

HILLSBOROUGH COUNTY ENVIRONMENTAL PROTECTION COMMISSION
ANNUAL OPERATING REPORT

Representing Calendar Year 1984
Date Submitted: March 8, 1985

SECTION I - GENERAL INFORMATION

Plant, Institution or Establishment Name: Tampa Electric Company (F.J. Gannon Station)
Plant Address: P.O. Box 111 Tampa Florida 33601
Street City State Zip
Telephone: (813) 228-4838

Person to Contact Regarding This Report A. Spencer Autry Title Manager, Environmental Planning
Mailing Address: P.O. Box 111 Tampa Florida 33601
Street City State Zip

Actual Operating Hours: 24 hrs/day 7 days/wk 52 wks/yr

SECTION II - FUEL COMBUSTION FOR GENERATION OF HEAT OR STEAM

Source Code	Type of Fuel a	Quantity c X 1,000	Annual Consumption b				Hourly Consumption		Heat Content BTU/Quan	Percent Sulfur d	Percent Ash d
			Percent Distribution by Season				Maximum	Average			
			Spring March/ May	Summer June/ Aug	Fall Sept/ Nov	Winter Dec/ Feb					
Gan 1	No. 6 Oil	10,602	18.98	35.57	24.60	20.85	8,044	4,354	149,319	0.95	NA
Gan 2	No. 6 Oil	12,392	22.64	26.49	30.95	19.92	8,044	4,626	149,319	0.95	NA
Gan 3	No. 6 Oil Bitum Coal	7,627/ 154	6.85	28.26	42.12	22.77	10,846 65	6,997/ 43.5	149,319 12,596	0.95 1.18	NA 7.85
Gan 4	Bitum. Coal	371	26.87	20.50	29.26	23.37	80	52.1	12,361	2.09	8.04

a. Coke, bituminous, anthracite, or lignite coal No. 1, 2, 3, 4, 5, or 6 Fuel Oil, Nat. Gas, LPG; Refinery or Coke Oven Gas Etc. Indicate if two or more fuels are burned in the same boiler and provide all data pertinent to each fuel type.

b. Fuel Data Reported on 'as burned' Basis

c. Solid Fuel: Tons, Liquid Fuel: Gals.: Gaseous Fuel: 1000 ft³

d. If unknown, please give name and address of fuel supplier.

SECTION III - AIR CLEANING EQUIPMENT

Source Code	Type of Air Cleaning Equipment a,b	Pollutant Removed c	Inlet Gas Temp °F	Inlet Gas Flow Rate ACFM	Maximum Pressure Drop PSI d	Efficiency e	
						Design Percent	Operating Percent
Gan 1	Not Applicable						
Gan 2	Not Applicable						
Gan 3	Electrostatic Precipitator	Particulate	250+55	574,000	1.60	99.07	99.25
Gan 4	Electrostatic Precipitator	Particulate	330	700,000	1.58	99.05	99.81

Wet scrubber, electrostatic precipitator, fabric filter, etc.

Please list future equipment separately

- c. Pollutants to be covered in this survey are specified in the accompanying instructions.
- d. Give maximum normal operating pressure drop across air cleaning system.
- e. Give efficiency in terms of pollutant removed.

SECTION IV - STACK AND POLLUTANT EMISSIONS DATA

Stack Data					Estimate of Pollutant Emissions				
Source Code	Height Above Grade Ft.	Inside Diameter at top ft	Exit Gas Velocity ft/sec	Exit Gas Temp °F	Pollutant	Technique	Quantity tons/yr	Average lb/hr	Maximum lb/hr
Gan 1	306	10.0	47.53	309	Particulate	Stack Test	23.7	19.5	37.7
					Sulf.Dioxide	Fuel Anal.	823.2	676.1	1,307.3
Gan 2	306	10.0	50.49	309	Particulate	Stack Test	37.0	27.6	50.3
					Sulf.Dioxide	Fuel Anal.	962.2	718.3	1,307.3
Gan 3	306	10.6	59.18	266	Particulate	Stack Test	73.0	30.6	95.9
					Sulf.Dioxide	Fuel Anal.	4,063.2	1,774.2	2,862.2
Gan 4	2 Stacks 306(ea)	9.6(ea)	43.48(ea)	286	Particulate	Stack Test	45.9	12.9	18.8
					Sulf.Dioxide	Fuel Anal.	8,401.9	2,357.0	3,433.1

HILLSBOROUGH COUNTY ENVIRONMENTAL PROTECTION COMMISSION
AIR POLLUTANT EMISSION REPORT

Representing Calendar Year 1984
Date submitted: March 1, 1985

SECTION I - GENERAL INFORMATION

Plant, institution, or establishment name Tampa Electric Company (Big Bend Station)
 Plant, institution, or establishment address: P.O. Box 111 Tampa Florida 33601
 (Street or Box Number) (City) (State) (Zip)
 Person to contact regarding this report: A. Spencer Autry Title Environmental Planning Telephone: 228-4838
 Mailing address: P.O. Box 111 Tampa Florida 33601
 (Street or Box Number) (City) (State) (Zip)

NOT APPLICABLE

SECTION II - PROCESS/OPERATIONS EMISSIONS

Normal operating schedule: Hours per day Days per week Weeks per year Hours per year.
 Seasonal and/or peak operation period:
 Dates of annually occurring shutdowns of operations: Additional operating info. enclosed

Source Code	Processes or Operations Releasing Pollutants to the Atmosphere	Raw Materials Used for Processes or Operations			Products of Processes or Operations			Intermittent Operation Only Average Hours/Week	
		Type	Quantity		Type	Quantity			
			Hourly Process Rate, lbs.			Hourly Process Rate, lbs.			
		Annual Average	Design	Maximum		Annual Average	Design	Maximum	

- List a separate code number to represent each source (e.g., IV-a, IV-b, IV-c, etc.) then enter required data on this page and for the same code number sources in Section III, IV, and V.
- Multiple sources may be grouped if similar in size and type.
- Sulfuric acid-contact; aluminum smelting-crucible furnace; cement manufacturing-dry process; etc (See instruction for examples and use approximate identification numbers); other non-listed processes and operations (specify).
- The pollutants to be covered in this report are listed in the accompanying instructions.
- Sulfur burned; pig, foundry returns, or scrap aluminum melted; limestone, cement rock, clay, iron ore used; etc.
- Pounds, tons, gallons, barrels, etc.
- Sulfuric acid produced; aluminum ingots produced; etc.
- For intermittent processes, indicate average number of hours per week of operation so that estimates of yearly emissions may be obtained.

BEST AVAILABLE COPY

GANNON STATION

1974

GANNON 1-4 FLYASH SILO

$$\text{EMISSION} = (1.32 \text{ lb/hr}) \left(\frac{8021 \text{ hrs OP.}}{\text{YR}} \right) \left(\frac{1 \text{ Ton}}{2000 \text{ lbs}} \right) = 5.29 \text{ TONS/YR}$$

GANNON 5+6 FLYASH SILO

$$\text{EMISSION} = (\overset{\text{DESIGN}}{2.07} \text{ lb/hr}) \left(\frac{8227 \text{ hrs OP.}}{\text{YR}} \right) \left(\frac{1 \text{ Ton}}{2000 \text{ lbs}} \right) = 8.58 \text{ TONS/YR}$$

GANNON 4 ELONDERIZER POW SILO

$$\text{EMISSION} = (\overset{\text{DESIGN}}{0.14} \text{ lb/hr}) \left(\frac{7133 \text{ hrs OP.}}{\text{YR}} \right) \left(\frac{1 \text{ Ton}}{2000 \text{ lbs}} \right) = 0.50 \text{ TONS/YR}$$

BEST AVAILABLE COPY

GANNON STATION

GAS TURBINE
FUEL CONSUMED

1984

TOTAL CONSUMPTION = 3174.11 BBL = 133,313 GALS.
TOTAL GENERATED = 885,000 KWH

AVG % Sulfur = 0.37
AVG Btu/lb = 19,468
AVG Density (lb/gal) = 7.121

AVG Hourly Consumption = $\frac{133,313 \text{ gal oil } 1984}{120 \text{ hrs. operation}} = 1111 \frac{\text{gal}}{\text{hr}}$

$V = (133,313 \text{ gal}) (7.121 \frac{\text{lb}}{\text{gal}}) \left(\frac{1 \text{ yr}}{120 \text{ hrs. op.}} \right) \left(\frac{1}{3000000} \right) \left(\frac{229.5 \text{ gal}}{\text{lb oil}} \right) \left(\frac{14970 \text{ ft}^3}{492 \text{ ft}^3} \right) \left(\frac{1}{95.7 \text{ ft}^3} \right) = 16.40 \text{ fps}$

Flow (avg) = $(16.40 \text{ fps}) (95.7 \text{ ft}^3) (60 \frac{\text{sec}}{\text{min}}) = 94,169 \text{ cfm}$

SULFUR DIOXIDE (AVG)

$(133,313 \frac{\text{gal}}{\text{yr}}) (7.121 \frac{\text{lb}}{\text{gal}}) (0.0037 \frac{\text{TON S}}{\text{TON OIL}}) (1.9 \frac{\text{TON SO}_2}{\text{TON S}}) (\frac{1 \text{ TON}}{2000 \text{ lb}}) = 3.3 \frac{\text{TON}}{\text{YR}}$
 $(1111 \text{ gal/hr}) (7.121 \frac{\text{lb}}{\text{gal}}) (0.0037 \frac{\text{TON S}}{\text{TON OIL}}) (1.9) = 55.6 \frac{\text{lb}}{\text{hr}}$

SULFUR DIOXIDE (MAX)

$(1885 \text{ gal/hr}) (7.121 \frac{\text{lb}}{\text{gal}}) (0.0037 \frac{\text{TON S}}{\text{TON OIL}}) (1.9 \frac{\text{TON SO}_2}{\text{TON S}}) = 94.4 \frac{\text{lb}}{\text{hr}}$

PARTICULATE (AVG)

$(133,313 \frac{\text{gal}}{\text{yr}}) (7.121 \frac{\text{lb}}{\text{gal}}) (19468 \frac{\text{Btu}}{\text{lb}}) (\frac{0.1 \text{ lb}}{\text{MM Btu}}) (\frac{1 \text{ TON}}{2000 \text{ lbs}}) = 0.9211 \frac{\text{TON}}{\text{YR}}$
 $(1111 \text{ gal/hr}) (7.121 \frac{\text{lb}}{\text{gal}}) (19,468 \frac{\text{Btu}}{\text{lb}}) (\frac{0.1 \text{ lb}}{\text{MM Btu}}) = 15.4 \frac{\text{lb}}{\text{hr}}$

PARTICULATE (MAX)

$(1885 \frac{\text{gal}}{\text{hr}}) (7.121 \frac{\text{lb}}{\text{gal}}) (19468 \frac{\text{Btu}}{\text{lb}}) (\frac{0.1 \text{ lb}}{\text{MM Btu}}) = 26.1 \frac{\text{lb}}{\text{hr}}$

BIG RENDUNIT: 1YEAR: 1984

$$138 \frac{\text{TONS}}{\text{HR}} \times \frac{2,000 \text{ lbs.}}{\text{TON}} \times \frac{11,664 \text{ BTU}}{\text{lb.}} = 3219 \frac{\text{MMBTU}}{\text{HR.}} \quad (\text{AVG})$$

$$\text{DESIGN} = 4037 \frac{\text{MMBTU}}{\text{HR.}} \quad (\text{MAX})$$

$$972,138 \frac{\text{TONS}}{\text{YR.}} \times \frac{2,000 \text{ lbs.}}{\text{TON}} \times \frac{11,664 \text{ BTU}}{\text{lb.}} = 226,780,35 \frac{\text{MMBTU}}{1984} \quad (\text{ACTUAL})$$

PARTICULATE EMISSIONS

$$0.03 \frac{\text{lbs. PART.}}{\text{MM BTU}} \times 3219 \frac{\text{MMBTU}}{\text{HR.}} = 96.6 \frac{\text{lbs. PART.}}{\text{HR.}} \quad (\text{AVG})$$

$$0.03 \frac{\text{lbs. PART.}}{\text{MM BTU}} \times 4037 \frac{\text{MMBTU}}{\text{HR.}} = 121.1 \frac{\text{lbs. PART.}}{\text{HR.}} \quad (\text{MAX})$$

$$0.03 \frac{\text{lbs. PART.}}{\text{MM BTU}} \times \frac{22,678,035 \text{ MMBTU}}{1984} \times \frac{1 \text{ TON}}{2,000 \text{ lb.}} = 340.2 \frac{\text{TONS PART.}}{1984}$$

SULFUR DIOXIDE EMISSIONS

$$4.92 \frac{\text{lbs. SO}_2}{\text{MM BTU}} \times 3219 \frac{\text{MMBTU}}{\text{HR.}} = 15837 \frac{\text{lbs. SO}_2}{\text{HR.}} \quad (\text{AVG})$$

$$4.92 \frac{\text{lbs. SO}_2}{\text{MM BTU}} \times 4037 \frac{\text{MMBTU}}{\text{HR.}} = 19862 \frac{\text{lbs. SO}_2}{\text{HR.}} \quad (\text{MAX})$$

$$4.92 \frac{\text{lbs. SO}_2}{\text{MM BTU}} \times \frac{22,678,035 \text{ MMBTU}}{1984} \times \frac{1 \text{ TON}}{2,000 \text{ lb.}} = 55,788 \frac{\text{TONS SO}_2}{1984}$$

* lbs. SO₂ value of 4.92 is a weighted average for 1984.
MM BTU

D. E. R.

MAR 11 1965

SOUTH WEST DISTRICT
TAMPA

GANDOW STATION

UNIT: 1

YEAR 1984

$$\frac{4354 \text{ GAL}}{\text{HR}} \times \frac{149,319 \text{ BTU}}{\text{GAL}} = 650.1 \text{ MMBTU HR. (AVG)}$$

$$\text{DESIGN} = 1257 \text{ MMBTU (MAX) HR.}$$

$$\frac{10,602,401 \text{ GALLON}}{\text{YR}} \times \frac{149,319 \text{ BTU}}{\text{GAL}} = \frac{1,583,147 \text{ MMBTU}}{1984} \text{ (ACTUAL)}$$

PARTICULATE EMISSIONS

$$0.03 \frac{\text{lbs. PART.}}{\text{MM BTU}} \times 650.1 \frac{\text{MMBTU}}{\text{HR.}} = 19.5 \frac{\text{lbs. PART.}}{\text{HR.}} \text{ (AVG)}$$

$$0.03 \frac{\text{lbs. PART.}}{\text{MM BTU}} \times 1,257 \frac{\text{MMBTU}}{\text{HR.}} = 37.7 \frac{\text{lbs. PART.}}{\text{HR.}} \text{ (MAX)}$$

$$0.03 \frac{\text{lbs. PART.}}{\text{MM BTU}} \times \frac{1,583,147 \text{ MMBTU}}{1984} \times \frac{1 \text{ TON}}{2,000 \text{ lb}} = 23.7 \frac{\text{TONS PART.}}{1984}$$

SULFUR DIOXIDE EMISSIONS

$$1.04^* \frac{\text{lbs. SO}_2}{\text{MM BTU}} \times 650.1 \frac{\text{MMBTU}}{\text{HR.}} = 676.1 \frac{\text{lbs. SO}_2}{\text{HR.}} \text{ (AVG)}$$

$$1.04^* \frac{\text{lbs. SO}_2}{\text{MM BTU}} \times 1,257 \frac{\text{MMBTU}}{\text{HR.}} = 1,307.3 \frac{\text{lbs. SO}_2}{\text{HR.}} \text{ (MAX)}$$

$$1.04^* \frac{\text{lbs. SO}_2}{\text{MM BTU}} \times \frac{1,583,147 \text{ MMBTU}}{1984} \times \frac{1 \text{ TON}}{2,000 \text{ lb}} = 823.2 \frac{\text{TONS SO}_2}{1984}$$

* lbs. SO₂ value of 1.04 is a weighted average for 1984.
MMBTU

D. E. R.

MAR 11 1965

SOUTH WEST DISTRICT
TAMPA

SECTION III - FUEL COMBUSTION FOR GENERATION OF HEAT, STEAM, AND/OR POWER

Source Code	Type of Fuel	Annual Consumption				Hourly Consumption		Heat Content BTU/Quan.	Percent Sulfur	Percent Ash (Solid) Fuel Only..1	
		Quantity X 1,000	Percent Distribution by Season				Maximum				Average Quantity
			Spring March/ May	Summer June/ Aug.	Fall Sept./ Nov.	Winter Dec./ Febr					
GT 1	#2 Oil	107.1	12.48	21.95	12.78	52.78	1,885	1,231	19,449	0.35	NA
GT 2	#2 Oil	1,545.6	17.70	31.14	17.09	34.07	6,600	4,329	19,449	0.35	NA
GT 3	#2 Oil	917.0	29.75	18.77	1.48	50.00	6,600	4,246	19,449	0.35	NA

- List code numbers corresponding to each emissions source reported in Section II.
- Coke, bituminous coal, anthracite coal, lignite; No. 1, 2, 4, 5, and 6 fuel oil; natural gas; LPG; refinery or coke oven gas; etc. (Note: Indicate if two or more fuels are burned in the same boiler and provide all data pertinent to each fuel type).
- Fuel data are to be reported on an "as burned" basis.
- Solid fuel, tons; liquid fuel, gallons; gaseous fuel, 1000 cubic feet.
- If unknown, please give name and address of fuel supplier.

SECTION IV - AIR CLEANING EQUIPMENT

Source Code	Type of Air Cleaning Equipment	Pollutant Removed	Inlet Gas Temperature °F	Inlet Gas Flow Rate ACFM	Maximum Pressure Drop, PSI.	Efficiency	
						Design Percent	Operating Percent
GT 1	Not Applicable						
GT 2	Not Applicable						
GT 3	Not Applicable						

- Wet scrubber, electrostatic precipitator, fabric filter, etc.
- Please list future equipment separately.
- The pollutants to be covered in this survey are specified in the accompanying instructions.
- Give efficiency in terms of pollutant removed.
- Give maximum normal operating pressure drop across air cleaning system.

SECTION V - STACK AND POLLUTANT EMISSIONS DATA

STACK DATA					ESTIMATE OF POLLUTANT EMISSIONS				
Source Code	Height Above Grade ft.	Inside Diameter at Top ft.	Exit Gas Velocity ft./sec.	Exit Gas Temperature °F.	Pollutant	Technique	Quantity tons/yr.	Average lb/hr.	Maximum lb/hr.
BB1	490	24	72.8	269	Particulate Sulf. Dioxide	Stack Test Fuel Anal.	340 55,788	97 15,837	121 19,862
BB2	Common	Stack with	Unit 1		Particulate Sulf. Dioxide	Stack Test Fuel Anal.	364 58,650	97 15,711	120 19,341
BB3	490	24	40.0	279	Particulate Sulf. Dioxide	Stack Test Fuel Anal.	685 43,013	182 11,470	206 12,921

- a. List code numbers corresponding to each emissions source reported in Section II, III, and IV.
- b. Values should be representative of average flow conditions for hours of operation.
- c. At actual flow conditions.
- d. The pollutants to be covered in this survey are specified in the accompanying instructions.
- e. Give stack test data if available (indicate stack sampling method used), otherwise, specify basis used. If unknown, please do not complete these columns.
- f. Note technique used to arrive at estimation; AP-42, stack test, etc.

SECTION V - STACK AND POLLUTANT EMISSIONS DATA

STACK DATA					ESTIMATE OF POLLUTANT EMISSIONS				
Source Code	Height Above Grade ft.	Inside Diameter at Top ft.	Exit Gas Velocity ft./sec.	Exit Gas Temperature °F.	Pollutant	Technique	Quantity tons/yr.	Average lb/hr.	Maximum lb/hr.
GT 1	35	95.7(1)	18.2	1,010	Particulate	Fuel Anal.	0.74	17.0	26.1
					Sulf. Dioxide	Fuel Anal.	2.5	30.6	94.2
GT 2	75	215.6(1)	26.8	928	Particulate	Fuel Anal.	10.7	59.8	91.3
					Sulf. Dioxide	Fuel Anal.	36.5	107.7	329.8
GT 3	75	215.6(1)	26.3	928	Particulate	Fuel Anal.	6.3	58.7	91.3
					Sulf. Dioxide	Fuel Anal.	21.7	105.6	329.8

- a. List code numbers corresponding to each emissions source reported in Section II, III, and IV.
- b. Values should be representative of average flow conditions for hours of operation.
- c. At actual flow conditions.
- d. The pollutants to be covered in this survey are specified in the accompanying instructions.
- e. Give stack test data if available (indicate stack sampling method used), otherwise, specify basis used. If unknown, please do not complete these columns.
- f. Note technique used to arrive at estimation; AP-42, stack test, etc.

(1) Exit Area (ft²)

SECTION V - STACK AND POLLUTANT EMISSIONS DATA

STACK DATA					ESTIMATE OF POLLUTANT EMISSIONS				
Source Code	Height Above Grade ft.	Inside Diameter at Top ft.	Exit Gas Velocity ft./sec.	Exit Gas Temperature °F.	Pollutant	Technique	Quantity tons/yr.	Average lb/hr.	Maximum lb/hr.
1 & 2 Flyash Silo	102	5.0(1)	51.7	250	Particulate	Calculated	12.9	2.95	2.95
Unit 3 Flyash Silo	112.5	2.0(1)	129.6	250	Particulate	Calculated	11.0	2.95	2.95

- a. List code numbers corresponding to each emissions source reported in Section II, III, and IV.
- b. Values should be representative of average flow conditions for hours of operation.
- c. At actual flow conditions.
- d. The pollutants to be covered in this survey are specified in the accompanying instructions.
- e. Give stack test data if available (indicate stack sampling method used), otherwise, specify basis used. If unknown, please do not complete these columns.
- f. Note technique used to arrive at estimation; AP-42, stack test, etc.

(1) Exit Area (ft²)

GANNON STATION

UNIT: 1

YEAR 1984

$$\frac{4354 \text{ GAL}}{\text{HR}} \times \frac{149,319 \text{ BTU}}{\text{GAL}} = \frac{650.1 \text{ MMBTU}}{\text{HR}} \quad (\text{AVG})$$

$$\text{DESIGN} = \frac{1257 \text{ MMBTU}}{\text{HR}} \quad (\text{MAX})$$

$$\frac{10,602,416 \text{ GAL OIL}}{\text{YR}} \times \frac{149,319 \text{ BTU}}{\text{GAL}} = \frac{1,583,147 \text{ MMBTU}}{1984} \quad (\text{ACTUAL})$$

PARTICULATE EMISSIONS

$$\frac{0.03 \text{ lbs. PART.}}{\text{MM BTU}} \times \frac{650.1 \text{ MMBTU}}{\text{HR}} = \frac{19.5 \text{ lbs. PART.}}{\text{HR}} \quad (\text{AVG})$$

$$\frac{0.03 \text{ lbs. PART.}}{\text{MM BTU}} \times \frac{1257 \text{ MMBTU}}{\text{HR}} = \frac{37.7 \text{ lbs. PART.}}{\text{HR}} \quad (\text{MAX})$$

$$\frac{0.03 \text{ lbs. PART.}}{\text{MM BTU}} \times \frac{1,583,147 \text{ MMBTU}}{1984} \times \frac{1 \text{ TON}}{2,000 \text{ lb}} = \frac{23.7 \text{ TONS PART.}}{1984}$$

SULFUR DIOXIDE EMISSIONS

$$\frac{1.04^* \text{ lbs. SO}_2}{\text{MM BTU}} \times \frac{650.1 \text{ MMBTU}}{\text{HR}} = \frac{676.1 \text{ lbs. SO}_2}{\text{HR}} \quad (\text{AVG})$$

$$\frac{1.04^* \text{ lbs. SO}_2}{\text{MM BTU}} \times \frac{1257 \text{ MMBTU}}{\text{HR}} = \frac{1307.3 \text{ lbs. SO}_2}{\text{HR}} \quad (\text{MAX})$$

$$\frac{1.04^* \text{ lbs. SO}_2}{\text{MM BTU}} \times \frac{1,583,147 \text{ MMBTU}}{1984} \times \frac{1 \text{ TON}}{2,000 \text{ lb}} = \frac{823.2 \text{ TONS SO}_2}{1984}$$

* lbs. SO₂ / MM BTU value of 1.04 is a weighted average for 1984.

HILLSBOROUGH COUNTY ENVIRONMENTAL PROTECTION COMMISSION
ANNUAL OPERATING REPORT

(Corrected Copy)

Representing Calendar Year 1984
Date Submitted: March 8, 1985

SECTION I - GENERAL INFORMATION

Plant, Institution or Establishment Name: Tampa Electric Company (F.J. Gannon Station)
Plant Address: P.O. Box 111 Tampa Florida 33601
Street City State Zip
Telephone: (813) 228-4838

Person to Contact Regarding This Report A. Spencer Autry Title Manager, Environmental Planner
Mailing Address: P.O. Box 111 Tampa Florida 33601
Street City State Zip

Actual Operating Hours: 24 hrs/day 7 days/wk 52 wks/yr

SECTION II - FUEL COMBUSTION FOR GENERATION OF HEAT OR STEAM

Source Code	Type of Fuel a	Quantity c X 1,000	Annual Consumption b				Hourly Consumption		Heat Content BTU/Quan	Percent Sulfur d	Percent Ash d
			Percent Distribution by Season				Maximum	Average			
			Spring March/ May	Summer June/ Aug	Fall Sept/ Nov	Winter Dec/ Feb					
Gan 1	No. 6 Oil	10,602	18.98	35.57	24.60	20.85	8,044	4,354	149,319	0.95	NA
Gan 2	No. 6 Oil	12,392	22.64	26.49	30.95	19.92	8,044	4,626	149,319	0.95	NA
Gan 3	No. 6 Oil Bitum. Coal	7,627/ 154	6.85	28.26	42.12	22.77	10,846 65	6,997/ 43.5	149,319 12,596	0.95 1.18	NA 7.85
Gan 4	Bitum. Coal	371	26.87	20.50	29.26	23.37	80	52.1	12,361	1.19	8.04

- Coke, bituminous, anthracite, or lignite coal No. 1, 2, 3, 4, 5, or 6 Fuel Oil, Nat. Gas, LPG; Refinery or Coke Oven Gas Etc. Indicate if two or more fuels are burned in the same boiler and provide all data pertinent to each fuel type.
- Fuel Data Reported on 'as burned' Basis
- Solid Fuel: Tons, Liquid Fuel: Gals.: Gaseous Fuel: 1000 ft³
- If unknown, please give name and address of fuel supplier.