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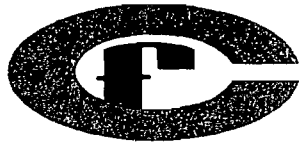
JAN 21 2000

BUREAU OF AIR REGULATION

CF Industries, Inc. (CFII)  
Plant City Phosphate Complex  
Title V Permit No. 0570005-007-AV  
Construction Permit Application  
A & B Phosphoric Acid Units  
Attachment 1

Compliance tests  
(Not actual Application)

P.O. Drawer L.  
Plant City, Florida 33564-9007  
Telephone: 813/782-1591



**CF Industries, Inc.**  
Plant City Phosphate Complex

July 2, 1999

Mr. Jerry Kissel  
Florida Department of  
Environmental Protection  
3804 Coconut Palm Drive  
Tampa, FL 33619-8318

SUBJECT: COMPLIANCE TEST - "A" PAP  
Permit No. 0570005-007-AV  
Emission Unit 004

Dear Mr. Kissel:

Enclosed are duplicate copies of the two recent compliance tests conducted at CF Industries, Inc., Plant City Phosphate Complex, on "A" Phosphoric Acid Plant. The tests were performed at the rates specified in FDEP's letter dated May 26, 1999, and otherwise in accordance with the conditions of Air Permit No. 0570005-007-AV. The approved elevated operating rates and the extra testing were in support of a permit application submitted to the FDEP on June 11, 1999.

If there are any questions concerning the results, please give Michael Messina a call at 813-782-1591, ext. 290.

Sincerely,

T.A. Edwards,  
Superintendent, Environmental Affairs

TAE/JHF/gm  
u:\envrpt\225960.doc  
Enclosures

cc: J.M. Messina  
T.V. Ortoski  
Sterlin Woodard/HCEPC

PERMIT NO. 0570005-007-AV

EMISSION UNIT 004

CF INDUSTRIES, INC.

PLANT CITY PHOSPHATE COMPLEX

"A" PHOSPHORIC ACID PRODUCTION

PLANT CITY, FLORIDA

June 22 & 23, 1999

TEST CONDUCTED BY:

Laboratory  
CF INDUSTRIES, INC.  
Plant City Phosphate Complex  
Plant City, Florida 33564

## INTRODUCTION:

The Environmental Control Laboratory of CF Industries, Inc., Plant City Phosphate Complex, conducted emission tests at "A" Phosphoric Acid Production Facility in Plant City, Florida on June 22 and 23, 1999. Six sixty minute (60) test runs were performed. The purpose of the tests was to obtain emission data demonstrating compliance with the State of Florida DEP performance standards at operating rates applied for in a permit application submitted on June 11, 1999. All results were within the permitted limits.

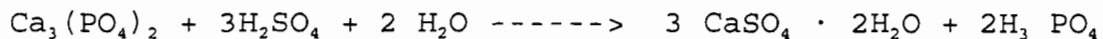
The measurements were made for fluoride, opacity and moisture at the stack outlet to the atmosphere.

Complete results are given in APPENDIX "A".

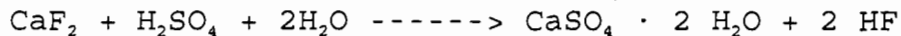
## PROCESS DESCRIPTION

Phosphoric Acid is made by reacting sulfuric acid with phosphate rock along with a given amount of water to make an acid slurry. The mixing of sulfuric acid, rock and water takes place in a continuous reactor.

The principal reaction takes place as follows:



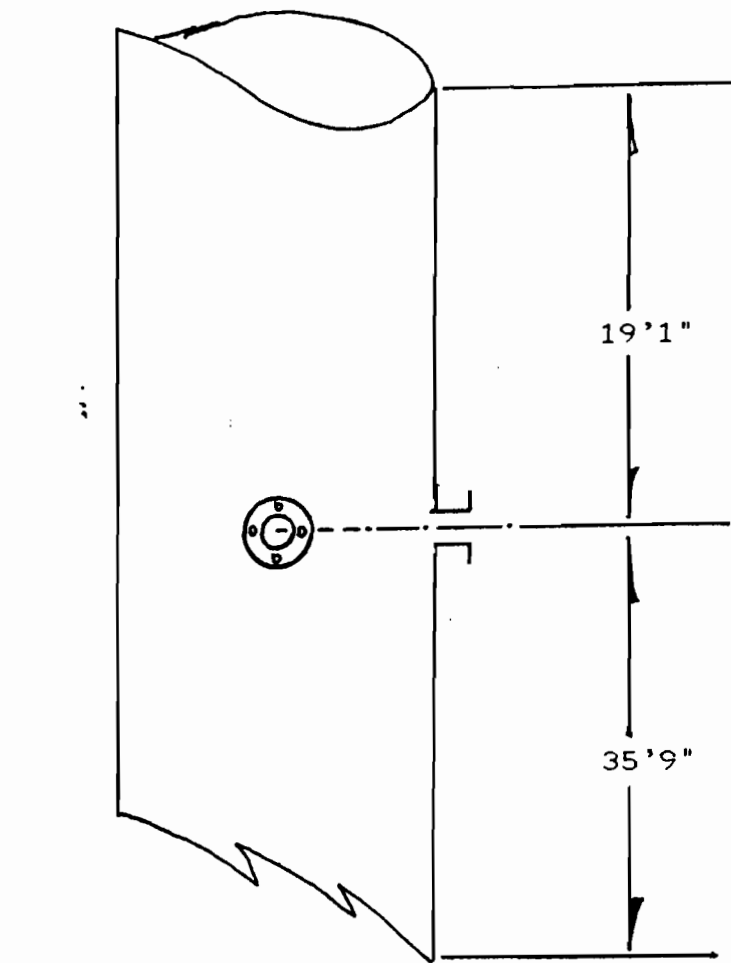
Other Reactions as follows:



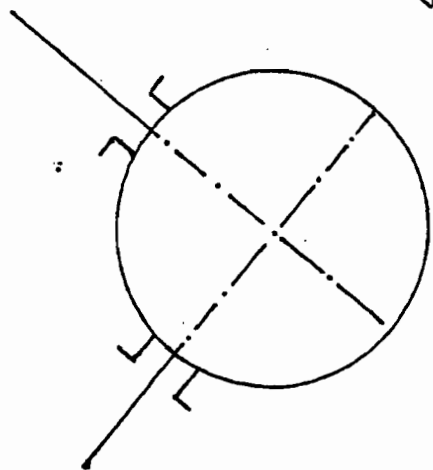
The resulting Phosphoric Acid will be 28 to 30%  $\text{P}_2\text{O}_5$  content. This 28 to 30%  $\text{P}_2\text{O}_5$  Phosphoric Acid solution will be further concentrated by evaporators until the acid strength reaches 52 to 54%  $\text{P}_2\text{O}_5$ .

## LOCATION OF SAMPLING POINTS

The sampling sites and number of traverse points were selected as per Figure 1-2 EPA Method 1 specified in 40 CFR 60, Appendix A.



Traverse Point Number	Distance from inside wall
1	1.56
2	4.92
3	8.76
4	13.56
5	20.52
6	39.48
7	46.44
8	51.24
9	55.08
10	58.44



60" I.D.

FIGURE 1

SAMPLE POINT DESCRIPTION

"A" PHOSPHORIC ACID STACK

## SAMPLING AND ANALYTICAL PROCEDURES

The methods described in EPA Methods 1, 2, 3, 4, 9 and 13B contained in 40 CFR 60, Appendix A and adopted by reference in Chapter 62-297.401 F.A.C. are used when testing during compliance by CF Industries, Inc.

APPENDIX "A"

EMISSION CALCULATIONS AND RESULTS



CF INDUSTRIES, INC.  
PLANT CITY PHOSPHATE COMPLEX

SOURCE SAMPLING NOMENCLATURE SHEET

Pb	= Barometric pressure, in Hg
Ps	= Stack pressure, in Hg
As	= Stack area, sq. ft.
As'	= Effective area of positive stack gas flow, sq. ft.
Ts	= Stack temperature 'R'
Tm	= Meter temperature "R"
$\Delta$ Pavg	= Average square root of velocity head in. H <sub>2</sub> O
Cp	= S-type pitot tube correction factor
Kp	= 85.48 ft/sec (lb mole - °R) <sup>1/2</sup>
Ms	= Molecular weight of gas at stack conditions
Md	= Molecular weight of gas at dry conditions
Bwo	= Proportion by volume of water vapor in gas stream
Vwstd	= Volume of water vapor in gas sample
V <sub>ic</sub>	= Total volume of liquid collected in impinger & silica jel
$\rho_{H_2O}$	= Density of water 1 gm/ml
MH <sub>2</sub> O	= Molecular weight of water 18 lb/lb mole
R	= Ideal gas constant, 28.83 in. Hg-cu ft/lb-mole °R
Tstd	= Absolute temp. at standard conditions, 528 °R
Pstd	= Absolute pressure at standard conditions, 29.92 in. Hg.
Vmstd	= Volume of gas sample through dry gas meter (standard condtions) cu. ft.
Vm	= Volume of gas sample through the dry gas meter (meter condition) cu. ft.
$\Delta H$	= Orifice pressure of sampling meter
S.T.P.	= Standard condition, dry, 528 °R, 29.92 in. Hg
An	= Sampling nozzle area, square feet
Vs	= Velocity of stack gas, feet per second
Qs	= Volumetric flow rate, dry basis, standard conditions, CFM
Cs	= Concentration of particulate matter in stack gas, gr/SCF
Cf	= Concentration of fluoride in stack gas gr/SCF
Mf	= Total amount of fluoride collected, mg.
Mn	= Total amount of particulate matter collected, mg
I	= Percent isokinetic volume sampled
O	= Sampling time

$$V_{wstd} = 0.04707 \text{ cuft/ml } (V_1)$$

$$V_{mstd} = V_m \left( \frac{T_{std}}{T_m} \right) \left( \frac{P_{bar} + \frac{\Delta H}{13.6}}{P_{std}} \right)$$

$$B_{wo} = \frac{V_{wstd}}{V_{wstd} + V_{mstd}}$$

$$M_s = M_d (1 - B_{wo}) + 18 (B_{wo})$$

$$V_s(\text{avg}) = K_p C_p \sqrt{P(\text{avg})} \sqrt{\frac{460 + T_s}{M_s P_s}}$$

$$Q_s = 60 (1 - B_{wo}) V_s A_s \left( \frac{T_{std}}{T_s} \right) \left( \frac{P_s}{P_{std}} \right)$$

PERCENT ISOKINETIC

$$I = \frac{T_s (1.667) \left[ (0.00267) V_1 + \left( \frac{T_{std}}{T_m} \right) P_{bar} + \frac{\Delta H}{13.6} \right]}{\theta V_s P_s A_n}$$

$$C_s = 0.0154 \text{ grs/mg} \frac{M_f \text{ or } M_n}{V_{mstd}}$$

$$\text{lbs/hr} = (C_s \times Q_s \times 60) / 7000$$

$$\text{lbs/day} = \text{lbs/hr} \times 24 \text{ hrs/day}$$

J. H. Falls  
3/15/93

# A PAP

Permit No. 0570005-007-AV  
Emission Unit 004

RUN NUMBER	1	2	3	4	5	6
DATE	22-Jun-99	22-Jun-99	22-Jun-99	23-Jun-99	23-Jun-99	23-Jun-99
TIME START	10:30 AM	12:15 PM	1:45 PM	10:20 AM	1:55 PM	3:25 PM
TIME END	11:45 AM	1:25 PM	3:00 PM	11:30 AM	3:05 PM	4:40 PM
BP, INCHES Hg	30.05	30.05	30.05	30.01	30.01	30.01
STACK PRESSURE, INCHES Hg	30.10	30.09	30.07	30.08	30.03	30.00
AVG.SQ.ROOT(VEL. HEAD) IN Hg	0.846	0.809	0.788	0.839	0.811	0.797
ORIFICE PRESS. OF METER, IN WATER	3.71	3.45	3.34	3.34	3.45	3.35
AVG STACK ,F	118.2	121.4	122.2	117.9	122.0	123.7
STACK, DRY BULB	118.2	121.4	122.2	117.9	122.0	123.7
METER TEMPERATURE, F	100.7	112.7	116.9	97.2	112.4	116.9
VOL. OF GAS, DM CONDITIONS, FT3	51.974	50.509	49.740	49.461	51.067	50.506
VOL. GAS, STP, DRY COND. FT3	49.602	47.164	46.095	47.395	47.647	46.745
STACK GAS MOISTURE, % VOLUME	7.89	8.38	8.33	7.39	8.26	8.66
MW OF STACK GAS, DRY COND.	28.85	28.85	28.85	28.85	28.85	28.85
MW OF STACK GAS, STACK COND.	27.99	27.94	27.95	28.05	27.95	27.91
PITOT CORRECTION FACTOR	0.84	0.84	0.84	0.84	0.84	0.84
STACK GAS VELOCITY, STACK COND. FT3/SEC	50.32	48.31	47.10	49.86	48.49	47.78
STACK AREA, FT2	19.63	19.63	19.63	19.63	19.63	19.63
EFFECTIVE STACK AREA, FT2	19.63	19.63	19.63	19.63	19.63	19.63
STACK GAS FLOW-RATE AT STP, SCFMD	50149	47610	46345	49952	47706	46624
NET TIME OF TEST, MINUTES	60	60	60	60	60	60
SAMPLE NOZZLE AREA, FT2	0.000324	0.000324	0.000324	0.000324	0.000324	0.000324
PERCENT ISOKINETIC	99.9	100.1	100.5	95.8	100.9	101.3
FLUORIDE, MG.	2.92	2.92	2.99	2.44	2.83	3.01
FLUORIDE, LB/HR	0.39	0.39	0.40	0.34	0.37	0.40
FLUORIDE, LB/DAY	9.35	9.34	9.52	8.15	8.98	9.51
FLUORIDE, LB/HR/LIMIT	1.18	1.18	1.18	1.18	1.18	1.18
FLUORIDE, LB/DAY/LIMIT	28.3	28.3	28.3	28.3	28.3	28.3
PRODUCTION RATE, TPH P2O5 (INPUT)	64.2	64.1	65.3	65.3	65.4	65.8
PRODUCTION RATE, TPH/TARGET	65.0	65.0	65.0	65.0	65.0	65.0
PRODUCTION RATE, TPD P2O5 (INPUT)	1541	1538	1567	1567	1570	1579
PRODUCTION RATE, TPD/TARGET	1560	1560	1560	1560	1560	1560
PHOSPHATE ROCK SLURRY,TPH	340.33	339.38	337.51	337.30	339.30	340.44
100% SULFURIC ACID, TPH	158.24	163.16	170.85	159.31	175.21	208.84
WATER, TPH	12.63	12.61	12.85	12.85	12.88	12.94
LBS F/TON OF P2O5 (INPUT)	0.006	0.006	0.006	0.005	0.006	0.006
LBS F/TON OF P2O5/LIMIT	0.020	0.020	0.020	0.020	0.020	0.020
VISIBLE EMISSIONS	0%					
VISIBLE EMISSIONS LIMIT	20%					

## EMISSION CALCULATIONS

Date: June 22, 1999

Unit: A PAP

Run no. 1

$$\begin{aligned} V_{wstd} &= 0.04707 \text{ Cuft/ml} \times (v_1) \\ &= 0.04707 \text{ Cuft/ml} \times 90.3 \text{ ml} \\ &= \mathbf{4.250 \text{ Cuft.}} \end{aligned}$$

$$\begin{aligned} V_{mstd} &= V_m \left[ \frac{T_{std}}{T_m + 460} \right] \left[ \frac{P_{bar} + (H / 13.6)}{P_{std}} \right] Y_i \\ &= 51.974 \text{ Cuft} \times \left[ \frac{528}{460 + 100.7} \right] \times \left[ \frac{(30.05 + (3.71 / 13.6))}{29.92} \right] \times 1.00 \\ &= \mathbf{49.602 \text{ Cuft.}} \end{aligned}$$

$$\begin{aligned} B_{wo} &= \frac{V_{wstd}}{V_{wstd} + V_{mstd}} \\ &= \frac{4.250}{4.250 + 49.602} \times 100 \\ &= \mathbf{7.89 \%} \end{aligned}$$

$$\begin{aligned} M_s &= M_d (1 - B_{wo}) + 18 (B_{wo}) \\ &= 28.85 \times (1 - 0.0789) + 18 \times 0.0789 \\ &= \mathbf{27.99} \end{aligned}$$

$$\begin{aligned} V_s (\text{avg}) &= K_p C_p \sqrt{P(\text{avg}) (460 + T_s) / (M_s P_s)} \\ &= 85.48 \times .84 \times 0.8460 \sqrt{(460 + 118.2) / (27.99 \times 30.10)} \\ &= \mathbf{50.32 \text{ ft/sec}} \end{aligned}$$

$$\begin{aligned} Q_s &= 60 (1 - B_{wo}) V_s A_s (T_{std} / T_s) (P_s / P_{std}) \\ &= 60 (1 - 0.0789) \times 50.32 \times 19.63 \times (528 / (460 + 118.2)) \times (30.10 / 29.92) \\ &= \mathbf{50,149 \text{ scfm}} \end{aligned}$$

$$\begin{aligned}
Cs &= 0.0154 \text{ grs/mg} \times (\text{total mg of sample}) / Vmstd \\
&= 0.0154 \text{ grs/mg} \times 2.92 \text{ mg} / 49.602 \text{ cuft} \\
&= \mathbf{0.0009 \text{ grs/cuft}}
\end{aligned}$$

$$\begin{aligned}
\text{lbs/hr} &= (Cs \times Qs \times 60 \text{ min/hr}) / 7000 \text{ grs/lb} \\
&= (0.0009 \times 50149 \times 60) / 7000 \\
&= \mathbf{0.39 \text{ lbs/hr Fluoride}}
\end{aligned}$$

$$\begin{aligned}
\text{lbs/day} &= \text{lbs/hr} \times 24 \text{ hrs/day} \\
&= 0.39 \times 24 \\
&= \mathbf{9.35 \text{ lbs/day Fluoride}}
\end{aligned}$$

Percent Isokinetic:

$$\begin{aligned}
I &= \frac{Ts (1.667) ((0.00267) V1) + (Vm / Tm) ((Pbar + (^H / 13.6)))}{0 Vs Ps An} \\
&= \frac{(460 + 118.2) (1.667) ((0.00267 \times 90.3) + (51.974 / (460 + 100.7))) \times ((30.05 + (3.71 / 13.6)))}{60 \times 50.32 \times 30.10 \times 0.000324} \\
&= \mathbf{99.9 \%}
\end{aligned}$$

## EMISSION CALCULATIONS

Date: June 23, 1999

Unit: A PAP

Run no. 4

$$\begin{aligned}
 V_{wstd} &= 0.04707 \text{ Cuft/ml} \times (v1) \\
 &= 0.04707 \text{ Cuft/ml} \times 80.4 \text{ ml} \\
 &= \mathbf{3.784 \text{ Cuft.}}
 \end{aligned}$$

$$\begin{aligned}
 V_{mstd} &= V_m \left[ \frac{T_{std}}{T_m + 460} \right] \left[ \frac{P_{bar} + (H / 13.6)}{P_{std}} \right] Y_i \\
 &= 49.461 \text{ Cuft} \times \left[ \frac{528}{460 + 97.2} \right] \times \left[ \frac{(30.01 + (3.34 / 13.6))}{29.92} \right] \times 1.00 \\
 &= \mathbf{47.395 \text{ Cuft.}}
 \end{aligned}$$

$$\begin{aligned}
 B_{wo} &= \frac{V_{wstd}}{V_{wstd} + V_{mstd}} \\
 &= \frac{3.784}{3.784 + 47.395} \times 100 \\
 &= \mathbf{7.39 \%}
 \end{aligned}$$

$$\begin{aligned}
 M_s &= M_d (1 - B_{wo}) + 18 (B_{wo}) \\
 &= 28.85 \times (1 - 0.0739) + 18 \times 0.0739 \\
 &= \mathbf{28.05}
 \end{aligned}$$

$$\begin{aligned}
 V_s (\text{avg}) &= K_p C_p \sqrt{P(\text{avg})} \sqrt{(460 + T_s) / (M_s P_s)} \\
 &= 85.48 \times .84 \times 0.8390 \times \sqrt{(460 + 117.9) / (28.05 \times 30.08)} \\
 &= \mathbf{49.86 \text{ ft/sec}}
 \end{aligned}$$

$$\begin{aligned}
 Q_s &= 60 (1 - B_{wo}) V_s A_s (T_{std} / T_s) (P_s / P_{std}) \\
 &= 60 (1 - 0.0739) \times 49.86 \times 19.63 \times (528 / (460 + 117.9)) \times (30.08 / 29.92) \\
 &= \mathbf{49,952 \text{ scfm}}
 \end{aligned}$$

$$\begin{aligned}
 Cs &= 0.0154 \text{ grs/mg} \times (\text{total mg of sample}) / Vmstd \\
 &= 0.0154 \text{ grs/mg} \times 2.44 \text{ mg} / 47.395 \text{ cuft} \\
 &= \mathbf{0.0008 \text{ grs/cuft}}
 \end{aligned}$$

$$\begin{aligned}
 \text{lbs/hr} &= (Cs \times Qs \times 60 \text{ min/hr}) / 7000 \text{ grs/lb} \\
 &= (0.0008 \times 49952 \times 60) / 7000 \\
 &= \mathbf{0.34 \text{ lbs/hr Fluoride}}
 \end{aligned}$$

$$\begin{aligned}
 \text{lbs/day} &= \text{lbs/hr} \times 24 \text{ hrs/day} \\
 &= 0.34 \times 24 \\
 &= \mathbf{8.15 \text{ lbs/day Fluoride}}
 \end{aligned}$$

Percent Isokinetic:

$$\begin{aligned}
 I &= \frac{Ts (1.667) ((0.00267) V1) + (Vm / Tm) ((Pbar + (^H / 13.6)))}{0 Vs Ps An} \\
 &= \frac{(460 + 117.9) (1.667) ((0.00267 \times 80.4) + (49.461 / (460 + 97.2))) \times ((30.01 + (3.34 / 13.6)))}{60 \times 49.86 \times 30.08 \times 0.000324} \\
 &= \mathbf{95.8 \%}
 \end{aligned}$$

DATE 6-22-99 SAMPLING TIME: FROM 10:30AM TO 3:00PM

**STATEMENT OF PROCESS WEIGHT:**

COMPANY NAME CF INDUSTRIES, INC., PLANT CITY PHOSPHATE COMPLEX  
 MAILING ADDRESS P.O. DRAWER L, PLANT CITY, FL. 33564  
 SOURCE IDENTIFICATION APAP PRODUCTION FACILITY  
 SOURCE LOCATION APAP PRODUCTION STACK

**DATA ON OPERATING CYCLE TIME:**

	Run # 1	Run # 2	Run # 3
START OF OPERATION, TIME	10:30AM	12:15PM	1:45PM
END OF OPERATION, TIME	11:45AM	1:25PM	3:00PM
ELAPSED TIME	75 MIN.	70 MIN.	75 MIN.
IDLE TIME DURING CYCLE	0	0	0

Type of Scrubber Liquid POND WATER

Liquid flow rate, gpm	Average	1870	1876	1868
	High	1976	1876	1868
Low	1864	1876	1868	

Liquid water pressure, psig	Average	52	52	52
	High	52	52	52
Low	52	52	52	

Total gas pressure drop, "w.g.	Average	11.25	11.5	11.5
	High	11.5	11.5	11.5
Low	11.0	11.5	11.5	

**DESIGN PROCESS RATING:**

PROCESS WEIGHT RATE (INPUT) 1416 T/D PRODUCT(OUTPUT) T/D

**DATA ON ACTUAL PROCESS RATE DURING OPERATION CYCLE:**

(Include specifications on fossil fuels)

MATERIAL	RATE*,TPH	340.33	339.38	337.51
<u>Phos Rock Slurry</u>	RATE*,TPH	158.24	167.16	170.85
<u>100% SULFURIC</u>	RATE*,TPH	12.63	12.61	12.85
<u>WATER</u>				

PRODUCT	TOTAL PROCESS WEIGHT RATE*	511.20	515.15	521.21
	RATE*,TPH			

INPUT RATE, TPH P2O5	64.19	64.10	65.31
TPD	1540.5	1538.5	1567.5

\*For phosphate process expressed as actual tons/hour and as tons of P2O5/hour.  
 For fossil fuel steam generators expressed as btu/hour heat input.  
 \*\*For sulfuric acid plants expressed as 100% H2SO4/hour.

I certify that the above statement is true to the best of my knowledge and belief:

Signature [Signature]  
 Title Plant Eng



DATE 6-23-77 SAMPLING TIME: FROM 10:20 AM TO 4:40 PM

STATEMENT OF PROCESS WEIGHT:

COMPANY NAME CF INDUSTRIES, INC., PLANT CITY PHOSPHATE COMPLEX  
 MAILING ADDRESS P.O. DRAWER L, PLANT CITY, FL. 33564  
 SOURCE IDENTIFICATION A PAP PRODUCTION FACILITY  
 SOURCE LOCATION A PAP PRODUCTION STACK

DATA ON OPERATING CYCLE TIME:

	Run # 1	Run # 2	Run # 3
START OF OPERATION, TIME	10:20 AM	1:55 PM	3:25 PM
END OF OPERATION, TIME	11:30 AM	3:05 PM	4:40 PM
ELAPSED TIME	78 MIN.	70 MIN.	75 MIN.
IDLE TIME DURING CYCLE	0	0	0

Type of Scrubber Liquid POND WATER

Liquid flow rate, gpm

	Average	High	Low
Run # 1	1872.5	1875	1870
Run # 2	1833	1833	1833
Run # 3	1833	1833	1833

Liquid water pressure, psig

	Average	High	Low
Run # 1	52	52	52
Run # 2	52	52	52
Run # 3	52	52	52

Total gas pressure drop, "w.g.

	Average	High	Low
Run # 1	11.0	11.0	11.0
Run # 2	11.0	11.0	11.0
Run # 3	11.0	11.0	11.0

DESIGN PROCESS RATING:

PROCESS WEIGHT RATE (INPUT) 1416 T/D PRODUCT(OUTPUT) \_\_\_\_\_ T/D

DATA ON ACTUAL PROCESS RATE DURING OPERATION CYCLE:  
 (Include specifications on fossil fuels)

MATERIAL	RATE*.TPH	Run # 1	Run # 2	Run # 3
<u>PHOS ROCK SLURRY</u>		337.30	339.30	340.44
<u>100% SULFURIC</u>		159.31	175.21	208.34
<u>WATER</u>		12.85	12.88	12.94

TOTAL PROCESS WEIGHT RATE\*

PRODUCT	RATE*.TPH	Run # 1	Run # 2	Run # 3
<u>PHOSPHORIC ACID SLURRY</u>		509.46	527.39	562.22

INPUT RATE, TPH P2O5

	Run # 1	Run # 2	Run # 3
	65.29	65.44	65.79
TPD	1567	1570.5	1579

\*For phosphate process expressed as actual tons/hour and as tons of P2O5/hour.  
 For fossil fuel steam generators expressed as btu/hour heat input.  
 \*\*For sulfuric acid plants expressed as 100% H2SO4/hour.

I certify that the above statement is true to the best of my knowledge and belief:

Signature [Signature]  
 Title Prod Eng.

14.

VISIBLE EMISSION OBSERVATION FORM

No. 1

COMPANY NAME  
*CF Industries, Inc. Plant City Complex*

STREET ADDRESS  
*10608 Paul Buchman Highway*

*10 miles north of Plant City*

CITY STATE ZIP  
*Plant City FL 33564*

PHONE (KEY CONTACT) SOURCE ID NUMBER  
*(813) 782-1591 (Ext. 290) 057000 004*

PROCESS EQUIPMENT *A Phosphoric Acid Production Facility* OPERATING MODE *Normal*

CONTROL EQUIPMENT *Packed bed scrubber with KinRay packing* OPERATING MODE *Normal*

DESCRIBE EMISSION POINT  
*Circular stack opening 5 feet in diameter*

HEIGHT ABOVE GROUND LEVEL *85'* HEIGHT RELATIVE TO OBSERVER  
Start *~85'* End *~85'*

DISTANCE FROM OBSERVER *Start ~200' End ~200'* DIRECTION FROM OBSERVER  
Start *W* End *W*

DESCRIBE EMISSIONS  
Start *None* End *None*

EMISSION COLOR *Start NA End NA* IF WATER DROPLET PLUME  
Attached  Detached

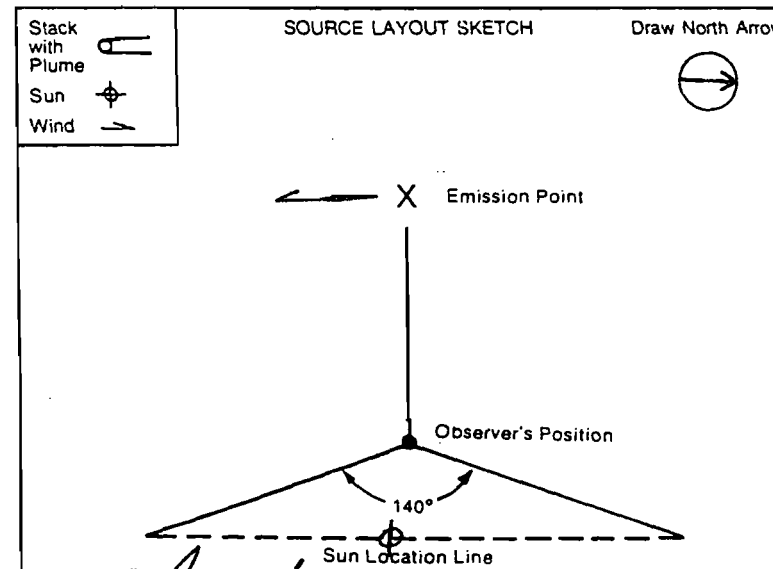
POINT IN THE PLUME AT WHICH OPACITY WAS DETERMINED  
Start *~5' From stack* End *~5' From stack*

DESCRIBE PLUME BACKGROUND  
Start *Scattered sky* End *Scattered sky*

BACKGROUND COLOR *Blue, gray, white* SKY CONDITIONS  
Start *Blue, gray, white* End *white* Start *Scattered* End *Scattered*

WIND SPEED *Start 4-8 mph End 8-12 mph* WIND DIRECTION  
Start *N* End *NW*

AMBIENT TEMP *Start 87°F End 88°F* WET BULB TEMP *72* RH, percent



ADDITIONAL INFORMATION  
*A. Harold Falls*  
*Chief Chemist*

OBSERVATION DATE		START TIME				END TIME
6/22/99		1035				1105
SEC	0	15	30	45	COMMENTS	
MIN						
1	0	0	0	0		
2	0	0	0	0		
3	0	0	0	0		
4	0	0	0	0		
5	0	0	0	0		
6	0	0	0	0		
7	0	0	0	0		
8	0	0	0	0		
9	0	0	0	0		
10	0	0	0	0		
11	0	0	0	0		
12	0	0	0	0		
13	0	0	0	0		
14	0	0	0	0		
15	0	0	0	0		
16	0	0	0	0		
17	0	0	0	0		
18	0	0	0	0		
19	0	0	0	0		
20	0	0	0	0		
21	0	0	0	0		
22	0	0	0	0		
23	0	0	0	0		
24	0	0	0	0		
25	0	0	0	0		
26	0	0	0	0		
27	0	0	0	0		
28	0	0	0	0		
29	0	0	0	0		
30	0	0	0	0		

OBSERVER'S NAME (PRINT)  
*Lloyd G. Camp*

OBSERVER'S SIGNATURE *Lloyd G. Camp* DATE *6/22/99*

ORGANIZATION  
*CF Industries, Inc. Plant City Complex*

CERTIFIED BY *Eastern Technical Associates* DATE *2/24/99*

CONTINUED ON VEO FORM NUMBER *2*

VISIBLE EMISSION OBSERVATION FORM

No. 2

COMPANY NAME  
*CF Industries, Inc. Plant City Complex*

STREET ADDRESS  
*10608 Paul Buchman Highway*  
*10 miles north of Plant City*

CITY *Plant City* STATE *FL* ZIP *33564*

PHONE (KEY CONTACT) *(813) 782-1591 (Ext. 290)* SOURCE ID NUMBER *057000 004*

PROCESS EQUIPMENT *A Phosphoric Acid Production Facility* OPERATING MODE *Normal*

CONTROL EQUIPMENT *Packed bed scrubber with Kin Ray packing* OPERATING MODE *Normal*

DESCRIBE EMISSION POINT  
*Circular stack opening 5 Feet in diameter*

HEIGHT ABOVE GROUND LEVEL *85'* HEIGHT RELATIVE TO OBSERVER  
Start *~ 85'* End *~ 85'*

DISTANCE FROM OBSERVER Start *~ 200'* End *~ 200'* DIRECTION FROM OBSERVER  
Start *W* End *W*

DESCRIBE EMISSIONS  
Start *None* End *None*

EMISSION COLOR Start *NA* End *NA* IF WATER DROPLET PLUME  
Attached  Detached

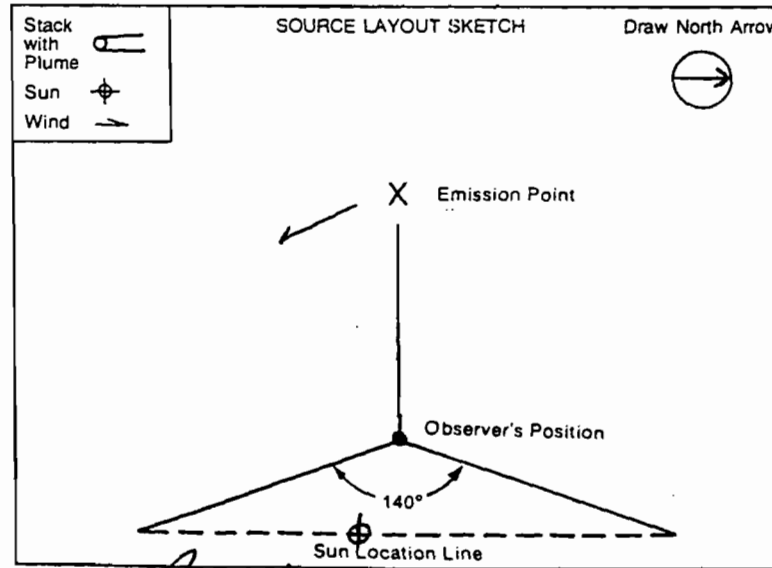
POINT IN THE PLUME AT WHICH OPACITY WAS DETERMINED  
Start *~ 5' from stack* End *~ 5' from stack*

DESCRIBE PLUME BACKGROUND  
Start *Scattered sky* End *Scattered sky*

BACKGROUND COLOR Start *Blue, gray, white* End *white* SKY CONDITIONS  
Start *Scattered* End *Scattered*

WIND SPEED Start *8-12 mph* End *10-14 mph* WIND DIRECTION  
Start *NW* End *NW*

AMBIENT TEMP Start *88°F* End *89°F* WET BULB TEMP *66* RH, percent



ADDITIONAL INFORMATION  
*Harold Falls*  
*Chief Chemist*

OBSERVATION DATE		START TIME			END TIME
6/22/99		1105			1135
SEC	0	15	30	45	COMMENTS
MIN					
1	0	0	0	0	
2	0	0	0	0	
3	0	0	0	0	
4	0	0	0	0	
5	0	0	0	0	
6	0	0	0	0	
7	0	0	0	0	
8	0	0	0	0	
9	0	0	0	0	
10	0	0	0	0	
11	0	0	0	0	
12	0	0	0	0	
13	0	0	0	0	
14	0	0	0	0	
15	0	0	0	0	
16	0	0	0	0	
17	0	0	0	0	
18	0	0	0	0	
19	0	0	0	0	
20	0	0	0	0	
21	0	0	0	0	
22	0	0	0	0	
23	0	0	0	0	
24	0	0	0	0	
25	0	0	0	0	
26	0	0	0	0	
27	0	0	0	0	
28	0	0	0	0	
29	0	0	0	0	
30	0	0	0	0	

OBSERVER'S NAME (PRINT) *Lloyd G. Camp*

OBSERVER'S SIGNATURE *Lloyd G. Camp* DATE *6/22/99*

ORGANIZATION *CF Industries, Inc. Plant City Complex*

CERTIFIED BY *Eastern Technical Associates* DATE *2/24/99*

CONTINUED ON VEO FORM NUMBER

APPENDIX "B"

FIELD DATA

METHOD 5 FIELD DATA

*Run 1*

Plant Site: Plant City, FL  
 Sampling Location: A PAP

Date: 06/22/1999  
 Stack ID (in): 60.00

Pt	Time min	Volume ft3	System Vacuum inHg	Delta P inH2O	Delta H inH2O	Ti °F	To °F	Ts °F	Tf °F	Timp °F
1	3.0	2.585	2.52	0.756	3.578	87.08	87.56	115.12	244.47	67.16
2	6.0	5.301	2.81	0.802	3.878	88.94	88.18	116.35	244.70	56.23
3	9.0	8.011	2.87	0.794	3.884	90.90	89.24	117.24	245.54	54.51
4	12.0	10.249	2.09	0.540	2.879	92.40	90.35	117.44	244.81	58.03
5	15.0	11.846	1.27	0.273	2.083	93.33	91.67	117.58	245.67	62.49
6	18.0	14.749	3.36	1.003	4.563	94.52	92.68	117.74	245.43	62.18
7	21.0	17.866	3.61	1.033	4.886	96.88	93.94	117.77	244.76	58.43
8	24.0	20.770	3.13	0.893	4.330	99.15	95.63	118.46	245.72	59.83
9	27.0	23.525	2.82	0.797	3.972	100.97	97.33	118.41	245.26	60.76
10	30.0	26.113	2.49	0.698	3.553	102.49	98.88	118.43	245.49	61.10
11	33.0	28.494	2.08	0.605	3.131	103.54	103.13	114.94	240.62	60.88
12	36.0	31.139	2.55	0.763	3.651	105.03	103.73	118.84	247.18	54.47
13	39.0	33.845	2.69	0.752	3.792	106.54	104.70	119.43	243.71	55.58
14	42.0	35.999	1.88	0.475	2.711	107.63	105.64	119.73	245.81	58.06
15	45.0	37.517	1.16	0.232	1.998	108.18	106.52	119.70	244.44	61.72
16	48.0	39.902	2.21	0.609	3.164	108.74	107.21	119.49	245.89	60.50
17	51.0	42.927	3.27	0.939	4.543	109.95	107.92	119.40	244.70	58.70
18	54.0	46.007	3.35	0.961	4.659	111.41	108.75	119.36	245.20	59.48
19	57.0	49.116	3.42	0.984	4.762	112.94	109.81	119.30	245.67	60.04
20	60.0	51.974	2.90	0.820	4.102	114.27	110.93	119.23	244.75	60.78

METHOD 5 FIELD DATA

*Run 2*

Plant Site: Plant City, FL  
 Sampling Location: A PAP

Date: 06/22/1999  
 Stack ID (in): 60.00

Pt	Time min	Volume ft3	System Vacuum inHg	Delta P inH2O	Delta H inH2O	Ti °F	To °F	Ts °F	Tf °F	Timp °F
1	3.0	2.501	2.07	0.652	3.270	111.05	110.91	118.42	240.91	68.03
2	6.0	5.112	2.28	0.694	3.487	111.15	110.67	120.95	246.80	57.74
3	9.0	7.655	2.23	0.654	3.343	111.44	110.53	121.28	244.74	56.96
4	12.0	9.647	1.53	0.393	2.409	111.59	110.42	121.33	244.84	60.83
5	15.0	10.832	0.82	0.139	1.604	111.44	110.37	121.02	245.76	64.99
6	18.0	13.606	2.65	0.893	4.060	111.40	110.32	121.03	245.37	63.04
7	21.0	16.606	2.92	0.914	4.415	112.22	110.49	120.98	245.46	62.98
8	24.0	19.438	2.62	0.805	3.972	112.93	110.77	120.73	245.49	63.36
9	27.0	22.148	2.42	0.739	3.691	113.81	111.37	120.87	245.54	62.80
10	30.0	24.522	1.95	0.562	2.981	114.32	111.97	120.70	245.48	62.69
11	33.0	26.833	1.88	0.572	2.914	112.54	111.99	119.17	239.90	64.62
12	36.0	29.376	2.21	0.646	3.356	113.20	112.25	121.48	247.26	58.60
13	39.0	32.028	2.37	0.702	3.541	113.95	112.55	121.97	244.54	59.46
14	42.0	34.269	1.86	0.502	2.734	114.25	112.67	122.39	244.86	62.16
15	45.0	36.018	1.38	0.391	2.315	114.20	112.82	122.35	244.28	64.66
16	48.0	38.454	2.13	0.580	3.107	114.45	113.09	121.79	246.80	59.98
17	51.0	41.394	2.87	0.885	4.270	114.98	113.33	122.99	244.28	55.33
18	54.0	44.431	3.00	0.928	4.471	115.87	113.66	123.14	246.04	54.77
19	57.0	47.559	3.17	0.979	4.707	116.89	114.21	122.96	244.33	55.34
20	60.0	50.509	2.88	0.874	4.273	117.68	114.77	122.71	244.52	56.22

METHOD 5 FIELD DATA

*R-43*

Plant Site: Plant City, FL  
 Sampling Location: A PAP

Date: 06/22/1999  
 Stack ID (in): 60.00

Pt	Time min	Volume ft3	System Vacuum inHg	Delta P inH2O	Delta H inH2O	Ti °F	To °F	Ts °F	Tf °F	Timp °F
1	3.0	2.451	2.10	0.614	3.136	115.54	115.20	118.73	241.58	68.96
2	6.0	5.103	2.49	0.702	3.539	115.89	115.10	120.68	246.68	59.34
3	9.0	7.508	2.16	0.574	3.018	116.42	115.27	121.21	244.62	61.89
4	12.0	9.619	1.80	0.458	2.638	116.65	115.30	121.82	246.03	64.42
5	15.0	10.860	0.91	0.146	1.666	116.32	115.12	122.42	245.16	62.12
6	18.0	13.591	2.70	0.837	3.902	116.02	114.92	122.66	246.02	59.38
7	21.0	16.547	2.98	0.872	4.246	116.59	114.95	122.75	244.71	59.31
8	24.0	19.326	2.66	0.766	3.810	117.43	115.33	122.63	245.24	61.86
9	27.0	21.900	2.37	0.658	3.382	118.01	115.75	122.53	246.18	60.50
10	30.0	24.136	1.88	0.493	2.709	118.20	116.07	122.36	245.26	59.68
11	33.0	26.476	1.98	0.561	2.925	116.61	115.95	118.72	242.43	60.77
12	36.0	29.031	2.31	0.656	3.328	117.28	116.15	122.74	248.80	51.85
13	39.0	31.707	2.51	0.706	3.572	117.90	116.34	123.22	243.80	50.92
14	42.0	33.934	1.93	0.493	2.722	118.25	116.48	123.56	245.68	50.86
15	45.0	35.518	1.24	0.243	2.007	118.42	116.80	123.54	245.52	53.10
16	48.0	37.968	2.27	0.628	3.187	118.35	116.88	123.55	245.81	52.80
17	51.0	40.986	3.14	0.910	4.408	118.82	117.02	123.29	244.93	53.18
18	54.0	44.025	3.16	0.912	4.444	119.88	117.50	122.44	241.84	53.53
19	57.0	47.101	3.24	0.939	4.576	120.93	118.06	122.22	248.68	53.12
20	60.0	49.740	2.50	0.684	3.506	121.55	118.57	122.31	245.08	54.42

## METHOD 5 FIELD DATA

Run 4

Plant Site: Plant City, FL  
Sampling Location: A PAPDate: 06/23/1999  
Stack ID (in): 60.00

Pt	Time min	Volume ft <sup>3</sup>	System Vacuum inHg	Delta P inH <sub>2</sub> O	Delta H inH <sub>2</sub> O	Ti °F	To °F	Ts °F	Tf °F	Timp °F
1	3.0	2.541	2.42	0.732	3.450	85.51	85.92	114.72	239.36	65.53
2	6.0	5.227	2.78	0.789	3.739	87.03	86.57	117.77	246.12	58.67
3	9.0	7.864	2.69	0.748	3.586	88.70	87.61	118.44	244.34	59.47
4	12.0	10.092	2.03	0.527	2.747	90.30	88.90	118.55	243.35	62.27
5	15.0	11.586	1.14	0.231	1.909	91.32	90.00	118.19	245.32	64.46
6	18.0	14.413	3.10	0.921	4.187	92.51	90.94	117.98	244.89	61.35
7	21.0	17.517	3.57	1.028	4.769	94.69	92.15	117.81	245.49	57.69
8	24.0	20.402	3.06	0.875	4.182	96.65	93.51	118.19	244.98	54.89
9	27.0	23.074	2.65	0.753	3.675	98.17	94.92	118.37	245.03	54.25
10	30.0	25.502	2.23	0.609	3.117	99.10	96.00	118.24	245.05	55.80
11	33.0	28.024	2.34	0.695	3.334	98.57	97.85	117.64	239.52	59.66
12	36.0	30.718	2.66	0.752	3.666	100.11	98.35	117.76	246.41	54.03
13	39.0	33.359	2.60	0.726	3.549	101.55	99.25	117.90	244.59	54.36
14	42.0	35.561	1.96	0.498	2.694	102.51	100.17	118.17	245.36	56.19
15	45.0	37.100	1.20	0.239	1.951	102.91	101.04	118.28	245.73	58.19
16	48.0	39.643	2.49	0.711	3.433	103.46	101.73	118.25	245.63	56.50
17	51.0	42.682	3.33	0.960	4.537	104.80	102.42	118.02	245.31	55.65
18	54.0	44.378	1.24	1.008	1.525	106.41	103.79	118.11	245.42	57.65
19	57.0	46.792	2.52	0.987	3.188	108.36	105.60	118.01	245.49	57.43
20	60.0	49.461	2.66	0.715	3.636	110.92	106.87	118.16	245.17	56.21



METHOD 5 FIELD DATA

*raws*

Plant Site: Plant City, FL  
 Sampling Location: A PAP

Date: 06/23/1999  
 Stack ID (in): 60.00

Pt	Time min	Volume ft3	System Vacuum inHg	Delta P inH2O	Delta H inH2O	Ti °F	To °F	Ts °F	Tf °F	Timp °F
1	3.0	2.379	2.03	0.584	2.848	107.20	107.77	117.43	245.48	78.68
2	6.0	4.982	2.42	0.690	3.309	106.74	107.71	120.04	245.77	66.92
3	9.0	7.558	2.44	0.666	3.270	107.18	107.82	120.96	245.24	63.15
4	12.0	9.599	1.75	0.416	2.380	107.74	107.94	120.96	245.65	63.61
5	15.0	10.737	0.88	0.127	1.427	108.25	108.19	120.86	245.76	65.29
6	18.0	13.519	2.88	0.884	3.990	108.73	108.61	121.37	246.19	62.75
7	21.0	16.606	3.34	0.968	4.566	109.73	109.04	121.98	245.96	59.21
8	24.0	19.630	3.21	0.918	4.375	111.22	109.71	122.31	245.38	60.37
9	27.0	22.445	2.86	0.800	3.917	112.65	110.66	122.51	245.81	60.12
10	30.0	25.081	2.55	0.692	3.485	113.69	111.50	122.31	246.16	59.10
11	33.0	27.742	2.57	0.740	3.580	114.09	113.42	122.65	241.70	60.09
12	36.0	30.352	2.51	0.677	3.404	115.04	113.79	123.48	248.71	53.75
13	39.0	32.943	2.52	0.666	3.372	115.66	114.01	123.17	244.36	56.87
14	42.0	35.101	1.95	0.455	2.585	116.25	114.44	123.29	246.28	58.32
15	45.0	36.624	1.27	0.220	1.925	116.28	114.70	123.30	245.01	60.20
16	48.0	38.979	2.28	0.585	2.989	116.10	114.83	123.12	244.90	59.29
17	51.0	41.915	3.14	0.855	4.164	116.59	114.95	122.85	246.76	58.19
18	54.0	44.933	3.32	0.909	4.419	117.65	115.37	122.49	245.63	59.07
19	57.0	48.051	3.48	0.955	4.645	118.75	115.94	122.20	245.60	60.32
20	60.0	51.067	3.33	0.895	4.391	119.84	116.61	121.93	246.09	61.69

METHOD 5 FIELD DATA

*Run 6*

Plant Site: Plant City, Fl  
 Sampling Location: A PAP

Date: 06/23/1999  
 Stack ID (in): 60.00

Pt	Time min	Volume ft3	System Vacuum inHg	Delta P inH2O	Delta H inH2O	Ti °F	To °F	Ts °F	Tf °F	Timp °F
1	3.0	2.633	2.33	0.706	3.482	116.48	115.94	121.87	244.39	64.48
2	6.0	5.283	2.41	0.691	3.507	116.91	115.86	122.03	245.43	55.93
3	9.0	7.937	2.49	0.695	3.523	117.37	115.91	122.49	245.51	57.30
4	12.0	10.057	1.76	0.433	2.541	117.54	115.91	122.54	245.85	61.24
5	15.0	11.773	1.40	0.351	2.246	117.30	115.88	122.57	245.78	66.25
6	18.0	14.617	2.78	0.797	3.958	117.50	115.93	123.31	245.89	57.39
7	21.0	17.670	3.10	0.923	4.453	118.14	116.09	123.77	245.95	54.63
8	24.0	20.535	2.76	0.806	3.978	118.88	116.37	123.87	244.30	56.03
9	27.0	23.214	2.47	0.703	3.553	119.26	116.56	123.79	246.51	56.58
10	30.0	25.549	1.99	0.535	2.864	119.24	116.67	123.62	245.25	56.67
11	33.0	28.152	2.32	0.696	3.420	117.00	116.11	123.70	238.16	56.82
12	36.0	30.830	2.46	0.710	3.542	117.33	116.07	124.65	248.47	50.97
13	39.0	33.458	2.42	0.682	3.423	117.59	115.91	124.63	242.14	53.44
14	42.0	35.683	1.90	0.482	2.658	117.85	116.09	124.77	247.52	57.04
15	45.0	37.074	1.08	0.183	1.782	117.39	115.88	124.54	243.03	62.07
16	48.0	39.214	1.85	0.471	2.569	117.00	115.75	124.50	247.10	60.69
17	51.0	41.924	2.61	0.736	3.637	117.09	115.74	124.75	245.06	56.45
18	54.0	44.841	2.95	0.840	4.103	117.65	115.85	124.52	246.00	55.91
19	57.0	47.919	3.20	0.937	4.496	118.20	115.98	124.27	244.66	57.07
20	60.0	50.506	2.42	0.650	3.339	118.69	116.25	124.03	245.05	59.04

METHOD 5 LEAK TEST DATA

Plant Site: Plant City, FL

Sampling Location: A PAP

Date: 06/22/1999

Stack ID: 004

Test	Leak Rate ft3/min	Sys Vac Pressure inHg	Initial Vol ft3	Final Vol ft3
RWV #1 < 1 10:20AM <i>ek</i>	0.01190	16.22	0.07200	0.08800
2 11:55AM <i>ek</i>	0.01190	6.64	52.00700	52.04200
RWV #2 < 3 12:05PM <i>ek</i>	0.01190	6.41	52.06100	52.08100
4 1:25PM <i>ek</i>	0.01190	6.64	50.54200	50.56600
RWV #3 < 5 1:40PM <i>ek</i>	0.01190	5.77	50.58500	50.60200
6 3:10PM <i>ek</i>	0.01190	6.61	49.77100	49.78800
7	0.00000	0.00	0.00000	0.00000
8	0.00000	0.00	0.00000	0.00000

METHOD 5 LEAK TEST DATA

Plant Site: Plant City, FL

Sampling Location: A PAP

Date: 06/23/1999

Stack ID: 004

Test	Leak Rate ft3/min	Sys Vac Pressure inHg	Initial Vol ft3	Final Vol ft3
RUN #4 < 1 10:15AM EK	0.01190	16.28	0.07600	0.08400
2 11:40AM EK	0.01190	6.73	49.49300	49.50800
RUN #5 < 3 1:50PM EK	0.01190	5.81	49.52700	49.57400
4 3:15PM EK	0.01190	6.69	51.10100	51.11600
RUN #6 < 5 3:20PM EK	0.01330	5.90	51.13600	51.20900
6 4:45PM EK	0.01190	6.68	50.53700	50.70400
7	0.00000	0.00	0.00000	0.00000
8	0.00000	0.00	0.00000	0.00000

# CF INDUSTRIES, INC.

## PLANT CITY PHOSPHATE COMPLEX LABORATORY ANALYSIS RECORD

DATE	<u>22-Jun-99</u>
TIME	<u>10:30 - 11:45</u>
STACK	<u>A PAP</u>
RUN	<u>#1</u>

### MOISTURE CONTENTS

IMPINGER	#1	#2	#3	#4
WEIGHT AFTER RUN, GRAMS	727.7	676.3	582.1	891.7
WEIGHT BEFORE RUN, GRAMS	670.4	658.6	578.1	880.4
WEIGHT GAIN/LOSS, GRAMS	57.3	17.7	4.0	11.3
TOTAL WEIGHT GAIN, GRAMS	<u>90.3</u>			

### SAMPLE SOLUTIONS ANALYSIS

	F
VOLUME OF SAMPLE, ML	<u>1000</u>
CONCENTRATION, UG/ML	<u>2.92</u>
TOTAL WEIGHT POLLUTANT, MGS	<u>2.92</u>

ANALYST Lloyd D. Camp

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padcomp.xls

# CF INDUSTRIES, INC.

## PLANT CITY PHOSPHATE COMPLEX LABORATORY ANALYSIS RECORD

DATE	<u>22-Jun-99</u>
TIME	<u>12:15 - 13:25</u>
STACK	<u>A PAP</u>
RUN	<u>#2</u>

### MOISTURE CONTENTS

IMPINGER	#1	#2	#3	#4
WEIGHT AFTER RUN, GRAMS	750.3	675.3	570.3	865.2
WEIGHT BEFORE RUN, GRAMS	<u>685.0</u>	<u>659.4</u>	<u>568.7</u>	<u>856.4</u>
WEIGHT GAIN/LOSS, GRAMS	<u>65.3</u>	<u>15.9</u>	<u>1.6</u>	<u>8.8</u>
TOTAL WEIGHT GAIN, GRAMS	<u>91.6</u>			

### SAMPLE SOLUTIONS ANALYSIS

	F
VOLUME OF SAMPLE, ML	<u>1000</u>
CONCENTRATION, UG/ML	<u>2.92</u>
TOTAL WEIGHT POLLUTANT, MGS	<u>2.92</u>

ANALYST *Thyde De Camp*  
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padcomp.xls

# CF INDUSTRIES, INC.

## PLANT CITY PHOSPHATE COMPLEX LABORATORY ANALYSIS RECORD

DATE	22-Jun-99
TIME	13:45 - 15:00
STACK	A PAP
RUN	#3

### MOISTURE CONTENTS

IMPINGER	#1	#2	#3	#4
WEIGHT AFTER RUN, GRAMS	737.6	694.2	578.8	859.3
WEIGHT BEFORE RUN, GRAMS	675.5	678.2	575.5	851.7
WEIGHT GAIN/LOSS, GRAMS	62.1	16.0	3.3	7.6
TOTAL WEIGHT GAIN, GRAMS	<u>89.0</u>			

### SAMPLE SOLUTIONS ANALYSIS

	F
VOLUME OF SAMPLE, ML	<u>1000</u>
CONCENTRATION, UG/ML	<u>2.99</u>
TOTAL WEIGHT POLLUTANT, MGS	<u>2.99</u>

ANALYST Lloyd B. Camp  
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padcomp.xls

# CF INDUSTRIES, INC.

## PLANT CITY PHOSPHATE COMPLEX LABORATORY ANALYSIS RECORD

DATE	<u>23-Jun-99</u>
TIME	<u>10:20 - 11:30</u>
STACK	<u>A PAP</u>
RUN	<u>#4</u>

### MOISTURE CONTENTS

IMPINGER	#1	#2	#3	#4
WEIGHT AFTER RUN, GRAMS	735.1	673.5	575.7	865.5
WEIGHT BEFORE RUN, GRAMS	<u>678.6</u>	<u>659.6</u>	<u>572.1</u>	<u>859.1</u>
WEIGHT GAIN/LOSS, GRAMS	<u>56.5</u>	<u>13.9</u>	<u>3.6</u>	<u>6.4</u>
TOTAL WEIGHT GAIN, GRAMS	<u>80.4</u>			

### SAMPLE SOLUTIONS ANALYSIS

VOLUME OF SAMPLE, ML	1000
CONCENTRATION, UG/ML	<u>2.44</u>
TOTAL WEIGHT POLLUTANT, MGS	<u>2.44</u>

ANALYST Floyd D. Camp  
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padcomp.xls



# CF INDUSTRIES, INC.

## PLANT CITY PHOSPHATE COMPLEX LABORATORY ANALYSIS RECORD

DATE	<u>23-Jun-99</u>
TIME	<u>13:55 - 15:05</u>
STACK	<u>A PAP</u>
RUN	<u>#5</u>

### MOISTURE CONTENTS

IMPINGER	#1	#2	#3	#4
WEIGHT AFTER RUN, GRAMS	<u>738.3</u>	<u>673.7</u>	<u>587.7</u>	<u>878.0</u>
WEIGHT BEFORE RUN, GRAMS	<u>668.7</u>	<u>659.3</u>	<u>586.3</u>	<u>872.3</u>
WEIGHT GAIN/LOSS, GRAMS	<u>69.6</u>	<u>14.4</u>	<u>1.4</u>	<u>5.7</u>
TOTAL WEIGHT GAIN, GRAMS	<u>91.1</u>			

### SAMPLE SOLUTIONS ANALYSIS

	<u>F</u>
VOLUME OF SAMPLE, ML	<u>1000</u>
CONCENTRATION, UG/ML	<u>2.83</u>
TOTAL WEIGHT POLLUTANT, MGS	<u>2.83</u>

ANALYST Lloyd B. Camp  
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padcomp.xls

# CF INDUSTRIES, INC.

## PLANT CITY PHOSPHATE COMPLEX LABORATORY ANALYSIS RECORD

DATE	<u>23-Jun-99</u>
TIME	<u>15:25 - 16:40</u>
STACK	<u>A PAP</u>
RUN	<u>#6</u>

### MOISTURE CONTENTS

IMPINGER	#1	#2	#3	#4
WEIGHT AFTER RUN, GRAMS	741.4	694.4	580.0	860.0
WEIGHT BEFORE RUN, GRAMS	<u>675.2</u>	<u>677.8</u>	<u>576.3</u>	<u>852.4</u>
WEIGHT GAIN/LOSS, GRAMS	<u>66.2</u>	<u>16.6</u>	<u>3.7</u>	<u>7.6</u>
TOTAL WEIGHT GAIN, GRAMS	<u>94.1</u>			

### SAMPLE SOLUTIONS ANALYSIS

VOLUME OF SAMPLE, ML	<u>1000</u>
CONCENTRATION, UG/ML	<u>3.01</u>
TOTAL WEIGHT POLLUTANT, MGS	<u>3.01</u>

ANALYST

*Floyd B. Camp*  
\_\_\_\_\_  
\_\_\_\_\_

padcomp.xls

# SAMPLE CHAIN OF CUSTODY

Plant Name CF INDUSTRIES, INC. PLANT CITY PHOSPHATE COMPLEX

Source Identification "A" PHOSPHORIC ACID PRODUCTION FACILITY

Date Sampled: JUNE 22, 1999 Sampling Time: 10:30 AM to 3:00 PM

Test for MOISTURE, FLUORIDE AND VISIBLE EMISSION

## SAMPLE RECOVERY

Sample Run	Description
1	#1 COLD BOX ASSEMBLY
2	#2 COLD BOX ASSEMBLY
3	#3 COLD BOX ASSEMBLY

Person engaged in sample recoveries:

Signature 

Title ANALYST II

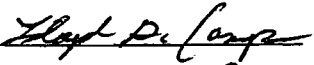
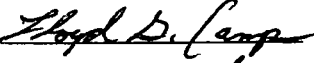
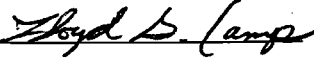
Location at which recovery "A" PHOSPHORIC ACID STACK

Laboratory person receiving samples:

Signature 

Title "A" CLASS TECHNICIAN

## ANALYSIS

Constituent	Method	Date	Time	Signature(s)
MOISTURE	EPA METHOD 4	6/22/99	12:15 - 15:30	
FLUORIDE	EPA METHOD 13 B	6/22/99	12:35 - 15:54	
VISIBLE EMISSION	EPA METHOD 9	6/22/99	10:35 - 11:35	

# SAMPLE CHAIN OF CUSTODY

Plant Name CF INDUSTRIES, INC. PLANT CITY PHOSPHATE COMPLEX

Source Identification "A" PHOSPHORIC ACID PRODUCTION FACILITY

Date Sampled: JUNE 23, 1999 Sampling Time: 10:20 AM to 4:40 PM

Test for MOISTURE AND FLUORIDE

## SAMPLE RECOVERY

Sample Run	Description
1	#1 COLD BOX ASSEMBLY
2	#2 COLD BOX ASSEMBLY
3	#3 COLD BOX ASSEMBLY

Person engaged in sample recoveries:

Signature *Paul J. Kottler*

Title ANALYST II

Location at which recovery "A" PHOSPHORIC ACID STACK

Laboratory person receiving samples:

Signature *Lloyd B. Camp*

Title "A" CLASS TECHNICIAN

## ANALYSIS


Constituent	Method	Date	Time	Signature(s)
MOISTURE	EPA METHOD 4	6/23/99	12:00 - 17:10	<i>Lloyd B. Camp</i>
FLUORIDE	EPA METHOD 13B	6/23/99	13:02 - 17:40	<i>Lloyd B. Camp</i>

**ANDERSEN**  
INSTRUMENTS INCORPORATED

DATE 7-14-98

TO WHOM IT MAY CONCERN:

THIS CERTIFIES THAT S-TYPE PITOT TUBES CONSTRUCTED AND CALIBRATED BY ANDERSEN INSTRUMENTS INC. COMPLY WITH PROCEDURES PROVIDED IN THE U.S. ENVIRONMENTAL PROTECTION AGENCY REFERENCE METHOD 2-DETERMINATION OF STACK GAS VELOCITY AND VOLUMETRIC FLOW RATE, VOL. 42, NO. 160 THURSDAY, AUGUST 18, 1977. ANDERSEN INSTRUMENTS INC. CERTIFIES THAT AT TIME OF SHIPMENT BASELINE COEFFICIENT VALUES OF 0.84 MAY BE ASSIGNED TO THE PITOT TUBES.

  
NATHAN D. CANUP  
SERVICE MANAGER

ANDERSEN INSTRUMENTS INC.  
A Subsidiary of Thermo Instruments Systems Inc.  
500 TECHNOLOGY COURT, SMYRNA, GA 30082-5211, USA  
TEL: 770 319 9999 - 800 241 6898 FAX: 770 319 0338

# CF INDUSTRIES

## TYPE S PITOT TUBE INSPECTION DATA FORM

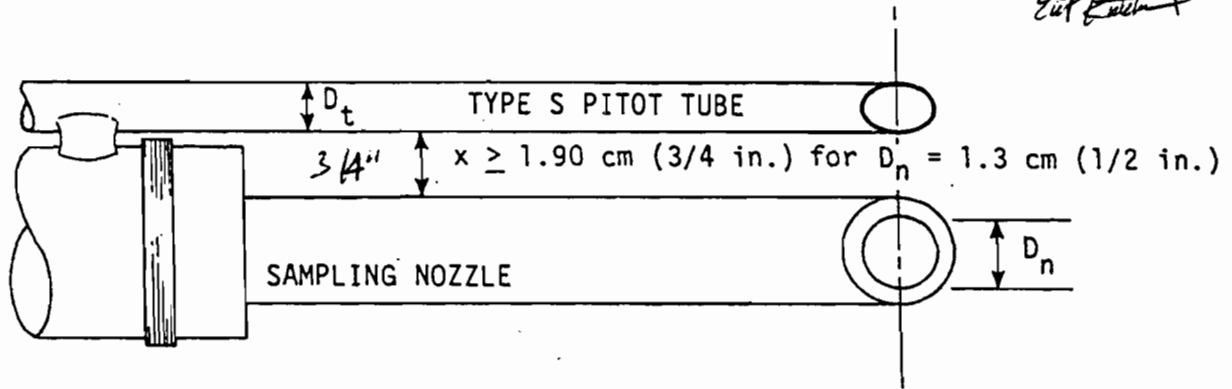
PROBE SS 60-1

MANUFACTURER ANDERSON INSTRUMENTS

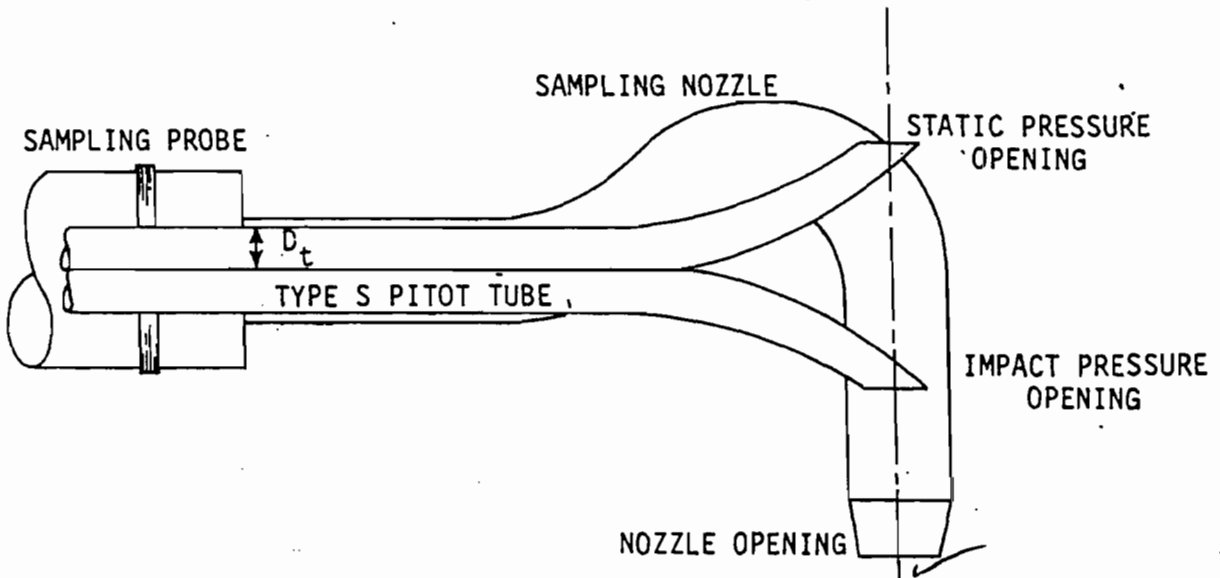
PROBE LENGTH 6'

DETACHABLE END PIECE SS N-02

6/16/99  
*Eut*



(a) BOTTOM VIEW: SHOWING MINIMUM PITOT-NOZZLE SEPARATION.



(b) SIDE VIEW: TO PREVENT PITOT TUBE FROM INTERFERING WITH GAS FLOW STREAMLINES APPROACHING THE NOZZLE, THE IMPACT PRESSURE OPENING PLANE OF THE PITOT TUBE SHALL BE EVEN WITH OR DOWNSTREAM FROM THE NOZZLE ENTRY PLANE

Figure 2.1 Required pitot tube-sampling nozzle configuration to prevent aerodynamic interference; buttonhook-type nozzle; centers of nozzle and pitot opening aligned; in respect to flow direction,  $D_t$  between 0.48 and 0.95 cm (3/16 and 3/8 in.).

# CF INDUSTRIES

## TYPE S PITOT TUBE INSPECTION DATA FORM

PROBE SS 60-1

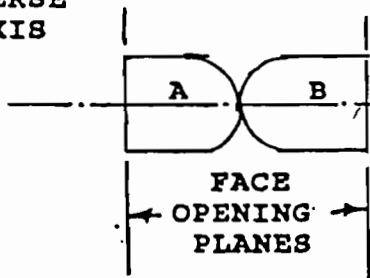
MANUFACTURER ANDERSON INSTRUMENTS

PROBE LENGTH 6'

DETACHABLE END PIECE SS N-02

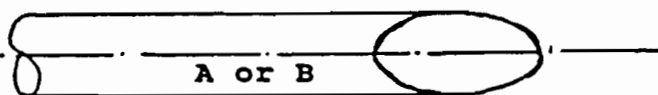
*6/16/99*

TRANSVERSE  
TUBE AXIS



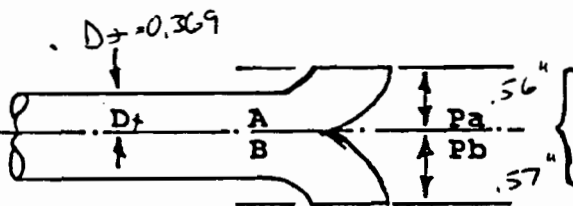
(a)

A SIDE PLANE



(c)

LONGITUDINAL  
TUBE AXIS



B SIDE PLANE

(b)

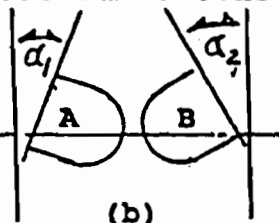
Note:

$$1.05 D \leq P \leq 1.5 D$$

$$P_a = P_b$$

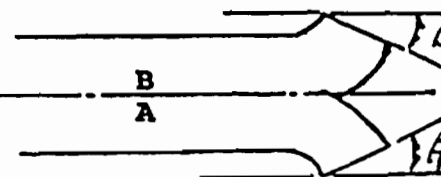
Figure 2.2 Properly constructed Type S pitot tube shown in: (a) end view: face opening planes perpendicular to transverse axis: (b) top view: face opening planes parallel to longitudinal axis: (c) side view: both legs of equal length and centerlines coincident, when viewed from both sides. Baseline coefficient values of 0.84 may be assigned to pitot tubes constructed this way.

TRANSVERSE  
TUBE AXIS

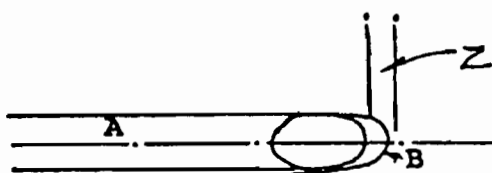


(b)

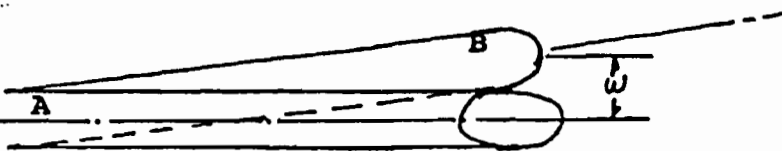
LONGITUDINAL  
TUBE AXIS



(a)



(c)



(d)

$\alpha_1$  3° Less than 10°

$\alpha_2$  4°

$z$  < 1/32" Less than 0.32 cm  
(1/8 ")

$\beta_1$  2° Less than 5°

$\beta_2$  3°

$w$  < 1/32" Less than 0.08 cm  
(1/32")

# CF INDUSTRIES

## TYPE S PITOT TUBE INSPECTION DATA FORM

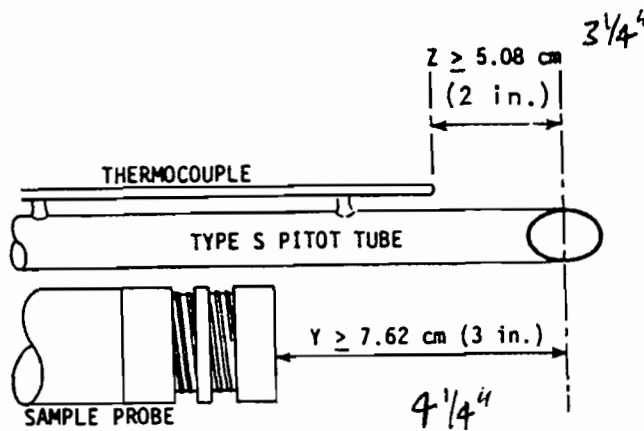
PROBE SS 60-1

MANUFACTOR ANDERSON INSTRUMENTS

PROBE LENGTH 6'

DETACHABLE END PIECE SS N-02

6/16/79 *[Signature]*



Required thermocouple and probe placement to prevent interference:  $D_t$  between 0.48 and 0.95 cm (3/16 and 3/8 in.).



CF INDUSTRIES, INC.  
Plant City Phosphate Complex  
LABORATORY ANALYSIS RECORD

"A" PAP Production Plant  
June 22, 1999


CF Industries, Inc., Plant City Phosphate Complex, uses a Fischer Accumet Model 50 pH meter with selective ion concentration capacity. The instrument has micro-processor function which calculates efficiency of the Orion Model 96-09 fluoride electrode being used and alerts the user in case of electrode malfunction.

STANDARDS

ELECTRODE  
EFFICIENCY

(See Technical Information Section)

0.1 $\mu\text{g/ml}$	0.9315
1.0 $\mu\text{g/ml}$	0.9922
2.0 $\mu\text{g/ml}$	
Quality Assurance Sample #1 - 0.38 $\mu\text{g/ml}$ . Analysis was 0.38 $\mu\text{g/ml}$ .	
Quality Assurance Sample #2 - 0.76 $\mu\text{g/ml}$ . Analysis was 0.77 $\mu\text{g/ml}$ .	
Quality Assurance Sample #3 - 1.90 $\mu\text{g/ml}$ . Analysis was 1.95 $\mu\text{g/ml}$ .	

  
J. Harold Falls  
Chief Chemist, Laboratory

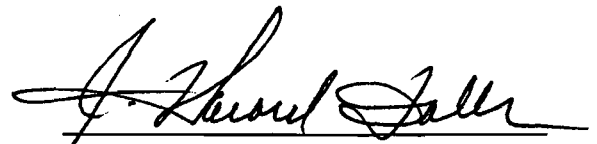
JHF/gm  
9/89

CF INDUSTRIES, INC.  
Plant City Phosphate Complex  
LABORATORY ANALYSIS RECORD

"A" PAP Production Plant  
June 23, 1999

CF Industries, Inc., Plant City Phosphate Complex, uses a Fischer Accumet Model 50 pH meter with selective ion concentration capacity. The instrument has micro-processor function which calculates efficiency of the Orion Model 96-09 fluoride electrode being used and alerts the user in case of electrode malfunction.

<u>STANDARDS</u>	<u>ELECTRODE</u> <u>EFFICIENCY</u>
	(See Technical Information Section)
0.1 $\mu\text{g/ml}$	0.9308
1.0 $\mu\text{g/ml}$	0.9827
2.0 $\mu\text{g/ml}$	
Quality Assurance Sample #1 - 0.38 $\mu\text{g/ml}$ . Analysis was 0.39 $\mu\text{g/ml}$ .	
Quality Assurance Sample #2 - 0.76 $\mu\text{g/ml}$ . Analysis was 0.75 $\mu\text{g/ml}$ .	
Quality Assurance Sample #3 - 1.90 $\mu\text{g/ml}$ . Analysis was 1.94 $\mu\text{g/ml}$ .	

  
J. Harold Falls  
Chief Chemist, Laboratory

JHF/gm  
9/89

## Overview

The Model 50 is a state-of-the-art, microprocessor based meter. It features uniquely simple operation with an extensive range of capabilities. The sealed keypad incorporates both numeric and function keys, including a convenient Help function. The large liquid crystal display offers a simultaneous display of a variety of information, including measurement results, time/date, standardization data and status icons. The large display size permits user information to be conveyed in simple, complete sentences—not the cryptic prompts more typical for laboratory meters.

The Model 50 includes dual input channels. A novel split-screen option allows the display to simultaneously track both inputs when desired. In addition to pH and millivolt measurement, this model also performs analyses with ion selective electrodes by direct potentiometry. Additionally, the Model 50 offers four incremental methods: known addition and subtraction and alternate addition and subtraction.

In pH operation, the meter may be set up to automatically recognize both Fisher color-coded buffers and NIST buffers, for maximum user convenience. Auto-recognized buffers are both identified and corrected by the meter for the temperature dependence of the buffer.

The Model 50 performs conductivity measurements in Siemens ( $\mu\text{hos}$ ) or salinity units. Probes with a variety of cell constants may be accommodated through software setup. Alternatively, the Model 50 may be set up to measure resistivity (ohms).

It is recommended that the user first complete the Installation instructions, then become familiar with Controls and Connectors, and finally consult the Operation sections for procedures of interest.

# Performance Characteristics

## Model 50

<b>Ranges</b>	-2 to 20 pH/pX -1800 to 1800 mV -5 to 105 °C 10 <sup>-9</sup> to 10 <sup>9</sup> Conc 0 to 40 ppt practical salinity 0 to 70 ppt NaCl equivalents 3 x 10 <sup>4</sup> μ-Siemens/cm 33 to ∞ Ω-cm
<b>Resolution</b>	0.1/0.01/0.001 pH 0.1 mV 0.1 °C 1, 2 or 3 significant figures ion 1, 2 or 3 significant figures conductivity
<b>Relative Accuracy</b>	+/-0.002 pH +/-0.1 mV @ 25 °C +/-0.2 °C

# Ion Operation

The Model 50 allows ion concentrations to be determined conveniently in any desired units of concentration, such as molarity, ppm or mg/L, and using any one of several techniques. Prior to analyzing samples by any of the ion methods, the operator should consult the following sections on *Method Selection*, *Low-Level Correction*, *Ionic Strength Adjustors* and *Temperature Compensation*.

## Method Selection

The Model 50 features a variety of methods for measuring ion concentrations in samples using ion selective electrodes (ISE's). Direct reading potentiometric methods offer speed and convenience, are applicable to wide ranges of sample concentrations and require no volumetric measurements. Conversely, sample-to-sample variations in ionic strength frequently require the use of an ionic strength adjusting buffer (ISA) with direct reading potentiometry.

Incremental methods offer a tolerance for samples of varying ionic strength and the ability to analyze samples containing complexing agents. One incremental method, analate subtraction, can even permit analyzing concentrations of ions to which no ion selective electrode directly responds. Conversely, volumetric measurements of both the sample and a standard increment are required by these methods. Additionally, the incremental methods are generally unworkable if sample concentrations are expected to vary over more than one or, at most two, orders of magnitude.

As a general rule, it is usually simplest to select direct reading unless prior knowledge about the sample indicates that incremental methods are to be preferred.

## Low-Level Correction

With samples containing very low levels of the ion of interest (often referred to as the "mud zone"), electrode response fails to conform to the Nernstian model. In the mud zone, changes in electrode output (slope) successively decrease as the sample concentration is further reduced. A plot of electrode output in millivolts versus logarithm of the sample concentration then becomes increasingly non-linear at very low concentrations.

The Model 50 offers two approaches to correcting for non-Nernstian response with low-level samples. In the first, the actual non-linear response curve of the electrode is approximated by a series of linear segments. Up to five different standards may be used, spanning the entire range of concentrations anticipated for samples. The meter then stores in memory a series of slope values corresponding to each successive pair of standards. These slopes, and the corresponding standard values, may be viewed individually by means of the slope key.

In linear segment measurements, the meter first identifies the general concentration range of the current sample, then computes its exact concentration by applying the nearest or bracketing standards. Use of the *Linear Segments* option can increase accuracy with dilute samples near the limits of the electrode's operating range.

The *Blank* feature provides an alternative means for measuring low-level samples. With this approach, the non-linear response curve of the electrode is fit by a mathematical model which assumes that all samples and standards have a constant background level of the species of interest. This situation may occur, for example, if the electrode can "self-sense" due to the finite solubility of the solid state sensing element. Standardization is performed with two standards from the electrode's linear region, as well as a blank sample. Measuring with the *Blank* option substantially enhances accuracy with dilute samples when the assumption of a constant background is true and a stable blank can be prepared.

---

## Ionic Strength Adjustors

Used directly, all selective ion electrodes respond to the *activity* of the ion of interest. The activity of an ion may be thought of as its effective concentration—a hybrid quantity derived from both the actual concentration of the ion as well as its mobility in the given solution.

In relatively dilute samples (typically less than 0.01 M), ions in the sample are relatively far removed from the influence of neighboring ions and act independently. In this event, ion activity and ion concentration are essentially identical. With more concentrated solutions, however, the presence of near neighbors acts to limit the mobility and effect of individual ions.

With increasing total ionic concentrations (ionic strength), ion activity becomes progressively diminished from actual ion concentration. This trend generally continues throughout the usable range of the electrode, although at extremely high concentrations, other effects may actually reverse it. In any event, in solutions of total ionic strength greater than perhaps 0.01 M, selective ion electrodes respond to an ion activity which may differ substantially from the ion concentration.

### Slope

The slope  $S$  of an electrode is defined as the change in its output voltage resulting from a decade change in the activity of the ion to which it responds. From the Nernst equation, the slope at any temperature  $T$  is given by

$$S_T = \xi (2.303 RT/F)$$

The quantity in the parentheses represents the slope for an ideal, monovalent, cation-sensing ISE (e.g., a pH or  $\text{Na}^+$  ion electrode), and has a value of 59.16 mV at 25 °C.

Because of their temperature dependence, the raw slope values do not provide a convenient measure of an electrode's performance. Consequently, slope values are usually mathematically corrected ("referenced") to a temperature of 25 °C:

$$S_{25} = S_T (298.16/T)$$

The value of its temperature referenced slope reflects the condition of an ISE since it may be compared simply and directly with the theoretical value of 59.16 at 25 °C. The Model 50 reports slope values temperature referenced to 25 °C.

### Efficiency Factor

Efficiency factor  $\xi$  is the actual slope value for an electrode, divided by its theoretical value. The efficiency factor for an electrode is thus easily interpretable in terms of its performance. For example, a pH electrode functioning ideally would exhibit an efficiency factor of exactly 1. Properly functioning, real pH electrodes typically will produce efficiency factors in the range of 0.90 to 1.05.

Efficiency factors for cation-sensing electrodes are positive, while those for anion-sensing electrodes are negative. Mathematically, the efficiency factor for an ideal electrode is always the reciprocal of the number of electrons exchanged in its electrode reaction, with the appropriate algebraic sign. Several examples appear in the table below:

ISE Type	Ideal Efficiency Factor
$\text{H}_3\text{O}^+$ (pH)	+ 1
$\text{F}^-$	- 1
$\text{Cl}^-$	- 1
$\text{Ca}^{+2}$	+ 0.5
$\text{S}^{-2}$	- 0.5

The efficiency factor for a real electrode, like its slope, may be determined experimentally from two-point (or more) standardization data.

---

### **Efficiency**

A related quantity, frequently used instead of efficiency factor, is electrode efficiency. The efficiency of an electrode is simply its efficiency factor expressed as a percent by multiplying by 100 and ignoring algebraic sign.

On this scale, properly functioning pH electrodes typically exhibit efficiencies between 90 and 105%. The Model 50 automatically compute and display electrode efficiencies, as well slopes temperature referenced to 25 °C, when the slope/eff key is pressed.

---

### **pH Measurements**

The pH of a solution is defined as

$$\text{pH} = -\log a_{\text{H}}$$

where  $a_{\text{H}}$  is the activity of the hydrogen ion in the solution. For hydrogen ions, the distinction between activity and concentration can usually be ignored.

Substituting the definitions of pH and slope into the Nernst equation, yields a working equation for computing sample pH:

$$E = E_0 + S_T \text{ pH}$$

In practice,  $E_0$  and  $S_T$  may be determined through standardization with buffers of known pH. The pH value of a sample then may be calculated from this equation and the measured output  $E$  of the electrode when placed in the sample.

---

### **Ion Measurements**

Ion measurements are complicated somewhat by the dependence of activity on the total ionic strength of the solution. For relatively dilute solutions, ion concentration and activity are essentially equivalent. However, to measure samples more concentrated than roughly 0.01 M, a special procedure is required to measure sample concentration directly.



---

## Section 1

# INTRODUCTION

### 1.1 Principle of Operation

The AST® Sampler is designed to sample gas stream effluents isokinetically in accordance with the U.S. Environmental Protection Agency (EPA) standards as outlined in the Code of Federal Regulations, Title 40, Part 60 (40CFR60), Appendix A. Stack gases are extracted through a nozzle and a heated probe into a heated filter chamber where the particulate is removed. The hot gases are then passed through a series of cold impingers where condensibles are removed and the gases are cooled before going to the pump, dry gas meter, and orifice.

The AST® Sampler is manufactured with all the mechanical hardware specified in 40CFR60 for EPA Methods 1, 2, 4 and 5. The AST® Sampler can be used with Andersen hardware to sample additional EPA Methods including methods 6, 8, 12, 13A, 13B, 17, 23, 26A, 29, 101, 101A, 103, 104, 108, 202, 315. Consult the Graseby Technical Sales Department or your local sales representative for application notes.



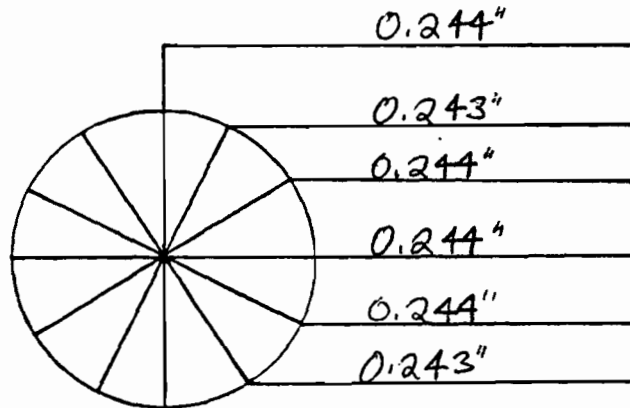
**CF Industries, Inc.**  
Plant City Phosphate Complex

PROBE NOZZLE CALIBRATION DATA

Nozzle Identification Number: 250-1

Calibrated by: Ernest Knutson

Date: 6/21/99



**Instructions:**

Measure to nearest 0.001"

**Tolerance:**

0.001" for mean of at least three readings.  
Maximum deviation between readings  $\leq 0.004$ "

Nozzle diameter,  $D_n$ : 0.244 In.

Nozzle area  $A_n$ : 0.000324 ft<sup>2</sup>

$$A_n = \frac{\pi}{144} \left( \frac{D_n}{2} \right)^2$$

**BEST AVAILABLE COPY**

Exhibit N

**ANNUAL GRASEBY STACKBOX THERMOCOUPLE CALIBRATIONS**

-UNIT #1200

DATE 7/13/98

FOR TEMPERATURES 0 TO 110 DEGREES C  
NIST Traceable Thermometer # J96-258

FOR TEMPERATURES 110 TO 200 DEGREES C  
NIST Traceable Thermometer # 90B-2024

Time: 1100-1530

Initial *[Signature]*

Thermocouple		Ice Water Point			Ambient Point			Hot Water Point			Hot Oil Point		
	Thermocouple Reading (Degrees F)	NIST Reading		Thermocouple Reading (Degrees F)	NIST Reading		Thermocouple Reading (Degrees F)	NIST Reading		Thermocouple Reading (Degrees F)	NIST Reading		
		Actual	Con- version to		Actual	Con- version to		Actual	Con- version to		Actual	Con- version to	
		Degrees			Degrees			Degrees			Degrees		
		C	F		C	F		C	F		C	F	
[1] Stack	Probe 4.5 ft. #45-1	32.6	0.6	33.1	78.1	26.6	79.8	184.4	86.3	187.4	N/A	N/A	N/A
	Probe 6.0ft. #60-1	32.1	0.6	33.1	81.3	29.2	84.6	184.6	86.3	187.4	N/A	N/A	N/A
	Probe 10.5ft. #105-1	32.6	0.8	33.4	71.8	22.4	72.3	188.2	87.2	189.0	N/A	N/A	N/A
	Probe 11.0ft. #110-1	32.1	0.6	33.1	80.7	28.4	83.1	183.3	86.0	186.8	N/A	N/A	N/A
[2] Probe (Probe Liner Heater)	Probe 4.5 ft. #45-1	31.8	0.8	33.1	82.6	29.0	84.2	N/A	N/A	N/A	234.6	113.4	236.1
	Probe 6.0ft. #60-1	32.8	0.8	33.4	82.2	29.2	84.6	N/A	N/A	N/A	234.8	113.2	235.8
	Probe 10.5ft. #105-1	32.4	1.0	33.8	71.4	22.2	72.0	N/A	N/A	N/A	238.6	115.6	240.1
	Probe 11.0ft. #110-1	32.6	0.8	33.4	81.9	28.4	83.1	N/A	N/A	N/A	235.1	114.6	238.3
[3] Hot Box	Box	32.4	1.0	33.8	82.2	28.6	83.5	N/A	N/A	N/A	237.1	115.2	239.4
	Filter Exit	32.2	1.0	33.8	82.3	28.6	83.5	N/A	N/A	N/A	238.2	115.0	239.0
[4] Umbilical	Coldbox Exit	33.6	1.0	33.8	82.8	28.4	83.1	185.1	85.6	186.1	N/A	N/A	N/A
[5] DGM Inlet	Control Box	33.2	1.0	33.8	81.9	28.6	83.5	185.1	85.4	185.7	N/A	N/A	N/A
[6] DGM Exit	Control Box	33.2	1.0	33.8	82.5	28.6	83.5	185.1	85.4	185.7	N/A	N/A	N/A
[7] Spare	Ambient	32.8	0.2	33.8	82.1	28.6	83.5	185.1	85.2	185.4	N/A	N/A	N/A

NOTE:

10.5FT PROBE SENSOR REPAIRED & CALIBRATED 4/1/99 *1/10*

ELK

# DRY GAS METER CALIBRATION

## Anderson AST Meter Box

Meter Box Number: 1200 Barometric Pressure: 30.03  
 Date: 12/16/98 Dry Gas Test Meter#: Rockwell 631105  
 Initial *Cal. Y. Kauter* Dry Gas AST Box Meter#: Schlumberger 1102

Flowrate Setting (CFM)	Gas Volume		Temperature		AST Box Meter Delta H (" H2O)	Time (Theta) min.	Actual Flowrate (CFM)	Yi (Software) (Setpoint)	Delta H@ in. H2O
	DGM Test Meter (Vw) ft.^3	AST Box Meter (Vd) ft.^3	DGM Test Meter (Tw) Deg F	AST Box Meter (Td) Deg F					
0.40	11.660	11.697	69.6	71.8	0.736	28.85	0.404	1.0000	2.512
0.50	7.500	7.556	69.6	74.2	1.152	14.83	0.506	1.0000	2.498
0.60	10.358	10.470	70.2	76.7	1.625	17.20	0.602	1.0000	2.477
0.70	31.644	32.310	70.2	82.3	2.232	45.40	0.697	1.0000	2.512
0.80	19.097	19.557	70.2	84.6	2.658	24.25	0.788	1.0000	2.333
0.90	14.301	14.684	70.7	86.1	3.237	16.18	0.884	1.0000	2.255
1.00	16.701	17.123	73.0	87.8	3.937	17.15	0.974	1.0000	2.271
1.10	7.302	7.491	73.0	88.3	4.722	6.87	1.063	1.0000	2.282
1.20	32.996	34.085	73.0	92.2	5.472	28.7	1.150	1.0000	2.247
Average								1.0000	2.376
Max. Diff.								0	0.136

$$Y_i = \frac{V_w P_b (t_d + 460)}{V_d (P_b + \Delta H / 13.6) (T_w + 460)}$$

$$\Delta H @ = \frac{.0317 (\Delta H)}{P_b (t_d + 460)} [(t_w + 460) (\theta) / V_w]^2$$

Where: Vw = Gas Volume passing through the std test meter, ft.^3.  
 Vd = Gas Volume passing through the dry gas meter, ft.^3.  
 Tw = Temperature of the gas in the std test meter, deg. F.  
 Td = Average temperature of the gas in the dry gas meter, deg.F.  
 Delta H = Pressure differential across orifice. in, H2O.  
 Yi = Ratio of accuracy of std test meter to dry gas meter for each run.  
 Y = Average ratio of accuracy of std test meter to dry gas meter.  
 Pb = Barometric pressure, in. Hg.  
 Theta = Time of calibration run, min.

# SOUTHERN ENVIRONMENTAL SCIENCES, INC.

## WET TEST METER CALIBRATION CHECK

Wet Test Meter No. P-576					
Date: 3/29/98					
Checked by: B. Nelson					
TEST NO.	Gas Volume		Temperature		Cal. Factor
	Liquid Displacement (F <sup>3</sup> )	Wet Test Meter (F <sup>3</sup> )	Liquid Displacement (°F)	Wet Test Meter (°F)	
1	1.115	1.10	78	78	1.020
2	1.090	1.10	78	78	.991
3	1.088	1.10	78	78	.989
Avg.					1.000

## Standard Dry Gas Meter Calibration

GAS METER MANUF.	ROCKWELL	PERFORMED FOR	C.F. INDUSTRIES
MODEL #	175-S	DATE	2/12/99
SERIAL #	JA 631105	BAROMETRIC PRES.	30.22
WET TEST METER #	P - 576	LEAK CHECK	0.00 CFM at 15" Hg

Approximate Flowrate (CFM)	Gas Volume		Temperature		Dry Gas Meter Delta P (" H2O)	Time (Theta) (min)	Flowrate (CFM)	DRY GAS METER COEFF. (Yds)	AVG. GAS METER COEFF. (Yds)
	Wet Test Meter (Vw) (ft.^3)	Dry Gas Meter (Vd) (ft.^3)	Wet Test Meter (Tw) (Deg F)	Dry Gas Meter (Td) (Deg F)					
0.40	5.000	4.931	71.0	72.0	0.06	14.05	0.357	1.016	1.016
0.40	5.000	4.921	71.0	72.0	0.06	14.02	0.358	1.014	
0.40	5.000	4.905	71.0	72.0	0.06	14.04	0.358	1.017	
0.60	5.000	4.944	71.0	72.0	0.1	8.25	0.608	1.009	1.008
0.60	5.000	4.949	71.0	73.0	0.1	8.21	0.611	1.006	
0.60	5.000	4.931	71.0	73.0	0.1	8.18	0.614	1.010	
0.80	5.000	4.945	72.0	73.5	0.12	5.91	0.848	1.008	1.009
0.80	5.000	4.936	72.0	73.5	0.12	5.96	0.841	1.010	
0.80	5.000	4.942	72.0	73.5	0.12	5.97	0.839	1.009	
1.00	5.000	4.962	72.0	73.5	0.17	4.90	1.022	1.004	1.005
1.00	5.000	4.957	72.0	73.5	0.17	4.86	1.031	1.005	
1.00	5.000	4.962	72.0	73.5	0.17	4.86	1.031	1.004	
1.20	5.000	4.955	72.0	73.5	0.20	4.08	1.228	1.006	1.006
1.20	5.000	4.955	72.0	73.5	0.20	4.09	1.225	1.006	
1.20	5.000	4.953	72.0	73.5	0.20	4.09	1.225	1.006	

$$Q = \frac{P_b \times V_w \times 528}{(T_w + 460) \times \Theta \times 29.92}$$

$$Y_{ds} = \frac{V_w}{V_d} \times \frac{(T_d + 460)}{(T_w + 460)} \times \frac{P_b}{[P_b + (\Delta P / 13.6)]}$$

where:

- Vw = Gas Volume passing through the std test meter, ft.^3.
- Vd = Gas Volume passing through the dry gas meter, ft.^3
- Tw = Temperature of the gas in the std test meter, deg. F.
- Td = Average temperature of the gas in the dry gas meter, Deg F.
- Delta H = Pressure differential across orifice, in. H2O.
- Yds = Dry gas meter coefficient.
- Pb = Barometric pressure, in. Hg.
- Theta = Time of calibration run, min.

# STANDARD METER CALIBRATION CURVE

GAS METER MANUF. ROCKWELL	PERFORMED FOR C.F. INDUSTRIES
MODEL # 175-S	DATE 2/12/99
SERIAL # JA 631105	

## Regression Output:

Flowrate (CFM)	DRY GAS METER COEFF. (Yds)
0.358	1.016
0.611	1.008
0.843	1.009
1.028	1.005
1.226	1.006

Constant	72.47
Std Err of Y Est	0.18
R Squared	0.78
No. of Observations	5.00
Degrees of Freedom	3.00

X Coefficient(s)	-71.04
Std Err of Coef.	21.53

## CALIBRATION CURVE

FLOW (CFM)	CORRECTION FACTOR
0.42	1.014
0.45	1.014
0.50	1.013
0.55	1.012
0.60	1.012
0.65	1.011
0.70	1.010
0.75	1.010
0.80	1.009
0.85	1.008
0.90	1.007
0.95	1.007
1.00	1.006
1.05	1.005
1.10	1.005
1.15	1.004
1.20	1.003

POSTTEST DRY GAS METER CALIBRATION DATA FORM (English units)

Test numbers \_\_\_\_\_ Date 6/24/99 Meter box number 1200 Plant APAD  
 Barometric pressure,  $P_b =$  30.02 in. Hg Dry gas meter number 1102 Pretest Y 1.000

Orifice manometer setting, ( $\Delta H$ ), in. H <sub>2</sub> O	Gas volume		Temperature				Time ( $\theta$ ), min	Vacuum setting, in. Hg	$Y_i$	$Y_i = \frac{V_w P_b (t_d + 460)}{V_d P_b + \frac{\Delta H}{13.6} t_w + 460}$
	Dry test meter ( $V_w$ ), ft <sup>3</sup>	Dry gas meter ( $V_d$ ), ft <sup>3</sup>	Dry test meter ( $t_w$ ), °F	Dry gas meter						
				Inlet ( $t_{d_i}$ ), °F	Outlet ( $t_{d_o}$ ), °F	Average ( $t_d$ ), °F				
(.842 CFM)										
3.08	12.739	13.0462	75.2°	87.7°	87.7°	87.7°	15.53	3.6	0.9917	$(12.739)(30.02)(547.7)$ $(13.0462)(30.246)(535.2)$
3.08	13.847	14.1061	75.2°	90.3°	90.3°	90.3°	16.80	3.6	1.0017	$(13.847)(30.02)(550.3)$ $(14.1061)(30.246)(535.2)$
3.08	13.706	14.0385	75.2°	92.9°	92.9°	92.9°	16.70	3.6	1.0029	$(13.706)(30.02)(552.9)$ $(14.0385)(30.246)(535.2)$
$Y = 0.9988$										

<sup>a</sup> If there is only one thermometer on the dry gas meter, record the temperature under  $t_d$ .

$V_w$  = Gas volume passing through the wet test meter, ft<sup>3</sup>.

$V_d$  = Gas volume passing through the dry gas meter, ft<sup>3</sup>.

$t_w$  = Temperature of the gas in the wet test meter, °F.

$t_{d_i}$  = Temperature of the inlet gas of the dry gas meter, °F.

$t_{d_o}$  = Temperature of the outlet gas of the dry gas meter, °F.

$t_d$  = Average temperature of the gas in the dry gas meter, obtained by the average of  $t_{d_i}$  and  $t_{d_o}$ , °F.

$\Delta H$  = Pressure differential across orifice, in H<sub>2</sub>O.

$Y_i$  = Ratio of accuracy of wet test meter to dry gas meter for each run.

$Y$  = Average ratio of accuracy of wet test meter to dry gas meter for all three runs; tolerance = pretest Y  $\pm 0.05Y$

$P_b$  = Barometric pressure, in. Hg.

$\theta$  = Time of calibration run, min.

Dry test meter number Rockwell-3A631105 Quality Assurance Handbook M5-2.4A

Within  $\pm 0.05Y$   
 6/24/99, 11:15 AM  
*[Signature]*



APPENDIX "C"

PROJECT PARTICIPANTS

PROJECT PARTICIPANTS

CF INDUSTRIES, INC.

PLANT CITY PHOSPHATE COMPLEX

H.E. Morris	General Manager
R.C. May	Manager of Engineering
T.A. Edwards	Supt., Environmental Affairs
J.M. Messina	Chief of Environmental Affairs
J.H. Falls	Chief Chemist, Laboratory
J.I. Longest	Staff Chemist
T. Ortoski	Environmental Supervisor
E. Kretschmar	Analyst II
S. Willoughby	"A" Class Technician
L. Camp	"A" Class Technician
W. Cherry	"A" Class Technician

813,744-6158 P.01/01  
TABLE: MEM. File  
BCM  
RGR



# Department of Environmental Protection

Jeb Bush  
Governor

Southwest District  
3804 Coconut Palm Drive  
Tampa, Florida 33619

David B. Scrubs  
Secretary

May 26, 1999

Mr. Thomas A. Edwards  
Superintendent, Environmental Affairs  
CF Industries, Inc.  
P.O. Drawer L  
Plant City, FL 33564-9007

Re: Compliance tests for A & B Phosphoric Acid Units, 0570005-007-AV

Dear Mr. Edwards:

This letter authorizes CF Industries, Inc., to temporarily operate A & B Phosphoric Acid Units at process rates approximately 10% beyond their current, maximum-permitted rates in order to conduct the annual compliance tests. Each unit's test must take no longer than 15 days (your letter indicates that each unit's test will take no longer than one week to complete), and each unit's production rate must be returned to the permitted range that existed before the test. Your estimates of the increases in emissions of fluoride indicate that existing limits will not be exceeded, even at the higher process rates. Test results at the temporary, higher rates will be used to support a subsequent application to modify the permit.

Notify the Hillsborough County Environmental Protection Commission of your schedule. If you have any questions, please contact Mr. Henry Gotsch, in our permitting division, at (813) 744-6100, ext. 113.

Sincerely,

FOR W.C. Thomas, P.E.,  
District Air Administrator  
Southwest District

cc: Mr. Rick Kirby, HCEPC

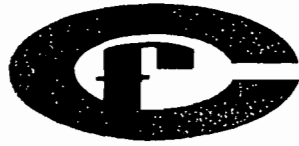
**RECEIVED**

JAN 21 2000

BUREAU OF AIR REGULATION

CF Industries, Inc. (CFII)  
Plant City Phosphate Complex  
Title V Permit No. 0570005-007-AV  
Construction Permit Application  
A & B Phosphoric Acid Units  
Attachment 2

P.O. Drawer L.  
Plant City, Florida 33564-9007  
Telephone: 813/782-1591



**CF Industries, Inc.**  
Plant City Phosphate Complex

June 21, 1999

Mr. Jerry Kissel  
Florida Department of  
Environmental Protection  
3804 Coconut Palm Drive  
Tampa, FL 33619-8318

SUBJECT: COMPLIANCE TEST - "B" PAP  
Permit No. 0570005-007-AV  
Emission Unit 009

Dear Mr. Kissel:

Enclosed are duplicate copies of the two recent compliance tests conducted at CF Industries, Inc., Plant City Phosphate Complex, on "B" Phosphoric Acid Plant. The tests were performed in accordance with "Specific Conditions 12 through 17" of Air Permit No. 0570005-007-AV, and at the rates specified in FDEP's letter dated May 26, 1999 (see Attachment 1).

In addition to the two compliance tests, CFII staff has enclosed copies of two preliminary test runs conducted on June 3, 1999, at 10% above the permitted rate, and June 4, 1999, at the permitted rate (see Attachment 2).

If there are any questions concerning the results, please give Michael Messina a call at 813-782-1591, ext. 290.

Sincerely,

T.A. Edwards,  
Superintendent, Environmental Affairs

TAE/JHF/gm  
u:\envrpt\225960.doc  
Enclosures

cc: ~~J.M. Messina~~  
T.V. Ortoski  
Sterlin Woodard/HCEPC

PERMIT NO. 0570005-007-Av

EMISSION UNIT 009

CF INDUSTRIES, INC.

PLANT CITY PHOSPHATE COMPLEX

"B" PHOSPHORIC ACID PRODUCTION

PLANT CITY, FLORIDA

June 7 & 8, 1999

TEST CONDUCTED BY:

Laboratory  
CF INDUSTRIES, INC.  
Plant City Phosphate Complex  
Plant City, Florida 33564

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PROCESS DESCRIPTION	1
LOCATION OF SAMPLING POINTS	2
DESCRIPTION OF SAMPLE POINTS	3
SAMPLING AND ANALYTICAL PROCEDURES	4
APPENDIX:	<u>PAGES</u>
APPENDIX "A" Emmission Calculation and Results	5 - 16
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INTRODUCTION:

The Environmental Control Laboratory of CF Industries, Inc., Plant City Phosphate Complex, conducted an emission test at "B" Phosphoric Acid Production Facility in Plant City, Florida on June 7 and 8, 1999. Six (6) 60-minute test runs were performed. The purpose of the test was to obtain emission data demonstrating compliance with the State of Florida DEP performance standards.

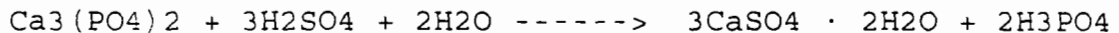
The measurements were made for fluoride and moisture at the stack outlet to the atmosphere. The measurements were within the permitted limits on all tests.

Complete results are give in APPENDIX "A".

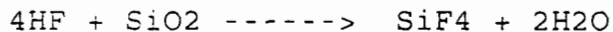
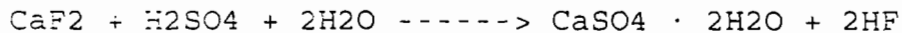
PROCESS DESCRIPTION

Phosphoric Acid is made by reacting sulfuric acid with phosphate rock along with a given amount of water to make an acid slurry. The mixing of sulfuric acid, rock and water takes place in a continuous reactor.

The principal reaction takes place as follows:



Other reactions as follows:



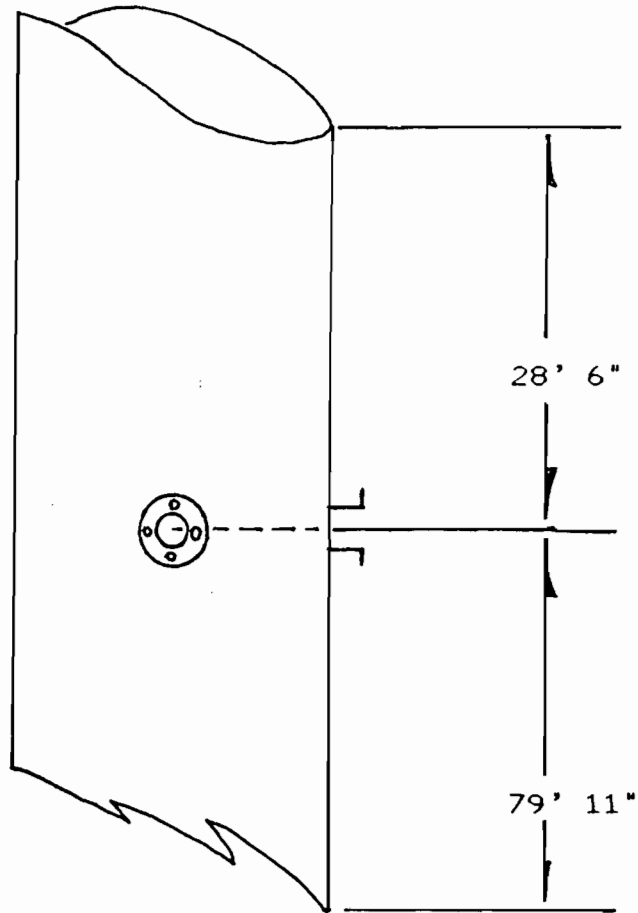
The resulting Phosphoric Acid will be 28 to 30% P2O5 content. This 28 to 30% P2O5 Phosphoric Acid solution will be further concentrated by evaporators until the acid strength reaches 52 to 54% P2O5.



LOCATION OF SAMPLING POINTS

The sampling sites and number of traverse points were selected as per Figure 1-2 EPA Method 1 specified in 40 CFR 60, Appendix A.

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Traverse Point Number	Distance from inside wall
1	2.1"
2	7.0"
3	14.2"
4	33.8"
5	41.0"
6	45.9"

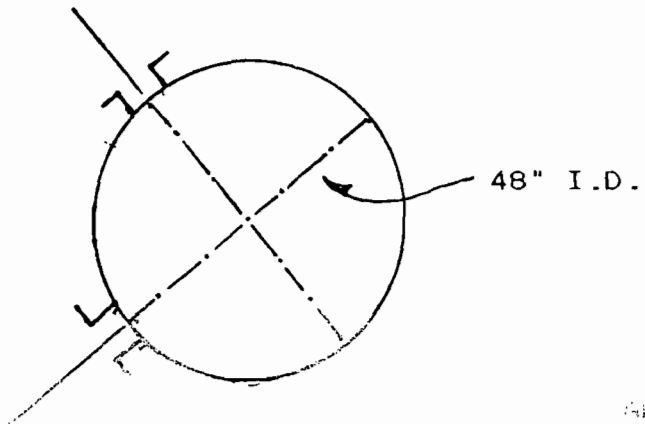


FIGURE 1

TRaverse POINT DESCRIPTION

"B" PAP PRODUCTION

## SAMPLING AND ANALYTICAL PROCEDURES

The methods described in EPA Methods 1, 2, 3, 4, 9 and 13B contained in 40 CFR 60, Appendix A and adopted by reference in Chapter 62-297.401 F.A.C. are used when testing during compliance by CF Industries, Inc.

APPENDIX "A"

EMISSION CALCULATIONS AND RESULTS

CF INDUSTRIES, INC.  
PLANT CITY PHOSPHATE COMPLEX

SOURCE SAMPLING NOMENCLATURE SHEET

Pb	= Barometric pressure, in Hg
Ps	= Stack pressure, in Hg
As	= Stack area, sq. ft.
As'	= Effective area of positive stack gas flow, sq. ft.
Ts	= Stack temperature °R
Tm	= Meter temperature °R
$\Delta$ Pavg	= Average square root of velocity head in. H <sub>2</sub> O
Cp	= S-type pitot tube correction factor
Kp	= 85.48 ft/sec (lb mole - °R) <sup>1/2</sup>
Ms	= Molecular weight of gas at stack conditions
Md	= Molecular weight of gas at dry conditions
Bwo	= Proportion by volume of water vapor in gas stream
Vwstd	= Volume of water vapor in gas sample
Vic	= Total volume of liquid collected in impinger & silica gel
$\rho_{H_2O}$	= Density of water 1 gm/ml
MH <sub>2</sub> O	= Molecular weight of water 18 lb/lb mole
R	= Ideal gas constant, 28.83 in. Hg-cu ft/lb-mole °R
Tstd	= Absolute temp. at standard conditions, 528 °R
Pstd	= Absolute pressure at standard conditions, 29.92 in. Hg.
Vmstd	= Volume of gas sample through dry gas meter (standard conditions) cu. ft.
Vm	= Volume of gas sample through the dry gas meter (meter condition) cu. ft.
$\Delta H$	= Orifice pressure of sampling meter
S.T.P.	= Standard condition, dry, 528 °R, 29.92 in. Hg
An	= Sampling nozzle area, square feet
Vs	= Velocity of stack gas, feet per second
Qs	= Volumetric flow rate, dry basis, standard conditions, CFM
Cs	= Concentration of particulate matter in stack gas, gr/SCF
Cf	= Concentration of fluoride in stack gas gr/SCF
Mf	= Total amount of fluoride collected, mg.
Mn	= Total amount of particulate matter collected, mg
I	= Percent isokinetic volume sampled
O	= Sampling time

$$V_{wstd} = 0.04707 \text{ cuft/ml } (V_1)$$

$$V_{mstd} = V_m \left( \frac{T_{std}}{T_m} \right) \left( \frac{P_{bar} + \frac{\Delta H}{13.6}}{P_{std}} \right)$$

$$B_{wo} = \frac{V_{wstd}}{V_{wstd} + V_{mstd}}$$

$$M_s = M_d (1 - B_{wo}) + 18 (B_{wo})$$

$$V_s(\text{avg}) = K_p C_p \sqrt{P(\text{avg})} \sqrt{\frac{460 + T_s}{M_s P_s}}$$

$$Q_s = 60 (1 - B_{wo}) V_s A_s \left( \frac{T_{std}}{T_s} \right) \left( \frac{P_s}{P_{std}} \right)$$

PERCENT ISOKINETIC

$$I = \frac{T_s (1.667) \left[ (0.00267) V_1 + \left( \frac{T_{std}}{T_m} \right) P_{bar} + \frac{\Delta H}{13.6} \right]}{\theta V_s P_s A_n}$$

$$C_s = 0.0154 \text{ grs/mg} \frac{M_f \text{ or } M_n}{V_{mstd}}$$

$$\text{lbs/hr} = (C_s \times Q_s \times 60) / 7000$$

$$\text{lbs/day} = \text{lbs/hr} \times 24 \text{ hrs/day}$$

J. H. Falls  
3/15/93

**BEST AVAILABLE COPY**

**B PAP**

**Permit No. 0570005-007-AV  
Emission Unit 009**

RUN NUMBER	1	2	3	4	5	6
DATE	07-Jun-99	07-Jun-99	07-Jun-99	08-Jun-99	08-Jun-99	08-Jun-99
TIME START	11:05 AM	3:12 PM	4:51 PM	10:40 AM	12:25 PM	2:10 PM
TIME END	12:17 PM	4:23 PM	6:00 PM	11:51 AM	1:35 PM	3:10 PM
BP, INCHES Hg	30.02	30.02	30.02	29.96	29.99	29.96
STACK PRESSURE, INCHES Hg	30.09	30.05	30.03	30.04	30.00	29.99
AVG.SQ.ROOT(VEL. HEAD) IN Hg	0.7040	0.6590	0.6470	0.6860	0.6590	0.6600
ORIFICE PRESS. OF METER, IN WATER	2.6200	2.3700	2.3400	2.6200	2.4600	2.3400
AVG STACK V, F	112.1	112.8	112.3	112.1	112.8	111.6
STACK, DRY BULB	112.1	112.8	112.3	112.1	112.8	111.6
METER TEMPERATURE, F	90.3	98.9	100.9	91.3	100.0	111.6
VOL. OF GAS, DM CONDITIONS, FT3	42.476	40.183	39.824	42.175	40.000	39.000
VOL. GAS, STP, DRY COND. FT3	41.153	38.309	37.829	40.707	38.633	37.435
STACK GAS MOISTURE, % VOLUME	6.46	6.97	7.04	7.08	7.25	7.05
MW OF STACK GAS, DRY COND.	28.85	28.85	28.85	28.85	28.85	28.85
MW OF STACK GAS, STACK COND.	28.15	28.09	28.09	28.08	28.08	28.09
PITOT CORRECTION FACTOR	0.84	0.84	0.84	0.84	0.84	0.84
STACK GAS VELOCITY, STACK COND. FT3/SEC	41.54	38.98	38.27	40.56	38.77	37.27
STACK AREA, FT2	12.566	12.566	12.566	12.566	12.566	12.566
EFFECTIVE STACK AREA, FT2	12.566	12.566	12.566	12.566	12.566	12.566
STACK GAS FLOW-RATE AT STP, SCFMD	27194	25309	24835	26333	25066	24181
NET TIME OF TEST, MINUTES	60	60	60	60	60	60
SAMPLE NOZZLE AREA, FT2	0.000325	0.000325	0.000325	0.000325	0.000325	0.000325
PERCENT ISOKINETIC	97.5	97.6	98.2	99.6	99.8	99.8
FLUORIDE, MG.	2.81	2.88	2.71	2.86	3.01	2.70
FLUORIDE, LB/HR	0.25	0.25	0.23	0.24	0.26	0.23
FLUORIDE, LB/DAY	5.88	6.03	5.64	5.86	6.16	5.50
FLUORIDE, LB/HR. LIMIT	1.04	1.04	1.04	1.04	1.04	1.04
FLUORIDE, LB/DAY LIMIT	24.9	24.9	24.9	24.9	24.9	24.9
PRODUCTION RATE, TPH P2O5 INPUT	96.5	96.5	96.5	96.5	96.4	96.4
PRODUCTION RATE, TPH LIMIT	97.0	97.0	97.0	97.0	97.0	97.0
PRODUCTION RATE, TPD P2O5 INPUT	2316	2316	2316	2316	2314	2314
PRODUCTION RATE, TPD LIMIT	2328	2328	2328	2328	2328	2328
PHOSPHATE ROCK SLURRY, TPH	476.37	476.37	476.37	469.62	467.97	467.83
100 % SULFURIC ACID, TPH	247.16	245.88	248.09	241.28	241.57	242.68
WATER, TPH	18.99	18.99	18.99	18.99	18.96	18.97
LBS F/TON OF P2O5 (INPUT)	0.003	0.003	0.002	0.002	0.003	0.002
LBS F/TON OF P2O5 LIMIT	0.02	0.02	0.02	0.02	0.02	0.02

## EMISSION CALCULATIONS

Date: June 7, 1999

Unit: B PAP

Run no. 1

$$\begin{aligned} V_{wstd} &= 0.04707 \text{ Cuft/ml} \times (v1) \\ &= 0.04707 \text{ Cuft/ml} \times 60.4 \text{ ml} \\ &= \mathbf{2.843 \text{ Cuft.}} \end{aligned}$$

$$\begin{aligned} V_{mstd} &= V_m \left[ \frac{T_{std}}{T_m + 460} \right] \left[ \frac{P_{bar} + (H / 13.6)}{P_{std}} \right] Y_i \\ &= 42.476 \text{ Cuft} \times \left[ \frac{528}{460 + 90.3} \right] \times \left[ \frac{(30.02 + (2.62 / 13.6))}{29.92} \right] \times 1.00 \\ &= \mathbf{41.153 \text{ Cuft.}} \end{aligned}$$

$$\begin{aligned} B_{wo} &= \frac{V_{wstd}}{V_{wstd} + V_{mstd}} \\ &= \frac{2.843}{2.843 + 41.153} \times 100 \\ &= \mathbf{6.46 \%} \end{aligned}$$

$$\begin{aligned} M_s &= M_d (1 - B_{wo}) + 18 (B_{wo}) \\ &= 28.85 \times (1 - 0.0646) + 18 \times 0.0646 \\ &= \mathbf{28.15} \end{aligned}$$

$$\begin{aligned} V_s (\text{avg}) &= K_p C_p \sqrt{P(\text{avg})} \sqrt{(460 + T_s) / (M_s P_s)} \\ &= 85.48 \times .84 \times 0.7040 \sqrt{(460 + 112.1) / (28.15 \times 30.09)} \\ &= \mathbf{41.54 \text{ ft/sec}} \end{aligned}$$

$$\begin{aligned} Q_s &= 60 (1 - B_{wo}) V_s A_s (T_{std} / T_s) (P_s / P_{std}) \\ &= 60 (1 - 0.0646) \times 41.54 \times 12.566 \times (528 / (460 + 112.1)) \times (30.09 / 29.92) \\ &= \mathbf{27,194 \text{ scfm}} \end{aligned}$$



$$\begin{aligned}
Cs &= 0.0154 \text{ grs/mg} \times (\text{total mg of sample}) / Vmstd \\
&= 0.0154 \text{ grs/mg} \times 2.81 \text{ mg} / 41.153 \text{ cuft} \\
&= 0.0011 \text{ grs/cuft}
\end{aligned}$$

$$\begin{aligned}
\text{lbs/hr} &= (Cs \times Qs \times 60 \text{ min/hr}) / 7000 \text{ grs/lb} \\
&= (0.0011 \times 27194 \times 60) / 7000 \\
&= 0.25 \text{ lbs/hr Fluoride}
\end{aligned}$$

$$\begin{aligned}
\text{lbs/day} &= \text{lbs/hr} \times 24 \text{ hrs/day} \\
&= 0.25 \times 24 \\
&= 5.88 \text{ lbs/day Fluoride}
\end{aligned}$$

Percent Isokinetic:

$$\begin{aligned}
I &= \frac{Ts (1.667) ((0.00267) V1) + (Vm / Tm) ((Pbar + (^H / 13.6)))}{0 Vs Ps An} \\
&= \frac{(460 + 112.1) (1.667) ((0.00267 \times 60.4) + (42.476 / (460 + 90.3))) \times ((30.02 + (2.62 / 13.6)))}{60 \times 41.54 \times 30.09 \times 0.000325} \\
&= 97.5 \%
\end{aligned}$$

## EMISSION CALCULATIONS

Date: June 8, 1999

Unit: B PAP

Run no. 4

$$\begin{aligned}V_{wstd} &= 0.04707 \text{ Cuft/ml} \times (v_1) \\ &= 0.04707 \text{ Cuft/ml} \times 65.9 \text{ ml} \\ &= \mathbf{3.102 \text{ Cuft.}}\end{aligned}$$

$$\begin{aligned}V_{mstd} &= V_m \left[ \frac{T_{std}}{T_m + 460} \right] \left[ \frac{P_{bar} + (H / 13.6)}{P_{std}} \right] Y_i \\ &= 42.175 \text{ Cuft} \times \left[ \frac{528}{460 + 91.3} \right] \times \left[ \frac{(29.96 + (2.62 / 13.6))}{29.92} \right] \times 1.00 \\ &= \mathbf{40.707 \text{ Cuft.}}\end{aligned}$$

$$\begin{aligned}B_{wo} &= \frac{V_{wstd}}{V_{wstd} + V_{mstd}} \\ &= \frac{3.102}{3.102 + 40.707} \times 100 \\ &= \mathbf{7.08 \%}\end{aligned}$$

$$\begin{aligned}M_s &= M_d (1 - B_{wo}) + 18 (B_{wo}) \\ &= 28.85 \times (1 - 0.0708) + 18 \times 0.0708 \\ &= \mathbf{28.08}\end{aligned}$$

$$\begin{aligned}V_s (\text{avg}) &= K_p C_p \sqrt{P(\text{avg}) (460 + T_s) / (M_s P_s)} \\ &= 85.48 \times .84 \times 0.6860 \sqrt{(460 + 112.1) / (28.08 \times 30.04)} \\ &= \mathbf{40.56 \text{ ft/sec}}\end{aligned}$$

$$\begin{aligned}Q_s &= 60 (1 - B_{wo}) V_s A_s (T_{std} / T_s) (P_s / P_{std}) \\ &= 60 (1 - 0.0708) \times 40.56 \times 12.566 \times (528 / (460 + 112.1)) \times (30.04 / 29.92) \\ &= \mathbf{26,333 \text{ scfm}}\end{aligned}$$

$$\begin{aligned}
Cs &= 0.0154 \text{ grs/mg} \times (\text{total mg of sample}) / Vmstd \\
&= 0.0154 \text{ grs/mg} \times 2.86 \text{ mg} / 40.707 \text{ cuft} \\
&= 0.0011 \text{ grs/cuft}
\end{aligned}$$

$$\begin{aligned}
\text{lbs/hr} &= (Cs \times Qs \times 60 \text{ min/hr}) / 7000 \text{ grs/lb} \\
&= (0.0011 \times 26333 \times 60) / 7000 \\
&= 0.24 \text{ lbs/hr Fluoride}
\end{aligned}$$

$$\begin{aligned}
\text{lbs/day} &= \text{lbs/hr} \times 24 \text{ hrs/day} \\
&= 0.24 \times 24 \\
&= 5.86 \text{ lbs/day Fluoride}
\end{aligned}$$

Percent Isokinetic:

$$\begin{aligned}
I &= \frac{Ts (1.667) ((0.00267) V1) + (Vm / Tm) ((Pbar + (^H / 13.6)))}{0 Vs Ps An} \\
&= \frac{(460 + 112.1) (1.667) ((0.00267 \times 65.9) + (42.175 / (460 + 91.3))) \times ((29.96 + (2.62 / 13.6)))}{60 \times 40.56 \times 30.04 \times 0.000325} \\
&= 99.6 \%
\end{aligned}$$

# Production Rate

DATE: 07-Jun-99

SAMPLING TIME FROM: 11:05 AM TO 6:00 PM

**STATEMENT OF PROCESS WEIGHT:**

COMPANY NAME: CF INDUSTRIES, INC. PLANT CITY PHOSPHATE COMPLEX  
 MAILING ADDRESS: P.O. DRAWER L PLANT CITY, FL 33564  
 SOURCE IDENTIFICATION: "B" PAP PRODUCTION FACILITY  
 SOURCE LOCATION: "B" PAP PRODUCTION STACK

PERMIT SOURCE: 0570005-007-AV  
 Emission Unit 009

**DATA ON OPERATING CYCLE TIME:**

START OF OPERATION, TIME  
 END OF OPERATION, TIME  
 ELAPSED TIME  
 IDLE TIME DURING CYCLE

	RUN #1	RUN #2	RUN #3	
START OF OPERATION, TIME	11:05 AM	3:12 PM	4:51 PM	
END OF OPERATION, TIME	12:17 PM	4:23 PM	6:00 PM	
ELAPSED TIME	72 MIN	71 MIN	69 MIN	
IDLE TIME DURING CYCLE	0	0	0	

**DESIGN PROCESS RATING:**

PROCESS WEIGHT RATE (INPUT) 773 TPH P2O5      PRODUCT (OUTPUT) \_\_\_\_\_ TPH

**DATA ON ACTUAL PROCESS RATE DURING OPERATION CYCLE:**

MATERIAL: PHOSPHATE ROCK, TPH P2O5  
 MATERIAL: 100 % SULFURIC ACID, TPH  
 MATERIAL: WATER, TPH

RUN #1	RUN #2	RUN #3
476.37	476.37	476.37
247.16	245.53	243.09
13.99	13.99	13.99

TOTAL PROCESS WEIGHT RATE:  
 PRODUCT: PHOSPHORIC ACID SLURRY, TPH  
 INPUT RATE: P2O5, TPH

RUN #1	RUN #2	RUN #3
742.52	741.24	743.45
96.50	96.50	96.50

I certify that the above statement is true to the best of my knowledge and belief:

Signature: *Fred Eng*

Title: Prod<sup>2</sup> Eng.

# Scrubber's Operating Parameters

DATE: 07-Jun-99

SAMPLING TIME FROM: 11:05 AM TO 6:00 PM

COMPANY NAME:  
MAILING ADDRESS:  
SOURCE IDENTIFICATION:  
SOURCE LOCATION:

CF INDUSTRIES, INC. PLANT CITY PHOSPHATE COMPLEX  
P.O. DRAWER L PLANT CITY, FL 33564  
"B" PAP PRODUCTION FACILITY  
"B" PAP PRODUCTION STACK

PERMIT SOURCE: 0570005-007-AV

TYPE OF SCRUBBER LIQUID:

Pond Water

PACKED BED SCRUBBER

	RUN #1	RUN #2	RUN #3	COMMENTS
START	11:05 AM	3:12 PM	4:51 PM	
END	12:17 PM	4:23 PM	6:00 PM	
AVERAGE	100'	102"	100"	
HIGH	100"	102"	100"	
LOW	100"	102"	100"	

OUTLET  
TEMPERATURES F

PACKED BED SCRUBBER

	RUN #1	RUN #2	RUN #3	COMMENTS
START	11:05 AM	3:12 PM	4:51 PM	
END	12:17 PM	4:23 PM	6:00 PM	
AVERAGE	151	177	151	
HIGH	151	177	151	
LOW	151	177	151	

FAN  
AMPS

I certify that the above statement is true to the best of my knowledge and belief:

Signature:

FE Sivamparan

Title:

Prod<sup>2</sup> Eng.

bpaprate.xls

# Production Rate

DATE: 08-Jun-99 SAMPLING TIME FROM: 10:40 AM TO 3:10 PM

**STATEMENT OF PROCESS WEIGHT:**

COMPANY NAME: CF INDUSTRIES, INC. PLANT CITY PHOSPHATE COMPLEX  
 MAILING ADDRESS: P.O. DRAWER L PLANT CITY, FL 33564  
 SOURCE IDENTIFICATION: "B" PAP PRODUCTION FACILITY  
 SOURCE LOCATION: "B" PAP PRODUCTION STACK

PERMIT SOURCE: 0570005-007-AV  
 Emission Unit 009

**DATA ON OPERATING CYCLE TIME:**

START OF OPERATION, TIME  
 END OF OPERATION, TIME  
 ELAPSED TIME  
 IDLE TIME DURING CYCLE

	RUN #1	RUN #2	RUN #3	
START OF OPERATION, TIME	10:40 AM	12:23 PM	2:00 PM	
END OF OPERATION, TIME	11:51 AM	1:35 PM	3:10 PM	
ELAPSED TIME	71 MIN	72 MIN	70 MIN	
IDLE TIME DURING CYCLE	0	0	0	

**DESIGN PROCESS RATING:**

PROCESS WEIGHT RATE (INPUT) 37.8 TPH P2O5 PRODUCT (OUTPUT) TPH

**DATA ON ACTUAL PROCESS RATE DURING OPERATION CYCLE:**

MATERIAL: PHOSPHATE ROCK, TPH P2O5  
 MATERIAL: 100 % SULFURIC ACID, TPH  
 MATERIAL: WATER, TPH

RUN #1	RUN #2	RUN #3
469.62	467.97	467.33
241.29	241.57	242.68
13.99	13.96	13.97

TOTAL PROCESS WEIGHT RATE:  
 PRODUCT: PHOSPHORIC ACID SLURRY, TPH  
 INPUT RATE: P2O5, TPH

RUN #1	RUN #2	RUN #3
729.39	728.50	729.43
96.50	96.33	96.42

I certify that the above statement is true to the best of my knowledge and belief:

Signature: J.E. Simpson  
 Title: Prod. Eng.

# Scrubber's Operating Parameters

DATE: 08-Jun-99

SAMPLING TIME FROM: 10:40 AM TO 3:10 PM

COMPANY NAME:  
MAILING ADDRESS:  
SOURCE IDENTIFICATION:  
SOURCE LOCATION:

CF INDUSTRIES, INC. PLANT CITY PHOSPHATE COMPLEX  
P.O. DRAWER L PLANT CITY, FL 33564  
"B" PAP PRODUCTION FACILITY  
"B" PAP PRODUCTION STACK

PERMIT SOURCE: 0570005-007-AV

TYPE OF SCRUBBER LIQUID:

Pond WATER

PACKED BED SCRUBBER

OUTLET  
TEMPERATURES F

	RUN #1	RUN #2	RUN #3	COMMENTS
START	10:40 AM	12:23 PM	2:00 PM	
END	11:51 AM	1:35 PM	3:10 PM	
AVERAGE	100°	101°	102°	
HIGH	100°	102°	102°	
LOW	100°	100°	102°	

PACKED BED SCRUBBER

FAN  
AMPS

	RUN #1	RUN #2	RUN #3	COMMENTS
START	10:40 AM	12:23 PM	2:00 PM	
END	11:51 AM	1:35 PM	3:10 PM	
AVERAGE	170	179.5	179	
HIGH	180	180	179	
LOW	170	179	179	

I certify that the above statement is true to the best of my knowledge and belief:

Signature:

FE Simpson

Title:

Prod. Eng

bpaprate.xls

APPENDIX "B"

FIELD DATA



## BEST AVAILABLE COPY

\*C0110

## METHOD 5 FIELD DATA

Run 1

Plant Site: Plant City, Fl.  
Sampling Location: B PapDate: 06/07/1999  
Stack ID (in): 48.00

Pt	Time min	Volume ft3	System Vacuum inHg	Delta P inH2O	Delta H inH2O	Ti °F	To °F	Ts °F	Tf °F	Tavg °F
1	5.0	2.958	1.28	0.353	2.093	81.44	81.82	106.14	240.75	58.30
2	10.0	6.779	1.94	0.600	2.901	83.00	82.73	112.14	242.33	59.24
3	15.0	10.793	2.10	0.649	3.123	85.10	84.26	113.33	242.27	61.90
4	20.0	14.518	1.86	0.558	2.780	87.19	85.98	113.22	241.01	61.55
5	25.0	18.067	1.69	0.498	2.584	89.04	87.66	113.41	244.46	63.45
6	30.0	21.171	1.38	0.383	2.237	90.48	89.16	112.53	242.49	64.42
7	35.0	24.405	1.45	0.414	2.302	92.29	92.17	109.06	239.05	59.74
8	40.0	28.162	1.84	0.551	2.779	93.61	92.83	112.46	240.17	55.74
9	45.0	32.093	1.98	0.603	2.981	95.12	93.87	113.61	243.29	56.14
10	50.0	35.872	1.86	0.553	2.801	96.49	94.93	113.49	244.29	56.56
11	55.0	39.651	1.87	0.555	2.811	97.57	95.94	113.39	242.06	57.09
12	60.0	42.476	1.21	0.305	2.055	98.34	96.92	112.95	243.21	58.73

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†C011©

METHOD 5 FIELD DATA

Run 2

Plant Site: Plant City Fla  
 Sampling Location: B Pap

Date: 06/07/1999  
 Stack ID (in): 48.00

Pt	Time min	Volume ft <sup>3</sup>	System Vacuum inHg	Delta P inH <sub>2</sub> O	Delta H inH <sub>2</sub> O	Ti °F	To °F	Ts °F	Tf °F	Tm °F
1	5.0	2.810	1.20	0.350	1.961	96.91	97.31	108.77	242.64	78.00
2	10.0	6.471	1.87	0.517	2.586	96.89	97.39	114.19	243.20	61.12
3	15.0	10.331	2.07	0.575	2.822	97.61	97.64	114.78	243.47	61.78
4	20.0	13.978	1.89	0.511	2.599	98.55	98.13	114.51	240.82	57.00
5	25.0	17.292	1.62	0.420	2.317	99.25	98.60	114.20	242.33	57.00
6	30.0	20.231	1.36	0.331	2.072	99.60	98.90	113.63	244.13	58.00
7	35.0	22.976	1.19	0.287	1.930	99.15	99.08	107.05	242.43	64.10
8	40.0	26.466	1.76	0.468	2.436	99.20	99.01	112.57	244.40	59.62
9	45.0	30.228	2.00	0.543	2.699	99.72	99.17	113.54	242.52	61.20
10	50.0	33.821	1.86	0.492	2.526	100.30	99.46	113.50	243.66	62.68
11	55.0	37.389	1.85	0.486	2.510	100.92	99.89	113.79	244.10	63.54
12	60.0	40.183	1.29	0.294	1.972	101.41	100.47	113.42	244.55	65.21

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METHOD 5 FIELD DATA

RUN 3

Plant Site: Plant City Fla  
 Sampling Location: BPap

Date: 06/07/1999  
 Stack ID (in): 48.00

Pt	Time min	Volume ft3	System Vacuum inHg	Delta P inH2O	Delta H inH2O	Ti °F	To °F	Ts °F	Tf °F	Temp °F
1	5.0	3.022	1.29	0.349	2.095	100.70	100.47	106.97	236.42	66.44
2	10.0	6.633	1.73	0.499	2.559	100.89	100.33	113.04	243.18	61.26
3	15.0	10.481	1.93	0.563	2.806	101.54	100.57	113.95	242.01	62.21
4	20.0	14.077	1.74	0.491	2.544	102.04	100.84	113.82	241.00	61.79
5	25.0	17.378	1.52	0.416	2.291	102.18	101.01	113.72	243.97	60.40
6	30.0	20.270	1.25	0.316	2.016	102.11	101.08	113.23	242.56	59.43
7	35.0	22.756	1.02	0.233	1.772	100.89	100.72	108.47	241.69	66.94
8	40.0	26.244	1.66	0.465	2.418	100.61	100.39	112.40	241.66	60.84
9	45.0	29.982	1.87	0.534	2.657	100.75	100.18	113.15	244.01	60.97
10	50.0	33.534	1.74	0.479	2.472	101.04	100.16	113.00	243.04	61.46
11	55.0	37.103	1.76	0.485	2.498	101.19	100.24	113.33	242.96	61.29
12	60.0	39.824	1.21	0.279	1.912	101.17	100.31	112.66	242.79	63.28

†C0110

METHOD 5 FIELD DATA

*Rw4*

Plant Site: Plant City, FL  
Sampling Location: B PAP

Date: 06/08/1999  
Stack ID (in): 48.00

Pt	Time	Volume	System Vacuum	Delta P	Delta H	Ti	To	Ts	Tf	Timp
	min	ft3	inHg	inH2O	inH2O	°F	°F	°F	°F	°F
1	5.0	3.135	1.53	0.385	2.224	82.63	82.92	107.24	238.47	60.49
2	10.0	7.045	2.25	0.600	3.015	84.35	83.94	112.30	243.22	55.13
3	15.0	11.138	2.42	0.649	3.236	86.55	85.45	113.27	240.75	58.03
4	20.0	14.940	2.12	0.556	2.862	88.74	87.18	113.23	243.17	58.87
5	25.0	18.464	1.86	0.476	2.573	90.54	88.85	113.29	243.38	56.54
6	30.0	21.618	1.56	0.377	2.270	91.97	90.41	112.79	244.05	56.62
7	35.0	24.478	1.31	0.318	2.052	93.20	93.00	107.80	241.49	62.20
8	40.0	28.219	2.03	0.529	2.761	94.36	93.54	112.38	242.04	56.84
9	45.0	32.143	2.21	0.578	2.977	95.79	94.48	113.46	243.32	57.94
10	50.0	35.906	2.06	0.529	2.783	97.09	95.47	113.14	243.11	58.64
11	55.0	39.676	2.07	0.526	2.787	98.16	96.45	113.36	242.88	58.87
12	60.0	42.175	1.14	0.230	1.870	98.73	97.32	112.68	245.22	61.33

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4C0110

METHOD 5 FIELD DATA

RUNS

Plant Site: Plant City, FL  
 Sampling Location: B PAP

Date: 06/08/1999  
 Stack ID (in): 48.00

Pt	Time min	Volume ft3	System Vacuum inHg	Delta P inH2O	Delta H inH2O	Ti °F	To °F	Ts °F	Tf °F	Tavg °F
1	5.0	2.993	1.28	0.331	2.112	98.83	98.91	108.17	240.24	54.40
2	10.0	6.733	1.90	0.520	2.732	99.20	98.90	113.02	244.42	55.12
3	15.0	10.708	2.14	0.586	3.010	99.86	99.06	114.01	243.00	59.58
4	20.0	14.390	1.88	0.498	2.667	100.87	99.64	113.78	242.44	57.72
5	25.0	17.748	1.61	0.415	2.382	101.38	100.14	113.66	243.61	57.81
6	30.0	20.704	1.32	0.319	2.106	101.56	100.47	113.29	243.53	57.51
7	35.0	23.377	1.10	0.275	1.921	100.85	100.64	108.84	244.28	52.82
8	40.0	26.962	1.78	0.474	2.548	100.93	100.55	113.30	243.64	56.10
9	45.0	30.799	2.02	0.544	2.817	101.52	100.75	114.07	241.96	57.75
10	50.0	34.445	1.86	0.487	2.618	102.29	101.23	114.08	245.37	59.42
11	55.0	38.063	1.84	0.477	2.588	102.85	101.69	114.39	241.79	60.29
12	60.0	40.941	1.31	0.301	2.051	103.27	102.17	113.95	245.50	61.95

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\*C0110

METHOD 5 FIELD DATA

*Run 6*

Plant Site: Plant City, FL  
 Sampling Location: B PAP

Date: 06/08/1999  
 Stack ID (in): 48.00

Pt	Time min	Volume ft3	System Vacuum inHg	Delta P inH2O	Delta H inH2O	Ti °F	To °F	Ts °F	Tf °F	Temp °F
1	5.0	2.749	1.08	0.273	1.941	101.39	101.39	104.13	239.51	59.62
2	10.0	6.330	1.65	0.468	2.559	101.16	100.98	111.49	242.71	58.67
3	15.0	10.193	1.87	0.546	2.828	101.50	100.89	113.44	243.83	59.36
4	20.0	13.768	1.66	0.467	2.535	101.98	101.04	113.34	242.95	59.21
5	25.0	17.039	1.45	0.391	2.278	102.11	101.13	113.01	242.95	59.21
6	30.0	19.895	1.21	0.298	2.017	102.14	101.25	112.73	243.80	58.96
7	35.0	22.754	1.20	0.302	2.003	101.43	101.27	108.61	239.57	59.51
8	40.0	26.345	1.70	0.473	2.537	101.53	101.16	111.85	242.37	58.33
9	45.0	30.086	1.82	0.510	2.679	101.83	101.14	112.74	242.01	58.35
10	50.0	33.652	1.70	0.462	2.498	102.28	101.33	112.26	244.72	57.58
11	55.0	37.112	1.62	0.436	2.411	102.58	101.54	112.62	242.89	61.09
12	60.0	39.537	1.03	0.214	1.771	102.51	101.67	112.47	242.82	62.87

†C011©

METHOD 5 LEAK TEST DATA

Plant Site: Plant City, FL

Sampling Location: B PAP

Date: 06/07/1999

Stack ID: 009

---

Test	Leak Rate ft3/min	Sys Vac Pressure inHg	Initial Vol ft3	Final Vol ft3
6:00 PM 1 <i>EL</i>	0.01250	16.10	0.07200	0.08100
10:50 AM 1				
12:35 PM 2 <i>EL</i>	0.01390	5.48	42.49800	42.51200
2:00 PM 3 <i>EL</i>	0.01200	4.75	42.52300	42.54700
4:30 PM 4 <i>EL</i>	0.01200	5.45	40.20200	40.21700
4:45 PM 5 <i>EL</i>	0.01200	14.13	40.27100	41.54900
6:10 PM 6 <i>EL</i>	0.01200	5.47	39.84400	39.85800
7	0.00000	0.00	0.00000	0.00000
8	0.00000	0.00	0.00000	0.00000

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METHOD 5 LEAK TEST DATA

Plant Site: Plant City, FL

Sampling Location: B PAP

Date: 06/08/1999

Stack ID: 009

---

Test	Leak Rate ft3/min	Sys Vac Pressure inHg	Initial Vol ft3	Final Vol ft3
6/8/99 10:30 AM 1 <i>EL</i>	0.01200	16.00	0.08000	0.09400
11:03 AM 2 <i>EL</i>	0.01200	5.40	42.19400	42.20900
12:11 PM 3 <i>EL</i>	0.01200	4.80	42.22100	42.23400
1:45 PM 4 <i>EL</i>	0.01200	5.33	40.96100	40.98900
1:55 PM 5 <i>EL</i>	0.01200	4.83	41.00000	41.02700
3:20 PM 6 <i>EL</i>	0.01200	6.82	39.59300	39.61900
7	0.00000	0.00	0.00000	0.00000
8	0.00000	0.00	0.00000	0.00000



# CF INDUSTRIES, INC.

## PLANT CITY PHOSPHATE COMPLEX LABORATORY ANALYSIS RECORD

DATE	07-Jun-99
TIME	11:05 - 12:17
STACK	B PAP
RUN	#1

### MOISTURE CONTENTS

IMPINGER	#1	#2	#3	#4
WEIGHT AFTER RUN, GRAMS	707.7	700.3	583.3	884.0
WEIGHT BEFORE RUN, GRAMS	676.0	678.8	580.9	879.2
WEIGHT GAIN/LOSS, GRAMS	31.7	21.5	2.4	4.8
TOTAL WEIGHT GAIN, GRAMS	<u>60.4</u>			

### SAMPLE SOLUTIONS ANALYSIS

	F
VOLUME OF SAMPLE, ML	<u>1000</u>
CONCENTRATION, UG/ML	<u>2.81</u>
TOTAL WEIGHT POLLUTANT, MGS	<u>2.81</u>

ANALYST

*Lloyd B. Camp*

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# CF INDUSTRIES, INC.

## PLANT CITY PHOSPHATE COMPLEX LABORATORY ANALYSIS RECORD

DATE	<u>07-Jun-99</u>
TIME	<u>15:12 - 16:23</u>
STACK	<u>B PAP</u>
RUN	<u>#2</u>

### MOISTURE CONTENTS

IMPINGER	#1	#2	#3	#4
WEIGHT AFTER RUN, GRAMS	717.1	669.9	580.7	876.0
WEIGHT BEFORE RUN, GRAMS	<u>672.1</u>	<u>660.8</u>	<u>579.4</u>	<u>870.4</u>
WEIGHT GAIN/LOSS, GRAMS	<u>45.0</u>	<u>9.1</u>	<u>1.3</u>	<u>5.6</u>
TOTAL WEIGHT GAIN, GRAMS	<u>61.0</u>			

### SAMPLE SOLUTIONS ANALYSIS

	F
VOLUME OF SAMPLE, ML	<u>1000</u>
CONCENTRATION, UG/ML	<u>2.88</u>
TOTAL WEIGHT POLLUTANT, MGS	<u>2.88</u>

ANALYST

Lloyd B. Camp

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CF INDUSTRIES, INC.

PLANT CITY PHOSPHATE COMPLEX  
LABORATORY ANALYSIS RECORD

DATE	07-Jul-99
TIME	16:51 - 18:00
STACK	8 FAP
RUN	78

MOISTURE CONTENTS

IMPINGER	#1	#2	#3	#4
WEIGHT AFTER RUN, GRAMS	712.5	667.9	588.7	385.5
WEIGHT BEFORE RUN, GRAMS	669.2	659.0	586.5	385.1
WEIGHT GAIN/LOSS, GRAMS	43.3	8.9	2.2	6.5
TOTAL WEIGHT GAIN, GRAMS	<u>60.9</u>			

SAMPLE SOLUTIONS ANALYSIS

	F
VOLUME OF SAMPLE, ML	<u>1000</u>
CONCENTRATION, UG/ML	<u>2.71</u>
TOTAL WEIGHT POLLUTANT, MGS	<u>2.71</u>

ANALYST Floyd B. Camp  
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CF INDUSTRIES, INC.

PLANT CITY PHOSPHATE COMPLEX  
LABORATORY ANALYSIS RECORD

DATE	<u>08-Jun-99</u>
TIME	<u>10:40 - 11:51</u>
STACK	<u>B PAP</u>
RUN	<u>54</u>

MOISTURE CONTENTS

IMPINGER	#1	#2	#3	#4
WEIGHT AFTER RUN, GRAMS	721.7	688.3	578.1	835.0
WEIGHT BEFORE RUN, GRAMS	676.0	677.8	576.0	827.4
WEIGHT GAIN/LOSS, GRAMS	45.7	10.5	2.1	7.6
TOTAL WEIGHT GAIN, GRAMS	<u>65.9</u>			

SAMPLE SOLUTIONS ANALYSIS

	F
VOLUME OF SAMPLE, ML	<u>1000</u>
CONCENTRATION, UG/ML	<u>2.86</u>
TOTAL WEIGHT POLLUTANT, MGS	<u>2.86</u>

ANALYST Floyd B. Camp  
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# CF INDUSTRIES, INC.

## PLANT CITY PHOSPHATE COMPLEX LABORATORY ANALYSIS RECORD

DATE	08-Jun-99
TIME	12:23 - 13:35
STACK	B PAP
RUN	#5

### MOISTURE CONTENTS

IMPINGER	#1	#2	#3	#4
WEIGHT AFTER RUN, GRAMS	715.7	668.5	580.8	880.2
WEIGHT BEFORE RUN, GRAMS	670.8	658.7	579.0	872.2
WEIGHT GAIN/LOSS, GRAMS	44.9	9.8	1.8	8.0
TOTAL WEIGHT GAIN, GRAMS	<u>64.5</u>			

### SAMPLE SOLUTIONS ANALYSIS

	F
VOLUME OF SAMPLE, ML	1000
CONCENTRATION, UG/ML	3.01
TOTAL WEIGHT POLLUTANT, MGS	3.01

ANALYST Floyd B. Camp  
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# CF INDUSTRIES, INC.

## PLANT CITY PHOSPHATE COMPLEX LABORATORY ANALYSIS RECORD

DATE	<u>08-Jun-99</u>
TIME	<u>14:00 - 15:10</u>
STACK	<u>B PAP</u>
RUN	<u>#6</u>

### MOISTURE CONTENTS

IMPINGER	#1	#2	#3	#4
WEIGHT AFTER RUN, GRAMS	713.4	667.8	587.3	870.1
WEIGHT BEFORE RUN, GRAMS	<u>668.9</u>	<u>658.7</u>	<u>586.5</u>	<u>864.2</u>
WEIGHT GAIN/LOSS, GRAMS	<u>44.5</u>	<u>9.1</u>	<u>0.8</u>	<u>5.9</u>
TOTAL WEIGHT GAIN, GRAMS	<u>60.3</u>			

### SAMPLE SOLUTIONS ANALYSIS

	F
VOLUME OF SAMPLE, ML	<u>1000</u>
CONCENTRATION, UG/ML	<u>2.70</u>
TOTAL WEIGHT POLLUTANT, MGS	<u>2.70</u>

ANALYST

Thay D. Camp

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padcomp.xls

**BEST AVAILABLE COPY**  
**VISIBLE EMISSION OBSERVATION FORM**

COMPANY NAME  
*CF Industries, Inc. Plant City Complex*

STREET ADDRESS  
*10608 Paul Buchman Highway*  
*10 miles north of Plant City*

CITY *Plant City* STATE *FL* ZIP *33564*

PHONE (KEY CONTACT) *(813) 782-1591 (Ext. 290)* SOURCE ID NUMBER *0570005 009*

OBSERVATION DATE <i>6/3/99</i>		START TIME <i>1350</i>			
SEC	0	15	30	45	
MIN					
1	0	0	0	0	
2	0	0	0	0	
3	0	0	0	0	
4	0	0	0	0	
5	0	0	0	0	
6	0	0	0	0	
7	0	0	0	0	
8	0	0	0	0	
9	0	0	0	0	
10	0	0	0	0	
11	0	0	0	0	
12	0	0	0	0	
13	0	0	0	0	
14	0	0	0	0	
15	0	0	0	0	
16	0	0	0	0	
17	0	0	0	0	
18	0	0	0	0	
19	0	0	0	0	
20	0	0	0	0	
21	0	0	0	0	
22	0	0	0	0	
23	0	0	0	0	
24	0	0	0	0	
25	0	0	0	0	
26	0	0	0	0	
27	0	0	0	0	
28	0	0	0	0	
29	0	0	0	0	
30	0	0	0	0	

PROCESS EQUIPMENT *3 Phosphoric Acid Production Facility* OPERATING MODE *Normal*

CONTROL EQUIPMENT *North American steel packed bed scrubber with Kimre packing or equivalent* OPERATING MODE *Normal*

DESCRIBE EMISSION POINT  
*Circular stack opening 4 feet in diameter*

HEIGHT ABOVE GROUND LEVEL *~108.5'* HEIGHT RELATIVE TO OBSERVER  
Start *~108.5'* End *~108.5'*

DISTANCE FROM OBSERVER Start *~275'* End *~275'* DIRECTION FROM OBSERVER  
Start *NE* End *NE*

DESCRIBE EMISSIONS  
Start *None* End *None*

EMISSION COLOR Start *NA* End *NA* IF WATER DROPLET PLUME  
Attached  Detached

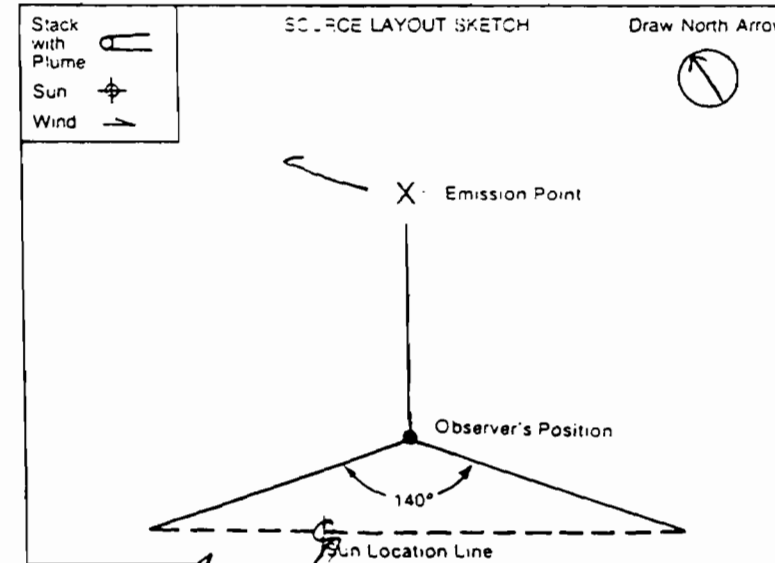
POINT IN THE PLUME AT WHICH OPACITY WAS DETERMINED  
Start *~4' from stack* End *~4' from stack*

DESCRIBE PLUME BACKGROUND  
Start *Scattered sky* End *Scattered sky*

BACKGROUND COLOR *Blue, gray* SKY CONDITIONS  
Start *Blue, gray, white* End *white* Start *Scattered* End *Scattered*

WIND SPEED Start *2-6 mph* End *4-8 mph* WIND DIRECTION  
Start *E* End *SE*

AMBIENT TEMP Start *83°F* End *85°F* WET BULB TEMP RH, percent  
Start *65%*



OBSERVER'S NAME (PRINT) *Lloyd G. Camp*

OBSERVER'S SIGNATURE *Lloyd G. Camp* *3/99*

ORGANIZATION *CF Industries, Inc. Plant City Complex*

CERTIFIED BY *Eastern Technical Associates* *2/24/99*

ADDITIONAL INFORMATION  
*David J. Jelle*  
*Chief Chemist*

# BEST AVAILABLE COPY

## VISIBLE EMISSION OBSERVATION FORM

No. 2

COMPANY NAME  
*CF Industries, Inc. Plant City Complex*

STREET ADDRESS  
*10608 Paul Buchman Highway*

*10 miles north of Plant City*

CITY STATE ZIP  
*Plant City FL 33564*

PHONE (KEY CONTACT) SOURCE ID NUMBER  
*(813) 782-1591 (Ext. 290) 0570005 009*

PROCESS EQUIPMENT *B Phosphoric Acid Production Facility* OPERATING MODE *Normal*

CONTROL EQUIPMENT *North American steel packed bed scrubber with kinetic packing or equivalent* OPERATING MODE *Normal*

DESCRIBE EMISSION POINT  
*Circular stack opening 4 Feet in diameter*

HEIGHT ABOVE GROUND LEVEL *~108.5'* HEIGHT RELATIVE TO OBSERVER  
Start *~108.5'* End *~108.5'*

DISTANCE FROM OBSERVER *Start ~275' End ~275'* DIRECTION FROM OBSERVER  
Start *NE* End *NE*

DESCRIBE EMISSIONS  
Start *None* End *None*

EMISSION COLOR *Start NA End NA* IF WATER DROPLET PLUME  
Attached  Detached

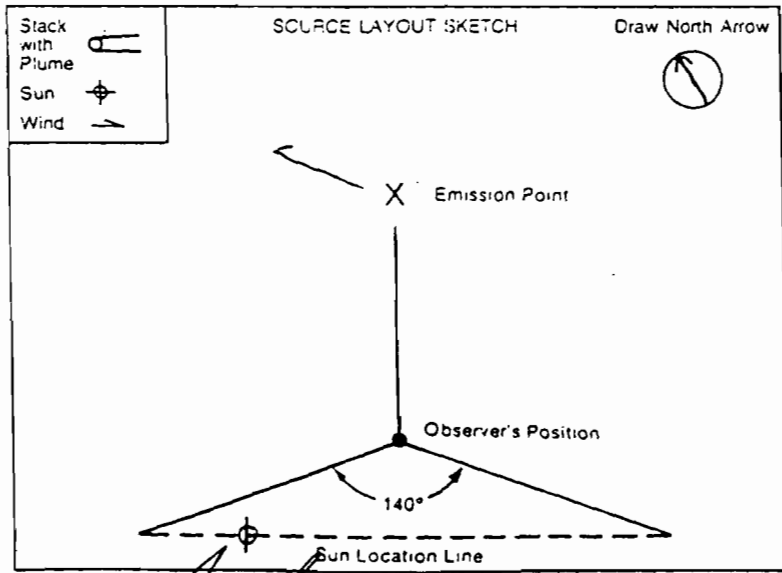
POINT IN THE PLUME AT WHICH OPACITY WAS DETERMINED  
Start *~4' from stack* End *~4' from stack*

DESCRIBE PLUME BACKGROUND  
Start *Scattered sky* End *Scattered sky*

BACKGROUND COLOR *Blue, gray, white* SKY CONDITIONS  
Start *Blue, gray, white* End *white* Start *Scattered* End *Scattered!*

WIND SPEED *Start ~5 mph End ~10 mph* WIND DIRECTION  
Start *SE* End *E*

AMBIENT TEMP *Start 87°F End 90°F* WET BULB TEMP *64* RH. percent



SEC MIN	OBSERVATION DATE <i>6/3/99</i>				START TIME <i>1420</i>		END TIME <i>1450</i>
	0	15	30	45			
1	0	0	0	0			
2	0	0	0	0			
3	0	0	0	0			
4	0	0	0	0			
5	0	0	0	0			
6	0	0	0	0			
7	0	0	0	0			
8	0	0	0	0			
9	0	0	0	0			
10	0	0	0	0			
11	0	0	0	0			
12	0	0	0	0			
13	0	0	0	0			
14	0	0	0	0			
15	0	0	0	0			
16	0	0	0	0			
17	0	0	0	0			
18	0	0	0	0			
19	0	0	0	0			
20	0	0	0	0			
21	0	0	0	0			
22	0	0	0	0			
23	0	0	0	0			
24	0	0	0	0			
25	0	0	0	0			
26	0	0	0	0			
27	0	0	0	0			
28	0	0	0	0			
29	0	0	0	0			
30	0	0	0	0			

OBSERVER'S NAME (PRINT)  
*Lloyd G. Camp*

OBSERVER'S SIGNATURE *Lloyd G. Camp* DATE *6/3/99*

ORGANIZATION  
*CF Industries, Inc. Plant City Complex*

CERTIFIED BY *Eastern Technical Associates* DATE *2/24/99*

ADDITIONAL INFORMATION  
*Harvest Fall*  
*Cheryl*



# SAMPLE CHAIN OF CUSTODY

Plant Name CF INDUSTRIES, INC. PLANT CITY PHOSPHATE COMPLEX

Source Identification "B" PHOSPHORIC ACID PRODUCTION FACILITY

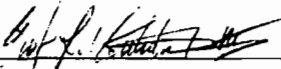
Date Sampled: JUNE 7, 1999 Sampling Time: 11:05 AM to 6:00 PM

Test for MOISTURE AND FLUORIDE

## SAMPLE RECOVERY

Sample Run	Description
1	#1 COLD BOX ASSEMBLY
2	#2 COLD BOX ASSEMBLY
3	#3 COLD BOX ASSEMBLY


Person engaged in sample recoveries:

Signature 

Title ANALYST II

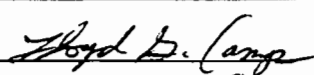
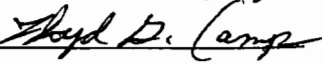
Location at which recovery "B" PHOSPHORIC ACID STACK

Laboratory person receiving samples:

Signature 

Title "A" CLASS TECHNICIAN

## ANALYSIS

Constituent	Method	Date	Time	Signature(s)
MOISTURE	EPA METHOD 4	6/7/99	12:47 - 18:30	
FLUORIDE	EPA METHOD 13 B	6/7/99	13:10 - 19:15	

# SAMPLE CHAIN OF CUSTODY

Plant Name CF INDUSTRIES, INC. PLANT CITY PHOSPHATE COMPLEX

Source Identification "B" PHOSPHORIC ACID PRODUCTION FACILITY

Date Sampled: JUNE 8, 1999 Sampling Time: 10:40 AM to 3:10 PM

Test for MOISTURE AND FLUORIDE

## SAMPLE RECOVERY

<u>Sample Run</u>	<u>Description</u>
<u>1</u>	<u>#1 COLD BOX ASSEMBLY</u>
<u>2</u>	<u>#2 COLD BOX ASSEMBLY</u>
<u>3</u>	<u>#3 COLD BOX ASSEMBLY</u>

Person engaged in sample recoveries:

Signature 

Title ANALYST II

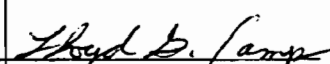

Location at which recovery "B" PHOSPHORIC ACID STACK

Laboratory person receiving samples:

Signature 

Title "A" CLASS TECHNICIAN

## ANALYSIS

<u>Constituent</u>	<u>Method</u>	<u>Date</u>	<u>Time</u>	<u>Signature(s)</u>
<u>MOISTURE</u>	<u>EPA METHOD 4</u>	<u>6/8/99</u>	<u>12:21 - 15:40</u>	<u></u>
<u>FLUORIDE</u>	<u>EPA METHOD 13 B</u>	<u>6/8/99</u>	<u>12:40 - 16:06</u>	<u></u>

# ANDERSEN

INSTRUMENTS INCORPORATED

DATE 7-14-98

TO WHOM IT MAY CONCERN:

THIS CERTIFIES THAT S-TYPE PITOT TUBES CONSTRUCTED AND CALIBRATED BY ANDERSEN INSTRUMENTS INC. COMPLY WITH PROCEDURES PROVIDED IN THE U.S. ENVIRONMENTAL PROTECTION AGENCY REFERENCE METHOD 2-DETERMINATION OF STACK GAS VELOCITY AND VOLUMETRIC FLOW RATE, VOL. 42, NO. 160 THURSDAY, AUGUST 18, 1977. ANDERSEN INSTRUMENTS INC. CERTIFIES THAT AT TIME OF SHIPMENT BASELINE COEFFICIENT VALUES OF 0.84 MAY BE ASSIGNED TO THE PITOT TUBES.

  
NATHAN D. CANUP  
SERVICE MANAGER

ANDERSEN INSTRUMENTS INC.  
A Subsidiary of Thermo Instruments Systems Inc.  
500 TECHNOLOGY COURT, SMYRNA, GA 30082-5211, USA  
TEL: 770 319 9999 - 800 241 6898 FAX: 770 319 0336

# CF INDUSTRIES

## TYPE S PITOT TUBE INSPECTION DATA FORM

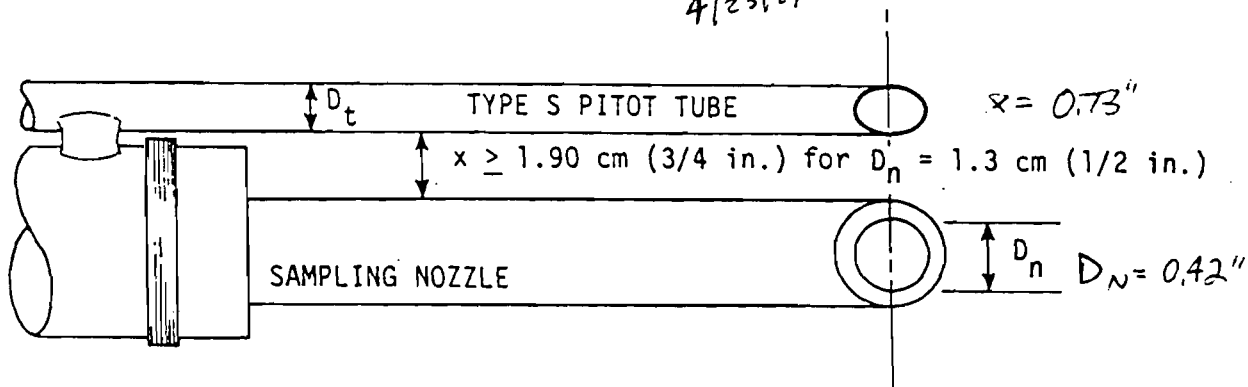
PROBE SS 45-1

MANUFACTURER ANDERSON INSTRUMENTS

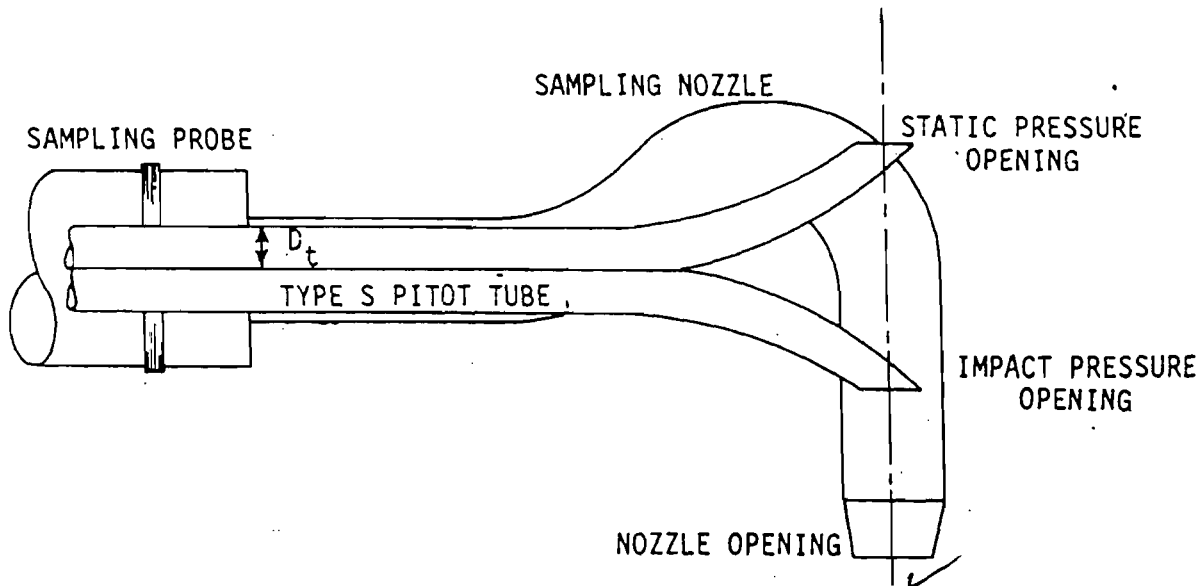
PROBE LENGTH 4.5'

DETACHABLE END PIECE SS N-01

*cut & kit  
4/23/79*



(a) BOTTOM VIEW: SHOWING MINIMUM PITOT-NOZZLE SEPARATION.



(b) SIDE VIEW: TO PREVENT PITOT TUBE FROM INTERFERING WITH GAS FLOW STREAMLINES APPROACHING THE NOZZLE, THE IMPACT PRESSURE OPENING PLANE OF THE PITOT TUBE SHALL BE EVEN WITH OR DOWNSTREAM FROM THE NOZZLE ENTRY PLANE

Figure 2.1 Required pitot tube-sampling nozzle configuration to prevent aerodynamic interference; buttonhook-type nozzle; centers of nozzle and pitot opening aligned; in respect to flow direction,  $D_t$  between 0.48 and 0.95 cm (3/16 and 3/8 in.).

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CF INDUSTRIES

TYPE S PITOT TUBE INSPECTION DATA FORM

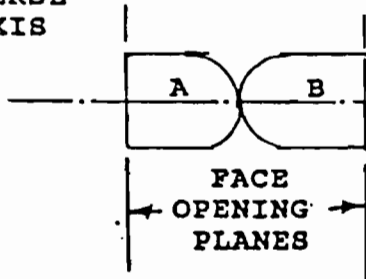
PROBE SS 45-1

MANUFACTURER ANDERSON INSTRUMENTS

PROBE LENGTH 4.5'

DETACHABLE END PIECE SS N-01

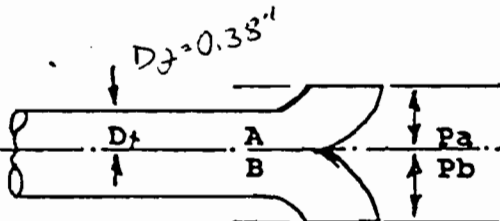
TRANSVERSE  
TUBE AXIS



(a)

A SIDE PLANE

LONGITUDINAL  
TUBE AXIS



B SIDE PLANE

(b)

$P_a = .63''$

Note:

$$1.05 D_t \leq P \leq 1.5 D_t$$

$$P_a = P_b$$

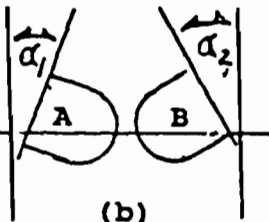
$P_o = .62''$

4/23/29  
Ed. ~~Ed.~~

(c)

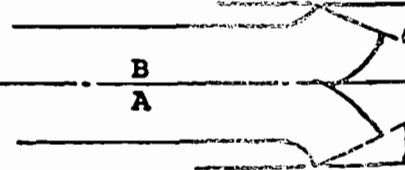
Figure 2.2 Properly constructed Type S pitot tube shown in: (a) end view: face opening planes perpendicular to transverse axis: (b) top view: face opening planes parallel to longitudinal axis: (c) side view: both legs of equal length and centerlines coincident, when viewed from both sides. Baseline coefficient values of 0.84 may be assigned to pitot tubes constructed this way.

TRANSVERSE  
TUBE AXIS



(b)

LONGITUDINAL  
TUBE AXIS



(a)



(c)



(d)

$\alpha_1$  1° Less than 10°  
 $\alpha_2$  1°  
 $Z$  < 1/32 Less than 0.32 cm  
 (1/8")

$\beta_1$  1° Less than 5°  
 $\beta_2$  1°  
 $w$  < 1/32° Less than 0.08 cm  
 (1/32")

# CF INDUSTRIES

## TYPE S PITOT TUBE INSPECTION DATA FORM

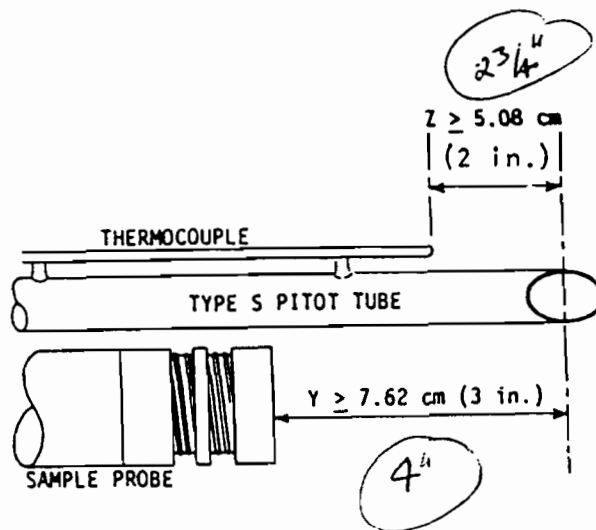
PROBE SS 45-1

MANUFACTURER ANDERSON INSTRUMENTS

PROBE LENGTH 4.5'

DETACHABLE END PIECE SS N-01

4/23/95 *[Signature]*



Required thermocouple and probe placement to prevent interference:  $D_t$  between 0.48 and 0.95 cm (3/16 and 3/8 in.).

CF INDUSTRIES, INC.  
Plant City Phosphate Complex  
LABORATORY ANALYSIS RECORD

"B" PAP Production Plant

June 7, 1999

CF Industries, Inc., Plant City Phosphate Complex, uses a Fischer Accumet Model 50 pH meter with selective ion concentration capacity. The instrument has microprocessor function which calculates efficiency of the Orion Model 96-09 fluoride electrode being used and alerts the user in case of electrode malfunction.

STANDARDS

ELECTRODE  
EFFICIENCY

(See Technical Information Section)

0.1  $\mu\text{g/ml}$

0.8981

1.0  $\mu\text{g/ml}$

0.9864

2.0  $\mu\text{g/ml}$

Quality Assurance Sample #1 - 0.38  $\mu\text{g/ml}$ .


Analysis was 0.37  $\mu\text{g/ml}$ .

Quality Assurance Sample #2 - 0.76  $\mu\text{g/ml}$ .

Analysis was 0.76  $\mu\text{g/ml}$ .

Quality Assurance Sample #3 - 1.90  $\mu\text{g/ml}$ .

Analysis was 1.90  $\mu\text{g/ml}$ .

  
J. Harold Falls  
Chief Chemist, Laboratory

JHF/gm  
9/89

CF INDUSTRIES, INC.  
Plant City Phosphate Complex  
LABORATORY ANALYSIS RECORD

"B" PAP Production Plant  
June 8, 1999

CF Industries, Inc., Plant City Phosphate Complex, uses a Fischer Accumet Model 50 pH meter with selective ion concentration capacity. The instrument has microprocessor function which calculates efficiency of the Orion Model 96-09 fluoride electrode being used and alerts the user in case of electrode malfunction.

STANDARDS

ELECTRODE  
EFFICIENCY

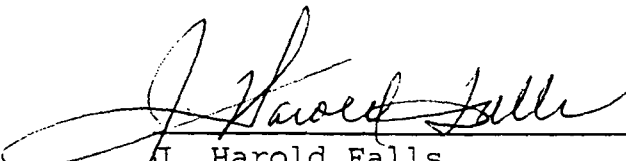
(See Technical Information Section)

0.1 $\mu\text{g/ml}$	0.8998
1.0 $\mu\text{g/ml}$	0.9780
2.0 $\mu\text{g/ml}$	

Quality Assurance Sample #1 - 0.38  $\mu\text{g/ml}$ .  
Analysis was 0.37  $\mu\text{g/ml}$ .

Quality Assurance Sample #2 - 0.76  $\mu\text{g/ml}$ .  
Analysis was 0.75  $\mu\text{g/ml}$ .

Quality Assurance Sample #3 - 1.90  $\mu\text{g/ml}$ .  
Analysis was 1.90  $\mu\text{g/ml}$ .

  
J. Harold Falls  
Chief Chemist, Laboratory

JHF/gm  
9/89



## Overview

The Model 50 is a state-of-the-art, microprocessor based meter designed for uniquely simple operation with an extensive range of capabilities. The sealed keypad incorporates both numeric and function keys, including a convenient Help function. The large liquid crystal display offers a simultaneous display of a variety of information, including measurement results, time/date, standardization data and status icons. The large display size permits user information to be conveyed in simple, complete sentences—not the cryptic prompts more typical for laboratory meters.

The Model 50 includes dual input channels. A novel split-screen action allows the display to simultaneously track both inputs when desired. In addition to pH and millivolt measurement, this model also performs analyses with ion selective electrodes by direct potentiometry. Additionally, the Model 50 offers four incremental methods: known addition and subtraction and alternate addition and subtraction.

In pH operation, the meter may be set up to automatically recognize both Fisher color-coded buffers and NIST buffers, for maximum user convenience. Auto-recognized buffers are both identified and corrected by the meter for the temperature dependence of the buffer.

The Model 50 performs conductivity measurements in Siemens (µhos) or salinity units. Probes with a variety of cell constants may be accommodated through software setup. Alternatively, the Model 50 may be set up to measure resistivity (ohms).

It is recommended that the user first complete the Installation instructions, then become familiar with Controls and Connectors, and finally review the Operation sections for procedures of interest.

# Performance Characteristics

	Model 50
Ranges	-2 to 20 pH/pX -1800 to 1800 mV -5 to 105 °C 10 <sup>-9</sup> to 10 <sup>9</sup> Conc 0 to 40 ppt practical salinity 0 to 70 ppt NaCl equivalents 3 x 10 <sup>4</sup> μ-Siemens/cm 33 to ∞ Ω-cm
Resolution	0.1/0.01/0.001 pH 0.1 mV 0.1 °C 1, 2 or 3 significant figures ion 1, 2 or 3 significant figures conductivity
Relative Accuracy	+/-0.002 pH +/-0.1 mV @ 25 °C +/-0.2 °C

## ***Ion Operation***

The Model 50 allows ion concentrations to be determined conveniently in any desired units of concentration, such as molarity, ppm or mg/L, and using any one of several techniques. Prior to analyzing samples by any of the ion methods, the operator should consult the following sections on *Method Selection, Low-Level Correction, Ionic Strength Adjustors and Temperature Compensation*.

## ***Method Selection***

The Model 50 features a variety of methods for measuring ion concentrations in samples using ion selective electrodes (ISE's). Direct reading potentiometric methods offer speed and convenience, are applicable to wide ranges of sample concentrations and require no volumetric measurements. Conversely, sample-to-sample variations in ionic strength frequently require the use of an ionic strength adjusting buffer (ISA) with direct reading potentiometry.

Incremental methods offer a tolerance for samples of varying ionic strength and the ability to analyze samples containing complexing agents. One incremental method, anate subtraction, can even permit analyzing concentrations of ions to which no ion selective electrode directly responds. Conversely, volumetric measurements of both the sample and a standard increment are required by these methods. Additionally, the incremental methods are generally unworkable if sample concentrations are expected to vary over more than one or, at most two, orders of magnitude.

As a general rule, it is usually simplest to select direct reading unless prior knowledge about the sample indicates that incremental methods are to be preferred.

## ***Low-Level Correction***

With samples containing very low levels of the ion of interest (often referred to as the "mud zone"), electrode response fails to conform to the Nernstian model. In the mud zone, changes in electrode output (slope) successively decrease as the sample concentration is further reduced. A plot of electrode output in millivolts versus logarithm of the sample concentration then becomes increasingly non-linear at very low concentrations.

The Model 50 offers two approaches to correcting for non-Nernstian response with low-level samples. In the first, the actual non-linear response curve of the electrode is approximated by a series of linear segments. Up to five different standards may be used, spanning the entire range of concentrations anticipated for samples. The meter then stores in memory a series of slope values corresponding to each successive pair of standards. These slopes, and the corresponding standard values, may be viewed individually by means of the slope key.

In linear segment measurements, the meter first identifies the general concentration range of the current sample, then computes its exact concentration by applying the nearest or bracketing standards. Use of the *Linear Segments* option can increase accuracy with dilute samples near the limits of the electrode's operating range.

The *Blank* feature provides an alternative means for measuring low-level samples. With this approach, the non-linear response curve of the electrode is fit by a mathematical model which assumes that all samples and standards have a constant background level of the species of interest. This situation may occur, for example, if the electrode can "self-sense" due to the finite solubility of the solid state sensing element. Standardization is performed with two standards from the electrode's linear region, as well as a blank sample. Measuring with the *Blank* option substantially enhances accuracy with dilute samples when the assumption of a constant background is true and a stable blank can be prepared.

---

## Ionic Strength Adjustors

Used directly, all selective ion electrodes respond to the *activity* of the ion of interest. The activity of an ion may be thought of as its effective concentration—a hybrid quantity derived from both the actual concentration of the ion as well as its mobility in the given solution.

In relatively dilute samples (typically less than 0.01 M), ions in the sample are relatively far removed from the influence of neighboring ions and act independently. In this event, ion activity and ion concentration are essentially identical. With more concentrated solutions, however, the presence of near neighbors acts to limit the mobility and effect of individual ions.

With increasing total ionic concentrations (ionic strength), ion activity becomes progressively diminished from actual ion concentration. This trend generally continues throughout the usable range of the electrode, although at extremely high concentrations, other effects may actually reverse it. In any event, in solutions of total ionic strength greater than perhaps 0.01 M, selective ion electrodes respond to an ion activity which may differ substantially from the ion concentration.

---

### Slope

The slope  $S$  of an electrode is defined as the change in its output voltage resulting from a decade change in the activity of the ion to which it responds. From the Nernst equation, the slope at any temperature  $T$  is given by

$$S_T = \xi (2.303 RT/F)$$

The quantity in the parentheses represents the slope for an ideal, monovalent, cation-sensing ISE (e.g., a pH or  $\text{Na}^+$  ion electrode), and has a value of 59.16 mV at 25 °C.

Because of their temperature dependence, the raw slope values do not provide a convenient measure of an electrode's performance. Consequently, slope values are usually mathematically corrected ("referenced") to a temperature of 25 °C:

$$S_{25} = S_T (298.16/T)$$

The value of its temperature referenced slope reflects the condition of an ISE since it may be compared simply and directly with the theoretical value of 59.16 at 25 °C. The Model 50 reports slope values temperature referenced to 25 °C.

---

### Efficiency Factor

Efficiency factor  $\xi$  is the actual slope value for an electrode, divided by its theoretical value. The efficiency factor for an electrode is thus easily interpretable in terms of its performance. For example, a pH electrode functioning ideally would exhibit an efficiency factor of exactly 1. Properly functioning, real pH electrodes typically will produce efficiency factors in the range of 0.90 to 1.05.

Efficiency factors for cation-sensing electrodes are positive, while those for anion-sensing electrodes are negative. Mathematically, the efficiency factor for an ideal electrode is always the reciprocal of the number of electrons exchanged in its electrode reaction, with the appropriate algebraic sign. Several examples appear in the table below:

ISE Type	Ideal Efficiency Factor
$\text{H}_3\text{O}^+$ (pH)	+ 1
$\text{F}^-$	- 1
$\text{Cl}^-$	- 1
$\text{Ca}^{+2}$	+ 0.5
$\text{S}^{-2}$	- 0.5

The efficiency factor for a real electrode, like its slope, may be determined experimentally from two-point (or more) standardization data.

---

### **Efficiency**

A related quantity, frequently used instead of efficiency factor, is electrode efficiency. The efficiency of an electrode is simply its efficiency factor expressed as a percent by multiplying by 100 and ignoring algebraic sign.

On this scale, properly functioning pH electrodes typically exhibit efficiencies between 90 and 105%. The Model 50 automatically compute and display electrode efficiencies, as well slopes temperature referenced to 25 °C, when the slope/eff key is pressed.

---

### **pH Measurements**

The pH of a solution is defined as

$$\text{pH} = -\log a_{\text{H}}$$

where  $a_{\text{H}}$  is the activity of the hydrogen ion in the solution. For hydrogen ions, the distinction between activity and concentration can usually be ignored.

Substituting the definitions of pH and slope into the Nernst equation, yields a working equation for computing sample pH:

$$E = E_0 + S_T \text{ pH}$$

In practice,  $E_0$  and  $S_T$  may be determined through standardization with buffers of known pH. The pH value of a sample then may be calculated from this equation and the measured output  $E$  of the electrode when placed in the sample.

---

### **Ion Measurements**

Ion measurements are complicated somewhat by the dependence of activity on the total ionic strength of the solution. For relatively dilute solutions, ion concentration and activity are essentially equivalent. However, to measure samples more concentrated than roughly 0.01 M, a special procedure is required to measure sample concentration directly.

**Section 1**

**INTRODUCTION**

**1.1 Principle of Operation**

The AST® Sampler is designed to sample gas stream effluents isokinetically in accordance with the U.S. Environmental Protection Agency (EPA) standards as outlined in the Code of Federal Regulations, Title 40, Part 60 (40CFR60), Appendix A. Stack gases are extracted through a nozzle and a heated probe into a heated filter chamber where the particulate is removed. The hot gases are then passed through a series of cooling impingers where condensibles are removed and the gases are cooled before going to the pump, dry gas meter, and orifice.

The AST® Sampler is manufactured with all the mechanical hardware specified in 40CFR60 for EPA Methods 1, 2, 4 and 5. The AST® Sampler can be used with Andersen hardware to sample additional EPA Methods including methods 6, 8, 12, 13A, 13B, 17, 23, 26A, 29, 101, 101A, 103, 104, 108, 202, 315. Consult the Graseby Technical Sales Department or your local sales representative for application notes.

P.O. Drawer L.  
 Plant City, Florida 33560-9007  
 Telephone: 813/782-1507



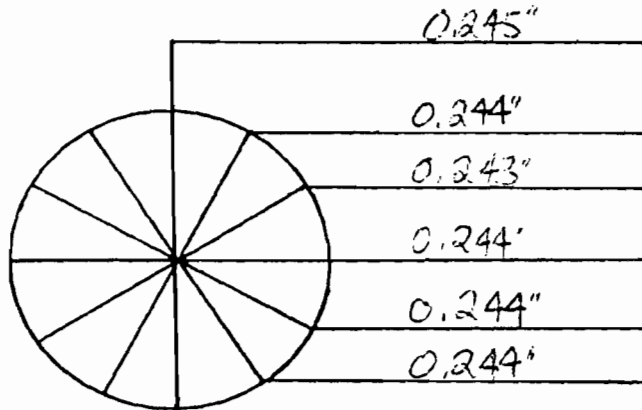
**CF Industries, Inc.**  
 Plant City Phosphate Complex

PROBE NOZZLE CALIBRATION DATA

Nozzle Identification Number: 250-1

Calibrated by: FORREST LEWIS-HAMAN

Date: 5/23/99



**Instructions:**

Measure to nearest 0.001"

**Tolerance:**

0.001" for mean of at least three readings.  
 Maximum deviation between readings  $\leq 0.004$ ".

Nozzle diameter,  $D_n$ : 0.244 In.

Nozzle area  $A_n$ : 0.000325 ft<sup>2</sup>

$$A_n = \frac{\pi}{144} \left( \frac{D_n}{2} \right)^2$$



**BEST AVAILABLE COPY**

Exhibit N

**ANNUAL GRASEBY STACKBOX THERMOCOUPLE CALIBRATIONS -UNIT #1200**

DATE 7/13/98

FOR TEMPERATURES 0 TO 110 DEGREES C FOR TEMPERATURES 110 TO 200 DEGREES C  
 NIST Traceable Thermometer # J96-258 NIST Traceable Thermometer # 90B-2024

Time: 1100-1530

Initial: *[Signature]*

Thermocouple		Ice Water Point			Ambient Point			Hot Water Point			Hot Oil Point		
		Thermocouple Reading (Degrees F)	NIST Reading		Thermocouple Reading (Degrees F)	NIST Reading		Thermocouple Reading (Degrees F)	NIST Reading		Thermocouple Reading (Degrees F)	NIST Reading	
			Actual	Con- version to		Actual	Con- version to		Actual	Con- version to		Actual	Con- version to
			Degrees			Degrees			Degrees			Degrees	
			C	F		C	F		C	F		C	F
[1] Stack	Probe 4.5 ft. #45-1	32.6	0.6	33.1	78.1	26.6	79.8	184.4	86.3	187.4	N/A	N/A	N/A
	Probe 6.0ft. #60-1	32.1	0.6	33.1	81.3	29.2	84.6	184.6	86.3	187.4	N/A	N/A	N/A
	Probe 10.5ft. #105-1	32.6	0.8	33.4	71.8	22.4	72.3	188.2	87.2	189.0	N/A	N/A	N/A
	Probe 11.0ft. #110-1	32.1	0.6	33.1	80.7	28.4	83.1	183.3	86.0	186.8	N/A	N/A	N/A
[2] Probe (Probe Liner Heater)	Probe 4.5 ft. #45-1	31.8	0.8	33.1	82.6	29.0	84.2	N/A	N/A	N/A	234.6	113.4	236.1
	Probe 6.0ft. #60-1	32.8	0.8	33.4	82.2	29.2	84.6	N/A	N/A	N/A	234.8	113.2	235.8
	Probe 10.5ft. #105-1	32.4	1.0	33.8	71.4	22.2	72.0	N/A	N/A	N/A	238.6	115.6	240.1
	Probe 11.0ft. #110-1	32.6	0.8	33.4	81.9	28.4	83.1	N/A	N/A	N/A	235.1	114.6	238.3
[3] Hot Box	Box	32.4	1.0	33.8	82.2	28.6	83.5	N/A	N/A	N/A	237.1	115.2	239.4
	Filter Exit	32.2	1.0	33.8	82.3	28.6	83.5	N/A	N/A	N/A	238.2	115.0	239.0
[4] Umbilical	Coldbox Exit	33.6	1.0	33.8	82.8	28.4	83.1	185.1	85.6	186.1	N/A	N/A	N/A
[5] DGM Inlet	Control Box	33.2	1.0	33.8	81.9	28.6	83.5	185.1	85.4	185.7	N/A	N/A	N/A
[6] DGM Exit	Control Box	33.2	1.0	33.8	82.5	28.6	83.5	185.1	85.4	185.7	N/A	N/A	N/A
[7] Spare	Ambient	32.8	0.2	33.8	82.1	28.6	83.5	185.1	85.2	185.4	N/A	N/A	N/A

NOTE:

10.5FT PROBE SENSOR REPAIRED & CALIBRATED 11/09 *11/09*

*4R*

ELK  
 10/19/98 11/13/98

# DRY GAS METER CALIBRATION

## Anderson AST Meter Box

Meter Box Number: 1200      Barometric Pressure: 30.03  
 Date: 12/16/98      Dry Gas Test Meter#: Rockwell 631105  
 Initial *Cal Y. Kautala*      Dry Gas AST Box Meter#: Schlumberger 1102

Flowrate Setting (CFM)	Gas Volume		Temperature		AST Box Meter Delta H (" H2O)	Time (Theta) min.	Actual Flowrate (CFM)	Yi (Software) (Setpoint)	Delta H@ in. H2O	
	DGM Test Meter (Vw) ft.^3	AST Box Meter (Vd) ft.^3	DGM Test Meter (Tw) Deg F	AST Box Meter (Td) Deg F						
0.40	11.660	11.697	69.6	71.8	0.736	28.85	0.404	1.0000	2.512	
0.50	7.500	7.556	69.6	74.2	1.152	14.83	0.506	1.0000	2.498	
0.60	10.358	10.470	70.2	76.7	1.625	17.20	0.602	1.0000	2.477	
0.70	31.644	32.310	70.2	82.3	2.232	45.40	0.697	1.0000	2.512	
0.80	19.097	19.557	70.2	84.6	2.658	24.25	0.788	1.0000	2.333	
0.90	14.301	14.684	70.7	86.1	3.237	16.18	0.884	1.0000	2.255	
1.00	16.701	17.123	73.0	87.8	3.937	17.15	0.974	1.0000	2.271	
1.10	7.302	7.491	73.0	88.3	4.722	6.87	1.063	1.0000	2.282	
1.20	32.996	34.085	73.0	92.2	5.472	28.7	1.150	1.0000	2.247	
								Average	1.0000	2.376
								Max. Diff.	0	0.136

$$Y_i = \frac{V_w P_b (t_d + 460)}{V_d (P_b + \Delta H/13.6) (T_w + 460)}$$

$$\Delta H@ = \frac{.0317 (\Delta H)}{P_b (t_d + 460)} [(t_w + 460) (\theta) / V_w]^2$$

Where: Vw = Gas Volume passing through the std test meter, ft.^3.  
 Vd = Gas Volume passing through the dry gas meter, ft.^3.  
 Tw = Temperature of the gas in the std test meter, deg. F.  
 Td = Average temperature of the gas in the dry gas meter, deg.F.  
 Delta H = Pressure differential across orifice. in, H2O.  
 Yi = Ratio of accuracy of std test meter to dry gas meter for each run.  
 Y = Average ratio of accuracy of std test meter to dry gas meter.  
 Pb = Barometric pressure, in. Hg.  
 Theta = Time of calibration run, min.

SOUTHERN ENVIRONMENTAL SCIENCES, INC.

WET TEST METER  
CALIBRATION CHECK

Wet Test Meter No. P-576					
Date: 3/29/98					
Checked by: B. Nelson					
TEST NO.	Gas Volume		Temperature		Cal Factor
	Liquid Displacement (Fc)	Wet Test Meter (Fc)	Liquid Displacement (°F)	Wet Test Meter (°F)	
1	1.115	1.10	78	78	1.020
2	1.090	1.10	78	78	.991
3	1.088	1.10	78	78	.989
Avg.					1.000

**Standard Dry Gas Meter Calibration**

GAS METER MANUF.	ROCKWELL	PERFORMED FOR	C.F. INDUSTRIES
MODEL #	175-S	DATE	2/12/99
SERIAL #	JA 631105	BAROMETRIC PRES.	30.22
WET TEST METER #	P - 576	LEAK CHECK	0.00 CFM at 15" Hg

Approximate Flowrate (CFM)	Gas Volume		Temperature		Dry Gas Meter Delta P (" H2O)	Time (Theta) (min)	Flowrate (CFM)	DRY GAS METER COEFF. (Yds)	AVG. GAS METER COEFF. (Yds)
	Wet Test Meter (Vw) (ft.^3)	Dry Gas Meter (Vd) (ft.^3)	Wet Test Meter (Tw) (Deg F)	Dry Gas Meter (Td) (Deg F)					
0.40	5.000	4.931	71.0	72.0	0.06	14.05	0.357	1.016	1.016
0.40	5.000	4.921	71.0	72.0	0.06	14.02	0.358	1.014	
0.40	5.000	4.905	71.0	72.0	0.06	14.04	0.358	1.017	
0.60	5.000	4.944	71.0	72.0	0.1	8.25	0.608	1.009	1.006
0.60	5.000	4.949	71.0	73.0	0.1	8.21	0.611	1.006	
0.60	5.000	4.931	71.0	73.0	0.1	8.18	0.614	1.010	
0.80	5.000	4.945	72.0	73.5	0.12	5.91	0.848	1.008	1.009
0.80	5.000	4.936	72.0	73.5	0.12	5.96	0.841	1.010	
0.80	5.000	4.942	72.0	73.5	0.12	5.97	0.839	1.009	
1.00	5.000	4.962	72.0	73.5	0.17	4.90	1.022	1.004	1.005
1.00	5.000	4.957	72.0	73.5	0.17	4.86	1.031	1.005	
1.00	5.000	4.962	72.0	73.5	0.17	4.86	1.031	1.004	
1.20	5.000	4.955	72.0	73.5	0.20	4.08	1.228	1.006	1.006
1.20	5.000	4.955	72.0	73.5	0.20	4.09	1.225	1.006	
1.20	5.000	4.953	72.0	73.5	0.20	4.09	1.225	1.006	

$$Q = \frac{P_b \times V_w \times 528}{(T_w + 460) \times \Theta \times 29.92}$$

$$Y_{ds} = \frac{V_w}{V_d} \times \frac{(T_d + 460)}{(T_w + 460)} \times \frac{P_b}{[P_b + (\Delta P / 13.6)]}$$

- where:
- Vw = Gas Volume passing through the std test meter, ft.^3.
  - Vd = Gas Volume passing through the dry gas meter, ft.^3
  - Tw = Temperature of the gas in the std test meter, deg. F.
  - Td = Average temperature of the gas in the dry gas meter, Deg F.
  - Delta H = Pressure differential across orifice, in. H2O.
  - Yds = Dry gas meter coefficient.
  - Pb = Barometric pressure, in. Hg.
  - Theta = Time of calibration run, min.

# STANDARD METER CALIBRATION CURVE

GAS METER MANUF. ROCKWELL	PERFORMED FOR C.F. INDUSTRIES
MODEL # 175-S	DATE 2/12/99
SERIAL # JA 631105	

### Regression Output:

Flowrate (CFM)	DRY GAS METER COEFF. (Yds)
0.358	1.016
0.611	1.008
0.843	1.009
1.028	1.005
1.226	1.006

Constant	72.47
Std Err of Y Est	0.18
R Squared	0.78
No. of Observations	5.00
Degrees of Freedom	3.00

X Coefficient(s)	-71.04
Std Err of Coef.	21.53

### CALIBRATION CURVE

FLOW (CFM)	CORRECTION FACTOR
0.42	1.014
0.45	1.014
0.50	1.013
0.55	1.012
0.60	1.012
0.65	1.011
0.70	1.010
0.75	1.010
0.80	1.009
0.85	1.008
0.90	1.007
0.95	1.007
1.00	1.006
1.05	1.005
1.10	1.005
1.15	1.004
1.20	1.003

**BEST AVAILABLE COPY**

POSTTEST DRY GAS METER CALIBRATION DATA FORM (English units)

Test numbers \_\_\_\_\_ Date 6/10/99 Meter box number 1200 Plant BPAD  
 Barometric pressure,  $P_b = 30.00$  in. Hg Dry gas meter number 1102 Pretest Y 1.000

Orifice manometer setting, ( $\Delta H$ ), in. H <sub>2</sub> O	Gas volume		Temperature			Time ( $\theta$ ), min	Vacuum setting, in. Hg	$Y_i$	$Y_i = \frac{V_w P_b (t_d + 460)}{V_d P_b + \frac{\Delta H}{13.6} (t_w + 460)}$	
	Dry test meter ( $V_w$ ), ft <sup>3</sup>	Dry gas meter ( $V_d$ ), ft <sup>3</sup>	Dry test meter ( $t_w$ ), °F	Dry gas meter						Average ( $t_d$ ), °F
				Inlet ( $t_{d,i}$ ), °F	Outlet ( $t_{d,o}$ ), °F					
<i>(.631 CFM)</i> 2.73	6.763	6.8085	73.4°	73.3°	73.3°	73.3°	10.00	2.4	0.9967	$\frac{(6.763)(30.00)(528.8)}{(6.8085)(30.20)(533.4)}$
2.73	6.772	6.8051	71.6°	71.9°	71.9°	71.9°	10.02	2.4	1.0040	$\frac{(6.772)(30.00)(534.9)}{(6.8051)(30.20)(531.6)}$
2.73	6.720	6.8090	71.2°	81.0°	81.0°	81.0°	10.00	2.4	0.9985	$\frac{(6.720)(30.00)(541.0)}{(6.809)(30.20)(531.2)}$
									$Y = 0.9997$	

<sup>a</sup> If there is only one thermometer on the dry gas meter, record the temperature under  $t_d$ .

$V_w$  = Gas volume passing through the wet test meter, ft<sup>3</sup>.

$V_d$  = Gas volume passing through the dry gas meter, ft<sup>3</sup>.

$t_w$  = Temperature of the gas in the wet test meter, °F.

$t_{d,i}$  = Temperature of the inlet gas of the dry gas meter, °F.

$t_{d,o}$  = Temperature of the outlet gas of the dry gas meter, °F.

$t_d$  = Average temperature of the gas in the dry gas meter, obtained by the average of  $t_{d,i}$  and  $t_{d,o}$ , °F.

$\Delta H$  = Pressure differential across orifice, in H<sub>2</sub>O.

$Y_i$  = Ratio of accuracy of wet test meter to dry gas meter for each run.

$Y$  = Average ratio of accuracy of wet test meter to dry gas meter for all three runs; tolerance = pretest Y  $\pm 0.05Y$

$P_b$  = Barometric pressure, in. Hg.

$\theta$  = Time of calibration run, min.

Dry test meter number Rockwell-JA631105

Quality Assurance Handbook M5-2.4A

*6/10/99 3:32 PM  
 within  $\pm 0.05Y$   
 but 4% tolerance*

APPENDIX "C"

PROJECT PARTICIPANTS

PROJECT PARTICIPANTS

CF INDUSTRIES, INC.

PLANT CITY PHOSPHATE COMPLEX

H.E. Morris	General Manager
R.C. May	Manager of Engineering
T.A. Edwards	Supt., Environmental Affairs
J.M. Messina	Chief of Environmental Affairs
J.H. Falls	Chief Chemist, Laboratory
J.I. Longest	Staff Chemist
T. Ortoski	Environmental Supervisor
E. Kretschmar	Analyst II
S. Willoughby	"A" Class Technician
L. Camp	"A" Class Technician
W. Cherry	"A" Class Technician



CF INDUSTRIES, INC.  
PLANT CITY PHOSPHATE COMPLEX  
COMPLIANCE TEST - B PAP  
PERMIT No. 0570005-007-AV  
EMISSION UNIT 009  
ATTACHMENT 1

813, 744-6100  
TAC cc: HEM  
QMM  
BCN  
RGR



Jeb Bush  
Governor

# Department of Environmental Protection

Southwest District  
3804 Coconut Palm Drive  
Tampa, Florida 33619

May 26, 1999

Mr. Thomas A. Edwards  
Superintendent, Environmental Affairs  
CF Industries, Inc.  
P.O. Drawer L  
Plant City, FL 33564-9007

Re: Compliance tests for A & B Phosphoric Acid Units, 0570005-007-AV

Dear Mr. Edwards:

This letter authorizes CF Industries, Inc., to temporarily operate A & B Phosphoric Acid Units at process rates approximately 10% beyond their current, maximum-permitted rates in order to conduct the annual compliance tests. Each unit's test must take no longer than 15 days (your letter indicates that each unit's test will take no longer than one week to complete), and each unit's production rate must be returned to the permitted range that existed before the test. Your estimates of the increases in emissions of fluoride indicate that existing limits will not be exceeded, even at the higher process rates. Test results at the temporary, higher rates will be used to support a subsequent application to modify the permit.

Notify the Hillsborough County Environmental Protection Commission of your schedule. If you have any questions, please contact Mr. Henry Gotsch, in our permitting division, at (813) 744-6100, ext. 113.

Sincerely,

FOR W.C. Thomas, P.E.,  
District Air Administrator  
Southwest District

cc: Mr. Rick Kirby, HCEPC

CF INDUSTRIES, INC.  
PLANT CITY PHOSPHATE COMPLEX  
COMPLIANCE TEST - B PAP  
PERMIT No. 0570005-007-AV  
EMISSION UNIT 009  
ATTACHMENT 2

PERMIT NO. 0570005-007-Av

EMISSION UNIT 009

CF INDUSTRIES, INC.

PLANT CITY PHOSPHATE COMPLEX

"B" PHOSPHORIC ACID PRODUCTION

PLANT CITY, FLORIDA

June 3 & 4, 1999

TEST CONDUCTED BY:

Laboratory  
CF INDUSTRIES, INC.  
Plant City Phosphate Complex  
Plant City, Florida 33564

## TABLE OF CONTENTS

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INTRODUCTION:

The Environmental Control Laboratory of CF Industries, Inc., Plant City Phosphate Complex, conducted an emission test at "B" Phosphoric Acid Production Facility in Plant City, Florida on June 3 and 4, 1999. Two (2) 60-minute test runs were performed. The purpose of the test was to obtain emission data demonstrating compliance with the State of Florida DEP performance standards.

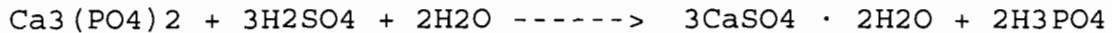
The measurements were made for fluoride and moisture at the stack outlet to the atmosphere. The measurements were within the permitted limits on all tests.

Complete results are give in APPENDIX "A".

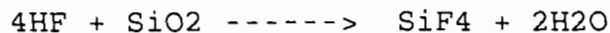
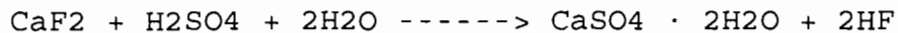
PROCESS DESCRIPTION

Phosphoric Acid is made by reacting sulfuric acid with phosphate rock along with a given amount of water to make an acid slurry. The mixing of sulfuric acid, rock and water takes place in a continuous reactor.

The principal reaction takes place as follows:



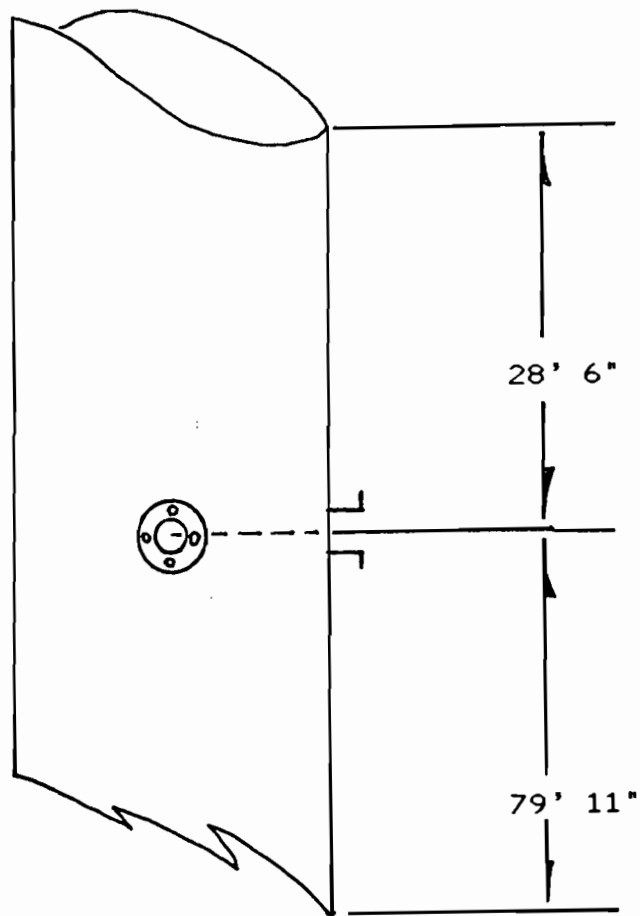
Other reactions as follows:



The resulting Phosphoric Acid will be 28 to 30% P2O5 content. This 28 to 30% P2O5 Phosphoric Acid solution will be further concentrated by evaporators until the acid strength reaches 52 to 54% P2O5.

## LOCATION OF SAMPLING POINTS

The sampling sites and number of traverse points were selected as per Figure 1-2 EPA Method 1 specified in 40 CFR 60, Appendix A.



Traverse Point Number	Distance from inside wall
1	2.1"
2	7.0"
3	14.2"
4	33.8"
5	41.0"
6	45.9"

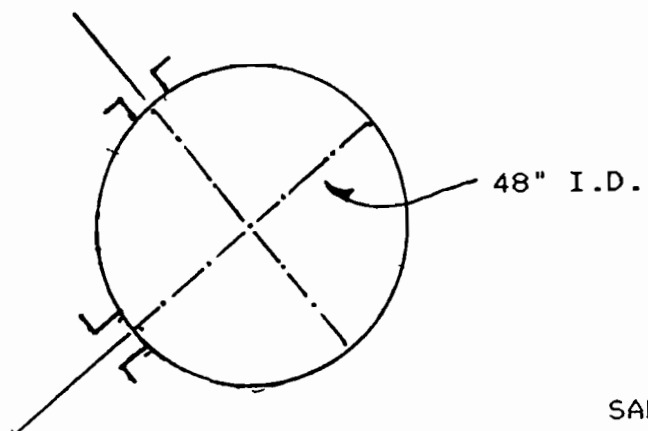


FIGURE 1

SAMPLE POINT DESCRIPTION

"B" PAP PRODUCTION



## SAMPLING AND ANALYTICAL PROCEDURES

The methods described in EPA Methods 1, 2, 3, 4, 9 and 13B contained in 40 CFR 60, Appendix A and adopted by reference in Chapter 62-297.401 F.A.C. are used when testing during compliance by CF Industries, Inc.

APPENDIX "A"

EMISSION CALCULATIONS AND RESULTS

# B PAP

Permit No. 0570005-007-AV  
Emission Unit 009

	1	1
RUN NUMBER		
DATE	03-Jun-99	04-Jun-99
TIME START	1:45 PM	10:33 AM
TIME END	2:55 PM	11:45 AM
BP, INCHES Hg	30.05	30.03
STACK PRESSURE, INCHES Hg	30.10	30.09
AVG.SQ.ROOT(VEL. HEAD) IN Hg	0.6650	0.6550
ORIFICE PRESS. OF METER, IN WATER	2.5400	2.4400
AVG STACK ,F	126.5	120.5
STACK, DRY BULB	126.5	120.5
METER TEMPERATURE, F	101.5	97.8
VOL. OF GAS, DM CONDITIONS, FT3	40.714	39.777
VOL. GAS, STP, DRY COND. FT3	38.690	38.016
STACK GAS MOISTURE, % VOLUME	10.23	8.81
MW OF STACK GAS, DRY COND.	28.85	28.85
MW OF STACK GAS, STACK COND.	27.74	27.89
PITOT CORRECTION FACTOR	0.84	0.84
STACK GAS VELOCITY, STACK COND. FT3/SEC	40.02	39.11
STACK AREA, FT2	12.566	12.566
EFFECTIVE STACK AREA, FT2	12.566	12.566
STACK GAS FLOW-RATE AT STP, SCFMD	24530	24599
NET TIME OF TEST, MINUTES	60	60
SAMPLE NOZZLE AREA, FT2	0.000325	0.000325
PERCENT ISOKINETIC	101.7	99.6
FLUORIDE, MG.	6.44	4.40
FLUORIDE, LB/HR	0.54	0.38
FLUORIDE, LB/DAY	12.94	9.02
FLUORIDE, LB/HR. LIMIT	1.04	1.04
FLUORIDE, LB/DAY LIMIT	24.9	24.9
PRODUCTION RATE, TPH P2O5 INPUT	96.8	86.3
PRODUCTION RATE, TPH LIMIT	97.0	87.8
PRODUCTION RATE, TPD P2O5 INPUT	2323	2071
PRODUCTION RATE, TPD LIMIT	2328	2107
PHOSPHATE ROCK SLURRY, TPH	478.74	437.02
100 % SULFURIC ACID, TPH	258.02	232.64
WATER, TPH	19.04	16.97
LBS F/TON OF P2O5 (INPUT)	0.006	0.004
LBS F/TON OF P2O5 LIMIT	0.02	0.02
VISIBLE EMISSIONS	0%	
VISIBLE EMISSIONS LIMIT	20%	

## EMISSION CALCULATIONS

Date: June 3, 1999

Unit: B PAP

Run no. 1

$$\begin{aligned}V_{wstd} &= 0.04707 \text{ Cuft/ml} \times (v_1) \\ &= 0.04707 \text{ Cuft/ml} \times 93.7 \text{ ml} \\ &= \mathbf{4.410 \text{ Cuft.}}\end{aligned}$$

$$\begin{aligned}V_{mstd} &= V_m \left[ \frac{T_{std}}{T_m + 460} \right] \left[ \frac{P_{bar} + (H / 13.6)}{P_{std}} \right] Y_i \\ &= 40.714 \text{ Cuft} \times \left[ \frac{528}{460 + 101.5} \right] \times \left[ \frac{(30.05 + (2.54 / 13.6))}{29.92} \right] \times 1.00 \\ &= \mathbf{38.690 \text{ Cuft.}}\end{aligned}$$

$$\begin{aligned}B_{wo} &= \frac{V_{wstd}}{V_{wstd} + V_{mstd}} \\ &= \frac{4.410}{4.410 + 38.690} \times 100 \\ &= \mathbf{10.23 \%}\end{aligned}$$

$$\begin{aligned}M_s &= M_d (1 - B_{wo}) + 18 (B_{wo}) \\ &= 28.85 \times (1 - 0.1023) + 18 \times 0.1023 \\ &= \mathbf{27.74}\end{aligned}$$

$$\begin{aligned}V_s (\text{avg}) &= K_p C_p \sqrt{P(\text{avg})} \sqrt{(460 + T_s) / (M_s P_s)} \\ &= 85.48 \times .84 \times 0.6650 \times \sqrt{(460 + 126.5) / (27.74 \times 30.10)} \\ &= \mathbf{40.02 \text{ ft/sec}}\end{aligned}$$

$$\begin{aligned}Q_s &= 60 (1 - B_{wo}) V_s A_s (T_{std} / T_s) (P_s / P_{std}) \\ &= 60 (1 - 0.1023) \times 40.02 \times 12.566 \times (528 / (460 + 126.5)) \times (30.10 / 29.92) \\ &= \mathbf{24,530 \text{ scfm}}\end{aligned}$$

$$\begin{aligned}
Cs &= 0.0154 \text{ grs/mg} \times (\text{total mg of sample}) / Vmstd \\
&= 0.0154 \text{ grs/mg} \times 6.44 \text{ mg} / 38.690 \text{ cuft} \\
&= \mathbf{0.0026 \text{ grs/cuft}}
\end{aligned}$$

$$\begin{aligned}
\text{lbs/hr} &= (Cs \times Qs \times 60 \text{ min/hr}) / 7000 \text{ grs/lb} \\
&= (0.0026 \times 24530 \times 60) / 7000 \\
&= \mathbf{0.54 \text{ lbs/hr Fluoride}}
\end{aligned}$$

$$\begin{aligned}
\text{lbs/day} &= \text{lbs/hr} \times 24 \text{ hrs/day} \\
&= 0.54 \times 24 \\
&= \mathbf{12.94 \text{ lbs/day Fluoride}}
\end{aligned}$$

Percent Isokinetic:

$$\begin{aligned}
I &= \frac{Ts (1.667) ((0.00267) V1) + (Vm / Tm) ((Pbar + (^H / 13.6)))}{0 Vs Ps An} \\
&= \frac{(460 + 126.5) (1.667) ((0.00267 \times 93.7) + (40.714 / (460 + 101.5))) \times ((30.05 + (2.54 / 13.6)))}{60 \times 40.02 \times 30.10 \times 0.000325} \\
&= \mathbf{101.7 \%}
\end{aligned}$$

## EMISSION CALCULATIONS

Date: June 4, 1999

Unit: B PAP

Run no. 1

$$\begin{aligned}
 V_{wstd} &= 0.04707 \text{ Cuft/ml} \times (v_1) \\
 &= 0.04707 \text{ Cuft/ml} \times 78.0 \text{ ml} \\
 &= \mathbf{3.671 \text{ Cuft.}}
 \end{aligned}$$

$$\begin{aligned}
 V_{mstd} &= V_m \left[ \frac{T_{std}}{T_m + 460} \right] \left[ \frac{P_{bar} + (H / 13.6)}{P_{std}} \right] Y_i \\
 &= 39.777 \text{ Cuft} \times \left[ \frac{528}{460 + 97.8} \right] \times \left[ \frac{(30.03 + (2.44 / 13.6))}{29.92} \right] \times 1.00 \\
 &= \mathbf{38.016 \text{ Cuft.}}
 \end{aligned}$$

$$\begin{aligned}
 B_{wo} &= \frac{V_{wstd}}{V_{wstd} + V_{mstd}} \\
 &= \frac{3.671}{3.671 + 38.016} \times 100 \\
 &= \mathbf{8.81 \%}
 \end{aligned}$$

$$\begin{aligned}
 M_s &= M_d (1 - B_{wo}) + 18 (B_{wo}) \\
 &= 28.85 \times (1 - 0.0881) + 18 \times 0.0881 \\
 &= \mathbf{27.89}
 \end{aligned}$$

$$\begin{aligned}
 V_s (\text{avg}) &= K_p C_p \sqrt{P(\text{avg})} \sqrt{(460 + T_s)} / (M_s P_s) \\
 &= 85.48 \times .84 \times 0.6550 \sqrt{(460 + 120.5)} / (27.89 \times 30.09) \\
 &= \mathbf{39.11 \text{ ft/sec}}
 \end{aligned}$$

$$\begin{aligned}
 Q_s &= 60 (1 - B_{wo}) V_s A_s (T_{std} / T_s) (P_s / P_{std}) \\
 &= 60 (1 - 0.0881) \times 39.11 \times 12.566 \times (528 / (460 + 120.5)) \times (30.09 / 29.92) \\
 &= \mathbf{24,599 \text{ scfm}}
 \end{aligned}$$

$$\begin{aligned}
Cs &= 0.0154 \text{ grs/mg} \times (\text{total mg of sample}) / Vmstd \\
&= 0.0154 \text{ grs/mg} \times 4.40 \text{ mg} / 38.016 \text{ cuft} \\
&= \mathbf{0.0018 \text{ grs/cuft}}
\end{aligned}$$

$$\begin{aligned}
\text{lbs/hr} &= (Cs \times Qs \times 60 \text{ min/hr}) / 7000 \text{ grs/lb} \\
&= (0.0018 \times 24599 \times 60) / 7000 \\
&= \mathbf{0.38 \text{ lbs/hr Fluoride}}
\end{aligned}$$

$$\begin{aligned}
\text{lbs/day} &= \text{lbs/hr} \times 24 \text{ hrs/day} \\
&= 0.38 \times 24 \\
&= \mathbf{9.02 \text{ lbs/day Fluoride}}
\end{aligned}$$

Percent Isokinetic:

$$\begin{aligned}
I &= \frac{Ts (1.667) ((0.00267) V1) + (Vm / Tm) ((Pbar + (^H / 13.6)))}{0 Vs Ps An} \\
&= \frac{(460 + 120.5) (1.667) ((0.00267 \times 78.0) + (39.777 / (460 + 97.8))) \times ((30.03 + (2.44 / 13.6)))}{60 \times 39.11 \times 30.09 \times 0.000325} \\
&= \mathbf{99.6 \%}
\end{aligned}$$

# Production Rate

DATE: 03-Jun-99

SAMPLING TIME FROM: 1:45 PM TO 2:55 PM

**STATEMENT OF PROCESS WEIGHT:**

COMPANY NAME: CF INDUSTRIES, INC. PLANT CITY PHOSPHATE COMPLEX  
 MAILING ADDRESS: P.O. DRAWER L PLANT CITY, FL 33564  
 SOURCE IDENTIFICATION: "B" PAP PRODUCTION FACILITY  
 SOURCE LOCATION: "B" PAP PRODUCTION STACK

PERMIT SOURCE: 0570005-007-AV  
 Emission Unit 009

**DATA ON OPERATING CYCLE TIME:**

START OF OPERATION, TIME  
 END OF OPERATION, TIME  
 ELAPSED TIME  
 IDLE TIME DURING CYCLE

	RUN #1			
	1:45 PM			
	2:55 PM			
	70 MIN			
	0			

**DESIGN PROCESS RATING:**

PROCESS WEIGHT RATE (INPUT) 87.8 TPH P2O5      PRODUCT (OUTPUT) \_\_\_\_\_ TPH

**DATA ON ACTUAL PROCESS RATE DURING OPERATION CYCLE:**

MATERIAL: PHOSPHATE ROCK, TPH P2O5  
 MATERIAL: 100 % SULFURIC ACID, TPH  
 MATERIAL: WATER, TPH

RUN #1		
478.74		
258.02		
19.04		

TOTAL PROCESS WEIGHT RATE:  
 PRODUCT: PHOSPHORIC ACID SLURRY, TPH  
 INPUT RATE: P2O5, TPH

RUN #1		
755.80		
96.79		

I certify that the above statement is true to the best of my knowledge and belief:

Signature: Frank Lupatini  
 Title: Prod Eng.



# Scrubber's Operating Parameters

DATE: 03-Jun-99

SAMPLING TIME FROM: 1:45 PM TO 2:55 PM

COMPANY NAME:  
MAILING ADDRESS:  
SOURCE IDENTIFICATION:  
SOURCE LOCATION:

CF INDUSTRIES, INC. PLANT CITY PHOSPHATE COMPLEX  
P.O. DRAWER L PLANT CITY, FL 33564  
"B" PAP PRODUCTION FACILITY  
"B" PAP PRODUCTION STACK

PERMIT SOURCE: 0570005-007-AV

TYPE OF SCRUBBER LIQUID: Pond Water

PACKED BED SCRUBBER	START	RUN #1	COMMENTS
	END	1:45 PM	
	AVERAGE	2:55 PM	
OUTLET TEMPERATURES F		106°	
	HIGH	106°	
	LOW	106°	

PACKED BED SCRUBBER	START	RUN #1	COMMENTS
	END	1:45 PM	
	AVERAGE	2:55 PM	
FAN AMPS		163	
	HIGH	163	
	LOW	163	

I certify that the above statement is true to the best of my knowledge and belief:

Signature: Frank Swengripis  
Title: Pond Eng.

bpaprate.xls

# Production Rate

DATE: 04-Jun-99

SAMPLING TIME FROM: 10:33 AM TO 11:45 AM

**STATEMENT OF PROCESS WEIGHT:**

COMPANY NAME: CF INDUSTRIES, INC. PLANT CITY PHOSPHATE COMPLEX  
 MAILING ADDRESS: P.O. DRAWER L PLANT CITY, FL 33564  
 SOURCE IDENTIFICATION: "B" PAP PRODUCTION FACILITY  
 SOURCE LOCATION: "B" PAP PRODUCTION STACK

PERMIT SOURCE: 0570005-007-AV  
 Emission Unit 009

**DATA ON OPERATING CYCLE TIME:**

START OF OPERATION, TIME  
 END OF OPERATION, TIME  
 ELAPSED TIME  
 IDLE TIME DURING CYCLE

	RUN #1			
	10:33 AM			
	11:45 AM			
	72 MIN			
	0			

**DESIGN PROCESS RATING:**

PROCESS WEIGHT RATE (INPUT) 37.8 TPH P2O5      PRODUCT (OUTPUT) \_\_\_\_\_ TPH

**DATA ON ACTUAL PROCESS RATE DURING OPERATION CYCLE:**

MATERIAL: PHOSPHATE ROCK, TPH P2O5  
 MATERIAL: 100 % SULFURIC ACID, TPH  
 MATERIAL: WATER, TPH

RUN #1		
437.02		
232.64		
16.97		

TOTAL PROCESS WEIGHT RATE:  
 PRODUCT: PHOSPHORIC ACID SLURRY, TPH  
 INPUT RATE: P2O5, TPH

RUN #1		
686.63		
86.25		

I certify that the above statement is true to the best of my knowledge and belief:

Signature: Frank Scumpia  
 Title: Prod Eng.

# Scrubber's Operating Parameters

DATE: 04-Jun-99

SAMPLING TIME FROM: 10:33 AM TO 11:45 AM

COMPANY NAME:  
MAILING ADDRESS:  
SOURCE IDENTIFICATION:  
SOURCE LOCATION:

CF INDUSTRIES, INC. PLANT CITY PHOSPHATE COMPLEX  
P.O. DRAWER L PLANT CITY, FL 33564  
"B" PAP PRODUCTION FACILITY  
"B" PAP PRODUCTION STACK

PERMIT SOURCE: 0570005-007-AV

TYPE OF SCRUBBER LIQUID: Pond Water

PACKED BED SCRUBBER  OUTLET TEMPERATURES F	START	RUN #1			COMMENTS
	END	10:33 AM			
	AVERAGE	11:45 AM			
	HIGH	96			
	LOW	100			
		92			

PACKED BED SCRUBBER  FAN AMPS	START	RUN #1			COMMENTS
	END	10:33 AM			
	AVERAGE	11:45 AM			
	HIGH	168.5			
	LOW	169			
		168			

I certify that the above statement is true to the best of my knowledge and belief:

Signature: Frank Swenson  
Title: Pond Eng.

VISIBLE EMISSION OBSERVATION FORM

No. 1

COMPANY NAME  
*CF Industries, Inc. Plant City Complex*

STREET ADDRESS  
*10608 Paul Buchman Highway*

*10 miles north of Plant City*

CITY *Plant City* STATE *FL* ZIP *33564*

PHONE (KEY CONTACT) *(813) 782-1591 (Ext. 290)* SOURCE ID NUMBER *057 0005 009*

OBSERVATION DATE		START TIME				END TIME
<i>6/3/99</i>		<i>1350</i>				<i>1420</i>
SEC	0	15	30	45	COMMENTS	
MIN						
1	0	0	0	0		
2	0	0	0	0		
3	0	0	0	0		
4	0	0	0	0		
5	0	0	0	0		
6	0	0	0	0		
7	0	0	0	0		
8	0	0	0	0		
9	0	0	0	0		
10	0	0	0	0		
11	0	0	0	0		
12	0	0	0	0		
13	0	0	0	0		
14	0	0	0	0		
15	0	0	0	0		
16	0	0	0	0		
17	0	0	0	0		
18	0	0	0	0		
19	0	0	0	0		
20	0	0	0	0		
21	0	0	0	0		
22	0	0	0	0		
23	0	0	0	0		
24	0	0	0	0		
25	0	0	0	0		
26	0	0	0	0		
27	0	0	0	0		
28	0	0	0	0		
29	0	0	0	0		
30	0	0	0	0		

PROCESS EQUIPMENT *B. Phosphoric Acid Production Facility* OPERATING MODE *Normal*

CONTROL EQUIPMENT *North American steel packed bed scrubber with Kimre packing or equivalent* OPERATING MODE *Normal*

DESCRIBE EMISSION POINT  
*Circular stack opening 4 feet in diameter*

HEIGHT ABOVE GROUND LEVEL *~108.5'* HEIGHT RELATIVE TO OBSERVER  
Start *~108.5'* End *~108.5'*

DISTANCE FROM OBSERVER Start *~275'* End *~275'* DIRECTION FROM OBSERVER  
Start *NE* End *NE*

DESCRIBE EMISSIONS  
Start *None* End *None*

EMISSION COLOR Start *NA* End *NA* IF WATER DROPLET PLUME  
Attached  Detached

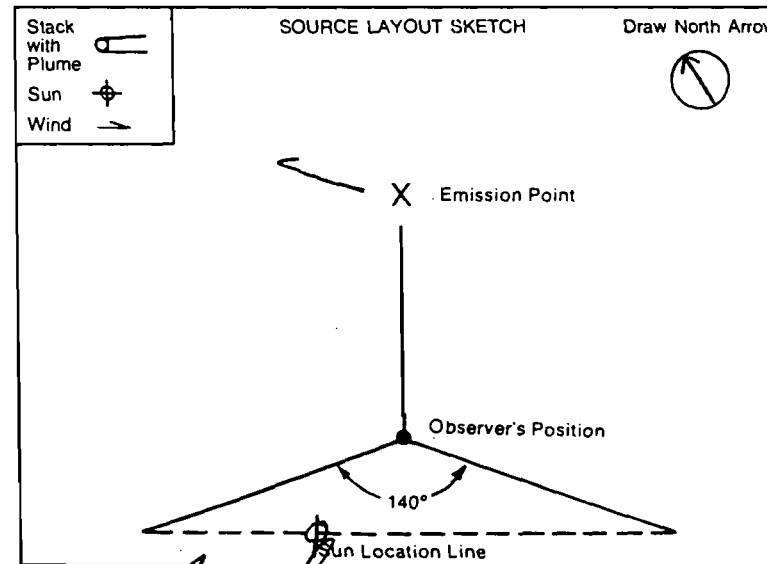
POINT IN THE PLUME AT WHICH OPACITY WAS DETERMINED  
Start *~4' from stack* End *~4' from stack*

DESCRIBE PLUME BACKGROUND  
Start *Scattered sky* End *Scattered sky*

BACKGROUND COLOR *Blue, gray, white* SKY CONDITIONS  
Start *Blue, gray, white* End *white* Start *Scattered* End *Scattered*

WIND SPEED Start *2-6 mph* End *4-8 mph* WIND DIRECTION  
Start *E* End *SE*

AMBIENT TEMP Start *88°F* End *89°F* WET BULB TEMP RH, percent  
Start *88°F* End *89°F* *65%*



ADDITIONAL INFORMATION  
*David J. Jelle*  
*Chief Chemist*

OBSERVER'S NAME (PRINT) *Lloyd G. Camp*

OBSERVER'S SIGNATURE *Lloyd G. Camp* DATE *6/3/99*

ORGANIZATION *CF Industries, Inc. Plant City Complex*

CERTIFIED BY *Eastern Technical Associates* DATE *2/24/99*

CONTINUED ON VEO FORM NUMBER *2*

VISIBLE EMISSION OBSERVATION FORM

No. 2

COMPANY NAME  
*CF Industries, Inc. Plant City Complex*

STREET ADDRESS  
*10608 Paul Buchman Highway*  
*10 miles north of Plant City*

CITY *Plant City* STATE *FL* ZIP *33564*

PHONE (KEY CONTACT) *(813) 782-1591 (Ext.290)* SOURCE ID NUMBER *0570005 009*

PROCESS EQUIPMENT *B Phosphoric Acid Production Facility* OPERATING MODE *Normal*

CONTROL EQUIPMENT *North American steel packed bed scrubber with Kimmre packing or equivalent* OPERATING MODE *Normal*

DESCRIBE EMISSION POINT  
*Circular stack opening 4 Feet in diameter*

HEIGHT ABOVE GROUND LEVEL *~ 108.5'* HEIGHT RELATIVE TO OBSERVER  
Start *~ 108.5'* End *~ 108.5'*

DISTANCE FROM OBSERVER Start *~ 275'* End *~ 275'* DIRECTION FROM OBSERVER  
Start *NE* End *NE*

DESCRIBE EMISSIONS  
Start *None* End *None*

EMISSION COLOR Start *NA* End *NA* IF WATER DROPLET PLUME Attached  Detached

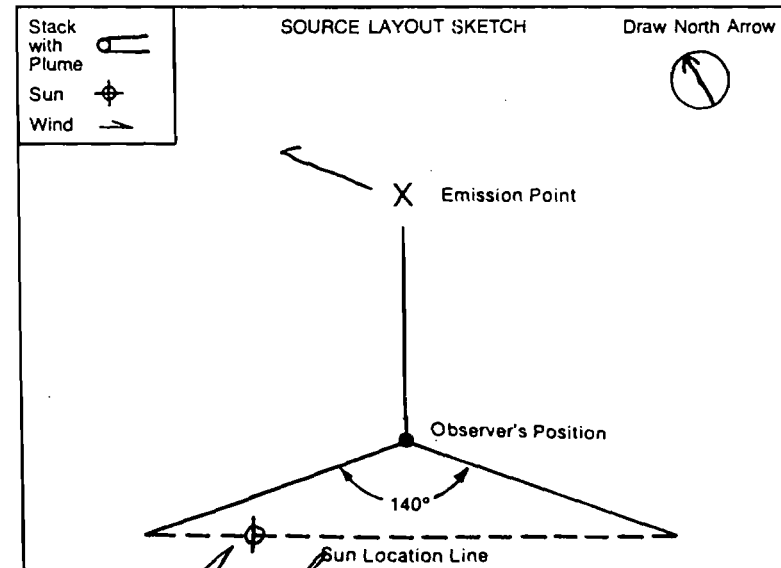
POINT IN THE PLUME AT WHICH OPACITY WAS DETERMINED  
Start *~ 4' From stack* End *~ 4' From stack*

DESCRIBE PLUME BACKGROUND  
Start *Scattered sky* End *Scattered sky*

BACKGROUND COLOR *Blue, gray, white* SKY CONDITIONS  
Start *Blue, gray, white* End *white* Start *Scattered* End *Scattered*

WIND SPEED Start *4-8mph* End *6-10mph* WIND DIRECTION Start *SE* End *E*

AMBIENT TEMP Start *89°F* End *90°F* WET BULB TEMP *64* RH, percent *64*



ADDITIONAL INFORMATION  
*Harvest Fall*  
*Cheryl Bennett*

OBSERVATION DATE		START TIME		END TIME	COMMENTS
6/3/99		1420		1450	
SEC	0	15	30	45	
MIN					
1	0	0	0	0	
2	0	0	0	0	
3	0	0	0	0	
4	0	0	0	0	
5	0	0	0	0	
6	0	0	0	0	
7	0	0	0	0	
8	0	0	0	0	
9	0	0	0	0	
10	0	0	0	0	
11	0	0	0	0	
12	0	0	0	0	
13	0	0	0	0	
14	0	0	0	0	
15	0	0	0	0	
16	0	0	0	0	
17	0	0	0	0	
18	0	0	0	0	
19	0	0	0	0	
20	0	0	0	0	
21	0	0	0	0	
22	0	0	0	0	
23	0	0	0	0	
24	0	0	0	0	
25	0	0	0	0	
26	0	0	0	0	
27	0	0	0	0	
28	0	0	0	0	
29	0	0	0	0	
30	0	0	0	0	

OBSERVER'S NAME (PRINT) *Lloyd G. Camp*

OBSERVER'S SIGNATURE *Lloyd G. Camp* DATE *6/3/99*

ORGANIZATION *CF Industries, Inc. Plant City Complex*

CERTIFIED BY *Eastern Technical Associates* DATE *2/24/99*

CONTINUED ON VEO FORM NUMBER

# SAMPLE CHAIN OF CUSTODY

Plant Name CF INDUSTRIES, INC. PLANT CITY PHOSPHATE COMPLEX

Source Identification "B" PHOSPHORIC ACID PRODUCTION FACILITY


Date Sampled: JUNE 3, 1999 Sampling Time: 1:45 PM to 2:55 PM

Test for MOISTURE, FLUORIDE, AND VISIBLE EMISSION

## SAMPLE RECOVERY

Sample Run	Description
1	#1 COLD BOX ASSEMBLY
2	#2 COLD BOX ASSEMBLY
3	#3 COLD BOX ASSEMBLY

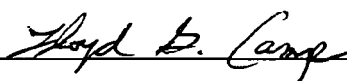
Person engaged in sample recoveries:

Signature 

Title ANALYST II

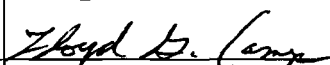


Location at which recovery "B" PHOSPHORIC ACID STACK

Laboratory person receiving samples:

Signature 

Title "A" CLASS TECHNICIAN

## ANALYSIS

Constituent	Method	Date	Time	Signature(s)
MOISTURE	EPA METHOD 4	6/3/99	15:15 - 15:25	
FLUORIDE	EPA METHOD 13 B	6/3/99	16:20 - 16:30	
VISIBLE EMISSION	EPA METHOD 9	6/3/99	13:50 - 14:50	

# SAMPLE CHAIN OF CUSTODY

Plant Name CF INDUSTRIES, INC. PLANT CITY PHOSPHATE COMPLEX

Source Identification "B" PHOSPHORIC ACID PRODUCTION FACILITY

Date Sampled: JUNE 4, 1999 Sampling Time: 10:33 AM to 11:45 AM

Test for MOISTURE AND FLUORIDE

## SAMPLE RECOVERY

Sample Run	Description
1	#1 COLD BOX ASSEMBLY
2	#2 COLD BOX ASSEMBLY
3	#3 COLD BOX ASSEMBLY

Person engaged in sample recoveries:

Signature 

Title ANALYST II

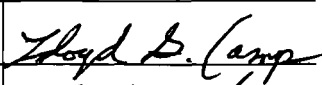
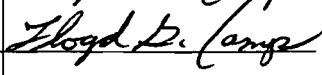
Location at which recovery "B" PHOSPHORIC ACID STACK

Laboratory person receiving samples:

Signature 

Title "A" CLASS TECHNICIAN

## ANALYSIS

Constituent	Method	Date	Time	Signature(s)
MOISTURE	EPA METHOD 4	6/4/99	12:05 - 12:15	
FLUORIDE	EPA METHOD 13 B	6/4/99	12:20 - 12:30	

CF INDUSTRIES, INC.  
Plant City Phosphate Complex  
LABORATORY ANALYSIS RECORD

"B" PAP Production Plant  
June 3, 1999

CF Industries, Inc., Plant City Phosphate Complex, uses a Fischer Accumet Model 50 pH meter with selective ion concentration capacity. The instrument has microprocessor function which calculates efficiency of the Orion Model 96-09 fluoride electrode being used and alerts the user in case of electrode malfunction.

STANDARDS

ELECTRODE  
EFFICIENCY

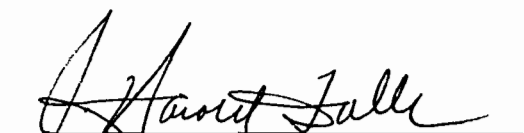
(See Technical Information Section)

0.1 $\mu\text{g/ml}$	0.9083
1.0 $\mu\text{g/ml}$	0.9739
2.0 $\mu\text{g/ml}$	

Quality Assurance Sample #1 - 0.38  $\mu\text{g/ml}$ .  
Analysis was 0.39  $\mu\text{g/ml}$ .

Quality Assurance Sample #2 - 0.76  $\mu\text{g/ml}$ .  
Analysis was 0.77  $\mu\text{g/ml}$ .

Quality Assurance Sample #3 - 1.90  $\mu\text{g/ml}$ .  
Analysis was 1.88  $\mu\text{g/ml}$ .

  
J. Harold Falls  
Chief Chemist, Laboratory

JHF/gm  
9/89



CF INDUSTRIES, INC.  
Plant City Phosphate Complex  
LABORATORY ANALYSIS RECORD

"B" PAP Production Plant  
June 4, 1999

CF Industries, Inc., Plant City Phosphate Complex, uses a Fischer Accumet Model 50 pH meter with selective ion concentration capacity. The instrument has microprocessor function which calculates efficiency of the Orion Model 96-09 fluoride electrode being used and alerts the user in case of electrode malfunction.

STANDARDS

ELECTRODE  
EFFICIENCY

(See Technical Information Section)

0.1  $\mu\text{g/ml}$  0.8964

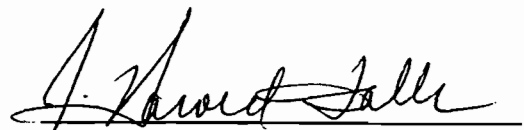
1.0  $\mu\text{g/ml}$  0.9729

2.0  $\mu\text{g/ml}$

Quality Assurance Sample #1 - 0.38  $\mu\text{g/ml}$ .  
Analysis was 0.40  $\mu\text{g/ml}$ .

Quality Assurance Sample #2 - 0.76  $\mu\text{g/ml}$ .  
Analysis was 0.77  $\mu\text{g/ml}$ .

Quality Assurance Sample #3 - 1.90  $\mu\text{g/ml}$ .  
Analysis was 1.89  $\mu\text{g/ml}$ .

  
J. Harold Falls  
Chief Chemist, Laboratory

JHF/gm  
9/89

APPENDIX "C"

PROJECT PARTICIPANTS

PROJECT PARTICIPANTS

CF INDUSTRIES, INC.

PLANT CITY PHOSPHATE COMPLEX

H.E. Morris	General Manager
R.C. May	Manager of Engineering
T.A. Edwards	Supt., Environmental Affairs
J.M. Messina	Chief of Environmental Affairs
J.H. Falls	Chief Chemist, Laboratory
J.I. Longest	Staff Chemist
T. Ortoski	Environmental Supervisor
E. Kretschmar	Analyst II
S. Willoughby	"A" Class Technician
L. Camp	"A" Class Technician
W. Cherry	"A" Class Technician