b/10^6 \text{ Btu})$	2.80E-04	neg.	4.90E-06
	(lb/hour)	1.13	0.00	2.11E-02
Emissions	(tons/year) <sup>b</sup>	4.97	0	0.093
Manganese				
Emissions		EPA (1989)		Test Results
	Basis (lb/10 <sup>6</sup> Btu)	2.60E-05	neg.	8.27E-06
	(lb/hour)	0.11	0.00	3.57E-02
Emissions	(tons/year) <sup>b</sup>	0.46	0	0.156
Nickel				
Emissions		EPA (1989)		Test Results
	Basis (lb/10 <sup>6</sup> Btu)	1.26E-03	neg.	1.50E-03
	(lb/hour)	5.10	0.00	6.48
Emissions	(tons/year) <sup>b</sup>	22.35	0	28.39

Table A-2. Maximum Estimated Emissions for Residual Oil, Natural Gas and Natural Gas/Orimulsion Firing at FPL Sanford Unit 4 (Non-regulated Pollutants) (Page 2 of 2)

	Data		Residual Oil	Natu Ga		Natural Gas and Orimulsion <sup>a</sup>
Phosphorus						
Emissions	Basis		EPA (1981)			Test Results
	Basis $(1b/10^6)$	Btu)	5.83E-05	т	neg.	1.26E-05
Emissions			0.24	(	0.00	0.054
	(tons/year)b		1.03		0	0.24
Selenium						
Emissions	Basis		EPA (1981)			Test Results
Emissions	Basis $(1b/10^6)$	Btu)	3.73E-05	T	neg.	5.19E-06
Emissions			0.15	(	0.00	0.022
Emissions	(tons/year) <sup>b</sup>		0.66		0	0.10
Silver						
Emissions			EPA (1981)			Test Results
	Basis ( $1b/10^6$	Btu)	1.63E-05		neg.	1.26E-06
Emissions			0.07	(	0.00	5.43E-03
Emissions	(tons/year) <sup>b</sup>		0.29		0	0.02
Thallium						
Emissions	_		EPA (1981)			Test Results
	Basis $(1b/10^6)$	Btu)	1.09E-05		neg.	ND
	(lb/hour)		0.04	•	0.00	ND
Emissions	(tons/year) <sup>b</sup>		0.19		0	
Vanadium						
Emissions			EPA (1981)			Test Results
	Basis $(1b/10^6)$	Btu)	8.52E-03		neg.	5.97E-03
	(lb/hour)		34.50		0.00	25.75
Emissions	(tons/year) <sup>b</sup>		151.11		0	112.79
Zinc						
Emissions			EPA (1981)			Test Results
	Basis (1b/10 <sup>6</sup>	Btu)	6.71E-05		neg.	1.48E-05
	(lb/hour)		0.27		0.00	0.064
Emissions	(tons/year)b		1.19		0	0.28

 $<sup>^{\</sup>rm a}$  Based on 60% of full load on natural gas (2,538  $10^{\rm 6}$  Btu/hr) and 40% of full load on Orimulsion (1,776  $10^{\rm 6}$  Btu/hr).

Sources: Environmental Protection Agency (EPA). 1989. Estimating Air Toxics Emissions from Coal and Oil Combustion Sources. EPA-450/2-89-001.

Environmental Protection Agency (EPA). 1981. Emissions Assessment of Conventional Stationary Systems: Volume III. External Combustion Sources of Electricity Generation. EPA-600/7-81-003a.

b assumes 8,760 hours per year operation.

gas, and natural gas/Orimulsion. EPA emission factors were used to estimate emissions of residual oil firing. Natural gas is believed to contain negligible quantities of these pollutants.

Table A-2 indicates that nonregulated pollutant emissions produced by cofiring natural gas and Orimulsion are generally lower than those for residual oil firing except for nickel. Nickel emissions for co-firing are estimated to be 1.38 lb/hr higher than those estimated for residual oil.

### 5.0 EMISSION CALCULATIONS

Table A-3 presents the emission calculations for co-firing the maximum amount of Orimulsion co-fired with natural gas. EPA emission factors and the summary from the Entropy Environmentalists Inc. tests are attached. Table A-4 presents example emission calculations for co-firing Orimulsion, natural gas, and residual oil. This example is based on firing 20 percent Orimulsion, 30 percent natural gas, and 50 percent residual oil as a percent of full load. All emission rates when co-firing Orimulsion, natural gas, and residual oil will be equal to or lower than the corresponding pollutant emission rates when either firing only residual oil or co-firing the maximum percentage of Orimulsion and natural gas.

### 6.0 AIR QUALITY IMPACTS

The impacts of co-firing natural gas and Orimulsion will not exceed federal or state ambient air quality standards or Prevention of Significant Deterioration increments. This conclusion has been demonstrated in the modeling analysis performed for the test burn which evaluated 100 percent Orimulsion firing for Unit 4. A copy of the analysis can be found in the application for test burn.

FDER previously requested that the maximum air quality impact be determined for any potential toxic pollutants that may be emitted during co-firing. To evaluate the potential impacts of toxic pollutants, FDER has proposed a list of ambient air concentration levels for toxic pollutants (FDER, 1991). These levels are referred to as No Threat Levels (NTLs) and are intended to provide an adequate margin of safety for the maintenance of public health.

Table A-3. Emission Calculations for Co-Firing of Orimulsion and Natural Gas (Page 1 of 3)

Data	Orimulsion	Natural Gas	Total
Full Load (%)	40.00%	60.00%	100.00%
Heat Input (10 <sup>6</sup> Btu/hr) <sup>a</sup>	1,776	2,538	4,314
Fuel Flow (lb/hr)	136,615	128,311	264,927
Sulfur Dioxide			
Emissions Basis	Fuel <sup>b</sup>	1 gr/100 cf	
Emissions Basis ( $1b/10^6$ Btu)	Fuel <sup>b</sup>	0.00286	1.60
Emissions (lb/hour)	6,895	7	6,902
Particulate Matter			
Emissions Basis	$Proposed^c$	AP-42	
Emissions Basis (1b/10 <sup>6</sup> Btu)	- Proposed <sup>c</sup>	0.0050	0.125
Emissions (lb/hour)	526	13	539
Particulate Matter (PM10)			
Emissions Basis	Proposed <sup>c</sup>	AP-42	
Emissions Basis (1b/10 <sup>6</sup> Btu)	Proposed <sup>c</sup>	0.0050	0.125
Emissions (lb/hour)	526	13	539
Nitrogen Oxides			
Emissions Basis	Test Results <sup>d</sup>	AP-42	
Emissions Basis (1b/10 <sup>6</sup> Btu)	0.58	0.55	0.562
Emissions (lb/hour)	1,030	1,396	2,426
Carbon Monoxide			
Emissions Basis	AP-42	AP-42	
Emissions Basis (lb/10 <sup>6</sup> Btu)	0.03	0.04	0.037
Emissions (lb/hour)	59	102	161
Volatile Organic Compounds			
Emissions Basis	Test Results <sup>d</sup>	AP-42	
Emissions Basis (lb/10 <sup>6</sup> Btu)	0.006	0.0014	0.003
Emissions (lb/hour)	10.1	3.6	13.7
Sulfuric Acid Mist			
Emissions Basis	Test Results	AP-42	
Emissions Basis (lb/10 <sup>6</sup> Btu)	0.0072	2.86E-05	0.0030
Emissions (lb/hour)	12.8	0.12	12.9
Total Fluorides			
Emissions Basis	EPA (1981)		
Emissions Basis (lb/10 <sup>6</sup> Btu)	6.29E-06	neg.	2.59E-06
Emissions (lb/hour)	0.01	0.00	1.12E-02
	- · - <del>-</del>		

Table A-3. Emission Calculations for Co-Firing of Orimulsion and Natural Gas (Page 2 of 3)

Data		Orimulsion	Natural Gas	Total
Basis Basis (1b/10 <sup>6</sup> I (1b/hour)	Btu)	Test Results 2.10E-07 3.73E-04	KBN (1992) 2.70E-08 6.85E-05	1.02E-07 4.41E-04
Basis Basis (1b/10 <sup>6</sup> I (1b/hour)	Btu)	Test Results 6.15E-08 1.09E-04	neg. 0.00	2.53E-08 1.09E-04
Basis (lb/l0 <sup>6</sup> l (lb/hour)		Test Results 2.45E-06 4.35E-03	neg. 0.00	1.01E-06 4.35E-03
Basis Basis (1b/10 <sup>6</sup> 1 (1b/hour)		Test Results 2.62E-06 4.65E-03	neg. 0.00	1.08E-06 4.65E-03
Basis Basis (1b/10 <sup>6</sup> ) (1b/hour)	Btu)	Test Results 4.17E-06 7.41E-03	neg. 0.00	1.72E-06 7.41E-03
Basis Basis (lb/10 <sup>6</sup> ) (lb/hour)	Btu)	Test Results 5.69E-06 1.01E-02	neg. 0.00	2.34E-06 1.01E-02
Basis Basis (1b/10 <sup>6</sup> ) (1b/hour)	Btu)	Test Results 1.96E-05 3.48E-02	neg. 0.00	8.07E-06 3.48E-02
Basis Basis (1b/10 <sup>6</sup> ) (1b/hour)	Btu)	Test Results 1.19E-05 2.11E-02	neg. 0.00	4.90E-06 2.11E-02
Basis Basis (1b/10 <sup>6</sup> ) (1b/hour)	Btu)	Test Results 2.01E-05 3.57E-02	neg. 0.00	8.27E-06 3.57E-02

Table A-3. Emission Calculations for Co-Firing of Orimulsion and Natural Gas (Page 3 of 3)

Data		Orimulsion	Natural Gas	Total
Nickel				
Emissions Basis		Test Results		
Emissions Basis	$(1b/10^6 \text{ Btu})$	3.65E-03	neg.	1.50E-03
Emissions (lb/ho	our)	6.48	0.00	6.48
Phosphorus				
Emissions Basis		Test Results		
Emissions Basis	$(1b/10^6 \text{ Btu})$	3.05E-05	neg.	1.26E-05
Emissions (lb/ho	our)	5.42E-02	0.00	5.42E-02
Selenium				
Emissions Basis		Test Results		
Emissions Basis	$(1b/10^6 \text{ Btu})$	1.26E-05	neg.	5.19E-06
Emissions (1b/ho	our)	2.24E-02	0.00	2.24E-02
Silver	F*,			
Emissions Basis		Test Results		
Emissions Basis	$(1b/10^6 Btu)$	3.06E-06	neg.	1.26E-06
Emissions (1b/ho		5.43E-03	0.00	5.43E-03
Vanadium				
Emissions Basis		Test Results		
Emissions Basis	$(1b/10^6 \text{ Btu})$	1.45E-02	neg.	5.97E-03
Emissions (1b/ho	• •	2.58E+01	0.00	2.58E+01
Zinc				
Emissions Basis		Test Results		
Emissions Basis	$(1b/10^6 \text{ Btu})$	3.60E-05	neg.	1.48E-05
Emissions (1b/ho	•	6.39E-02	0.00	6.39E-02
Emissions (lb/ho	our)	6.39E-02	0.00	6.39E-02

Note: lb/hr is calculated based on the heat input for the fuel specified.
"Test Results" refer to the stack tests performed by Entropy
Environmentalists Inc., April 1-5 and 8-12, 1991.

<sup>&</sup>lt;sup>a</sup> The heat input based on 40% Orimulsion and 60% natural gas of full load. Orimulsion =  $4,440\ 10^6$  Btu/hr \*  $0.40 = 1,776\ 10^6$  Btu/hr Natural Gas =  $4,230\ 10^6$  Btu/hr \*  $0.60 = 2,538\ 10^6$  Btu/hr The approximate sulfur dioxide-emission rate of Orimulsion under these conditions would be about  $3.9\ 1b/10^6$  BTU, which is in the lower sulfur range received during the co-firing test burn. This emission rate is equivalent to about 2.5 percent sulfur in Orimulsion.

<sup>&</sup>lt;sup>b</sup> Based on a maximum emission rate when co-firing of  $1.6 \text{ lb}/10^6 \text{ Btu}$ .

<sup>&</sup>lt;sup>c</sup> Based on a maximum emission rate when co-firing of  $0.1~\rm{lb/10^6}$  Btu under steady state (21 hours) and less than  $0.3~\rm{lb/10^6}$  Btu for soot blowing/load changes (3 hours); PM and PM10 are assumed to be the same.

<sup>&</sup>lt;sup>d</sup> Maximum from Entropy stack tests.

Table A-4. Example Emission Calculations for Co-Firing of Orimulsion, Natural Gas and Residual Oil (Page 1 of 2)

Data	Orimulsion	Natural Gas	Residual Oil	Total
ull Load (%)	20.00%	30.00%	50.00%	100.00%
eat Input (10° Btu/hr)	888	1,269	2,025	4,182
uel Flow (lb/hr)	68.308	64,156	110,656	243,119
, , , , , , , , , , , , , , , , , , , ,	00,000	• 1,	,	,
lfur Dioxide				
Emissions Basis	Fuel <sup>b</sup>	1 gr/100 cf	Fuel <sup>b</sup>	
Emissions Basis (lb/10° Btu)	Fuel	0.00286	1.6	1.60
Emissions (lb/hour)	3,448	7	3,236	6,691
articulate Matter Emissions Basis	Proposed	AP-42	Permitted	
Emissions Basis (1b/10° Btu)	Proposed <sup>c</sup>	0.0050	0.125	0.125
Emissions (lb/hour)	257	13	253	523
•				
articulate Matter (PM10)			_	
Emissions Basis	Proposed	AP-42	Permitted	
Emissions Basis (lb/106 Btu)	Proposed	.0.0050	0.125	0.125
Emissions (lb/hour)	257	_ 13	253	523
trogen Oxides				
Emissions Basis	Test Resultsd	AP-42	AP-42	
Emissions Basis (1b/106 Btu)	0.58	0.55	0.70	0.610
Emissions (lb/hour)	<i>₹</i> 515	698	1,417	2,630
•	* 2			
rbon Monoxide				
Emissions Basis	AP-42	AP-42	AP-42	
Emissions Basis (lb/10° Btu)	0.03	0.04	0.03	0.034
Emissions (lb/hour)	30	51	67	148
latile Organic Compounds		•		
Emissions Basis	Test Results <sup>d</sup>	AP-42	AP-42	
Emissions Basis (1b/10° Btu)	0.006	0.0014	0.0051	0.004
Emissions (lb/hour)	5.1	1.8	10.3	17
lfuric Acid Mist	Tost D14-	AD_42	A D _ 1. 2	
Emissions Basis Emissions Basis (1b/106 Btu)	Test Results 0.0072	AP-42 2.86E-05	AP-42 4.83E-02	0.0242
Emissions (lb/hour)	0.0072 6.4	0.0	4.83E-02 97.8	104
	0.4	0.0	37.0	204
otal Fluorides				
Emissions Basis	EPA (1981)		EPA (1981)	
Emissions Basis (lb/106 Btu)	6.29E-06	neg.	6.29E-06	4.25E-06
Emissions (lb/hour)	5.59E-03	0.00E+00	1.27E-02	1.83E-02
ercury	Took Decules	VDW (1002)	EDA (1000)	
Emissions Basis Emissions Basis (1b/106 Btu)	Test Results 2.10E-07	KBN (1992) 2.70E-08	EPA (1989) 3.20E-06	1.55E-06
Emissions Basis (1D/10° Btu) Emissions (1b/hour)	2.10E-07 1.86E-04	3.43E-05	6.48E-03	6.70E-03
	1.002 04	U. 10H 05	0,.00 00	3.702 00
ryllium				
Emissions Basis	Test Results		EPA (1989)	
Emissions Basis (1b/106 Btu)	6.15E-08	neg.	4.20E-06	1.98E-06
Emissions (lb/hour)	5.46E-05	0.00	8.51E-03	8.56E-03
rsenic				
rsenic Emissions Basis	Test Results		EPA (1989)	
Emissions Basis (1b/106 Btu)	2.45E-06	neg.	1.90E-05	9.42E-06
Emissions (lb/hour)	2.18E-03	0.00	3.85E-02	4.07E-02
,		-,		
ntimony				
Emissions Basis	Test Results		EPA (1981)	
Emissions Basis (lb/106 Btu)	2.62E-06	neg.	2.33E-05	1.15E-05
Emissions (lb/hour)	2.33E-03	0.00	4.72E-02	4.95E-02
- u.f				
rium Emissions Basis	Test Results		EPA (1981)	
Emissions Basis (1b/106 Btu)	4.17E-06	neo	6.71E-05	3.24E-05
Emissions Basis (15/10° Btu) Emissions (1b/hour)	3.70E-03	neg. 0.00	1.36E-01	1.40E-01
PHISSIONS (ID/NOUL)	3./UE-U3	0.00	1.305-01	1.406-01

Table A-4. Example Emission Calculations for Co-Firing of Orimulsion, Natural Gas and Residual Oil (Page 2 of 2)

				Residual	
	Dáta	Orimulsion	Natural Gas	Oil	Total
Cadmium					
Emissions	Basis	Test Results		EPA (1989)	
Emissions	Basis (lb/106 Btu)	5.69E-06	neg.	1.57E-05	8.54E-06
Emissions	(lb/hour)	5.05E-03	0.00	3.18E-02	3.68E-02
Chromium					
Emissions		Test Results		EPA (1989)	
	Basis (lb/106 Btu)	1.96E-05	neg.	2.10E-05	1.39E-05
Emissions	(lb/hour)	1.74E-02	0.00	4.25E-02	5.99E-02
Copper					
Emissions		Test Results		EPA (1989)	
	Basis (lb/106 Btu)	1.19E-05	neg.	`2.80E-04	1.34E-04
Emissions	(lb/hour)	1.06E-02	0.00	5.67E-01	5.78E-01
langanese	<b>.</b>	m		PDA (1000)	
Emissions		Test Results	. =	EPA (1989)	1 605 06
	Basis (lb/106 Btu)	2.01E-05	neg.	2.60E-05	1.63E-05
Emissions	(lb/hour)	1.78E-02	0.00	5.27E-02	7.05E-02
lickel				-D. (1000)	
Emissions		Test Results		EPA (1989)	1 0/7 00
	Basis (lb/106 Btu)	3.65E-03	neg.	1.26E-03	1.34E-03
Emissions	(lb/hour)	3.24	0.00	2.55	5.79E+00
Phosphorus	<b>.</b>			TD4 (1001)	
Emissions		Test Results		EPA (1981)	2 265 05
	Basis (lb/106 Btu)	3.05E-05	neg.	5.83E-05	3.36E-05
Emissions	(Lb/hour)	2.71E-02	0.00	1.18E-01	1.45E-01
Selenium	D	T D14		EDA (1001)	
Emissions	Basis (lb/106 Btu)	Test Results 1.26E-05		EPA (1981) 3.73E-05	2.01E-05
Emissions		1.12E-02	neg. 0.00	7.55E-02	8.67E-02
Silver					
Emissions	Basis	Test Results		EPA (1981)	
	Basis (lb/106 Btu)	3.06E-06	neg.	1.63E-05	8.29E-06
	(lb/hour)	2.72E-03	0.00	3.30E-02	3.57E-02
Vanadium					
Emissions	Basis	Test Results		EPA (1981)	
	Basis (lb/106 Btu)	1.45E-02	neg.	8.52E-03	6.98E-03
	(lb/hour)	1.29E+01	0.00	1.72E+01	3.01E+01
Zinc					
Emissions	Basis	Test Results		EPA (1981)	
Emissions	Basis (lb/106 Btu)	3.60E-05	neg.	6.71E-05	3.89E-05
Emissions	(lb/hour)	3.20E-02	0.00	1.36E-01	1.68E-01

Note: lb/hr is calculated based on the heat input for the fuel specified. "Test Results" refer to the stack tests performed by Entropy Environmentalists Inc., April 1-5 and 8-12, 1991.

<sup>\*</sup> The heat input based on 20% Orimulsion, 30% natural gas and 50% oil of full load. Orimulsion = 4,440 106 Btu/hr \* 0.20 = 888 106 Btu/hr
Natural Gas = 4,230 106 Btu/hr \* 0.30 = 1,269 106 Btu/hr
Residual Oil = 4,050 106 Btu/hr \* 0.5 = 2,025 106 Btu/hr

<sup>&</sup>lt;sup>6</sup> Based on a maximum emission rate when co-firing of 1.6 lb/10<sup>6</sup> Btu.

<sup>&</sup>lt;sup>c</sup> Based on a maximum emission rate when co-firing of 0.1 lb/10° Btu under steady state (21 hours) and less than 0.3 lb/10° Btu for soot blowing/load changes (3 hours); PM and PM10 are assumed to be the same.

d Maximum from Entropy stack tests.

If the maximum air quality impacts are below the NTL, the source is not considered to pose a health risk to the public. Maximum toxic element impacts of the FPL Sanford plant were determined using current regulatory-accepted air quality modeling techniques.

The appropriate model for predicting impacts for the Sanford plant is the Industrial Source Complex Short-Term (ISCST) model (EPA, 1990). The ISCST is approved by both EPA and FDER. The modeling was performed using a 5-year meteorological record of Orlando surface and Ruskin upper air data for the years 1982 to 1986.

A conservative modeling methodology was used initially to determine all total facility toxic pollutant impacts. First, the maximum impacts were determined for each Sanford unit separately using a generic emission rate. For the screening analysis, concentrations were predicted for each Sanford unit using a polar receptor grid with 10 ring distances of 900, 1200, 1600, 2000, 2500, 3000, 3500, 4000, 4500, and 5000 meters from the stack. The angular interval between adjacent receptors on the same ring was 10 degrees. Based on the screening modeling results, modeling refinements were made for the highest annual, 8-hour, and 24-hour predicted concentrations from each unit. The refined grid included downwind receptors every 200 m for the annual average and every 100 m for the 8-hour and 24-hour averaging times. The refined grid angular interval was 2 degrees.

The maximum concentrations for each toxic element were determined by multiplying the applicable generic maximum concentrations times each unit's toxic pollutant emission rate for each applicable averaging time and dividing by the generic emission rate. The maximum concentrations for each unit were then summed, regardless of their receptor location (thereby making the analysis conservative). The resulting summed concentrations were then compared to the NTL for each applicable averaging time. Some elements, such as nickel, have multiple NTLs for different forms. If the form of the element emitted did not have an NTL or if the NTL was not

known, a conservative NTL was chosen from the other available element forms (assuming the form selected could be reasonably emitted).

For most pollutants examined, the above procedure predicted maximum impacts significantly below the NTLs. The results for nickel, however, suggested that further modeling refinements be performed. For this element, a multisource ISCST modeling analysis was performed, inputting each source's actual nickel element emission rate into the ISCST model. The screening and refinement modeling analyses were then conducted as before. The maximum obtained annual, 8-hour, and 24-hour concentrations were then compared directly to NTLs.

The maximum toxic element concentrations for the annual, 8-hour, and 24-hour averaging times are presented in Table A-5. The results of the modeling analysis indicate that all predicted element concentration levels are below their respective NTLs except for the maximum annual impact predicted for nickel. It should be recognized that the maximum annual impacts were determined by assuming each unit operates at 100 percent capacity factor and maximum emissions. This assumption is extremely conservative in that capacity factors for FPL's fossil steam units rarely exceed 70 percent. Therefore, it is expected that the annual impact of nickel emissions would be less than the NTL. Based on this analysis, toxic emissions from the Sanford plant as a result of co-firing an amount of Orimulsion with natural gas which meets the proposed emission limits are not considered to pose a health risk to the public.

### 7.0 SUMMARY

From an evaluation of the proposed co-firing of Orimulsion, natural gas, and residual oil in Sanford Unit 4, it can be concluded that: 1) emissions will be less than or equal to the applicable emission limits, 2) the maximum predicted impacts will be less than the federal and state ambient air quality standards and Prevention of Significant Deterioration (PSD) increments, 3) emissions are not considered to pose a health risk to the public, and 4) neither the new source performance standards (NSPS) nor the

Table A-5. FPL Sanford Maximum Predicted Trace Element Impacts<sup>a</sup> - Units 3 & 5 on Residual Oil and Unit 4 Co-Firing Orimulsion and Natural Gas (Page 1 of 2)

Pollutant	Faci Emiss		Total Facility issions <u>Concentration(µg/m</u> (lb/hr) 8-Hr 24-Hr Ar			
Total Fluorides	ALL UNITS	0.0471	0.0016	0.0007	0.00003 NA	
	NTL/Impact		15707	9001	NA	
Mercury	ALL UNITS NTL NTL/Impact	0.0187	0.0007 0.5 686	0.0003 0.12 384	0.00001 0.3 22623	
Beryllium	ALL UNITS	0.0240	0.0009	0.0004 0.0048	0.00002	
	NTL/Impact		21	12	24	
Arsenic	ALL UNITS NTL NTL/Impact	0.1126	0.0043 2 461	0.0019 0.48 259	0.0001 0.00023 3	
Antimony	ALL UNITS NTL NTL/Impact	0.1375	0.0053 5 941	0.0023 0.12 53	0.0001 0.3 3107	
Barium	ALL UNITS NTL NTL/Impact	0.3902	0.0152 5 329	0.0065 1.2 184	0.0003 50 180429	
Cadmium	ALL UNITS NTL NTL/Impact	0.0996	0.0037 0.5 136	0.0016 0.12 76	0.0001 0.00056 8	
Chromium (metal)	ALL UNITS NTL NTL/Impact	0.1546	0.0053 5 949	0.0022 1.2 543	0.0001 1000 10 <sup>6</sup>	
Copper	ALL UNITS NTL NTL/Impact	1.6115	0.0631 1 16	0.0271 0.24 9	0.0011 NA NA	
Manganese	ALL UNITS NTL, NTL/Impact	0.1905	0.0067 50 7499	0.0028 12 4271	0.0001 NA NA	
Nickel <sup>b</sup>	ALL UNITS NTL NTL/Impact	13.6577	0.24 0.5 2.1	0.08 0.12 1.5	0.0046 0.0042 0.9	

Table A-5. FPL Sanford Maximum Predicted Trace Element Impacts<sup>a</sup> - Units 3 & 5 on Residual Oil and Unit 4 Co-Firing Orimulsion and Natural Gas (Page 2 of 2)

		Total Facility Emissions	Conc	entration(	μg/m)
Pollutant		(1b/hr)	8-Hr	24-Hr	Annual
Phosphorus	ALL UNITS	0.3920	0.0142	0.0060 0.24	0.0003 NA
	NTL/Impact		71	40	NA
Selenium	ALL UNITS NTL NTL/Impact	0.2351	0.0087 2 230	0.0037 0.48 130	0.0002 NA NA
Silver	ALL UNITS NTL NTL/Impact	0.1039	0.0040 0.1 25	0.0017 0.024 14	0.0001 3 41687
Thallium	ALL UNITS NTL NTL/Impact	0.0563	0.0022 1 450	0.0010 0.24 252	0.00004 0.5 12330
Vanadium Pentoxide <sup>o</sup>	ALL UNITS NTL NTL/Impact	8.6763	0.2729 0.5 1.8	0.1128 0.12 1.1	0.0047 20 4270
Zinc (oxide)	ALL UNITS NTL NTL/Impact	0.4440	0.0160 50 3126	0.0068 12 1772	0.0003 NA NA

Note: NTL = No-threat level.

<sup>&</sup>lt;sup>a</sup> Maximum concentrations for each averaging time = Unit 3 Only Maximum + Unit 4 Only Maximum + Unit 5 Only Maximum.

b Maximum impacts determined from refined ISCST modeling of all three units.

<sup>&</sup>lt;sup>c</sup> The vanadium pentoxide emission rate, based on worst-case estimate from Entropy tests, was  $1.72 \times 10^{-3}$  lb/ $10^6$  Btu. The same emission factor was also used for residual oil firing. Using this factor for residual oil would produce conservative results since the concentration of vanadium in Orimulsion is generally higher than in residual oil being burned at the Sanford Plant.

PSD requirements are applicable to the proposed co-firing of Orimulsion, natural gas, and residual oil.

1

### **ATTACHMENT B**

### **EMISSION FACTORS**

United States Environmental Protection Agency Office of Air Quality
Planning And Standards
Research Triangle Park, NC 27711

EPA-450/2-89-001 April 1989

AIR



# ESTIMATING AIR TOXICS EMISSIONS FROM COAL AND OIL COMBUSTION SOURCES

REPRODUCED BY
U.S. DEPARTMENT OF COMMERCE
NATIONAL TECHNICAL
INFORMATION SERVICE
SPRINGFIELD, VA 22161

TABLE 4-1. SUMMARY OF TOXIC POLLUTANT EMISSION FACTORS FOR OIL COMBUSTION<sup>a</sup>

	Emission Factor (1b/10 12 Btu)				
Pollutant	Residual Oil	Distillate Oil			
Arsenic	19	4.2			
Beryllium	4.2	2.5			
Cadmium	15.7	10.5			
Chromium	21	48			
Copper	280	280			
Lead	28 <sup>c</sup>	8.9 <sup>d</sup>			
Mercury	3.2	3.0			
Manganese	26	14			
Nickel	1260	170			
POM	8.4 <sup>b</sup>	22.5			
Formaldehyde	405 <sup>e</sup>	405 <sup>e</sup>			
		• •			

<sup>&</sup>lt;sup>a</sup>All emission factors are uncontrolled, and are applicable to oil-fired boilers and furnaces in all combustion sectors unless otherwise noted.

This value was calculated using all available residual oil data given in Table 4-35. If the upper end of the range of available data is excluded when calculating an average value (which could be used in this table), the average factor for POM from residual oil combustion becomes 4.1 lb/10<sup>12</sup> BTU.

<sup>&</sup>lt;sup>C</sup>Applicable to utility boilers only.

d Applicable to industrial, commercial, and residential boilers.

<sup>&</sup>lt;sup>e</sup>The formaldehyde factors are based on very limited and relatively old data. Consult Table 4-37 and accompanying discussion for more detailed information.

PB81-145195

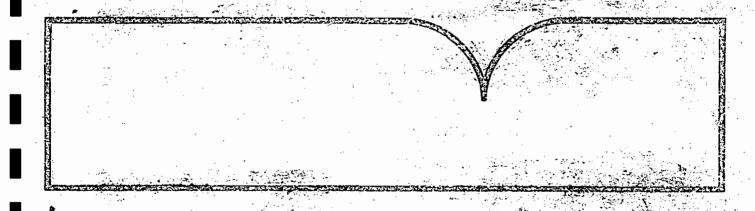
Emissions Assessment of Conventional Stationary Systems: Volume III. External Combustion Sources For Electricity Generations

TRW Environmental Engineering Div. Redondo Beach, CA

Prepared for

Industrial Anvironmental Research Lab

I and B



U.S. Department of Commerce National Technical Information Service

NIES.

TABLE 71. EMISSION FACTORS AND MEAN SOURCE SEVERITIES OF TRACE ELEMENT EMISSIONS FROM OIL-FIRED UTILITY BOILERS

	Concentration,	Emission	Mean Severit	
Trace Element	ppm	Factor,	Tangentially-	Wall-fired
		pg/J	fired Boilers	Boilers
Aluminum (Al)	3.8	87	0.0074	0.0027
Arsenic (As)	0.8	. 18	0.016	0.0059
Boron (B)	0.41	9.4	0.0013	0.0005
Barium (Ba)	1.26	28.8	0.025	0.0094
Beryllium (Be)	0.08	1.8	0.40	0.15
Bromine (Br)	0.13	3.0	0.0001	<0.0001
Calcium (Ca)	14	320	0.014	0.0052
Cadmium (Cd)	2.27	51.9	0.11	0.042
Chlorine (C1)	12	274	0.018	0.0066
Cobalt (Co)	2.21	50.5	0.22	0.082
Chromium (Cr)	1.3	- 30	0.026	0.0098
Copper (Cu)	2.8	64	0.14	0.052
Fluorine (F)	0.12	· 2.7	0.0005	0.0002
Iron (Fe)	18	411	0.023	0.0086
Mercury (Hg)	0.04	0.9	0.0079	0.0029
Potassium (K)	34	777	0.0064	0.0024
Lithium (Li)	0.06	1.4	0.028	0.010
Magnesium (Mg)	13	297	0.022	0.0081
Manganese (Mn)	1.33	30.4	0.0027	0.0010
Molybdenum (Mo)	0.9	21	0.0018	0.0007
Sodium (Na)	31	708	0.0059	0.0022
Nickel (Ni)	42.2	964	4.2	1.6
Phosphorus (P)	1.1	25	0.11	0.041
Lead (Pb)	3.5	80	0.23	0.087
Antimony (Sb)	0.44	10	0.0088	0.0033
Selenium (Se)	0.7	16	0.035	0.013
Silicon (Si)	17.5	400	0.018	0.0065
Tin (Sn)	6.2	142	0.031	0.012
Strontium (Sr)	0.15	3.4	0.0005	0.0002
Thorium (Th)	<0.001	<0.02	<0.0001	<0.0001
Uranium (U)	0,7	16	0.035	0.013
Vanadium (V)	160	3656	3.2	1.2
Zinc (Zn)	1.26	28.8	0.0032	0.0012

Air

SEPA

Health Impacts,
Emissions, and Emission
Factors for Noncriteria
Pollutants Subject to
De Minimis Guidelines and
Emitted from Stationary
Conventional Combustion
Processes

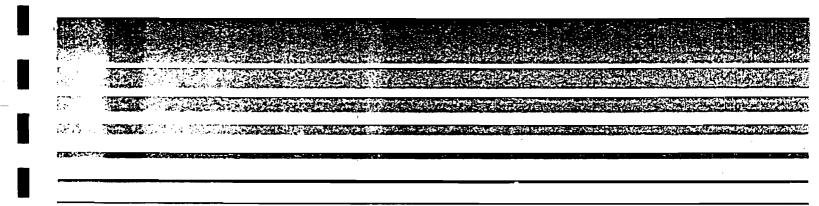


TABLE 4-3 TRACE ELEMENT EMISSION FACTORS FOR OIL-FIRED AND GAS-FIRED UTILITY AND INDUSTRIAL BOILERS

FURNACE TYPE	RESIDUAL OIL <sup>a</sup> pg/J				NATURAL GASb		
	Hg	Ве	F	•	Нд	Ве	F
UNCONTROLLED <sup>C</sup>			······				
Tangential firing	23C	24C	. 23C 🖎		4.9	N11	Nil
Wall firing	23C	24C	23C		4.9	Ni1	Nil

- (a) Emission factors for residual oil are calculated based on characterization of eleven residual oil samples and the assumption that all trace elements in the oil feed are emitted through the stack (Shih, et al, October 1979). C indicates the concentration of trace element in residual oil, in ppm.
- (b) Based on stack test measurements for gas-fired utility boilers (1.).
- (c) When boilers are equipped with wet scrubbers (used for flue gas desulfurization), the emission factor for Be may be assumed to be 0.01 times the uncontrolled factor given above, and emissions of Hg and F are .2 times the values given above (1.).

NOTE: To convert emission factor units to LB/10<sup>12</sup>BTU, multiply factors by 2.33.

## RECEIVED

MAY 1 4 1991

# ENTROPY

ENV. PERMITTING

POST OFFICE BOX 12291 RESEARCH TRIANGLE PARK NORTH CAROLINA 27709-2291 919-781-3550

STATIONARY SOURCE SAMPLING REPORT
REFERENCE NO. 8165A

FLORIDA POWER AND LIGHT COMPANY
SANFORD PLANT
SANFORD, FLORIDA

### EMISSIONS TESTING FOR:

Metals
Nitrogen Oxides
Particulate
Sulfur Dioxide
Sulfur Trioxide
Sulfuric Acid Mist
Total Hydrocarbons

UNIT NO. 4

APRIL 1 THROUGH 5 AND 8 THROUGH 12, 1991

TABLE 2-1

### EMISSION RATES SUMMARY, LB/MMBTU

Unit No. 4 Stack

		Repetition			
	1	2	3	<u>Averaqe</u>	
April 1, 1991					
Nitrogen Oxides	0.512	0.472	0.485	0.490	
Particulate	0.126	0.134	0.123	0.128	
Sulfur Dioxide	4.228	4.198	4.208	4.211	
Total Hydrocarbons	0.00336	0.00174	0.00120	0.00210	
April 2, 1991					
Nitrogen Oxides	0.516	0.513	0.496	0.508	
Particulate	0.137	0.138	0.126	0.134	
Sulfur Dioxide	4.208	4.190	4.224	4.207	
Total Hydrocarbons	0.00676	0.00596	0.00438	0.00570	
April 3, 1991					
Nitrogen Oxides	6 0.534	0.559	0.552	0.548	
Particulate	0.220	0.166	0.182	0.189	
Sulfur Dioxide	4.233	4.189	4.237	4.220	
Total Hydrocarbons	0.00272	0.00205	0.00259	0.00245	
April 4, 1991					
Nitrogen Oxides	0.542	0.599	0.588	0.576	
Particulate	0.156	0.169	0.169	0.165	
Sulfur Dioxide	4.202	4.146	4.199	4.182	
Total Hydrocarbons	0.00302	0.00286	0.00147	0.00245	
April 5, 1991					
Nitrogen Oxides	0.466	0.480	0.442	0.463	
Particulate	0.173	0.187	0.127	0.162	
Sulfur Dioxide	4.170	4.155	4.232	4.186	
Total Hydrocarbons	0.00210	0.00185	0.00168	0.00187	
<u>April 8, 1991</u>					
Metals					
Antimony	3.62E-006	1.72E-006	2.52E-006	2.62E-006	
Arsenic	2.62E-006	2.33E-006	2.39E-006	2.45E-006	
Barium	ND	1.25E-005	ND	4.17E-006	
Beryllium	7.50E-008	6.43E-008	4.51E-008	6.15E-008	
Cadmium	5.09E-006	5.64E-006	6.35E-006	5.69E-006	

Note: Compliance limits are 0.3 lb/MMBtu and 4.3 lb/MMBtu, for particulate and sulfur dioxide, respectively.

(continued next page)



### TABLE 2-1 (continued)

### EMISSION RATES SUMMARY, LB/MMBTU

### Unit No. 4 Stack

		- Repetition		
	1	2	3	<u>Average</u>
April 8, 1991				
Metals				
Chromium	2.22E-005	2.01E-005	1.65E-005	1.96E-005
Copper	1.46E-005	1.16E-005	9.53E-006	1.19E-005
Lead	ND	ND	ND	ND
Manganese	2.10E-005	1.76E-005	2.16E-005	2.01E-005
Mercury	2.00E-007	2.48E-007	1.81E-007	2.10E-007
Nickel	0.00394	0.00353	0.00349	0.00365
Phosphorous	3.40E-005	3.10E-005	2.65E-005	3.05E-005
Selenium	1.56E-005	1.16E-005	1.07E-005	1.26E-005
Silver	5.09E-006	4.08E-006	ND	3.06E-006
Thallium	ND	ND	ND	ND
Vanadium	0.0155	0.0141	0.0140	0.0145
Zinc	4.00E-005	2.98E-005	3.81E-005	3.60E-005
Nitrogen Oxides	0.534	0.556	0.571	0.554
Particulate	0.199	0.155	0.153	0.169
Sulfur Dioxide	4.282	4.214	4.187	4.228
Total Hydrocarbons	0.000897	0.00146	0.000677	0.00101
April 9, 1991				
Nitrogen Oxides	0.466	0.477	0.484	0.476
Particulate	0.195	0.186	0.263	0.215
Sulfur Dioxide	4.159	4.159	4.135	4.151
Total Hydrocarbons	0.00133	0.00151	0.00129	0.00137
April 10, 1991				
Nitrogen Oxides	0.548	0.437	0.549	0.511
Particulate	0.154	0.161	0.147	0.154
Sulfur Dioxide	4.216	4.233	4.206	4.218
Sulfuric Acid Mist (including SO3)	0.00395	0.0101	0.00753	0.00719
Total Hydrocarbons	0.000423	0.000339	0.000678	0.000480

Note: Compliance limits are 0.3 lb/MMBtu and 4.3 lb/MMBtu, for particulate and sulfur dioxide, respectively.



### TABLE 2-1 (continued)

### EMISSION RATES SUMMARY, LB/MMBTU

Unit No. 4 Stack

		Repetition		
	1	2	3	<u>Average</u>
April 11, 1991				
Nitrogen Oxides	0.437	0.510	0.509	0.485
Particulate	0.189	0.234	0.210	0.211
Sulfur Dioxide	4.196	4.147	4.155	4.166
Total Hydrocarbons	0.000754	0.00115	0.00111	0.00101
April 12, 1991				
Nitrogen Oxides	0.485	0.520	0.518	0.508
Particulate	0.180	0.179	0.174	0.178
Sulfur Dioxide	4.166	4.133	4.154	4.151
Total Hydrocarbons	0.000043	0.000474	0.000517	0.000345

Note: Compliance limits are 0.3 lb/MMBtu and 4.3 lb/MMBtu, for particulate and sulfur dioxide, respectively.