

FEDERAL/STATE
TECHNICAL GUIDANCE MEETING
NOV. 6, 1979
TALLAHASSEE, FLORIDA

JACKSONVILLE ELECTRIC AUTHORITY
COAL-FIRED POWER PLANT
TWO 600 MWe UNITS

INTRODUCTION

H. S. Oven, Jr.
Administrator, Power Plant Siting Section
Florida Dept. of Environmental Regulation

PROJECT STATUS/SITE SELECTION

R. Breitmoser
Chief, Research and Environmental Affairs Division
JACKSONVILLE ELECTRIC AUTHORITY

THE PLANT

W. D. Rezak
Project Manager
EBASCO SERVICES INCORPORATED

SITE CERTIFICATION APPLICATION AND
ENVIRONMENTAL IMPACT ASSESSMENT
PLAN OF STUDY

D. H. Lucas
Environmental Project Coordinator
ENVIROSPHERE COMPANY

PSD-FL-010
0310001-NA-AC

ENVIRONMENTAL STUDY PLANS

- A. Air Quality/Meteorology
 - D. Fulle
Supervisor, Air Quality/Meteorology
- B. Surface Water Hydrology/Water Quality
 - H. Frediani
Senior Hydrothermal Engineer
 - R. Boyd
Supervisor, Water and Wastewater
- C. Groundwater Hydrology/Water Quality
 - F. Titus
Manager, Geosciences
- D. Geology/Soils
 - G. Bain
Geologist/Hydrologist
- E. Terrestrial Ecology
 - B. Floyd
Terrestrial Ecologist
- F. Aquatic Ecology
 - H. L. Davis
Supervisor, Water Resources
- G. Land Use/Socioeconomics
 - S. Kangisser
Resource Planner
- H. Noise
 - D. Fulle
Supervisor, Air Quality/Meteorology

JACKSONVILLE ELECTRIC AUTHORITY

Overall Project Schedule

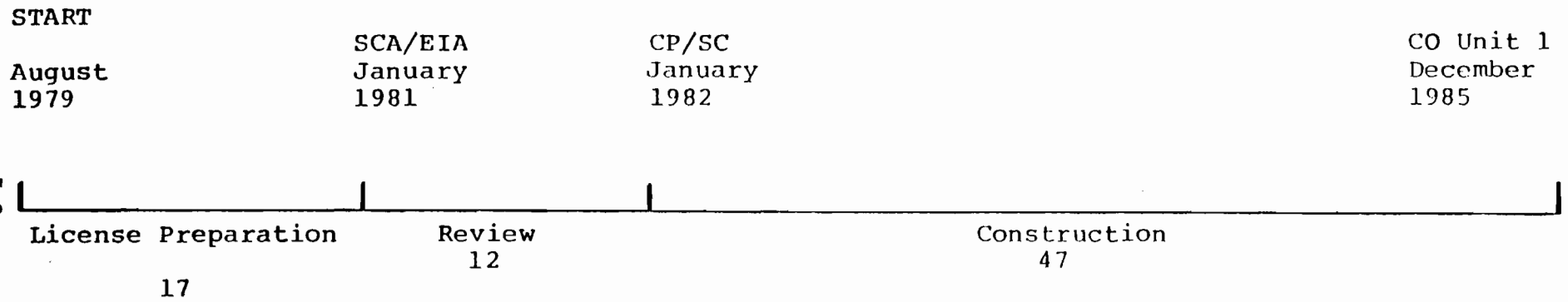


EXHIBIT 5.1-1

JACKSONVILLE ELECTRIC AUTHORITY
Environmental Licensing Milestone Schedule

5-3

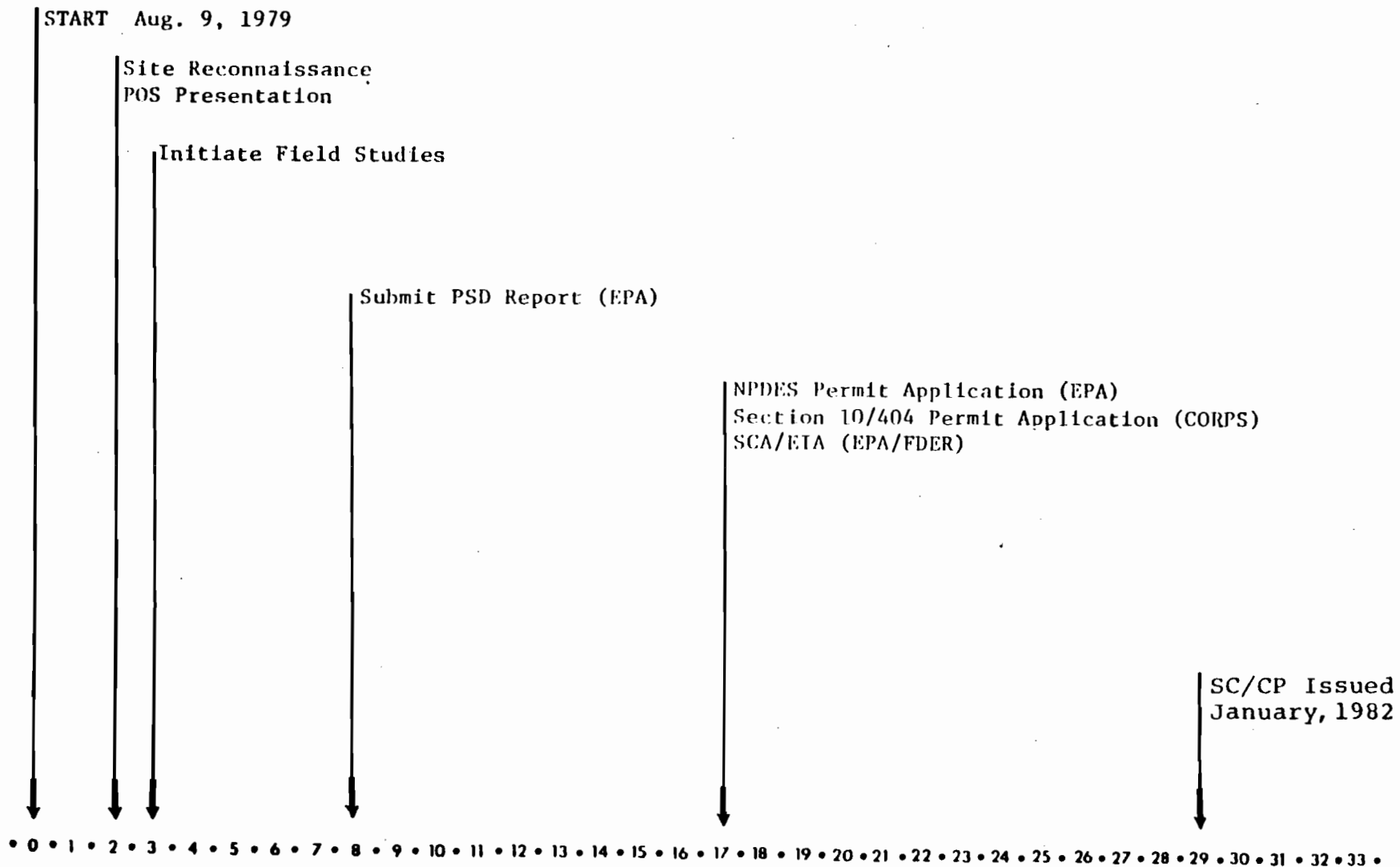


EXHIBIT 5.2-1

AIR QUALITY/METEOROLOGY
STUDY PLAN OBJECTIVES

- TO DEFINE THE EXISTING AIR QUALITY/METEOROLOGICAL CONDITIONS.
- TO EVALUATE VARIOUS PLANT DESIGN ALTERNATIVES.
- TO ASSESS THE IMPACT OF PLANT CONSTRUCTION AND OPERATION.
- TO SUGGEST AN APPROPRIATE OPERATIONAL MONITORING PROGRAM.
- TO SATISFY THE REQUIREMENTS OF THE SCA, NEPA, AND PSD REGULATIONS AND PROVIDE SUFFICIENT INFORMATION TO ALLOW INFORMED DECISION MAKING BY THE REGULATORY AUTHORITIES.

AIR QUALITY/METEOROLOGY
STUDY PLAN TASKS

- LITERATURE SURVEY/DATA SEARCH
- AIR QUALITY/METEOROLOGY MONITORING PROGRAM
- DESCRIPTION OF BASELINE CONDITIONS
- DESCRIPTION OF PLANT AIR QUALITY CONTROL SYSTEMS
- ASSESSMENT OF IMPACT OF PLANT CONSTRUCTION
- ASSESSMENT OF IMPACT OF PLANT OPERATION
- ASSESSMENT OF COOLING SYSTEM IMPACTS
- EVALUATION OF ALTERNATIVES
- DEVELOPMENT OF PROPOSED OPERATIONAL MONITORING PROGRAM
- REPORT PREPARATION

AIR QUALITY/METEOROLOGY
STUDY PLAN TASK DESCRIPTIONS

1. LITERATURE SURVEY/DATA SEARCH

• TOPICS

- REGIONAL CLIMATE
- LOCAL DISPERSION CONDITIONS
- BACKGROUND AIR QUALITY
- EMISSION INVENTORY

• SOURCES

- NATIONAL CLIMATE CENTER
- FDER
- EPA
- JACKSONVILLE BES
- PREVIOUS STUDIES

2. AIR QUALITY/METEOROLOGY MONITORING PROGRAM

- LOCATIONS

- ONE MILE NORTH OF EASTPORT
- BETWEEN WILLIS POINT AND WALKILL

- PARAMETERS

- SULFUR DIOXIDE
- NITROGEN DIOXIDE
- CARBON MONOXIDE
- OZONE
- TOTAL SUSPENDED PARTICULATES
- METEOROLOGY (WIND SPEED, WIND DIRECTION, TEMPERATURE, DEWPOINT, SIGMA THETA, PRECIPITATION)

- OPERATION

- ONSITE TECHNICIAN/FIELD COORDINATOR
- DATA LOGGERS/FLOPPY DISKS/STRIP CHARTS
- QUALITY ASSURANCE PER "APPENDIX B"

3. DESCRIPTION OF BASELINE CONDITIONS

- SOURCES

- TASK 1 (LITERATURE SURVEY)

- TASK 2 (ON-SITE MONITORING PROGRAM)

- RESULTS

- INPUT TO PSD AND SCA/EIA REPORTS

- INPUT TO PLANT DESIGN

4. DESCRIPTION OF PLANT AIR QUALITY CONTROL SYSTEMS

- FUEL CHARACTERISTICS

- EMISSION SOURCES

- BEST AVAILABLE CONTROL TECHNOLOGY DEMONSTRATION

- (1) ECONOMICS

- (2) ENERGY

- (3) ENVIRONMENT

5. ASSESSMENT OF PLANT CONSTRUCTION IMPACTS

- FUGITIVE DUST
- VEHICULAR EMISSIONS
- OPEN BURNING

6. ASSESSMENT OF PLANT OPERATION IMPACTS

· CONSIDERATIONS

- COMPLIANCE WITH FAAQS AND NAAQS
- CONSUMPTION OF PSD INCREMENTS
- IMPACT ON NONATTAINMENT AREAS
- VISIBILITY, ACID RAIN, TRACE ELEMENTS

· ANALYTICAL TOOLS

- CRSTEM, AQUAL, RAM FOR SHORT RANGE
- IMPACT, MESODIF, NOAA FOR LONG RANGE
- LITERATURE SURVEY FOR OTHER EFFECTS

7. ASSESSMENT OF COOLING SYSTEM IMPACTS

- CONSIDERATIONS/ANALYTICAL TOOLS
 - FOGGING - GRDFOG
 - DRIFT DEPOSITION - SALDEP
 - VISIBLE VAPOR PLUMES - ELEPLUME

8. EVALUATION OF ALTERNATIVES

- AQCS - BACT
- STACKHEIGHT
- FUEL QUALITY
- COOLING SYSTEMS
- SITES

9. DEVELOP PROPOSED OPERATIONAL MONITORING PROGRAM

- REGULATION CONSIDERATIONS
- STACK EMISSIONS
- AMBIENT AIR QUALITY
- METEOROLOGY

10. REPORT PREPARATION

- PSD REPORT
- SCA/EIA

SURFACE WATER HYDROLOGY/HYDROTHERMAL STUDIES
STUDY PLAN OBJECTIVES

- TO ESTABLISH THE EXISTING SURFACE WATER HYDROLOGICAL CHARACTERISTICS OF THE RECEIVING AND ON-SITE WATER BODIES.
- TO EVALUATE AND DESCRIBE HEAT DISSIPATION SYSTEM ALTERNATIVES IN ORDER TO MINIMIZE IMPACT ON THE RECEIVING WATER BODY.
- TO PREDICT THE IMPACTS OF PLANT CONSTRUCTION AND OPERATION ON THE RECEIVING AND ON-SITE WATER BODIES.

SURFACE WATER HYDROLOGY/HYDROTHERMAL STUDIES
STUDY PLAN TASKS

- LITERATURE SURVEY/DATA SEARCH
- BASELINE MONITORING PROGRAM
- DESCRIPTION OF PLANT HEAT DISSIPATION SYSTEM
- ASSESSMENT OF IMPACT OF PLANT CONSTRUCTION
- ASSESSMENT OF IMPACT OF PLANT OPERATION
- HEAT DISSIPATION ALTERNATIVES
- REPORT PREPARATION

SURFACE WATER HYDROLOGY/HYDROTHERMAL STUDIES
STUDY PLAN TASK DESCRIPTIONS

1. LITERATURE SURVEY/DATA SEARCH

• SOURCES

- GOVERNMENTAL AGENCIES
- UNIVERSITIES
- UTILITIES
- OTHER INDUSTRIES
- TECHNICAL JOURNAL

• INFORMATION

- FLOWS
- STAGES
- CURRENTS
- BOTTOM AND SHORELINE CONFIGURATIONS
- AMBIENT TEMPERATURES
- APPLICABLE THERMAL STANDARDS
- MODELS
- TECHNIQUES

2. HEAT DISSIPATION SYSTEM

- INTAKE LOCATION, DIMENSION, VELOCITY
- CONDENSER COOLING SYSTEM DESIGN AND OPERATION
- DISCHARGE LOCATION, TYPE, DIMENSION

3. PLANT CONSTRUCTION IMPACT

- SITE DRAINAGE IMPACT ON ON-SITE WATER BODIES
- IMPACT ON ST. JOHNS RIVER OF INTAKE AND DISCHARGE STRUCTURES CONSTRUCTION

4. PLANT OPERATION IMPACT

- THERMAL PLUME
 - SHAPE AND LENGTH
 - AREAL AND VOLUMETRIC EXTENT
 - TIME OF TRAVEL
 - RATE OF TEMPERATURE CHANGE
- INTAKE
 - INTAKE FLOW RATE
 - AMBIENT FLOWS AND STAGES
 - AVERAGE EXTREME VELOCITIES

5. HEAT DISSIPATION ALTERNATIVES

- ONCE-THROUGH VS. CLOSED CYCLE COOLING
 - (1) PONDS
 - (2) SPRAYS
 - (3) NATURAL DRAFT TOWERS
 - (4) MECHANICAL DRAFT TOWERS
- OFFSHORE VS. ONSHORE INTAKE, DISCHARGE
- SURFACE VS. SUBSURFACE INTAKE, DISCHARGE
- INTAKE AND DISCHARGE VELOCITIES

6. REPORT PREPARATION

- ASSUMPTIONS
- METHODOLOGY
- DATA
- RESULTS
- DESIGN RATIONALE

SURFACE WATER QUALITY
STUDY PLAN OBJECTIVES

- IDENTIFY AMBIENT SURFACE WATER QUALITY ON AND ADJACENT TO PROPOSED PLANT SITE
- ASSESS IMPACT ON WATER QUALITY ASSOCIATED WITH PLANT CONSTRUCTION ACTIVITIES
- ASSESS IMPACT ON WATER QUALITY ASSOCIATED WITH PROPOSED PLANT OPERATIONS
- ASSESS IMPACT ON WATER QUALITY FROM PROPOSED ACTION AND ASSOCIATED ALTERNATIVES
- ESTABLISH SURFACE WATER QUALITY MONITORING FOR CONSTRUCTION AND OPERATION PHASES
- REPORT PREPARATION TO SATISFY THE REQUIREMENTS OF THE SCA, NEPA, AND OTHER REGULATIONS

SURFACE WATER QUALITY
STUDY PLAN TASKS

- LITERATURE SURVEY/DATA SEARCH
- SURFACE WATER QUALITY MONITORING PROGRAM
- DESCRIPTION OF PLANT WATER USE AND WASTE HANDLING PLANS
- ASSESSMENT OF IMPACT OF PLANT CONSTRUCTION
- ASSESSMENT OF IMPACT OF PLANT OPERATION
- ASSESSMENT OF WATER QUALITY IMPACTS OF DESIGN ALTERNATIVES
- PREPARATION OF PLANS FOR MONITORING APPROPRIATE WATER QUALITY PARAMETERS DURING PLANT CONSTRUCTION AND OPERATION
- REPORT PREPARATION

SURFACE WATER QUALITY
STUDY PLAN TASK DESCRIPTIONS

1. LITERATURE SURVEY/DATA SEARCH

• FEDERAL AGENCIES

- (1) EPA
- (2) USGS
- (3) U. S. ARMY CORPS OF ENGINEERS

• STATE AGENCIES

- (1) DER
- (2) DNR

• ST. JOHNS RIVER WATER MANAGEMENT DISTRICT

• LOCAL GOVERNMENT AGENCIES/GROUPS

- (1) JACKSONVILLE BIO--ENVIRONMENTAL SERVICES
- (2) CITY OF JACKSONVILLE PUBLIC WORKS DEPARTMENT
- (3) CITY OF PALATKA WATER DEPARTMENT

• UNIVERSITY PERSONNEL

• SEMINOLE ELECTRICAL COOPERATIVE, INC.

• OTHER

2. SURFACE WATER QUALITY MONITORING PROGRAM

- PRELIMINARY SURVEY
- FACTORS FOR PHYSICAL AND CHEMICAL VARIABLE SELECTION
 - (1) EFFLUENT GUIDELINES AND STANDARDS
 - (2) FLORIDA WATER QUALITY RULES
 - (3) AQUATIC ECOLOGY
 - (4) PLANT WATER REQUIREMENTS
 - (5) PROXIMITY OF OTHER DISCHARGES
- FACTORS IN SAMPLING PROCEDURE AND METHODOLOGY SELECTION
 - (1) SALT WATER INFLUENCE
 - (2) TIDAL PHASE
 - (3) FRESH WATER FLOW
 - (4) RIVER CONFIGURATION
 - (5) TIME OF YEAR
 - (6) HISTORICAL DATA AVAILABILITY AND APPLICABILITY

3. DESCRIPTION OF PLANT WATER USE AND WASTE HANDLING PLAN

- IDENTIFY PLANT WATER MAKEUP REQUIREMENTS
- IDENTIFY PLANT WASTEWATER AND SOLID WASTE CHARACTERISTICS
- IDENTIFY HANDLING AND TREATMENT METHODS FOR WASTES
- IDENTIFY PLANT WASTEWATER DISCHARGE CHARACTERISTICS
- PREPARE SCHEMATIC DIAGRAM OF PLANT WATER BALANCE

4. ASSESSMENT OF IMPACT OF PLANT CONSTRUCTION

- IDENTIFY CONSTRUCTION ACTIVITY SCHEDULE AND PHASING
- DEVELOP SEDIMENT AND EROSION CONTROL MEASURES
- PHASE SEDIMENT AND EROSION CONTROL PLAN WITH CONSTRUCTION ACTIVITIES
- IDENTIFY OTHER WASTE HANDLING AND TREATMENT METHODS REQUIRED
- DETERMINE APPROXIMATE LEVELS OF PHYSICAL AND CHEMICAL DISCHARGES DURING CONSTRUCTION
- DISCUSS INTERACTION BETWEEN CONSTRUCTION-RELATED DISCHARGES AND EXISTING SURFACE WATER BODIES

5. ASSESSMENT OF IMPACT OF PLANT OPERATION

- DESCRIBE PROPOSED PLANT WATER AND WASTEWATER MANAGEMENT PLAN
- CHARACTERIZE QUALITY AND QUANTITY OF DISCHARGES IDENTIFIED IN PLAN
- DESCRIBE RECEIVING SURFACE WATER BASELINE WATER QUALITY CONDITIONS
- DESCRIBE RESULTANT WATER QUALITY VARIATIONS IN RECEIVING SURFACE WATERS

6. ASSESSMENT OF WATER QUALITY IMPACTS OF DESIGN ALTERNATIVES

- IDENTIFY VIABLE WATER AND WASTEWATER MANAGEMENT PLAN ALTERNATIVES
- DESCRIBE RESULTANT WATER QUALITY VARIATIONS FROM EACH DESIGN ALTERNATIVE
- COMPARE IMPACTS ON SURFACE WATER QUALITY FOR PROPOSED ACTION AND ALTERNATIVES

7. PREPARATION OF PLANS FOR MONITORING WATER QUALITY PARAMETERS DURING PLANT CONSTRUCTION AND OPERATION

- IDENTIFY PARAMETERS OF CONCERN DURING THE CONSTRUCTION AND OPERATION
- IDENTIFY DESIRED MONITORING LOCATIONS
- IDENTIFY FEASIBLE ANALYTICAL TECHNIQUES (I.E., IN-SITU VS. LABORATORY)
- IDENTIFY SAMPLING FREQUENCY AND DURATION

8. REPORT PREPARATION

- SCA/EIA

GROUNDWATER HYDROLOGY/WATER QUALITY
STUDY PLAN OBJECTIVES

- DETERMINE PHYSICAL AND CHEMICAL CHARACTERISTICS OF THE SYSTEM
- EVALUATE, AND PROVIDE INPUT TO, DESIGN ALTERNATIVES AFFECT-
ING GROUNDWATER
- PREDICT AND MONITOR IMPACTS OF FACILITY CONSTRUCTION
AND OPERATION

GROUNDWATER HYDROLOGY/WATER QUALITY
STUDY PLAN TASKS

- LITERATURE SURVEY/DATA SEARCH
- SUBSURFACE INVESTIGATION
- DATA REDUCTION AND EVALUATION
- DESCRIPTION OF PLANT FACILITIES AND OPERATIONS AFFECTING GROUNDWATER
- ASSESSMENT OF DESIGN ALTERNATIVES
- DESIGN AND IMPLEMENTATION OF PRECONSTRUCTION MONITORING PROGRAM
- IMPACT EVALUATION
- REPORT PREPARATION

GEOLOGY/SOILS
STUDY PLAN OBJECTIVES

- PROVIDE A PICTURE OF THE PHYSIOGRAPHY, REGIONAL GEOLOGY, REGIONAL SEISMIC HISTORY, AND GENERAL SOIL AND ROCK CHARACTERISTICS OF THE SITE REGION
- PROVIDE SUPPLEMENTARY INFORMATION ON LOCATION OF REGIONAL AND LOCAL STRUCTURES
- COLLECT FIELD DATA ON SURFICIAL GEOLOGICAL CONDITIONS, SUBSURFACE SOIL AND ROCK MATERIALS, AND GROUNDWATER CONDITIONS
- QUANTIFY AND SUPPLEMENT THE DESCRIPTIONS OF SOIL AND ROCK PROPERTIES
- EVALUATE THE GEOLOGICAL CONSEQUENCES OF ALTERNATE PLANT AND TRANSMISSION CORRIDOR LAYOUTS
- DESCRIBE BASELINE CONDITIONS RELEVANT TO THE REGION AND SITE AND POTENTIAL IMPACTS ON PLANT CONSTRUCTION AND OPERATION

GEOLOGY/SOILS
STUDY PLAN TASKS

- LITERATURE SURVEY/DATA SEARCH
- REMOTE SENSING ANALYSIS AND INTERPRETATION
- SURFACE AND SUBSURFACE FIELD INVESTIGATIONS
- LABORATORY TESTING
- EVALUATION OF PLANT LAYOUT ALTERNATIVES
- REPORT PREPARATION

GEOLOGY/SOILS
STUDY PLAN TASK DESCRIPTIONS

1. LITERATURE SURVEY/DATA SEARCH

- COLLECT DATA FROM AVAILABLE MAPS, TECHNICAL PAPERS AND SEARCH FEDERAL, STATE, AND UNIVERSITY FILES.

2. REMOTE SENSING

- STUDY AERIAL PHOTOS, PHOTO MOSAICS, AND/OR ERTS IMAGERY FOR ADDITIONAL GEOLOGICAL INFORMATION, I.E., LINEAMENTS, SINKHOLES AND OTHER GEOLOGIC HAZARDS.

3. SURFACE AND SUBSURFACE FIELD INVESTIGATIONS

- CORE AND LOG GEOLOGIC MATERIALS TO DETERMINE LOAD BEARING CHARACTER, HYDROLOGY, LIQUIFACTION POTENTIAL, AND ENVIRONMENTAL IMPACT.
- MEASURE AND RECORD GROUNDWATER LEVELS.

4. LABORATORY TESTING

- TEST SOIL AND ROCK MATERIALS IN ACCORDANCE WITH (ASTM) STANDARDS TO DEFINE MATERIAL PROPERTIES DATA.

5. EVALUATION OF PLANT LAYOUT

- EVALUATE GEOLOGIC, HYDROLOGIC AND SOILS IMPACT ON PLANT LAYOUT AND DESIGN.

6. REPORT PREPARATION

- DESCRIBE, ACCORDING TO APPLICABLE REGULATIONS, BASELINE CONDITIONS AND POTENTIAL ENVIRONMENTAL IMPACT OF PLANT CONSTRUCTION AND OPERATION.

TERRESTRIAL ECOLOGY
STUDY PLAN OBJECTIVES

- CHARACTERIZE THE VEGETATION OF THE PROPOSED POWER PLANT SITE AND DIRECTLY ASSOCIATED TRANSMISSION LINE CORRIDORS.
- CHARACTERIZE FAUNAL POPULATION (MAMMALS, AVIFAUNA, REPTILES, AND AMPHIBIANS) WHICH OCCUR ON THE PROPOSED POWER PLANT SITE AND DIRECTLY ASSOCIATED TRANSMISSION CORRIDORS.
- EVALUATE THE WILDLIFE HABITAT OF THE PROPOSED POWER PLANT SITE AND DIRECTLY ASSOCIATED TRANSMISSION LINE CORRIDORS.
- DETERMINE THE PRESENCE OF RARE, THREATENED OR ENDANGERED FLORAL AND FAUNAL SPECIES ON THE PROPOSED POWER PLANT SITE AND DIRECTLY ASSOCIATED TRANSMISSION LINE CORRIDORS.
- IDENTIFY AND EVALUATE THE POTENTIAL EFFECTS ASSOCIATED WITH THE CONSTRUCTION AND OPERATION OF THE PROPOSED POWER PLANT AND DIRECTLY ASSOCIATED TRANSMISSION LINE CORRIDORS.

TERRESTRIAL ECOLOGY
STUDY PLAN TASKS

- LITERATURE REVIEW
- PRELIMINARY SITE RECONNAISSANCE
- FIELD SAMPLING PROGRAM
- DATA ANALYSIS
- SITE DESCRIPTION
- IMPACT ASSESSMENT
- REPORT PREPARATION

TERRESTRIAL ECOLOGY
STUDY PLAN TASK DESCRIPTIONS

1. LITERATURE REVIEW

- BIOSIS, APTIC
- PERSONAL CONTACT

2. PRELIMINARY SITE RECONNAISSANCE

- IDENTIFY PREDOMINANT VEGETATION COMMUNITIES/
WILDLIFE HABITAT
- AID IN FINALIZATION OF FIELD SAMPLING PROGRAM

3. FIELD PROGRAM

- VEGETATION DESCRIPTION
- INVENTORY OF MAMMALS
- INVENTORY OF AVIFAUNA
- INVENTORY OF REPTILES AND AMPHIBIANS
- INVENTORY OF IMPORTANT SPECIES

4. DATA ANALYSIS

- RUDIMENTARY STATISTICAL TREATMENT

5. SITE DESCRIPTION

- FLORAL COMMUNITIES
- EXISTING PERTURBATIONS
- WILDLIFE SPECIES
- WILDLIFE HABITAT EVALUATION
- SOIL TYPES

6. IMPACT ASSESSMENT

- CONSTRUCTION RELATED EFFECTS
- OPERATIONAL RELATED EFFECTS

7. REPORT PREPARATION

AQUATIC ECOLOGY
STUDY PLAN OBJECTIVES

- TO SATISFY THE REQUIREMENTS OF THE SCA AND NEPA
- TO DESCRIBE THE ECOLOGY OF THE AQUATIC SYSTEMS ON THE SITE AS WELL AS THOSE SUBJECT TO POTENTIAL IMPACT BY THE PROPOSED POWER PLANT AND ASSOCIATED TRANSMISSION FACILITIES
- TO EVALUATE VARIOUS PLANT DESIGN ALTERNATIVES
- TO PREDICT THE EFFECTS OF THE CONSTRUCTION AND OPERATION OF THE PLANT AND TRANSMISSION FACILITIES ON THE AQUATIC ECOSYSTEM

AQUATIC ECOLOGY
STUDY PLAN TASKS

- LITERATURE SURVEY/DATA SEARCH
- DEVELOPMENT OF FIELD DATA ACQUISITION PROGRAM
- BASELINE MONITORING
- DATA MANAGEMENT AND ANALYSIS
- PREPARATION OF SCA/EIA REPORT

AQUATIC ECOLOGY
DESCRIPTION OF TASKS

1. LITERATURE SURVEY/DATA SEARCH

- COLLECT AVAILABLE PUBLISHED AND UNPUBLISHED DATA:
 - (1) SPORT AND COMMERCIAL FISHERIES
 - (2) RARE AND ENDANGERED SPECIES
 - (3) LOCAL, REGIONAL, STATE, AND FEDERAL AGENCY SURVEYS
- ENVIRONMENTAL LICENSING REPORTS
- BIOLOGICAL AND ECOLOGICAL REPORTS, THESES AND DISSERTATIONS

2. DEVELOPMENT OF FIELD DATA ACQUISITION PROGRAM

- OBTAIN SCIENTIFIC COLLECTORS PERMITS
- PRELIMINARY SAMPLING TO SELECT APPROPRIATE METHODOLOGY
- DELINEATE SAMPLING ZONES
- REFINEMENT OF FIELD TECHNIQUES
 - (1) SPECIES SATURATION CURVES
 - (2) CATCH PER UNIT EFFORT

3. BASELINE MONITORING

- MEROPLANKTON
- ZOOPLANKTON
- PHYTOPLANKTON
- PERIPHYTON
- MACROPHYTES
- MACROINVERTEBRATES
- FISHERIES
- MANATEES AND OTHER RARE AND ENDANGERED SPECIES
- HABITAT MAPPING

4. DATA MANAGEMENT AND ANALYSIS

- STORAGE/RETRIEVAL
- GRAPHICS AND MAPPING
- STATISTICAL ANALYSIS OF DISTRIBUTION AND ABUNDANCE OF ORGANISMS (TIME AND SPACE)
- IMPACT PROJECTIONS FOR:
 - (1) PLANT CONSTRUCTION
 - (2) TRANSMISSION LINE CONSTRUCTION
 - (3) SITE RUNOFF AND SEDIMENTATION
 - (4) DREDGE AND FILL
 - (5) BLOWDOWN
 - (6) ENTRAINMENT, IMPINGEMENT, ENTRAPMENT
 - (7) COAL STORAGE RUNOFF
- ASSESSMENT OF DESIGN ALTERNATIVES
- DEVELOP AQUATIC MONITORING PROGRAM FOR CONSTRUCTION AND OPERATIONAL PHASES

5. PREPARATION OF SCA/EIA REPORT

- AQUATIC ECOLOGY - SETTING
- SITE PREPARATION AND PLANT CONSTRUCTION
- CONSTRUCTION OF DIRECTLY ASSOCIATED TRANSMISSION FACILITIES
- WATER DISCHARGES
- COOLING WATER INTAKE
- PRE-APPLICATION MONITORING
- CONSTRUCTION AND OPERATIONAL MONITORING
- CONDENSER SYSTEM

LAND USE/SOCIOECONOMICS
STUDY PLAN OBJECTIVES

TO DETERMINE WHAT EFFECTS THE CONSTRUCTION AND OPERATION OF THE
POWER PLANT WILL HAVE ON:

- CURRENT AND PROJECTED LAND USE PATTERNS
- HISTORICAL AND ARCHEOLOGICAL SITES
- AESTHETIC VALUE OF THE AREA
- DEMOGRAPHIC PROFILES AND SOCIAL STRUCTURE
- EMPLOYMENT AND INCOME
- GOVERNMENT FISCAL CONDITIONS
- COMMUNITY SERVICES
- HOUSING
- TRANSPORTATION
- RECREATIONAL OPPORTUNITIES

LAND USE/SOCIOECONOMICS
STUDY PLAN TASKS

IN ORDER TO MEET STUDY OBJECTIVES THE FOLLOWING TASKS WILL
BE PERFORMED:

1. LITERATURE SURVEY
2. AERIAL PHOTO INTERPRETATION
3. FIELD SURVEYS
 ARCHEOLOGIC
 VIEWSHED
 INTERVIEWS
4. FORECASTS AND ANALYSIS
5. DETERMINATION OF PROJECT BENEFITS AND COSTS
6. REPORT PREPARATION

LAND USE/SOCIOECONOMICS
STUDY PLAN TASK DESCRIPTIONS

1. LITERATURE SURVEY

- LOCAL GOVERNMENT OFFICIALS
- REGIONAL GOVERNMENT OFFICIALS
- STATE GOVERNMENT OFFICIALS
- FEDERAL AGENCY OFFICIALS
- UNIVERSITY PERSONNEL
- LOCAL DEVELOPERS
- HISTORICAL SOCIETIES
- COMPUTER DATA BASES
- LIBRARY SEARCH
- OTHER

2. AERIAL PHOTO INTERPRETATION

- OPEN
- AGRICULTURAL
- RESIDENTIAL
- INDUSTRIAL
- COMMERCIAL
- ROAD
- RECREATIONAL
- ENVIRONMENTALLY SENSITIVE AREAS
- OPEN WATER
- WOODED LANDS
- HISTORIC SITES/ARTIFACTS
- OTHER

3. FIELD SURVEY

- DATA VERIFICATION
- VIEWSHED SURVEY
 - (1) DOMINANT SCENIC ELEMENTS
 - (2) VARIETY OF SCENERY
 - (3) DISTANCE
 - (4) VIEWERS
- COMMUNITY SERVICES
 - (1) POLICE
 - (2) FIRE
 - (3) MEDICAL
 - (4) SCHOOLS
- HOUSING

4. FORECASTS AND ANALYSIS

• FORECASTS

- (1) EMPLOYMENT RATE AND LABOR FORCE
- (2) HOUSING DEMAND
- (3) INCOME LEVEL AND DISTRIBUTION
- (4) POPULATION GROWTH
- (5) TRANSPORTATION
- (6) COMMUNITY SERVICES

• ANALYSIS

- (1) LAND USE IMPACTS
 - A. REMOVAL OF LAND
 - B. NOISE
 - C. COOLING TOWER FOGGING
 - D. AESTHETIC IMPACTS
 - E. FUGITIVE DUST
- (2) EMPLOYMENT AND INCOME
 - A. REGIONAL EMPLOYMENT BY INDUSTRY
 - B. UNEMPLOYMENT RATES
 - C. LABOR FORCE
 - D. SIZE OF LABOR FORCE
 - E. REGIONAL INCOME DISTRIBUTION
- (3) SOCIAL IMPACTS
- (4) HISTORICAL AND ARCHEOLOGICAL SITES
- (5) VIEWSHED
- (6) COMMUNITY SERVICES
- (7) HOUSING
- (8) TRANSPORTATION
- (9) RECREATION

5. BENEFITS AND COSTS ANALYSIS

- DEMOGRAPHY
- COMMUNITY SERVICES
- EMPLOYMENT AND INCOME
- INFRASTRUCTURE
- HOUSING
- OTHER

6. REPORT PREPARATION

- SCA/EIA SECTIONS

LAND USE ANALYSIS

- OPEN
- AGRICULTURAL
- RESIDENTIAL
- INDUSTRIAL
- COMMERCIAL
- ROAD
- RECREATIONAL
- ENVIRONMENTALLY SENSITIVE AREAS
- OPEN WATER
- WOODED LANDS
- HISTORIC SITES/ARTIFACTS
- OTHER

NOISE
STUDY PLAN OBJECTIVES

- TO DEFINE THE EXISTING NOISE ENVIRONMENT AND LOCATE NOISE SENSITIVE AREAS
- TO DETERMINE THE REGULATORY FRAMEWORK
- TO ASSESS THE NOISE IMPACTS OF PLANT CONSTRUCTION AND PLANT OPERATION
- TO SATISFY THE REQUIREMENTS OF THE SCA AND NEPA REGULATIONS

NOISE
STUDY PLAN TASKS

1. LITERATURE SURVEY/DATA SEARCH
2. SITE SURVEY FOR NOISE SENSITIVE AREAS
3. PLAN AMBIENT NOISE SURVEY
4. CONDUCT AMBIENT NOISE SURVEY
5. ANALYZE DATA
6. COMPARE EXISTING NOISE LEVELS WITH GUIDELINES
7. ACQUIRE NOISE LEVEL DATA ON CONSTRUCTION EQUIPMENT & SCHEDULE
8. CALCULATE/ESTIMATE CONSTRUCTION NOISE IMPACT
9. COMPARE CONSTRUCTION NOISE PLUS AMBIENT WITH GUIDELINES
10. ACQUIRE NOISE LEVEL DATA ON PLANT OPERATION
11. CALCULATE/ESTIMATE OPERATIONAL NOISE IMPACT
12. COMPARE OPERATIONAL NOISE PLUS AMBIENT WITH GUIDELINES
13. REPORT PREPARATION

NOISE
STUDY PLAN TASK DESCRIPTIONS

1. LITERATURE SURVEY/DATA SEARCH
 - IDENTIFY APPLICABLE ORDINANCES, STANDARDS, GUIDELINES
 - COLLECT THE RESULTS OF ANY AVAILABLE NOISE SURVEYS
2. SITE SURVEY FOR NOISE SENSITIVE AREAS
 - MAP REVIEW AND FIELD SURVEY
 - WORK WITH SOCIOECONOMICS TASK ON LAND USE
 - LOCATE SCHOOLS, HOSPITALS, RESIDENTIAL AREAS
3. PLAN AMBIENT NOISE SURVEY
 - DETERMINE SAMPLING LOCATIONS
 - DETERMINE SAMPLING SCHEDULE
4. CONDUCT AMBIENT NOISE SURVEY
 - CONTINUOUS 24-HOUR OPERATION AT EACH SITE
 - COMPUTATION OF LEQ , LDN , L_{10} , L_{50} , L_{90}
 - CORRELATION WITH METEOROLOGICAL DATA

NOISE

5. ANALYZE DATA
 - VARIATIONS BY MONITORING LOCATION
 - DAY/NIGHT VARIATIONS
 - SEASONAL VARIATIONS
6. COMPARE EXISTING NOISE LEVELS WITH GUIDELINES
7. ACQUIRE NOISE LEVEL DATA ON CONSTRUCTION EQUIPMENT AND OBTAIN CONSTRUCTION SCHEDULE
 - LITERATURE/VENDOR INFORMATION
 - NUMBERS, TYPES, & SCHEDULE FOR EQUIPMENT OPERATION
8. CALCULATE/ESTIMATE CONSTRUCTION NOISE IMPACT
 - EXTRAPOLATE SITE NOISE LEVELS TO RECEPTORS
 - IDENTIFY CRITICAL AREAS AND CRITICAL TIMES
9. COMPARE CONSTRUCTION NOISE PLUS AMBIENT WITH GUIDELINES

NOISE

10. ACQUIRE NOISE LEVEL DATA ON PLANT OPERATION

- LITERATURE/VENDOR INFORMATION
- LOCATIONS - PLANT LAYOUT
- FANS, CRUSHERS, CONVEYORS, COOLING TOWERS, COAL YARD, UNLOADING AREA, ETC.

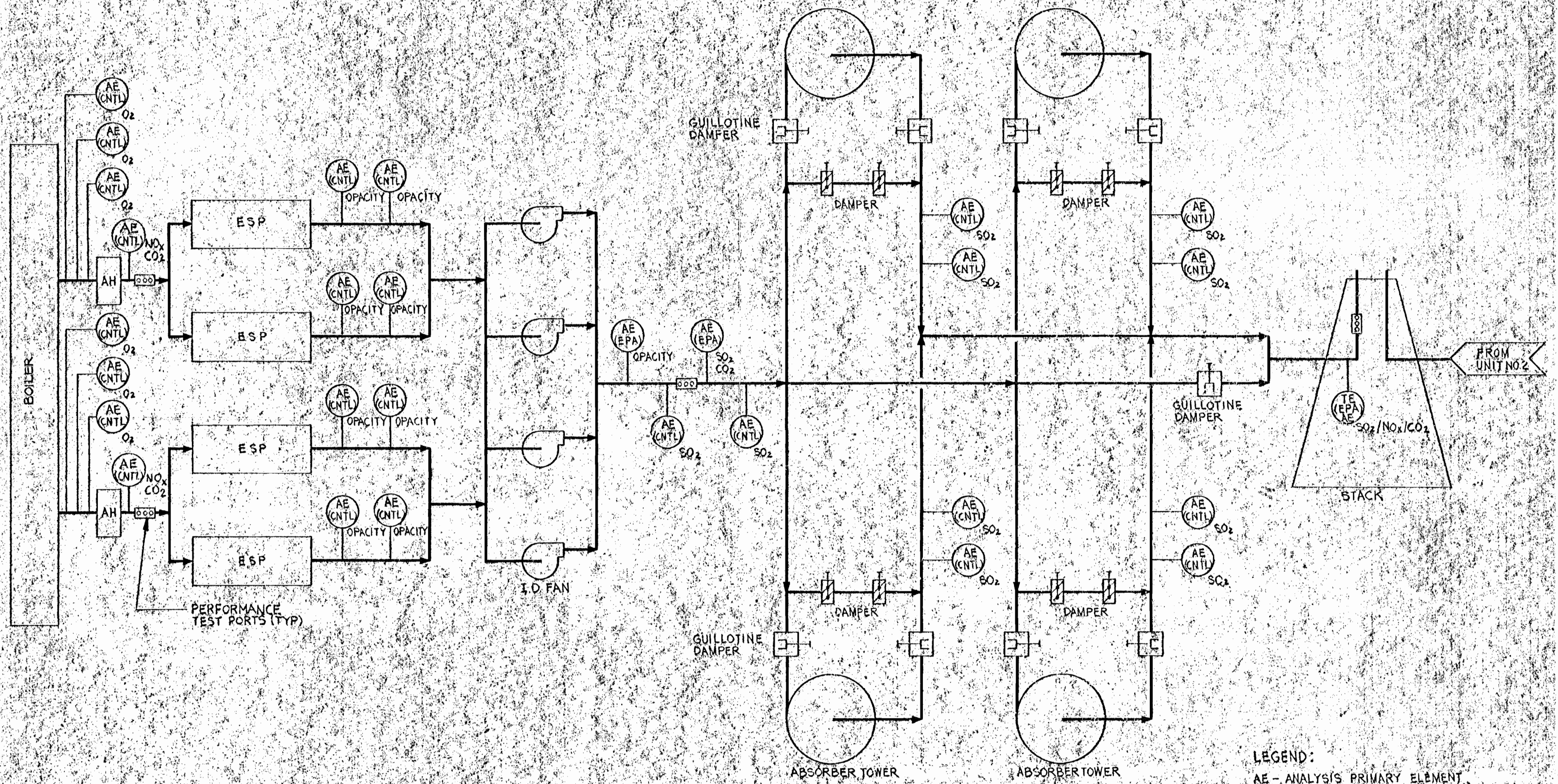
11. CALCULATE/ESTIMATE OPERATIONAL NOISE IMPACT

- CONTINUOUS SOURCES - FANS, COOLING TOWERS, ETC.
- INTERMITTENT SOURCES - COAL TRAINS, ETC.
- EXTRAPOLATE TO RECEPTORS
- IDENTIFY CRITICAL AREAS AND CRITICAL TIMES

12. COMPARE OPERATIONAL NOISE PLUS AMBIENT WITH GUIDELINES

13. REPORT PREPARATION

- SCA/EIA



FLUE GAS EMISSIONS MONITORING EQUIPMENT
(TYPICAL FOR EACH UNIT)

LEGEND:
 AE - ANALYSIS PRIMARY ELEMENT
 TE - TEMPERATURE PRIMARY ELEMENT
 EPA - ENVIRONMENTAL PROTECTION AGENCY THE SERVICE OF THE AE SHALL BE FOR THE EPA MONITORING REPORT
 CNTL - (CONTROL) THE SERVICE OF THE AE SHALL BE FOR SYSTEM CONTROL

INCHES
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POLYTRAC 033

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UNITED STATES ENVIRONMENTAL PROTECTION AGENCY

REGION IV
345 COURTLAND STREET
ATLANTA, GEORGIA 30365

DER
MAR 19 1982
BAQM

MAR 12 1982

REF: 4AW-AF

CERTIFIED MAIL RETURN RECEIPT REQUESTED

Mr. Dale A. Moehle
Division Chief
Jacksonville Electric Authority
P.O. Box 53015
Jacksonville, Florida 32201

Re: PSD-FL-010

Dear Mr. Moehle:

Review of your May 28, 1980 application to construct a 1200 MW electric generating station (plus two (2) 127 MMBtu auxiliary boilers) in Duval County, Florida has been completed. The construction is subject to rules for the Prevention of Significant Air Quality Deterioration (PSD) contained in 40 CFR §52.21. The U. S. Environmental Protection Agency performed the preliminary determination concerning the proposed construction and published a request for public comment on October 29, 1981. The only comments received were submitted by your company.

The Environmental Protection Agency has determined that the construction as described in the application meets all the applicable requirements of 40 CFR §52.21. Accordingly, enclosed with this letter is a Permit to Construct - Part I Specific Conditions and Part II General Conditions. This authority to construct is based solely on the requirements of 40 CFR §52.21, the federal regulations governing significant deterioration of air quality.

It does not authorize construction for the purposes of the NPDES program. Under that program, new source facilities may not commence construction prior to final agency action on the NPDES permit (40 CFR, §122.66). Your proposed facility has been determined to be a new source under Section 306 of the Clean Water Act, and environmental review under the National Environmental Policy Act is proceeding. Therefore, from an EPA permitting standpoint, you may not begin construction until after completion of the NEPA review process and final issuance of the Final Environmental Impact Statement (FEIS) and NPDES permit.

Please be advised that a violation of any condition issued as part of this approval, as well as any construction which proceeds in material variance with information submitted in your application, will be subject to enforcement action.

This final permitting decision is subject to appeal under 40 CFR §124.19 by petitioning the Administrator of the U. S. EPA within 30 days after receipt of this letter of approval to construct. The petitioner must submit a statement of reasons for the appeal and the Administrator must decide on the petition within a reasonable time period. If the petition is denied, the permit becomes immediately effective. The petitioner may then seek judicial review.

Authority to modify this facility will take effect on the date specified in the permit. The complete analysis which justifies this approval has been fully documented for future reference, if necessary. Any questions concerning this approval may be directed to Dr. Kent Williams, Chief, New Source Review Section, Air and Waste Management Division at (404) 881-4552.

Sincerely yours,



Charles R. Jeter
Regional Administrator

Enclosures

Best Available Copy



UNITED STATES ENVIRONMENTAL PROTECTION AGENCY

REGIONAL OFFICE
343 COURTLAND STREET
ATLANTA, GEORGIA 30336

PSD-FL-010

PERMIT TO CONSTRUCT UNDER THE RULES FOR THE
PREVENTION OF SIGNIFICANT DETERIORATION OF AIR QUALITY

Pursuant to and in accordance with the provisions of Part C, Subpart 1 of the Clean Air Act, as amended, 42 U.S.C. §7470 et seq., and the regulations promulgated thereunder at 40 C.F.R. §52.21, as amended at 45 Fed. Reg. 52676, 52735-41 (August 7, 1980),

Jacksonville Electric Authority
P.O. Box 53015
233 W. Duval
Jacksonville, Florida 32201

is hereby authorized to construct/modify a stationary source at the following location:

St. Johns River Power Park
Duval County, Florida

UTM Coordinates: 446.9 Km East - 3366.3 Km North

Upon completion of this authorized construction and commencement of operation/production, this stationary source shall be operated in accordance with the emission limitations, sampling requirements, monitoring requirements and other conditions set forth in the attached Specific Conditions (Part I) and General Conditions (Part II).

MAR 12 1982

This permit shall become effective on _____

If construction does not commence within 18 months after the effective date of this permit, or if construction is discontinued for a period of 18 months or more, or if construction is not completed within a reasonable time this permit shall expire and authorization to construct shall become invalid.

This authorization to construct/modify shall not relieve the owner or operator of the responsibility to comply fully with all applicable provisions of Federal, State, and Local law.

MAR 12 1982

Date Signed

Charles R. Jeter
Regional Administrator

Part II:

GENERAL CONDITIONS

1. The permittee shall notify the permitting authority in writing of the beginning of construction of the permitted source within 30 days of such action and the estimated date of start-up of operation.
2. The permittee shall notify the permitting authority in writing of the actual start-up of the permitted source within 30 days of such action and the estimated date of demonstration of compliance.
3. Each emission point for which an emission test method is established in this permit shall be tested in order to determine compliance with the emission limitations contained herein within sixty (60) days of achieving the maximum production rate, but in no event later than 180 days after initial start-up of the permitted source. The permittee shall notify the permitting authority of the scheduled date of compliance testing at least thirty (30) days in advance of such test. Compliance test results shall be submitted to the permitting authority within forty-five (45) days after the complete testing. The permittee shall provide (1) sampling ports adequate for test methods applicable to such facility, (2) safe sampling platforms, (3) safe access to sampling platforms, and (4) utilities for sampling and testing equipment.
4. The permittee shall retain records of all information resulting from monitoring activities and information indicating operating parameters as specified in the specific conditions of this permit for a minimum of two (2) years from the date of recording.
5. If, for any reason, the permittee does not comply with or will not be able to comply with the emission limitations specified in this permit, the permittee shall provide the permitting authority with the following information in writing postmarked within five (5) days of such conditions:
 - (a) description of noncomplying emission(s),
 - (b) cause of noncompliance,
 - (c) anticipated time the noncompliance is expected to continue or, if corrected, the duration of the period of noncompliance,
 - (d) steps taken by the permittee to reduce and eliminate the noncomplying emission,

and

- (e) steps taken by the permittee to prevent recurrence of the noncomplying emission.

Failure to provide the above information when appropriate shall constitute a violation of the terms and conditions of this permit. Submittal of this report does not constitute a waiver of the emission limitations contained within this permit.

- 6. Any change in the information submitted in the application regarding facility emissions or changes in the quantity or quality of materials processed that will result in new or increased emissions must be reported to the permitting authority. If appropriate, modifications to the permit may then be made by the permitting authority to reflect any necessary changes in the permit conditions. In no case are any new or increased emissions allowed that will cause violation of the emission limitations specified herein.
- 7. In the event of any change in control or ownership of the source described in the permit, the permittee shall notify the succeeding owner of the existence of this permit by letter and forward a copy of such letter to the permitting authority.
- 8. The permittee shall allow representatives of the state environmental control agency and/or representatives of the Environmental Protection Agency, upon the presentation of credentials:
 - (a) to enter upon the permittee's premises, or other premises under the control of the permittee, where an air pollutant source is located or in which any records are required to be kept under the terms and conditions of the permit;
 - (b) to have access to and copy at reasonable times any records required to be kept under the terms and conditions of this permit, or the Act;
 - (c) to inspect at reasonable times any monitoring equipment or monitoring method required in this permit;
 - (d) to sample at reasonable times any emission of pollutants;and
 - (e) to perform at reasonable times an operation and maintenance inspection of the permitted source.

9. All correspondence required to be submitted by this permit to the permitting agency shall be mailed to the:

Chief, Air Facilities Branch
Air and Waste Management Division
U. S. Environmental Protection Agency
Region IV
345 Courtland Street, NE
Atlanta, GA 30365

10. The conditions of this permit are severable, and if any provision of this permit, or the application of any provision of this permit to any circumstance, is held invalid, the application of such provision to other circumstances and the remainder of this permit, shall not be affected thereby.

The emission of any pollutant more frequently or at a level in excess of that authorized by this permit shall constitute a violation of the terms and conditions of this permit.

Final Determination
Jacksonville Electric Authority
PSD-FL-010

I. Applicant

Jacksonville Electric Authority
P.O. Box 53015
233 W. Duval Street
Jacksonville, Florida 32201

II. Location

The Jacksonville Electric Authority (JEA), in cooperation with Florida Power and Light Company (FPL), proposes to construct a new power generating facility consisting of two 600 megawatt (MW) coal-fired steam generating units in Duval County, Florida. The construction site, known as the St. Johns River Power Park, is located adjacent to the existing JEA Northside Generating Station, approximately 15 kilometers northeast of downtown Jacksonville, Florida. The UTM coordinates of the proposed source are 446.9 kilometers east and 3366.3 kilometers north.

III, Project Description

The applicant proposes to construct a new power generating station consisting of two 600 MW turbine-generator units powered by two pulverized coal-fired steam generators (boilers), two auxiliary boilers, and coal, limestone, and fly ash handling facilities. The two proposed steam generators will fire a maximum of 6144 million Btu's per hour (MMBtu/hr) each or approximately 292.6 tons per hour each of a medium bituminous coal having a minimum higher heating value of 10,500 Btu/lb. Of the coals under consideration, the maximum sulfur content coal has 4.0 percent sulfur by weight.

Two 127 MMBtu/hr auxiliary boilers will be utilized to provide start-up and shutdown capability for the two turbine-generating units. The auxiliary boilers will be fired with No. 2 fuel oil having a maximum sulfur content of .76 percent by weight (wt. %) and an approximate heating value of 19,500 Btu/lb.

The cooling system will consist of two counterflow natural draft cooling towers located at the north end of the plant.

The coal handling facility provides for water delivery of coal by ocean-going barge or ship to a marine terminal located on Blount Island, Florida where a 30-acre coal surge pile will be operated. The coal will be transferred from the marine terminal to the proposed plant site. The facility also will be capable of receiving direct rail car coal shipments. The coal handling equipment at the proposed plant site includes a rotary car dumper, yard area coal storage, transfer system, coal silos, and tripper floor distribution system. On the average, less than 10,000 tons per day of coal will be unloaded at the proposed source.

Limestone will be delivered to the proposed source by rail and stored in an open pile or day storage silos.

IV. Source Impact Analysis

PSD regulations amended in the August 7, 1980, Federal Register require that a new fossil fuel-fired steam electric plant with potential emissions of 100 or more tons per year of any pollutant regulated under the Act undergo a PSD review for each pollutant which results in a significant net increase in emissions. Table 1 presents an emissions summary for the proposed new source. The proposed new source has potential emission increases of sulfur dioxide (SO₂) and other pollutants of greater than 100 tons per year and significant increases in particulate matter (PM), nitrogen oxides (NO_x), carbon monoxide (CO) and SO₂. Therefore, a PSD review is required for SO₂, NO_x, PM, and CO. A full PSD review consists of the following:

- A. A demonstration that Best Available Control Technology (BACT) is being applied to all facilities emitting SO₂, PM, NO_x, and CO;
- B. An analysis of existing air quality;
- C. A demonstration that the source will not cause or contribute to any NAAQS violations;

- D. A PSD increment analysis;
- E. A growth analysis;
- F. An analysis of impacts on soils, vegetation, and visibility; and
- G. A Class I area analysis

The proposed new source will be located in an area considered attainment for all pollutants under review. A non-attainment area for PM is located in the vicinity of Jacksonville, Florida, approximately 9 kilometers from the proposed new source at its closest point. Also Duval County is nonattainment for ozone. The source however, has insignificant emissions of VOC and therefore is not subject to review for this pollutant.

The JEA's application was considered complete prior to August 7, 1980. It should be noted that Table 1 in the Preliminary Determination and the Public Notice misrepresented emissions estimates for SO₂, NO_x, CO, and PM (pounds per hour in place of tons per year). Table 1 of this determination correctly summarizes these emissions rates. A notice of correction was published for public information.

A preliminary determination and public notice were made previously regarding the proposed construction. Subsequent design modifications to the plant, necessitated the issuance of revised preliminary determination. Where necessary, additional analysis of emissions, controls, etc. were provided by the applicant. This final determination correctly reflects the design of the proposed power generating station.

A. Best Available Control Technology (BACT)

Paragraph (i)(9) of the August 7, 1980 PSD regulations exempts this source from paragraph (j) of the regulations. Instead, paragraph (j) of the June 19, 1978 PSD regulations applies. Therefore, BACT must be applied to all emission units emitting SO₂, PM, NO_x, and CO because allowable emissions of these pollutants are greater than 50 tons per year.

Sulfur Dioxide

BACT must be applied to the two proposed steam generators (boilers) and the auxiliary boiler to control SO₂ emissions.

The applicant proposes to install a lime/limestone flue gas desulfurization (FGD) system on each of the proposed steam generators as BACT for SO₂. The SO₂ removal efficiency of single FGD system is 90 percent (.76 lb/MM Btu SO₂ emissions determined in a 30-day rolling average). The applicant will maintain a minimum 70 percent control efficiency consistent with the NSPS requirements for steam generating electric plants (40 CFR 60 Subpart Da) when emission rates are below 0.6 lbs/MMBtu.

Two other emissions control systems, a lime/limestone FGD with a 95 percent SO₂ removal efficiency and a lime spray drying FGD with a 90 percent SO₂ removal efficiency, were examined. The incremental cost of the higher efficiency lime/limestone FGD system was determined not to be cost effective with respect to the resulting improvement in air quality. The lime spray drying FGD system also was rejected on the basis of economics and the existence of unfavorable operating experience. The New Source Performance Standard (NSPS) for electric utility steam generation was promulgated June 11, 1979. The NSPS limits SO₂ emissions to 10 percent of potential SO₂ emissions and a maximum emission rate of 1.2 lb/MMBtu heat input except when the emissions are less than 0.6 lb/MMBtu. At the latter emission rate, a minimum of 70 percent reduction (30 percent of potential emitted) in potential SO₂ emissions is required. The percentage reduction in potential SO₂ emissions is dependent upon the sulfur content of the coal. The proposed SO₂ control system meets all requirements of the NSPS for electric utility steam generation stations for the control of SO₂ emissions. A continuous monitor for sulfur dioxide emissions will be installed in the flue of both steam generators in accordance with 40 CFR 60.47a. The above emissions control system represents BACT for SO₂ emissions from the two proposed steam generators.

Auxiliary boilers will be fired with a maximum .76 wt. % sulfur fuel oil. The SO₂ emissions from the auxiliary boilers are small when compared to those of the main units. BACT for SO₂ emissions from the auxiliary boilers has been determined to be the firing of a maximum .76 wt.

Particulate Matter

Application of BACT is required for the emissions of PM from the two steam generators (boilers), auxiliary boilers and coal, fly ash, and limestone handling facilities.

BACT for PM emissions from the two steam generators has been determined to be the installation of an electrostatic precipitator with a PM removal efficiency of 99.78 percent (.03 lb/MMBtu). Two alternative systems, an electrostatic precipitator with a PM removal efficiency of 99.85 percent (.02 lb/MMBtu) and a fabric filter with a PM removal efficiency of 99.85 percent (.02 lb/MMBtu), were examined in the BACT analysis. The higher efficiency electrostatic precipitator was determined not to be cost effective with respect to the resulting improvement in ambient quality. The fabric filter system also was rejected on the basis of economics and the existence of unfavorable operating experience. The NSPS for electric utility steam generation limits PM emissions to .03 lb/MMBtu heat input. The proposed PM emissions control system meets the NSPS requirements for control of PM emissions. A continuous opacity monitor will be installed in the flue of both steam generators in accordance with 40 CFR 60.47a. The above system has been determined to be BACT for PM emissions from the two steam generators.

Control and collection of particulate matter emissions from the coal handling system will be accomplished by several different methods including totally enclosed conveying systems, water spray dust collection systems, and dust collection systems utilizing fabric filters.

Control of fugitive dust from limestone handling will be accomplished by the use of totally enclosed conveyors, fabric filter dust collectors, and wet suppression systems.

Fugitive fly ash emissions will be controlled at all transfer and discharge locations by fabric filters. The handling system utilized to transfer fly ash to and from ash storage silos is enclosed and exhausted to fabric filters. Transfer from silo storage will be through gravity feed chutes to covered trucks for disposal in landfills or for sale.

Fugitive dissolved and suspended particulate emissions from the cooling tower will be controlled by high efficiency drift eliminators. Table 2 presents a fugitive emissions and control summary.

The above emission control systems represents BACT for fugitive emissions.

BACT for PM emissions from the auxiliary boilers has been determined to be the firing of No. 2 fuel oil with a maximum ash content of 0.01 wt. %. Therefore, no air pollution control equipment for the purpose of PM reduction is warranted.

Nitrogen Oxides and Carbon Monoxide

BACT must be applied to the two steam generators and the auxiliary boilers to control NO_x and CO emissions. Emissions of NO_x and CO resulting from the combustion of coal is dependent on boiler design, the amount of excess air in the combustion chamber, flame temperature, burner spacing and burner design.

The applicant proposes to use combustion controls and modern boiler design for a maximum NO_x emission rate of 0.6 lb/MMBtu and to minimize CO emissions.

B. Analysis of Existing Air Quality

Paragraph (i)(9) of the August 7, 1980 PSD regulations exempts this source from paragraph (m)(1) of the regulations. Instead, paragraph (n) of the June 19, 1978 PSD regulations applies. Therefore, an analysis of existing air quality for SO₂, PM, NO_x, and CO is required as deemed necessary by the Administrator because the allowable emissions increases of these pollutants are greater than 50 tons per year.

An air quality analysis, using meteorological data from the on site monitoring program, determined the maximum pollutant concentrations at the monitoring site when the contributions from large existing sources of pollution were negligible. The sources were the JEA Northside plant and the St. Regis Paper Company. These maximum background pollutant concentrations were determined to be representative of the existing air quality in the region of the proposed source. All monitoring, data collection procedures, and modeling analyses were conducted using EPA-approved techniques. The monitoring data was utilized in the NAAQS analysis in projecting the maximum ambient air concentrations of each pollutant under review. The results are shown in Table 3.

C. NAAQS Analysis

The EPA-approved dispersion models CRSTER (modified for use with multiple point sources of emissions) and ISCST were utilized to assess the total ambient air concentrations of SO₂, PM, NO_x and CO within 50 km of the proposed plant site. Meteorological data for the years 1970 - 1974 were obtained from weather stations located at Jacksonville International Airport (surface data) and Waycross, Georgia (upper air observations). The meteorological data was determined to be representative of the weather conditions at the proposed construction site.

An emissions inventory of all increment consuming and other sources within 50 km of the proposed plant, and new sources within 100 km of the nearest Class I area was compiled. For the purpose of the modeling analysis, the main steam generating units were considered to operate continuously. This is a conservative assumption because the plant capability factor is expected to be no greater than 74 percent.

An initial modeling analysis determined that the 1973 meteorological data represented the "worst-case" year assuming a 100 percent plant load. Additional modeling at 75 percent and 50 percent load showed that a 100 percent continuous operating load resulted in the highest ground level concentrations. Therefore, the more detailed analyses were conducted using the emission parameters for the 100 percent load level. All modeling was conducted using EPA-approved modeling techniques. All stacks were modeled at Good Engineering Practice (GEP) stack height. No downwash is expected to occur as a result of turbulent building wake effects because all stacks meet GEP stack height.

The maximum ambient air concentrations for the pollutants under review were determined by modeling emissions from the proposed new source along with emissions from the JEA Northside plant and ST. Regis Paper Company. The maximum concentrations obtained from the modeling analysis were added to the maximum background concentrations (which did not include contributions from the St. Regis Paper Company or the JEA Northside plant) to obtain the maximum ambient air concentrations of each pollutant under review. This analysis is considered conservative because both the maximum monitored background and modeled concentration were not located at the same geographical point. The result of the NAAQS analysis are presented in Table 3.

A modeling analysis was conducted to determine the impact of PM emissions (including fugitive PM emissions) from the proposed new source on the PM non-attainment area located in downtown Jacksonville, Florida. The maximum impacts were projected to be below 1 ug/m^3 on an annual average and 5 ug/m^3 on a 24-hr average. These values are below the PSD ambient significance levels as defined in the June 19, 1978 PSD regulations, 43 FR 26358. Therefore, the proposed new source will not significantly impact the PM non-attainment area, in compliance with the August 7, 1980 PSD regulations paragraph (f)(4)(a).

The VOC emissions from the proposed new source are not expected to impact the ozone non-attainment area located near Jacksonville, Florida. Presently, no EPA-approved dispersion models exist with which to model ozone emissions (of which VOC is a precursor). The VOC emission levels from the proposed new source are small and not expected to significantly impact the ozone non-attainment area under any meteorological conditions.

D. Increment Analysis

The models and meteorology for determination of PM and SO₂ increment consumption were the same as those discussed in the NAAQS analysis (above). All increment consuming sources potentially affecting the ambient air quality in the area of the proposed new source were included in the modeling analysis. No violations of the Class II increment standards were predicted. The results are presented in Table 4.

E. Growth Analysis

The proposed new source is expected to directly employ about 400 people. Most of these workers will come from the local work force. No air quality impacts resulting from industrial, commercial, or residential growth associated with the proposed new source are expected.

F. Soils, Vegetation and Visibility Analysis

No soils vegetation or visibility impacts are expected to occur due to emissions from the proposed new source because of the relatively small increase in ambient pollutant concentrations.

G. Class I Area Analysis

The nearest Class I area to the proposed new source is the Okefenokee Swamp whose borders are located between 61 and 73 kilometers in a northwesterly direction. The models and meteorology used in the increment and NAAQS analyses were utilized to predict the maximum SO₂ and PM increment consumption at the borders of the Class I area. All increment consuming sources potentially impacting the Class I area were included in the modeling analysis. Five years of meteorological data were modeled. No violations of the Class I increments were predicted. The results are presented in Table 5.

No impacts on Class I area soils, vegetation or visibility are expected due to the low level of ambient air concentrations projected in the Class I area for any pollutant under review. The results of this analysis has been forwarded to the Federal Land Managers responsible for this Class I area for comment.

V. Conclusion

EPA proposes a final determination of approval with conditions for construction of the steam - electric generating station proposed by the Jacksonville Electric Authority. This final determination is based on the application received May 28, 1980 and additional information submittals dated July 8, 1980, November 26, 1980, March 6, 1981, July 30, 1981, July 31, 1981, September 8, 1981, September 21, 1981 and October 21, 1981. The application was determined to be complete as of July 9, 1980.

Approval to construct is contingent upon the following conditions;

1. The proposed steam generating station will be constructed and operated in accordance with the capacities and specifications contained in the application.
2. Emissions will not exceed the allowable emissions listed in Table 6 for SO₂, PM, and NO_x.
3. Compliance with the allowable emission limits for emission point 1 and 2, in Table 6 will be demonstrated with performance tests conducted in accordance with the provisions of 40 CFR 60.46a, 48a and 49a, including applicable test methods, sampling procedures, sample volumes, sampling periods, etc. Compliance with the emission limitations of all emission points in Table 6 will be in accordance with 40 CFR 60, Appendix A; Method 5, Determination of Particulate Emissions from Stationary Sources; Method 7, Determination of Nitrogen Oxide Emissions from Stationary Sources; Method 9, Determination of the Opacity of Emissions from Stationary Sources.

Emission points 3 thru 13 of Table 6 are exempted from mass emission rate compliance tests unless opacity limits are exceeded or the Administrator (or his representative) otherwise determines that such performance testing is required. All facilities will operate within 10 percent of maximum operating capacity during performance testing.

4. The applicant will install and maintain a continuous monitoring and recording opacity meter, sulfur dioxide, nitrogen oxide and carbon monoxide analyzers for each steam generator (emissions units 1 and 2 Table 6) in accordance with the provisions of 40 CFR 60.47a.
5. Emission points 1 and 2 of Table 6 shall fire coal with an ash content not to exceed 18% and a sulfur content not to exceed 4% by weight. Coal sulfur content shall be determined and recorded in accordance with 40 CFR 60.47a.

Emission point 3 of Table 6 shall fire No. 2 fuel oil with a maximum sulfur content of .76 percent by weight and a maximum ash content of .01 percent by weight. Samples of all fuel oil fired in the boilers shall be taken and analyzed for sulfur and ash content. Accordingly, samples shall be taken of each fuel oil shipment received. Records of the analyses shall be recorded and kept for public inspection for a minimum of two years after the data is recorded.

6. The following requirements will be met to minimize fugitive emissions of particulate matter from the coal storage and handling facilities, the limestone storage and handling facilities, haul roads and general plant operations:
 - a. All conveyors and conveyor transfer points will be enclosed to preclude PM emissions (except those directly associated with the coal stacker/reclaimer for which enclosure is operationally infeasible).
 - b. Inactive coal storage piles will be shaped, compacted and oriented to minimize wind erosion:
 - c. Water sprays or chemical wetting agents and stabilizers will be applied to storage piles, handling equipment, etc. during dry periods and as necessary to all facilities to maintain an opacity of less than or equal to 10 percent.
 - d. Limestone handling will be from bottom dump rail car delivery with wet dust suppression, and open storage or day storage silos.
 - e. The fly ash handling system (including transfer and silo storage) will be totally enclosed and vented (including pneumatic system exhaust) through fabric filters.
7. The applicant will comply with all requirements and provisions of the New Source Performance Standard for electric utility steam generating units (40 CFR 60 Part Da). In addition, the applicant must comply with the provisions and the requirements of the attached General Conditions.

Jacksonville Electric

PSD-FL-010

8. As a requirement of this specific condition, the applicant will comply with all emissions limits and enforceable restrictions required by the State of Florida Department of Environmental Regulation which are more strict operating requirements and equipment specifications than the requirements of specific conditions 1-9 of this permit.
9. This PSD approval to construct shall be valid only in the event that the stacks at the Southside (Unit 1-5) and Kennedy (Units 8, 9, 10) plants are raised to 84 meters as presented in the ambient air quality analysis for this determination; or additional modeling of air quality impacts (considering federally enforceable system operating restrictions) is submitted which demonstrate that the NAAQS will not be violated at the lower stack height under valid worst case conditions. If such modeling is to be used to show compliance with NAAQS it should be submitted prior to construction of the new units at the St. Johns River Power Park.

Table 1. EMISSIONS SUMMARY OF THE PROPOSED JEA
POWER GENERATING PLANT

Pollutant	Potential Emissions ^a (Tons per Year)	PSD Significance Levels (Tons per Year)
SO ₂	41,800	40
PM	1670	25
NO _x	32,700	40
CO	2,870	100
VOC	28 ^b	40

^a Potential emissions calculations are based on a continuous maximum operating capacity.

^b Applicant estimated 0.0005 lb VOC/MMBtu (27 tons/yr) average emissions rate from the boilers.

Table 2. Fugitive Emissions and Control Summary

Process	Type	Amount	Factor	Control	Technique	Emissions (Grams/Sec)
Ship Unloading	Grab Bucket	10,000 Tons/Day	0.4 lb/Ton ^a	(99.9%) ^b	Dry Collection on Hoppers	0.04
Ship Unloading Transfer Points	6 Points	10,000 Tons/Day	0.2 lb/Ton ^c	(99.9%) ^b	Dry Collection	0.06
Ship Unloading Transfer Points	3 Points	10,000 Tons/Day	0.2 lb/Ton ^c	(97%) ^b	Wet Suppression	0.95
Ship Unloading Facility Train	Loading Shed	10,000 Tons/Day	0.4 lb/Ton ^a	(99.9%) ^b	Dry Collection	0.02
Ship Unloading Facility Coal Surge Pile	Active	30 Acres	13 lb/Acre/Day ^a	(90%) ^a	Wetting Agent	0.20
Rail Car Unloading	Rotary Dumper	10,000 Tons/Day	0.4 lb/Ton ^a	(97%) ^b	Wet Suppression	0.63
Coal Handling Transfer Points	2 Points	10,000 Tons/Day	0.2 lb/Ton ^c	(99.9%) ^b	Dry Collection	0.02
Coal Handling Transfer Points	2 Points	3,300 Tons/Day	0.2 lb/Ton ^c	(99.9%) ^b	Dry Collection	0.01
Coal Handling Transfer Points	6 Points	3,300 Tons/Day	0.2 lb/Ton ^c	(97%) ^b	Wet Suppression	0.62
Coal Handling Transfer Points	7 Points	5,000 Tons/Day	0.2 lb/Ton ^c	(99.9%) ^b	Dry Collection	0.04
Coal Storage at Plant	Active	8 Acres	13 lb/Acre/Day ^a	(90%) ^a	Wetting Agent	0.05
Coal Storage at Plant	2 Inactive Piles	15 Acres	3.5 lb/Acre/Day ^a	(99%) ^a	Wetting Agent	0.01
Limestone Unloading	Rail Dumper	750 Tons/Day	0.4 lb/Ton ^a	(97%) ^b	Wet Suppression	0.05
Limestone Transfer	1 Point	750 Tons/Day	0.2 lb/Ton ^a	(99.9%) ^b	Dry Collection	0.001
Cooling Towers	Drift	2 x 243,500 gal/min	51,450 ppm solids (maximum) (40% < 50 microns diameter)	99.998%	Drift Eliminators	12.66
Solid Waste Disposal Area	Active	10 Acres	13 lb/Acre/Day ^a	(90%) ^a	Wetting Agent	0.07

a Pedco, 1977

b Stoughton, 1980

c USEPA, 1979

Table 3. NAAQS ANALYSIS

Pollutant/ averaging time	Monitored ^a background concentration (ug/m ³)	Maximum ^b projected concentration (ug/m ³)	Total concentration (ug/m ³)	NAAQS (ug/m ³)
SO ₂				
3-hour	90	987	1077	1,300
24-hour	21	195	216	365
annual	4	13	17	30
PM				
24-hour	50	30	80	150
annual	27	3	30	75
NO ₂				
annual	10	10	20	100
CO				
1-hour	-- ^c 5200	108 ^d	5308	40,000
8-hour	-- ^c 4500	<100 ^d	4600	20,000

^aThese values do not include contributions from the JEA Northside Plant and the St. Regis Paper Co.

^bThese concentrations include contributions from the proposed JEA steam electric generating station, the existing JEA Northside Plant and the existing St. Regis Paper Co.

^cThese values were estimated from the projected SO₂ ambient air concentrations based on worst-case operating load and meteorological conditions.

Table 4. CLASS II INCREMENT ANALYSIS

Pollutant/ averaging time	Maximum ^a Class II increment consumption (ug/m ³)	PSD Class II increment (ug/m ³)
SO ₂		
3-hour	346	512
24-hour	44	91
annual	2	20
PM		
24-hour	10	37
annual	2	19

^aThese values include contributions from all increment consuming sources impacting the ambient air quality within 50 kilometers of the proposed new source, including the proposed JEA steam electric generating station. Five years of meteorological data was used in the analysis; therefore, these values represent the highest, second highest concentrations.

Table 5. CLASS I INCREMENT ANALYSIS

Pollutant/ averaging time	Maximum ^a Class I increment consumption (ug/m ³)	PSD Class I increment (ug/m ³)
SO ₂		
3-hour	19	25
24-hour	4	5
annual	<1	2
PM		
24-hour	<1	5
annual	<1	10

^aThese values include contributions from all increment consuming sources within 100 kilometers of the Class I area including the proposed JEA electric steam generating station. Five years of meteorological data was used in the analysis; therefore, these values represent the highest, second highest concentrations.

Table 6. ALLOWABLE EMISSION LIMITS
(lb/hour; lb/MMBtu)

Emission Unit	SO ₂	NO _x	PM	Opacity (Percent)
1. Steam generating boiler no. 1 (6,144 MMBtu/hr maximum heat input)	4,669; 0.76 (30 day rolling average)	3,686; 0.6	184; 0.03	20
2. Steam generating boiler no. 2 (6,144 MMBtu/hr maximum heat input)	4,669; 0.76 (30 day rolling average)	3,686; 0.6	184; 0.03	20
3. Auxiliary boilers (254 MMBtu/hr maximum heat input total)	203; 0.8		25.0; 0.1	20
4. Ship unloading (Grab Bucket)			0.32	10
5. Ship unloading transfer points (6 dry collection points)			0.1 (ea.)	10
6. Ship unloading (3 wet suppression points)			7.5	10
7. Ship unloading facility train (loading shed)			0.2	10
8. Ship unloading facility coal storage pile (30 acres)			1.6	10

Table 6. ALLOWABLE EMISSION LIMITS
 (lb/hour; lb/MMBtu)
 (continued)

Emission Unit	SO ₂	NO _x	PM	Opacity (Percent)
9. Rail car unloading (Rotary Dumper)			5	10
10. Coal handling transfer points (6 wet suppression points)			5 (each)	10
11. Coal handling transfer points (11 dry collection)			0.1 (each)	10
12. Coal storage at plant (8 acres active)			0.4	10
13. Coal storage at plant (2-15 acre inactive piles)			0.1	10
14. Limestone unloading (rail dumper)			0.1	10
15. Limestone transfer points			0.4 (each)	10
16. Cooling towers			67 (each tower)	N/A

PM
1 Jul
Tax, FL

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Jacksonville Electric Authority

233 WEST DUVAL STREET • P. O. BOX 53015 • JACKSONVILLE, FLORIDA 32201



June 14, 1982

Mr. Kent Williams, Chief
New Source Review Section
Air Facilities Branch
U.S. Environmental Protection Agency
Region IV
345 Courtland Street, N.E.
Atlanta, Georgia 30308

RECEIVED

JUN 21 1982

DIV. ENVIRONMENTAL
PERMITTING

Dear Mr. Williams:

Subject: St. Johns River Power Park Units 1 & 2
Jacksonville Electric Authority
Florida Power & Light Company
PSD Permit Condition - Existing Stack Heights
at Southside and Kennedy

As you know, the PSD Permit for the subject units (PSD-FL-10, dated March 12, 1982) contains a specific condition (#9) regarding demonstrating compliance with the NAAQS given the existing stack heights at JEA's Southside and Kennedy plants. This condition was imposed because higher than existing stack heights were assumed in the air quality modelling supporting the PSD application.

JEA's plans at the time of the PSD modelling called for raising the stacks at Southside Units 1-5 and Kennedy 8-10 to 84 meters. However, JEA now feels that it would be more appropriate to be constrained by certain system operating restrictions as a condition of state certification than to construct the taller stacks. This position is being taken because of the planned importation of large blocks of power from Georgia Power Company which is to begin in August, 1982. This low cost purchased power combined with the subsequent operation of SJRPP will displace much of the generation from Southside and Kennedy, allowing the JEA to commit to a system operating restraint described in the State Conditions of Certification, Section I.E., in order to maintain compliance with the stringent state 24-hour SO₂ standard.

A modelling study was conducted demonstrating compliance with the State standard which assumed that Southside Units 1 and 2 would be shut down and that all other sources would operate at full load

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(CONT.)

JUN 25 1987

DIVISION CHIEF
RESEARCH & ENV. AFF.

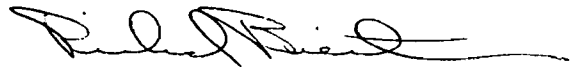
Mr. Kent Williams
June 14, 1982
Page 2.

(see letter from R. Breitmoser to H. S. Oven, Jr. dated October 7, 1981). Although this or some other system operating restriction will ultimately become a federally enforceable permit condition through a State Condition of Certification, we understand, based on an April 27, 1982 meeting with Mr. Brandon and L. Nagler of EPA, that the PSD permit condition will be satisfied by a demonstration of compliance with the NAAQS under the assumption of all JEA sources operating at full load with existing stack heights. The necessity of considering system operating restrictions to meet the more stringent State Air Quality Standards is therefore not addressed.

The attached analysis is intended to satisfy Condition #9 of the PSD Permit. A detailed modelling analysis is presented for SO₂ (Attachment 1). For TSP, an analysis is presented (Attachment 2) demonstrating that SJRPP's impacts in the vicinities of Southside and Kennedy are insignificant; thus, the stack height question is irrelevant for TSP. Discussions are presented (Attachment 3) for the remaining criteria pollutants. All results indicate compliance with NAAQS.

If you have questions on this material, please contact D. Fulle or G. Crow of Envirosphere at (404) 449-6639.

Very truly yours,



Richard Breitmoser, P.E.
Division Chief
Research & Environmental
Affairs Division

RB/lwr

cc: H. Oven (FDER)
L. Leskovjan
J. Jackson
Chief, New Generation

Attachments: As Noted

ATTACHMENT 1

SULFUR DIOXIDE

The impact of using the existing stack heights at Southside and Kennedy in the multisource modelling of SO₂ concentrations in the vicinities of those two sources was evaluated in several steps, in accordance with discussions with L. Nagler and M. Brandon of EPA on April 27, 1982. First, existing multiple source CRSTER runs were used to identify for further study a number of "worst-case" days from a short-term SO₂ standpoint in the vicinities of Southside and Kennedy for the years 1970, 1972, 1973, and 1974. These CRSTER runs (copies attached) were based on tall stacks at Southside and Kennedy, used a coarse receptor grid, and consolidated SO₂ emission sources into six sources: SJRPP, Northside Unit 3, Northside Units 1 & 2, St. Regis, Kennedy, and Southside. The results, which were reported in the PSD Application, indicated that 1973 was the worst-case year for SO₂ concentrations in the vicinity of SJRPP. These results have been re-examined to identify a series of worse-case 3-hour and 24-hour averages for the Southside and Kennedy vicinities. The days containing those periods and therefore selected for further study are listed in Table 1. The year 1971 has been identified by Florida DER as producing the worst-case 24-hour averages in the Southside and Kennedy vicinities in the 1970-1974 data base (see letter from T. Rogers to D. Lucas dated September 21, 1981). Thus, 1971 was selected for analysis in its entirety.

The next step was to run ISCST on all of 1971 and the 47 worst-case days from the other years on a .5 km spacing grid (see Figure 1) using the latest emission parameters from all of the major sources in the area and the existing stack heights at Southside and Kennedy. As can be seen from Figure 1, the receptor grid was expanded somewhat for the full year (1971) run since the results of the partial year runs indicated that high concentrations occurred near the edge of the original receptor grid in some cases. Copies of these ISCST coarse grid runs are attached.

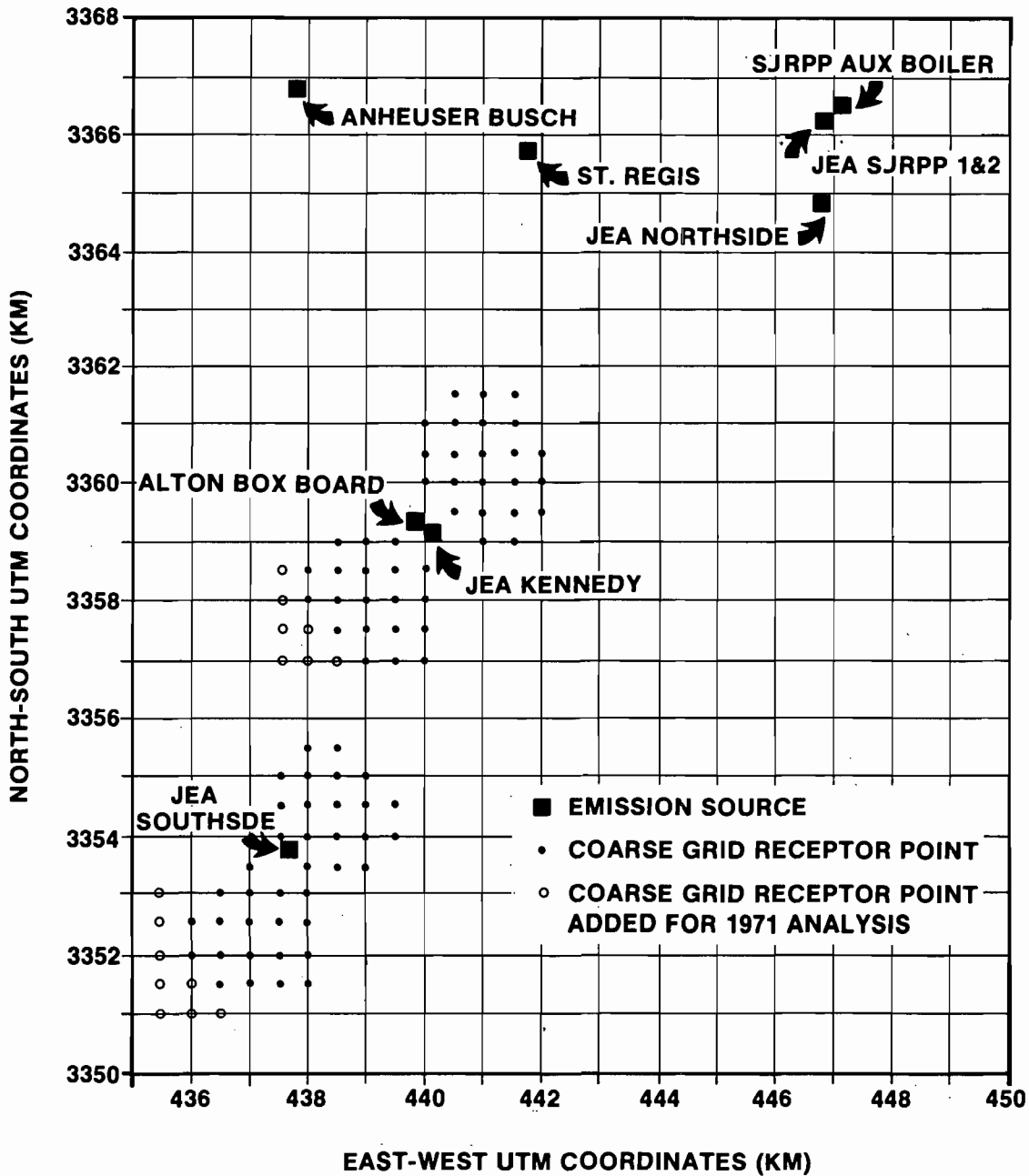
Finally, a total of 35 worst-case days were identified from the coarse grid results for further analysis using the same model and a fine (.1 km spacing) receptor grid (see Table 2). It was necessary to employ various .1 km spacing receptor grid arrays for the detailed analyses because of the variation of locations of high concentrations calculated from the 5-year coarse grid analyses. The general technique was to spatially envelope (by about 500 meters) the locations of highest concentrations identified from the coarse receptor grid analyses using the fine receptor grid. The results of the fine grid analysis are presented in Table 3, which also includes background SO₂ concentrations determined from the on-site air quality monitoring program (see Table 3 of the PSD Permit). Copies of the ISCST model runs which produced the highest and second-highest concentrations are also attached. The final results indicate compliance with the NAAQS in the Southside and Kennedy vicinities considering the existing stack heights at those facilities and all plants operating at full capacity.

TABLE 1

WORST-CASE DAYS IDENTIFIED BY
CRSTER FOR COARSE GRID ISCST ANALYSIS

<u>Year</u>	<u>Days</u>
1970	2, 15, 16, 49, 67, 102, 138, 195, 273, 290
1971	All 365 days
1972	26, 39, 40, 42, 80, 96, 131, 147, 163, 189, 204, 224, 231, 276, 285
1973	3, 7, 59, 205, 264, 278, 279, 294 295, 315, 323
1974	110, 237, 252, 263, 278, 279, 285, 295, 331, 337, 360

FIGURE 1 RECEPTOR GRID



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TABLE 2

WORST-CASE DAYS IDENTIFIED BY
ISCST FOR FINE GRID ANALYSIS

<u>Year</u>	<u>Days</u>
1970	2, 15, 16, 67, 273, 290
1971	100, 101, 110, 112, 180, 207, 273, 352, 356, 357
1972	26, 39, 42, 163, 189, 204, 231, 276, 285
1973	7, 59, 279, 294, 323
1974	237, 252, 278, 279, 331

TABLE 3
 PREDICTED MAXIMUM SO₂ CONCENTRATIONS (ug/m³)
 FROM FINE GRID ISCST ANALYSES

<u>Concentration</u>	<u>Annual</u>	<u>24-Hour</u>	<u>3-Hour</u>
Highest (Day, Year)	25 [*] -	331 (257, 1971)	828 (2, 1970)
Second Highest (Day, Year)	-	289 (356, 1971)	669 (180, 1971)
Monitored Background	4	21	90
Total	29	310	759
NAAQS	80	365	1300

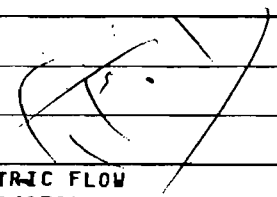
* Determined from 1971 coarse grid ISCST run only.

CRSTER ANALYSES OF
1970, 1972, 1973, and 1974
FOR WORST-CASE DAYS SELECTION

1970

CRSTER ANALYSIS
FOR WORST-CASE DAYS SELECTION

STACK # 1--JEA EASTPORT UNITS 1 AND 2		
SOURCE LOCATION FROM CENTER OF RECEPTOR GRID (DIR,DIST(KM))	0.00	0.00
STACK # 2--JEA NORTHSIDE UNITS 1 AND 2		
SOURCE LOCATION FROM CENTER OF RECEPTOR GRID (DIR,DIST(KM))	180.00	1.40
STACK # 3--JEA NORTHSIDE UNIT 3		
SOURCE LOCATION FROM CENTER OF RECEPTOR GRID (DIR,DIST(KM))	180.60	1.40
STACK # 4--JEA KENNEDY UNITS 7,8,9		
SOURCE LOCATION FROM CENTER OF RECEPTOR GRID (DIR,DIST(KM))	223.99	10.01
STACK # 5--JEA SOUTHSIDE UNITS 1,2,3,4,5		
SOURCE LOCATION FROM CENTER OF RECEPTOR GRID (DIR,DIST(KM))	216.80	15.61
STACK # 6--ST. REGIS PAPER ALL SOURCES		
SOURCE LOCATION FROM CENTER OF RECEPTOR GRID (DIR,DIST(KM))	265.76	6.77



STACK	MONTH	EMISSION RATE (GMS/SEC)	HEIGHT (METERS)	DIAMETER (METERS)	EXIT VELOCITY (M/SEC)	TEMP (DEG.K)	VOLUMETRIC FLOW (M ³ /SEC)
1	ALL	1138.3000	194.16	10.13	18.29	327.60	1474.08
2	ALL	1256.7000	91.40	5.33	8.50	408.00	189.65
3	ALL	1194.9000	106.70	7.01	17.40	407.00	671.54
4	ALL	308.4000	84.00	4.12	23.20	408.00	309.29
5	ALL	465.8000	84.00	4.27	21.60	422.00	309.31
6	ALL	208.4000	32.30	2.13	16.10	433.00	57.37

70

SO₂ CRATOR
 Worst Case days
 2000-2400
 JEA SS + Kennedy

PLANT NAME: JACKSONVILLE ELECTRIC AU POLLUTANT: THORITY EMISSION UNITS: GM/SEC AIR QUALITY UNITS: GM/H**3

MAXIMUM MEAN CONC= 9.3497E-06 DIRECTION= 24 DISTANCE= 7.5 KM

ANNUAL MEAN CONCENTRATION AT EACH RECEPTOR

DIR	RANGE	7.5 KM	11.0 KM	12.0 KM	16.5 KM	17.5 KM
20		7.96803E-06	5.66418E-06	5.34699E-06	4.34095E-06	4.64400E-06
21		8.14648E-06	7.03095E-06	7.10508E-06	3.93700E-06	3.73798E-06
22		9.05958E-06	7.08845E-06	6.14580E-06	4.06165E-06	4.04312E-06
23		7.78359E-06	5.57692E-06	5.59725E-06	6.00224E-06	5.11004E-06
24		9.34966E-06	8.50368E-06	7.68694E-06	7.47040E-06	7.02492E-06

PLANT NAME: JACKSONVILLE ELECTRIC AU POLLUTANT: THORITY EMISSION UNITS: GM/SEC AIR QUALITY UNITS: GM/M**3

YEARLY MAXIMUM 24-HOUR CONC= 9.4291E-05 DIRECTION= 23 DISTANCE= 7.5 KM DAY=290

HIGHEST 24-HOUR CONCENTRATION AT EACH RECEPTOR

RANGE	7.5 KM	11.0 KM	12.0 KM	16.5 KM	17.5 KM
DIR					
20	8.6645E-05 (2)	5.5325E-05 (2)	5.0949E-05 (2)	4.1478E-05 (2)	4.3041E-05 (2)
21	8.6209E-05 (14)	6.1932E-05 (14)	5.4401E-05 (14)	5.5891E-05 (37)	5.0338E-05 (37)
22	8.2102E-05 (16)	7.1957E-05 (16)	6.6468E-05 (16)	5.2591E-05 (16)	5.0173E-05 (16)
23	9.4291E-05 (290)	6.8850E-05 (290)	6.1591E-05 (290)	5.5564E-05 (16)	5.5848E-05 (38)
24	9.0757E-05 (256)	9.0482E-05 (38)	9.0505E-05 (38)	9.2291E-05 (38)	8.5441E-05 (38)

PLANT NAME: JACKSONVILLE ELECTRIC AU POLLUTANT: THORITY EMISSION UNITS: GM/SEC AIR QUALITY UNITS: GM/M**3

YEARLY SECOND MAXIMUM 24-HOUR CONC= 8.4755E-05 DIRECTION= 24 DISTANCE= 17.5 KM DAY= 15

SECOND HIGHEST 24-HOUR CONCENTRATION AT EACH RECEPTOR

RANGE	7.5 KM	11.0 KM	12.0 KM	16.5 KM	17.5 KM
DIR					
20	7.5695E-05 (348)	5.3599E-05 (13)	4.9157E-05 (13)	3.9502E-05 (13)	3.8843E-05 (13)
21	5.6976E-05 (38)	5.8803E-05 (272)	5.0515E-05 (36)	4.4866E-05 (13)	4.3403E-05 (13)
22	5.7730E-05 (125)	7.1212E-05 (275)	5.7404E-05 (275)	4.8440E-05 (13)	4.6035E-05 (14)
23	7.5970E-05 (15)	5.5095E-05 (38)	4.9824E-05 (38)	5.3631E-05 (290)	5.4871E-05 (16)
24	8.4485E-05 (180)	7.4001E-05 (102)	7.6437E-05 (102)	8.3741E-05 (21)	8.4755E-05 (15)

PLANT NAME: JACKSONVILLE ELECTRIC AU POLLUTANT: THORITY EMISSION UNITS: GM/SEC AIR QUALITY UNITS: GM/H**3

YEARLY MAXIMUM 3-HOUR CONC= 4.6547E-04 DIRECTION= 20 DISTANCE= 7.5 KM DAY= 2 TIME PERIOD= 4

DIR	3-HOUR CONCENTRATION AT EACH RECEPTOR				
	HIGHEST 7.5 KM	11.0 KM	12.0 KM	16.5 KM	17.5 KM
20	4.6547E-04 (2, 4)	3.4947E-04 (2) 4)	3.2266E-04 (2) 4)	2.3789E-04 (2, 4)	2.2464E-04 (2) 4)
21	2.4842E-04 (14, 4)	2.2255E-04 (3) 1)	2.0855E-04 (38, 1)	1.8474E-04 (37, 6)	1.8792E-04 (37, 6)
22	2.4991E-04 (227, 5)	1.9533E-04 (272, 4)	1.8619E-04 (67, 7)	2.0356E-04 (67) 7)	2.0375E-04 (67, 7)
23	2.5178E-04 (65, 4)	1.7722E-04 (125, 5)	1.7321E-04 (341, 4)	1.6669E-04 (168, 3)	1.6239E-04 (284, 6)
24	2.4363E-04 (138, 4)	2.4231E-04 (103) 5)	2.5441E-04 (102) 5)	2.2199E-04 (108) 5)	2.0834E-04 (102) 5)

> 240

> 240

PLANT NAME: JACKSONVILLE ELECTRIC AU POLLUTANT: THORITY EMISSION UNITS: GM/SEC AIR QUALITY UNITS: GM/M**3

YEARLY SECOND MAXIMUM 3-HOUR CONC= 2.5656E-04 DIRECTION= 20 DISTANCE= 7.5 KM DAY=275 TIME PERIOD= 4

RANGE	SECOND HIGHEST	3-HOUR CONCENTRATION AT EACH RECEPTOR			
	7.5 KM	11.0 KM	12.0 KM	16.5 KM	17.5 KM
DIR					
20	2.5656E-04 (275, 4)	1.9096E-04 (266, 3)	1.7890E-04 (266, 3)	1.9112E-04 (195, 19)	2.0500E-04 (195, 11)
21	2.3068E-04 (299, 4)	2.1294E-04 (49, 1)	1.8114E-04 (86, 3)	1.7107E-04 (86, 3)	1.7270E-04 (141, 8)
22	2.0099E-04 (290, 1)	1.7294E-04 (67, 7)	1.8478E-04 (272, 4)	1.8137E-04 (273, 6)	1.8308E-04 (273, 6)
23	1.9977E-04 (5, 4)	1.7499E-04 (341, 4)	1.6899E-04 (125, 5)	1.6545E-04 (330, 4)	1.6160E-04 (38, 3)
24	2.2114E-04 (251, 4)	1.9181E-04 (342, 6)	1.8339E-04 (342, 6)	1.9221E-04 (138, 7)	1.9816E-04 (138, 7)

1972

CRSTER ANALYSIS
FOR WORST-CASE DAYS SELECTION

STACK # 1--JEA EASTPORT UNITS 1 AND 2

SOURCE LOCATION FROM CENTER OF RECEPTOR GRID (DIR,DIST(KM)) 0.00 0.00

STACK # 2--JEA NORTHSIDE UNITS 1 AND 2

SOURCE LOCATION FROM CENTER OF RECEPTOR GRID (DIR,DIST(KM)) 180.00 1.40

STACK # 3--JEA NORTHSIDE UNIT 3

SOURCE LOCATION FROM CENTER OF RECEPTOR GRID (DIR,DIST(KM)) 180.00 1.40

STACK # 4--JEA KENNEDY UNITS 7,8,9

SOURCE LOCATION FROM CENTER OF RECEPTOR GRID (DIR,DIST(KM)) 223.99 10.01

STACK # 5--JEA SOUTHSIDE UNITS 1,2,3,4,5

SOURCE LOCATION FROM CENTER OF RECEPTOR GRID (DIR,DIST(KM)) 216.80 15.61

STACK # 6--ST. REGIS PAPER ALL SOURCES

SOURCE LOCATION FROM CENTER OF RECEPTOR GRID (DIR,DIST(KM)) 265.76 6.77

STACK	MONTH	EMISSION RATE (GMS/SEC)	HEIGHT (METERS)	DIAMETER (METERS)	EXIT VELOCITY (M/SEC)	TEMP (DEG.K)	VOLUMETRIC FLOW (M**3/SEC)
1	ALL	1138.3000	194.16	10.13	18.29	327.60	1474.08
2	ALL	1256.7000	91.40	5.33	8.50	408.00	189.65
3	ALL	1194.9000	106.70	7.01	17.40	407.00	671.54
4	ALL	308.4000	84.00	4.12	23.20	408.00	309.29
5	ALL	465.8000	84.00	4.27	21.60	422.00	309.31
6	ALL	208.4000	32.30	2.13	16.10	433.00	57.37

PLANT NAME: JACKSONVILLE ELECTRIC AU POLLUTANT: THORITY EMISSION UNITS: GM/SEC AIR QUALITY UNITS: GM/M**3

MAXIMUM MEAN CONC= 1.3099E-05 DIRECTION= 23 DISTANCE= 7.5 KM

ANNUAL MEAN CONCENTRATION AT EACH RECEPTOR

DIR	RANGE	7.5 KM	11.0 KM	12.0 KM	16.5 KM	17.5 KM
20		8.83945E-06	8.56783E-06	7.83199E-06	7.33785E-06	7.52563E-06
21		1.06674E-05	9.73782E-06	1.02099E-05	7.19759E-06	6.75801E-06
22		1.26133E-05	1.11838E-05	1.02183E-05	8.68249E-06	9.22195E-06
23		1.30985E-05	1.16026E-05	1.19889E-05	1.00544E-05	9.50683E-06
24		1.16091E-05	1.08774E-05	1.08002E-05	1.01323E-05	9.99659E-06

PLANT NAME: JACKSONVILLE ELECTRIC AU POLLUTANT: THORITY EMISSION UNITS: GM/SEC AIR QUALITY UNITS: GM/M**3

YEARLY MAXIMUM 24-HOUR CONC= 1.2144E-04 DIRECTION= 23 DISTANCE= 7.5 KM DAY=163

HIGHEST 24-HOUR CONCENTRATION AT EACH RECEPTOR

RANGE	7.5 KM	11.0 KM	12.0 KM	16.5 KM	17.5 KM
DIR					
20	5.4369E-05 (39)	6.8579E-05 (40)	7.1507E-05 (40)	7.3354E-05 (40)	7.2914E-05 (40)
21	7.9583E-05 (285)	9.7634E-05 (39)	9.9960E-05 (39)	9.1849E-05 (39)	8.6957E-05 (39)
22	8.6153E-05 (100)	8.3740E-05 (26)	8.0707E-05 (26)	7.7206E-05 (285)	7.9111E-05 (285)
23	1.2144E-04 (163)	8.9449E-05 (26)	8.6736E-05 (26)	8.3905E-05 (26)	8.4558E-05 (26)
24	5.9524E-05 (66)	7.2398E-05 (80)	7.1285E-05 (80)	7.4475E-05 (163)	7.6864E-05 (163)

PLANT NAME: JACKSONVILLE ELECTRIC AU POLLUTANT: THORITY EMISSION UNITS: GM/SEC AIR QUALITY UNITS: GM/M**3

YEARLY SECOND MAXIMUM 24-HOUR CONC= 8.8565E-05 DIRECTION= 23 DISTANCE= 7.5 KM DAY=131

SECOND HIGHEST 24-HOUR CONCENTRATION AT EACH RECEPTOR

RANGE	7.5 KM	11.0 KM	12.0 KM	16.5 KM	17.5 KM
DIR					
20	5.3831E-05 (246)	5.3819E-05 (39)	5.2664E-05 (39)	5.2846E-05 (17)	5.4064E-05 (17)
21	7.4148E-05 (334)	8.1729E-05 (42)	8.2471E-05 (42)	6.6031E-05 (329)	6.4165E-05 (42)
22	8.5793E-05 (284)	7.9246E-05 (342)	7.8858E-05 (342)	7.2636E-05 (342)	7.1420E-05 (342)
23	8.8565E-05 (131)	7.8062E-05 (276)	8.1426E-05 (276)	7.7513E-05 (276)	7.5925E-05 (276)
24	5.8888E-05 (33)	6.5844E-05 (346)	7.0256E-05 (96)	6.3347E-05 (80)	5.9871E-05 (276)

PLANT NAME: JACKSONVILLE ELECTRIC AU POLLUTANT: THORITY EMISSION UNITS: GM/SEC AIR QUALITY UNITS: GM/H**3

YEARLY MAXIMUM 3-HOUR CONC= 3.5234E-04 DIRECTION= 21 DISTANCE= 7.5 KM DAY=224 TIME PERIOD= 3

DIR	3-HOUR CONCENTRATION AT EACH RECEPTOR				
	HIGHEST RANGE 7.5 KM	11.0 KM	12.0 KM	16.5 KM	17.5 KM
20	3.1662E-04 (314, 4)	2.1789E-04 (17, 3)	2.2278E-04 (17, 3)	2.1289E-04 (17, 3)	2.0772E-04 (17, 3)
21	3.5234E-04 (224, 3)	2.9195E-04 (23, 6)	2.8190E-04 (231, 6)	2.3563E-04 (231, 6)	2.2640E-04 (231, 6)
22	2.4128E-04 (117, 5)	2.2838E-04 (99, 7)	2.2190E-04 (99, 7)	2.0750E-04 (117, 4)	2.0295E-04 (117, 4)
23	3.0264E-04 (163, 3)	2.7641E-04 (204, 4)	2.5240E-04 (204, 4)	2.3553E-04 (189, 6)	2.3244E-04 (189, 6)
24	2.5804E-04 (121, 5)	2.5685E-04 (80, 4)	2.6373E-04 (131, 7)	2.3949E-04 (131, 7)	2.2677E-04 (131, 7)

PLANT NAME: JACKSONVILLE ELECTRIC AU POLLUTANT: THORITY EMISSION UNITS: GM/SEC AIR QUALITY UNITS: GM/M**3

YEARLY SECOND MAXIMUM 3-HOUR CONC= 3.2195E-04 DIRECTION= 21 DISTANCE= 7.5 KM DAY=231 TIME PERIOD= 6

DIR	SECOND HIGHEST		3-HOUR CONCENTRATION AT EACH RECEPTOR			
	RANGE	7.5 KM	11.0 KM	12.0 KM	16.5 KM	17.5 KM
20	3.0112E-04	(231, 6)	2.0579E-04 (243, 1)	2.0045E-04 (245, 3)	1.8806E-04 (341, 6)	1.9571E-04 (341, 6)
21	3.2195E-04	(231, 6)	2.6184E-04 (224, 3)	2.1124E-04 (224, 3)	1.7578E-04 (304, 7)	2.0471E-04 (348, 1)
22	2.2497E-04	(100, 2)	2.2103E-04 (295, 5)	2.1976E-04 (156, 3)	1.9390E-04 (244, 5)	2.0069E-04 (244, 5)
23	2.8570E-04	(353, 5)	2.6679E-04 (147, 6)	2.4807E-04 (189, 6)	2.1063E-04 (204, 4)	2.0447E-04 (204, 4)
24	2.4729E-04	(235, 6)	2.4932E-04 (131, 7)	2.5748E-04 (80, 4)	1.9550E-04 (80, 4)	1.7964E-04 (80, 4)

1973

CRSTER ANALYSIS
FOR WORST-CASE DAYS SELECTION

STACK # 1--JEA EASTPORT UNITS 1 AND 2		
SOURCE LOCATION FROM CENTER OF RECEPTOR GRID (DIR,DIST(KM))	0.00	0.00
STACK # 2--JEA NORTHSIDE UNITS 1 AND 2		
SOURCE LOCATION FROM CENTER OF RECEPTOR GRID (DIR,DIST(KM))	180.00	1.40
STACK # 3--JEA NORTHSIDE UNIT 3		
SOURCE LOCATION FROM CENTER OF RECEPTOR GRID (DIR,DIST(KM))	180.00	1.40
STACK # 4--JEA KENNEDY UNITS 7,8,9		
SOURCE LOCATION FROM CENTER OF RECEPTOR GRID (DIR,DIST(KM))	223.99	10.01
STACK # 5--JEA SOUTHSIDE UNITS 1,2,3,4,5		
SOURCE LOCATION FROM CENTER OF RECEPTOR GRID (DIR,DIST(KM))	216.80	15.61
STACK # 6--ST. REGIS PAPER ALL SOURCES		
SOURCE LOCATION FROM CENTER OF RECEPTOR GRID (DIR,DIST(KM))	265.76	6.77

STACK	MONTH	EMISSION RATE (GMS/SEC)	HEIGHT (METERS)	DIAMETER (METERS)	EXIT VELOCITY (M/SEC)	TEMP (DEG.K)	VOLUMETRIC FLOW (M**3/SEC)
1	ALL	1138.3000	194.16	10.13	18.29	327.60	1474.09
2	ALL	1256.7000	91.40	5.33	8.50	408.00	189.65
3	ALL	1194.9000	106.70	7.01	17.40	407.00	671.54
4	ALL	308.4000	84.00	6.12	23.20	408.00	309.29
5	ALL	465.8000	84.00	4.27	21.60	422.00	309.31
6	ALL	208.4000	32.30	2.13	16.10	433.00	57.37

MAXIMUM MEAN CONC= 1.2510E-05 DIRECTION= 24 DISTANCE= 7.5 KM

FORM 4513

DIR	RANGE	ANNUAL MEAN CONCENTRATION AT EACH RECEPTOR				
		7.5 KM	11.0 KM	12.0 KM	16.5 KM	17.5 KM
2		6.10739E-05	6.09518E-06	5.77724E-06	5.65451E-06	5.57470E-06
3		6.65070E-06	6.30487E-06	6.33169E-06	5.87145E-06	5.72773E-06
4		7.61290E-06	7.32344E-06	7.13549E-06	6.37423E-06	6.21143E-06
5		7.69724E-05	6.74780E-06	6.53704E-06	5.67196E-06	5.54242E-06
6		7.98860E-06	7.09585E-06	6.87406E-06	6.23751E-06	6.04377E-06
7		8.51708E-06	7.18157E-06	6.86273E-06	5.69547E-06	5.49209E-06
8		7.12156E-05	5.76763E-06	5.39190E-06	4.33751E-06	4.22880E-06
9		6.06540E-05	4.52750E-06	4.30109E-06	3.54083E-06	3.37471E-06
10		5.16897E-05	3.46196E-06	3.49324E-06	3.15397E-06	3.00209E-06
11		6.29911E-06	3.77152E-06	3.95296E-06	3.11643E-06	3.00242E-06
12		6.42545E-06	5.06836E-06	4.81538E-06	3.32917E-06	2.93976E-06
20		7.31164E-06	7.33370E-06	5.29215E-06	4.74520E-06	4.59207E-06
21		1.00750E-05	8.36895E-06	8.14618E-06	5.33315E-06	4.96410E-06
22		1.14586E-05	9.54312E-06	8.33667E-06	7.10096E-06	7.63646E-06
23		1.8669E-05	8.94090E-06	8.49028E-06	7.22314E-06	6.97363E-06
24		1.25097E-05	9.59506E-06	9.03445E-06	9.25675E-06	8.77766E-06
25		1.18217E-05	9.92826E-06	9.84340E-06	8.71945E-06	8.29513E-06
26		1.12824E-05	1.05186E-05	9.80124E-06	6.54379E-06	6.28045E-06
27		1.09724E-05	8.22456E-06	7.65217E-06	4.10707E-06	4.09084E-06
28		9.36503E-06	8.94375E-06	7.65993E-06	4.22000E-06	4.07243E-06
29		1.23087E-05	8.20937E-06	8.20090E-06	4.82629E-06	4.72004E-06
30		1.21654E-05	7.87491E-06	7.49807E-06	5.05717E-06	5.22593E-06

YEARLY MAXIMUM 24-HOUR CONC= 1.0672E-04 DIRECTION= 30 DISTANCE= 7.5 KM DAY=339

HIGHEST 24-HOUR CONCENTRATION AT EACH RECEPTOR

RANGE	7.5 KM	11.0 KM	12.0 KM	16.5 KM	17.5 KM
DIR					
2	5.8490E-05 (331)	6.4934E-05 (329)	5.5592E-05 (364)	6.3378E-05 (329)	6.1892E-05 (329)
3	7.0343E-05 (196)	7.2239E-05 (347)	7.2900E-05 (347)	6.7775E-05 (347)	6.8314E-05 (347)
4	7.3314E-05 (347)	6.1077E-05 (347)	5.6606E-05 (197)	4.7943E-05 (140)	4.7424E-05 (329)
5	7.4266E-05 (329)	5.2921E-05 (329)	5.1079E-05 (144)	4.6703E-05 (289)	4.6485E-05 (289)
6	1.0670E-04 (289)	9.9230E-05 (289)	9.5279E-05 (289)	7.7772E-05 (289)	7.4340E-05 (289)
7	1.0091E-04 (137)	7.1917E-05 (137)	6.5339E-05 (137)	4.5046E-05 (289)	4.2697E-05 (289)
8	5.5752E-05 (165)	4.6909E-05 (357)	4.5828E-05 (357)	3.9543E-05 (357)	3.7957E-05 (357)
9	5.5923E-05 (229)	5.1253E-05 (229)	4.8831E-05 (229)	3.7740E-05 (253)	3.8388E-05 (131)
10	5.4036E-05 (137)	3.7380E-05 (355)	3.7619E-05 (131)	5.6270E-05 (34)	5.5779E-05 (34)
11	4.9199E-05 (27)	4.7335E-05 (141)	4.4490E-05 (141)	4.2046E-05 (78)	3.9933E-05 (78)
12	6.3897E-05 (180)	4.3574E-05 (169)	4.6309E-05 (169)	6.4620E-05 (351)	4.3170E-05 (351)
20	5.8936E-05 (3)	8.9150E-05 (294)	5.1795E-05 (234)	5.2853E-05 (294)	7.4262E-05 (294)
21	9.2308E-05 (59)	7.1600E-05 (315)	6.4596E-05 (295)	5.3560E-05 (294)	5.6605E-05 (294)
22	7.4988E-05 (236)	6.9725E-05 (279)	6.3019E-05 (310)	8.5224E-05 (7)	8.5598E-05 (7)
23	6.3180E-05 (278)	6.9998E-05 (279)	5.6157E-05 (259)	7.1052E-05 (279)	7.0713E-05 (279)
24	7.9059E-05 (231)	5.6781E-05 (17)	5.9819E-05 (275)	5.9852E-05 (276)	5.7236E-05 (275)
25	7.4181E-05 (12)	5.9664E-05 (283)	5.6704E-05 (87)	6.4939E-05 (83)	6.5009E-05 (83)
26	8.8878E-05 (245)	7.0981E-05 (245)	6.2920E-05 (244)	5.1040E-05 (245)	4.4074E-05 (245)
27	8.7766E-05 (120)	8.3683E-05 (56)	7.0452E-05 (55)	4.4514E-05 (158)	3.3334E-05 (105)
28	7.5717E-05 (157)	7.2457E-05 (244)	5.5696E-05 (61)	3.9997E-05 (133)	4.6731E-05 (61)
29	8.1975E-05 (360)	5.7095E-05 (120)	6.1352E-05 (120)	5.3648E-05 (120)	5.2807E-05 (120)
30	1.0672E-04 (339)	8.7771E-05 (127)	8.1430E-05 (127)	6.6664E-05 (127)	6.0787E-05 (127)

YEARLY SECOND MAXIMUM 24-HOUR CONC= 9.7125E-05 DIRECTION= 7 DISTANCE= 7.5 KM DAY= 95

FORM 4111

RANGE DIR	SECOND HIGHEST 24-HOUR CONCENTRATION AT EACH RECEPTOR				
	7.5 KM	11.0 KM	12.0 KM	16.5 KM	17.5 KM
2	5.8255E-05 (223)	5.5462E-05 (364)	5.1643E-05 (304)	5.4527E-05 (364)	5.3894E-05 (364)
3	6.2221E-05 (75)	6.6285E-05 (75)	6.2801E-05 (75)	4.9922E-05 (196)	4.9515E-05 (195)
4	6.5592E-05 (123)	5.9752E-05 (304)	5.5341E-05 (123)	4.7682E-05 (329)	4.5745E-05 (140)
5	6.3565E-05 (171)	4.9908E-05 (147)	4.8904E-05 (147)	4.4655E-05 (144)	4.3361E-05 (144)
6	9.0212E-05 (186)	7.8911E-05 (186)	7.4471E-05 (185)	6.5441E-05 (137)	6.5903E-05 (137)
7	9.7125E-05 (85)	7.0286E-05 (85)	6.2739E-05 (85)	4.4685E-05 (137)	4.2301E-05 (140)
8	5.5057E-05 (233)	4.1546E-05 (233)	3.8820E-05 (233)	3.2631E-05 (313)	3.2029E-05 (175)
9	5.4250E-05 (117)	4.9867E-05 (253)	4.7643E-05 (253)	3.6725E-05 (131)	3.6159E-05 (253)
10	5.2929E-05 (143)	3.5157E-05 (143)	3.5529E-05 (309)	3.2881E-05 (76)	3.8682E-05 (76)
11	4.8340E-05 (209)	3.8927E-05 (53)	3.7070E-05 (180)	3.4438E-05 (274)	3.3179E-05 (274)
12	6.3466E-05 (165)	4.1460E-05 (351)	4.0623E-05 (29)	4.1746E-05 (169)	3.4269E-05 (169)
20	5.7662E-05 (294)	5.3516E-05 (293)	4.8099E-05 (177)	4.4641E-05 (295)	5.7895E-05 (9)
21	7.5414E-05 (7)	7.0590E-05 (7)	6.1736E-05 (7)	5.4873E-05 (315)	5.0856E-05 (315)
22	6.7483E-05 (279)	6.4471E-05 (295)	6.1632E-05 (295)	7.0453E-05 (59)	7.6072E-05 (59)
23	5.8638E-05 (238)	5.8281E-05 (206)	5.3648E-05 (205)	6.3860E-05 (280)	6.3921E-05 (290)
24	7.1250E-05 (184)	5.1900E-05 (276)	5.1329E-05 (281)	4.7944E-05 (281)	4.7545E-05 (358)
25	6.3983E-05 (182)	4.9215E-05 (87)	5.4239E-05 (283)	5.2617E-05 (246)	5.9537E-05 (246)
26	7.6286E-05 (182)	6.3375E-05 (182)	6.2756E-05 (245)	4.6783E-05 (244)	4.3879E-05 (244)
27	7.0052E-05 (203)	6.9804E-05 (241)	6.3959E-05 (241)	3.5260E-05 (105)	3.2375E-05 (55)
28	5.8697E-05 (133)	6.3538E-05 (203)	5.5039E-05 (111)	3.4113E-05 (247)	3.9365E-05 (133)
29	7.7655E-05 (120)	5.6900E-05 (243)	5.9325E-05 (243)	3.5757E-05 (324)	4.9307E-05 (269)
30	9.2568E-05 (127)	6.8246E-05 (159)	6.4515E-05 (159)	4.0907E-05 (160)	4.8801E-05 (32)

YEARLY MAXIMUM 3-HOUR CONC= 3.9860E-04 DIRECTION= 6 DISTANCE= 7.5 KM DAY=289 TIME PERIOD= 5

FORM 8111

RANGE DIR	3-HOUR CONCENTRATION AT EACH RECEPTOR				
	HIGHEST 7.5 KM	11.0 KM	12.0 KM	16.5 KM	17.5 KM
2	3.0965E-04 (331, 4)	2.3766E-04 (331, 4)	2.3625E-04 (364, 3)	2.1939E-04 (364, 3)	2.1398E-04 (364, 3)
3	2.9792E-04 (311, 5)	2.8233E-04 (179, 3)	2.7704E-04 (179, 3)	2.4603E-04 (179, 3)	2.3899E-04 (179, 3)
4	2.9196E-04 (347, 8)	2.3729E-04 (347, 8)	2.3822E-04 (323, 1)	2.9224E-04 (323, 1)	2.9552E-04 (323, 1)
5	2.9795E-04 (329, 5)	2.2761E-04 (329, 5)	2.0455E-04 (329, 5)	1.9967E-04 (320, 2)	2.0164E-04 (320, 2)
6	3.9860E-04 (289, 5)	3.1253E-04 (289, 5)	2.9040E-04 (289, 4)	2.5498E-04 (289, 4)	2.4685E-04 (289, 4)
7	3.9495E-04 (289, 4)	2.2475E-04 (186, 3)	2.0910E-04 (197, 3)	1.9952E-04 (348, 6)	1.9622E-04 (343, 6)
8	3.0647E-04 (357, 4)	3.0070E-04 (357, 4)	2.7875E-04 (357, 4)	1.9311E-04 (357, 4)	1.7953E-04 (357, 4)
9	3.2151E-04 (229, 3)	2.3558E-04 (253, 3)	2.3720E-04 (253, 3)	1.8104E-04 (98, 3)	1.7658E-04 (93, 3)
10	2.7991E-04 (193, 1)	2.2160E-04 (6, 4)	2.2255E-04 (6, 4)	2.1030E-04 (6, 4)	2.0184E-04 (3, 4)
11	3.1015E-04 (335, 5)	2.4311E-04 (335, 6)	2.2429E-04 (303, 4)	1.9758E-04 (303, 4)	1.8996E-04 (303, 4)
12	2.5668E-04 (307, 6)	1.9122E-04 (198, 5)	1.8045E-04 (198, 5)	1.5801E-04 (54, 4)	1.6002E-04 (103, 3)
20	3.9621E-04 (3, 5)	3.5582E-04 (3, 5)	3.3350E-04 (3, 5)	2.5162E-04 (3, 5)	2.3815E-04 (3, 5)
21	2.5040E-04 (296, 5)	3.5003E-04 (278, 3)	2.1969E-04 (278, 3)	1.9119E-04 (290, 5)	1.8530E-04 (290, 5)
22	3.5018E-04 (236, 4)	2.9786E-04 (323, 5)	2.7489E-04 (323, 5)	1.8386E-04 (323, 5)	1.7050E-04 (273, 6)
23	3.4861E-04 (265, 4)	2.7143E-04 (205, 3)	2.7465E-04 (254, 3)	2.4687E-04 (205, 3)	2.4216E-04 (205, 3)
24	3.0581E-04 (281, 4)	2.4887E-04 (260, 6)	2.4024E-04 (260, 6)	2.0967E-04 (87, 5)	2.0896E-04 (87, 5)
25	2.2730E-04 (183, 5)	2.1855E-04 (87, 6)	2.1126E-04 (254, 5)	2.0149E-04 (182, 7)	2.0552E-04 (182, 7)
26	2.5556E-04 (207, 5)	2.4157E-04 (240, 6)	2.0347E-04 (240, 6)	2.2596E-04 (87, 7)	2.2409E-04 (87, 7)
27	3.8121E-04 (120, 4)	3.6146E-04 (242, 6)	3.0493E-04 (242, 6)	2.3328E-04 (158, 8)	1.9256E-04 (153, 8)
28	2.5987E-04 (155, 5)	2.2774E-04 (126, 8)	1.9552E-04 (244, 4)	1.8429E-04 (111, 6)	1.9159E-04 (111, 6)
29	2.6577E-04 (121, 5)	2.2088E-04 (249, 5)	2.1223E-04 (106, 6)	1.9073E-04 (106, 6)	1.9379E-04 (105, 6)
30	2.5203E-04 (194, 3)	2.7432E-04 (194, 3)	2.5514E-04 (32, 4)	2.1966E-04 (269, 2)	2.2950E-04 (269, 2)

7141

> 210

YEARLY SECOND MAXIMUM 3-HOUR CONC= 3.3023E-04 DIRECTION= 7 DISTANCE= 7.5 KM DAY=187 TIME PERIOD= 3

FORM 4113

DIR	RANGE	SECOND HIGHEST	3-HOUR CONCENTRATION AT EACH RECEPTOR							
		7.5 KM	11.0 KM	12.0 KM	16.5 KM	17.5 KM				
2	2.8302E-04	(115, 5)	2.3630E-04	(364, 3)	2.2352E-04	(331, 4)	2.0556E-04	(329, 3)	2.3591E-04	(329, 3)
3	2.8833E-04	(116, 5)	2.7195E-04	(116, 7)	2.5910E-04	(116, 7)	2.0313E-04	(312, 3)	1.9982E-04	(312, 3)
4	2.7218E-04	(194, 4)	2.2428E-04	(194, 4)	2.1664E-04	(347, 8)	2.0305E-04	(171, 3)	1.9953E-04	(171, 3)
5	2.8965E-04	(171, 3)	1.9632E-04	(164, 3)	1.9139E-04	(167, 3)	1.8073E-04	(257, 3)	1.7719E-04	(257, 3)
6	3.2868E-04	(187, 3)	2.9578E-04	(289, 4)	2.8913E-04	(289, 5)	2.4553E-04	(123, 7)	2.4108E-04	(197, 7)
7	3.3023E-04	(187, 3)	2.1779E-04	(35, 5)	2.0611E-04	(186, 3)	1.9127E-04	(197, 3)	1.8589E-04	(197, 3)
8	2.5403E-04	(233, 4)	1.8724E-04	(300, 4)	1.7562E-04	(300, 4)	1.4028E-04	(94, 4)	1.3642E-04	(94, 4)
9	2.2200E-04	(71, 5)	2.2739E-04	(229, 3)	2.0429E-04	(229, 3)	1.5640E-04	(253, 3)	1.4682E-04	(253, 3)
10	2.3758E-04	(137, 3)	1.6411E-04	(129, 5)	1.6861E-04	(129, 5)	1.9954E-04	(318, 3)	1.7349E-04	(34, 1)
11	2.5068E-04	(19, 5)	2.2308E-04	(303, 4)	1.8687E-04	(53, 6)	1.8390E-04	(332, 8)	1.8634E-04	(332, 8)
12	2.4878E-04	(303, 4)	1.7901E-04	(351, 1)	1.7869E-04	(351, 1)	1.5522E-04	(103, 3)	1.5890E-04	(56, 4)
20	3.0049E-04	(206, 3)	2.4568E-04	(294, 2)	2.5058E-04	(294, 2)	2.3823E-04	(294, 2)	2.3228E-04	(294, 2)
21	2.4133E-04	(278, 3)	2.0703E-04	(295, 6)	2.0085E-04	(295, 6)	1.7879E-04	(294, 3)	1.7508E-04	(294, 3)
22	3.0066E-04	(323, 5)	2.1010E-04	(295, 5)	1.9333E-04	(295, 5)	1.7688E-04	(278, 6)	1.6920E-04	(1, 2)
23	3.2376E-04	(278, 5)	2.1634E-04	(236, 4)	2.6995E-04	(205, 3)	2.1773E-04	(279, 5)	2.1781E-04	(279, 5)
24	2.9658E-04	(184, 4)	2.3809E-04	(17, 5)	2.2497E-04	(17, 5)	1.9911E-04	(112, 3)	1.9996E-04	(112, 3)
25	2.2822E-04	(237, 4)	2.1401E-04	(254, 5)	2.0539E-04	(87, 6)	1.7839E-04	(83, 7)	1.8191E-04	(83, 7)
26	2.6369E-04	(182, 6)	2.0918E-04	(281, 4)	1.9432E-04	(199, 6)	1.9602E-04	(159, 1)	1.8418E-04	(103, 7)
27	3.0968E-04	(121, 5)	3.1408E-04	(241, 4)	2.6487E-04	(68, 4)	1.6924E-04	(105, 8)	1.8988E-04	(63, 4)
28	2.2887E-04	(157, 4)	2.0051E-04	(109, 4)	1.8149E-04	(207, 7)	1.7123E-04	(153, 7)	1.8126E-04	(153, 7)
29	2.6230E-04	(178, 5)	2.0673E-04	(106, 6)	1.9629E-04	(249, 5)	1.7508E-04	(155, 6)	1.7703E-04	(153, 6)
30	2.9332E-04	(127, 5)	2.6114E-04	(32, 4)	2.5230E-04	(194, 3)	1.9641E-04	(32, 4)	1.9790E-04	(27, 4)

7210

725

1974

CRSTER ANALYSIS
FOR WORST-CASE DAYS SELECTION

PLANT NAME: JACKSONVILLE ELECTRIC AU POLLUTANT: THORITY EMISSION UNITS: GM/SEC AIR QUALITY UNITS: GM/H**3

JAX. ELEC. AUTHORITY SU2

SURFACE DATA FROM JACKSONVILLE

MIXING HEIGHT DATA FROM WAYCROSS GA

GLENN CROW MAY 1980

	MET FILE	REQUESTED
	STN NO. YR	STN NO. YR
SURFACE	13889 74	13889 74
UPPER AIR	13861 74	13861 74

PLANT LOCATION: RURAL

ANEMOMETER HEIGHT IS 7.0 METERS

WIND PROFILE EXPONENTS ARE: 0.100 0.150 0.200 0.250 0.300 0.300

NO TAPE OUTPUT

MET DATA WILL NOT BE PRINTED

DAY--	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1
	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1
	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1
	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1
	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1
	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1
	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1
	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1
	1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 0			

* * * * * N O T E * * * * *

ALL TABLES, INCLUDING SOURCE CONTRIBUTION, THAT CONTAIN "ANNUAL" IN THE HEADING ARE BASED ONLY ON THOSE DAYS MARKED BY "1" IN THE ABOVE TABLE

RING DISTANCES(KM)= 7.50 11.00 12.00 16.50 17.50

PLANT ELEVATION (FEET ABOVE SEA LEVEL)-- 0.0

PLANT ELEVATION (METERS ABOVE SEA LEVEL)-- 0.0

RECEPTOR ELEVATIONS (FEET ABOVE SEA LEVEL)

RECEPTOR ELEVATIONS (METERS ABOVE SEA LEVEL)

DIRECTION	RING#1	RING#2	RING#3	RING#4	RING#5
20	0.0	0.0	0.0	0.0	0.0
21	0.0	0.0	0.0	0.0	0.0
22	0.0	0.0	0.0	0.0	0.0
23	0.0	0.0	0.0	0.0	0.0
24	0.0	0.0	0.0	0.0	0.0

RING#1	RING#2	RING#3	RING#4	RING#5
0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0

STACK # 1--JEA EASTPORT UNITS 1 AND 2

SOURCE LOCATION FROM CENTER OF RECEPTOR GRID (DIR,DIST(KM)) 0.00 0.00

STACK # 2--JEA NORTHSIDE UNITS 1 AND 2

SOURCE LOCATION FROM CENTER OF RECEPTOR GRID (DIR,DIST(KM)) 180.00 1.40

STACK # 3--JEA NORTHSIDE UNIT 3

SOURCE LOCATION FROM CENTER OF RECEPTOR GRID (DIR,DIST(KM)) 180.00 1.40

STACK # 4--JEA KENNEDY UNITS 7,8,9

SOURCE LOCATION FROM CENTER OF RECEPTOR GRID (DIR,DIST(KM)) 223.99 10.01

STACK # 5--JEA SOUTHSIDE UNITS 1,2,3,4,5

SOURCE LOCATION FROM CENTER OF RECEPTOR GRID (DIR,DIST(KM)) 216.80 15.61

STACK # 6--ST. REGIS PAPER ALL SOURCES

SOURCE LOCATION FROM CENTER OF RECEPTOR GRID (DIR,DIST(KM)) 265.76 6.77

STACK	MONTH	EMISSION RATE (GMS/SEC)	HEIGHT (METERS)	DIAMETER (METERS)	EXIT VELOCITY (M/SEC)	TEMP (DEG.K)	VOLUMETRIC FLOW (M**3/SEC)
1	ALL	1138.3000	194.16	10.13	18.29	327.60	1474.08
2	ALL	1256.7000	91.40	5.33	8.50	408.00	189.65
3	ALL	1194.9000	106.70	7.01	17.40	407.00	671.54
4	ALL	308.4000	84.00	4.12	23.20	408.00	309.29
5	ALL	465.8000	84.00	4.27	21.60	422.00	309.31
6	ALL	208.4000	32.30	2.13	16.10	433.00	57.37

PLANT NAME: JACKSONVILLE ELECTRIC AU POLLUTANT: THORITY EMISSION UNITS: GM/SEC AIR QUALITY UNITS: GM/M**3

MAXIMUM MEAN CONC= 1.1735E-05 DIRECTION= 22 DISTANCE= 7.5 KM

ANNUAL MEAN CONCENTRATION AT EACH RECEPTOR

DIR	RANGE 7.5 KM	11.0 KM	12.0 KM	16.5 KM	17.5 KM
20	7.70741E-06	7.85599E-06	6.67883E-06	6.17508E-06	6.06273E-06
21	9.18787E-06	7.33317E-06	7.43586E-06	5.68226E-06	5.39094E-06
22	1.17345E-05	1.00986E-05	9.77426E-06	8.15139E-06	8.54348E-06
23	1.10362E-05	9.51834E-06	1.00641E-05	8.67114E-06	7.56720E-06
24	1.14913E-05	1.06410E-05	9.30051E-06	9.61685E-06	9.36955E-06

PLANT NAME: JACKSONVILLE ELECTRIC AU POLLUTANT: THORITY EMISSION UNITS: GM/SEC AIR QUALITY UNITS: GM/M**3

YEARLY MAXIMUM 24-HOUR CONC= 9.9377E-05 DIRECTION= 22 DISTANCE= 11.0 KM DAY=360

HIGHEST 24-HOUR CONCENTRATION AT EACH RECEPTOR

RANGE	7.5 KM	11.0 KM	12.0 KM	16.5 KM	17.5 KM
DIR					
20	9.3622E-05 (278)	9.4451E-05 (278)	9.5096E-05 (278)	7.5973E-05 (278)	7.4114E-05 (278)
21	9.1727E-05 (279)	9.3692E-05 (279)	9.1063E-05 (279)	7.8471E-05 (279)	7.6139E-05 (279)
22	8.6160E-05 (294)	9.9377E-05 (360)	9.6805E-05 (360)	9.5040E-05 (279)	9.0338E-05 (279)
23	7.2726E-05 (73)	5.9784E-05 (277)	5.3483E-05 (277)	7.1678E-05 (255)	5.3569E-05 (340)
24	8.4688E-05 (110)	6.3956E-05 (155)	6.3792E-05 (155)	7.1991E-05 (110)	6.7501E-05 (141)

PLANT NAME: JACKSONVILLE ELECTRIC AU POLLUTANT: THORITY EMISSION UNITS: GM/SEC AIR QUALITY UNITS: GM/M**3

YEARLY SECOND MAXIMUM 24-HOUR CONC= 9.2150E-05 DIRECTION= 22 DISTANCE= 16.5 KM DAY=360

7.5

7.5

SECOND HIGHEST 24-HOUR CONCENTRATION AT EACH RECEPTOR

RANGE	7.5 KM	11.0 KM	12.0 KM	16.5 KM	17.5 KM
DIR					
20	5.2257E-05 (276)	5.5127E-05 (266)	5.4868E-05 (266)	5.0241E-05 (266)	5.1930E-05 (312)
21	5.9763E-05 (13)	6.2254E-05 (13)	6.3484E-05 (293)	6.3909E-05 (295)	5.8690E-05 (295)
22	8.2233E-05 (72)	7.9139E-05 (279)	8.3918E-05 (279)	9.2150E-05 (360)	8.9486E-05 (360)
23	6.2075E-05 (281)	5.6556E-05 (266)	4.9073E-05 (348)	5.2564E-05 (340)	5.2688E-05 (269)
24	8.2307E-05 (203)	6.2800E-05 (110)	6.0862E-05 (110)	6.3498E-05 (285)	6.4754E-05 (110)

PLANT NAME: JACKSONVILLE ELECTRIC AU POLLUTANT: THORITY EMISSION UNITS: GM/SEC AIR QUALITY UNITS: GM/H**3

YEARLY MAXIMUM 3-HOUR CONC= 3.5960E-04 DIRECTION= 21 DISTANCE= 7.5 KM DAY=237 TIME PERIOD= 4

DIR	3-HOUR CONCENTRATION AT EACH RECEPTOR				
	HIGHEST 7.5 KM	11.0 KM	12.0 KM	16.5 KM	17.5 KM
20	3.5908E-04 (331, 4)	2.5076E-04 (33, 4)	2.2743E-04 (331, 4)	1.7435E-04 (276, 2)	1.6664E-04 (276, 2)
21	3.5960E-04 (237, 4)	2.5895E-04 (237, 4)	2.3580E-04 (237, 4)	1.8577E-04 (106, 4)	1.7429E-04 (106, 4)
22	3.5378E-04 (282, 4)	3.1855E-04 (252, 6)	3.1508E-04 (252, 6)	2.6667E-04 (252, 6)	2.5361E-04 (252, 6)
23	3.0552E-04 (304, 4)	2.2186E-04 (348, 4)	2.1558E-04 (348, 4)	2.1561E-04 (348, 4)	2.1637E-04 (348, 4)
24	2.9738E-04 (305, 5)	2.3291E-04 (285, 5)	2.3724E-04 (285, 5)	2.4644E-04 (263, 6)	2.4323E-04 (263, 6)

> 290

> 200

PLANT NAME: JACKSONVILLE ELECTRIC AU POLLUTANT: THORITY EMISSION UNITS: GM/SEC AIR QUALITY UNITS: GM/H**3

YEARLY SECOND MAXIMUM 3-HOUR CONC= 3.2166E-04 DIRECTION= 22 DISTANCE= 7.5 KM DAY=109 TIME PERIOD= 4

DIR	SECOND HIGHEST		3-HOUR CONCENTRATION AT EACH RECEPTOR			
	RANGE	7.5 KM	11.0 KM	12.0 KM	16.5 KM	17.5 KM
20	2.5166E-04	(344, 4)	2.1590E-04 (276, 2)	2.0993E-04 (276, 2)	1.7058E-04 (313, 4)	1.6462E-04 (313, 4)
21	3.0868E-04	(294, 6)	2.2155E-04 (294, 6)	1.9730E-04 (295, 7)	1.7372E-04 (258, 2)	1.6853E-04 (295, 7)
22	3.2166E-04	(109, 4)	2.2643E-04 (333, 4)	2.2250E-04 (333, 4)	2.3177E-04 (360, 7)	2.2827E-04 (360, 7)
23	2.4527E-04	(255, 4)	1.9815E-04 (266, 8)	2.0030E-04 (266, 8)	1.8399E-04 (255, 6)	1.8240E-04 (255, 6)
24	2.6502E-04	(254, 6)	1.9112E-04 (100, 5)	2.1188E-04 (263, 6)	2.0185E-04 (285, 5)	1.9078E-04 (285, 5)

1970

ISCST COARSE GRID ANALYSIS

Best Available Copy

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

CALCULATE (CONCENTRATION=1,DEPOSITION=2)	ISW(1) = 1
RECEPTOR GRID SYSTEM (RECTANGULAR=1 OR 3, POLAR=2 OR 4)	ISW(2) = 1
DISCRETE RECEPTOR SYSTEM (RECTANGULAR=1,POLAR=2)	ISW(3) = 1
TERRAIN ELEVATIONS ARE READ (YES=1,NO=0)	ISW(4) = 0
CALCULATIONS ARE WRITTEN TO TAPE (YES=1,NO=0)	ISW(5) = 0
LIST ALL INPUT DATA (NO=0,YES=1,MET DATA ALSO=2)	ISW(6) = 1
COMPUTE AVERAGE CONCENTRATION (OR TOTAL DEPOSITION)	
WITH THE FOLLOWING TIME PERIODS:	
HOURLY (YES=1,NO=0)	ISW(7) = 0
2-HOUR (YES=1,NO=0)	ISW(8) = 0
3-HOUR (YES=1,NO=0)	ISW(9) = 1
4-HOUR (YES=1,NO=0)	ISW(10) = 0
6-HOUR (YES=1,NO=0)	ISW(11) = 0
8-HOUR (YES=1,NO=0)	ISW(12) = 0
12-HOUR (YES=1,NO=0)	ISW(13) = 0
24-HOUR (YES=1,NO=0)	ISW(14) = 1
PRINT 'N'-DAY TABLE(S) (YES=1,NO=0)	ISW(15) = 1
PRINT THE FOLLOWING TYPES OF TABLES WHOSE TIME PERIODS ARE	
SPECIFIED BY ISW(7) THROUGH ISW(14):	
DAILY TABLES (YES=1,NO=0)	ISW(16) = 0
HIGHEST & SECOND HIGHEST TABLES (YES=1,NO=0)	ISW(17) = 1
MAXIMUM 50 TABLES (YES=1,NO=0)	ISW(18) = 1
METEOROLOGICAL DATA INPUT METHOD (PRE-PROCESSED=1,CARD=2)	ISW(19) = 1
RURAL-URBAN OPTION (RURAL=0,URBAN MODE 1=1,URBAN MODE 2=2)	ISW(20) = 0
WIND PROFILE EXPONENT VALUES (DEFAULTS=1,USER ENTERS=2,3)	ISW(21) = 1
VERTICAL POT. TEMP. GRADIENT VALUES (DEFAULTS=1,USER ENTERS=2,3)	ISW(22) = 1
SCALE EMISSION RATES FOR ALL SOURCES (NO=0,YES>0)	ISW(23) = 0
PROGRAM CALCULATES FINAL PLUME RISE ONLY (YES=1,NO=2)	ISW(24) = 1
PROGRAM ADJUSTS ALL STACK HEIGHTS FOR DOWNWASH (YES=2,NO=1)	ISW(25) = 1
NUMBER OF INPUT SOURCES	NSOURC = 17
NUMBER OF SOURCE GROUPS (=0,ALL SOURCES)	NGROUP = 0
TIME PERIOD INTERVAL TO BE PRINTED (=0,ALL INTERVALS)	IPERD = 0
NUMBER OF X (RANGE) GRID VALUES	NXPNTS = 0
NUMBER OF Y (THETA) GRID VALUES	NYPNTS = 0
NUMBER OF DISCRETE RECEPTORS	NXWYPT = 80
SOURCE EMISSION RATE UNITS CONVERSION FACTOR	TK = .10000E+07
ENTRAINMENT COEFFICIENT FOR UNSTABLE ATMOSPHERE	BETA1 = 0.600
ENTRAINMENT COEFFICIENT FOR STABLE ATMOSPHERE	BETA2 = 0.600
HEIGHT ABOVE GROUND AT WHICH WIND SPEED WAS MEASURED	ZR = 7.00 METERS
LOGICAL UNIT NUMBER OF METEOROLOGICAL DATA	IMET = 9
DECAY COEFFICIENT FOR PHYSICAL OR CHEMICAL DEPLETION	DECAY = 0.000000E+00
SURFACE STATION NO.	ISS = 13889
YEAR OF SURFACE DATA	ISY = 70
UPPER AIR STATION NO.	IUS = 13861
YEAR OF UPPER AIR DATA	IUY = 70
ALLOCATED DATA STORAGE	LIMIT = 43500 WORDS
REQUIRED DATA STORAGE FOR THIS PROBLEM RUN	MIMIT = 5257 WORDS

(10) SE 70

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

*** X,Y COORDINATES OF DISCRETE RECEPTORS ***
(METERS)

(440500.0, 361500.0),	(441000.0, 361500.0),	(441500.0, 361500.0),	(440000.0, 361000.0),	(440500.0, 361000.0),
(441000.0, 361000.0),	(441500.0, 361000.0),	(440000.0, 360500.0),	(440500.0, 360500.0),	(441000.0, 360500.0),
(441500.0, 360500.0),	(442000.0, 360500.0),	(440000.0, 360000.0),	(440500.0, 360000.0),	(441000.0, 360000.0),
(441500.0, 360000.0),	(442000.0, 360000.0),	(440500.0, 359500.0),	(441000.0, 359500.0),	(441500.0, 359500.0),
(442000.0, 359500.0),	(441000.0, 359000.0),	(441500.0, 359000.0),	(438500.0, 359000.0),	(439000.0, 359000.0),
(439500.0, 359000.0),	(438000.0, 358500.0),	(438500.0, 358500.0),	(439000.0, 358500.0),	(439500.0, 358500.0),
(440000.0, 358500.0),	(438000.0, 358000.0),	(438500.0, 358000.0),	(439000.0, 358000.0),	(439500.0, 358000.0),
(440000.0, 358000.0),	(438500.0, 357500.0),	(439000.0, 357500.0),	(439500.0, 357500.0),	(440000.0, 357500.0),
(439000.0, 357000.0),	(439500.0, 357000.0),	(438000.0, 355500.0),	(438500.0, 355500.0),	(437500.0, 355000.0),
(438000.0, 355000.0),	(438500.0, 355000.0),	(439000.0, 355000.0),	(437500.0, 354500.0),	(438000.0, 354500.0),
(438500.0, 354500.0),	(439000.0, 354500.0),	(439500.0, 354500.0),	(437500.0, 354000.0),	(438000.0, 354000.0),
(438500.0, 354000.0),	(439000.0, 354000.0),	(439500.0, 354000.0),	(438000.0, 353500.0),	(438500.0, 353500.0),
(439000.0, 353500.0),	(437000.0, 353500.0),	(436500.0, 353000.0),	(437000.0, 353000.0),	(437500.0, 353000.0),
(438000.0, 353000.0),	(436000.0, 352500.0),	(436500.0, 352500.0),	(437000.0, 352500.0),	(437500.0, 352500.0),
(438000.0, 352500.0),	(436000.0, 352000.0),	(436500.0, 352000.0),	(437000.0, 352000.0),	(437500.0, 352000.0),
(438000.0, 352000.0),	(436500.0, 351500.0),	(437000.0, 351500.0),	(437500.0, 351500.0),	(438000.0, 351500.0),

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

*** SOURCE DATA ***

SOURCE NUMBER	T W Y A NUMBER	PART. CATS.	EMISSION RATE		X (METERS)	Y (METERS)	BASE ELEV. (METERS)	HEIGHT (METERS)	TEMP.	EXIT VEL.		BLDG. HEIGHT (METERS)	BLDG. LENGTH (METERS)	BLDG. WIDTH (METERS)
			TYPE=0,1 (GRAMS/SEC)	TYPE=2 (GRAMS/SEC)					(DEG.K); VERT.DIM TYPE=1 (METERS)	(M/SEC); HORZ.DIM TYPE=1,2 (METERS)	DIAMETER TYPE=0 (METERS)			
1	0 0	0	0.11766E+04	446900.0	366300.0	0.0	194.20	327.60	18.29	10.13	0.00	0.00	0.00	
2	0 0	0	0.70570E+03	446900.0	364900.0	0.0	76.20	401.00	20.10	5.03	0.00	0.00	0.00	
3	0 0	0	0.70570E+03	446900.0	364900.0	0.0	91.40	408.20	8.50	5.33	0.00	0.00	0.00	
4	0 0	0	0.12556E+04	446900.0	364900.0	0.0	106.70	438.80	19.20	7.01	0.00	0.00	0.00	
5	0 0	0	0.23160E+03	446900.0	364900.0	0.0	10.10	779.80	18.30	6.56	0.00	0.00	0.00	
6	0 0	0	0.13180E+03	437670.0	353900.0	0.0	40.70	433.20	11.70	2.44	0.00	0.00	0.00	
7	0 0	0	0.90600E+02	437670.0	353900.0	0.0	40.70	406.50	10.30	3.05	0.00	0.00	0.00	
8	0 0	0	0.11030E+03	437670.0	353900.0	0.0	43.70	422.10	11.80	3.35	0.00	0.00	0.00	
9	0 0	0	0.20970E+03	437670.0	353900.0	0.0	44.20	416.50	13.70	3.05	0.00	0.00	0.00	
10	0 0	0	0.16520E+03	440080.0	359150.0	0.0	45.70	414.30	7.80	3.20	0.00	0.00	0.00	
11	0 0	0	0.20480E+03	440080.0	359150.0	0.0	41.50	405.40	15.50	2.74	0.00	0.00	0.00	
12	0 0	0	0.19120E+03	440080.0	359150.0	0.0	13.70	714.30	8.80	5.84	0.00	0.00	0.00	
13	0 0	0	0.13800E+02	440080.0	359150.0	0.0	6.30	766.50	11.80	3.13	0.00	0.00	0.00	
14	0 0	0	0.20840E+03	441800.0	365600.0	0.0	32.30	433.00	16.10	2.13	0.00	0.00	0.00	
15	0 0	0	0.82200E+02	437900.0	366800.0	0.0	15.90	505.00	8.60	1.37	0.00	0.00	0.00	
16	0 0	0	0.54400E+02	439900.0	359300.0	0.0	76.20	477.00	9.20	3.78	0.00	0.00	0.00	
17	0 0	0	0.25600E+02	447040.0	366570.0	0.0	85.40	441.00	12.20	2.08	0.00	0.00	0.00	

Source NO.

Source Name

1	SJRPP Units 1 & 2
2	Northside Unit 1
3	Northside Unit 2
4	Northside Unit 3
5	Northside CT 3, 4, 5, 6
6	Southside Units 1 & 2
7	Southside Unit 3
8	Southside Unit 4
9	Southside Unit 5
10	Kennedy Units 8 & 9
11	Kennedy Unit 10
12	Kennedy CT 3, 4, 5, 6
13	Kennedy CT 1
14	St. Regis (All major sources)
15	Anheuser Busch (All major sources)
16	Alton Box Board (All major sources)
17	SJRPP Aux. Boiler

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY,PER.)	- X -	- Y -	CON.	(DAY,PER.)
440500.0	361500.0	268.19748	(15, 7)	441000.0	361500.0	215.73340	(15, 7)
441500.0	361500.0	171.12498	(2, 5)	440000.0	361000.0	234.77420	(15, 7)
440500.0	361000.0	166.96355	(290, 2)	441000.0	361000.0	166.34209	(290, 2)
441500.0	361000.0	180.50815	(273, 1)	440000.0	360500.0	174.93445	(290, 2)
440500.0	360500.0	149.12485	(290, 2)	441000.0	360500.0	128.18619	(195, 2)
441500.0	360500.0	183.32544	(273, 1)	442000.0	360500.0	180.17026	(290, 1)
440000.0	360000.0	156.78638	(102, 8)	440500.0	360000.0	123.45834	(16, 3)
441000.0	360000.0	167.55095	(290, 1)	441500.0	360000.0	182.06413	(290, 1)
442000.0	360000.0	190.03809	(67, 7)	440500.0	359500.0	178.88316	(290, 1)
441000.0	359500.0	180.59354	(290, 1)	441500.0	359500.0	194.71780	(67, 7)
442000.0	359500.0	265.38065	(67, 7)	441000.0	359000.0	196.62695	(67, 7)
441500.0	359000.0	268.45880	(67, 7)	438500.0	359000.0	253.71271	(2, 5)
439000.0	359000.0	294.53470	(49, 1)	439500.0	359000.0	143.29903	(16, 3)
438000.0	358500.0	305.83261	(273, 4)	438500.0	358500.0	267.26874	(138, 4)
439000.0	358500.0	316.53522	(49, 1)	439500.0	358500.0	205.71478	(273, 5)
440000.0	358500.0	172.05779	(290, 1)	438000.0	358000.0	334.03973	(15, 7)
438500.0	35rB						
	r2B&:BJb						
	J"Jr*Br-r"						
	*B"Jb						
	J						
358000.0	194.81786	(67, 7)		439500.0	358000.0	383.77634	(2, 4)
							440000.0
438500.0	357500.0	323.54776	(67, 7)	439000.0	357500.0	308.86411	(49, 1)
439500.0	357500.0	452.01328	(2, 4)	440000.0	357500.0	259.68835	(67, 7)
439000.0	357000.0	371.53619	(2, 4)	439500.0	357000.0	253.06198	(67, 7)
438000.0	355500.0	232.67178	(67, 7)	438500.0	355500.0	320.69128	(2, 4)
437500.0	355000.0	231.31851	(67, 7)	438000.0	355000.0	252.87445	(67, 7)
438500.0	355000.0	278.36264	(2, 4)	439000.0	355000.0	193.13634	(273, 6)
437500.0	354500.0	247.40927	(67, 7)	438000.0	354500.0	260.46555	(2, 4)
438500.0	354500.0	211.82361	(2, 4)	439000.0	354500.0	175.89792	(67, 8)
439500.0	354500.0	255.16801	(49, 1)	437500.0	354000.0	237.73642	(67, 7)
438000.0	354000.0	245.16470	(2, 4)	438500.0	354000.0	212.44119	(273, 7)
439000.0	354000.0	174.76855	(67, 8)	439500.0	354000.0	254.50458	(49, 1)
438000.0	353500.0	208.55717	(2, 4)	438500.0	353500.0	194.42346	(273, 7)
439000.0	353500.0	151.97971	(67, 8)	437000.0	353500.0	236.12338	(67, 7)
436500.0	353000.0	259.27301	(16, 5)	437000.0	353000.0	292.27350	(273, 5)
437500.0	353000.0	267.65482	(2, 4)	438000.0	353000.0	246.14995	(273, 7)
436000.0	352500.0	310.85052	(16, 3)	436500.0	352500.0	530.68298	(67, 7)
437000.0	352500.0	731.89252	(2, 4)	437500.0	352500.0	230.87323	(67, 8)
438000.0	352500.0	248.93167	(273, 7)	436000.0	352000.0	628.20935	(67, 7)
436500.0	352000.0	380.42194	(16, 5)	437000.0	352000.0	719.74847	(2, 4)
437500.0	352000.0	288.18594	(67, 8)	438000.0	352000.0	221.28563	(273, 7)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
 * FROM ALL SOURCES *
 * FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY, PER.)	- X -	- Y -	CON.	(DAY, PER.)
436500.0	351500.0	551.84729	(2, 4)	437000.0	351500.0	439.25952	(2, 4)
437500.0	351500.0	294.17511	(67, 8)	438000.0	351500.0	183.25952	(273, 7)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY,PER.)	- X -	- Y -	CON.	(DAY,PER.)
440500.0	361500.0	208.64354	(138, 7)	441000.0	361500.0	182.52917	(138, 7)
441500.0	361500.0	170.09464	(273, 1)	440000.0	361000.0	210.86333	(138, 7)
440500.0	361000.0	157.77368	(2, 5)	441000.0	361000.0	148.65555	(2, 5)
441500.0	361000.0	136.92455	(195, 2)	440000.0	360500.0	141.47247	(2, 5)
440500.0	360500.0	128.14171	(2, 5)	441000.0	360500.0	106.66443	(16, 3)
441500.0	360500.0	150.64890	(290, 1)	442000.0	360500.0	160.92734	(273, 5)
440000.0	360000.0	141.88919	(195, 2)	440500.0	360000.0	109.15761	(290, 1)
441000.0	360000.0	145.08698	(16, 3)	441500.0	360000.0	181.18253	(273, 1)
442000.0	360000.0	162.85199	(273, 5)	440500.0	359500.0	151.65042	(15, 2)
441000.0	359500.0	141.78128	(15, 2)	441500.0	359500.0	176.00189	(273, 1)
442000.0	359500.0	208.62358	(195, 3)	441000.0	359000.0	153.95383	(290, 5)
441500.0	359000.0	194.59476	(273, 6)	438500.0	359000.0	149.67667	(138, 2)
439000.0	359000.0	158.30235	(2, 5)	439500.0	359000.0	139.97444	(290, 1)
438000.0	358500.0	263.16968	(138, 4)	438500.0	358500.0	228.98102	(273, 4)
439000.0	358500.0	238.88889	(2, 5)	439500.0	358500.0	194.59654	(290, 1)
440000.0	358500.0	150.02702	(15, 2)	438000.0	358000.0	276.52563	(16, 4)
438500.0	358000.0	254.95602	(16, 3)	439000.0	358000.0	292.84903	(273, 5)
439500.0	358000.0	235.85490	(273, 5)	440000.0	358000.0	150.48050	(290, 5)
438500.0	357500.0	310.00519	(290, 5)	439000.0	357500.0	279.10522	(273, 5)
439500.0	357500.0	191.75949	(67, 7)	440000.0	357500.0	193.42136	(273, 6)
439000.0	357000.0	287.48672	(49, 1)	439500.0	357000.0	216.12827	(2, 4)
438000.0	355500.0	205.58073	(16, 5)	438500.0	355500.0	258.16760	(67, 7)
437500.0	355000.0	197.54784	(273, 6)	438000.0	355000.0	236.10405	(2, 4)
438500.0	355000.0	237.12012	(67, 7)	439000.0	355000.0	176.44046	(49, 1)
437500.0	354500.0	199.43640	(273, 6)	438000.0	354500.0	238.24271	(67, 7)
438500.0	354500.0	196.82809	(273, 6)	439000.0	354500.0	175.63025	(16, 1)
439500.0	354500.0	231.46600	(67, 8)	437500.0	354000.0	205.89085	(273, 6)
438000.0	354000.0	198.47881	(273, 6)	438500.0	354000.0	171.07486	(16, 1)
439000.0	354000.0	170.35493	(16, 1)	439500.0	354000.0	202.65173	(67, 8)
438000.0	353500.0	199.36227	(273, 7)	438500.0	353500.0	174.29655	(16, 1)
439000.0	353500.0	142.01321	(16, 1)	437000.0	353500.0	202.77098	(273, 6)
436500.0	353000.0	243.28366	(67, 7)	437000.0	353000.0	276.31412	(67, 7)
437500.0	353000.0	214.68930	(195, 1)	438000.0	353000.0	174.91368	(16, 1)
436000.0	352500.0	299.33978	(290, 1)	436500.0	352500.0	475.77573	(273, 6)
437000.0	352500.0	293.51984	(273, 4)	437500.0	352500.0	215.22525	(2, 4)
438000.0	352500.0	191.22447	(195, 4)	436000.0	352000.0	547.98535	(273, 6)
436500.0	352000.0	305.34088	(2, 4)	437000.0	352000.0	279.68207	(195, 1)
437500.0	352000.0	236.90721	(273, 7)	438000.0	352000.0	191.47955	(195, 4)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY, PER.)	- X -	- Y -	CON.	(DAY, PER.)
436500.0	351500.0	326.07184	(195, 1)	437000.0	351500.0	204.76506	(273, 7)
437500.0	351500.0	258.34616	(273, 7)	438000.0	351500.0	177.28241	(273, 3)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* 50 MAXIMUM 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *

* FROM ALL SOURCES *

RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y(METERS) OR DIRECTION (DEGREES)	RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y(METERS) OR DIRECTION (DEGREES)
1	731.89252	4	2	437000.0	352500.0	26	297.68146	3	16	438500.0	357500.0
2	719.74847	4	2	437000.0	352000.0	27	294.53470	1	49	439000.0	359000.0
3	628.20935	7	67	436000.0	352000.0	28	294.17511	8	67	437500.0	351500.0
4	551.84729	4	2	436500.0	351500.0	29	293.51984	4	273	437000.0	352500.0
5	547.98535	6	273	436000.0	352000.0	30	292.84903	5	273	439000.0	358000.0
6	530.68298	7	67	436500.0	352500.0	31	292.27350	5	273	437000.0	353000.0
7	475.77573	6	273	436500.0	352500.0	32	288.18594	8	67	437500.0	352000.0
8	452.01328	4	2	439500.0	357500.0	33	287.48672	1	49	439000.0	357000.0
9	439.25952	4	2	437000.0	351500.0	34	285.96210	1	290	438500.0	357500.0
10	383.77634	4	2	439500.0	358000.0	35	282.90051	5	15	436500.0	352500.0
11	380.42194	5	16	436500.0	352000.0	36	282.60236	5	290	436000.0	352000.0
12	371.53619	4	2	439000.0	357000.0	37	281.68207	1	290	438500.0	358000.0
13	334.03973	7	15	438000.0	358000.0	38	279.90134	7	67	436000.0	352500.0
14	326.07184	1	195	436500.0	351500.0	39	279.68207	1	195	437000.0	352000.0
15	323.54776	7	67	438500.0	357500.0	40	279.10522	5	273	439000.0	357500.0
16	320.69128	4	2	438500.0	355500.0	41	278.36264	4	2	438500.0	355000.0
17	320.14105	1	49	439000.0	358000.0	42	276.52563	4	16	438000.0	358000.0
18	316.53522	1	49	439000.0	358500.0	43	276.31412	7	67	437000.0	353000.0
19	310.85052	3	16	436000.0	352500.0	44	274.66214	5	273	436500.0	352500.0
20	310.00519	5	290	438500.0	357500.0	45	273.17886	5	290	439000.0	358000.0
21	308.86411	1	49	439000.0	357500.0	46	271.66403	2	15	438500.0	357500.0
22	305.83261	4	273	438000.0	358500.0	47	269.36780	5	15	436000.0	352000.0
23	305.34088	4	2	436500.0	352000.0	48	268.45880	7	67	441500.0	359000.0
24	302.44775	6	67	436500.0	352000.0	49	268.19748	7	15	440500.0	361500.0
25	299.33978	1	290	436000.0	352500.0	50	268.17947	5	15	436500.0	351500.0

*** ISC RUN FOR JAX ELEC. AUTH. (SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY,PER.)	- X -	- Y -	CON.	(DAY,PER.)
440500.0	361500.0	95.24966	(15, 1)	441000.0	361500.0	86.37755	(290, 1)
441500.0	361500.0	78.78962	(290, 1)	440000.0	361000.0	92.09961	(15, 1)
440500.0	361000.0	88.65032	(290, 1)	441000.0	361000.0	73.07622	(290, 1)
441500.0	361000.0	60.07512	(273, 1)	440000.0	360500.0	79.96538	(290, 1)
440500.0	360500.0	63.69267	(290, 1)	441000.0	360500.0	51.56373	(16, 1)
441500.0	360500.0	66.62725	(273, 1)	442000.0	360500.0	71.34319	(16, 1)
440000.0	360000.0	54.98575	(290, 1)	440500.0	360000.0	57.41286	(16, 1)
441000.0	360000.0	70.21822	(16, 1)	441500.0	360000.0	74.53501	(273, 1)
442000.0	360000.0	65.52447	(273, 1)	440500.0	359500.0	73.62288	(16, 1)
441000.0	359500.0	75.91058	(16, 1)	441500.0	359500.0	81.29933	(273, 1)
442000.0	359500.0	69.85354	(273, 1)	441000.0	359000.0	68.06529	(273, 1)
441500.0	359000.0	84.94022	(273, 1)	438500.0	359000.0	73.62252	(290, 1)
439000.0	359000.0	59.11644	(290, 1)	439500.0	359000.0	65.97252	(16, 1)
438000.0	358500.0	97.55245	(138, 1)	438500.0	358500.0	115.71334	(138, 1)
439000.0	358500.0	104.92279	(290, 1)	439500.0	358500.0	81.34571	(16, 1)
440000.0	358500.0	76.56594	(16, 1)	438000.0	358000.0	153.75150	(290, 1)
438500.0	358000.0	129.17532	(16, 1)	439000.0	358000.0	124.17617	(16, 1)
439500.0	358000.0	88.58060	(16, 1)	440000.0	358000.0	65.32341	(16, 1)
438500.0	357500.0	151.35526	(16, 1)	439000.0	357500.0	113.70177	(16, 1)
439500.0	357500.0	69.16222	(2, 1)	440000.0	357500.0	59.64932	(67, 1)
439000.0	357000.0	82.34985	(16, 1)	439500.0	357000.0	51.70981	(16, 1)
438000.0	355500.0	80.10554	(16, 1)	438500.0	355500.0	63.65120	(273, 1)
437500.0	355000.0	90.81697	(67, 1)	438000.0	355000.0	65.68878	(273, 1)
438500.0	355000.0	63.92360	(273, 1)	439000.0	355000.0	52.41511	(273, 1)
437500.0	354500.0	76.77312	(67, 1)	438000.0	354500.0	63.86595	(273, 1)
438500.0	354500.0	65.96705	(273, 1)	439000.0	354500.0	47.93360	(273, 1)
439500.0	354500.0	71.79524	(273, 1)	437500.0	354000.0	65.71577	(273, 1)
438000.0	354000.0	64.32759	(273, 1)	438500.0	354000.0	62.61216	(273, 1)
439000.0	354000.0	44.15095	(273, 1)	439500.0	354000.0	77.95039	(273, 1)
438000.0	353500.0	66.15065	(273, 1)	438500.0	353500.0	54.55061	(273, 1)
439000.0	353500.0	41.87154	(273, 1)	437000.0	353500.0	73.71301	(67, 1)
436500.0	353000.0	119.34962	(16, 1)	437000.0	353000.0	106.48213	(273, 1)
437500.0	353000.0	65.35016	(273, 1)	438000.0	353000.0	65.38682	(273, 1)
436000.0	352500.0	175.16132	(16, 1)	436500.0	352500.0	138.25079	(67, 1)
437000.0	352500.0	143.56053	(2, 1)	437500.0	352500.0	71.29165	(273, 1)
438000.0	352500.0	60.67180	(273, 1)	436000.0	352000.0	158.93216	(67, 1)
436500.0	352000.0	104.38873	(67, 1)	437000.0	352000.0	110.88467	(2, 1)
437500.0	352000.0	84.56429	(273, 1)	438000.0	352000.0	59.45518	(273, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY, PER.)	- X -	- Y -	CON.	(DAY, PER.)
436500.0	351500.0	96.20515	(2, 1)	437000.0	351500.0	70.07867	(2, 1)
437500.0	351500.0	98.71010	(273, 1)	438000.0	351500.0	65.07350	(273, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY,PER.)	- X -	- Y -	CON.	(DAY,PER.)
440500.0	361500.0	79.45328	(290, 1)	441000.0	361500.0	79.63403	(15, 1)
441500.0	361500.0	58.77488	(273, 1)	440000.0	361000.0	86.30772	(290, 1)
440500.0	361000.0	62.10139	(15, 1)	441000.0	361000.0	40.74035	(16, 1)
441500.0	361000.0	51.50440	(290, 1)	440000.0	360500.0	47.59656	(15, 1)
440500.0	360500.0	42.93909	(16, 1)	441000.0	360500.0	49.77696	(290, 1)
441500.0	360500.0	65.27515	(16, 1)	442000.0	360500.0	57.79721	(273, 1)
440000.0	360000.0	46.47394	(16, 1)	440500.0	360000.0	46.29574	(290, 1)
441000.0	360000.0	50.38856	(290, 1)	441500.0	360000.0	74.27524	(16, 1)
442000.0	360000.0	61.58038	(16, 1)	440500.0	359500.0	50.16137	(290, 1)
441000.0	359500.0	51.20785	(290, 1)	441500.0	359500.0	63.61624	(16, 1)
442000.0	359500.0	50.83827	(67, 1)	441000.0	359000.0	64.79060	(16, 1)
441500.0	359000.0	55.62982	(67, 1)	438500.0	359000.0	51.03310	(16, 1)
439000.0	359000.0	55.03754	(16, 1)	439500.0	359000.0	46.47096	(290, 1)
438000.0	358500.0	93.10440	(290, 1)	438500.0	358500.0	98.00819	(290, 1)
439000.0	358500.0	95.09619	(16, 1)	439500.0	358500.0	57.42604	(290, 1)
440000.0	358500.0	49.18505	(290, 1)	438000.0	358000.0	145.74933	(15, 1)
438500.0	358000.0	115.63326	(290, 1)	439000.0	358000.0	82.87421	(290, 1)
439500.0	358000.0	72.39320	(273, 1)	440000.0	358000.0	45.27695	(67, 1)
438500.0	357500.0	93.66191	(290, 1)	439000.0	357500.0	77.99995	(273, 1)
439500.0	357500.0	65.13589	(16, 1)	440000.0	357500.0	51.48223	(16, 1)
439000.0	357000.0	72.29383	(273, 1)	439500.0	357000.0	49.13494	(67, 1)
438000.0	355500.0	78.15050	(67, 1)	438500.0	355500.0	62.36514	(2, 1)
437500.0	355000.0	82.78380	(16, 1)	438000.0	355000.0	64.87389	(67, 1)
438500.0	355000.0	52.63382	(67, 1)	439000.0	355000.0	49.29982	(67, 1)
437500.0	354500.0	68.82216	(273, 1)	438000.0	354500.0	56.77400	(67, 1)
438500.0	354500.0	49.73927	(67, 1)	439000.0	354500.0	44.02597	(67, 1)
439500.0	354500.0	43.39512	(67, 1)	437500.0	354000.0	64.52678	(67, 1)
438000.0	354000.0	51.48325	(67, 1)	438500.0	354000.0	45.00684	(67, 1)
439000.0	354000.0	37.81292	(67, 1)	439500.0	354000.0	38.12508	(67, 1)
438000.0	353500.0	46.50814	(67, 1)	438500.0	353500.0	38.95423	(67, 1)
439000.0	353500.0	32.31541	(67, 1)	437000.0	353500.0	68.13153	(273, 1)
436500.0	353000.0	98.32779	(67, 1)	437000.0	353000.0	87.00106	(67, 1)
437500.0	353000.0	52.05655	(2, 1)	438000.0	353000.0	40.81047	(67, 1)
436000.0	352500.0	118.00008	(67, 1)	436500.0	352500.0	121.35146	(273, 1)
437000.0	352500.0	110.69089	(273, 1)	437500.0	352500.0	50.44854	(67, 1)
438000.0	352500.0	34.97305	(67, 1)	436000.0	352000.0	126.73849	(16, 1)
436500.0	352000.0	103.88966	(273, 1)	437000.0	352000.0	78.55335	(273, 1)
437500.0	352000.0	52.28620	(67, 1)	438000.0	352000.0	30.01611	(67, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY,PER.)	- X -	- Y -	CON.	(DAY,PER.)
436500.0	351500.0	86.74744	(273, 1)	437000.0	351500.0	66.70023	(273, 1)
437500.0	351500.0	50.57537	(67, 1)	438000.0	351500.0	26.27819	(16, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* 50 MAXIMUM 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *

* FROM ALL SOURCES *

RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y (METERS) OR DIRECTION (DEGREES)	RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y (METERS) OR DIRECTION (DEGREES)
1	175.16132	1	16	436000.0	352500.0	26	100.10683	1	16	436500.0	352500.0
2	158.93216	1	67	436000.0	352000.0	27	98.71010	1	273	437500.0	351500.0
3	153.75150	1	290	438000.0	358000.0	28	98.32779	1	67	436500.0	353000.0
4	151.35526	1	16	438500.0	357500.0	29	98.00819	1	290	438500.0	358500.0
5	145.74933	1	15	438000.0	358000.0	30	97.55245	1	138	438000.0	358500.0
6	138.25079	1	67	436500.0	352500.0	31	96.20515	1	2	436500.0	351500.0
7	129.17532	1	16	438500.0	358000.0	32	95.24966	1	15	440500.0	361500.0
8	126.73849	1	16	436000.0	352000.0	33	95.09619	1	16	439000.0	358500.0
9	125.82399	1	16	438000.0	358000.0	34	93.66191	1	290	438500.0	357500.0
10	124.17617	1	16	439000.0	358000.0	35	93.10440	1	290	438000.0	358500.0
11	121.35146	1	273	436500.0	352500.0	36	92.76855	1	290	436000.0	352500.0
12	119.34962	1	16	436500.0	353000.0	37	92.09961	1	15	440000.0	361000.0
13	118.53210	1	273	436000.0	352000.0	38	90.98262	1	16	436500.0	352000.0
14	118.00008	1	67	436000.0	352500.0	39	90.81697	1	67	437500.0	355000.0
15	115.71334	1	138	438500.0	358500.0	40	88.65032	1	290	440500.0	361000.0
16	115.63326	1	290	438500.0	358000.0	41	88.58060	1	16	439500.0	358000.0
17	113.70177	1	16	439000.0	357500.0	42	87.54312	1	16	438500.0	358500.0
18	113.56053	1	2	437000.0	352500.0	43	87.00106	1	67	437000.0	353000.0
19	110.88467	1	2	437000.0	352000.0	44	86.74744	1	273	436500.0	351500.0
20	110.69089	1	273	437000.0	352500.0	45	86.37755	1	290	441000.0	361500.0
21	106.48213	1	273	437000.0	353000.0	46	86.30772	1	290	440000.0	361000.0
22	106.22353	1	138	438000.0	358000.0	47	84.94022	1	273	441500.0	359000.0
23	104.92279	1	290	439000.0	358500.0	48	84.56429	1	273	437500.0	352000.0
24	104.38873	1	67	436500.0	352000.0	49	82.87421	1	290	439000.0	358000.0
25	103.88966	1	273	436500.0	352000.0	50	82.78380	1	16	437500.0	355000.0

1971

ISCST COARSE GRID ANALYSIS

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

CALCULATE (CONCENTRATION=1,DEPOSITION=2) ISW(1) = 1
RECEPTOR GRID SYSTEM (RECTANGULAR=1 OR 3, POLAR=2 OR 4) ISW(2) = 1
DISCRETE RECEPTOR SYSTEM (RECTANGULAR=1,POLAR=2) ISW(3) = 1
TERRAIN ELEVATIONS ARE READ (YES=1,NO=0) ISW(4) = 0
CALCULATIONS ARE WRITTEN TO TAPE (YES=1,NO=0) ISW(5) = 0
LIST ALL INPUT DATA (NO=0,YES=1,MET DATA ALSO=2) ISW(6) = 1

COMPUTE AVERAGE CONCENTRATION (OR TOTAL DEPOSITION)
WITH THE FOLLOWING TIME PERIODS:

HOURLY (YES=1,NO=0) ISW(7) = 0
2-HOUR (YES=1,NO=0) ISW(8) = 0
3-HOUR (YES=1,NO=0) ISW(9) = 1
4-HOUR (YES=1,NO=0) ISW(10) = 0
6-HOUR (YES=1,NO=0) ISW(11) = 0
8-HOUR (YES=1,NO=0) ISW(12) = 0
12-HOUR (YES=1,NO=0) ISW(13) = 0
24-HOUR (YES=1,NO=0) ISW(14) = 1
PRINT 'N'-DAY TABLE(S) (YES=1,NO=0) ISW(15) = 1

PRINT THE FOLLOWING TYPES OF TABLES WHOSE TIME PERIODS ARE
SPECIFIED BY ISW(7) THROUGH ISW(14):

DAILY TABLES (YES=1,NO=0) ISW(16) = 0
HIGHEST & SECOND HIGHEST TABLES (YES=1,NO=0) ISW(17) = 1
MAXIMUM 50 TABLES (YES=1,NO=0) ISW(18) = 1
METEOROLOGICAL DATA INPUT METHOD (PRE-PROCESSED=1,CARD=2) ISW(19) = 1
RURAL-URBAN OPTION (RURAL=0,URBAN MODE 1=1,URBAN MODE 2=2) ISW(20) = 0
WIND PROFILE EXPONENT VALUES (DEFAULTS=1,USER ENTERS=2,3) ISW(21) = 1
VERTICAL POT. TEMP. GRADIENT VALUES (DEFAULTS=1,USER ENTERS=2,3) ISW(22) = 1
SCALE EMISSION RATES FOR ALL SOURCES (NO=0,YES>0) ISW(23) = 0
PROGRAM CALCULATES FINAL PLUME RISE ONLY (YES=1,NO=2) ISW(24) = 1
PROGRAM ADJUSTS ALL STACK HEIGHTS FOR DOWNWASH (YES=2,NO=1) ISW(25) = 1

NUMBER OF INPUT SOURCES NSOURC = 17
NUMBER OF SOURCE GROUPS (=0,ALL SOURCES) NGROUP = 0
TIME PERIOD INTERVAL TO BE PRINTED (=0,ALL INTERVALS) IPERD = 0
NUMBER OF X (RANGE) GRID VALUES NXPNTS = 0
NUMBER OF Y (THETA) GRID VALUES NYPNTS = 0
NUMBER OF DISCRETE RECEPTORS NXWYPT = 95
SOURCE EMISSION RATE UNITS CONVERSION FACTOR TK = .100000E+07
ENTRAINMENT COEFFICIENT FOR UNSTABLE ATMOSPHERE BETA1 = 0.600
ENTRAINMENT COEFFICIENT FOR STABLE ATMOSPHERE BETA2 = 0.600
HEIGHT ABOVE GROUND AT WHICH WIND SPEED WAS MEASURED ZR = 7.00 METERS
LOGICAL UNIT NUMBER OF METEOROLOGICAL DATA IMET = 9
DECAY COEFFICIENT FOR PHYSICAL OR CHEMICAL DEPLETION DECAPY = 0.000000E+00
SURFACE STATION NO. ISS = 13889
YEAR OF SURFACE DATA ISY = 71
UPPER AIR STATION NO. IUS = 13861
YEAR OF UPPER AIR DATA IUY = 71
ALLOCATED DATA STORAGE LIMIT = 43500 WORDS
REQUIRED DATA STORAGE FOR THIS PROBLEM RUN MIMIT = 5482 WORDS

TOT 71

clean

course

1971

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

*** X,Y COORDINATES OF DISCRETE RECEPTORS ***
(METERS)

(440500.0, 361500.0), (441000.0, 361500.0), (441500.0, 361500.0), (440000.0, 361000.0), (440500.0, 361000.0),
(441000.0, 361000.0), (441500.0, 361000.0), (440000.0, 360500.0), (440500.0, 360500.0), (441000.0, 360500.0),
(441500.0, 360500.0), (442000.0, 360500.0), (440000.0, 360000.0), (440500.0, 360000.0), (441000.0, 360000.0),
(441500.0, 360000.0), (442000.0, 360000.0), (440500.0, 359500.0), (441000.0, 359500.0), (441500.0, 359500.0),
(442000.0, 359500.0), (441000.0, 359000.0), (441500.0, 359000.0), (438500.0, 359000.0), (439000.0, 359000.0),
(439500.0, 359000.0), (438000.0, 358500.0), (438500.0, 358500.0), (439000.0, 358500.0), (439500.0, 358500.0),
(440000.0, 358500.0), (438000.0, 358000.0), (438500.0, 358000.0), (439000.0, 358000.0), (439500.0, 358000.0),
(440000.0, 358000.0), (438500.0, 357500.0), (439000.0, 357500.0), (439500.0, 357500.0), (440000.0, 357500.0),
(439000.0, 357000.0), (439500.0, 357000.0), (438000.0, 355500.0), (438500.0, 355500.0), (437500.0, 355000.0),
(438000.0, 355000.0), (438500.0, 355000.0), (439000.0, 355000.0), (437500.0, 354500.0), (438000.0, 354500.0),
(438500.0, 354500.0), (439000.0, 354500.0), (439500.0, 354500.0), (437500.0, 354000.0), (438000.0, 354000.0),
(438500.0, 354000.0), (439000.0, 354000.0), (439500.0, 354000.0), (438000.0, 353500.0), (438500.0, 353500.0),
(439000.0, 353500.0), (437000.0, 353500.0), (436500.0, 353000.0), (437000.0, 353000.0), (437500.0, 353000.0),
(438000.0, 353000.0), (436000.0, 352500.0), (436500.0, 352500.0), (437000.0, 352500.0), (437500.0, 352500.0),
(438000.0, 352500.0), (436000.0, 352000.0), (436500.0, 352000.0), (437000.0, 352000.0), (437500.0, 352000.0),
(438000.0, 352000.0), (436500.0, 351500.0), (437000.0, 351500.0), (437500.0, 351500.0), (438000.0, 351500.0),
(437500.0, 358500.0), (437500.0, 358000.0), (437500.0, 357500.0), (437500.0, 357000.0), (438000.0, 357500.0),
(438000.0, 357000.0), (438500.0, 357000.0), (435500.0, 353000.0), (435500.0, 352500.0), (435500.0, 352000.0),
(435500.0, 351500.0), (435500.0, 351000.0), (436000.0, 351500.0), (436000.0, 351000.0), (436500.0, 351000.0),

*** SOURCE DATA ***

SOURCE NUMBER	T W P K E E	Y A NUMBER PART. CATS.	EMISSION RATE		X (METERS)	Y (METERS)	BASE ELEV. (METERS)	HEIGHT (METERS)	TEMP.	EXIT VEL.		BLDG. HEIGHT (METERS)	BLDG. LENGTH (METERS)	BLDG. WIDTH (METERS)
			TYPE=0,1 (GRAMS/SEC)	TYPE=2 (GRAMS/SEC)					(DEG.K); VERT.DIM TYPE=1 (METERS)	TYPE=0 (M/SEC); HORZ.DIM TYPE=1,2 (METERS)	DIAMETER TYPE=0 (METERS)			
1	0	0	0	0.11766E+04	446900.0	366300.0	0.0	194.20	327.60	18.29	10.13	0.00	0.00	0.00
2	0	0	0	0.70570E+03	446900.0	364900.0	0.0	76.20	401.00	20.10	5.03	0.00	0.00	0.00
3	0	0	0	0.70570E+03	446900.0	364900.0	0.0	91.40	408.20	8.50	5.33	0.00	0.00	0.00
4	0	0	0	0.12556E+04	446900.0	364900.0	0.0	106.70	438.80	19.20	7.01	0.00	0.00	0.00
5	0	0	0	0.23160E+03	446900.0	364900.0	0.0	10.10	779.80	18.30	6.56	0.00	0.00	0.00
6	0	0	0	0.13180E+03	437670.0	353900.0	0.0	40.70	433.20	11.70	2.44	0.00	0.00	0.00
7	0	0	0	0.90600E+02	437670.0	353900.0	0.0	40.70	406.50	10.30	3.05	0.00	0.00	0.00
8	0	0	0	0.11030E+03	437670.0	353900.0	0.0	43.70	422.10	11.80	3.35	0.00	0.00	0.00
9	0	0	0	0.20970E+03	437670.0	353900.0	0.0	44.20	416.50	13.70	3.05	0.00	0.00	0.00
10	0	0	0	0.16520E+03	440080.0	359150.0	0.0	45.70	414.30	7.80	3.20	0.00	0.00	0.00
11	0	0	0	0.20480E+03	440080.0	359150.0	0.0	41.50	405.40	15.50	2.74	0.00	0.00	0.00
12	0	0	0	0.19120E+03	440080.0	359150.0	0.0	13.70	714.30	8.80	5.84	0.00	0.00	0.00
13	0	0	0	0.13800E+02	440080.0	359150.0	0.0	6.30	766.50	11.80	3.13	0.00	0.00	0.00
14	0	0	0	0.20840E+03	441800.0	365600.0	0.0	32.30	433.00	16.10	2.13	0.00	0.00	0.00
15	0	0	0	0.82200E+02	437900.0	366800.0	0.0	15.90	505.00	8.60	1.37	0.00	0.00	0.00
16	0	0	0	0.54400E+02	439900.0	359300.0	0.0	76.20	477.00	9.20	3.78	0.00	0.00	0.00
17	0	0	0	0.25600E+02	447040.0	366570.0	0.0	85.40	441.00	12.20	2.08	0.00	0.00	0.00

Source NO.

Source Name

1	SJRPP Units 1 & 2
2	Northside Unit 1
3	Northside Unit 2
4	Northside Unit 3
5	Northside CT 3, 4, 5, 6
6	Southside Units 1 & 2
7	Southside Unit 3
8	Southside Unit 4
9	Southside Unit 5
10	Kennedy Units 8 & 9
11	Kennedy Unit 10
12	Kennedy CT 3, 4, 5, 6
13	Kennedy CT 1
14	St. Regis (All major sources)
15	Anheuser Busch (All major sources)
16	Alton Box Board (All major sources)
17	SJRPP Aux. Boiler

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* 365-DAY AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *

* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	- X -	- Y -	CON.	- X -	- Y -	CON.
440500.0	361500.0	17.67433	441000.0	361500.0	18.08750	441500.0	361500.0	19.09088
440000.0	361000.0	19.17542	440500.0	361000.0	17.98204	441000.0	361000.0	18.20363
441500.0	361000.0	19.54855	440000.0	360500.0	18.60927	440500.0	360500.0	17.98582
441000.0	360500.0	18.00718	441500.0	360500.0	20.55819	442000.0	360500.0	23.56859
440000.0	360000.0	16.94951	440500.0	360000.0	16.77623	441000.0	360000.0	19.69917
441500.0	360000.0	23.40416	442000.0	360000.0	24.28517	440500.0	359500.0	14.71892
441000.0	359500.0	20.34607	441500.0	359500.0	22.81765	442000.0	359500.0	24.50185
441000.0	359000.0	21.82258	441500.0	359000.0	24.99736	438500.0	359000.0	20.85518
439000.0	359000.0	18.76475	439500.0	359000.0	14.76569	438000.0	358500.0	21.76360
438500.0	358500.0	19.23601	439000.0	358500.0	17.67843	439500.0	358500.0	15.99954
440000.0	358500.0	14.51776	438000.0	358000.0	21.31855	438500.0	358000.0	19.55879
439000.0	358000.0	18.49304	439500.0	358000.0	17.69237	440000.0	358000.0	16.33193
438500.0	357500.0	20.27527	439000.0	357500.0	19.11932	439500.0	357500.0	17.90369
440000.0	357500.0	17.56500	439000.0	357000.0	19.04783	439500.0	357000.0	17.55768
438000.0	355500.0	19.11149	438500.0	355500.0	19.59950	437500.0	355000.0	17.32100
438000.0	355000.0	17.68969	438500.0	355000.0	19.69620	439000.0	355000.0	22.20863
437500.0	354500.0	14.33277	438000.0	354500.0	14.80128	438500.0	354500.0	21.74306
439000.0	354500.0	23.04416	439500.0	354500.0	21.06245	437500.0	354000.0	11.74421
438000.0	354000.0	12.50887	438500.0	354000.0	20.86220	439000.0	354000.0	23.08855
439500.0	354000.0	22.67976	438000.0	353500.0	13.01476	438500.0	353500.0	19.22931
439000.0	353500.0	20.10248	437000.0	353500.0	14.34233	436500.0	353000.0	17.58803
437000.0	353000.0	16.14608	437500.0	353000.0	13.80299	438000.0	353000.0	15.27895
436000.0	352500.0	17.53942	436500.0	352500.0	18.38854	437000.0	352500.0	16.17446
437500.0	352500.0	14.96514	438000.0	352500.0	15.50492	436000.0	352000.0	18.22078
436500.0	352000.0	17.08994	437000.0	352000.0	15.76376	437500.0	352000.0	15.48043
438000.0	352000.0	15.20385	436500.0	351500.0	15.97446	437000.0	351500.0	15.23230
437500.0	351500.0	15.59920	438000.0	351500.0	14.72243	437500.0	358500.0	22.03390
437500.0	358000.0	20.55791	437500.0	357500.0	20.68414	437500.0	357000.0	19.69702
438000.0	357500.0	20.52993	438000.0	357000.0	21.16177	438500.0	357000.0	20.64293
435500.0	353000.0	17.64968	435500.0	352500.0	18.33331	435500.0	352000.0	17.11076
435500.0	351500.0	17.53009	435500.0	351000.0	16.57657	436000.0	351500.0	17.09834
436000.0	351000.0	15.49944	436500.0	351000.0	15.31245			

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY, PER.)	- X -	- Y -	CON.	(DAY, PER.)
440500.0	361500.0	306.12793	(182, 5)	441000.0	361500.0	423.86389	(57, 4)
441500.0	361500.0	410.39868	(101, 4)	440000.0	361000.0	343.85876	(87, 5)
440500.0	361000.0	403.86322	(182, 5)	441000.0	361000.0	387.53101	(101, 4)
441500.0	361000.0	381.56784	(101, 4)	440000.0	360500.0	451.25641	(320, 8)
440500.0	360500.0	494.97345	(57, 4)	441000.0	360500.0	386.42868	(197, 6)
441500.0	360500.0	369.08029	(296, 6)	442000.0	360500.0	357.27057	(350, 5)
440000.0	360000.0	371.77576	(321, 1)	440500.0	360000.0	446.78217	(206, 4)
441000.0	360000.0	389.02316	(127, 6)	441500.0	360000.0	434.66125	(201, 4)
442000.0	360000.0	372.16638	(207, 5)	440500.0	359500.0	338.26453	(320, 8)
441000.0	359500.0	482.61728	(274, 4)	441500.0	359500.0	486.10162	(274, 4)
442000.0	359500.0	396.32312	(112, 5)	441000.0	359000.0	523.00897	(195, 5)
441500.0	359000.0	484.16156	(171, 4)	438500.0	359000.0	431.08545	(105, 4)
439000.0	359000.0	466.30917	(105, 4)	439500.0	359000.0	380.16595	(146, 5)
438000.0	358500.0	390.70590	(330, 5)	438500.0	358500.0	397.46472	(285, 5)
439000.0	358500.0	606.29041	(101, 4)	439500.0	358500.0	315.83017	(222, 5)
440000.0	358500.0	382.67978	(194, 5)	438000.0	358000.0	462.17847	(101, 4)
438500.0	358000.0	602.82153	(101, 4)	439000.0	358000.0	505.58005	(356, 6)
439500.0	358000.0	412.85812	(277, 4)	440000.0	358000.0	462.71252	(311, 5)
438500.0	357500.0	565.12256	(356, 6)	439000.0	357500.0	340.19339	(358, 4)
439500.0	357500.0	403.90637	(319, 4)	440000.0	357500.0	498.10205	(311, 5)
439000.0	357000.0	302.65982	(356, 6)	439500.0	357000.0	347.12265	(335, 7)
438000.0	355500.0	367.41382	(182, 5)	438500.0	355500.0	372.48190	(206, 4)
437500.0	355000.0	400.49338	(212, 4)	438000.0	355000.0	426.49945	(57, 4)
438500.0	355000.0	512.91663	(113, 5)	439000.0	355000.0	476.87012	(133, 6)
437500.0	354500.0	378.53485	(231, 5)	438000.0	354500.0	458.97974	(192, 5)
438500.0	354500.0	410.27783	(196, 4)	439000.0	354500.0	624.84998	(207, 5)
439500.0	354500.0	559.59088	(274, 4)	437500.0	354000.0	299.67645	(330, 7)
438000.0	354000.0	285.27136	(245, 1)	438500.0	354000.0	719.51672	(100, 5)
439000.0	354000.0	587.35107	(112, 5)	439500.0	354000.0	468.31235	(60, 5)
438000.0	353500.0	302.29712	(303, 8)	438500.0	353500.0	540.04224	(172, 5)
439000.0	353500.0	463.31906	(177, 4)	437000.0	353500.0	391.80612	(222, 5)
436500.0	353000.0	620.39136	(101, 4)	437000.0	353000.0	494.96457	(356, 7)
437500.0	353000.0	324.62839	(137, 4)	438000.0	353000.0	675.08899	(273, 4)
436000.0	352500.0	441.24091	(326, 5)	436500.0	352500.0	582.40491	(312, 5)
437000.0	352500.0	518.75116	(277, 4)	437500.0	352500.0	393.27222	(311, 5)
438000.0	352500.0	523.47626	(273, 4)	436000.0	352000.0	585.21423	(291, 5)
436500.0	352000.0	489.87103	(336, 1)	437000.0	352000.0	484.69699	(301, 6)
437500.0	352000.0	449.72675	(83, 4)	438000.0	352000.0	471.60004	(149, 6)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY, PER.)	- X -	- Y -	CON.	(DAY, PER.)
436500.0	351500.0	562.04199	(293, 5)	437000.0	351500.0	508.63031	(301, 6)
437500.0	351500.0	433.64291	(83, 4)	438000.0	351500.0	503.69406	(149, 6)
437500.0	358500.0	354.53326	(218, 6)	437500.0	358000.0	323.58038	(245, 3)
437500.0	357500.0	482.62997	(101, 4)	437500.0	357000.0	464.65036	(8, 3)
438000.0	357500.0	462.30164	(336, 4)	438000.0	357000.0	559.27856	(356, 6)
438500.0	357000.0	384.56699	(356, 7)	435500.0	353000.0	397.49994	(267, 6)
435500.0	352500.0	474.67126	(101, 4)	435500.0	352000.0	408.57202	(336, 3)
435500.0	351500.0	534.08923	(291, 5)	435500.0	351000.0	566.29559	(356, 7)
436000.0	351500.0	581.58691	(356, 7)	436000.0	351000.0	509.85822	(357, 5)
436500.0	351000.0	501.36536	(339, 4)				

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY, PER.)	- X -	- Y -	CON.	(DAY, PER.)
440500.0	361500.0	278.95471	(145, 3)	441000.0	361500.0	408.96387	(182, 5)
441500.0	361500.0	306.30356	(197, 6)	440000.0	361000.0	290.78558	(320, 8)
440500.0	361000.0	338.96100	(101, 4)	441000.0	361000.0	368.88373	(341, 4)
441500.0	361000.0	335.63184	(113, 5)	440000.0	360500.0	376.33762	(87, 5)
440500.0	360500.0	453.69589	(182, 5)	441000.0	360500.0	364.02280	(126, 4)
441500.0	360500.0	354.87360	(127, 6)	442000.0	360500.0	310.54431	(201, 4)
440000.0	360000.0	356.88623	(320, 8)	440500.0	360000.0	395.98163	(199, 4)
441000.0	360000.0	377.18555	(173, 6)	441500.0	360000.0	402.34131	(81, 5)
442000.0	360000.0	335.11218	(296, 5)	440500.0	359500.0	295.55685	(146, 4)
441000.0	359500.0	479.41049	(207, 5)	441500.0	359500.0	358.90610	(107, 4)
442000.0	359500.0	294.05902	(134, 4)	441000.0	359000.0	429.18567	(179, 4)
441500.0	359000.0	468.69952	(195, 5)	438500.0	359000.0	383.07748	(218, 5)
439000.0	359000.0	428.09393	(251, 4)	439500.0	359000.0	327.23996	(222, 5)
438000.0	358500.0	354.52792	(109, 5)	438500.0	358500.0	362.95355	(321, 4)
439000.0	358500.0	426.77466	(7, 5)	439500.0	358500.0	309.12756	(107, 5)
440000.0	358500.0	252.32964	(356, 6)	438000.0	358000.0	372.94089	(90, 4)
438500.0	358000.0	505.36969	(336, 4)	439000.0	358000.0	389.25446	(326, 5)
439500.0	358000.0	338.11627	(284, 4)	440000.0	358000.0	343.16101	(311, 4)
438500.0	357500.0	389.34949	(336, 3)	439000.0	357500.0	321.11749	(319, 5)
439500.0	357500.0	332.26691	(301, 6)	440000.0	357500.0	361.20392	(75, 4)
439000.0	357000.0	301.82639	(31, 1)	439500.0	357000.0	304.23639	(301, 6)
438000.0	355500.0	324.28387	(188, 4)	438500.0	355500.0	369.00439	(197, 6)
437500.0	355000.0	378.80466	(191, 4)	438000.0	355000.0	403.87927	(232, 4)
438500.0	355000.0	393.03998	(126, 4)	439000.0	355000.0	412.35449	(127, 6)
437500.0	354500.0	367.77585	(181, 5)	438000.0	354500.0	338.22818	(206, 4)
438500.0	354500.0	388.43954	(234, 5)	439000.0	354500.0	524.17761	(296, 5)
439500.0	354500.0	422.32550	(307, 5)	437500.0	354000.0	242.42172	(214, 8)
438000.0	354000.0	269.79611	(252, 1)	438500.0	354000.0	596.35864	(180, 4)
439000.0	354000.0	574.46686	(171, 4)	439500.0	354000.0	457.64703	(166, 4)
438000.0	353500.0	280.37732	(245, 1)	438500.0	353500.0	520.51770	(127, 4)
439000.0	353500.0	461.26855	(275, 5)	437000.0	353500.0	384.94122	(147, 4)
436500.0	353000.0	539.37836	(326, 5)	437000.0	353000.0	464.61548	(94, 5)
437500.0	353000.0	321.32834	(194, 5)	438000.0	353000.0	389.09198	(256, 4)
436000.0	352500.0	401.92230	(226, 4)	436500.0	352500.0	569.54065	(291, 5)
437000.0	352500.0	433.38510	(284, 4)	437500.0	352500.0	369.68344	(311, 4)
438000.0	352500.0	415.07272	(70, 4)	436000.0	352000.0	536.76703	(312, 5)
436500.0	352000.0	477.26709	(357, 5)	437000.0	352000.0	482.83624	(319, 4)
437500.0	352000.0	424.59335	(311, 5)	438000.0	352000.0	398.05768	(70, 4)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
 * FROM ALL SOURCES *
 * FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY,PER.)	- X -	- Y -	CON.	(DAY,PER.)
436500.0	351500.0	472.05585	(357, 5)	437000.0	351500.0	426.19519	(358, 3)
437500.0	351500.0	377.33115	(311, 5)	438000.0	351500.0	344.31848	(308, 7)
437500.0	358500.0	341.32266	(109, 5)	437500.0	358000.0	315.28021	(330, 7)
437500.0	357500.0	416.74460	(336, 4)	437500.0	357000.0	444.10870	(336, 3)
438000.0	357500.0	444.31995	(8, 3)	438000.0	357000.0	400.57935	(336, 3)
438500.0	357000.0	339.14288	(356, 8)	435500.0	353000.0	396.27148	(321, 4)
435500.0	352500.0	423.86243	(226, 5)	435500.0	352000.0	386.61639	(8, 3)
435500.0	351500.0	463.30481	(337, 2)	435500.0	351000.0	533.80255	(302, 8)
436000.0	351500.0	524.03662	(34, 1)	436000.0	351000.0	502.08783	(33, 8)
436500.0	351000.0	452.61057	(293, 5)				

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* 50 MAXIMUM 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *

* FROM ALL SOURCES *

RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y(METERS) OR DIRECTION (DEGREES)	RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y(METERS) OR DIRECTION (DEGREES)
1	719.51672	5	100	438500.0	354000.0	26	526.49817	5	257	438500.0	354000.0
2	675.08899	4	273	438000.0	353000.0	27	524.17761	5	296	439000.0	354500.0
3	624.84998	5	207	439000.0	354500.0	28	524.03662	1	34	436000.0	351500.0
4	620.39136	4	101	436500.0	353000.0	29	523.47626	4	273	438000.0	352500.0
5	606.29041	4	101	439000.0	358500.0	30	523.00897	5	195	441000.0	359000.0
6	602.82153	4	101	438500.0	358000.0	31	520.51770	4	127	438500.0	353500.0
7	596.35864	4	180	438500.0	354000.0	32	518.75116	4	277	437000.0	352500.0
8	587.35107	5	112	439000.0	354000.0	33	513.11365	4	166	439000.0	354000.0
9	585.21423	5	291	436000.0	352000.0	34	512.91663	5	113	438500.0	355000.0
10	582.40491	5	312	436500.0	352500.0	35	509.85822	5	357	436000.0	351000.0
11	581.58691	7	356	436000.0	351500.0	36	508.63031	6	301	437000.0	351500.0
12	574.46686	4	171	439000.0	354000.0	37	507.27252	5	129	439000.0	354000.0
13	569.54065	5	291	436500.0	352500.0	38	506.48996	7	356	436500.0	352500.0
14	566.29559	7	356	435500.0	351000.0	39	505.58005	6	356	439000.0	358000.0
15	565.12256	6	356	438500.0	357500.0	40	505.36969	4	336	438500.0	358000.0
16	562.04199	5	293	436500.0	351500.0	41	503.69406	6	149	438000.0	351500.0
17	561.13525	5	100	439000.0	354000.0	42	502.08783	8	33	436000.0	351000.0
18	559.59088	4	274	439500.0	354500.0	43	501.36536	4	339	436500.0	351000.0
19	559.27856	6	356	438000.0	357000.0	44	498.10205	5	311	440000.0	357500.0
20	540.04224	5	172	438500.0	353500.0	45	495.55896	4	315	438500.0	353500.0
21	539.37836	5	326	436500.0	353000.0	46	494.97345	4	57	440500.0	360500.0
22	536.76703	5	312	436000.0	352000.0	47	494.96457	7	356	437000.0	353000.0
23	534.08923	5	291	435500.0	351500.0	48	489.87103	1	336	436500.0	352000.0
24	533.80255	8	302	435500.0	351000.0	49	488.19928	1	336	436000.0	351500.0
25	528.42871	5	94	436500.0	352500.0	50	486.10162	4	274	441500.0	359500.0

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY, PER.)	- X -	(- Y -	CON.	(DAY, PER.)
440500.0	361500.0	83.07513	(354, 1)	441000.0	361500.0	120.81758	(57, 1)
441500.0	361500.0	100.19295	(226, 1)	440000.0	361000.0	79.63293	(321, 1)
440500.0	361000.0	88.45162	(226, 1)	441000.0	361000.0	99.20267	(199, 1)
441500.0	361000.0	143.99655	(30, 1)	440000.0	360500.0	100.70564	(321, 1)
440500.0	360500.0	116.06352	(57, 1)	441000.0	360500.0	110.53021	(336, 1)
441500.0	360500.0	103.30037	(336, 1)	442000.0	360500.0	112.14468	(118, 1)
440000.0	360000.0	123.34929	(321, 1)	440500.0	360000.0	121.06829	(336, 1)
441000.0	360000.0	103.43726	(336, 1)	441500.0	360000.0	126.24191	(118, 1)
442000.0	360000.0	128.18002	(118, 1)	440500.0	359500.0	107.26869	(336, 1)
441000.0	359500.0	100.46371	(274, 1)	441500.0	359500.0	123.22857	(274, 1)
442000.0	359500.0	120.53543	(112, 1)	441000.0	359000.0	111.06869	(171, 1)
441500.0	359000.0	142.69626	(166, 1)	438500.0	359000.0	125.83321	(218, 1)
439000.0	359000.0	117.18444	(218, 1)	439500.0	359000.0	112.15710	(336, 1)
438000.0	358500.0	113.39308	(336, 1)	438500.0	358500.0	124.28598	(336, 1)
439000.0	358500.0	150.49509	(336, 1)	439500.0	358500.0	104.30471	(336, 1)
440000.0	358500.0	85.95309	(336, 1)	438000.0	358000.0	166.93472	(336, 1)
438500.0	358000.0	230.68285	(336, 1)	439000.0	358000.0	146.56500	(356, 1)
439500.0	358000.0	136.49843	(357, 1)	440000.0	358000.0	108.93835	(311, 1)
438500.0	357500.0	151.01956	(356, 1)	439000.0	357500.0	177.88818	(356, 1)
439500.0	357500.0	115.17342	(34, 1)	440000.0	357500.0	117.23199	(311, 1)
439000.0	357000.0	181.35779	(357, 1)	439500.0	357000.0	113.67022	(291, 1)
438000.0	355500.0	159.61026	(357, 1)	438500.0	355500.0	144.74054	(34, 1)
437500.0	355000.0	153.09161	(356, 1)	438000.0	355000.0	155.53340	(357, 1)
438500.0	355000.0	129.81586	(34, 1)	439000.0	355000.0	117.83496	(358, 1)
437500.0	354500.0	148.60669	(357, 1)	438000.0	354500.0	134.89206	(302, 1)
438500.0	354500.0	118.59074	(34, 1)	439000.0	354500.0	125.85403	(201, 1)
439500.0	354500.0	117.25936	(274, 1)	437500.0	354000.0	145.02177	(357, 1)
438000.0	354000.0	128.23822	(301, 1)	438500.0	354000.0	125.65123	(100, 1)
439000.0	354000.0	128.07133	(129, 1)	439500.0	354000.0	117.80849	(165, 1)
438000.0	353500.0	123.22568	(301, 1)	438500.0	353500.0	120.86086	(358, 1)
439000.0	353500.0	119.93289	(173, 1)	437000.0	353500.0	140.44615	(302, 1)
436500.0	353000.0	182.62845	(336, 1)	437000.0	353000.0	209.17279	(356, 1)
437500.0	353000.0	126.81698	(34, 1)	438000.0	353000.0	115.23077	(273, 1)
436000.0	352500.0	221.29399	(336, 1)	436500.0	352500.0	268.98730	(302, 1)
437000.0	352500.0	283.34348	(357, 1)	437500.0	352500.0	126.25921	(357, 1)
438000.0	352500.0	116.66637	(358, 1)	436000.0	352000.0	268.77042	(302, 1)
436500.0	352000.0	303.20560	(357, 1)	437000.0	352000.0	212.00682	(34, 1)
437500.0	352000.0	129.63107	(357, 1)	438000.0	352000.0	116.46083	(358, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY,PER.)	- X -	- Y -	CON.	(DAY,PER.)
436500.0	351500.0	292.64243	(357, 1)	437000.0	351500.0	193.36188	(34, 1)
437500.0	351500.0	125.21410	(357, 1)	438000.0	351500.0	112.50574	(358, 1)
437500.0	358500.0	133.77841	(225, 1)	437500.0	358000.0	134.11522	(336, 1)
437500.0	357500.0	206.52945	(336, 1)	437500.0	357000.0	224.86780	(336, 1)
438000.0	357500.0	241.75189	(336, 1)	438000.0	357000.0	151.73160	(336, 1)
438500.0	357000.0	201.58224	(356, 1)	435500.0	353000.0	150.64932	(302, 1)
435500.0	352500.0	187.79039	(336, 1)	435500.0	352000.0	208.09555	(336, 1)
435500.0	351500.0	245.56625	(302, 1)	435500.0	351000.0	280.22867	(302, 1)
436000.0	351500.0	277.99655	(302, 1)	436000.0	351000.0	286.27521	(357, 1)
436500.0	351000.0	237.05724	(34, 1)				

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY,PER.)	- X -	- Y -	CON.	(DAY,PER.)
440500.0	361500.0	73.12303	(199, 1)	441000.0	361500.0	95.86400	(126, 1)
441500.0	361500.0	87.30342	(225, 1)	440000.0	361000.0	79.31332	(303, 1)
440500.0	361000.0	86.44029	(57, 1)	441000.0	361000.0	88.99993	(336, 1)
441500.0	361000.0	101.12585	(336, 1)	440000.0	360500.0	90.79242	(320, 1)
440500.0	360500.0	108.37225	(336, 1)	441000.0	360500.0	78.68936	(199, 1)
441500.0	360500.0	98.83282	(30, 1)	442000.0	360500.0	98.47258	(133, 1)
440000.0	360000.0	110.85159	(336, 1)	440500.0	360000.0	90.03716	(126, 1)
441000.0	360000.0	86.17375	(200, 1)	441500.0	360000.0	126.16621	(201, 1)
442000.0	360000.0	87.16455	(201, 1)	440500.0	359500.0	74.15281	(320, 1)
441000.0	359500.0	81.80592	(234, 1)	441500.0	359500.0	80.05948	(327, 1)
442000.0	359500.0	98.00912	(274, 1)	441000.0	359000.0	107.67101	(160, 1)
441500.0	359000.0	109.62134	(160, 1)	438500.0	359000.0	123.20544	(154, 1)
439000.0	359000.0	113.93288	(105, 1)	439500.0	359000.0	82.76505	(146, 1)
438000.0	358500.0	109.52831	(359, 1)	438500.0	358500.0	106.03537	(267, 1)
439000.0	358500.0	122.70049	(225, 1)	439500.0	358500.0	96.02855	(272, 1)
440000.0	358500.0	74.65022	(321, 1)	438000.0	358000.0	134.69850	(225, 1)
438500.0	358000.0	132.44031	(95, 1)	439000.0	358000.0	133.65742	(336, 1)
439500.0	358000.0	98.15991	(356, 1)	440000.0	358000.0	84.32204	(272, 1)
438500.0	357500.0	149.93869	(336, 1)	439000.0	357500.0	148.42638	(357, 1)
439500.0	357500.0	104.51208	(308, 1)	440000.0	357500.0	86.11364	(312, 1)
439000.0	357000.0	146.25169	(34, 1)	439500.0	357000.0	104.48190	(34, 1)
438000.0	355500.0	139.28271	(302, 1)	438500.0	355500.0	131.97427	(357, 1)
437500.0	355000.0	139.95932	(302, 1)	438000.0	355000.0	140.31863	(302, 1)
438500.0	355000.0	118.96947	(357, 1)	439000.0	355000.0	111.75937	(302, 1)
437500.0	354500.0	139.12167	(302, 1)	438000.0	354500.0	134.57599	(34, 1)
438500.0	354500.0	116.19678	(357, 1)	439000.0	354500.0	120.49551	(358, 1)
439500.0	354500.0	100.98529	(356, 1)	437500.0	354000.0	139.91954	(302, 1)
438000.0	354000.0	126.71295	(34, 1)	438500.0	354000.0	114.77298	(358, 1)
439000.0	354000.0	121.46926	(112, 1)	439500.0	354000.0	103.06935	(129, 1)
438000.0	353500.0	119.24411	(34, 1)	438500.0	353500.0	119.81878	(136, 1)
439000.0	353500.0	119.74182	(150, 1)	437000.0	353500.0	139.97754	(357, 1)
436500.0	353000.0	170.84454	(302, 1)	437000.0	353000.0	203.69725	(357, 1)
437500.0	353000.0	126.49628	(302, 1)	438000.0	353000.0	114.74631	(301, 1)
436000.0	352500.0	180.36392	(356, 1)	436500.0	352500.0	262.01141	(356, 1)
437000.0	352500.0	189.52440	(34, 1)	437500.0	352500.0	122.88482	(34, 1)
438000.0	352500.0	113.07625	(301, 1)	436000.0	352000.0	248.09930	(356, 1)
436500.0	352000.0	239.27814	(302, 1)	437000.0	352000.0	194.20288	(357, 1)
437500.0	352000.0	125.69843	(301, 1)	438000.0	352000.0	112.46926	(301, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY,PER.)	- X -	- Y -	CON.	(DAY,PER.)
436500.0	351500.0	238.79601	(34, 1)	437000.0	351500.0	171.75462	(358, 1)
437500.0	351500.0	123.73064	(301, 1)	438000.0	351500.0	110.65660	(292, 1)
437500.0	358500.0	105.16618	(226, 1)	437500.0	358000.0	126.69850	(225, 1)
437500.0	357500.0	155.47969	(225, 1)	437500.0	357000.0	149.53168	(95, 1)
438000.0	357500.0	151.70805	(95, 1)	438000.0	357000.0	143.48502	(356, 1)
438500.0	357000.0	169.08539	(302, 1)	435500.0	353000.0	137.46179	(356, 1)
435500.0	352500.0	182.91960	(302, 1)	435500.0	352000.0	187.82639	(356, 1)
435500.0	351500.0	225.56670	(356, 1)	435500.0	351000.0	260.60281	(356, 1)
436000.0	351500.0	275.16095	(356, 1)	436000.0	351000.0	227.70621	(302, 1)
436500.0	351000.0	213.49170	(339, 1)				

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* 50 MAXIMUM 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *

* FROM ALL SOURCES *

RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y(METERS) OR DIRECTION (DEGREES)	RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y(METERS) OR DIRECTION (DEGREES)
1	303.20560	1	357	436500.0	352000.0	26	216.90707	1	357	436500.0	352500.0
2	292.64243	1	357	436500.0	351500.0	27	213.49170	1	339	436500.0	351000.0
3	286.27521	1	357	436000.0	351000.0	28	212.64488	1	357	435500.0	351000.0
4	283.34348	1	357	437000.0	352500.0	29	212.00682	1	34	437000.0	352000.0
5	280.22867	1	302	435500.0	351000.0	30	211.65121	1	34	436500.0	352000.0
6	277.99655	1	302	436000.0	351500.0	31	210.61090	1	302	436500.0	351500.0
7	275.16095	1	356	436000.0	351500.0	32	209.17279	1	356	437000.0	353000.0
8	268.98730	1	302	436500.0	352500.0	33	208.09555	1	336	435500.0	352000.0
9	268.77042	1	302	436000.0	352000.0	34	206.52945	1	336	437500.0	357500.0
10	262.01141	1	356	436500.0	352500.0	35	204.96806	1	356	436000.0	351000.0
11	260.60281	1	356	435500.0	351000.0	36	204.00049	1	357	436500.0	351000.0
12	248.09930	1	356	436000.0	352000.0	37	203.69725	1	357	437000.0	353000.0
13	245.62973	1	357	436000.0	351500.0	38	201.58224	1	356	438500.0	357000.0
14	245.56625	1	302	435500.0	351500.0	39	199.04149	1	34	436000.0	351500.0
15	241.75189	1	336	438000.0	357500.0	40	195.80975	1	302	437000.0	353000.0
16	239.27814	1	302	436500.0	352000.0	41	195.20297	1	339	436500.0	351500.0
17	238.79601	1	34	436500.0	351500.0	42	194.20288	1	357	437000.0	352000.0
18	237.05724	1	34	436500.0	351000.0	43	193.36188	1	34	437000.0	351500.0
19	232.26726	1	356	436500.0	352000.0	44	190.67882	1	339	437000.0	352000.0
20	230.68285	1	336	438500.0	358000.0	45	189.52440	1	34	437000.0	352500.0
21	227.70621	1	302	436000.0	351000.0	46	187.82639	1	356	435500.0	352000.0
22	225.56670	1	356	435500.0	351500.0	47	187.79039	1	336	435500.0	352500.0
23	224.86780	1	336	437500.0	357000.0	48	186.27257	1	357	436000.0	352000.0
24	221.29399	1	336	436000.0	352500.0	49	185.89738	1	291	436000.0	352000.0
25	217.30077	1	34	436000.0	351000.0	50	182.98975	1	291	436500.0	352500.0

1972

ISCST COARSE GRID ANALYSIS

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

CALCULATE (CONCENTRATION=1,DEPOSITION=2)	ISW(1) = 1
RECEPTOR GRID SYSTEM (RECTANGULAR=1 OR 3, POLAR=2 OR 4)	ISW(2) = 1
DISCRETE RECEPTOR SYSTEM (RECTANGULAR=1,POLAR=2)	ISW(3) = 1
TERRAIN ELEVATIONS ARE READ (YES=1,NO=0)	ISW(4) = 0
CALCULATIONS ARE WRITTEN TO TAPE (YES=1,NO=0)	ISW(5) = 0
LIST ALL INPUT DATA (NO=0,YES=1,MET DATA ALSO=2)	ISW(6) = 1
COMPUTE AVERAGE CONCENTRATION (OR TOTAL DEPOSITION)	
WITH THE FOLLOWING TIME PERIODS:	
HOURLY (YES=1,NO=0)	ISW(7) = 0
2-HOUR (YES=1,NO=0)	ISW(8) = 0
3-HOUR (YES=1,NO=0)	ISW(9) = 1
4-HOUR (YES=1,NO=0)	ISW(10) = 0
6-HOUR (YES=1,NO=0)	ISW(11) = 0
8-HOUR (YES=1,NO=0)	ISW(12) = 0
12-HOUR (YES=1,NO=0)	ISW(13) = 0
24-HOUR (YES=1,NO=0)	ISW(14) = 1
PRINT 'N'-DAY TABLE(S) (YES=1,NO=0)	ISW(15) = 1
PRINT THE FOLLOWING TYPES OF TABLES WHOSE TIME PERIODS ARE	
SPECIFIED BY ISW(7) THROUGH ISW(14):	
DAILY TABLES (YES=1,NO=0)	ISW(16) = 0
HIGHEST & SECOND HIGHEST TABLES (YES=1,NO=0)	ISW(17) = 1
MAXIMUM 50 TABLES (YES=1,NO=0)	ISW(18) = 1
METEOROLOGICAL DATA INPUT METHOD (PRE-PROCESSED=1,CARD=2)	ISW(19) = 1
RURAL-URBAN OPTION (RURAL=0,URBAN MODE 1=1,URBAN MODE 2=2)	ISW(20) = 0
WIND PROFILE EXPONENT VALUES (DEFAULTS=1,USER ENTERS=2,3)	ISW(21) = 1
VERTICAL POT. TEMP. GRADIENT VALUES (DEFAULTS=1,USER ENTERS=2,3)	ISW(22) = 1
SCALE EMISSION RATES FOR ALL SOURCES (NO=0,YES>0)	ISW(23) = 0
PROGRAM CALCULATES FINAL PLUME RISE ONLY (YES=1,NO=2)	ISW(24) = 1
PROGRAM ADJUSTS ALL STACK HEIGHTS FOR DOWNWASH (YES=2,NO=1)	ISW(25) = 1
NUMBER OF INPUT SOURCES	NSOURC = 17
NUMBER OF SOURCE GROUPS (=0,ALL SOURCES)	NGROUP = 0
TIME PERIOD INTERVAL TO BE PRINTED (=0,ALL INTERVALS)	IPERD = 0
NUMBER OF X (RANGE) GRID VALUES	NXPNTS = 0
NUMBER OF Y (THETA) GRID VALUES	NYPNTS = 0
NUMBER OF DISCRETE RECEPTORS	NXWYPT = 80
SOURCE EMISSION RATE UNITS CONVERSION FACTOR	TK = .10000E+07
ENTRAINMENT COEFFICIENT FOR UNSTABLE ATMOSPHERE	BETA1 = 0.600
ENTRAINMENT COEFFICIENT FOR STABLE ATMOSPHERE	BETA2 = 0.600
HEIGHT ABOVE GROUND AT WHICH WIND SPEED WAS MEASURED	ZR = 7.00 METERS
LOGICAL UNIT NUMBER OF METEOROLOGICAL DATA	IMET = 9
DECAY COEFFICIENT FOR PHYSICAL OR CHEMICAL DEPLETION	DECAY = 0.000000E+00
SURFACE STATION NO.	ISS = 13889
YEAR OF SURFACE DATA	ISY = 72
UPPER AIR STATION NO.	IUS = 13861
YEAR OF UPPER AIR DATA	IUY = 72
ALLOCATED DATA STORAGE	LIMIT = 43500 WORDS
REQUIRED DATA STORAGE FOR THIS PROBLEM RUN	MIMIT = 5257 WORDS

72
COARSE
GRID

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

*** X,Y COORDINATES OF DISCRETE RECEPTORS ***
(METERS)

(440500.0, 361500.0), (441000.0, 361500.0), (441500.0, 361500.0), (440000.0, 361000.0), (440500.0, 361000.0),
(441000.0, 361000.0), (441500.0, 361000.0), (440000.0, 360500.0), (440500.0, 360500.0), (441000.0, 360500.0),
(441500.0, 360500.0), (442000.0, 360500.0), (440000.0, 360000.0), (440500.0, 360000.0), (441000.0, 360000.0),
(441500.0, 360000.0), (442000.0, 360000.0), (440500.0, 359500.0), (441000.0, 359500.0), (441500.0, 359500.0),
(442000.0, 359500.0), (441000.0, 359000.0), (441500.0, 359000.0), (438500.0, 359000.0), (439000.0, 359000.0),
(439500.0, 359000.0), (438000.0, 358500.0), (438500.0, 358500.0), (439000.0, 358500.0), (439500.0, 358500.0),
(440000.0, 358500.0), (438000.0, 358000.0), (438500.0, 358000.0), (439000.0, 358000.0), (439500.0, 358000.0),
(440000.0, 358000.0), (438500.0, 357500.0), (439000.0, 357500.0), (439500.0, 357500.0), (440000.0, 357500.0),
(439000.0, 357000.0), (439500.0, 357000.0), (438000.0, 355500.0), (438500.0, 355500.0), (437500.0, 355000.0),
(438000.0, 355000.0), (438500.0, 355000.0), (439000.0, 355000.0), (437500.0, 354500.0), (438000.0, 354500.0),
(438500.0, 354500.0), (439000.0, 354500.0), (439500.0, 354500.0), (437500.0, 354000.0), (438000.0, 354000.0),
(438500.0, 354000.0), (439000.0, 354000.0), (439500.0, 354000.0), (438000.0, 353500.0), (438500.0, 353500.0),
(439000.0, 353500.0), (437000.0, 353500.0), (436500.0, 353000.0), (437000.0, 353000.0), (437500.0, 353000.0),
(438000.0, 353000.0), (436000.0, 352500.0), (436500.0, 352500.0), (437000.0, 352500.0), (437500.0, 352500.0),
(438000.0, 352500.0), (436000.0, 352000.0), (436500.0, 352000.0), (437000.0, 352000.0), (437500.0, 352000.0),
(438000.0, 352000.0), (436500.0, 351500.0), (437000.0, 35150.0), (437500.0, 351500.0), (438000.0, 351500.0),

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

*** SOURCE DATA ***

SOURCE NUMBER	T W Y A P K E E	PART. CATS.	EMISSION RATE		X (METERS)	Y (METERS)	BASE ELEV. (METERS)	HEIGHT (METERS)	TEMP.	EXIT VEL.	BLDG. HEIGHT (METERS)	BLDG. LENGTH (METERS)	BLDG. WIDTH (METERS)
			TYPE=0,1 (GRAMS/SEC)	TYPE=2 (GRAMS/SEC)					(DEG.K); VERT.DIM TYPE=1 (METERS)	(M/SEC); HORZ.DIM TYPE=1,2 (METERS)			
1	0 0 0	0	0.11766E+04	446900.0	366300.0	0.0	194.20	327.60	18.29	10.13	0.00	0.00	0.00
2	0 0 0	0	0.70570E+03	446900.0	364900.0	0.0	76.20	401.00	20.10	5.03	0.00	0.00	0.00
3	0 0 0	0	0.70570E+03	446900.0	364900.0	0.0	91.40	408.20	8.50	5.33	0.00	0.00	0.00
4	0 0 0	0	0.12556E+04	446900.0	364900.0	0.0	106.70	438.80	19.20	7.01	0.00	0.00	0.00
5	0 0 0	0	0.23160E+03	446900.0	364900.0	0.0	10.10	779.80	18.30	6.56	0.00	0.00	0.00
6	0 0 0	0	0.13180E+03	437670.0	353900.0	0.0	40.70	433.20	11.70	2.44	0.00	0.00	0.00
7	0 0 0	0	0.90600E+02	437670.0	353900.0	0.0	40.70	406.50	10.30	3.05	0.00	0.00	0.00
8	0 0 0	0	0.11030E+03	437670.0	353900.0	0.0	43.70	422.10	11.80	3.35	0.00	0.00	0.00
9	0 0 0	0	0.20970E+03	437670.0	353900.0	0.0	44.20	416.50	13.70	3.05	0.00	0.00	0.00
10	0 0 0	0	0.16520E+03	440080.0	359150.0	0.0	45.70	414.30	7.80	3.20	0.00	0.00	0.00
11	0 0 0	0	0.20480E+03	440080.0	359150.0	0.0	41.50	405.40	15.50	2.74	0.00	0.00	0.00
12	0 0 0	0	0.19120E+03	440080.0	359150.0	0.0	13.70	714.30	8.80	5.84	0.00	0.00	0.00
13	0 0 0	0	0.13800E+02	440080.0	359150.0	0.0	6.30	766.50	11.80	3.13	0.00	0.00	0.00
14	0 0 0	0	0.20840E+03	441800.0	365600.0	0.0	32.30	433.00	16.10	2.13	0.00	0.00	0.00
15	0 0 0	0	0.82200E+02	437900.0	366800.0	0.0	15.90	505.00	8.60	1.37	0.00	0.00	0.00
16	0 0 0	0	0.54400E+02	439900.0	359300.0	0.0	76.20	477.00	9.20	3.78	0.00	0.00	0.00
17	0 0 0	0	0.25600E+02	447040.0	366570.0	0.0	85.40	441.00	12.20	2.08	0.00	0.00	0.00

Source NO.

Source Name

- 1 SJRPP Units 1 & 2
- 2 Northside Unit 1
- 3 Northside Unit 2
- 4 Northside Unit 3
- 5 Northside CT 3, 4, 5, 6
- 6 Southside Units 1 & 2
- 7 Southside Unit 3
- 8 Southside Unit 4
- 9 Southside Unit 5
- 10 Kennedy Units 8 & 9
- 11 Kennedy Unit 10
- 12 Kennedy CT 3, 4, 5, 6
- 13 Kennedy CT 1
- 14 St. Regis (All major sources)
- 15 Anheuser Busch (All major sources)
- 16 Alton Box Board (All major sources)
- 17 SJRPP Aux. Boiler

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY, PER.)	- X -	- Y -	CON.	(DAY, PER.)
440500.0	361500.0	254.77898	(163, 4)	441000.0	361500.0	311.05231	(2, 3)
441500.0	361500.0	290.19870	(147, 6)	440000.0	361000.0	264.19925	(163, 3)
440500.0	361000.0	269.68176	(163, 3)	441000.0	361000.0	324.12106	(2, 3)
441500.0	361000.0	312.16248	(204, 4)	440000.0	360500.0	295.67438	(147, 6)
440500.0	360500.0	297.34842	(204, 4)	441000.0	360500.0	293.34314	(204, 4)
441500.0	360500.0	248.75218	(204, 4)	442000.0	360500.0	192.80791	(276, 2)
440000.0	360000.0	287.16602	(204, 4)	440500.0	360000.0	271.04843	(204, 4)
441000.0	360000.0	222.43974	(204, 4)	441500.0	360000.0	164.70209	(224, 5)
442000.0	360000.0	220.18179	(224, 3)	440500.0	359500.0	231.00961	(224, 4)
441000.0	359500.0	359.84308	(231, 4)	441500.0	359500.0	357.85812	(231, 4)
442000.0	359500.0	258.45016	(224, 3)	441000.0	359000.0	355.07245	(231, 5)
441500.0	359000.0	323.18402	(231, 5)	438500.0	359000.0	330.83575	(204, 4)
439000.0	359000.0	390.74387	(204, 4)	439500.0	359000.0	409.05847	(204, 4)
438000.0	358500.0	284.14700	(204, 4)	438500.0	358500.0	306.40472	(204, 4)
439000.0	358500.0	428.07111	(131, 4)	439500.0	358500.0	217.22733	(224, 3)
440000.0	358500.0	171.57408	(276, 5)	438000.0	358000.0	383.60791	(204, 4)
438500.0	358000.0	518.94592	(189, 6)	439000.0	358000.0	324.24423	(285, 5)
439500.0	358000.0	217.94360	(224, 3)	440000.0	358000.0	223.75700	(131, 4)
438500.0	357500.0	366.95959	(276, 5)	439000.0	357500.0	295.22824	(224, 3)
439500.0	357500.0	221.20030	(40, 1)	440000.0	357500.0	258.33691	(131, 3)
439000.0	357000.0	283.55420	(231, 6)	439500.0	357000.0	235.75946	(40, 4)
438000.0	355500.0	288.89667	(231, 6)	438500.0	355500.0	232.39218	(39, 5)
437500.0	355000.0	252.67743	(231, 6)	438000.0	355000.0	264.11005	(231, 6)
438500.0	355000.0	252.14166	(224, 5)	439000.0	355000.0	261.54071	(80, 3)
437500.0	354500.0	262.41052	(231, 6)	438000.0	354500.0	245.42966	(285, 8)
438500.0	354500.0	258.92917	(80, 3)	439000.0	354500.0	247.09711	(231, 4)
439500.0	354500.0	289.24344	(231, 4)	437500.0	354000.0	242.76042	(231, 6)
438000.0	354000.0	269.05811	(285, 8)	438500.0	354000.0	332.42798	(231, 4)
439000.0	354000.0	227.61485	(231, 5)	439500.0	354000.0	237.37790	(231, 6)
438000.0	353500.0	245.51224	(285, 8)	438500.0	353500.0	256.88934	(42, 8)
439000.0	353500.0	292.19250	(231, 5)	437000.0	353500.0	256.00293	(131, 4)
436500.0	353000.0	429.98102	(131, 4)	437000.0	353000.0	404.77048	(231, 6)
437500.0	353000.0	273.08887	(285, 8)	438000.0	353000.0	273.69739	(231, 4)
436000.0	352500.0	340.80521	(26, 6)	436500.0	352500.0	428.11826	(224, 3)
437000.0	352500.0	433.49017	(231, 6)	437500.0	352500.0	241.24417	(285, 8)
438000.0	352500.0	250.27518	(96, 3)	436000.0	352000.0	403.99902	(224, 3)
436500.0	352000.0	534.80811	(231, 6)	437000.0	352000.0	399.20050	(39, 5)
437500.0	352000.0	262.25781	(40, 5)	438000.0	352000.0	338.10449	(131, 3)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
 * FROM ALL SOURCES *
 * FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY, PER.)	- X -	- Y -	CON.	(DAY, PER.)
436500.0	351500.0	484.76181	(231, 6)	437000.0	351500.0	370.04037	(40, 1)
437500.0	351500.0	273.74033	(40, 5)	438000.0	351500.0	344.63129	(131, 3)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY, PER.)	- X -	- Y -	CON.	(DAY, PER.)
440500.0	361500.0	204.84329	(163, 3)	441000.0	361500.0	265.76630	(163, 3)
441500.0	361500.0	289.69696	(204, 4)	440000.0	361000.0	250.90472	(163, 4)
440500.0	361000.0	268.76331	(147, 6)	441000.0	361000.0	299.54929	(204, 4)
441500.0	361000.0	282.38974	(189, 6)	440000.0	360500.0	272.52832	(204, 4)
440500.0	360500.0	272.59717	(2, 3)	441000.0	360500.0	281.48322	(189, 6)
441500.0	360500.0	212.03146	(42, 4)	442000.0	360500.0	171.73251	(204, 4)
440000.0	360000.0	280.35358	(189, 6)	440500.0	360000.0	264.85550	(189, 6)
441000.0	360000.0	207.93961	(26, 6)	441500.0	360000.0	159.62622	(224, 3)
442000.0	360000.0	195.85086	(276, 5)	440500.0	359500.0	201.06004	(26, 6)
441000.0	359500.0	163.48605	(276, 5)	441500.0	359500.0	202.93254	(224, 3)
442000.0	359500.0	232.24530	(231, 4)	441000.0	359000.0	198.12614	(276, 5)
441500.0	359000.0	237.70343	(224, 3)	438500.0	359000.0	272.99207	(131, 5)
439000.0	359000.0	270.79919	(189, 6)	439500.0	359000.0	228.56357	(42, 4)
438000.0	358500.0	268.71509	(189, 6)	438500.0	358500.0	285.00269	(80, 4)
439000.0	358500.0	383.29431	(204, 4)	439500.0	358500.0	192.88504	(285, 5)
440000.0	358500.0	168.72023	(342, 6)	438000.0	358000.0	346.50021	(163, 3)
438500.0	358000.0	469.88104	(204, 4)	439000.0	358000.0	309.75671	(276, 5)
439500.0	358000.0	192.87775	(231, 6)	440000.0	358000.0	207.64319	(131, 3)
438500.0	357500.0	340.87192	(26, 3)	439000.0	357500.0	288.32687	(231, 6)
439500.0	357500.0	214.88799	(204, 3)	440000.0	357500.0	225.14359	(224, 3)
439000.0	357000.0	223.30768	(39, 6)	439500.0	357000.0	233.79733	(39, 4)
438000.0	355500.0	266.31207	(39, 6)	438500.0	355500.0	223.61064	(231, 6)
437500.0	355000.0	248.04218	(224, 3)	438000.0	355000.0	193.77817	(224, 3)
438500.0	355000.0	242.33582	(40, 1)	439000.0	355000.0	234.03014	(224, 5)
437500.0	354500.0	231.46141	(39, 6)	438000.0	354500.0	222.29993	(231, 6)
438500.0	354500.0	239.42169	(40, 1)	439000.0	354500.0	220.05496	(40, 4)
439500.0	354500.0	256.58112	(2, 4)	437500.0	354000.0	207.71347	(285, 8)
438000.0	354000.0	229.49377	(39, 5)	438500.0	354000.0	244.27930	(80, 3)
439000.0	354000.0	224.35245	(231, 4)	439500.0	354000.0	199.98541	(40, 5)
438000.0	353500.0	212.77299	(80, 3)	438500.0	353500.0	232.55496	(231, 5)
439000.0	353500.0	215.98837	(231, 6)	437000.0	353500.0	238.28815	(231, 6)
436500.0	353000.0	393.53607	(285, 3)	437000.0	353000.0	341.11838	(224, 3)
437500.0	353000.0	220.16745	(39, 5)	438000.0	353000.0	222.71194	(42, 8)
436000.0	352500.0	336.72131	(26, 4)	436500.0	352500.0	406.84961	(231, 6)
437000.0	352500.0	311.42035	(147, 3)	437500.0	352500.0	237.05676	(131, 4)
438000.0	352500.0	249.50632	(42, 8)	436000.0	352000.0	401.44513	(26, 5)
436500.0	352000.0	488.84009	(39, 6)	437000.0	352000.0	387.70468	(40, 1)
437500.0	352000.0	206.26318	(42, 8)	438000.0	352000.0	313.04279	(96, 3)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY, PER.)	- X -	- Y -	CON.	(DAY, PER.)
436500.0	351500.0	366.13690	(39, 6)	437000.0	351500.0	277.06830	(39, 5)
437500.0	351500.0	225.00662	(42, 8)	438000.0	351500.0	293.85635	(96, 3)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* 50 MAXIMUM 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *

* FROM ALL SOURCES *

RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y(METERS) OR DIRECTION (DEGREES)	RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y(METERS) OR DIRECTION (DEGREES)
1	534.80811	6	231	436500.0	352000.0	26	392.01300	3	285	438500.0	358000.0
2	518.94592	6	189	438500.0	358000.0	27	390.74387	4	204	439000.0	359000.0
3	488.84009	6	39	436500.0	352000.0	28	390.69690	4	285	436500.0	352500.0
4	484.76181	6	231	436500.0	351500.0	29	387.70468	1	40	437000.0	352000.0
5	469.88104	4	204	438500.0	358000.0	30	383.60791	4	204	438000.0	358000.0
6	449.01379	7	39	436500.0	352000.0	31	383.29431	4	204	439000.0	358500.0
7	445.29736	4	42	438500.0	358000.0	32	378.09335	4	276	438500.0	358000.0
8	440.93381	6	26	438500.0	358000.0	33	376.16138	8	285	436000.0	352000.0
9	433.49017	6	231	437000.0	352500.0	34	375.12317	4	285	436000.0	352000.0
10	429.98102	4	131	436500.0	353000.0	35	370.04037	1	40	437000.0	351500.0
11	428.11826	3	224	436500.0	352500.0	36	369.39166	2	276	438500.0	358000.0
12	428.07111	4	131	439000.0	358500.0	37	366.95959	5	276	438500.0	357500.0
13	424.22699	8	39	436500.0	352000.0	38	366.13690	6	39	436500.0	351500.0
14	409.05847	4	204	439500.0	359000.0	39	364.46738	2	26	436500.0	352500.0
15	406.84961	6	231	436500.0	352500.0	40	362.84216	4	147	436000.0	352000.0
16	405.30078	4	26	438500.0	358000.0	41	360.71457	3	147	436500.0	351500.0
17	404.77048	6	231	437000.0	353000.0	42	359.84308	4	231	441000.0	359500.0
18	403.99902	3	224	436000.0	352000.0	43	358.29053	6	189	436500.0	353000.0
19	401.44513	5	26	436000.0	352000.0	44	358.28448	5	26	436500.0	352500.0
20	401.13556	8	285	436500.0	352500.0	45	357.85812	4	231	441500.0	359500.0
21	400.23447	4	131	438500.0	358000.0	46	355.07245	5	231	441000.0	359000.0
22	399.20050	5	39	437000.0	352000.0	47	351.35739	4	189	436500.0	353000.0
23	397.20343	2	26	436000.0	352000.0	48	346.50021	3	163	438000.0	358000.0
24	394.75195	8	342	436500.0	352000.0	49	344.63129	3	131	438000.0	351500.0
25	393.53607	3	285	436500.0	353000.0	50	344.62036	5	163	438500.0	358000.0

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY,PER.)	- X -	- Y -	CON.	(DAY,PER.)
440500.0	361500.0	106.63268	(163, 1)	441000.0	361500.0	106.43108	(163, 1)
441500.0	361500.0	88.89363	(163, 1)	440000.0	361000.0	116.33653	(163, 1)
440500.0	361000.0	100.52022	(163, 1)	441000.0	361000.0	97.80225	(147, 1)
441500.0	361000.0	92.66827	(26, 1)	440000.0	360500.0	94.43697	(163, 1)
440500.0	360500.0	92.72295	(26, 1)	441000.0	360500.0	98.46889	(26, 1)
441500.0	360500.0	91.50211	(26, 1)	442000.0	360500.0	81.22649	(26, 1)
440000.0	360000.0	95.89180	(26, 1)	440500.0	360000.0	103.69292	(26, 1)
441000.0	360000.0	90.90643	(26, 1)	441500.0	360000.0	82.50233	(26, 1)
442000.0	360000.0	80.86186	(26, 1)	440500.0	359500.0	91.21584	(26, 1)
441000.0	359500.0	83.41998	(26, 1)	441500.0	359500.0	88.34557	(231, 1)
442000.0	359500.0	99.85464	(285, 1)	441000.0	359000.0	82.78799	(26, 1)
441500.0	359000.0	99.03676	(285, 1)	438500.0	359000.0	98.61139	(276, 1)
439000.0	359000.0	93.90997	(131, 1)	439500.0	359000.0	93.98332	(26, 1)
438000.0	358500.0	102.33351	(276, 1)	438500.0	358500.0	140.30334	(276, 1)
439000.0	358500.0	141.02750	(276, 1)	439500.0	358500.0	95.04604	(26, 1)
440000.0	358500.0	85.99292	(26, 1)	438000.0	358000.0	196.83844	(163, 1)
438500.0	358000.0	201.24203	(276, 1)	439000.0	358000.0	148.63281	(285, 1)
439500.0	358000.0	84.35802	(26, 1)	440000.0	358000.0	84.89574	(26, 1)
438500.0	357500.0	173.05701	(26, 1)	439000.0	357500.0	151.32729	(39, 1)
439500.0	357500.0	93.61404	(40, 1)	440000.0	357500.0	92.74172	(285, 1)
439000.0	357000.0	124.16009	(39, 1)	439500.0	357000.0	99.78957	(40, 1)
438000.0	355500.0	148.95465	(39, 1)	438500.0	355500.0	112.81487	(42, 1)
437500.0	355000.0	150.51608	(39, 1)	438000.0	355000.0	115.84222	(39, 1)
438500.0	355000.0	119.05963	(42, 1)	439000.0	355000.0	100.76225	(42, 1)
437500.0	354500.0	128.37054	(39, 1)	438000.0	354500.0	108.69783	(285, 1)
438500.0	354500.0	121.23797	(42, 1)	439000.0	354500.0	94.41093	(42, 1)
439500.0	354500.0	102.44016	(39, 1)	437500.0	354000.0	106.89558	(285, 1)
438000.0	354000.0	113.94803	(42, 1)	438500.0	354000.0	120.80530	(42, 1)
439000.0	354000.0	110.52126	(231, 1)	439500.0	354000.0	112.27474	(39, 1)
438000.0	353500.0	120.30374	(42, 1)	438500.0	353500.0	117.92828	(42, 1)
439000.0	353500.0	108.55573	(39, 1)	437000.0	353500.0	117.28087	(285, 1)
436500.0	353000.0	182.50082	(285, 1)	437000.0	353000.0	164.84349	(285, 1)
437500.0	353000.0	110.04425	(42, 1)	438000.0	353000.0	124.69443	(42, 1)
436000.0	352500.0	202.47549	(26, 1)	436500.0	352500.0	263.05243	(285, 1)
437000.0	352500.0	168.74008	(39, 1)	437500.0	352500.0	118.12228	(44, 1)
438000.0	352500.0	125.13545	(42, 1)	436000.0	352000.0	271.21216	(285, 1)
436500.0	352000.0	260.01950	(39, 1)	437000.0	352000.0	158.26517	(42, 1)
437500.0	352000.0	123.69107	(42, 1)	438000.0	352000.0	121.44244	(42, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY,PER.)	- X -	- Y -	CON.	(DAY,PER.)
436500.0	351500.0	204.67467	(39, 1)	437000.0	351500.0	169.89447	(42, 1)
437500.0	351500.0	127.46336	(39, 1)	438000.0	351500.0	114.61014	(42, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY,PER.)	- X -	- Y -	CON.	(DAY,PER.)
440500.0	361500.0	82.70304	(147, 1)	441000.0	361500.0	105.58108	(147, 1)
441500.0	361500.0	81.25932	(147, 1)	440000.0	361000.0	90.66949	(147, 1)
440500.0	361000.0	80.62075	(147, 1)	441000.0	361000.0	79.23526	(163, 1)
441500.0	361000.0	89.90301	(276, 1)	440000.0	360500.0	90.29678	(147, 1)
440500.0	360500.0	82.42374	(276, 1)	441000.0	360500.0	88.34146	(276, 1)
441500.0	360500.0	84.41832	(276, 1)	442000.0	360500.0	77.61769	(276, 1)
440000.0	360000.0	90.35815	(276, 1)	440500.0	360000.0	88.14534	(276, 1)
441000.0	360000.0	77.40872	(276, 1)	441500.0	360000.0	65.16103	(276, 1)
442000.0	360000.0	76.24078	(285, 1)	440500.0	359500.0	73.48436	(276, 1)
441000.0	359500.0	68.72173	(231, 1)	441500.0	359500.0	81.75089	(26, 1)
442000.0	359500.0	86.73564	(231, 1)	441000.0	359000.0	77.02036	(285, 1)
441500.0	359000.0	74.09864	(26, 1)	438500.0	359000.0	94.36453	(131, 1)
439000.0	359000.0	93.71280	(276, 1)	439500.0	359000.0	88.54643	(276, 1)
438000.0	358500.0	91.80037	(26, 1)	438500.0	358500.0	104.60399	(163, 1)
439000.0	358500.0	127.82229	(163, 1)	439500.0	358500.0	84.65279	(276, 1)
440000.0	358500.0	60.24986	(342, 1)	438000.0	358000.0	186.43295	(276, 1)
438500.0	358000.0	187.36168	(26, 1)	439000.0	358000.0	148.14517	(26, 1)
439500.0	358000.0	74.79230	(342, 1)	440000.0	358000.0	75.17134	(285, 1)
438500.0	357500.0	162.75117	(285, 1)	439000.0	357500.0	116.06705	(42, 1)
439500.0	357500.0	90.05533	(26, 1)	440000.0	357500.0	80.08359	(26, 1)
439000.0	357000.0	103.69783	(342, 1)	439500.0	357000.0	98.63598	(26, 1)
438000.0	355500.0	114.87515	(342, 1)	438500.0	355500.0	108.78928	(285, 1)
437500.0	355000.0	120.79694	(42, 1)	438000.0	355000.0	108.66155	(285, 1)
438500.0	355000.0	112.82477	(40, 1)	439000.0	355000.0	95.44521	(40, 1)
437500.0	354500.0	105.89876	(285, 1)	438000.0	354500.0	106.85748	(42, 1)
438500.0	354500.0	112.29474	(40, 1)	439000.0	354500.0	86.99797	(39, 1)
439500.0	354500.0	85.64528	(231, 1)	437500.0	354000.0	106.44373	(39, 1)
438000.0	354000.0	101.40810	(285, 1)	438500.0	354000.0	102.81435	(231, 1)
439000.0	354000.0	100.03579	(39, 1)	439500.0	354000.0	96.87344	(231, 1)
438000.0	353500.0	100.27487	(39, 1)	438500.0	353500.0	94.20455	(39, 1)
439000.0	353500.0	87.87557	(42, 1)	437000.0	353500.0	111.07790	(39, 1)
436500.0	353000.0	159.14125	(26, 1)	437000.0	353000.0	147.52647	(39, 1)
437500.0	353000.0	108.80810	(39, 1)	438000.0	353000.0	101.65328	(39, 1)
436000.0	352500.0	177.34256	(285, 1)	436500.0	352500.0	150.87592	(39, 1)
437000.0	352500.0	123.09016	(42, 1)	437500.0	352500.0	114.98788	(39, 1)
438000.0	352500.0	103.65520	(39, 1)	436000.0	352000.0	183.04883	(342, 1)
436500.0	352000.0	176.85313	(42, 1)	437000.0	352000.0	154.04944	(40, 1)
437500.0	352000.0	120.75346	(39, 1)	438000.0	352000.0	105.76085	(39, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY,PER.)	- X -	- Y -	CON.	(DAY,PER.)
436500.0	351500.0	154.47813	(42, 1)	437000.0	351500.0	166.68620	(40, 1)
437500.0	351500.0	126.57458	(40, 1)	438000.0	351500.0	107.26178	(39, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* 50 MAXIMUM 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *

* FROM ALL SOURCES *

RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y(METERS) OR DIRECTION (DEGREES)	RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y(METERS) OR DIRECTION (DEGREES)
1	271.21216	1	285	436000.0	352000.0	26	153.77901	1	276	436500.0	353000.0
2	263.05243	1	285	436500.0	352500.0	27	153.02780	1	39	437000.0	352000.0
3	260.01950	1	39	436500.0	352000.0	28	151.32729	1	39	439000.0	357500.0
4	204.67467	1	39	436500.0	351500.0	29	150.87592	1	39	436500.0	352500.0
5	202.47549	1	26	436000.0	352500.0	30	150.51608	1	39	437500.0	355000.0
6	201.24203	1	276	438500.0	358000.0	31	150.16681	1	342	436000.0	352500.0
7	196.83844	1	163	438000.0	358000.0	32	148.95465	1	39	438000.0	355500.0
8	187.36168	1	26	438500.0	358000.0	33	148.63281	1	285	439000.0	358000.0
9	186.43295	1	276	438000.0	358000.0	34	148.14517	1	26	439000.0	358000.0
10	183.04883	1	342	436000.0	352000.0	35	147.68558	1	276	438500.0	357500.0
11	182.50082	1	285	436500.0	353000.0	36	147.52647	1	39	437000.0	353000.0
12	177.34256	1	285	436000.0	352500.0	37	147.36411	1	39	437000.0	351500.0
13	176.85313	1	42	436500.0	352000.0	38	144.31438	1	42	436000.0	352500.0
14	173.05701	1	26	438500.0	357500.0	39	143.60129	1	342	436500.0	352500.0
15	169.89447	1	42	437000.0	351500.0	40	142.61349	1	39	436000.0	352000.0
16	169.49985	1	276	436000.0	352500.0	41	141.02750	1	276	439000.0	358500.0
17	168.74008	1	39	437000.0	352500.0	42	140.31720	1	26	436500.0	352500.0
18	166.68620	1	40	437000.0	351500.0	43	140.30334	1	276	438500.0	358500.0
19	165.87082	1	26	436000.0	352000.0	44	139.77802	1	285	436500.0	352000.0
20	164.84349	1	285	437000.0	353000.0	45	135.23041	1	342	438500.0	357500.0
21	162.75117	1	285	438500.0	357500.0	46	132.15814	1	163	438500.0	358000.0
22	159.14125	1	26	436500.0	353000.0	47	130.71545	1	276	439000.0	358000.0
23	158.26517	1	42	437000.0	352000.0	48	128.95193	1	26	438000.0	358000.0
24	154.47813	1	42	436500.0	351500.0	49	128.38014	1	42	436000.0	352000.0
25	154.04944	1	40	437000.0	352000.0	50	128.37054	1	39	437500.0	354500.0

1973

ISCST COARSE GRID ANALYSIS

CALCULATE (CONCENTRATION=1,DEPOSITION=2) ISW(1) = 1
 RECEPTOR GRID SYSTEM (RECTANGULAR=1 OR 3, POLAR=2 OR 4) ISW(2) = 1
 DISCRETE RECEPTOR SYSTEM (RECTANGULAR=1,POLAR=2) ISW(3) = 1
 TERRAIN ELEVATIONS ARE READ (YES=1,NO=0) ISW(4) = 0
 CALCULATIONS ARE WRITTEN TO TAPE (YES=1,NO=0) ISW(5) = 0
 LIST ALL INPUT DATA (NO=0,YES=1,MET DATA ALSO=2) ISW(6) = 1

COMPUTE AVERAGE CONCENTRATION (OR TOTAL DEPOSITION)
 WITH THE FOLLOWING TIME PERIODS:

HOURLY (YES=1,NO=0) ISW(7) = 0
 2-HOUR (YES=1,NO=0) ISW(8) = 0
 3-HOUR (YES=1,NO=0) ISW(9) = 1
 4-HOUR (YES=1,NO=0) ISW(10) = 0
 6-HOUR (YES=1,NO=0) ISW(11) = 0
 8-HOUR (YES=1,NO=0) ISW(12) = 0
 12-HOUR (YES=1,NO=0) ISW(13) = 0
 24-HOUR (YES=1,NO=0) ISW(14) = 1
 PRINT 'N'-DAY TABLE(S) (YES=1,NO=0) ISW(15) = 1

PRINT THE FOLLOWING TYPES OF TABLES WHOSE TIME PERIODS ARE
 SPECIFIED BY ISW(7) THROUGH ISW(14):

DAILY TABLES (YES=1,NO=0) ISW(16) = 0
 HIGHEST & SECOND HIGHEST TABLES (YES=1,NO=0) ISW(17) = 1
 MAXIMUM 50 TABLES (YES=1,NO=0) ISW(18) = 1
 METEOROLOGICAL DATA INPUT METHOD (PRE-PROCESSED=1,CARD=2) ISW(19) = 1
 RURAL-URBAN OPTION (RURAL=0,URBAN MODE 1=1,URBAN MODE 2=2) ISW(20) = 0
 WIND PROFILE EXPONENT VALUES (DEFAULTS=1,USER ENTERS=2,3) ISW(21) = 1
 VERTICAL POT. TEMP. GRADIENT VALUES (DEFAULTS=1,USER ENTERS=2,3) ISW(22) = 1
 SCALE EMISSION RATES FOR ALL SOURCES (NO=0,YES>0) ISW(23) = 0
 PROGRAM CALCULATES FINAL PLUME RISE ONLY (YES=1,NO=2) ISW(24) = 1
 PROGRAM ADJUSTS ALL STACK HEIGHTS FOR DOWNWASH (YES=2,NO=1) ISW(25) = 1

NUMBER OF INPUT SOURCES NSOURC = 17
 NUMBER OF SOURCE GROUPS (=0,ALL SOURCES) NGROUP = 0
 TIME PERIOD INTERVAL TO BE PRINTED (=0,ALL INTERVALS) IPERD = 0
 NUMBER OF X (RANGE) GRID VALUES NXPNTS = 0
 NUMBER OF Y (THETA) GRID VALUES NYPNTS = 0
 NUMBER OF DISCRETE RECEPTORS NXWYPT = 80
 SOURCE EMISSION RATE UNITS CONVERSION FACTOR TK = .10000E+07
 ENTRAINMENT COEFFICIENT FOR UNSTABLE ATMOSPHERE BETA1 = 0.600
 ENTRAINMENT COEFFICIENT FOR STABLE ATMOSPHERE BETA2 = 0.600
 HEIGHT ABOVE GROUND AT WHICH WIND SPEED WAS MEASURED ZR = 7.00 METERS
 LOGICAL UNIT NUMBER OF METEOROLOGICAL DATA IMET = 9
 DECAY COEFFICIENT FOR PHYSICAL OR CHEMICAL DEPLETION DECAY = 0.000000E+00
 SURFACE STATION NO. ISS = 13889
 YEAR OF SURFACE DATA ISY = 73
 UPPER AIR STATION NO. IUS = 13861
 YEAR OF UPPER AIR DATA IUY = 73
 ALLOCATED DATA STORAGE LIMIT = 43500 WORDS
 REQUIRED DATA STORAGE FOR THIS PROBLEM RUN MIMIT = 5257 WORDS

73
 COARSE

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

*** X,Y COORDINATES OF DISCRETE RECEPTORS ***
(METERS)

(440500.0, 361500.0), (441000.0, 361500.0), (441500.0, 361500.0), (440000.0, 361000.0), (440500.0, 361000.0),
(441000.0, 361000.0), (441500.0, 361000.0), (440000.0, 360500.0), (440500.0, 360500.0), (441000.0, 360500.0),
(441500.0, 360500.0), (442000.0, 360500.0), (440000.0, 360000.0), (440500.0, 360000.0), (441000.0, 360000.0),
(441500.0, 360000.0), (442000.0, 360000.0), (440500.0, 359500.0), (441000.0, 359500.0), (441500.0, 359500.0),
(442000.0, 359500.0), (441000.0, 359000.0), (441500.0, 359000.0), (438500.0, 359000.0), (439000.0, 359000.0),
(439500.0, 359000.0), (438000.0, 358500.0), (438500.0, 358500.0), (439000.0, 358500.0), (439500.0, 358500.0),
(440000.0, 358500.0), (438000.0, 358000.0), (438500.0, 358000.0), (439000.0, 358000.0), (439500.0, 358000.0),
(440000.0, 358000.0), (438500.0, 357500.0), (439000.0, 357500.0), (439500.0, 357500.0), (440000.0, 357500.0),
(439000.0, 357000.0), (439500.0, 357000.0), (438000.0, 355500.0), (438500.0, 355500.0), (437500.0, 355000.0),
(438000.0, 355000.0), (438500.0, 355000.0), (439000.0, 355000.0), (437500.0, 354500.0), (438000.0, 354500.0),
(438500.0, 354500.0), (439000.0, 354500.0), (439500.0, 354500.0), (437500.0, 354000.0), (438000.0, 354000.0),
(438500.0, 354000.0), (439000.0, 354000.0), (439500.0, 354000.0), (438000.0, 353500.0), (438500.0, 353500.0),
(439000.0, 353500.0), (437000.0, 353500.0), (436500.0, 353000.0), (437000.0, 353000.0), (437500.0, 353000.0),
(438000.0, 353000.0), (436000.0, 352500.0), (436500.0, 352500.0), (437000.0, 352500.0), (437500.0, 352500.0),
(438000.0, 352500.0), (436000.0, 352000.0), (436500.0, 352000.0), (437000.0, 352000.0), (437500.0, 352000.0),
(438000.0, 352000.0), (436500.0, 351500.0), (437000.0, 351500.0), (437500.0, 351500.0), (438000.0, 351500.0),
(

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

*** SOURCE DATA ***

SOURCE NUMBER	T W Y A P K E E	NUMBER PART. CATS.	EMISSION RATE		X (METERS)	Y (METERS)	BASE ELEV. (METERS)	HEIGHT (METERS)	TEMP.	EXIT VEL.		BLDG. HEIGHT (METERS)	BLDG. LENGTH (METERS)	BLDG. WIDTH (METERS)
			TYPE=0,1 (GRAMS/SEC)	TYPE=2 (GRAMS/SEC)					TYPE=0 (DEG.K)	TYPE=0 (M/SEC)	VERT. DIM TYPE=1 (METERS)			
1	0	0	0	0.11766E+04	446900.0	366300.0	0.0	194.20	327.60	18.29	10.13	0.00	0.00	0.00
2	0	0	0	0.70570E+03	446900.0	364900.0	0.0	76.20	401.00	20.10	5.03	0.00	0.00	0.00
3	0	0	0	0.70570E+03	446900.0	364900.0	0.0	91.40	408.20	8.50	5.33	0.00	0.00	0.00
4	0	0	0	0.12556E+04	446900.0	364900.0	0.0	106.70	438.80	19.20	7.01	0.00	0.00	0.00
5	0	0	0	0.23160E+03	446900.0	364900.0	0.0	10.10	779.80	18.30	6.56	0.00	0.00	0.00
6	0	0	0	0.13180E+03	437670.0	353900.0	0.0	40.70	433.20	11.70	2.44	0.00	0.00	0.00
7	0	0	0	0.90600E+02	437670.0	353900.0	0.0	40.70	406.50	10.30	3.05	0.00	0.00	0.00
8	0	0	0	0.11030E+03	437670.0	353900.0	0.0	43.70	422.10	11.80	3.35	0.00	0.00	0.00
9	0	0	0	0.20970E+03	437670.0	353900.0	0.0	44.20	416.50	13.70	3.05	0.00	0.00	0.00
10	0	0	0	0.16520E+03	440080.0	359150.0	0.0	45.70	414.30	7.80	3.20	0.00	0.00	0.00
11	0	0	0	0.20480E+03	440080.0	359150.0	0.0	41.50	405.40	15.50	2.74	0.00	0.00	0.00
12	0	0	0	0.19120E+03	440080.0	359150.0	0.0	13.70	714.30	8.80	5.84	0.00	0.00	0.00
13	0	0	0	0.13800E+02	440080.0	359150.0	0.0	6.30	766.50	11.80	3.13	0.00	0.00	0.00
14	0	0	0	0.20840E+03	441800.0	365600.0	0.0	32.30	433.00	16.10	2.13	0.00	0.00	0.00
15	0	0	0	0.82200E+02	437900.0	366800.0	0.0	15.90	505.00	8.60	1.37	0.00	0.00	0.00
16	0	0	0	0.54400E+02	439900.0	359300.0	0.0	76.20	477.00	9.20	3.78	0.00	0.00	0.00
17	0	0	0	0.25600E+02	447040.0	366570.0	0.0	85.40	441.00	12.20	2.08	0.00	0.00	0.00

Source NO.

Source Name

- 1 SJRPP Units 1 & 2
- 2 Northside Unit 1
- 3 Northside Unit 2
- 4 Northside Unit 3
- 5 Northside CT 3, 4, 5, 6
- 6 Southside Units 1 & 2
- 7 Southside Unit 3
- 8 Southside Unit 4
- 9 Southside Unit 5
- 10 Kennedy Units 8 & 9
- 11 Kennedy Unit 10
- 12 Kennedy CT 3, 4, 5, 6
- 13 Kennedy CT 1
- 14 St. Regis (All major sources)
- 15 Anheuser Busch (All major sources)
- 16 Alton Box Board (All major sources)
- 17 SJRPP Aux. Boiler

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
 * FROM ALL SOURCES *
 * FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY, PER.)	- X -	- Y -	CON.	(DAY, PER.)
440500.0	361500.0	322.00415	(278, 5)	441000.0	361500.0	331.98480	(278, 5)
441500.0	361500.0	247.36746	(278, 5)	440000.0	361000.0	322.56366	(278, 5)
440500.0	361000.0	274.58716	(278, 5)	441000.0	361000.0	204.72836	(205, 3)
441500.0	361000.0	284.50461	(279, 5)	440000.0	360500.0	205.71600	(278, 5)
440500.0	360500.0	226.00446	(279, 5)	441000.0	360500.0	307.52667	(279, 5)
441500.0	360500.0	270.10251	(279, 5)	442000.0	360500.0	260.12598	(323, 5)
440000.0	360000.0	264.23590	(279, 5)	440500.0	360000.0	308.83527	(279, 5)
441000.0	360000.0	241.58282	(279, 5)	441500.0	360000.0	269.91611	(323, 5)
442000.0	360000.0	303.99600	(323, 5)	440500.0	359500.0	212.83733	(279, 5)
441000.0	359500.0	275.07388	(323, 5)	441500.0	359500.0	301.47250	(323, 5)
442000.0	359500.0	263.08160	(323, 1)	441000.0	359000.0	297.23221	(323, 5)
441500.0	359000.0	265.62595	(323, 1)	438500.0	359000.0	242.50420	(279, 5)
439000.0	359000.0	291.81461	(279, 5)	439500.0	359000.0	275.65305	(279, 5)
438000.0	358500.0	259.61102	(279, 5)	438500.0	358500.0	287.65784	(279, 5)
439000.0	358500.0	330.92151	(279, 5)	439500.0	358500.0	283.46255	(323, 5)
440000.0	358500.0	276.72372	(323, 5)	438000.0	358000.0	428.70447	(278, 5)
438500.0	358000.0	600.89490	(279, 5)	439000.0	358000.0	429.43567	(323, 5)
439500.0	358000.0	277.22479	(323, 5)	440000.0	358000.0	286.27621	(323, 5)
438500.0	357500.0	485.20856	(323, 5)	439000.0	357500.0	312.30249	(323, 5)
439500.0	357500.0	280.16510	(323, 5)	440000.0	357500.0	250.04895	(323, 5)
439000.0	357000.0	283.86453	(3, 5)	439500.0	357000.0	245.62408	(323, 5)
438000.0	355500.0	253.31346	(278, 4)	438500.0	355500.0	304.13184	(294, 2)
437500.0	355000.0	238.06326	(323, 5)	438000.0	355000.0	256.04041	(279, 3)
438500.0	355000.0	325.09149	(294, 2)	439000.0	355000.0	242.18756	(59, 2)
437500.0	354500.0	238.66998	(278, 4)	438000.0	354500.0	277.29181	(279, 3)
438500.0	354500.0	256.56085	(294, 2)	439000.0	354500.0	227.52148	(7, 7)
439500.0	354500.0	256.72766	(278, 3)	437500.0	354000.0	253.13541	(279, 3)
438000.0	354000.0	294.45288	(294, 2)	438500.0	354000.0	234.99081	(7, 5)
439000.0	354000.0	195.57944	(7, 7)	439500.0	354000.0	261.14093	(278, 3)
438000.0	353500.0	272.86969	(294, 2)	438500.0	353500.0	206.59625	(7, 5)
439000.0	353500.0	171.94682	(315, 5)	437000.0	353500.0	217.73466	(278, 4)
436500.0	353000.0	457.16586	(279, 5)	437000.0	353000.0	319.68286	(59, 2)
437500.0	353000.0	254.55875	(279, 3)	438000.0	353000.0	243.94598	(294, 8)
436000.0	352500.0	414.64560	(279, 5)	436500.0	352500.0	520.10284	(59, 2)
437000.0	352500.0	296.14258	(294, 2)	437500.0	352500.0	256.21811	(294, 2)
438000.0	352500.0	229.11606	(294, 8)	436000.0	352000.0	535.51361	(59, 2)
436500.0	352000.0	452.93304	(294, 3)	437000.0	352000.0	477.31073	(294, 2)
437500.0	352000.0	243.71405	(315, 7)	438000.0	352000.0	210.75735	(264, 3)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
 * FROM ALL SOURCES *
 * FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY, PER.)	- X -	- Y -	CON.	(DAY, PER.)
436500.0	351500.0	357.07068	(294, 3)	437000.0	351500.0	361.68475	(294, 2)
437500.0	351500.0	254.87071	(315, 7)	438000.0	351500.0	176.44603	(7, 8)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY, PER.)	- X -	- Y -	CON.	(DAY, PER.)
440500.0	361500.0	133.85072	(294, 2)	441000.0	361500.0	129.90282	(205, 6)
441500.0	361500.0	175.55972	(205, 3)	440000.0	361000.0	175.90469	(294, 2)
440500.0	361000.0	155.34435	(205, 3)	441000.0	361000.0	172.22574	(279, 5)
441500.0	361000.0	227.27444	(205, 3)	440000.0	360500.0	182.80365	(205, 3)
440500.0	360500.0	220.78954	(205, 3)	441000.0	360500.0	223.75432	(279, 4)
441500.0	360500.0	196.62254	(294, 4)	442000.0	360500.0	162.37103	(264, 3)
440000.0	360000.0	224.81451	(205, 3)	440500.0	360000.0	221.54727	(279, 4)
441000.0	360000.0	199.22691	(294, 4)	441500.0	360000.0	156.55513	(264, 3)
442000.0	360000.0	278.24210	(323, 1)	440500.0	359500.0	210.42917	(323, 5)
441000.0	359500.0	149.74956	(264, 3)	441500.0	359500.0	197.15143	(323, 1)
442000.0	359500.0	262.83099	(323, 5)	441000.0	359000.0	171.33014	(278, 6)
441500.0	359000.0	261.04651	(323, 5)	438500.0	359000.0	216.75693	(205, 3)
439000.0	359000.0	222.61484	(264, 5)	439500.0	359000.0	215.47301	(264, 3)
438000.0	358500.0	213.52692	(205, 3)	438500.0	358500.0	250.22423	(205, 4)
439000.0	358500.0	299.53128	(278, 5)	439500.0	358500.0	256.84900	(264, 3)
440000.0	358500.0	191.13071	(264, 3)	438000.0	358000.0	314.11676	(279, 5)
438500.0	358000.0	431.44556	(279, 4)	439000.0	358000.0	305.97949	(3, 5)
439500.0	358000.0	239.90155	(264, 3)	440000.0	358000.0	180.44025	(315, 3)
438500.0	357500.0	292.82648	(278, 6)	439000.0	357500.0	242.59990	(278, 3)
439500.0	357500.0	237.65520	(3, 5)	440000.0	357500.0	184.62842	(278, 6)
439000.0	357000.0	275.52774	(323, 5)	439500.0	357000.0	217.56125	(7, 5)
438000.0	355500.0	247.22504	(3, 3)	438500.0	355500.0	276.06253	(3, 5)
437500.0	355000.0	237.34660	(278, 4)	438000.0	355000.0	213.88300	(278, 4)
438500.0	355000.0	250.40538	(3, 5)	439000.0	355000.0	236.50464	(7, 7)
437500.0	354500.0	221.75218	(3, 3)	438000.0	354500.0	254.38200	(294, 2)
438500.0	354500.0	249.32384	(294, 8)	439000.0	354500.0	212.45738	(59, 2)
439500.0	354500.0	200.82367	(315, 7)	437500.0	354000.0	206.07422	(59, 2)
438000.0	354000.0	262.96002	(279, 3)	438500.0	354000.0	220.32268	(59, 2)
439000.0	354000.0	170.08122	(315, 5)	439500.0	354000.0	199.92679	(315, 7)
438000.0	353500.0	234.87292	(294, 8)	438500.0	353500.0	181.81767	(294, 8)
439000.0	353500.0	171.78622	(278, 3)	437000.0	353500.0	215.02678	(279, 3)
436500.0	353000.0	298.61765	(279, 4)	437000.0	353000.0	295.91534	(59, 5)
437500.0	353000.0	253.93051	(294, 2)	438000.0	353000.0	216.48326	(294, 2)
436000.0	352500.0	336.10150	(279, 4)	436500.0	352500.0	493.24243	(59, 5)
437000.0	352500.0	284.71552	(315, 5)	437500.0	352500.0	223.27745	(279, 3)
438000.0	352500.0	222.03618	(264, 3)	436000.0	352000.0	519.96521	(59, 5)
436500.0	352000.0	444.95953	(315, 5)	437000.0	352000.0	331.57294	(294, 8)
437500.0	352000.0	237.02989	(294, 8)	438000.0	352000.0	203.16241	(294, 8)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY, PER.)	- X -	- Y -	CON.	(DAY, PER.)
436500.0	351500.0	340.34283	(315, 5)	437000.0	351500.0	352.58432	(294, 8)
437500.0	351500.0	241.72134	(294, 8)	438000.0	351500.0	175.41687	(264, 3)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* 50 MAXIMUM 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *

* FROM ALL SOURCES *

RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y(METERS) OR DIRECTION (DEGREES)	RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y(METERS) OR DIRECTION (DEGREES)
1	600.89490	5	279	438500.0	358000.0	26	361.68475	2	294	437000.0	351500.0
2	535.51361	2	59	436000.0	352000.0	27	357.07068	3	294	436500.0	351500.0
3	520.10284	2	59	436500.0	352500.0	28	355.82639	6	315	436500.0	352000.0
4	519.96521	5	59	436000.0	352000.0	29	352.71796	7	7	436000.0	352000.0
5	493.24243	5	59	436500.0	352500.0	30	352.58432	8	294	437000.0	351500.0
6	485.20856	5	323	438500.0	357500.0	31	351.24854	3	59	436000.0	352000.0
7	477.31073	2	294	437000.0	352000.0	32	343.74652	5	323	436500.0	352500.0
8	457.16586	5	279	436500.0	353000.0	33	341.38690	4	59	436500.0	352500.0
9	452.93304	3	294	436500.0	352000.0	34	340.34283	5	315	436500.0	351500.0
10	444.95953	5	315	436500.0	352000.0	35	336.10150	4	279	436000.0	352500.0
11	431.44556	4	279	438500.0	358000.0	36	332.04770	4	294	436000.0	352500.0
12	429.43567	5	323	439000.0	358000.0	37	332.01855	5	3	436500.0	351500.0
13	428.70447	5	278	438000.0	358000.0	38	331.98480	5	278	441000.0	361500.0
14	423.01196	4	315	436500.0	352000.0	39	331.57294	8	294	437000.0	352000.0
15	420.54492	4	294	438500.0	358000.0	40	331.16840	6	278	436000.0	352000.0
16	417.92737	4	278	436500.0	352000.0	41	330.92151	5	279	439000.0	358500.0
17	414.64560	5	279	436000.0	352500.0	42	329.52118	2	294	436500.0	351500.0
18	397.68140	5	323	436000.0	352000.0	43	326.46133	5	7	436000.0	352000.0
19	390.23181	6	279	436000.0	352000.0	44	326.14771	5	3	437000.0	352000.0
20	386.35739	6	279	436500.0	352500.0	45	325.09149	2	294	438500.0	355000.0
21	380.78760	4	278	436000.0	352000.0	46	322.56366	5	278	440000.0	361000.0
22	369.56317	3	205	438500.0	358000.0	47	322.00415	5	278	440500.0	361500.0
23	367.42465	4	278	436500.0	352500.0	48	320.80145	3	279	436500.0	351500.0
24	364.45361	2	7	436000.0	352000.0	49	319.68286	2	59	437000.0	353000.0
25	364.20578	3	59	436500.0	352500.0	50	318.77530	4	59	436000.0	352000.0

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY,PER.)	- X -	- Y -	CON.	(DAY,PER.)
440500.0	361500.0	52.14711	(278, 1)	441000.0	361500.0	54.27247	(278, 1)
441500.0	361500.0	56.89033	(279, 1)	440000.0	361000.0	60.56355	(294, 1)
440500.0	361000.0	54.78568	(279, 1)	441000.0	361000.0	69.36052	(279, 1)
441500.0	361000.0	84.34978	(279, 1)	440000.0	360500.0	70.87299	(279, 1)
440500.0	360500.0	75.88243	(279, 1)	441000.0	360500.0	88.81647	(279, 1)
441500.0	360500.0	81.47879	(279, 1)	442000.0	360500.0	63.24629	(279, 1)
440000.0	360000.0	86.05952	(279, 1)	440500.0	360000.0	89.48909	(279, 1)
441000.0	360000.0	77.06812	(279, 1)	441500.0	360000.0	66.87787	(279, 1)
442000.0	360000.0	79.61215	(323, 1)	440500.0	359500.0	77.51804	(279, 1)
441000.0	359500.0	63.66956	(279, 1)	441500.0	359500.0	69.92089	(323, 1)
442000.0	359500.0	83.63495	(59, 1)	441000.0	359000.0	64.19327	(7, 1)
441500.0	359000.0	79.58591	(59, 1)	438500.0	359000.0	83.52610	(205, 1)
439000.0	359000.0	112.97829	(279, 1)	439500.0	359000.0	111.50645	(279, 1)
438000.0	358500.0	88.12343	(205, 1)	438500.0	358500.0	103.32974	(205, 1)
439000.0	358500.0	139.60307	(279, 1)	439500.0	358500.0	111.64253	(279, 1)
440000.0	358500.0	63.80999	(279, 1)	438000.0	358000.0	139.49989	(279, 1)
438500.0	358000.0	186.99603	(279, 1)	439000.0	358000.0	141.63745	(279, 1)
439500.0	358000.0	97.88818	(279, 1)	440000.0	358000.0	76.72439	(7, 1)
438500.0	357500.0	152.23361	(279, 1)	439000.0	357500.0	114.37112	(7, 1)
439500.0	357500.0	95.93645	(279, 1)	440000.0	357500.0	88.10501	(7, 1)
439000.0	357000.0	104.17342	(294, 1)	439500.0	357000.0	122.27444	(7, 1)
438000.0	355500.0	116.57354	(7, 1)	438500.0	355500.0	116.37122	(294, 1)
437500.0	355000.0	130.43375	(7, 1)	438000.0	355000.0	110.93045	(59, 1)
438500.0	355000.0	119.37733	(59, 1)	439000.0	355000.0	126.15932	(59, 1)
437500.0	354500.0	110.87764	(7, 1)	438000.0	354500.0	123.76717	(59, 1)
438500.0	354500.0	126.50314	(59, 1)	439000.0	354500.0	112.64406	(7, 1)
439500.0	354500.0	99.85250	(315, 1)	437500.0	354000.0	118.85802	(59, 1)
438000.0	354000.0	127.41152	(59, 1)	438500.0	354000.0	118.50624	(59, 1)
439000.0	354000.0	100.89046	(7, 1)	439500.0	354000.0	103.55117	(315, 1)
438000.0	353500.0	119.73016	(59, 1)	438500.0	353500.0	108.99023	(7, 1)
439000.0	353500.0	87.50465	(7, 1)	437000.0	353500.0	117.29031	(59, 1)
436500.0	353000.0	166.69232	(279, 1)	437000.0	353000.0	178.26114	(59, 1)
437500.0	353000.0	114.65582	(59, 1)	438000.0	353000.0	103.25320	(59, 1)
436000.0	352500.0	180.87070	(279, 1)	436500.0	352500.0	264.56842	(59, 1)
437000.0	352500.0	125.55347	(294, 1)	437500.0	352500.0	105.48394	(294, 1)
438000.0	352500.0	101.06213	(7, 1)	436000.0	352000.0	277.50391	(59, 1)
436500.0	352000.0	166.46146	(59, 1)	437000.0	352000.0	164.73199	(294, 1)
437500.0	352000.0	106.88499	(294, 1)	438000.0	352000.0	93.30394	(7, 1)

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SGROUP# 1
*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY,PER.)	- X -	- Y -	CON.	(DAY,PER.)
436500.0	351500.0	156.06030	(294, 1)	437000.0	351500.0	139.74402	(294, 1)
437500.0	351500.0	108.17181	(315, 1)	438000.0	351500.0	83.79280	(315, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY, PER.)	- X -	- Y -	CON.	(DAY, PER.)
440500.0	361500.0	46.54774	(294, 1)	441000.0	361500.0	48.70855	(279, 1)
441500.0	361500.0	54.25879	(205, 1)	440000.0	361000.0	60.41775	(279, 1)
440500.0	361000.0	48.45556	(205, 1)	441000.0	361000.0	52.98751	(205, 1)
441500.0	361000.0	52.62576	(205, 1)	440000.0	360500.0	63.36343	(294, 1)
440500.0	360500.0	50.72436	(205, 1)	441000.0	360500.0	48.43515	(3, 1)
441500.0	360500.0	45.00079	(3, 1)	442000.0	360500.0	57.69975	(323, 1)
440000.0	360000.0	59.38523	(294, 1)	440500.0	360000.0	46.35749	(7, 1)
441000.0	360000.0	52.66552	(3, 1)	441500.0	360000.0	53.90998	(3, 1)
442000.0	360000.0	61.02394	(279, 1)	440500.0	359500.0	52.03133	(3, 1)
441000.0	359500.0	60.25533	(3, 1)	441500.0	359500.0	66.40648	(279, 1)
442000.0	359500.0	72.64474	(7, 1)	441000.0	359000.0	62.57072	(279, 1)
441500.0	359000.0	75.11820	(7, 1)	438500.0	359000.0	82.34569	(279, 1)
439000.0	359000.0	62.22505	(294, 1)	439500.0	359000.0	65.70319	(294, 1)
438000.0	358500.0	85.92735	(279, 1)	438500.0	358500.0	99.37321	(279, 1)
439000.0	358500.0	95.68660	(205, 1)	439500.0	358500.0	72.21061	(264, 1)
440000.0	358500.0	62.70111	(7, 1)	438000.0	358000.0	95.04210	(278, 1)
438500.0	358000.0	94.26900	(3, 1)	439000.0	358000.0	102.68752	(7, 1)
439500.0	358000.0	82.52824	(278, 1)	440000.0	358000.0	67.01890	(279, 1)
438500.0	357500.0	129.00748	(7, 1)	439000.0	357500.0	110.08900	(278, 1)
439500.0	357500.0	94.58171	(7, 1)	440000.0	357500.0	83.86185	(59, 1)
439000.0	357000.0	103.50711	(278, 1)	439500.0	357000.0	86.66915	(279, 1)
438000.0	355500.0	98.80868	(294, 1)	438500.0	355500.0	103.22723	(7, 1)
437500.0	355000.0	96.30566	(59, 1)	438000.0	355000.0	102.82031	(7, 1)
438500.0	355000.0	114.30699	(294, 1)	439000.0	355000.0	121.83291	(7, 1)
437500.0	354500.0	103.30661	(59, 1)	438000.0	354500.0	100.15749	(294, 1)
438500.0	354500.0	114.49532	(7, 1)	439000.0	354500.0	111.97515	(59, 1)
439500.0	354500.0	80.38575	(7, 1)	437500.0	354000.0	99.52345	(7, 1)
438000.0	354000.0	103.17715	(294, 1)	438500.0	354000.0	114.02538	(7, 1)
439000.0	354000.0	89.31770	(59, 1)	439500.0	354000.0	78.80009	(278, 1)
438000.0	353500.0	103.75491	(7, 1)	438500.0	353500.0	101.05135	(59, 1)
439000.0	353500.0	87.33742	(315, 1)	437000.0	353500.0	105.06509	(7, 1)
436500.0	353000.0	146.13319	(59, 1)	437000.0	353000.0	121.53332	(7, 1)
437500.0	353000.0	97.90152	(7, 1)	438000.0	353000.0	103.24117	(7, 1)
436000.0	352500.0	172.05551	(59, 1)	436500.0	352500.0	191.25192	(7, 1)
437000.0	352500.0	120.43579	(59, 1)	437500.0	352500.0	98.75633	(315, 1)
438000.0	352500.0	84.81210	(59, 1)	436000.0	352000.0	228.06787	(7, 1)
436500.0	352000.0	156.57585	(315, 1)	437000.0	352000.0	118.45152	(7, 1)
437500.0	352000.0	106.84839	(315, 1)	438000.0	352000.0	76.36385	(294, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY, PER.)	- X -	- Y -	CON.	(DAY, PER.)
436500.0	351500.0	117.95309	(315, 1)	437000.0	351500.0	136.43198	(7, 1)
437500.0	351500.0	103.36328	(294, 1)	438000.0	351500.0	82.95727	(7, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* 50 MAXIMUM 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *

* FROM ALL SOURCES *

RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y(METERS) OR DIRECTION (DEGREES)	RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y(METERS) OR DIRECTION (DEGREES)
1	277.50391	1	59	436000.0	352000.0	26	133.19205	1	294	436500.0	352000.0
2	264.56842	1	59	436500.0	352500.0	27	130.43375	1	7	437500.0	355000.0
3	228.06787	1	7	436000.0	352000.0	28	129.33102	1	278	436500.0	352500.0
4	191.25192	1	7	436500.0	352500.0	29	129.00748	1	7	438500.0	357500.0
5	186.99603	1	279	438500.0	358000.0	30	128.73982	1	7	436500.0	353000.0
6	180.87070	1	279	436000.0	352500.0	31	127.91920	1	279	436500.0	352500.0
7	178.26114	1	59	437000.0	353000.0	32	127.43387	1	278	436000.0	352000.0
8	172.05551	1	59	436000.0	352500.0	33	127.41152	1	59	438000.0	354000.0
9	166.69232	1	279	436500.0	353000.0	34	126.50314	1	59	438500.0	354500.0
10	166.46146	1	59	436500.0	352000.0	35	126.15932	1	59	439000.0	355000.0
11	164.73199	1	294	437000.0	352000.0	36	125.55347	1	294	437000.0	352500.0
12	164.06300	1	7	436000.0	352500.0	37	125.20570	1	3	436500.0	352500.0
13	156.57585	1	315	436500.0	352000.0	38	124.94290	1	278	436500.0	352000.0
14	156.06030	1	294	436500.0	351500.0	39	123.76717	1	59	438000.0	354500.0
15	155.71843	1	7	436500.0	352000.0	40	122.80627	1	59	438500.0	357500.0
16	152.23361	1	279	438500.0	357500.0	41	122.27444	1	7	439500.0	357000.0
17	147.87177	1	3	436000.0	352000.0	42	121.83291	1	7	439000.0	355000.0
18	146.13319	1	59	436500.0	353000.0	43	121.53332	1	7	437000.0	353000.0
19	141.68961	1	279	436000.0	352000.0	44	120.43579	1	59	437000.0	352500.0
20	141.63745	1	279	439000.0	358000.0	45	119.73016	1	59	438000.0	353500.0
21	139.74402	1	294	437000.0	351500.0	46	119.37733	1	59	438500.0	355000.0
22	139.60307	1	279	439000.0	358500.0	47	118.85802	1	59	437500.0	354000.0
23	139.49989	1	279	438000.0	358000.0	48	118.73088	1	3	438500.0	357500.0
24	137.89052	1	3	436000.0	352500.0	49	118.50624	1	59	438500.0	354000.0
25	136.43198	1	7	437000.0	351500.0	50	118.45152	1	7	437000.0	352000.0

1974

ISCST COARSE GRID ANALYSIS

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

CALCULATE (CONCENTRATION=1,DEPOSITION=2)	ISW(1) = 1
RECEPTOR GRID SYSTEM (RECTANGULAR=1 OR 3, POLAR=2 OR 4)	ISW(2) = 1
DISCRETE RECEPTOR SYSTEM (RECTANGULAR=1,POLAR=2)	ISW(3) = 1
TERRAIN ELEVATIONS ARE READ (YES=1,NO=0)	ISW(4) = 0
CALCULATIONS ARE WRITTEN TO TAPE (YES=1,NO=0)	ISW(5) = 0
LIST ALL INPUT DATA (NO=0,YES=1,MET DATA ALSO=2)	ISW(6) = 1

COMPUTE AVERAGE CONCENTRATION (OR TOTAL DEPOSITION) WITH THE FOLLOWING TIME PERIODS:	
HOURLY (YES=1,NO=0)	ISW(7) = 0
2-HOUR (YES=1,NO=0)	ISW(8) = 0
3-HOUR (YES=1,NO=0)	ISW(9) = 1
4-HOUR (YES=1,NO=0)	ISW(10) = 0
6-HOUR (YES=1,NO=0)	ISW(11) = 0
8-HOUR (YES=1,NO=0)	ISW(12) = 0
12-HOUR (YES=1,NO=0)	ISW(13) = 0
24-HOUR (YES=1,NO=0)	ISW(14) = 1
PRINT 'N'-DAY TABLE(S) (YES=1,NO=0)	ISW(15) = 1

PRINT THE FOLLOWING TYPES OF TABLES WHOSE TIME PERIODS ARE SPECIFIED BY ISW(7) THROUGH ISW(14):	
DAILY TABLES (YES=1,NO=0)	ISW(16) = 0
HIGHEST & SECOND HIGHEST TABLES (YES=1,NO=0)	ISW(17) = 1
MAXIMUM 50 TABLES (YES=1,NO=0)	ISW(18) = 1
METEOROLOGICAL DATA INPUT METHOD (PRE-PROCESSED=1,CARD=2)	ISW(19) = 1
RURAL-URBAN OPTION (RURAL=0,URBAN MODE 1=1,URBAN MODE 2=2)	ISW(20) = 0
WIND PROFILE EXPONENT VALUES (DEFAULTS=1,USER ENTERS=2,3)	ISW(21) = 1
VERTICAL POT. TEMP. GRADIENT VALUES (DEFAULTS=1,USER ENTERS=2,3)	ISW(22) = 1
SCALE EMISSION RATES FOR ALL SOURCES (NO=0,YES>0)	ISW(23) = 0
PROGRAM CALCULATES FINAL PLUME RISE ONLY (YES=1,NO=2)	ISW(24) = 1
PROGRAM ADJUSTS ALL STACK HEIGHTS FOR DOWNWASH (YES=2,NO=1)	ISW(25) = 1

NUMBER OF INPUT SOURCES	NSOURC = 17
NUMBER OF SOURCE GROUPS (=0,ALL SOURCES)	NGROUP = 0
TIME PERIOD INTERVAL TO BE PRINTED (=0,ALL INTERVALS)	IPERD = 0
NUMBER OF X (RANGE) GRID VALUES	NXPNTS = 0
NUMBER OF Y (THETA) GRID VALUES	NYPNTS = 0
NUMBER OF DISCRETE RECEPTORS	NXWYPT = 80
SOURCE EMISSION RATE UNITS CONVERSION FACTOR	TK = .10000E+07
ENTRAINMENT COEFFICIENT FOR UNSTABLE ATMOSPHERE	BETA1 = 0.600
ENTRAINMENT COEFFICIENT FOR STABLE ATMOSPHERE	BETA2 = 0.600
HEIGHT ABOVE GROUND AT WHICH WIND SPEED WAS MEASURED	ZR = 7.00 METERS
LOGICAL UNIT NUMBER OF METEOROLOGICAL DATA	IMET = 9
DECAY COEFFICIENT FOR PHYSICAL OR CHEMICAL DEPLETION	DECAY = 0.000000E+00
SURFACE STATION NO.	ISS = 13889
YEAR OF SURFACE DATA	ISY = 74
UPPER AIR STATION NO.	IUS = 13861
YEAR OF UPPER AIR DATA	IUY = 74
ALLOCATED DATA STORAGE	LIMIT = 43500 WORDS
REQUIRED DATA STORAGE FOR THIS PROBLEM RUN	MIMIT = 5257 WORDS

COPIES

74

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

*** X,Y COORDINATES OF DISCRETE RECEPTORS ***
(METERS)

(440500.0, 361500.0), (441000.0, 361500.0), (441500.0, 361500.0), (440000.0, 361000.0), (440500.0, 361000.0),
(441000.0, 361000.0), (441500.0, 361000.0), (440000.0, 360500.0), (440500.0, 360500.0), (441000.0, 360500.0),
(441500.0, 360500.0), (442000.0, 360500.0), (440000.0, 360000.0), (440500.0, 360000.0), (441000.0, 360000.0),
(441500.0, 360000.0), (442000.0, 360000.0), (440500.0, 359500.0), (441000.0, 359500.0), (441500.0, 359500.0),
(442000.0, 359500.0), (441000.0, 359000.0), (441500.0, 359000.0), (438500.0, 359000.0), (439000.0, 359000.0),
(439500.0, 359000.0), (438000.0, 358500.0), (438500.0, 358500.0), (439000.0, 358500.0), (439500.0, 358500.0),
(440000.0, 358500.0), (438000.0, 358000.0), (438500.0, 358000.0), (439000.0, 358000.0), (439500.0, 358000.0),
(440000.0, 358000.0), (438500.0, 357500.0), (439000.0, 357500.0), (439500.0, 357500.0), (440000.0, 357500.0),
(439000.0, 357000.0), (439500.0, 357000.0), (438000.0, 355500.0), (438500.0, 355500.0), (437500.0, 355000.0),
(438000.0, 355000.0), (438500.0, 355000.0), (439000.0, 355000.0), (437500.0, 354500.0), (438000.0, 354500.0),
(438500.0, 354500.0), (439000.0, 354500.0), (439500.0, 354500.0), (437500.0, 354000.0), (438000.0, 354000.0),
(438500.0, 354000.0), (439000.0, 354000.0), (439500.0, 354000.0), (438000.0, 353500.0), (438500.0, 353500.0),
(439000.0, 353500.0), (437000.0, 353500.0), (436500.0, 353000.0), (437000.0, 353000.0), (437500.0, 353000.0),
(438000.0, 353000.0), (436000.0, 352500.0), (436500.0, 352500.0), (437000.0, 352500.0), (437500.0, 352500.0),
(438000.0, 352500.0), (436000.0, 352000.0), (436500.0, 352000.0), (437000.0, 352000.0), (437500.0, 352000.0),
(438000.0, 352000.0), (436500.0, 351500.0), (437000.0, 351500.0), (437500.0, 351500.0), (438000.0, 351500.0),

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

*** SOURCE DATA ***

SOURCE NUMBER	T W P K E E	Y A NUMBER PART. CATS.	EMISSION RATE		X (METERS)	Y (METERS)	BASE ELEV. (METERS)	HEIGHT (METERS)	TEMP.	EXIT VEL.	BLDG. HEIGHT (METERS)	BLDG. LENGTH (METERS)	BLDG. WIDTH (METERS)
			TYPE=0,1 (GRAMS/SEC)	TYPE=2 (GRAMS/SEC)					TYPE=0 (DEG.K); VERT.DIM TYPE=1 (METERS)	TYPE=0 (M/SEC); HORZ.DIM DIAMETER TYPE=1,2 TYPE=0 (METERS)			
1	0 0	0	0.11766E+04	446900.0	366300.0	0.0	194.20	327.60	18.29	10.13	0.00	0.00	0.00
2	0 0	0	0.70570E+03	446900.0	364900.0	0.0	76.20	401.00	20.10	5.03	0.00	0.00	0.00
3	0 0	0	0.70570E+03	446900.0	364900.0	0.0	91.40	408.20	8.50	5.33	0.00	0.00	0.00
4	0 0	0	0.12556E+04	446900.0	364900.0	0.0	106.70	438.80	19.20	7.01	0.00	0.00	0.00
5	0 0	0	0.23160E+03	446900.0	364900.0	0.0	10.10	779.80	18.30	6.56	0.00	0.00	0.00
6	0 0	0	0.13180E+03	437670.0	353900.0	0.0	40.70	433.20	11.70	2.44	0.00	0.00	0.00
7	0 0	0	0.90600E+02	437670.0	353900.0	0.0	40.70	406.50	10.30	3.05	0.00	0.00	0.00
8	0 0	0	0.11030E+03	437670.0	353900.0	0.0	43.70	422.10	11.80	3.35	0.00	0.00	0.00
9	0 0	0	0.20970E+03	437670.0	353900.0	0.0	44.20	416.50	13.70	3.05	0.00	0.00	0.00
10	0 0	0	0.16520E+03	440080.0	359150.0	0.0	45.70	414.30	7.80	3.20	0.00	0.00	0.00
11	0 0	0	0.20480E+03	440080.0	359150.0	0.0	41.50	405.40	15.50	2.74	0.00	0.00	0.00
12	0 0	0	0.19120E+03	440080.0	359150.0	0.0	13.70	714.30	8.80	5.84	0.00	0.00	0.00
13	0 0	0	0.13800E+02	440080.0	359150.0	0.0	6.30	766.50	11.80	3.13	0.00	0.00	0.00
14	0 0	0	0.20840E+03	441800.0	365600.0	0.0	32.30	433.00	16.10	2.13	0.00	0.00	0.00
15	0 0	0	0.82200E+02	437900.0	366800.0	0.0	15.90	505.00	8.60	1.37	0.00	0.00	0.00
16	0 0	0	0.54400E+02	439900.0	359300.0	0.0	76.20	477.00	9.20	3.78	0.00	0.00	0.00
17	0 0	0	0.25600E+02	447040.0	366570.0	0.0	85.40	441.00	12.20	2.08	0.00	0.00	0.00

Source NO.

Source Name

1	SJRPP Units 1 & 2
2	Northside Unit 1
3	Northside Unit 2
4	Northside Unit 3
5	Northside CT 3, 4, 5, 6
6	Southside Units 1 & 2
7	Southside Unit 3
8	Southside Unit 4
9	Southside Unit 5
10	Kennedy Units 8 & 9
11	Kennedy Unit 10
12	Kennedy CT 3, 4, 5, 6
13	Kennedy CT 1
14	St. Regis (All major sources)
15	Anheuser Busch (All major sources)
16	Alton Box Board (All major sources)
17	SJRPP Aux. Boiler

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY, PER.)	- X -	- Y -	CON.	(DAY, PER.)
440500.0	361500.0	231.78654	(237, 5)	441000.0	361500.0	237.44872	(237, 5)
441500.0	361500.0	217.14568	(237, 5)	440000.0	361000.0	216.98175	(252, 7)
440500.0	361000.0	200.12405	(237, 5)	441000.0	361000.0	171.91843	(237, 5)
441500.0	361000.0	161.15836	(295, 6)	440000.0	360500.0	165.43506	(237, 5)
440500.0	360500.0	184.86356	(252, 7)	441000.0	360500.0	184.37341	(295, 6)
441500.0	360500.0	171.46106	(295, 6)	442000.0	360500.0	205.93228	(360, 6)
440000.0	360000.0	164.13422	(331, 7)	440500.0	360000.0	241.57709	(252, 7)
441000.0	360000.0	164.88184	(295, 6)	441500.0	360000.0	213.71672	(360, 6)
442000.0	360000.0	290.01556	(252, 6)	440500.0	359500.0	178.80716	(360, 6)
441000.0	359500.0	224.27310	(252, 6)	441500.0	359500.0	297.74738	(252, 6)
442000.0	359500.0	278.05597	(252, 6)	441000.0	359000.0	301.68948	(252, 6)
441500.0	359000.0	285.82959	(252, 6)	438500.0	359000.0	271.05200	(237, 5)
439000.0	359000.0	271.30389	(237, 5)	439500.0	359000.0	189.82806	(295, 6)
438000.0	358500.0	355.83350	(263, 1)	438500.0	358500.0	276.72491	(110, 5)
439000.0	358500.0	375.49158	(237, 5)	439500.0	358500.0	215.94072	(360, 6)
440000.0	358500.0	239.75916	(252, 6)	438000.0	358000.0	352.91211	(263, 1)
438500.0	358000.0	365.12546	(295, 6)	439000.0	358000.0	355.21225	(360, 6)
439500.0	358000.0	328.38458	(331, 4)	440000.0	358000.0	301.60159	(252, 6)
438500.0	357500.0	448.92407	(252, 6)	439000.0	357500.0	325.38733	(237, 4)
439500.0	357500.0	298.50256	(252, 6)	440000.0	357500.0	291.50208	(252, 6)
439000.0	357000.0	298.66882	(331, 4)	439500.0	357000.0	310.40704	(278, 3)
438000.0	355500.0	328.30194	(263, 1)	438500.0	355500.0	314.24976	(278, 6)
437500.0	355000.0	289.08563	(252, 6)	438000.0	355000.0	322.45447	(263, 1)
438500.0	355000.0	235.94397	(278, 6)	439000.0	355000.0	261.12744	(278, 3)
437500.0	354500.0	239.75833	(252, 6)	438000.0	354500.0	316.51740	(263, 1)
438500.0	354500.0	226.23936	(279, 6)	439000.0	354500.0	232.97087	(278, 3)
439500.0	354500.0	247.57687	(295, 7)	437500.0	354000.0	223.61455	(278, 4)
438000.0	354000.0	310.54626	(263, 1)	438500.0	354000.0	212.94098	(237, 4)
439000.0	354000.0	267.91873	(295, 7)	439500.0	354000.0	244.91879	(295, 7)
438000.0	353500.0	304.58405	(263, 1)	438500.0	353500.0	220.24841	(237, 4)
439000.0	353500.0	288.57416	(295, 7)	437000.0	353500.0	214.97369	(237, 5)
436500.0	353000.0	253.29791	(237, 5)	437000.0	353000.0	398.83212	(237, 4)
437500.0	353000.0	206.32896	(278, 6)	438000.0	353000.0	298.66425	(263, 1)
436000.0	352500.0	372.85349	(360, 6)	436500.0	352500.0	496.83908	(237, 4)
437000.0	352500.0	619.36609	(331, 4)	437500.0	352500.0	199.12936	(237, 4)
438000.0	352500.0	292.81265	(263, 1)	436000.0	352000.0	476.46472	(252, 6)
436500.0	352000.0	494.19000	(237, 4)	437000.0	352000.0	464.60107	(331, 4)
437500.0	352000.0	201.43669	(237, 4)	438000.0	352000.0	287.04871	(263, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
! * FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY, PER.)	- X -	- Y -	CON.	(DAY, PER.)
436500.0	351500.0	484.88086	(331, 4)	437000.0	351500.0	415.94806	(278, 3)
437500.0	351500.0	237.19402	(278, 2)	438000.0	351500.0	281.02368	(263, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY, PER.)	- X -	- Y -	CON.	(DAY, PER.)
440500.0	361500.0	215.32034	(263, 6)	441000.0	361500.0	170.92113	(110, 3)
441500.0	361500.0	128.98834	(237, 6)	440000.0	361000.0	210.34579	(237, 5)
440500.0	361000.0	166.19699	(331, 8)	441000.0	361000.0	132.21095	(110, 3)
441500.0	361000.0	132.47258	(237, 5)	440000.0	360500.0	152.25365	(331, 7)
440500.0	360500.0	136.85573	(237, 5)	441000.0	360500.0	140.33682	(331, 8)
441500.0	360500.0	140.91391	(360, 6)	442000.0	360500.0	194.54985	(252, 6)
440000.0	360000.0	158.39458	(295, 6)	440500.0	360000.0	194.61038	(295, 6)
441000.0	360000.0	162.64769	(360, 6)	441500.0	360000.0	211.53329	(252, 6)
442000.0	360000.0	199.41711	(279, 4)	440500.0	359500.0	175.26817	(252, 7)
441000.0	359500.0	217.24968	(360, 6)	441500.0	359500.0	199.39417	(279, 4)
442000.0	359500.0	217.53522	(237, 4)	441000.0	359000.0	213.90752	(252, 7)
441500.0	359000.0	218.48782	(279, 4)	438500.0	359000.0	199.70531	(110, 4)
439000.0	359000.0	190.20195	(295, 6)	439500.0	359000.0	171.38847	(252, 8)
438000.0	358500.0	332.17496	(110, 5)	438500.0	358500.0	276.38492	(237, 5)
439000.0	358500.0	205.41844	(295, 6)	439500.0	358500.0	201.55620	(252, 8)
440000.0	358500.0	216.13956	(360, 6)	438000.0	358000.0	320.18799	(237, 5)
438500.0	358000.0	234.80740	(237, 5)	439000.0	358000.0	355.11813	(252, 6)
439500.0	358000.0	246.91803	(252, 6)	440000.0	358000.0	205.82858	(333, 4)
438500.0	357500.0	420.87521	(360, 6)	439000.0	357500.0	301.49261	(252, 6)
439500.0	357500.0	274.91754	(331, 4)	440000.0	357500.0	209.71713	(279, 4)
439000.0	357000.0	298.31979	(252, 6)	439500.0	357000.0	288.99280	(252, 6)
438000.0	355500.0	285.35483	(252, 6)	438500.0	355500.0	248.50714	(278, 4)
437500.0	355000.0	263.00537	(279, 5)	438000.0	355000.0	248.51801	(278, 4)
438500.0	355000.0	235.15930	(279, 6)	439000.0	355000.0	211.95909	(237, 4)
437500.0	354500.0	238.62436	(279, 2)	438000.0	354500.0	278.54749	(278, 6)
438500.0	354500.0	199.20061	(263, 1)	439000.0	354500.0	227.96605	(237, 4)
439500.0	354500.0	243.08252	(237, 4)	437500.0	354000.0	213.52251	(278, 6)
438000.0	354000.0	230.66312	(278, 6)	438500.0	354000.0	200.32532	(263, 1)
439000.0	354000.0	232.05766	(237, 4)	439500.0	354000.0	230.17430	(237, 4)
438000.0	353500.0	200.33476	(237, 4)	438500.0	353500.0	202.09354	(278, 3)
439000.0	353500.0	224.99956	(237, 4)	437000.0	353500.0	208.54437	(279, 2)
436500.0	353000.0	244.63651	(295, 6)	437000.0	353000.0	316.98157	(279, 7)
437500.0	353000.0	193.48413	(279, 3)	438000.0	353000.0	208.80508	(237, 4)
436000.0	352500.0	322.01791	(295, 6)	436500.0	352500.0	420.35504	(279, 4)
437000.0	352500.0	445.44061	(278, 6)	437500.0	352500.0	195.86009	(279, 3)
438000.0	352500.0	209.60472	(237, 4)	436000.0	352000.0	460.92419	(279, 4)
436500.0	352000.0	481.14294	(279, 7)	437000.0	352000.0	359.67856	(278, 6)
437500.0	352000.0	164.42540	(295, 7)	438000.0	352000.0	207.15276	(331, 7)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY, PER.)	- X -	- Y -	CON.	(DAY, PER.)
436500.0	351500.0	425.65259	(278, 6)	437000.0	351500.0	323.30072	(331, 3)
437500.0	351500.0	197.61301	(237, 4)	438000.0	351500.0	230.54834	(331, 7)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* 50 MAXIMUM 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *

\$

* FROM ALL SOURCES *

RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y(METERS) OR DIRECTION (DEGREES)	RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y(METERS) OR DIRECTION (DEGREES)
1	619.36609	4	331	437000.0	352500.0	26	386.40659	8	279	436500.0	352000.0
2	496.83908	4	237	436500.0	352500.0	27	385.03098	4	278	437000.0	352500.0
3	494.19000	4	237	436500.0	352000.0	28	378.95407	4	333	438500.0	357500.0
4	484.88086	4	331	436500.0	351500.0	29	375.49158	5	237	439000.0	358500.0
5	481.14294	7	279	436500.0	352000.0	30	372.85349	6	360	436000.0	352500.0
6	476.46472	6	252	436000.0	352000.0	31	372.14743	6	279	436000.0	352000.0
7	464.60107	4	331	437000.0	352000.0	32	369.30255	2	279	436000.0	352000.0
8	460.92419	4	279	436000.0	352000.0	33	365.85107	7	278	436500.0	351500.0
9	448.92407	6	252	438500.0	357500.0	34	365.12546	6	295	438500.0	358000.0
10	446.96863	2	279	436500.0	352000.0	35	362.75290	5	295	436000.0	352000.0
11	445.44061	6	278	437000.0	352500.0	36	359.67856	6	278	437000.0	352000.0
12	442.13928	5	279	436000.0	352000.0	37	355.83350	1	263	438000.0	358500.0
13	425.65259	6	278	436500.0	351500.0	38	355.21225	6	360	439000.0	358000.0
14	420.87521	6	360	438500.0	357500.0	39	355.11813	6	252	439000.0	358000.0
15	420.35504	4	279	436500.0	352500.0	40	353.36652	4	279	438500.0	357500.0
16	415.94806	3	278	437000.0	351500.0	41	352.91211	1	263	438000.0	358000.0
17	415.83871	1	279	436000.0	352000.0	42	348.92365	5	360	436000.0	352000.0
18	413.69995	7	360	436000.0	352000.0	43	345.08261	4	278	436500.0	352500.0
19	409.10214	4	237	436000.0	352000.0	44	341.19656	2	279	436500.0	352500.0
20	402.41049	5	360	436500.0	352500.0	45	338.66162	3	279	437000.0	352000.0
21	398.83212	4	237	437000.0	353000.0	46	337.46927	3	279	436500.0	351500.0
22	397.46481	6	279	436500.0	352500.0	47	333.87347	1	279	436500.0	352500.0
23	396.64218	4	278	436500.0	351500.0	48	332.17496	5	110	438000.0	358500.0
24	388.30670	6	252	436500.0	352500.0	49	328.38458	4	331	439500.0	358000.0
25	386.79224	5	279	436500.0	352500.0	50	328.30194	1	263	438000.0	355500.0

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY,PER.)	- X -	- Y -	CON.	(DAY,PER.)
440500.0	361500.0	70.13333	(285, 1)	441000.0	361500.0	48.39106	(237, 1)
441500.0	361500.0	44.36129	(237, 1)	440000.0	361000.0	54.45741	(285, 1)
440500.0	361000.0	59.00741	(331, 1)	441000.0	361000.0	38.87117	(295, 1)
441500.0	361000.0	53.03902	(295, 1)	440000.0	360500.0	48.55576	(331, 1)
440500.0	360500.0	49.25462	(252, 1)	441000.0	360500.0	63.76252	(295, 1)
441500.0	360500.0	64.98949	(295, 1)	442000.0	360500.0	77.68185	(360, 1)
440000.0	360000.0	51.09865	(331, 1)	440500.0	360000.0	61.90421	(295, 1)
441000.0	360000.0	74.63667	(295, 1)	441500.0	360000.0	77.36292	(360, 1)
442000.0	360000.0	86.45797	(279, 1)	440500.0	359500.0	68.89302	(360, 1)
441000.0	359500.0	79.57434	(360, 1)	441500.0	359500.0	86.92380	(279, 1)
442000.0	359500.0	108.09146	(279, 1)	441000.0	359000.0	90.13497	(252, 1)
441500.0	359000.0	107.32967	(279, 1)	438500.0	359000.0	62.38981	(237, 1)
439000.0	359000.0	58.22964	(237, 1)	439500.0	359000.0	65.10252	(295, 1)
438000.0	358500.0	110.07125	(110, 1)	438500.0	358500.0	97.54702	(110, 1)
439000.0	358500.0	72.73378	(237, 1)	439500.0	358500.0	81.59825	(360, 1)
440000.0	358500.0	88.60522	(360, 1)	438000.0	358000.0	96.55575	(263, 1)
438500.0	358000.0	107.27306	(295, 1)	439000.0	358000.0	155.46857	(279, 1)
439500.0	358000.0	132.05515	(279, 1)	440000.0	358000.0	95.43919	(360, 1)
438500.0	357500.0	172.88914	(360, 1)	439000.0	357500.0	201.25572	(279, 1)
439500.0	357500.0	137.74376	(279, 1)	440000.0	357500.0	106.80457	(279, 1)
439000.0	357000.0	182.43582	(279, 1)	439500.0	357000.0	142.43051	(279, 1)
438000.0	355500.0	198.64218	(279, 1)	438500.0	355500.0	157.05118	(278, 1)
437500.0	355000.0	192.97588	(279, 1)	438000.0	355000.0	160.94302	(279, 1)
438500.0	355000.0	140.98846	(278, 1)	439000.0	355000.0	105.41246	(279, 1)
437500.0	354500.0	173.49866	(279, 1)	438000.0	354500.0	139.21555	(278, 1)
438500.0	354500.0	115.97890	(278, 1)	439000.0	354500.0	95.79543	(279, 1)
439500.0	354500.0	87.10256	(279, 1)	437500.0	354000.0		
						JJ:B:B:Jb	
						J	
128.79073	(278, 1)	438500.0	354000.0	100.11562	(279, 1)	438000.0	354000.0
439000.0	354000.0	93.41628	(279, 1)	439500.0	354000.0	90.42892	(279, 1)
438000.0	353500.0	109.00426	(278, 1)	438500.0	353500.0	95.07970	(279, 1)
439000.0	353500.0	94.72273	(279, 1)	437000.0	353500.0	148.21509	(279, 1)
436500.0	353000.0	157.00192	(279, 1)	437000.0	353000.0	216.28561	(279, 1)
437500.0	353000.0	123.63838	(278, 1)	438000.0	353000.0	94.90536	(279, 1)
436000.0	352500.0	174.11349	(279, 1)	436500.0	352500.0	289.32715	(279, 1)
437000.0	352500.0	215.08871	(278, 1)	437500.0	352500.0	114.38327	(278, 1)
436500.0	352000.0	93.63665	(279, 1)	437000.0	352000.0	300.70346	(279, 1)
436500.0	352000.0	288.45782	(279, 1)	437000.0	352000.0	226.94560	(278, 1)
437500.0	352000.0	113.86557	(278, 1)	438000.0	352000.0	94.13095	(279, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY, PER.)	- X -	- Y -	CON.	(DAY, PER.)
436500.0	351500.0	221.20651	(278, 1)	437000.0	351500.0	185.59964	(278, 1)
437500.0	351500.0	118.18765	(278, 1)	438000.0	351500.0	94.73820	(279, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY,PER.)	- X -	- Y -	CON.	(DAY,PER.)
440500.0	361500.0	59.36013	(331, 1)	441000.0	361500.0	44.79194	(110, 1)
441500.0	361500.0	32.48444	(295, 1)	440000.0	361000.0	48.43383	(278, 1)
440500.0	361000.0	43.22787	(285, 1)	441000.0	361000.0	36.94936	(237, 1)
441500.0	361000.0	28.69841	(237, 1)	440000.0	360500.0	37.09625	(278, 1)
440500.0	360500.0	48.65523	(331, 1)	441000.0	360500.0	37.40297	(331, 1)
441500.0	360500.0	53.04441	(360, 1)	442000.0	360500.0	55.44996	(295, 1)
440000.0	360000.0	39.61294	(295, 1)	440500.0	360000.0	57.80228	(252, 1)
441000.0	360000.0	59.47390	(360, 1)	441500.0	360000.0	63.70335	(295, 1)
442000.0	360000.0	85.32269	(360, 1)	440500.0	359500.0	63.46964	(295, 1)
441000.0	359500.0	73.98362	(295, 1)	441500.0	359500.0	85.83817	(360, 1)
442000.0	359500.0	83.70547	(360, 1)	441000.0	359000.0	88.49388	(279, 1)
441500.0	359000.0	83.74217	(360, 1)	438500.0	359000.0	50.77842	(295, 1)
439000.0	359000.0	49.13122	(295, 1)	439500.0	359000.0	56.36641	(331, 1)
438000.0	358500.0	66.46747	(263, 1)	438500.0	358500.0	74.83786	(295, 1)
439000.0	358500.0	63.47150	(295, 1)	439500.0	358500.0	73.48602	(279, 1)
440000.0	358500.0	64.62354	(295, 1)	438000.0	358000.0	91.29897	(285, 1)
438500.0	358000.0	84.73215	(360, 1)	439000.0	358000.0	135.21382	(360, 1)
439500.0	358000.0	101.41757	(331, 1)	440000.0	358000.0	91.80458	(279, 1)
438500.0	357500.0	169.19687	(279, 1)	439000.0	357500.0	110.18645	(295, 1)
439500.0	357500.0	131.30519	(278, 1)	440000.0	357500.0	95.39822	(360, 1)
439000.0	357000.0	137.34464	(278, 1)	439500.0	357000.0	118.68375	(278, 1)
438000.0	355500.0	107.95940	(278, 1)	438500.0	355500.0	145.80850	(279, 1)
437500.0	355000.0	115.43743	(295, 1)	438000.0	355000.0	129.07619	(278, 1)
438500.0	355000.0	126.24991	(279, 1)	439000.0	355000.0	102.05284	(278, 1)
437500.0	354500.0	104.13094	(278, 1)	438000.0	354500.0	128.88782	(279, 1)
438500.0	354500.0	110.95299	(279, 1)	439000.0	354500.0	85.31268	(278, 1)
439500.0	354500.0	83.01732	(295, 1)	437500.0	354000.0	115.82574	(278, 1)
438000.0	354000.0	109.84558	(279, 1)	438500.0	354000.0	98.10305	(278, 1)
439000.0	354000.0	76.21771	(331, 1)	439500.0	354000.0	88.23305	(295, 1)
438000.0	353500.0	99.63846	(279, 1)	438500.0	353500.0	87.27505	(278, 1)
439000.0	353500.0	82.58627	(295, 1)	437000.0	353500.0	95.95320	(278, 1)
436500.0	353000.0	130.44203	(295, 1)	437000.0	353000.0	140.77425	(278, 1)
437500.0	353000.0	107.54710	(279, 1)	438000.0	353000.0	92.43096	(278, 1)
436000.0	352500.0	169.48547	(360, 1)	436500.0	352500.0	157.19843	(278, 1)
437000.0	352500.0	194.51456	(279, 1)	437500.0	352500.0	101.36517	(279, 1)
438000.0	352500.0	83.12035	(278, 1)	436000.0	352000.0	189.30423	(360, 1)
436500.0	35200.0	163.39975	(278, 1)	437000.0	352000.0	155.30228	(279, 1)
437500.0	352000.0	96.24496	(279, 1)	438000.0	352000.0	83.52173	(278, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
 * FROM ALL SOURCES *
 * FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY,PER.)	- X -	- Y -	CON.	(DAY,PER.)
436500.0	351500.0	196.77879	(279, 1)	437000.0	351500.0	137.63115	(279, 1)
437500.0	351500.0	94.63753	(279, 1)	438000.0	351500.0	90.99691	(278, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* 50 MAXIMUM 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *

* FROM ALL SOURCES *

RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y(METERS) OR DIRECTION (DEGREES)	RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y(METERS) OR DIRECTION (DEGREES)
1	300.70346	1	279	436000.0	352000.0	26	157.05118	1	278	438500.0	355500.0
2	289.32715	1	279	436500.0	352500.0	27	157.00192	1	279	436500.0	353000.0
3	288.45782	1	279	436500.0	352000.0	28	155.46857	1	279	439000.0	358000.0
4	226.94560	1	278	437000.0	352000.0	29	155.30228	1	279	437000.0	352000.0
5	221.20651	1	278	436500.0	351500.0	30	148.91150	1	360	436500.0	352500.0
6	216.28561	1	279	437000.0	353000.0	31	148.21509	1	279	437000.0	353500.0
7	215.08871	1	278	437000.0	352500.0	32	145.80850	1	279	438500.0	355500.0
8	201.25572	1	279	439000.0	357500.0	33	142.43051	1	279	439500.0	357000.0
9	198.64218	1	279	438000.0	355500.0	34	142.36661	1	278	436000.0	352000.0
10	196.77879	1	279	436500.0	351500.0	35	140.98846	1	278	438500.0	355000.0
11	194.51456	1	279	437000.0	352500.0	36	140.77425	1	278	437000.0	353000.0
12	192.97588	1	279	437500.0	355000.0	37	139.29787	1	279	437500.0	354000.0
13	189.30423	1	360	436000.0	352000.0	38	139.21555	1	278	438000.0	354500.0
14	185.59964	1	278	437000.0	351500.0	39	137.74376	1	279	439500.0	357500.0
15	182.43582	1	279	439000.0	357000.0	40	137.63115	1	279	437000.0	351500.0
16	174.11349	1	279	436000.0	352500.0	41	137.34464	1	278	439000.0	357000.0
17	173.49866	1	279	437500.0	354500.0	42	136.41620	1	295	436500.0	352500.0
18	172.88914	1	360	438500.0	357500.0	43	135.21382	1	360	439000.0	358000.0
19	169.48547	1	360	436000.0	352500.0	44	132.99098	1	295	438500.0	357500.0
20	169.19687	1	279	438500.0	357500.0	45	132.08054	1	331	437000.0	352000.0
21	165.38443	1	295	436000.0	352500.0	46	132.05515	1	279	439500.0	358000.0
22	163.39975	1	278	436500.0	352000.0	47	131.30519	1	278	439500.0	357500.0
23	160.94302	1	279	438000.0	355000.0	48	130.44203	1	295	436500.0	353000.0
24	158.37761	1	295	436000.0	352000.0	49	130.21332	1	252	436000.0	352000.0
25	157.19843	1	278	436500.0	352500.0	50	129.23761	1	295	436500.0	352000.0

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ISCST FINE GRID ANALYSIS
PRODUCING HIGHEST 3-HOUR AVERAGE

Best Available Copy

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

CALCULATE (CONCENTRATION=1,DEPOSITION=2) ISW(1) = 1
RECEPTOR GRID SYSTEM (RECTANGULAR=1 OR 3, POLAR=2 OR 4) ISW(2) = 3
DISCRETE RECEPTOR SYSTEM (RECTANGULAR=1,POLAR=2) ISW(3) = 1
TERRAIN ELEVATIONS ARE READ (YES=1,NO=0) ISW(4) = 0
CALCULATIONS ARE WRITTEN TO TAPE (YES=1,NO=0) ISW(5) = 0
LIST ALL INPUT DATA (NO=0,YES=1,MET DATA ALSO=2) ISW(6) = 2

COMPUTE AVERAGE CONCENTRATION (OR TOTAL DEPOSITION)
WITH THE FOLLOWING TIME PERIODS:

HOURLY (YES=1,NO=0) ISW(7) = 0
2-HOUR (YES=1,NO=0) ISW(8) = 0
3-HOUR (YES=1,NO=0) ISW(9) = 1
4-HOUR (YES=1,NO=0) ISW(10) = 0
6-HOUR (YES=1,NO=0) ISW(11) = 0
8-HOUR (YES=1,NO=0) ISW(12) = 0
12-HOUR (YES=1,NO=0) ISW(13) = 0
24-HOUR (YES=1,NO=0) ISW(14) = 1
PRINT 'N'-DAY TABLE(S) (YES=1,NO=0) ISW(15) = 0

PRINT THE FOLLOWING TYPES OF TABLES WHOSE TIME PERIODS ARE
SPECIFIED BY ISW(7) THROUGH ISW(14):

DAILY TABLES (YES=1,NO=0) ISW(16) = 0
HIGHEST & SECOND HIGHEST TABLES (YES=1,NO=0) ISW(17) = 1
MAXIMUM 50 TABLES (YES=1,NO=0) ISW(18) = 1
METEOROLOGICAL DATA INPUT METHOD (PRE-PROCESSED=1,CARD=2) ISW(19) = 1
RURAL-URBAN OPTION (RURAL=0,URBAN MODE 1=1,URBAN MODE 2=2) ISW(20) = 0
WIND PROFILE EXPONENT VALUES (DEFAULTS=1,USER ENTERS=2,3) ISW(21) = 1
VERTICAL POT. TEMP. GRADIENT VALUES (DEFAULTS=1,USER ENTERS=2,3) ISW(22) = 1
SCALE EMISSION RATES FOR ALL SOURCES (NO=0,YES>0) ISW(23) = 0
PROGRAM CALCULATES FINAL PLUME RISE ONLY (YES=1,NO=2) ISW(24) = 1
PROGRAM ADJUSTS ALL STACK HEIGHTS FOR DOWNWASH (YES=2,NO=1) ISW(25) = 1

NUMBER OF INPUT SOURCES
NUMBER OF SOURCE GROUPS (=0,ALL SOURCES)
TIME PERIOD INTERVAL TO BE PRINTED (=0,ALL INTERVALS)
NUMBER OF X (RANGE) GRID VALUES
NUMBER OF Y (THETA) GRID VALUES
NUMBER OF DISCRETE RECEPTORS
SOURCE EMISSION RATE UNITS CONVERSION FACTOR
ENTRAINMENT COEFFICIENT FOR UNSTABLE ATMOSPHERE
ENTRAINMENT COEFFICIENT FOR STABLE ATMOSPHERE
HEIGHT ABOVE GROUND AT WHICH WIND SPEED WAS MEASURED
LOGICAL UNIT NUMBER OF METEOROLOGICAL DATA
DECAY COEFFICIENT FOR PHYSICAL OR CHEMICAL DEPLETION
SURFACE STATION NO.
YEAR OF SURFACE DATA
UPPER AIR STATION NO.
YEAR OF UPPER AIR DATA
ALLOCATED DATA STORAGE
REQUIRED DATA STORAGE FOR THIS PROBLEM RUN

NSOURC = 17
NGROUP = 0
IPERD = 0
NXPNTS = 20
NYPNTS = 18
NXWYPT = 0
TK = .10000E+07
BETA1 = 0.600
BETA2 = 0.600
ZR = 7.00 METERS
IMET = 9
DECAY = 0.000000E+00
ISS = 13889
ISY = 70
IUS = 13861
IUY = 70
LIMIT = 43500 WORDS
MIMIT = 8415 WORDS

1970

DMT 70

From Grid 1970

H13-6

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

*** X-COORDINATES OF RECTANGULAR GRID SYSTEM ***
(METERS)

435500.0, 435600.0, 435700.0, 435800.0, 435900.0, 436000.0, 436100.0, 436200.0, 436300.0, 436400.0,
436500.0, 436600.0, 436700.0, 436800.0, 436900.0, 437000.0, 437100.0, 437200.0, 437300.0, 437400.0,

*** Y-COORDINATES OF RECTANGULAR GRID SYSTEM ***
(METERS)

351700.0, 351800.0, 351900.0, 352000.0, 352100.0, 352200.0, 352300.0, 352400.0, 352500.0, 352600.0,
352700.0, 352800.0, 352900.0, 353000.0, 353100.0, 353200.0, 353300.0, 353400.0,

*** SOURCE DATA ***

SOURCE NUMBER	T W Y A P K E E	PART. CATS.	EMISSION RATE		X (METERS)	Y (METERS)	BASE ELEV. (METERS)	HEIGHT (METERS)	TEMP.	EXIT VEL.	BLDG. HEIGHT (METERS)	BLDG. LENGTH (METERS)	BLDG. WIDTH (METERS)
			TYPE=0,1 (GRAMS/SEC)	TYPE=2 (GRAMS/SEC)					TYPE=0 (DEG.K); VERT.DIM (METERS)	TYPE=0 (M/SEC); HORZ.DIM (METERS)			
1	0 0	0	0.11766E+04	446900.0	366300.0	0.0	194.20	327.60	18.29	10.13	0.00	0.00	0.00
2	0 0	0	0.70570E+03	446900.0	364900.0	0.0	76.20	401.00	20.10	5.03	0.00	0.00	0.00
3	0 0	0	0.70570E+03	446900.0	364900.0	0.0	91.40	408.20	8.50	5.33	0.00	0.00	0.00
4	0 0	0	0.12556E+04	446900.0	364900.0	0.0	106.70	438.80	19.20	7.01	0.00	0.00	0.00
5	0 0	0	0.23160E+03	446900.0	364900.0	0.0	10.10	779.80	18.30	6.56	0.00	0.00	0.00
6	0 0	0	0.13180E+03	437670.0	353900.0	0.0	40.70	433.20	11.70	2.44	0.00	0.00	0.00
7	0 0	0	0.90600E+02	437670.0	353900.0	0.0	40.70	406.50	10.30	3.05	0.00	0.00	0.00
8	0 0	0	0.11030E+03	437670.0	353900.0	0.0	43.70	422.10	11.80	3.35	0.00	0.00	0.00
9	0 0	0	0.20970E+03	437670.0	353900.0	0.0	44.20	416.50	13.70	3.05	0.00	0.00	0.00
10	0 0	0	0.16520E+03	440080.0	359150.0	0.0	45.70	414.30	7.80	3.20	0.00	0.00	0.00
11	0 0	0	0.20480E+03	440080.0	359150.0	0.0	41.50	405.40	15.50	2.74	0.00	0.00	0.00
12	0 0	0	0.19120E+03	440080.0	359150.0	0.0	13.70	714.30	8.80	5.84	0.00	0.00	0.00
13	0 0	0	0.13800E+02	440080.0	359150.0	0.0	6.30	766.50	11.80	3.13	0.00	0.00	0.00
14	0 0	0	0.20840E+03	441800.0	365600.0	0.0	32.30	433.00	16.10	2.13	0.00	0.00	0.00
15	0 0	0	0.82200E+02	437900.0	366800.0	0.0	15.90	505.00	8.60	1.37	0.00	0.00	0.00
16	0 0	0	0.54400E+02	439900.0	359300.0	0.0	76.20	477.00	9.20	3.78	0.00	0.00	0.00
17	0 0	0	0.25600E+02	447040.0	366570.0	0.0	85.40	441.00	12.20	2.08	0.00	0.00	0.00

Source NO.	Source Name
1	SJRPP Units 1 & 2
2	Northside Unit 1
3	Northside Unit 2
4	Northside Unit 3
5	Northside CT 3, 4, 5, 6
6	Southside Units 1 & 2
7	Southside Unit 3
8	Southside Unit 4
9	Southside Unit 5
10	Kennedy Units 8 & 9
11	Kennedy Unit 10
12	Kennedy CT 3, 4, 5, 6
13	Kennedy CT 1
14	St. Regis (All major sources)
15	Anheuser Busch (All major sources)
16	Alton Box Board (All major sources)
17	SJRPP Aux. Boiler

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* METEOROLOGICAL DATA FOR DAY 2 *

HOUR	FLOW VECTOR (DEGREES)	RANDOM FLOW VECTOR (DEGREES)	WIND SPEED (MPS)	MIXING HEIGHT (METERS)	TEMP. (DEG. K)	INPUT STABILITY CATEGORY	ADJUSTED STABILITY CATEGORY
1	140.0	136.0	3.09	623.4	278.7	5	5
2	120.0	122.0	4.12	624.5	278.7	4	4
3	150.0	152.0	4.12	625.6	278.7	4	4
4	140.0	140.0	5.14	626.8	278.2	4	4
5	150.0	146.0	4.12	627.9	277.0	5	5
6	140.0	137.0	3.09	629.0	276.5	6	6
7	150.0	149.0	3.60	630.1	275.9	5	5
8	170.0	166.0	4.12	52.8	275.9	4	4
9	150.0	150.0	6.17	150.3	277.0	4	4
10	200.0	201.0	4.63	247.9	278.7	3	3
11	200.0	205.0	4.12	345.4	280.4	3	3
12	200.0	201.0	4.12	442.9	282.0	3	3
13	240.0	239.0	3.60	540.5	283.2	2	2
14	270.0	267.0	3.60	638.0	283.7	3	3
15	270.0	270.0	4.12	638.0	283.7	4	4
16	260.0	264.0	3.60	638.0	283.2	4	4
17	220.0	218.0	2.57	638.0	282.6	4	4
18	250.0	251.0	3.09	634.3	282.0	4	4
19	180.0	182.0	4.12	626.5	282.0	4	4
20	170.0	175.0	3.60	618.6	281.5	4	4
21	200.0	204.0	4.12	610.7	281.5	4	4
22	220.0	225.0	3.60	602.9	282.0	4	4
23	160.0	157.0	2.57	595.0	282.0	4	4
24	140.0	138.0	6.17	587.1	280.9	4	4

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* METEOROLOGICAL DATA FOR DAY 15 *

HOURL	FLOW VECTOR (DEGREES)	RANDOM FLOW VECTOR (DEGREES)	WIND SPEED (MPS)	MIXING HEIGHT (METERS)	TEMP. (DEG. K)	INPUT STABILITY CATEGORY	ADJUSTED STABILITY CATEGORY
1	280.0	280.0	3.60	699.9	283.7	4	4
2	250.0	252.0	4.12	670.3	284.3	4	4
3	220.0	218.0	4.12	640.7	284.3	4	4
4	230.0	230.0	4.12	611.1	283.7	4	4
5	220.0	225.0	4.63	581.5	283.7	4	4
6	230.0	230.0	4.12	551.9	284.3	4	4
7	250.0	249.0	5.14	522.3	285.9	4	4
8	240.0	242.0	4.63	492.7	285.9	4	4
9	270.0	267.0	7.20	463.0	285.9	4	4
10	280.0	277.0	5.66	433.4	287.0	4	4
11	270.0	272.0	8.23	403.8	286.5	4	4
12	240.0	240.0	6.69	374.2	285.9	4	4
13	200.0	204.0	7.20	344.6	285.4	4	4
14	220.0	220.0	7.72	315.0	284.8	4	4
15	240.0	243.0	7.20	315.0	285.4	4	4
16	260.0	256.0	7.72	315.0	285.4	4	4
17	240.0	243.0	6.69	315.0	285.4	4	4
18	230.0	227.0	7.20	317.3	284.8	4	4
19	240.0	241.0	7.72	325.0	284.8	4	4
20	240.0	242.0	7.20	332.7	284.8	4	4
21	240.0	244.0	9.26	340.3	284.8	4	4
22	240.0	243.0	7.72	348.0	284.8	4	4
23	240.0	239.0	6.17	355.7	284.3	4	4
24	210.0	210.0	4.63	363.4	283.7	4	4

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* METEOROLOGICAL DATA FOR DAY 16 *

HOUR	FLOW VECTOR (DEGREES)	RANDOM FLOW VECTOR (DEGREES)	WIND SPEED (MPS)	MIXING HEIGHT (METERS)	TEMP. (DEG. K)	INPUT STABILITY CATEGORY	ADJUSTED STABILITY CATEGORY
1	220.0	216.0	5.66	371.0	283.2	4	4
2	230.0	229.0	6.17	378.7	283.2	4	4
3	220.0	217.0	5.66	386.4	283.2	4	4
4	230.0	229.0	6.17	394.1	283.7	4	4
5	240.0	244.0	5.66	401.8	284.3	4	4
6	220.0	222.0	5.66	409.5	284.3	4	4
7	230.0	232.0	6.17	417.2	284.3	4	4
8	230.0	228.0	5.14	424.9	284.3	4	4
9	220.0	222.0	6.17	432.5	285.4	4	4
10	230.0	227.0	6.69	440.2	285.4	4	4
11	240.0	241.0	8.75	447.9	286.5	4	4
12	240.0	242.0	6.69	455.6	286.5	4	4
13	230.0	232.0	7.20	463.3	285.9	4	4
14	210.0	210.0	7.72	471.0	285.4	4	4
15	210.0	211.0	8.23	471.0	286.5	4	4
16	230.0	235.0	6.17	471.0	285.9	4	4
17	230.0	226.0	6.17	471.0	285.4	4	4
18	250.0	251.0	5.66	485.6	285.4	4	4
19	250.0	249.0	4.63	537.2	284.8	4	4
20	240.0	240.0	5.14	588.7	284.3	4	4
21	230.0	226.0	5.14	640.3	284.8	4	4
22	250.0	246.0	4.12	691.9	284.8	4	4
23	240.0	239.0	4.12	743.5	284.8	5	5
24	260.0	262.0	3.60	795.0	284.3	4	4

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* METEOROLOGICAL DATA FOR DAY 67 *

HOUR	FLOW VECTOR (DEGREES)	RANDOM FLOW VECTOR (DEGREES)	WIND SPEED (MPS)	MIXING HEIGHT (METERS)	TEMP. (DEG. K)	INPUT STABILITY CATEGORY	ADJUSTED STABILITY CATEGORY
1	210.0	212.0	2.57	1045.1	288.7	5	5
2	230.0	228.0	3.09	975.4	288.7	5	5
3	220.0	218.0	2.57	905.7	288.2	4	4
4	250.0	246.0	4.63	836.0	288.2	4	4
5	250.0	252.0	4.63	766.3	288.2	4	4
6	270.0	274.0	5.14	696.6	288.7	4	4
7	270.0	268.0	3.09	626.9	288.7	4	4
8	240.0	240.0	4.12	557.2	288.2	4	4
9	280.0	280.0	6.17	487.5	288.7	4	4
10	220.0	224.0	5.14	417.8	288.2	4	4
11	260.0	261.0	5.66	348.1	288.7	4	4
12	270.0	270.0	8.75	278.4	289.3	4	4
13	280.0	283.0	7.72	208.7	288.7	4	4
14	230.0	235.0	5.66	139.0	288.7	4	4
15	260.0	261.0	9.77	139.0	289.3	4	4
16	230.0	232.0	5.14	139.0	288.7	4	4
17	210.0	209.0	5.14	139.0	287.6	4	4
18	210.0	214.0	6.69	139.0	287.6	4	4
19	220.0	224.0	6.69	193.4	287.6	4	4
20	220.0	220.0	6.69	286.5	287.0	4	4
21	220.0	221.0	6.17	379.7	286.5	4	4
22	220.0	216.0	6.69	472.8	287.0	4	4
23	220.0	217.0	5.14	565.9	287.0	4	4
24	180.0	184.0	6.17	659.1	287.0	4	4

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* METEOROLOGICAL DATA FOR DAY 273 *

HOURL	FLOW VECTOR (DEGREES)	RANDOM FLOW VECTOR (DEGREES)	WIND SPEED (MPS)	MIXING HEIGHT (METERS)	TEMP. (DEG. K)	INPUT STABILITY CATEGORY	ADJUSTED STABILITY CATEGORY
1	180.0	182.0	4.12	1470.9	289.3	5	5
2	180.0	185.0	4.12	1476.5	289.3	5	5
3	180.0	183.0	4.12	1482.0	288.7	5	5
4	180.0	185.0	4.63	1487.5	288.7	5	5
5	180.0	179.0	4.12	1493.1	288.2	5	5
6	180.0	183.0	4.12	1498.6	288.2	5	5
7	180.0	176.0	4.63	130.2	288.2	4	4
8	180.0	176.0	5.14	332.1	290.4	4	4
9	180.0	185.0	5.14	533.9	293.2	4	4
10	210.0	206.0	4.63	735.7	295.9	3	3
11	250.0	251.0	5.14	937.5	298.7	3	3
12	260.0	256.0	4.63	1139.4	298.7	3	3
13	270.0	273.0	5.14	1341.2	299.8	3	3
14	230.0	226.0	4.12	1543.0	299.3	3	3
15	210.0	212.0	5.14	1543.0	299.3	3	3
16	220.0	220.0	6.17	1543.0	298.2	4	4
17	220.0	218.0	5.14	1543.0	297.6	4	4
18	220.0	224.0	5.14	1543.0	296.5	4	4
19	200.0	198.0	4.12	1549.9	294.8	5	5
20	220.0	217.0	4.12	1558.1	288.2	5	5
21	210.0	213.0	4.12	1566.3	292.6	5	5
22	220.0	220.0	1.54	1574.5	292.0	6	6
23	160.0	159.0	3.09	1582.7	290.4	6	6
24	140.0	143.0	1.54	1591.0	289.3	6	6

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* METEOROLOGICAL DATA FOR DAY 290 *

HOUR	FLOW VECTOR (DEGREES)	RANDOM FLOW VECTOR (DEGREES)	WIND SPEED (MPS)	MIXING HEIGHT (METERS)	TEMP. (DEG. K)	INPUT STABILITY CATEGORY	ADJUSTED STABILITY CATEGORY
1	240.0	239.0	6.69	1793.0	292.6	4	4
2	230.0	229.0	7.20	1745.8	292.0	4	4
3	230.0	228.0	6.17	1698.7	291.5	4	4
4	240.0	236.0	7.20	1651.5	291.5	4	4
5	240.0	239.0	6.69	1604.4	291.5	4	4
6	250.0	248.0	6.69	1557.2	292.0	4	4
7	250.0	250.0	4.63	1510.1	292.0	4	4
8	180.0	177.0	6.17	1462.9	287.6	4	4
9	150.0	154.0	6.17	1415.8	289.8	4	4
10	240.0	241.0	7.72	1368.6	294.3	4	4
11	250.0	250.0	8.75	1321.5	294.8	4	4
12	260.0	263.0	8.23	1274.3	293.7	4	4
13	240.0	242.0	8.75	1227.2	294.3	4	4
14	220.0	222.0	7.72	1180.0	293.7	4	4
15	230.0	227.0	7.72	1180.0	293.7	4	4
16	260.0	257.0	7.72	1180.0	293.2	4	4
17	240.0	244.0	6.69	1180.0	292.6	4	4
18	240.0	237.0	7.20	1185.9	291.5	4	4
19	230.0	232.0	5.66	1221.2	290.4	4	4
20	240.0	240.0	5.14	1256.4	290.4	4	4
21	230.0	228.0	5.14	1291.7	290.9	5	5
22	240.0	239.0	4.12	1326.9	291.5	4	4
23	260.0	257.0	4.12	1362.2	291.5	4	4
24	110.0	108.0	3.60	1397.4	285.9	5	5

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 827.82611 AND OCCURRED AT (437100.0, 352500.0) *

Y-AXIS / (METERS) /	X-AXIS (METERS)				
	435500.0	435600.0	435700.0	435800.0	435900.0
353400.0 /	310.42834 (273, 4)	341.81357 (273, 4)	373.53925 (273, 4)	403.97052 (273, 4)	430.69992 (273, 4)
353300.0 /	354.20074 (273, 4)	375.27744 (273, 4)	391.98682 (273, 4)	401.95490 (273, 4)	402.44727 (273, 4)
353200.0 /	344.63068 (273, 4)	347.64178 (273, 4)	343.07288 (273, 4)	329.38901 (273, 4)	305.56354 (273, 4)
353100.0 /	289.37860 (273, 4)	275.44928 (273, 4)	260.31979 (67, 7)	253.39841 (67, 7)	310.13293 (15, 7)
353000.0 /	273.03821 (273, 6)	262.36191 (273, 6)	331.85437 (15, 7)	400.47702 (15, 7)	441.71933 (15, 7)
352900.0 /	343.65216 (15, 7)	408.60349 (15, 7)	450.98083 (15, 7)	453.41858 (15, 7)	405.47711 (15, 7)
352800.0 /	450.43442 (15, 7)	459.73212 (15, 7)	426.72299 (15, 7)	352.30078 (15, 7)	288.97406 (290, 2)
352700.0 /	435.65414 (15, 7)	377.45493 (15, 7)	291.24063 (15, 7)	297.72321 (290, 2)	270.41782 (290, 2)
352600.0 /	319.39777 (15, 7)	302.40939 (290, 2)	293.31778 (290, 2)	252.97581 (290, 2)	257.77124 (16, 5)
352500.0 /	301.98981 (290, 2)	279.48495 (290, 2)	242.49307 (67, 6)	270.98700 (16, 3)	301.67035 (16, 3)
352400.0 /	259.81360 (290, 2)	257.19916 (67, 6)	289.98218 (16, 3)	316.56119 (16, 3)	322.41901 (16, 3)
352300.0 /	269.47266 (67, 6)	305.52148 (16, 3)	327.95605 (16, 3)	330.93402 (16, 3)	353.97766 (67, 7)
352200.0 /	317.80759 (16, 3)	336.28992 (16, 3)	336.83447 (16, 3)	361.86548 (67, 7)	446.37329 (67, 7)
352100.0 /	342.00745 (16, 3)	340.53363 (16, 3)	368.40961 (67, 7)	450.73645 (67, 7)	542.24304 (67, 7)
352000.0 /	342.40399 (16, 3)	373.72571 (67, 7)	453.41968 (67, 7)	541.59637 (67, 7)	611.22375 (67, 7)
351900.0 /	377.94199 (67, 7)	454.70419 (67, 7)	539.28992 (67, 7)	608.20093 (67, 7)	631.36688 (67, 7)
351800.0 /	454.79245 (67, 7)	535.69653 (67, 7)	603.30072 (67, 7)	631.18323 (67, 7)	599.25525 (67, 7)
351700.0 /	530.75073 (67, 7)	596.88544 (67, 7)	628.36829 (67, 7)	606.23596 (67, 7)	543.14642 (273, 6)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 827.82611 AND OCCURRED AT (437100.0, 352500.0) *

Y-AXIS / (METERS) /	X-AXIS (METERS)				
	436000.0	436100.0	436200.0	436300.0	436400.0
353400.0 /	450.41589 (273, 4)	458.91318 (273, 4)	451.42401 (273, 4)	423.52460 (273, 4)	372.86435 (273, 4)
353300.0 /	390.67343 (273, 4)	364.38007 (273, 4)	322.78870 (273, 4)	267.77670 (273, 4)	290.56607 (15, 7)
353200.0 /	271.57819 (273, 4)	275.76056 (15, 7)	345.43445 (15, 7)	375.64023 (15, 7)	336.55713 (15, 7)
353100.0 /	380.77783 (15, 7)	418.32578 (15, 7)	396.82880 (15, 7)	309.89795 (15, 7)	238.52855 (67, 7)
353000.0 /	434.11145 (15, 7)	367.79004 (15, 7)	257.26465 (15, 7)	239.15695 (290, 2)	240.51266 (16, 5)
352900.0 /	312.87280 (15, 7)	273.57471 (290, 2)	240.99216 (290, 2)	260.64661 (16, 5)	272.51627 (16, 5)
352800.0 /	278.91632 (290, 2)	239.06084 (67, 7)	274.52765 (16, 5)	278.63950 (16, 5)	293.92291 (67, 7)
352700.0 /	248.78070 (16, 5)	281.94592 (16, 5)	278.89847 (16, 5)	308.24005 (67, 7)	388.26953 (67, 7)
352600.0 /	283.59955 (16, 5)	295.79544 (16, 3)	321.67618 (67, 7)	405.71680 (67, 7)	502.09631 (67, 7)
352500.0 /	310.85052 (16, 3)	333.87534 (67, 7)	420.00598 (67, 7)	518.04639 (67, 7)	573.67700 (67, 7)
352400.0 /	344.65927 (67, 7)	431.34045 (67, 7)	529.33319 (67, 7)	591.15204 (67, 7)	564.23889 (67, 7)
352300.0 /	440.01868 (67, 7)	536.68311 (67, 7)	602.64728 (67, 7)	589.89258 (67, 7)	487.16431 (67, 7)
352200.0 /	540.78198 (67, 7)	609.20966 (67, 7)	608.44409 (67, 7)	521.84924 (67, 7)	428.40353 (273, 6)
352100.0 /	611.79248 (67, 7)	620.88086 (67, 7)	549.98236 (67, 7)	462.76620 (273, 6)	377.46454 (67, 8)
352000.0 /	628.20935 (67, 7)	571.85144 (67, 7)	491.25781 (273, 6)	396.18649 (67, 8)	339.48181 (67, 8)
351900.0 /	588.03894 (67, 7)	513.85669 (273, 6)	424.76263 (273, 6)	369.66940 (67, 8)	359.68158 (16, 5)
351800.0 /	530.95239 (273, 6)	453.35535 (273, 6)	392.40350 (67, 8)	331.14612 (16, 5)	388.70233 (16, 5)
351700.0 /	477.23349 (273, 6)	407.57382 (67, 8)	351.32477 (67, 8)	373.36484 (16, 5)	383.16632 (16, 5)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 827.82611 AND OCCURRED AT (437100.0, 352500.0) *

Y-AXIS / (METERS) /	X-AXIS (METERS)				
	436500.0	436600.0	436700.0	436800.0	436900.0
353400.0 /	301.66742 (273, 4)	240.63770 (67, 7)	239.91928 (67, 7)	242.71996 (2, 5)	235.80457 (67, 7)
353300.0 /	308.95914 (15, 7)	251.17393 (15, 7)	245.03838 (2, 5)	235.88666 (67, 7)	236.08946 (67, 7)
353200.0 /	238.89157 (67, 7)	237.57727 (67, 7)	236.86345 (67, 7)	242.81757 (67, 7)	267.99319 (67, 7)
353100.0 /	237.63824 (67, 7)	239.25035 (67, 7)	252.70721 (67, 7)	292.48547 (67, 7)	339.74182 (67, 7)
353000.0 /	259.27301 (16, 5)	265.22388 (67, 7)	318.61621 (67, 7)	381.83130 (67, 7)	373.00546 (67, 7)
352900.0 /	279.30713 (67, 7)	344.16296 (67, 7)	420.40479 (67, 7)	427.26889 (67, 7)	327.97699 (67, 7)
352800.0 /	367.64893 (67, 7)	453.60132 (67, 7)	475.90686 (67, 7)	384.44812 (67, 7)	321.37311 (273, 5)
352700.0 /	480.78989 (67, 7)	516.71777 (67, 7)	439.46210 (67, 7)	316.66577 (273, 6)	327.13931 (273, 5)
352600.0 /	549.16492 (67, 7)	488.89658 (67, 7)	364.83167 (273, 6)	317.41797 (273, 5)	412.40881 (2, 4)
352500.0 /	530.68298 (67, 7)	410.74786 (273, 6)	309.12894 (67, 8)	340.56284 (2, 4)	526.76825 (2, 4)
352400.0 /	451.42148 (273, 6)	345.83807 (273, 6)	318.85120 (16, 5)	434.29169 (2, 4)	632.12207 (2, 4)
352300.0 /	388.86957 (273, 6)	313.11761 (67, 8)	368.76694 (16, 5)	529.34875 (2, 4)	713.56848 (2, 4)
352200.0 /	349.57578 (67, 8)	358.44733 (16, 5)	438.61322 (2, 4)	613.28235 (2, 4)	763.85083 (2, 4)
352100.0 /	333.17505 (16, 5)	385.51096 (16, 5)	516.39020 (2, 4)	677.32117 (2, 4)	782.82214 (2, 4)
352000.0 /	380.42194 (16, 5)	431.99304 (2, 4)	583.57239 (2, 4)	717.50378 (2, 4)	775.02069 (2, 4)
351900.0 /	388.75949 (16, 5)	495.69861 (2, 4)	634.85303 (2, 4)	734.07410 (2, 4)	747.07471 (2, 4)
351800.0 /	419.30511 (2, 4)	550.18774 (2, 4)	667.92932 (2, 4)	730.08533 (2, 4)	705.78418 (2, 4)
351700.0 /	471.94638 (2, 4)	592.12079 (2, 4)	683.05920 (2, 4)	709.95740 (2, 4)	657.03864 (2, 4)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 827.82611 AND OCCURRED AT (437100.0, 352500.0) *

Y-AXIS (METERS) /	X-AXIS (METERS)				
	437000.0	437100.0	437200.0	437300.0	437400.0
353400.0 /	232.74139 (67, 7)	231.37213 (67, 7)	226.98145 (67, 7)	213.17027 (67, 7)	225.59593 (2, 4)
353300.0 /	244.91373 (67, 7)	250.67786 (67, 7)	225.47910 (67, 7)	233.81163 (2, 4)	282.92889 (2, 4)
353200.0 /	294.70554 (67, 7)	261.28336 (67, 7)	229.96036 (2, 4)	327.30411 (2, 4)	363.01218 (2, 4)
353100.0 /	317.70697 (67, 7)	271.87817 (273, 5)	326.84503 (2, 4)	462.02563 (2, 4)	422.29333 (2, 4)
353000.0 /	292.27350 (273, 5)	304.61795 (273, 5)	475.28375 (2, 4)	578.89423 (2, 4)	441.88681 (2, 4)
352900.0 /	323.25937 (273, 5)	429.57544 (2, 4)	626.42944 (2, 4)	639.24487 (2, 4)	429.23288 (2, 4)
352800.0 /	366.62286 (2, 4)	580.84546 (2, 4)	733.29956 (2, 4)	641.87061 (2, 4)	399.33112 (2, 4)
352700.0 /	497.31589 (2, 4)	712.01563 (2, 4)	777.95557 (2, 4)	605.21277 (2, 4)	363.98572 (2, 4)
352600.0 /	627.50220 (2, 4)	796.45087 (2, 4)	767.85736 (2, 4)	549.49414 (2, 4)	329.81238 (2, 4)
352500.0 /	731.89252 (2, 4)	827.82611 (2, 4)	721.22961 (2, 4)	489.18674 (2, 4)	299.59454 (2, 4)
352400.0 /	796.61029 (2, 4)	814.31702 (2, 4)	656.10016 (2, 4)	432.37958 (2, 4)	273.96951 (2, 4)
352300.0 /	819.96283 (2, 4)	769.94775 (2, 4)	585.73151 (2, 4)	382.55893 (2, 4)	252.59268 (2, 4)
352200.0 /	808.39130 (2, 4)	708.46527 (2, 4)	518.16364 (2, 4)	340.52106 (2, 4)	234.78082 (2, 4)
352100.0 /	771.71844 (2, 4)	640.54919 (2, 4)	457.39490 (2, 4)	305.73801 (2, 4)	227.80627 (67, 8)
352000.0 /	719.74847 (2, 4)	573.29431 (2, 4)	404.81049 (2, 4)	277.16876 (2, 4)	238.34691 (67, 8)
351900.0 /	660.53955 (2, 4)	510.77112 (2, 4)	360.32275 (2, 4)	253.68045 (2, 4)	247.84955 (67, 8)
351800.0 /	599.90564 (2, 4)	454.88193 (2, 4)	323.13495 (2, 4)	234.23978 (2, 4)	256.02844 (67, 8)
351700.0 /	541.59253 (2, 4)	406.14587 (2, 4)	292.19455 (2, 4)	221.51898 (273, 7)	262.70349 (67, 8)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 565.04376 AND OCCURRED AT (435800.0, 351700.0) *

Y-AXIS / (METERS) /	435500.0	435600.0	X-AXIS (METERS) 435700.0	435800.0	435900.0
353400.0 /	302.20068 (67, 7)	295.41824 (273, 6)	287.65469 (273, 6)	277.16220 (273, 6)	264.85815 (273, 6)
353300.0 /	295.15302 (273, 6)	288.40784 (273, 6)	278.87054 (273, 6)	267.35010 (273, 6)	256.38116 (67, 7)
353200.0 /	288.85776 (273, 6)	280.25879 (273, 6)	269.53992 (273, 6)	258.37375 (67, 7)	251.72601 (67, 7)
353100.0 /	281.34232 (273, 6)	271.43323 (273, 6)	260.10950 (273, 6)	248.28380 (273, 6)	248.10754 (67, 7)
353000.0 /	270.55157 (67, 7)	262.20447 (67, 7)	255.07071 (67, 7)	263.07932 (16, 4)	307.70825 (16, 4)
352900.0 /	264.35690 (273, 6)	275.26123 (16, 4)	318.85779 (16, 4)	340.09454 (16, 4)	324.91934 (16, 4)
352800.0 /	323.63846 (16, 4)	347.19052 (16, 4)	340.96576 (16, 4)	299.62033 (16, 4)	251.61333 (15, 7)
352700.0 /	348.63104 (16, 4)	318.75446 (16, 4)	291.07233 (290, 2)	241.61693 (67, 7)	239.91216 (67, 7)
352600.0 /	284.76965 (290, 2)	245.26727 (67, 7)	242.22406 (67, 7)	240.60338 (67, 7)	252.70200 (67, 6)
352500.0 /	246.18481 (67, 7)	243.00421 (67, 7)	241.60718 (67, 7)	266.21109 (67, 6)	280.56836 (16, 5)
352400.0 /	243.97278 (67, 7)	250.63885 (16, 3)	276.66364 (67, 6)	274.54889 (67, 6)	312.80716 (290, 1)
352300.0 /	269.35718 (16, 3)	284.06964 (67, 6)	279.70215 (290, 1)	321.84808 (290, 1)	320.89343 (290, 1)
352200.0 /	288.64670 (67, 6)	291.22217 (290, 1)	327.11896 (290, 1)	322.40479 (16, 3)	363.49521 (273, 6)
352100.0 /	299.60236 (290, 1)	329.26617 (290, 1)	326.08221 (16, 3)	370.09302 (273, 6)	438.87891 (273, 6)
352000.0 /	328.88232 (290, 1)	328.06134 (16, 3)	375.30615 (273, 6)	441.91107 (273, 6)	505.48926 (273, 6)
351900.0 /	328.63226 (16, 3)	379.31235 (273, 6)	443.44418 (273, 6)	505.40720 (273, 6)	549.75507 (273, 6)
351800.0 /	382.22620 (273, 6)	443.75354 (273, 6)	503.74606 (273, 6)	549.02509 (273, 6)	562.90692 (273, 6)
351700.0 /	442.68768 (273, 6)	500.75586 (273, 6)	546.34692 (273, 6)	<u>565.04376 (273, 6)</u>	528.78479 (67, 7)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 565.04376 AND OCCURRED AT (435800.0, 351700.0) *

Y-AXIS (METERS) /	X-AXIS (METERS)				
	436000.0	436100.0	436200.0	436300.0	436400.0
353400.0 /	254.35905 (67, 7)	248.45093 (67, 7)	244.52496 (67, 7)	242.29782 (67, 7)	241.28940 (67, 7)
353300.0 /	250.07079 (67, 7)	245.64043 (67, 7)	242.89233 (67, 7)	241.41937 (67, 7)	240.69870 (67, 7)
353200.0 /	246.84009 (67, 7)	243.59843 (67, 7)	241.66663 (67, 7)	256.04614 (290, 5)	254.31470 (16, 4)
353100.0 /	250.55573 (290, 5)	287.56857 (16, 4)	297.05630 (16, 4)	255.83525 (15, 8)	218.35010 (290, 2)
353000.0 /	324.49698 (16, 4)	297.39447 (16, 4)	250.23705 (290, 2)	238.36578 (67, 7)	238.31067 (67, 7)
352900.0 /	269.88373 (16, 4)	239.33702 (67, 7)	238.50931 (67, 7)	239.77466 (67, 7)	248.88530 (67, 7)
352800.0 /	239.50455 (67, 7)	235.11455 (16, 5)	242.10513 (67, 7)	255.75139 (67, 7)	282.41016 (273, 5)
352700.0 /	240.09294 (67, 7)	260.13739 (16, 3)	276.88513 (16, 3)	283.95709 (290, 1)	315.25674 (273, 5)
352600.0 /	282.92215 (16, 3)	280.86301 (290, 1)	300.55396 (290, 1)	320.08640 (273, 6)	389.37549 (273, 6)
352500.0 /	299.33978 (290, 1)	311.63104 (290, 1)	333.71454 (273, 6)	405.04395 (273, 6)	465.07068 (273, 6)
352400.0 /	318.11731 (290, 1)	345.44867 (273, 6)	417.48608 (273, 6)	480.55304 (273, 6)	501.41754 (273, 6)
352300.0 /	355.33478 (273, 6)	427.02612 (273, 6)	491.70038 (273, 6)	520.63501 (273, 6)	485.44312 (273, 6)
352200.0 /	434.03354 (273, 6)	499.16513 (273, 6)	534.22473 (273, 6)	512.52191 (273, 6)	385.91428 (67, 7)
352100.0 /	503.57306 (273, 6)	543.06104 (273, 6)	533.03900 (273, 6)	423.14487 (67, 7)	364.68222 (16, 1)
352000.0 /	547.98535 (273, 6)	547.71344 (273, 6)	456.52499 (67, 7)	391.85144 (273, 6)	329.43182 (16, 1)
351900.0 /	557.38879 (273, 6)	485.34662 (67, 7)	406.39032 (67, 8)	361.04871 (16, 1)	316.61353 (67, 6)
351800.0 /	509.39362 (67, 7)	409.36545 (67, 8)	385.75885 (16, 1)	322.09851 (67, 6)	313.61597 (67, 6)
351700.0 /	417.66266 (67, 7)	403.18713 (16, 1)	346.87494 (16, 1)	327.67456 (67, 6)	355.60242 (2, 4)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 565.04376 AND OCCURRED AT (435800.0, 351700.0) *

Y-AXIS (METERS) /	X-AXIS (METERS)				
	436500.0	436600.0	436700.0	436800.0	436900.0
353400.0 /	240.92674 (67, 7)	219.08043 (273, 4)	226.16087 (2, 5)	238.37836 (67, 7)	227.04681 (2, 5)
353300.0 /	240.18234 (67, 7)	239.37122 (67, 7)	237.89275 (67, 7)	227.23875 (2, 5)	203.97740 (273, 6)
353200.0 /	230.98962 (15, 7)	227.17099 (2, 5)	211.00267 (16, 5)	207.11734 (273, 6)	242.49561 (273, 5)
353100.0 /	215.89117 (16, 5)	238.38249 (16, 5)	239.51974 (273, 5)	281.77374 (273, 5)	278.05176 (273, 5)
353000.0 /	243.28366 (67, 7)	263.14178 (273, 5)	305.82715 (273, 5)	306.10278 (273, 5)	312.19257 (273, 6)
352900.0 /	276.75381 (273, 5)	317.24368 (273, 5)	322.24759 (273, 6)	351.42148 (273, 6)	311.08942 (273, 6)
352800.0 /	319.39368 (273, 5)	347.76300 (273, 6)	387.54236 (273, 6)	358.75449 (273, 6)	271.00415 (273, 6)
352700.0 /	370.27463 (273, 6)	418.82306 (273, 6)	403.77606 (273, 6)	309.74078 (273, 5)	308.26782 (2, 4)
352600.0 /	444.64240 (273, 6)	443.19333 (273, 6)	350.82373 (67, 7)	267.47015 (67, 8)	321.13806 (16, 5)
352500.0 /	475.77573 (273, 6)	399.96924 (67, 7)	302.17239 (273, 6)	333.16968 (16, 5)	302.36264 (16, 5)
352400.0 /	446.17319 (67, 7)	342.31854 (67, 8)	296.99658 (273, 5)	352.90131 (16, 5)	282.15680 (273, 4)
352300.0 /	365.23969 (67, 8)	297.48599 (16, 1)	358.18799 (2, 4)	317.04135 (16, 5)	279.92664 (273, 4)
352200.0 /	334.81784 (16, 1)	298.58792 (2, 4)	366.29266 (16, 5)	264.91919 (273, 4)	290.57263 (15, 5)
352100.0 /	303.07822 (67, 8)	364.20880 (2, 4)	320.26172 (16, 5)	279.11804 (15, 5)	287.75220 (15, 5)
352000.0 /	305.34088 (2, 4)	367.15878 (16, 5)	253.80759 (16, 5)	293.92352 (15, 5)	270.22095 (15, 5)
351900.0 /	362.34067 (2, 4)	316.17322 (16, 5)	278.35925 (15, 5)	292.92291 (15, 5)	244.10393 (15, 5)
351800.0 /	360.17474 (16, 5)	251.84447 (16, 5)	292.33334 (15, 5)	278.38272 (15, 5)	215.14214 (15, 5)
351700.0 /	307.73270 (16, 5)	274.35779 (15, 5)	292.74911 (15, 5)	254.95007 (15, 5)	187.26077 (15, 5)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 565.04376 AND OCCURRED AT (435800.0, 351700.0) *

Y-AXIS (METERS) /	X-AXIS (METERS)				
	437000.0	437100.0	437200.0	437300.0	437400.0
353400.0 /	202.94717 (273, 6)	204.14404 (273, 6)	204.95946 (273, 6)	201.57005 (273, 6)	202.53307 (67, 7)
353300.0 /	209.35631 (273, 6)	215.80614 (273, 6)	209.15833 (273, 6)	204.03935 (67, 7)	195.13400 (273, 6)
353200.0 /	239.63174 (273, 6)	233.48257 (273, 6)	228.84393 (273, 5)	195.27519 (273, 6)	191.26462 (273, 6)
353100.0 /	273.10754 (273, 6)	235.76732 (67, 7)	252.53470 (273, 5)	194.29478 (273, 4)	186.80832 (273, 6)
353000.0 /	276.31412 (67, 7)	298.25568 (2, 4)	237.90454 (273, 4)	203.66386 (15, 5)	181.79935 (273, 6)
352900.0 /	262.79718 (2, 4)	288.84790 (273, 5)	264.37335 (273, 4)	196.99109 (15, 5)	176.28062 (273, 6)
352800.0 /	321.23462 (273, 5)	281.17181 (273, 4)	254.22124 (273, 4)	181.59074 (15, 5)	170.30174 (273, 6)
352700.0 /	285.16644 (273, 5)	292.93542 (273, 4)	227.15933 (15, 5)	171.20557 (273, 6)	167.64996 (67, 8)
352600.0 /	290.99927 (273, 4)	275.94211 (273, 4)	207.02698 (15, 5)	165.00470 (273, 6)	175.24039 (67, 8)
352500.0 /	293.51984 (273, 4)	255.09125 (15, 5)	184.09764 (15, 5)	166.96812 (67, 8)	184.15549 (67, 8)
352400.0 /	280.48517 (15, 5)	233.64075 (15, 5)	165.71191 (16, 1)	171.13309 (67, 8)	194.28427 (67, 8)
352300.0 /	275.54443 (15, 5)	206.74358 (15, 5)	168.62476 (16, 1)	175.55453 (67, 8)	205.27054 (67, 8)
352200.0 /	255.39604 (15, 5)	180.67639 (15, 5)	170.76950 (16, 1)	180.40186 (67, 8)	216.62018 (67, 8)
352100.0 /	227.76443 (15, 5)	169.91768 (16, 1)	173.36755 (273, 7)	188.04753 (273, 7)	219.81766 (2, 4)
352000.0 /	199.02100 (15, 5)	173.31035 (273, 7)	181.41296 (273, 7)	196.91698 (273, 7)	217.33594 (273, 7)
351900.0 /	172.82597 (15, 5)	181.56987 (273, 7)	189.09225 (273, 7)	205.51158 (273, 7)	225.48953 (273, 7)
351800.0 /	182.71701 (273, 7)	188.51901 (273, 7)	196.58344 (273, 7)	213.74164 (273, 7)	232.91739 (273, 7)
351700.0 /	192.04124 (273, 7)	194.66551 (273, 7)	203.98027 (273, 7)	217.97873 (2, 4)	239.52530 (273, 7)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* 50 MAXIMUM 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *

* FROM ALL SOURCES *

RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y(METERS) OR DIRECTION (DEGREES)	RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y(METERS) OR DIRECTION (DEGREES)
1	827.82611	4	2	437100.0	352500.0	26	705.78418	4	2	436900.0	351800.0
2	819.96283	4	2	437000.0	352300.0	27	683.05920	4	2	436700.0	351700.0
3	814.31702	4	2	437100.0	352400.0	28	677.32117	4	2	436800.0	352100.0
4	808.39130	4	2	437000.0	352200.0	29	667.92932	4	2	436700.0	351800.0
5	796.61029	4	2	437000.0	352400.0	30	660.53955	4	2	437000.0	351900.0
6	796.45087	4	2	437100.0	352600.0	31	657.03864	4	2	436900.0	351700.0
7	782.82214	4	2	436900.0	352100.0	32	656.10016	4	2	437200.0	352400.0
8	777.95557	4	2	437200.0	352700.0	33	641.87061	4	2	437300.0	352800.0
9	775.02069	4	2	436900.0	352000.0	34	640.54919	4	2	437100.0	352100.0
10	771.71844	4	2	437000.0	352100.0	35	639.24487	4	2	437300.0	352900.0
11	769.94775	4	2	437100.0	352300.0	36	634.85303	4	2	436700.0	351900.0
12	767.85736	4	2	437200.0	352600.0	37	632.12207	4	2	436900.0	352400.0
13	763.85083	4	2	436900.0	352200.0	38	631.36688	7	67	435900.0	351900.0
14	747.07471	4	2	436900.0	351900.0	39	631.18323	7	67	435800.0	351800.0
15	734.07410	4	2	436800.0	351900.0	40	628.36829	7	67	435700.0	351700.0
16	733.29956	4	2	437200.0	352800.0	41	628.20935	7	67	436000.0	352000.0
17	731.89252	4	2	437000.0	352500.0	42	627.50220	4	2	437000.0	352600.0
18	730.08533	4	2	436800.0	351800.0	43	626.42944	4	2	437200.0	352900.0
19	721.22961	4	2	437200.0	352500.0	44	620.88086	7	67	436100.0	352100.0
20	719.74847	4	2	437000.0	352000.0	45	613.28235	4	2	436800.0	352200.0
21	717.50378	4	2	436800.0	352000.0	46	611.79248	7	67	436000.0	352100.0
22	713.56848	4	2	436900.0	352300.0	47	611.22375	7	67	435900.0	352000.0
23	712.01563	4	2	437100.0	352700.0	48	609.20966	7	67	436100.0	352200.0
24	709.95740	4	2	436800.0	351700.0	49	608.44409	7	67	436200.0	352200.0
25	708.46527	4	2	437100.0	352200.0	50	608.20093	7	67	435800.0	351900.0

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 197.74132 AND OCCURRED AT (435600.0, 352800.0) *

Y-AXIS / (METERS) /	X-AXIS (METERS)				
	435500.0	435600.0	435700.0	435800.0	435900.0
353400.0 /	117.05527 (67, 1)	114.95039 (67, 1)	112.62731 (67, 1)	116.12479 (273, 1)	119.48427 (273, 1)
353300.0 /	109.81103 (67, 1)	111.44112 (273, 1)	113.78702 (273, 1)	115.05396 (273, 1)	114.94808 (273, 1)
353200.0 /	109.23092 (67, 1)	109.86102 (16, 1)	110.60789 (16, 1)	111.00009 (16, 1)	111.30911 (16, 1)
353100.0 /	119.50012 (16, 1)	120.29193 (16, 1)	121.17979 (16, 1)	124.62941 (15, 1)	143.28046 (15, 1)
353000.0 /	129.49033 (16, 1)	136.58069 (15, 1)	155.05397 (15, 1)	172.55882 (15, 1)	183.14224 (15, 1)
352900.0 /	163.47391 (15, 1)	180.28764 (15, 1)	191.27898 (15, 1)	191.06427 (15, 1)	176.04161 (15, 1)
352800.0 /	196.01215 (15, 1)	<u>197.74132 (15, 1)</u>	186.87840 (15, 1)	163.21869 (15, 1)	149.53113 (290, 1)
352700.0 /	193.72751 (15, 1)	174.72295 (15, 1)	159.44812 (290, 1)	145.71002 (290, 1)	130.95262 (16, 1)
352600.0 /	164.95146 (290, 1)	155.74408 (290, 1)	139.34363 (290, 1)	135.73889 (16, 1)	144.34213 (16, 1)
352500.0 /	149.27507 (290, 1)	135.70325 (16, 1)	140.77760 (16, 1)	151.47154 (16, 1)	164.70485 (16, 1)
352400.0 /	138.33586 (16, 1)	145.74519 (16, 1)	157.76723 (16, 1)	171.14520 (16, 1)	180.99106 (16, 1)
352300.0 /	150.39548 (16, 1)	163.12408 (16, 1)	176.22412 (16, 1)	185.28203 (16, 1)	185.83383 (16, 1)
352200.0 /	167.52132 (16, 1)	180.05704 (16, 1)	188.23529 (16, 1)	188.25845 (16, 1)	178.24438 (16, 1)
352100.0 /	182.78174 (16, 1)	190.04825 (16, 1)	189.57849 (16, 1)	179.91302 (16, 1)	162.62610 (16, 1)
352000.0 /	190.90430 (16, 1)	189.98601 (16, 1)	180.67058 (16, 1)	164.41953 (16, 1)	154.69272 (67, 1)
351900.0 /	189.64899 (16, 1)	180.67876 (16, 1)	165.40945 (16, 1)	155.88040 (67, 1)	160.50943 (67, 1)
351800.0 /	180.03917 (16, 1)	165.72919 (16, 1)	156.61221 (67, 1)	161.52567 (67, 1)	162.34854 (67, 1)
351700.0 /	165.32776 (16, 1)	156.93187 (67, 1)	162.07069 (67, 1)	163.55801 (67, 1)	160.92703 (67, 1)

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 PERMITTING
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*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 197.74132 AND OCCURRED AT (435600.0, 352800.0) *

Y-AXIS / (METERS) /	436000.0	436100.0	X-AXIS (METERS) 436200.0	436300.0	436400.0
353400.0 /	121.79265 (273, 1)	122.58276 (273, 1)	121.27550 (273, 1)	117.26875 (273, 1)	110.19165 (273, 1)
353300.0 /	113.18270 (273, 1)	109.51503 (273, 1)	103.82947 (273, 1)	108.43126 (15, 1)	123.73190 (15, 1)
353200.0 /	112.06386 (16, 1)	127.75436 (15, 1)	144.97096 (15, 1)	152.38254 (15, 1)	141.04086 (15, 1)
353100.0 /	161.05952 (15, 1)	170.56404 (15, 1)	163.88376 (15, 1)	138.33716 (15, 1)	109.92229 (290, 1)
353000.0 /	180.19388 (15, 1)	160.15610 (15, 1)	132.95114 (290, 1)	113.93105 (16, 1)	114.02068 (16, 1)
352900.0 /	148.90280 (290, 1)	134.02594 (290, 1)	120.86839 (16, 1)	125.64870 (16, 1)	133.79384 (16, 1)
352800.0 /	130.87794 (290, 1)	128.60864 (16, 1)	137.04034 (16, 1)	146.87593 (16, 1)	149.54211 (16, 1)
352700.0 /	136.60245 (16, 1)	147.56131 (16, 1)	158.19186 (16, 1)	160.69330 (16, 1)	149.42131 (16, 1)
352600.0 /	156.83655 (16, 1)	167.60750 (16, 1)	169.73611 (16, 1)	158.58344 (16, 1)	136.16617 (16, 1)
352500.0 /	175.16132 (16, 1)	176.80125 (16, 1)	165.86008 (16, 1)	144.30936 (16, 1)	138.60510 (67, 1)
352400.0 /	182.09094 (16, 1)	171.42419 (16, 1)	150.88484 (16, 1)	143.56873 (67, 1)	144.58594 (67, 1)
352300.0 /	175.48190 (16, 1)	156.02234 (16, 1)	147.52583 (67, 1)	149.66473 (67, 1)	144.82436 (67, 1)
352200.0 /	159.88068 (16, 1)	150.61761 (67, 1)	153.64537 (67, 1)	150.31813 (67, 1)	140.65706 (67, 1)
352100.0 /	152.96982 (67, 1)	156.68628 (67, 1)	154.66446 (67, 1)	146.80559 (67, 1)	133.14850 (67, 1)
352000.0 /	158.93216 (67, 1)	158.02283 (67, 1)	151.75061 (67, 1)	140.11838 (67, 1)	123.58769 (67, 1)
351900.0 /	160.54079 (67, 1)	155.65414 (67, 1)	145.84381 (67, 1)	131.29283 (67, 1)	113.37212 (67, 1)
351800.0 /	158.66811 (67, 1)	150.46762 (67, 1)	137.81079 (67, 1)	121.49782 (67, 1)	103.48589 (67, 1)
351700.0 /	154.13889 (67, 1)	143.21629 (67, 1)	128.62155 (67, 1)	111.66928 (67, 1)	95.30103 (273, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 197.74132 AND OCCURRED AT (435600.0, 352800.0) *

Y-AXIS / (METERS) /	X-AXIS (METERS)				
	436500.0	436600.0	436700.0	436800.0	436900.0
353400.0 /	100.30080 (273, 1)	97.90762 (15, 1)	97.91460 (15, 1)	81.64429 (67, 1)	77.14681 (67, 1)
353300.0 /	127.84579 (15, 1)	111.76778 (15, 1)	86.26769 (67, 1)	82.19629 (67, 1)	76.56445 (67, 1)
353200.0 /	110.76680 (15, 1)	93.50873 (16, 1)	89.89983 (16, 1)	88.37672 (16, 1)	87.49496 (273, 1)
353100.0 /	103.02507 (16, 1)	104.32012 (16, 1)	104.86004 (16, 1)	94.83099 (16, 1)	98.10275 (273, 1)
353000.0 /	119.34962 (16, 1)	121.19443 (16, 1)	110.50985 (16, 1)	104.01369 (273, 1)	105.77354 (273, 1)
352900.0 /	136.29257 (16, 1)	125.20995 (16, 1)	108.05090 (273, 1)	111.23217 (273, 1)	110.86272 (273, 1)
352800.0 /	138.27913 (16, 1)	115.02902 (16, 1)	116.52257 (67, 1)	114.67398 (273, 1)	114.49767 (273, 1)
352700.0 /	126.38952 (16, 1)	125.16116 (67, 1)	121.34304 (67, 1)	115.52713 (273, 1)	117.47805 (273, 1)
352600.0 /	132.50650 (67, 1)	130.52573 (67, 1)	120.01509 (67, 1)	115.80501 (273, 1)	118.79880 (273, 1)
352500.0 /	138.25079 (67, 1)	129.77261 (67, 1)	114.95742 (273, 1)	115.92180 (273, 1)	117.31833 (273, 1)
352400.0 /	138.02048 (67, 1)	124.15160 (67, 1)	113.30449 (273, 1)	114.91051 (273, 1)	113.08590 (273, 1)
352300.0 /	133.14722 (67, 1)	115.13940 (67, 1)	111.74010 (273, 1)	112.10836 (273, 1)	112.51160 (2, 1)
352200.0 /	124.83086 (67, 1)	109.01641 (273, 1)	109.45346 (273, 1)	107.65073 (273, 1)	119.98186 (2, 1)
352100.0 /	114.70848 (67, 1)	106.45086 (273, 1)	106.08746 (273, 1)	109.20860 (2, 1)	122.80231 (2, 1)
352000.0 /	104.38873 (67, 1)	103.49834 (273, 1)	101.77832 (273, 1)	115.58757 (2, 1)	121.50533 (2, 1)
351900.0 /	100.82109 (273, 1)	99.98690 (273, 1)	104.99519 (2, 1)	118.23326 (2, 1)	117.08159 (2, 1)
351800.0 /	97.60721 (273, 1)	95.98946 (273, 1)	110.59036 (2, 1)	117.48754 (2, 1)	110.61662 (2, 1)
351700.0 /	94.16235 (273, 1)	100.55405 (2, 1)	113.15420 (2, 1)	114.04671 (2, 1)	103.06039 (2, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 197.74132 AND OCCURRED AT (435600.0, 352800.0) *

Y-AXIS / (METERS) /	X-AXIS (METERS)				
	437000.0	437100.0	437200.0	437300.0	437400.0
353400.0 /	72.17838 (67, 1)	72.92790 (273, 1)	72.15631 (273, 1)	72.75331 (273, 1)	71.46284 (273, 1)
353300.0 /	80.22705 (273, 1)	80.52515 (273, 1)	80.70454 (273, 1)	83.72157 (273, 1)	75.15431 (273, 1)
353200.0 /	90.06332 (273, 1)	89.68266 (273, 1)	94.06084 (273, 1)	92.26845 (273, 1)	75.56146 (273, 1)
353100.0 /	98.71478 (273, 1)	101.24423 (273, 1)	105.60372 (273, 1)	93.90176 (273, 1)	73.67426 (273, 1)
353000.0 /	106.48213 (273, 1)	111.78072 (273, 1)	109.84994 (273, 1)	92.44814 (2, 1)	74.76180 (2, 1)
352900.0 /	113.70007 (273, 1)	117.62011 (273, 1)	106.94118 (273, 1)	99.86819 (2, 1)	72.71982 (2, 1)
352800.0 /	118.93468 (273, 1)	117.09047 (273, 1)	112.26134 (2, 1)	99.85259 (2, 1)	68.42569 (2, 1)
352700.0 /	120.14000 (273, 1)	111.57518 (273, 1)	117.82999 (2, 1)	94.77142 (2, 1)	66.61567 (273, 1)
352600.0 /	116.96786 (273, 1)	121.19019 (2, 1)	116.20297 (2, 1)	87.20840 (2, 1)	66.42887 (273, 1)
352500.0 /	113.56053 (2, 1)	125.25268 (2, 1)	109.76235 (2, 1)	79.01003 (2, 1)	66.81689 (273, 1)
352400.0 /	122.59155 (2, 1)	123.18133 (2, 1)	100.88046 (2, 1)	71.21057 (2, 1)	67.71304 (273, 1)
352300.0 /	125.81139 (2, 1)	116.87744 (2, 1)	91.29342 (2, 1)	66.42330 (273, 1)	69.05848 (273, 1)
352200.0 /	123.99487 (2, 1)	108.24174 (2, 1)	82.04390 (2, 1)	66.24581 (273, 1)	70.80352 (273, 1)
352100.0 /	118.53645 (2, 1)	98.74348 (2, 1)	73.64617 (2, 1)	66.55571 (273, 1)	72.90566 (273, 1)
352000.0 /	110.88467 (2, 1)	89.34136 (2, 1)	66.27956 (2, 1)	67.29543 (273, 1)	75.32582 (273, 1)
351900.0 /	102.23042 (2, 1)	80.57121 (2, 1)	65.48566 (273, 1)	68.41823 (273, 1)	78.00957 (273, 1)
351800.0 /	93.41433 (2, 1)	72.67474 (2, 1)	65.27324 (273, 1)	69.86853 (273, 1)	80.81065 (273, 1)
351700.0 /	84.95782 (2, 1)	65.71284 (2, 1)	65.42947 (273, 1)	71.61691 (273, 1)	83.73696 (273, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 164.03651 AND OCCURRED AT (435600.0, 352700.0) *

Y-AXIS (METERS) /	X-AXIS (METERS)				
	435500.0	435600.0	435700.0	435800.0	435900.0
353400.0 /	102.81295 (273, 1)	107.58965 (273, 1)	112.07338 (273, 1)	110.27425 (67, 1)	108.07202 (67, 1)
353300.0 /	108.27299 (273, 1)	109.07361 (67, 1)	108.30904 (67, 1)	107.50627 (67, 1)	106.63583 (67, 1)
353200.0 /	108.78299 (16, 1)	109.14825 (67, 1)	108.76579 (67, 1)	108.10559 (67, 1)	107.19008 (67, 1)
353100.0 /	110.35359 (67, 1)	110.01033 (67, 1)	109.39688 (15, 1)	122.57458 (16, 1)	124.69964 (16, 1)
353000.0 /	120.76653 (15, 1)	131.30916 (16, 1)	133.70959 (16, 1)	136.19353 (16, 1)	137.42874 (16, 1)
352900.0 /	140.76926 (16, 1)	143.26434 (16, 1)	144.68413 (16, 1)	146.22028 (290, 1)	152.26414 (290, 1)
352800.0 /	150.06128 (16, 1)	149.81329 (290, 1)	157.92810 (290, 1)	158.78499 (290, 1)	131.45752 (16, 1)
352700.0 /	160.25720 (290, 1)	<u>164.03651 (290, 1)</u>	146.61850 (15, 1)	132.19589 (16, 1)	125.60299 (290, 1)
352600.0 /	158.66461 (15, 1)	137.21103 (16, 1)	133.59967 (16, 1)	124.13875 (67, 1)	123.28993 (67, 1)
352500.0 /	136.60968 (16, 1)	131.91519 (290, 1)	126.72641 (67, 1)	125.46867 (67, 1)	121.83722 (67, 1)
352400.0 /	127.79916 (67, 1)	128.59387 (67, 1)	127.03732 (67, 1)	123.70904 (67, 1)	120.81203 (67, 1)
352300.0 /	129.85077 (67, 1)	128.13470 (67, 1)	125.25516 (67, 1)	123.30163 (67, 1)	124.72528 (67, 1)
352200.0 /	128.87991 (67, 1)	126.54013 (67, 1)	125.48041 (67, 1)	127.64670 (67, 1)	133.88060 (67, 1)
352100.0 /	127.60896 (67, 1)	127.35934 (67, 1)	130.12425 (67, 1)	136.45544 (67, 1)	145.10904 (67, 1)
352000.0 /	128.95078 (67, 1)	132.18143 (67, 1)	138.52715 (67, 1)	146.90640 (67, 1)	144.99031 (16, 1)
351900.0 /	133.84650 (67, 1)	140.14273 (67, 1)	148.22597 (67, 1)	147.11365 (16, 1)	129.61491 (16, 1)
351800.0 /	141.33549 (67, 1)	149.12610 (67, 1)	148.52399 (16, 1)	131.81833 (16, 1)	118.27213 (273, 1)
351700.0 /	149.56635 (67, 1)	149.29819 (16, 1)	133.42616 (16, 1)	120.11193 (16, 1)	117.04791 (273, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 164.03651 AND OCCURRED AT (435600.0, 352700.0) *

Y-AXIS / (METERS) /	436000.0	436100.0	X-AXIS (METERS) 436200.0	436300.0	436400.0
353400.0 /	106.13017 (67, 1)	104.42416 (67, 1)	102.76864 (67, 1)	100.85323 (67, 1)	98.33553 (67, 1)
353300.0 /	105.63754 (67, 1)	104.39764 (67, 1)	102.72768 (67, 1)	100.89084 (16, 1)	102.16225 (16, 1)
353200.0 /	109.73958 (15, 1)	113.67763 (16, 1)	115.67429 (16, 1)	116.00108 (16, 1)	111.79403 (16, 1)
353100.0 /	127.04688 (16, 1)	127.94670 (16, 1)	127.40173 (290, 1)	125.31041 (290, 1)	108.06052 (16, 1)
353000.0 /	139.17953 (290, 1)	141.88832 (290, 1)	126.54845 (15, 1)	112.28322 (290, 1)	103.93906 (67, 1)
352900.0 /	147.30116 (15, 1)	123.34520 (16, 1)	111.84319 (67, 1)	109.01153 (67, 1)	103.09634 (67, 1)
352800.0 /	126.76409 (16, 1)	116.55306 (67, 1)	113.25774 (67, 1)	107.41451 (67, 1)	103.29803 (67, 1)
352700.0 /	120.35753 (67, 1)	116.73489 (67, 1)	111.32121 (67, 1)	108.41341 (67, 1)	111.98265 (67, 1)
352600.0 /	119.55132 (67, 1)	114.85110 (67, 1)	113.18108 (67, 1)	117.65698 (67, 1)	126.40973 (67, 1)
352500.0 /	118.00008 (67, 1)	117.49799 (67, 1)	122.69094 (67, 1)	131.71727 (67, 1)	119.74267 (16, 1)
352400.0 /	121.34415 (67, 1)	127.03839 (67, 1)	136.15749 (67, 1)	127.08359 (16, 1)	121.89459 (273, 1)
352300.0 /	130.75612 (67, 1)	139.81093 (67, 1)	133.19563 (16, 1)	121.72697 (273, 1)	120.72337 (273, 1)
352200.0 /	142.76823 (67, 1)	138.14766 (16, 1)	121.01280 (273, 1)	121.06216 (273, 1)	116.48360 (273, 1)
352100.0 /	142.04085 (16, 1)	123.11321 (16, 1)	120.91064 (273, 1)	117.18081 (273, 1)	111.10883 (273, 1)
352000.0 /	126.73849 (16, 1)	120.33605 (273, 1)	117.62669 (273, 1)	111.60754 (273, 1)	106.17773 (273, 1)
351900.0 /	119.42674 (273, 1)	117.74933 (273, 1)	112.26093 (273, 1)	105.99178 (273, 1)	102.11678 (273, 1)
351800.0 /	117.54461 (273, 1)	112.86663 (273, 1)	106.32771 (273, 1)	101.16409 (273, 1)	98.60937 (273, 1)
351700.0 /	113.30193 (273, 1)	106.95039 (273, 1)	100.90919 (273, 1)	97.08974 (273, 1)	94.35150 (67, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 164.03651 AND OCCURRED AT (435600.0, 352700.0) *

Y-AXIS (METERS) /	X-AXIS (METERS)				
	436500.0	436600.0	436700.0	436800.0	436900.0
353400.0 /	94.96615 (67, 1)	90.74804 (67, 1)	86.09148 (67, 1)	79.36203 (15, 1)	68.41357 (273, 1)
353300.0 /	101.53918 (16, 1)	95.77754 (16, 1)	85.62804 (16, 1)	77.52453 (16, 1)	75.30483 (273, 1)
353200.0 /	102.65863 (16, 1)	92.02686 (67, 1)	87.62082 (67, 1)	81.53340 (67, 1)	79.27394 (16, 1)
353100.0 /	98.14906 (67, 1)	93.12146 (67, 1)	86.84069 (67, 1)	93.19625 (273, 1)	87.27121 (67, 1)
353000.0 /	98.32779 (67, 1)	92.37334 (67, 1)	97.25905 (273, 1)	96.29039 (67, 1)	95.94316 (67, 1)
352900.0 /	97.91313 (67, 1)	99.87018 (273, 1)	105.00983 (67, 1)	106.67800 (67, 1)	99.10768 (67, 1)
352800.0 /	105.71972 (67, 1)	113.04015 (67, 1)	115.08114 (273, 1)	110.77040 (67, 1)	96.54137 (67, 1)
352700.0 /	120.19189 (67, 1)	117.48897 (273, 1)	117.76437 (273, 1)	108.82513 (67, 1)	89.52008 (67, 1)
352600.0 /	118.70029 (273, 1)	119.99846 (273, 1)	116.95290 (273, 1)	101.94727 (67, 1)	81.11855 (67, 1)
352500.0 /	121.35146 (273, 1)	118.49239 (273, 1)	113.68013 (67, 1)	92.66106 (67, 1)	85.94863 (2, 1)
352400.0 /	119.82677 (273, 1)	115.02232 (273, 1)	104.25870 (67, 1)	83.56454 (67, 1)	100.70912 (2, 1)
352300.0 /	115.69008 (273, 1)	111.67863 (273, 1)	94.22467 (67, 1)	86.93200 (2, 1)	106.99808 (273, 1)
352200.0 /	111.04460 (273, 1)	104.81401 (67, 1)	85.09429 (67, 1)	99.34295 (2, 1)	100.13750 (273, 1)
352100.0 /	107.12871 (273, 1)	94.82977 (67, 1)	86.05093 (2, 1)	102.11595 (273, 1)	93.41814 (273, 1)
352000.0 /	103.88966 (273, 1)	85.90314 (67, 1)	96.58452 (2, 1)	96.17784 (273, 1)	87.45456 (273, 1)
351900.0 /	94.79556 (67, 1)	84.18933 (2, 1)	96.87794 (273, 1)	90.43333 (273, 1)	82.53203 (273, 1)
351800.0 /	86.17293 (67, 1)	93.25283 (2, 1)	91.79364 (273, 1)	85.32085 (273, 1)	78.66655 (273, 1)
351700.0 /	81.86975 (2, 1)	91.69354 (273, 1)	86.91681 (273, 1)	81.08246 (273, 1)	75.67665 (273, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 164.03651 AND OCCURRED AT (435600.0, 352700.0) *

Y-AXIS (METERS) /	437000.0	437100.0	X-AXIS (METERS) 437200.0	437300.0	437400.0
353400.0 /	70.46062 (273, 1)	67.78416 (67, 1)	64.32320 (67, 1)	60.46945 (67, 1)	57.11079 (67, 1)
353300.0 /	72.03754 (67, 1)	69.43254 (67, 1)	64.62286 (67, 1)	59.16182 (67, 1)	55.56513 (67, 1)
353200.0 /	78.07710 (67, 1)	73.16127 (67, 1)	64.60386 (67, 1)	60.82549 (2, 1)	65.46615 (2, 1)
353100.0 /	84.96618 (67, 1)	75.18045 (67, 1)	62.64351 (67, 1)	77.77287 (2, 1)	72.65610 (2, 1)
353000.0 /	87.00106 (67, 1)	72.24979 (67, 1)	79.26909 (2, 1)	90.20931 (273, 1)	71.15599 (273, 1)
352900.0 /	83.91913 (67, 1)	73.13823 (2, 1)	98.59056 (2, 1)	84.43098 (273, 1)	68.97311 (273, 1)
352800.0 /	77.42448 (67, 1)	92.74978 (2, 1)	99.99632 (273, 1)	78.79601 (273, 1)	67.44648 (273, 1)
352700.0 /	81.79531 (2, 1)	109.99942 (2, 1)	91.99823 (273, 1)	74.23408 (273, 1)	63.38583 (2, 1)
352600.0 /	99.23438 (2, 1)	103.59408 (273, 1)	84.72499 (273, 1)	70.88937 (273, 1)	58.45511 (2, 1)
352500.0 /	110.69089 (273, 1)	95.25536 (273, 1)	78.85950 (273, 1)	68.60313 (273, 1)	54.01202 (2, 1)
352400.0 /	103.00826 (273, 1)	87.81554 (273, 1)	74.42406 (273, 1)	67.16981 (273, 1)	50.16686 (2, 1)
352300.0 /	95.31374 (273, 1)	81.77068 (273, 1)	71.17311 (273, 1)	64.26365 (2, 1)	46.90388 (2, 1)
352200.0 /	88.48514 (273, 1)	77.10580 (273, 1)	68.83186 (273, 1)	58.28649 (2, 1)	46.65564 (67, 1)
352100.0 /	82.90303 (273, 1)	73.56239 (273, 1)	67.18922 (273, 1)	53.23146 (2, 1)	46.93896 (67, 1)
352000.0 /	78.55335 (273, 1)	70.84474 (273, 1)	66.10562 (273, 1)	48.98648 (2, 1)	47.25953 (67, 1)
351900.0 /	75.15683 (273, 1)	68.69019 (273, 1)	59.93852 (2, 1)	45.42596 (2, 1)	47.56890 (67, 1)
351800.0 /	72.45770 (273, 1)	66.99887 (273, 1)	54.53078 (2, 1)	42.43364 (2, 1)	47.83100 (67, 1)
351700.0 /	70.22785 (273, 1)	65.70938 (273, 1)	49.93367 (2, 1)	42.33555 (67, 1)	48.02185 (67, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* 50 MAXIMUM 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *

* FROM ALL SOURCES *

RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y(METERS) OR DIRECTION (DEGREES)	RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y(METERS) OR DIRECTION (DEGREES)
1	197.74132	1	15	435600.0	352800.0	26	179.91302	1	16	435800.0	352100.0
2	196.01215	1	15	435500.0	352800.0	27	178.24438	1	16	435900.0	352200.0
3	193.72751	1	15	435500.0	352700.0	28	176.80125	1	16	436100.0	352500.0
4	191.27898	1	15	435700.0	352900.0	29	176.22412	1	16	435700.0	352300.0
5	191.06427	1	15	435800.0	352900.0	30	176.04161	1	15	435900.0	352900.0
6	190.90430	1	16	435500.0	352000.0	31	175.48190	1	16	436000.0	352300.0
7	190.04825	1	16	435600.0	352100.0	32	175.16132	1	16	436000.0	352500.0
8	189.98601	1	16	435600.0	352000.0	33	174.72295	1	15	435600.0	352700.0
9	189.64899	1	16	435500.0	351900.0	34	172.55882	1	15	435800.0	353000.0
10	189.57849	1	16	435700.0	352100.0	35	171.42419	1	16	436100.0	352400.0
11	188.25845	1	16	435800.0	352200.0	36	171.14520	1	16	435800.0	352400.0
12	188.23529	1	16	435700.0	352200.0	37	170.56404	1	15	436100.0	353100.0
13	186.87840	1	15	435700.0	352800.0	38	169.73611	1	16	436200.0	352600.0
14	185.83383	1	16	435900.0	352300.0	39	167.60750	1	16	436100.0	352600.0
15	185.28203	1	16	435800.0	352300.0	40	167.52132	1	16	435500.0	352200.0
16	183.14224	1	15	435900.0	353000.0	41	165.86008	1	16	436200.0	352500.0
17	182.78174	1	16	435500.0	352100.0	42	165.72919	1	16	435600.0	351800.0
18	182.09094	1	16	436000.0	352400.0	43	165.40945	1	16	435700.0	351900.0
19	180.99106	1	16	435900.0	352400.0	44	165.32776	1	16	435500.0	351700.0
20	180.67876	1	16	435600.0	351900.0	45	164.95146	1	290	435500.0	352600.0
21	180.67058	1	16	435700.0	352000.0	46	164.70485	1	16	435900.0	352500.0
22	180.28764	1	15	435600.0	352900.0	47	164.41953	1	16	435800.0	352000.0
23	180.19388	1	15	436000.0	353000.0	48	164.03651	1	290	435600.0	352700.0
24	180.05704	1	16	435600.0	352200.0	49	163.88376	1	15	436200.0	353100.0
25	180.03917	1	16	435500.0	351800.0	50	163.55801	1	67	435800.0	351700.0

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ISCST FINE GRID ANALYSIS
PRODUCING SECOND-HIGHEST 3-HOUR AVERAGE

CALCULATE (CONCENTRATION=1,DEPOSITION=2)
RECEPTOR GRID SYSTEM (RECTANGULAR=1 OR 3, POLAR=2 OR 4)
DISCRETE RECEPTOR SYSTEM (RECTANGULAR=1,POLAR=2)
TERRAIN ELEVATIONS ARE READ (YES=1,NO=0)
CALCULATIONS ARE WRITTEN TO TAPE (YES=1,NO=0)
LIST ALL INPUT DATA (NO=0,YES=1,MET DATA ALSO=2)

ISW(1) = 1
ISW(2) = 3
ISW(3) = 1
ISW(4) = 0
ISW(5) = 0
ISW(6) = 2

COMPUTE AVERAGE CONCENTRATION (OR TOTAL DEPOSITION)
WITH THE FOLLOWING TIME PERIODS:

HOURLY (YES=1,NO=0)
2-HOUR (YES=1,NO=0)
3-HOUR (YES=1,NO=0)
4-HOUR (YES=1,NO=0)
6-HOUR (YES=1,NO=0)
8-HOUR (YES=1,NO=0)
12-HOUR (YES=1,NO=0)
24-HOUR (YES=1,NO=0)
PRINT 'N'-DAY TABLE(S) (YES=1,NO=0)

ISW(7) = 0
ISW(8) = 0
ISW(9) = 1
ISW(10) = 0
ISW(11) = 0
ISW(12) = 0
ISW(13) = 0
ISW(14) = 1
ISW(15) = 0

PRINT THE FOLLOWING TYPES OF TABLES WHOSE TIME PERIODS ARE
SPECIFIED BY ISW(7) THROUGH ISW(14):

DAILY TABLES (YES=1,NO=0)
HIGHEST & SECOND HIGHEST TABLES (YES=1,NO=0)
MAXIMUM 50 TABLES (YES=1,NO=0)
METEOROLOGICAL DATA INPUT METHOD (PRE-PROCESSED=1,CARD=2)
RURAL-URBAN OPTION (RURAL=0,URBAN MODE 1=1,URBAN MODE 2=2)
WIND PROFILE EXPONENT VALUES (DEFAULTS=1,USER ENTERS=2,3)
VERTICAL POT. TEMP. GRADIENT VALUES (DEFAULTS=1,USER ENTERS=2,3)
SCALE EMISSION RATES FOR ALL SOURCES (NO=0,YES>0)
PROGRAM CALCULATES FINAL PLUME RISE ONLY (YES=1,NO=2)
PROGRAM ADJUSTS ALL STACK HEIGHTS FOR DOWNWASH (YES=2,NO=1)

ISW(16) = 0
ISW(17) = 1
ISW(18) = 1
ISW(19) = 1
ISW(20) = 0
ISW(21) = 1
ISW(22) = 1
ISW(23) = 0
ISW(24) = 1
ISW(25) = 1

NUMBER OF INPUT SOURCES
NUMBER OF SOURCE GROUPS (=0,ALL SOURCES)
TIME PERIOD INTERVAL TO BE PRINTED (=0,ALL INTERVALS)
NUMBER OF X (RANGE) GRID VALUES
NUMBER OF Y (THETA) GRID VALUES
NUMBER OF DISCRETE RECEPTORS
SOURCE EMISSION RATE UNITS CONVERSION FACTOR
ENTRAINMENT COEFFICIENT FOR UNSTABLE ATMOSPHERE
ENTRAINMENT COEFFICIENT FOR STABLE ATMOSPHERE
HEIGHT ABOVE GROUND AT WHICH WIND SPEED WAS MEASURED
LOGICAL UNIT NUMBER OF METEOROLOGICAL DATA
DECAY COEFFICIENT FOR PHYSICAL OR CHEMICAL DEPLETION
SURFACE STATION NO.
YEAR OF SURFACE DATA
UPPER AIR STATION NO.
YEAR OF UPPER AIR DATA
ALLOCATED DATA STORAGE
REQUIRED DATA STORAGE FOR THIS PROBLEM RUN

NSOURC = 17
NGROUP = 0
IPERD = 0
NXPNTS = 18
NYPNTS = 21
NXWYPT = 0
TK = .10000E+07
BETA1 = 0.600
BETA2 = 0.600
ZR = 7.00 METERS
IMET = 9
DECAY = 0.000000E+00
ISS = 13889
ISY = 71
IUS = 13861
IUY = 71
LIMIT = 43500 WORDS
MIMIT = 8632 WORDS

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*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

*** X-COORDINATES OF RECTANGULAR GRID SYSTEM ***
(METERS)

437500.0, 437600.0, 437700.0, 437800.0, 437900.0, 438000.0, 438100.0, 438200.0, 438300.0, 438400.0,
438500.0, 438600.0, 438700.0, 438800.0, 438900.0, 439000.0, 439100.0, 439200.0,

*** Y-COORDINATES OF RECTANGULAR GRID SYSTEM ***
(METERS)

352700.0, 352800.0, 352900.0, 353000.0, 353100.0, 353200.0, 353300.0, 353400.0, 353500.0, 353600.0,
353700.0, 353800.0, 353900.0, 354000.0, 354100.0, 354200.0, 354300.0, 354400.0, 354500.0, 354600.0,
354700.0,

*** SOURCE DATA ***

SOURCE NUMBER	T W Y A NUMBER P K PART. E E CATS.	EMISSION RATE TYPE=0,1 (GRAMS/SEC) TYPE=2 (GRAMS/SEC) *PER METER**2	X (METERS)	Y (METERS)	BASE ELEV. (METERS)	HEIGHT (METERS)	TEMP.	EXIT VEL.	BLDG. HEIGHT (METERS)	BLDG. LENGTH (METERS)	BLDG. WIDTH (METERS)	
							(DEG.K); VERT. DIM TYPE=1 (METERS)	(M/SEC); HORZ. DIM DIAMETER TYPE=1,2 (METERS)				
1	0 0	0.11766E+04	446900.0	366300.0	0.0	194.20	327.60	18.29	10.13	0.00	0.00	0.00
2	0 0	0.70570E+03	446900.0	364900.0	0.0	76.20	401.00	20.10	5.03	0.00	0.00	0.00
3	0 0	0.70570E+03	446900.0	364900.0	0.0	91.40	408.20	8.50	5.33	0.00	0.00	0.00
4	0 0	0.12556E+04	446900.0	364900.0	0.0	106.70	438.80	19.20	7.01	0.00	0.00	0.00
5	0 0	0.23160E+03	446900.0	364900.0	0.0	10.10	779.80	18.30	6.56	0.00	0.00	0.00
6	0 0	0.13180E+03	437670.0	353900.0	0.0	40.70	433.20	11.70	2.44	0.00	0.00	0.00
7	0 0	0.90600E+02	437670.0	353900.0	0.0	40.70	406.50	10.30	3.05	0.00	0.00	0.00
8	0 0	0.11030E+03	437670.0	353900.0	0.0	43.70	422.10	11.80	3.35	0.00	0.00	0.00
9	0 0	0.20970E+03	437670.0	353900.0	0.0	44.20	416.50	13.70	3.05	0.00	0.00	0.00
10	0 0	0.16520E+03	440080.0	359150.0	0.0	45.70	414.30	7.80	3.20	0.00	0.00	0.00
11	0 0	0.20480E+03	440080.0	359150.0	0.0	41.50	405.40	15.50	2.74	0.00	0.00	0.00
12	0 0	0.19120E+03	440080.0	359150.0	0.0	13.70	714.30	8.80	5.84	0.00	0.00	0.00
13	0 0	0.13800E+02	440080.0	359150.0	0.0	6.30	766.50	11.80	3.13	0.00	0.00	0.00
14	0 0	0.20840E+03	441800.0	365600.0	0.0	32.30	433.00	16.10	2.13	0.00	0.00	0.00
15	0 0	0.82200E+02	437900.0	366800.0	0.0	15.90	505.00	8.60	1.37	0.00	0.00	0.00
16	0 0	0.54400E+02	439900.0	359300.0	0.0	76.20	477.00	9.20	3.78	0.00	0.00	0.00
17	0 0	0.25600E+02	447040.0	366570.0	0.0	85.40	441.00	12.20	2.08	0.00	0.00	0.00

Source NO.	Source Name
1	SJRPP Units 1 & 2
2	Northside Unit 1
3	Northside Unit 2
4	Northside Unit 3
5	Northside CT 3, 4, 5, 6
6	Southside Units 1 & 2
7	Southside Unit 3
8	Southside Unit 4
9	Southside Unit 5
10	Kennedy Units 8 & 9
11	Kennedy Unit 10
12	Kennedy CT 3, 4, 5, 6
13	Kennedy CT 1
14	St. Regis (All major sources)
15	Anheuser Busch (All major sources)
16	Alton Box Board (All major sources)
17	SJRPP Aux. Boiler

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SOURCE-RECEPTOR COMBINATIONS LESS THAN 100 METERS OR THREE BUILDING
HEIGHTS IN DISTANCE. NO AVERAGE CONCENTRATION IS CALCULATED *

SOURCE NUMBER	-- RECEPTOR LOCATION --		DISTANCE BETWEEN (METERS)
	X OR RANGE (METERS)	Y (METERS) OR DIRECTION (DEGREES)	
6	437600.0	353900.0	70.00
6	437700.0	353900.0	30.00
7	437600.0	353900.0	70.00
7	437700.0	353900.0	30.00
8	437600.0	353900.0	70.00
8	437700.0	353900.0	30.00
9	437600.0	353900.0	70.00
9	437700.0	353900.0	30.00

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* METEOROLOGICAL DATA FOR DAY 100 *

HOUR	FLOW VECTOR (DEGREES)	RANDOM FLOW VECTOR (DEGREES)	WIND SPEED (MPS)	MIXING HEIGHT (METERS)	TEMP. (DEG. K)	INPUT STABILITY CATEGORY	ADJUSTED STABILITY CATEGORY
1	50.0	50.0	2.57	2093.5	286.5	6	6
2	50.0	54.0	3.09	2123.8	285.9	6	6
3	50.0	48.0	3.09	2154.2	285.9	6	6
4	80.0	78.0	2.57	2184.5	283.2	6	6
5	80.0	84.0	1.00	2214.9	282.0	6	6
6	120.0	118.0	1.54	2245.2	280.4	6	6
7	120.0	124.0	1.00	2267.1	282.0	6	6
8	70.0	66.0	2.06	584.4	287.0	5	5
9	60.0	64.0	3.09	901.6	291.5	4	4
10	90.0	86.0	2.06	1218.9	294.3	3	3
11	140.0	142.0	2.57	1536.2	297.6	2	2
12	80.0	84.0	4.12	1853.5	298.7	2	2
13	80.0	81.0	2.06	2170.7	299.8	1	1
14	80.0	83.0	3.60	2488.0	300.4	2	2
15	90.0	88.0	3.09	2488.0	300.9	2	2
16	70.0	68.0	2.06	2488.0	300.9	2	2
17	310.0	308.0	6.17	2488.0	298.2	3	3
18	310.0	311.0	4.63	2488.0	295.9	4	4
19	310.0	312.0	2.57	2485.8	293.7	5	5
20	340.0	344.0	2.06	2476.8	290.9	6	6
21	340.0	339.0	1.00	2467.8	288.7	6	6
22	340.0	343.0	1.00	2458.8	288.2	6	6
23	70.0	72.0	2.57	2449.9	285.9	6	6
24	250.0	246.0	1.54	2440.9	285.4	6	6

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* METEOROLOGICAL DATA FOR DAY 101 *

HOUR	FLOW VECTOR (DEGREES)	RANDOM FLOW VECTOR (DEGREES)	WIND SPEED (MPS)	MIXING HEIGHT (METERS)	TEMP. (DEG. K)	INPUT STABILITY CATEGORY	ADJUSTED STABILITY CATEGORY
1	250.0	246.0	1.00	2431.9	284.8	6	6
2	250.0	250.0	1.00	2422.9	283.2	6	6
3	330.0	330.0	1.54	2413.9	282.6	6	6
4	330.0	326.0	1.00	2404.9	282.0	6	6
5	330.0	334.0	1.00	2396.0	281.5	6	6
6	270.0	270.0	1.54	2387.0	281.5	6	6
7	190.0	195.0	2.57	253.7	282.0	6	6
8	180.0	180.0	1.54	548.1	287.6	5	5
9	230.0	234.0	1.54	842.6	292.0	4	4
10	240.0	237.0	3.60	1137.1	294.8	3	3
11	230.0	234.0	5.14	1431.6	297.6	3	3
12	240.0	236.0	5.66	1726.0	298.7	3	3
13	280.0	279.0	4.63	2020.5	298.7	2	2
14	270.0	274.0	6.17	2315.0	298.7	3	3
15	260.0	264.0	5.14	2315.0	298.7	3	3
16	240.0	242.0	6.17	2315.0	297.6	4	4
17	240.0	243.0	6.69	2315.0	296.5	4	4
18	260.0	261.0	5.14	2315.0	294.8	4	4
19	250.0	248.0	3.09	2312.7	291.5	5	5
20	270.0	266.0	3.09	2302.8	289.8	6	6
21	330.0	326.0	3.09	2292.8	287.6	6	6
22	310.0	309.0	2.06	2282.9	287.6	6	6
23	310.0	315.0	1.00	2273.0	285.4	6	6
24	180.0	177.0	1.54	2263.0	284.3	6	6

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* METEOROLOGICAL DATA FOR DAY 110 *

HOUR	FLOW VECTOR (DEGREES)	RANDOM FLOW VECTOR (DEGREES)	WIND SPEED (MPS)	MIXING HEIGHT (METERS)	TEMP. (DEG. K)	INPUT STABILITY CATEGORY	ADJUSTED STABILITY CATEGORY
1	240.0	239.0	2.57	2429.7	292.0	5	5
2	240.0	238.0	1.00	2458.7	290.9	6	6
3	240.0	239.0	1.00	2487.6	290.4	6	6
4	240.0	243.0	1.00	2516.6	289.3	6	6
5	240.0	245.0	1.00	2545.5	289.3	6	6
6	240.0	244.0	1.00	10.4	288.7	6	6
7	240.0	239.0	1.00	359.9	289.8	5	5
8	320.0	318.0	3.09	709.3	294.3	4	4
9	320.0	323.0	4.12	1058.8	296.5	3	3
10	40.0	44.0	4.12	1408.2	298.2	3	3
11	10.0	7.0	4.12	1757.7	299.3	2	2
12	60.0	65.0	3.09	2107.1	301.5	2	2
13	150.0	146.0	1.54	2456.6	302.6	1	1
14	130.0	126.0	4.12	2806.0	303.2	2	2
15	130.0	133.0	2.06	2806.0	302.6	3	3
16	50.0	53.0	5.66	2806.0	303.7	4	4
17	80.0	82.0	5.14	2806.0	303.2	4	4
18	80.0	79.0	3.09	2806.0	301.5	4	4
19	70.0	73.0	2.57	2800.9	298.7	5	5
20	70.0	66.0	2.57	2764.5	297.0	6	6
21	50.0	52.0	3.60	2728.0	295.4	5	5
22	50.0	48.0	2.57	2691.6	294.8	6	6
23	70.0	71.0	3.60	2655.2	292.6	5	5
24	70.0	75.0	3.60	2618.8	292.6	5	5

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* METEOROLOGICAL DATA FOR DAY 112 *

HOUR	FLOW VECTOR (DEGREES)	RANDOM FLOW VECTOR (DEGREES)	WIND SPEED (MPS)	MIXING HEIGHT (METERS)	TEMP. (DEG. K)	INPUT STABILITY CATEGORY	ADJUSTED STABILITY CATEGORY
1	60.0	60.0	4.12	2379.1	293.7	5	5
2	70.0	70.0	3.60	2423.3	293.7	5	5
3	60.0	56.0	2.57	2467.4	293.7	6	6
4	70.0	67.0	2.57	2511.6	293.2	6	6
5	50.0	50.0	3.09	2555.7	293.2	6	6
6	40.0	37.0	3.09	23.8	293.7	5	5
7	50.0	55.0	4.63	390.0	294.3	4	4
8	60.0	61.0	5.66	756.1	295.9	4	4
9	90.0	86.0	7.72	1122.3	297.6	4	4
10	100.0	104.0	7.20	1488.4	299.8	4	4
11	70.0	69.0	5.66	1854.6	300.9	3	3
12	90.0	91.0	7.20	2220.7	302.0	3	3
13	80.0	85.0	6.17	2586.9	303.7	3	3
14	80.0	84.0	6.17	2953.0	303.7	3	3
15	80.0	80.0	9.26	2953.0	304.3	4	4
16	80.0	81.0	7.72	2953.0	303.2	4	4
17	80.0	79.0	7.20	2953.0	302.0	4	4
18	110.0	113.0	6.69	2953.0	296.5	4	4
19	100.0	99.0	6.69	2946.2	295.4	4	4
20	50.0	54.0	2.06	2889.9	293.7	5	5
21	60.0	56.0	3.60	2833.5	293.2	4	4
22	60.0	58.0	1.00	2777.1	293.2	5	5
23	60.0	64.0	1.00	2720.7	293.2	6	6
24	40.0	37.0	3.60	2664.3	292.6	5	5

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* METEOROLOGICAL DATA FOR DAY 180 *

HOUR	FLOW VECTOR (DEGREES)	RANDOM FLOW VECTOR (DEGREES)	WIND SPEED (MPS)	MIXING HEIGHT (METERS)	TEMP. (DEG. K)	INPUT STABILITY CATEGORY	ADJUSTED STABILITY CATEGORY
1	50.0	46.0	1.54	1416.3	295.4	6	6
2	360.0	359.0	1.54	1412.7	294.8	6	6
3	360.0	2.0	1.00	1409.2	294.8	6	6
4	360.0	2.0	1.00	1405.6	294.8	6	6
5	360.0	359.0	1.00	1402.0	294.3	6	6
6	360.0	356.0	1.00	78.8	294.3	6	6
7	50.0	49.0	1.54	240.2	296.5	5	5
8	80.0	78.0	2.06	401.6	298.7	4	4
9	120.0	120.0	2.06	563.0	300.4	3	3
10	120.0	125.0	1.00	724.4	302.0	2	2
11	80.0	82.0	1.54	885.8	303.7	1	1
12	80.0	82.0	2.57	1047.2	304.3	1	1
13	250.0	255.0	1.54	1208.6	304.3	1	1
14	340.0	336.0	7.72	1370.0	297.6	2	2
15	70.0	74.0	1.54	1370.0	297.0	3	3
16	10.0	15.0	1.54	1370.0	296.5	3	3
17	110.0	113.0	2.06	1370.0	297.0	3	3
18	160.0	157.0	2.57	1370.0	297.0	3	3
19	50.0	55.0	2.06	1370.0	297.0	4	4
20	50.0	52.0	2.06	1377.2	296.5	5	5
21	80.0	79.0	1.54	1390.7	296.5	4	4
22	190.0	192.0	1.54	1404.1	295.9	5	5
23	250.0	254.0	2.06	1417.5	295.4	6	6
24	250.0	247.0	1.00	1431.0	295.4	6	6

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* METEOROLOGICAL DATA FOR DAY 207 *

HOUR -----	FLOW VECTOR (DEGREES)	RANDOM FLOW VECTOR (DEGREES)	WIND SPEED (MPS)	MIXING HEIGHT (METERS)	TEMP. (DEG. K)	INPUT STABILITY CATEGORY	ADJUSTED STABILITY CATEGORY
-----	-----	-----	-----	-----	-----	-----	-----
1	10.0	10.0	1.54	2093.8	297.6	6	6
2	10.0	15.0	1.54	2088.8	297.6	6	6
3	10.0	13.0	1.00	2083.8	297.6	6	6
4	10.0	6.0	1.00	2078.9	297.0	6	6
5	360.0	358.0	2.06	2073.9	297.0	6	6
6	360.0	356.0	2.57	64.9	297.0	5	5
7	30.0	27.0	1.54	310.4	297.6	4	4
8	50.0	49.0	3.09	555.9	298.7	4	4
9	360.0	357.0	2.57	801.4	300.9	3	3
10	10.0	14.0	4.12	1046.9	303.2	3	3
11	360.0	360.0	2.57	1292.4	303.2	2	2
12	50.0	46.0	1.54	1538.0	303.7	1	1
13	60.0	63.0	4.63	1783.5	304.8	2	2
14	70.0	68.0	4.12	2029.0	305.9	2	2
15	60.0	63.0	4.12	2029.0	306.5	3	3
16	60.0	59.0	4.63	2029.0	307.0	4	4
17	90.0	94.0	4.12	2029.0	303.2	4	4
18	70.0	74.0	1.54	2029.0	302.6	3	3
19	330.0	333.0	1.54	2029.0	299.8	3	3
20	330.0	328.0	1.00	2015.7	299.3	4	4
21	330.0	329.0	1.00	1995.3	298.7	5	5
22	330.0	330.0	1.54	1974.8	298.2	6	6
23	330.0	329.0	1.00	1954.4	298.7	6	6
24	330.0	327.0	1.00	1934.0	298.2	6	6

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* METEOROLOGICAL DATA FOR DAY 273 *

HOURL	FLOW VECTOR (DEGREES)	RANDOM FLOW VECTOR (DEGREES)	WIND SPEED (MPS)	MIXING HEIGHT (METERS)	TEMP. (DEG. K)	INPUT STABILITY CATEGORY	ADJUSTED STABILITY CATEGORY
1	120.0	122.0	2.06	1785.6	291.5	6	6
2	130.0	135.0	2.06	1776.5	291.5	6	6
3	130.0	133.0	2.06	1767.4	290.9	6	6
4	120.0	125.0	2.06	1758.2	290.4	6	6
5	100.0	99.0	1.54	1749.1	290.4	6	6
6	120.0	123.0	2.57	1740.0	289.3	6	6
7	130.0	126.0	2.57	140.7	290.4	5	5
8	150.0	146.0	3.09	358.7	293.2	4	4
9	180.0	185.0	4.12	576.8	295.9	3	3
10	160.0	156.0	3.60	794.8	298.2	2	2
11	160.0	161.0	3.09	1012.9	300.4	2	2
12	170.0	166.0	3.09	1230.9	302.0	2	2
13	170.0	173.0	3.60	1449.0	303.2	2	2
14	160.0	156.0	4.12	1667.0	303.7	3	3
15	180.0	182.0	2.57	1667.0	304.3	2	2
16	190.0	190.0	3.60	1667.0	304.3	3	3
17	140.0	138.0	3.09	1667.0	303.7	4	4
18	140.0	144.0	1.00	1667.0	301.5	3	3
19	60.0	58.0	1.54	1687.3	297.0	4	4
20	60.0	57.0	1.00	1711.5	295.4	5	5
21	50.0	53.0	2.06	1735.8	294.3	6	6
22	110.0	110.0	2.06	1760.0	293.2	6	6
23	110.0	109.0	1.00	1784.3	292.0	6	6
24	130.0	133.0	1.54	1808.5	292.6	6	6

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 724.50140 AND OCCURRED AT (438700.0, 354400.0) *

Y-AXIS / (METERS) /	X-AXIS (METERS)				
	437500.0	437600.0	437700.0	437800.0	437900.0
354700.0 /	114.77422 (180, 5)	114.02963 (207, 4)	228.05188 (110, 4)	258.70633 (110, 4)	161.64139 (110, 4)
354600.0 /	156.65990 (180, 5)	80.32417 (110, 4)	197.16815 (110, 4)	213.11998 (110, 4)	109.10553 (110, 4)
354500.0 /	202.50671 (180, 5)	59.10878 (101, 3)	141.08450 (110, 4)	140.97137 (110, 4)	72.31924 (101, 3)
354400.0 /	227.42998 (180, 5)	58.81205 (101, 3)	70.01780 (110, 4)	69.83521 (101, 3)	72.09447 (101, 3)
354300.0 /	180.41423 (180, 5)	58.52753 (101, 3)	64.96870 (101, 3)	69.51020 (101, 3)	71.96971 (101, 3)
354200.0 /	64.24567 (180, 5)	58.25893 (101, 3)	64.64801 (101, 3)	69.25433 (101, 3)	71.96029 (101, 3)
354100.0 /	50.40421 (101, 3)	58.01089 (101, 3)	64.37196 (101, 3)	69.08008 (101, 3)	72.08199 (101, 3)
354000.0 /	50.26210 (101, 3)	57.78908 (101, 3)	64.15001 (101, 3)	69.00105 (101, 3)	72.35061 (101, 3)
353900.0 /	50.13318 (101, 3)	57.60026 (101, 3)	63.99285 (101, 3)	69.03154 (101, 3)	72.78138 (101, 3)
353800.0 /	50.02207 (101, 3)	57.45235 (101, 3)	63.91232 (101, 3)	69.18633 (101, 3)	73.38853 (101, 3)
353700.0 /	49.93434 (101, 3)	57.35445 (101, 3)	63.92121 (101, 3)	69.48016 (101, 3)	74.18494 (101, 3)
353600.0 /	49.87656 (101, 3)	57.31670 (101, 3)	64.03294 (101, 3)	69.92741 (101, 3)	75.18204 (101, 3)
353500.0 /	49.85636 (101, 3)	57.35034 (101, 3)	64.26141 (101, 3)	70.54170 (101, 3)	76.39015 (101, 3)
353400.0 /	49.88240 (101, 3)	57.46739 (101, 3)	64.62050 (101, 3)	83.16903 (273, 4)	129.66838 (273, 4)
353300.0 /	49.96438 (101, 3)	70.87260 (273, 5)	142.33115 (273, 5)	185.58569 (273, 4)	297.77835 (273, 4)
353200.0 /	50.49209 (273, 5)	147.25868 (273, 5)	243.92319 (273, 5)	275.94135 (273, 4)	455.29150 (273, 4)
353100.0 /	98.05727 (273, 5)	227.36040 (273, 5)	332.82623 (273, 5)	328.71939 (273, 4)	553.16870 (273, 4)
353000.0 /	149.04300 (273, 5)	293.63812 (273, 5)	396.04724 (273, 5)	366.99347 (273, 5)	587.30206 (273, 4)
352900.0 /	193.88687 (273, 5)	339.38327 (273, 5)	432.61728 (273, 5)	404.32065 (273, 5)	575.09973 (273, 4)
352800.0 /	228.00633 (273, 5)	365.35345 (273, 5)	447.27393 (273, 5)	421.48029 (273, 5)	536.21448 (273, 4)
352700.0 /	250.74084 (273, 5)	375.44894 (273, 5)	446.08618 (273, 5)	423.61761 (273, 5)	485.35175 (273, 4)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 724.50140 AND OCCURRED AT (438700.0, 354400.0) *

Y-AXIS (METERS) /	X-AXIS (METERS)				
	438000.0	438100.0	438200.0	438300.0	438400.0
354700.0 /	90.61794 (207, 4)	109.77438 (207, 4)	165.50266 (207, 4)	202.64490 (207, 4)	207.22009 (207, 4)
354600.0 /	85.55386 (207, 4)	165.92291 (207, 4)	243.41562 (207, 4)	270.35645 (207, 4)	249.90997 (207, 4)
354500.0 /	102.68792 (207, 4)	231.35211 (207, 4)	316.35657 (207, 4)	317.75900 (207, 4)	264.64798 (207, 4)
354400.0 /	100.99275 (207, 4)	251.71562 (207, 4)	331.00500 (207, 4)	305.29568 (207, 4)	382.80359 (207, 5)
354300.0 /	72.63785 (101, 3)	170.72388 (207, 4)	238.24918 (207, 4)	422.57700 (207, 5)	620.85107 (207, 5)
354200.0 /	73.10876 (101, 3)	138.44035 (207, 5)	361.44418 (207, 5)	544.96967 (207, 5)	606.16602 (207, 5)
354100.0 /	73.76456 (101, 3)	159.71588 (207, 5)	296.63904 (207, 5)	476.50684 (180, 4)	555.70129 (180, 4)
354000.0 /	74.61856 (101, 3)	119.21326 (180, 4)	387.16339 (180, 4)	623.13715 (180, 4)	673.99487 (100, 5)
353900.0 /	75.68202 (101, 3)	83.56921 (180, 4)	289.48846 (180, 4)	493.27789 (180, 4)	562.91010 (100, 5)
353800.0 /	76.96431 (101, 3)	80.57813 (101, 3)	99.81955 (180, 4)	222.16991 (180, 4)	287.91583 (180, 4)
353700.0 /	78.47368 (101, 3)	82.96823 (101, 3)	88.44550 (101, 3)	95.84074 (101, 3)	105.36246 (101, 3)
353600.0 /	80.21847 (101, 3)	109.17090 (110, 5)	141.81865 (110, 5)	121.16138 (110, 5)	111.10970 (101, 3)
353500.0 /	82.20911 (101, 3)	198.13605 (110, 5)	281.13885 (110, 5)	277.07056 (110, 5)	220.30821 (110, 5)
353400.0 /	197.03551 (110, 5)	301.33423 (110, 5)	365.21936 (110, 5)	380.56833 (110, 5)	343.65399 (110, 5)
353300.0 /	275.97775 (110, 5)	356.22241 (110, 5)	380.71411 (110, 5)	392.01828 (110, 5)	385.93243 (110, 5)
353200.0 /	429.29382 (273, 4)	334.87817 (110, 5)	348.02893 (110, 5)	349.14612 (110, 5)	358.12888 (110, 5)
353100.0 /	584.90125 (273, 4)	422.00000 (273, 4)	291.56058 (110, 5)	290.30457 (110, 5)	299.87964 (110, 5)
353000.0 /	675.08899 (273, 4)	557.63757 (273, 4)	350.26947 (273, 4)	233.30505 (110, 5)	239.07011 (110, 5)
352900.0 /	702.77460 (273, 4)	643.60254 (273, 4)	461.73267 (273, 4)	270.02692 (273, 4)	229.87878 (100, 4)
352800.0 /	685.37402 (273, 4)	679.57568 (273, 4)	541.50555 (273, 4)	358.09949 (273, 4)	206.94218 (100, 4)
352700.0 /	641.17749 (273, 4)	676.20898 (273, 4)	585.84229 (273, 4)	428.08154 (273, 4)	270.20016 (273, 4)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 724.50140 AND OCCURRED AT (438700.0, 354400.0) *

Y-AXIS / (METERS) /	X-AXIS (METERS)				
	438500.0	438600.0	438700.0	438800.0	438900.0
354700.0 /	214.22519 (110, 4)	190.97101 (110, 4)	186.23489 (207, 5)	288.14874 (207, 5)	391.62302 (207, 5)
354600.0 /	204.85446 (207, 4)	242.64755 (207, 5)	373.25519 (207, 5)	493.72128 (207, 5)	576.68805 (207, 5)
354500.0 /	311.55881 (207, 5)	473.36276 (207, 5)	602.93835 (207, 5)	669.54419 (207, 5)	671.07349 (207, 5)
354400.0 /	571.07898 (207, 5)	692.87177 (207, 5)	724.50140 (207, 5)	683.60815 (207, 5)	602.64215 (207, 5)
354300.0 /	714.01404 (207, 5)	700.99695 (207, 5)	623.58990 (207, 5)	523.15894 (207, 5)	424.83139 (207, 5)
354200.0 /	568.07050 (207, 5)	484.27487 (207, 5)	392.64911 (207, 5)	386.28073 (100, 5)	392.19635 (100, 5)
354100.0 /	552.06763 (100, 5)	578.53223 (100, 5)	581.32336 (100, 5)	568.43726 (100, 5)	599.55029 (112, 5)
354000.0 /	719.51672 (100, 5)	717.72113 (100, 5)	691.15283 (100, 5)	651.95886 (100, 5)	608.71106 (112, 5)
353900.0 /	612.10767 (100, 5)	616.93848 (100, 5)	598.06232 (100, 5)	566.88660 (100, 5)	530.05609 (100, 5)
353800.0 /	324.46710 (100, 5)	355.90894 (100, 5)	368.23053 (100, 5)	367.56381 (100, 5)	358.41541 (100, 5)
353700.0 /	116.68265 (180, 4)	136.38730 (100, 5)	159.91772 (100, 5)	176.40025 (100, 5)	186.54985 (100, 5)
353600.0 /	118.66510 (101, 3)	116.49681 (101, 3)	124.71632 (180, 8)	154.52907 (180, 8)	171.63394 (180, 8)
353500.0 /	154.86670 (110, 5)	116.84703 (101, 3)	134.17104 (180, 8)	161.65659 (180, 8)	175.09805 (180, 8)
353400.0 /	275.69620 (110, 5)	203.23306 (110, 5)	143.18173 (180, 8)	167.94444 (180, 8)	177.66122 (180, 8)
353300.0 /	349.57190 (110, 5)	290.39142 (110, 5)	225.10033 (110, 5)	173.35582 (180, 8)	179.36630 (180, 8)
353200.0 /	357.29150 (110, 5)	331.44714 (110, 5)	284.65607 (110, 5)	229.75049 (110, 5)	180.26733 (180, 8)
353100.0 /	319.53058 (110, 5)	327.43649 (110, 5)	310.60339 (110, 5)	273.24966 (110, 5)	226.77655 (110, 5)
353000.0 /	262.21100 (110, 5)	291.64941 (110, 5)	305.79861 (110, 5)	294.59259 (110, 5)	263.09204 (110, 5)
352900.0 /	232.11316 (100, 4)	239.02628 (110, 5)	274.82294 (110, 5)	292.36252 (110, 5)	284.22342 (110, 5)
352800.0 /	233.68845 (100, 4)	224.37051 (100, 4)	226.67389 (110, 5)	265.67322 (110, 5)	284.54327 (110, 5)
352700.0 /	213.86203 (100, 4)	226.39249 (100, 4)	210.42291 (100, 4)	221.03720 (110, 5)	260.92062 (110, 5)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 724.50140 AND OCCURRED AT (438700.0, 354400.0) *

Y-AXIS / (METERS) /	X-AXIS (METERS)		
	439000.0	439100.0	439200.0
354700.0 /	476.07861 (207, 5)	527.58209 (207, 5)	542.83667 (207, 5)
354600.0 /	610.34967 (207, 5)	599.07422 (207, 5)	556.06409 (207, 5)
354500.0 /	624.84998 (207, 5)	552.89355 (207, 5)	472.94299 (207, 5)
354400.0 /	508.99347 (207, 5)	419.16656 (207, 5)	340.60648 (207, 5)
354300.0 /	339.45877 (207, 5)	269.61383 (207, 5)	258.42999 (100, 5)
354200.0 /	389.89011 (100, 5)	434.48260 (112, 5)	479.63071 (112, 5)
354100.0 /	623.63196 (112, 5)	627.34204 (112, 5)	616.52258 (112, 5)
354000.0 /	587.35107 (112, 5)	558.99231 (112, 5)	527.21826 (112, 5)
353900.0 /	491.52313 (100, 5)	453.59399 (100, 5)	417.56958 (100, 5)
353800.0 /	344.07208 (100, 5)	326.85846 (100, 5)	308.37466 (100, 5)
353700.0 /	191.45367 (100, 5)	192.27811 (100, 5)	190.09856 (100, 5)
353600.0 /	171.77336 (180, 8)	157.48199 (180, 8)	151.92250 (112, 4)
353500.0 /	171.71051 (180, 8)	155.20032 (180, 8)	152.80490 (112, 4)
353400.0 /	170.98692 (180, 8)	152.58807 (180, 8)	129.91263 (180, 8)
353300.0 /	169.67859 (180, 8)	149.70660 (180, 8)	126.73035 (180, 8)
353200.0 /	167.86020 (180, 8)	146.61049 (180, 8)	123.62984 (112, 6)
353100.0 /	180.63098 (110, 5)	143.34772 (180, 8)	120.25610 (180, 8)
353000.0 /	222.14017 (110, 5)	180.57549 (110, 5)	143.17206 (110, 5)
352900.0 /	256.11121 (110, 5)	218.47632 (110, 5)	179.79794 (110, 5)
352800.0 /	277.99786 (110, 5)	251.98294 (110, 5)	216.43431 (110, 5)
352700.0 /	279.86914 (110, 5)	274.20670 (110, 5)	249.75421 (110, 5)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 668.64221 AND OCCURRED AT (438400.0, 354000.0) *

Y-AXIS (METERS) /	X-AXIS (METERS)				
	437500.0	437600.0	437700.0	437800.0	437900.0
354700.0 /	53.50818 (207, 4)	105.26517 (110, 4)	140.87848 (207, 4)	150.04764 (207, 4)	136.79626 (207, 4)
354600.0 /	51.20547 (101, 3)	65.88618 (207, 4)	84.83220 (207, 4)	90.45308 (207, 4)	77.43354 (207, 4)
354500.0 /	51.04008 (101, 3)	48.01003 (110, 4)	65.71253 (101, 3)	70.21812 (101, 3)	53.52244 (110, 4)
354400.0 /	50.87573 (101, 3)	52.37605 (180, 5)	65.32585 (101, 3)	61.24740 (110, 4)	16.29640 (101, 8)
354300.0 /	50.71370 (101, 3)	44.10421 (180, 5)	15.92779 (110, 4)	10.99502 (110, 4)	16.15911 (101, 8)
354200.0 /	50.55574 (101, 3)	20.22494 (180, 5)	4.04166 (101, 8)	8.42359 (101, 8)	16.02331 (101, 8)
354100.0 /	3.06565 (273, 3)	2.86479 (273, 3)	4.04753 (101, 8)	8.38894 (101, 8)	15.88903 (101, 8)
354000.0 /	3.03945 (273, 3)	2.84367 (273, 3)	4.05285 (101, 8)	8.35409 (101, 8)	15.75623 (101, 8)
353900.0 /	3.01458 (273, 3)	2.82431 (273, 3)	4.05764 (101, 8)	8.31904 (101, 8)	15.62490 (101, 8)
353800.0 /	2.99113 (273, 3)	2.80693 (273, 3)	4.06192 (101, 8)	8.28381 (101, 8)	15.49503 (101, 8)
353700.0 /	2.96925 (273, 3)	2.79173 (273, 3)	4.06571 (101, 8)	8.24841 (101, 8)	15.36661 (101, 8)
353600.0 /	2.94910 (273, 3)	2.77929 (273, 3)	4.06899 (101, 8)	8.21288 (101, 8)	15.23960 (101, 8)
353500.0 /	2.93546 (273, 3)	3.97943 (273, 5)	11.01505 (273, 5)	16.66813 (273, 4)	26.20090 (273, 4)
353400.0 /	4.45911 (273, 5)	20.77422 (273, 5)	55.64506 (273, 5)	71.33565 (101, 3)	77.81915 (101, 3)
353300.0 /	17.83624 (273, 5)	57.68055 (101, 3)	65.12384 (101, 3)	127.25185 (273, 5)	132.79369 (110, 5)
353200.0 /	50.11291 (101, 3)	58.00286 (101, 3)	84.43070 (273, 4)	221.78922 (273, 5)	146.59030 (273, 5)
353100.0 /	67.74767 (273, 6)	84.85194 (273, 3)	112.09762 (273, 4)	305.71487 (273, 5)	212.74557 (273, 5)
353000.0 /	107.47942 (273, 6)	123.78458 (273, 3)	127.79424 (273, 4)	344.97751 (273, 4)	265.35214 (273, 5)
352900.0 /	144.06781 (273, 6)	158.48260 (273, 3)	133.06496 (273, 4)	336.08273 (273, 4)	302.22079 (273, 5)
352800.0 /	172.61986 (273, 6)	185.89789 (273, 3)	131.09631 (273, 4)	313.25650 (273, 4)	324.76471 (273, 5)
352700.0 /	191.69266 (273, 6)	205.35599 (273, 3)	124.80389 (273, 4)	284.42352 (273, 4)	335.60736 (273, 5)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 668.64221 AND OCCURRED AT (438400.0, 354000.0) *

Y-AXIS / (METERS) /	X-AXIS (METERS)				
	438000.0	438100.0	438200.0	438300.0	438400.0
354700.0 /	72.28697 (101, 3)	69.56793 (101, 3)	68.44984 (101, 8)	104.29066 (110, 4)	187.63065 (110, 4)
354600.0 /	72.17834 (101, 3)	69.96864 (101, 3)	67.50140 (101, 8)	138.85706 (110, 4)	176.67926 (110, 4)
354500.0 /	72.18929 (101, 3)	70.54564 (101, 3)	81.16420 (110, 4)	124.71233 (110, 4)	163.97128 (207, 5)
354400.0 /	72.33679 (101, 3)	71.31497 (101, 3)	70.17136 (101, 3)	193.09770 (207, 5)	230.72148 (207, 4)
354300.0 /	51.16877 (207, 4)	72.29051 (101, 3)	197.00656 (207, 5)	212.28445 (207, 4)	188.91325 (110, 4)
354200.0 /	27.82358 (101, 8)	73.48352 (101, 3)	99.99451 (180, 4)	233.01476 (180, 4)	324.39963 (180, 4)
354100.0 /	34.03289 (207, 5)	74.90252 (101, 3)	263.92261 (180, 4)	367.16577 (100, 5)	488.88092 (100, 5)
354000.0 /	27.19591 (101, 8)	76.55399 (101, 3)	284.91791 (100, 5)	539.95984 (100, 5)	668.64221 (180, 4)
353900.0 /	26.88984 (101, 8)	78.44357 (101, 3)	211.11015 (100, 5)	434.47150 (100, 5)	544.48096 (180, 4)
353800.0 /	26.58881 (101, 8)	41.86295 (101, 8)	85.01038 (101, 3)	171.23203 (100, 5)	265.52991 (100, 5)
353700.0 /	26.29273 (101, 8)	41.32587 (101, 8)	59.67825 (101, 8)	79.19459 (101, 8)	96.59137 (101, 8)
353600.0 /	36.32624 (110, 5)	85.63046 (101, 3)	92.22314 (101, 3)	100.87374 (101, 3)	95.51894 (101, 8)
353500.0 /	77.03989 (110, 5)	88.58889 (101, 3)	96.37668 (101, 3)	106.25525 (101, 3)	116.80949 (101, 3)
353400.0 /	84.46004 (101, 3)	91.87437 (101, 3)	100.93010 (101, 3)	111.91779 (101, 3)	122.27260 (101, 3)
353300.0 /	239.62549 (273, 4)	113.35454 (273, 4)	110.25121 (100, 4)	117.75172 (101, 3)	127.29800 (101, 3)
353200.0 /	261.79962 (110, 5)	258.80414 (273, 4)	154.48581 (100, 4)	162.33272 (100, 4)	131.69142 (101, 3)
353100.0 /	204.33517 (110, 5)	272.15115 (110, 5)	223.62149 (273, 4)	203.98906 (100, 4)	192.19339 (100, 4)
353000.0 /	228.31119 (273, 5)	203.72685 (110, 5)	230.16367 (110, 5)	208.28024 (100, 4)	227.86127 (100, 4)
352900.0 /	255.29266 (273, 5)	254.57561 (273, 5)	189.19994 (273, 5)	184.84232 (100, 4)	187.48065 (110, 5)
352800.0 /	267.37964 (273, 5)	278.08997 (273, 5)	251.56187 (273, 5)	156.93913 (273, 5)	202.25903 (273, 4)
352700.0 /	270.90765 (273, 5)	279.36252 (273, 5)	286.70709 (273, 5)	220.57278 (273, 5)	171.84842 (100, 4)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 668.64221 AND OCCURRED AT (438400.0, 354000.0) *

Y-AXIS (METERS) /	X-AXIS (METERS)				
	438500.0	438600.0	438700.0	438800.0	438900.0
354700.0 /	186.90331 (207, 4)	154.59041 (207, 4)	164.15506 (110, 4)	156.96355 (110, 4)	165.37502 (110, 4)
354600.0 /	167.86261 (110, 4)	159.49652 (110, 4)	170.87700 (110, 4)	191.97539 (110, 4)	209.34312 (110, 4)
354500.0 /	196.55479 (207, 4)	187.52446 (110, 4)	221.08585 (110, 4)	240.51189 (110, 4)	243.10934 (110, 4)
354400.0 /	199.61273 (110, 4)	242.55087 (110, 4)	260.17236 (110, 4)	255.20844 (110, 4)	266.79504 (112, 4)
354300.0 /	235.76074 (110, 4)	249.37750 (110, 4)	267.09055 (112, 4)	264.36359 (112, 4)	239.65929 (112, 4)
354200.0 /	349.93018 (180, 4)	342.05975 (100, 5)	370.13217 (100, 5)	310.68698 (207, 5)	296.74976 (112, 5)
354100.0 /	527.34711 (180, 4)	455.91379 (180, 4)	468.56635 (112, 5)	549.16827 (112, 5)	545.55670 (100, 5)
354000.0 /	596.35864 (180, 4)	565.41589 (112, 5)	607.41229 (112, 5)	617.81329 (112, 5)	607.21051 (100, 5)
353900.0 /	492.86682 (180, 4)	409.95868 (180, 4)	358.11972 (112, 5)	365.31088 (112, 5)	362.49338 (112, 5)
353800.0 /	289.17889 (180, 4)	258.39117 (180, 4)	220.30020 (180, 4)	227.69043 (112, 4)	231.16479 (112, 4)
353700.0 /	114.04571 (101, 3)	120.37124 (180, 4)	116.23107 (112, 4)	146.62225 (180, 8)	167.24049 (180, 8)
353600.0 /	107.39733 (101, 8)	111.14819 (101, 8)	105.89900 (101, 8)	101.93811 (112, 4)	127.11620 (112, 4)
353500.0 /	122.56721 (101, 3)	110.63165 (101, 8)	105.92602 (101, 8)	93.48776 (101, 8)	76.06934 (101, 8)
353400.0 /	125.59563 (101, 3)	116.19786 (101, 3)	141.74231 (110, 5)	95.57335 (110, 5)	92.77044 (112, 6)
353300.0 /	127.64105 (101, 3)	119.83961 (180, 8)	151.63306 (180, 8)	166.09357 (110, 5)	118.57207 (110, 5)
353200.0 /	128.64859 (101, 3)	129.37814 (180, 8)	159.42853 (180, 8)	177.87558 (180, 8)	177.28659 (110, 5)
353100.0 /	147.47476 (100, 4)	138.60287 (180, 8)	166.49220 (180, 8)	181.50787 (180, 8)	180.42619 (180, 8)
353000.0 /	202.36688 (100, 4)	153.61118 (100, 4)	172.76878 (180, 8)	184.27310 (180, 8)	179.90923 (180, 8)
352900.0 /	204.65593 (110, 5)	199.54288 (100, 4)	178.22269 (180, 8)	186.20523 (180, 8)	178.78549 (180, 8)
352800.0 /	157.03857 (110, 5)	184.67979 (110, 5)	189.50214 (100, 4)	187.34879 (180, 8)	177.12369 (180, 8)
352700.0 /	150.49326 (273, 4)	170.27954 (180, 8)	186.61078 (180, 8)	187.75627 (180, 8)	174.99142 (180, 8)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 668.64221 AND OCCURRED AT (438400.0, 354000.0) *

Y-AXIS / X-AXIS (METERS)
(METERS) / 439000.0 439100.0 439200.0

354700.0 /	177.83568 (110, 4)	186.40179 (110, 4)	188.16479 (110, 4)
354600.0 /	216.62051 (110, 4)	213.46863 (110, 4)	204.69200 (100, 6)
354500.0 /	232.30869 (110, 4)	243.45239 (112, 4)	245.31555 (112, 4)
354400.0 /	266.00797 (112, 4)	247.43835 (112, 4)	219.38817 (112, 4)
354300.0 /	246.09947 (100, 5)	254.55884 (100, 5)	216.86295 (112, 5)
354200.0 /	372.61975 (112, 5)	381.45300 (100, 5)	368.84531 (100, 5)
354100.0 /	516.87769 (100, 5)	485.41693 (100, 5)	453.29184 (100, 5)
354000.0 /	561.13525 (100, 5)	516.20612 (100, 5)	473.81943 (100, 5)
353900.0 /	353.13376 (112, 5)	339.78369 (112, 5)	324.22815 (112, 5)
353800.0 /	229.32202 (112, 4)	223.93510 (112, 4)	216.32278 (112, 4)
353700.0 /	171.10052 (180, 8)	159.36549 (180, 8)	154.86208 (112, 4)
353600.0 /	143.12747 (112, 4)	150.70222 (112, 4)	136.03827 (180, 8)
353500.0 /	98.65343 (112, 4)	129.47708 (112, 4)	133.02556 (180, 8)
353400.0 /	87.89403 (112, 6)	72.37103 (112, 6)	81.51986 (112, 4)
353300.0 /	105.97454 (112, 6)	122.45486 (112, 6)	120.45123 (112, 6)
353200.0 /	132.60251 (110, 5)	97.10501 (110, 5)	123.50443 (180, 8)
353100.0 /	165.60320 (180, 8)	139.87238 (110, 5)	107.70535 (180, 3)
353000.0 /	162.97498 (180, 8)	139.96033 (180, 8)	124.45804 (180, 3)
352900.0 /	160.03772 (180, 8)	136.48428 (180, 8)	113.75906 (180, 8)
352800.0 /	156.84814 (180, 8)	132.95030 (180, 8)	110.53595 (180, 8)
352700.0 /	153.45732 (180, 8)	129.38435 (180, 8)	108.13177 (180, 4)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* 50 MAXIMUM 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *

* FROM ALL SOURCES *

RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y(METERS) OR DIRECTION (DEGREES)	RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y(METERS) OR DIRECTION (DEGREES)
1	724.50140	5	207	438700.0	354400.0	26	620.85107	5	207	438400.0	354300.0
2	719.51672	5	100	438500.0	354000.0	27	617.81329	5	112	438800.0	354000.0
3	717.72113	5	100	438600.0	354000.0	28	616.93848	5	100	438600.0	353900.0
4	714.01404	5	207	438500.0	354300.0	29	616.52258	5	112	439200.0	354100.0
5	702.77460	4	273	438000.0	352900.0	30	612.10767	5	100	438500.0	353900.0
6	700.99695	5	207	438600.0	354300.0	31	610.34967	5	207	439000.0	354600.0
7	692.87177	5	207	438600.0	354400.0	32	608.71106	5	112	438900.0	354000.0
8	691.15283	5	100	438700.0	354000.0	33	607.41229	5	112	438700.0	354000.0
9	685.37402	4	273	438000.0	352800.0	34	607.21051	5	100	438900.0	354000.0
10	683.60815	5	207	438800.0	354400.0	35	606.16602	5	207	438400.0	354200.0
11	679.57568	4	273	438100.0	352800.0	36	602.93835	5	207	438700.0	354500.0
12	676.20898	4	273	438100.0	352700.0	37	602.64215	5	207	438900.0	354400.0
13	675.08899	4	273	438000.0	353000.0	38	599.55029	5	112	438900.0	354100.0
14	673.99487	5	100	438400.0	354000.0	39	599.07422	5	207	439100.0	354600.0
15	671.07349	5	207	438900.0	354500.0	40	598.06232	5	100	438700.0	353900.0
16	669.54419	5	207	438800.0	354500.0	41	596.35864	4	180	438500.0	354000.0
17	668.64221	4	180	438400.0	354000.0	42	587.35107	5	112	439000.0	354000.0
18	651.95886	5	100	438800.0	354000.0	43	587.30206	4	273	437900.0	353000.0
19	643.60254	4	273	438100.0	352900.0	44	585.84229	4	273	438200.0	352700.0
20	641.17749	4	273	438000.0	352700.0	45	584.90125	4	273	438000.0	353100.0
21	627.34204	5	112	439100.0	354100.0	46	581.32336	5	100	438700.0	354100.0
22	624.84998	5	207	439000.0	354500.0	47	578.53223	5	100	438600.0	354100.0
23	623.63196	5	112	439000.0	354100.0	48	576.68805	5	207	438900.0	354600.0
24	623.58990	5	207	438700.0	354300.0	49	575.09973	4	273	437900.0	352900.0
25	623.13715	4	180	438300.0	354000.0	50	571.07898	5	207	438500.0	354400.0

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 129.67303 AND OCCURRED AT (439200.0, 354100.0) *

Y-AXIS / (METERS) /	X-AXIS (METERS)				
	438000.0	438100.0	438200.0	438300.0	438400.0
354700.0 /	12.85611 (101, 1)	14.70102 (101, 1)	20.74823 (207, 1)	25.82735 (207, 1)	28.05002 (207, 1)
354600.0 /	12.77416 (101, 1)	20.76383 (207, 1)	30.78671 (207, 1)	35.92760 (207, 1)	38.35597 (207, 1)
354500.0 /	12.84011 (207, 1)	29.10699 (207, 1)	41.41909 (207, 1)	47.66196 (207, 1)	53.71335 (207, 1)
354400.0 /	12.67281 (207, 1)	32.71596 (207, 1)	49.33401 (207, 1)	62.35221 (207, 1)	77.19724 (207, 1)
354300.0 /	12.65523 (101, 1)	27.41401 (207, 1)	54.41833 (207, 1)	79.49981 (207, 1)	96.71490 (207, 1)
354200.0 /	12.66263 (101, 1)	23.24803 (207, 1)	56.32862 (207, 1)	79.02724 (207, 1)	83.53117 (207, 1)
354100.0 /	12.69594 (101, 1)	20.38551 (207, 1)	38.36492 (207, 1)	60.79395 (180, 1)	83.17758 (100, 1)
354000.0 /	12.75642 (101, 1)	15.40500 (180, 1)	49.24850 (180, 1)	89.64385 (100, 1)	114.86919 (100, 1)
353900.0 /	12.84514 (101, 1)	15.12514 (101, 1)	37.18784 (180, 1)	72.07977 (100, 1)	94.20071 (100, 1)
353800.0 /	12.96301 (101, 1)	15.31978 (101, 1)	18.19851 (101, 1)	29.77640 (180, 1)	42.01593 (100, 1)
353700.0 /	13.11082 (101, 1)	15.54837 (101, 1)	18.52437 (101, 1)	21.88619 (101, 1)	25.24934 (101, 1)
353600.0 /	13.28943 (101, 1)	15.81281 (101, 1)	18.89531 (101, 1)	22.38744 (101, 1)	25.83257 (101, 1)
353500.0 /	13.49997 (101, 1)	24.76701 (110, 1)	35.14236 (110, 1)	34.63382 (110, 1)	27.53853 (110, 1)
353400.0 /	24.62944 (110, 1)	37.66678 (110, 1)	45.65242 (110, 1)	47.57104 (110, 1)	42.95675 (110, 1)
353300.0 /	37.54012 (273, 1)	44.52780 (110, 1)	47.58926 (110, 1)	49.00229 (110, 1)	48.24155 (110, 1)
353200.0 /	69.64089 (273, 1)	41.85977 (110, 1)	43.50362 (110, 1)	43.64326 (110, 1)	44.76611 (110, 1)
353100.0 /	97.74953 (273, 1)	71.23024 (273, 1)	37.73353 (273, 1)	36.28807 (110, 1)	37.48495 (110, 1)
353000.0 /	115.23077 (273, 1)	97.84726 (273, 1)	61.75346 (273, 1)	31.92000 (273, 1)	29.88376 (110, 1)
352900.0 /	122.21223 (273, 1)	115.39519 (273, 1)	85.34100 (273, 1)	50.19014 (273, 1)	28.73485 (100, 1)
352800.0 /	121.70303 (273, 1)	122.99385 (273, 1)	103.26687 (273, 1)	69.62600 (273, 1)	40.59542 (273, 1)
352700.0 /	116.78649 (273, 1)	122.89373 (273, 1)	113.36034 (273, 1)	86.44655 (273, 1)	55.82142 (273, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 129.67303 AND OCCURRED AT (439200.0, 354100.0) *

Y-AXIS (METERS) /	X-AXIS (METERS)				
	437500.0	437600.0	437700.0	437800.0	437900.0
354700.0 /	14.34894 (180, 1)	15.43522 (207, 1)	28.50649 (110, 1)	32.33830 (110, 1)	20.20519 (110, 1)
354600.0 /	19.58526 (180, 1)	10.04053 (110, 1)	24.64603 (110, 1)	26.64001 (110, 1)	13.63821 (110, 1)
354500.0 /	25.31692 (180, 1)	7.80355 (101, 1)	17.63557 (110, 1)	17.62143 (110, 1)	11.20350 (101, 1)
354400.0 /	28.43338 (180, 1)	7.73292 (101, 1)	8.80375 (101, 1)	9.90044 (101, 1)	11.13744 (101, 1)
354300.0 /	22.55778 (180, 1)	7.66977 (101, 1)	8.73531 (101, 1)	9.83507 (101, 1)	11.08780 (101, 1)
354200.0 /	8.03846 (180, 1)	7.61363 (101, 1)	8.67568 (101, 1)	9.78197 (101, 1)	11.05585 (101, 1)
354100.0 /	6.50064 (101, 1)	7.56426 (101, 1)	8.62517 (101, 1)	9.74209 (101, 1)	11.04304 (101, 1)
354000.0 /	6.46426 (101, 1)	7.52168 (101, 1)	8.58436 (101, 1)	9.71661 (101, 1)	11.05088 (101, 1)
353900.0 /	6.43301 (101, 1)	7.48614 (101, 1)	8.55407 (101, 1)	9.70688 (101, 1)	11.08090 (101, 1)
353800.0 /	6.40689 (101, 1)	7.45813 (101, 1)	8.53536 (101, 1)	9.71439 (101, 1)	11.13457 (101, 1)
353700.0 /	6.38613 (101, 1)	7.43838 (101, 1)	8.52947 (101, 1)	9.74066 (101, 1)	11.21323 (101, 1)
353600.0 /	6.37109 (101, 1)	7.42779 (101, 1)	8.53778 (101, 1)	9.78724 (101, 1)	11.31810 (101, 1)
353500.0 /	6.36241 (101, 1)	7.42748 (101, 1)	8.56176 (101, 1)	9.85562 (101, 1)	11.45028 (101, 1)
353400.0 /	6.36089 (101, 1)	7.43870 (101, 1)	10.12402 (273, 1)	17.44181 (273, 1)	20.68079 (273, 1)
353300.0 /	6.36749 (101, 1)	13.52965 (273, 1)	25.80114 (273, 1)	40.27030 (273, 1)	48.31323 (273, 1)
353200.0 /	13.04926 (273, 1)	29.32667 (273, 1)	44.91356 (273, 1)	63.61060 (273, 1)	76.79609 (273, 1)
353100.0 /	26.69407 (273, 1)	47.52047 (273, 1)	62.37471 (273, 1)	81.16302 (273, 1)	97.42626 (273, 1)
353000.0 /	42.68214 (273, 1)	64.15115 (273, 1)	75.59450 (273, 1)	91.61127 (273, 1)	108.42615 (273, 1)
352900.0 /	57.96731 (273, 1)	77.08207 (273, 1)	84.14315 (273, 1)	96.17598 (273, 1)	111.72247 (273, 1)
352800.0 /	70.60829 (273, 1)	85.82072 (273, 1)	88.66507 (273, 1)	96.63625 (273, 1)	109.96690 (273, 1)
352700.0 /	79.87347 (273, 1)	90.79192 (273, 1)	90.11593 (273, 1)	94.51784 (273, 1)	105.32964 (273, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 129.67303 AND OCCURRED AT (439200.0, *354100.0) *

Y-AXIS / (METERS) /	X-AXIS (METERS)				
	438500.0	438600.0	438700.0	438800.0	438900.0
354700.0 /	29.50639 (207, 1)	32.74179 (207, 1)	39.69131 (207, 1)	50.86105 (207, 1)	63.85593 (207, 1)
354600.0 /	42.32560 (207, 1)	50.87437 (207, 1)	63.85318 (207, 1)	77.00159 (207, 1)	85.23830 (207, 1)
354500.0 /	64.44908 (207, 1)	78.75549 (207, 1)	90.47552 (207, 1)	94.75488 (207, 1)	91.53048 (207, 1)
354400.0 /	92.33533 (207, 1)	100.82488 (207, 1)	99.64541 (207, 1)	91.18858 (207, 1)	79.35477 (207, 1)
354300.0 /	101.40851 (207, 1)	94.89651 (207, 1)	82.31422 (207, 1)	68.36286 (207, 1)	63.61854 (100, 1)
354200.0 /	75.76816 (207, 1)	71.10934 (100, 1)	79.58449 (100, 1)	84.34489 (100, 1)	86.16611 (100, 1)
354100.0 /	99.12209 (100, 1)	107.74702 (100, 1)	110.89085 (100, 1)	110.31721 (100, 1)	117.97655 (112, 1)
354000.0 /	125.65123 (100, 1)	127.69781 (100, 1)	124.87182 (100, 1)	120.20494 (112, 1)	122.17374 (112, 1)
353900.0 /	103.79082 (100, 1)	105.81990 (100, 1)	103.70300 (100, 1)	99.50558 (100, 1)	94.44516 (100, 1)
353800.0 /	52.23333 (100, 1)	58.09449 (100, 1)	60.79365 (100, 1)	61.35910 (100, 1)	60.58476 (100, 1)
353700.0 /	27.79685 (101, 1)	28.34723 (101, 1)	28.77595 (180, 1)	31.58415 (180, 1)	33.15746 (180, 1)
353600.0 /	28.26078 (101, 1)	28.45782 (101, 1)	25.93405 (101, 1)	26.44111 (180, 1)	28.71536 (180, 1)
353500.0 /	28.63453 (101, 1)	28.43653 (101, 1)	25.59402 (101, 1)	26.38780 (180, 1)	28.84287 (180, 1)
353400.0 /	34.46202 (110, 1)	28.28769 (101, 1)	25.18191 (101, 1)	29.57253 (180, 1)	32.57095 (180, 1)
353300.0 /	43.69649 (110, 1)	36.29893 (110, 1)	28.13754 (110, 1)	32.85295 (180, 1)	36.95657 (180, 1)
353200.0 /	44.66144 (110, 1)	41.43089 (110, 1)	35.58201 (110, 1)	34.13385 (180, 1)	39.36762 (180, 1)
353100.0 /	39.94132 (110, 1)	40.92956 (110, 1)	38.82542 (110, 1)	34.15621 (110, 1)	38.87919 (180, 1)
353000.0 /	32.77637 (110, 1)	36.45618 (110, 1)	38.22483 (110, 1)	36.82407 (110, 1)	36.35452 (180, 1)
352900.0 /	29.01414 (100, 1)	29.87828 (110, 1)	34.35287 (110, 1)	36.54531 (110, 1)	35.52793 (110, 1)
352800.0 /	29.21106 (100, 1)	28.04631 (100, 1)	28.33424 (110, 1)	33.20915 (110, 1)	35.56791 (110, 1)
352700.0 /	33.86489 (273, 1)	28.29906 (100, 1)	26.30286 (100, 1)	27.62965 (110, 1)	32.61508 (110, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 129.67303 AND OCCURRED AT (439200.0, 354100.0) *

Y-AXIS /			X-AXIS (METERS)
(METERS) /	439000.0	439100.0	439200.0

354700.0 /	74.35326 (207, 1)	79.40273 (207, 1)	78.92955 (207, 1)
354600.0 /	86.67995 (207, 1)	82.66935 (207, 1)	75.63223 (207, 1)
354500.0 /	83.52963 (207, 1)	73.64313 (207, 1)	63.85994 (207, 1)
354400.0 /	67.19551 (207, 1)	56.38499 (207, 1)	52.92637 (100, 1)
354300.0 /	66.01308 (100, 1)	66.79657 (100, 1)	66.50305 (100, 1)
354200.0 /	85.94160 (100, 1)	97.63203 (112, 1)	107.44366 (112, 1)
354100.0 /	125.28198 (112, 1)	128.91029 (112, 1)	129.67303 (112, 1)
354000.0 /	121.46926 (112, 1)	118.96524 (112, 1)	115.31093 (112, 1)
353900.0 /	89.20627 (100, 1)	85.19641 (112, 1)	82.37694 (112, 1)
353800.0 /	59.03833 (100, 1)	57.09790 (100, 1)	55.00086 (100, 1)
353700.0 /	34.20624 (112, 1)	36.44424 (112, 1)	37.81604 (112, 1)
353600.0 /	28.79050 (180, 1)	29.93397 (112, 1)	32.85856 (112, 1)
353500.0 /	28.80242 (180, 1)	26.84028 (180, 1)	25.34591 (112, 1)
353400.0 /	32.78802 (180, 1)	30.83897 (180, 1)	27.80350 (180, 1)
353300.0 /	38.20933 (180, 1)	37.09408 (180, 1)	34.57078 (180, 1)
353200.0 /	42.10571 (180, 1)	42.56458 (180, 1)	41.42950 (180, 1)
353100.0 /	42.81481 (180, 1)	45.02538 (180, 1)	45.79583 (180, 1)
353000.0 /	40.49670 (180, 1)	43.87041 (180, 1)	46.42143 (180, 1)
352900.0 /	36.59940 (180, 1)	40.06210 (180, 1)	43.59143 (180, 1)
352800.0 /	34.74973 (110, 1)	35.24792 (180, 1)	38.71746 (180, 1)
352700.0 /	34.98364 (110, 1)	34.27584 (110, 1)	33.37448 (180, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 119.57732 AND OCCURRED AT (438800.0, 354000.0) *

Y-AXIS (METERS) /	X-AXIS (METERS)				
	437500.0	437600.0	437700.0	437800.0	437900.0
354700.0 /	7.11069 (207, 1)	13.15815 (110, 1)	18.43185 (207, 1)	18.89108 (207, 1)	17.10451 (207, 1)
354600.0 /	6.77402 (101, 1)	8.58169 (207, 1)	10.84070 (207, 1)	11.33224 (207, 1)	11.28494 (101, 1)
354500.0 /	6.70469 (101, 1)	6.00126 (110, 1)	8.88097 (101, 1)	9.97743 (101, 1)	6.69032 (110, 1)
354400.0 /	6.64365 (101, 1)	6.55644 (180, 1)	8.75223 (110, 1)	7.65593 (110, 1)	1.83796 (207, 1)
354300.0 /	6.58982 (101, 1)	5.52524 (180, 1)	1.99098 (110, 1)	1.37439 (110, 1)	1.01921 (273, 1)
354200.0 /	6.54236 (101, 1)	2.54379 (180, 1)	0.87996 (273, 1)	0.94865 (273, 1)	1.07400 (273, 1)
354100.0 /	0.84407 (273, 1)	0.86066 (273, 1)	0.90369 (273, 1)	0.98829 (273, 1)	1.13600 (273, 1)
354000.0 /	0.85173 (273, 1)	0.87664 (273, 1)	0.93185 (273, 1)	1.03380 (273, 1)	1.20533 (273, 1)
353900.0 /	0.86187 (273, 1)	0.89610 (273, 1)	0.96471 (273, 1)	1.08538 (273, 1)	1.28205 (273, 1)
353800.0 /	0.87476 (273, 1)	0.91932 (273, 1)	1.00255 (273, 1)	1.14320 (273, 1)	1.36609 (273, 1)
353700.0 /	0.89062 (273, 1)	0.94655 (273, 1)	1.04554 (273, 1)	1.20737 (273, 1)	1.45740 (273, 1)
353600.0 /	0.90971 (273, 1)	0.97976 (273, 1)	1.12750 (273, 1)	1.38711 (273, 1)	1.69622 (273, 1)
353500.0 /	0.94199 (273, 1)	1.24820 (273, 1)	2.46612 (273, 1)	4.20467 (273, 1)	5.15720 (273, 1)
353400.0 /	1.41057 (273, 1)	4.11172 (273, 1)	8.60296 (101, 1)	9.94722 (101, 1)	11.61087 (101, 1)
353300.0 /	4.54923 (273, 1)	7.46284 (101, 1)	8.66289 (101, 1)	10.06334 (101, 1)	16.59921 (110, 1)
353200.0 /	6.38332 (101, 1)	7.50134 (101, 1)	8.74308 (101, 1)	10.20529 (101, 1)	17.02347 (110, 1)
353100.0 /	6.40965 (101, 1)	7.55573 (101, 1)	8.84495 (101, 1)	10.37440 (101, 1)	13.46179 (110, 1)
353000.0 /	6.44782 (101, 1)	7.62750 (101, 1)	8.96995 (101, 1)	10.57221 (101, 1)	12.56827 (101, 1)
352900.0 /	6.49926 (101, 1)	7.71820 (101, 1)	9.11955 (101, 1)	10.80067 (101, 1)	12.89897 (101, 1)
352800.0 /	6.56544 (101, 1)	7.82942 (101, 1)	9.29553 (101, 1)	11.06224 (101, 1)	13.27359 (101, 1)
352700.0 /	6.64787 (101, 1)	7.96308 (101, 1)	9.50033 (101, 1)	11.36016 (101, 1)	13.69657 (101, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 119.57732 AND OCCURRED AT (438800.0, 354000.0) *

Y-AXIS (METERS) /	X-AXIS (METERS)				
	438000.0	438100.0	438200.0	438300.0	438400.0
354700.0 /	11.32730 (207, 1)	13.72445 (207, 1)	16.89512 (101, 1)	19.22188 (101, 1)	23.56035 (110, 1)
354600.0 /	10.69454 (207, 1)	14.65084 (101, 1)	16.90422 (101, 1)	19.32558 (101, 1)	22.93992 (110, 1)
354500.0 /	12.71246 (101, 1)	14.62803 (101, 1)	16.94675 (101, 1)	19.46407 (101, 1)	21.78802 (101, 1)
354400.0 /	12.67233 (101, 1)	14.63390 (101, 1)	17.02305 (101, 1)	19.63664 (101, 1)	22.08462 (101, 1)
354300.0 /	6.83158 (207, 1)	14.66958 (101, 1)	17.13320 (101, 1)	19.84295 (101, 1)	23.74392 (110, 1)
354200.0 /	3.44424 (207, 1)	14.73598 (101, 1)	17.27709 (101, 1)	30.17463 (180, 1)	42.89641 (100, 1)
354100.0 /	4.28394 (207, 1)	14.83375 (101, 1)	33.71698 (180, 1)	58.40833 (100, 1)	71.56129 (180, 1)
354000.0 /	1.47771 (180, 1)	14.96333 (101, 1)	47.22320 (100, 1)	79.33900 (180, 1)	86.05166 (180, 1)
353900.0 /	1.58555 (273, 1)	11.03803 (180, 1)	36.14622 (100, 1)	63.36254 (180, 1)	70.96875 (180, 1)
353800.0 /	1.70230 (273, 1)	3.05317 (180, 1)	13.65470 (180, 1)	26.71925 (100, 1)	39.40690 (180, 1)
353700.0 /	1.82647 (273, 1)	3.51454 (110, 1)	3.77954 (110, 1)	9.00201 (180, 1)	15.83400 (180, 1)
353600.0 /	4.54078 (110, 1)	13.64636 (110, 1)	17.72733 (110, 1)	15.14517 (110, 1)	10.51134 (110, 1)
353500.0 /	9.62999 (110, 1)	16.11595 (101, 1)	19.31534 (101, 1)	22.93437 (101, 1)	26.41112 (101, 1)
353400.0 /	13.74412 (101, 1)	16.46153 (101, 1)	19.78738 (101, 1)	23.51846 (101, 1)	26.96132 (101, 1)
353300.0 /	34.49722 (110, 1)	18.45292 (273, 1)	20.31193 (101, 1)	24.12595 (101, 1)	27.45806 (101, 1)
353200.0 /	32.72495 (110, 1)	41.70520 (273, 1)	20.88592 (101, 1)	24.73820 (101, 1)	27.87704 (101, 1)
353100.0 /	25.54190 (110, 1)	34.01889 (110, 1)	36.44507 (110, 1)	25.49863 (100, 1)	28.19707 (101, 1)
353000.0 /	18.18062 (110, 1)	25.46586 (110, 1)	28.77046 (110, 1)	29.16313 (110, 1)	28.48266 (100, 1)
352900.0 /	15.57967 (101, 1)	18.94843 (101, 1)	22.80441 (101, 1)	26.37257 (101, 1)	28.48097 (101, 1)
352800.0 /	16.09690 (101, 1)	19.59684 (101, 1)	23.45337 (101, 1)	26.77120 (101, 1)	28.43053 (101, 1)
352700.0 /	16.66983 (101, 1)	20.27921 (101, 1)	24.07071 (101, 1)	27.06336 (101, 1)	28.25272 (101, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 119.57732 AND OCCURRED AT (438800.0, 354000.0) *

Y-AXIS / (METERS) /	X-AXIS (METERS)				
	438500.0	438600.0	438700.0	438800.0	438900.0
354700.0 /	27.99229 (110, 1)	28.66466 (110, 1)	29.36872 (110, 1)	29.03369 (110, 1)	27.38431 (110, 1)
354600.0 /	24.74874 (110, 1)	26.52892 (110, 1)	27.45332 (110, 1)	27.61291 (110, 1)	27.74570 (110, 1)
354500.0 /	23.48367 (101, 1)	26.53870 (110, 1)	29.07406 (110, 1)	30.54857 (110, 1)	32.84018 (100, 1)
354400.0 /	25.95716 (110, 1)	30.67081 (110, 1)	32.95261 (100, 1)	40.47816 (100, 1)	46.14222 (100, 1)
354300.0 /	30.82686 (100, 1)	42.28259 (100, 1)	51.94128 (100, 1)	59.06174 (100, 1)	55.69577 (207, 1)
354200.0 /	58.66605 (100, 1)	63.33447 (207, 1)	50.86448 (207, 1)	58.07173 (112, 1)	71.65699 (112, 1)
354100.0 /	69.51178 (180, 1)	69.33920 (112, 1)	90.16885 (112, 1)	106.32381 (112, 1)	107.49860 (100, 1)
354000.0 /	83.83447 (112, 1)	102.31380 (112, 1)	114.46118 (112, 1)	119.57732 (100, 1)	113.27099 (100, 1)
353900.0 /	70.92989 (112, 1)	80.64606 (112, 1)	86.38710 (112, 1)	88.65951 (112, 1)	88.77919 (112, 1)
353800.0 /	41.84727 (180, 1)	41.31584 (180, 1)	43.16771 (112, 1)	47.40993 (112, 1)	50.07084 (112, 1)
353700.0 /	21.23141 (180, 1)	25.32519 (180, 1)	26.18369 (101, 1)	27.84432 (100, 1)	30.97175 (112, 1)
353600.0 /	11.89248 (180, 1)	17.19022 (180, 1)	22.32341 (180, 1)	21.47975 (101, 1)	21.54620 (112, 1)
353500.0 /	19.35834 (110, 1)	15.95026 (180, 1)	21.73342 (180, 1)	21.07175 (101, 1)	16.13489 (101, 1)
353400.0 /	28.89861 (101, 1)	25.40413 (110, 1)	24.14134 (180, 1)	20.65242 (101, 1)	15.84358 (101, 1)
353300.0 /	29.03946 (101, 1)	28.02147 (101, 1)	26.39116 (180, 1)	20.76170 (110, 1)	15.56958 (101, 1)
353200.0 /	29.05028 (101, 1)	27.65228 (101, 1)	27.08163 (180, 1)	28.71881 (110, 1)	22.16082 (110, 1)
353100.0 /	28.93110 (101, 1)	27.19723 (101, 1)	26.68342 (180, 1)	33.29174 (180, 1)	28.34707 (110, 1)
353000.0 /	28.68812 (101, 1)	26.67445 (101, 1)	26.11131 (180, 1)	31.50626 (180, 1)	32.88651 (110, 1)
352900.0 /	28.33256 (101, 1)	26.10183 (101, 1)	25.68079 (180, 1)	29.74673 (180, 1)	33.26006 (180, 1)
352800.0 /	27.87921 (101, 1)	25.49604 (101, 1)	25.35160 (180, 1)	28.25427 (180, 1)	30.44263 (180, 1)
352700.0 /	27.34500 (101, 1)	24.87182 (101, 1)	25.14046 (180, 1)	26.98007 (180, 1)	28.05344 (180, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 119.57732 AND OCCURRED AT (438800.0, 354000.0) *

Y-AXIS (METERS) /	439000.0	439100.0	X-AXIS (METERS) 439200.0
354700.0 /	25.81499 (110, 1)	27.45146 (112, 1)	30.22731 (112, 1)
354600.0 /	27.93483 (112, 1)	31.23623 (100, 1)	34.35812 (100, 1)
354500.0 /	37.58625 (100, 1)	40.81181 (100, 1)	42.67881 (100, 1)
354400.0 /	49.90216 (100, 1)	52.03120 (100, 1)	47.52078 (207, 1)
354300.0 /	46.67337 (112, 1)	53.69573 (112, 1)	62.49290 (112, 1)
354200.0 /	85.37954 (112, 1)	84.44564 (100, 1)	82.25813 (100, 1)
354100.0 /	103.50940 (100, 1)	99.04882 (100, 1)	94.53250 (100, 1)
354000.0 /	106.78339 (100, 1)	100.54407 (100, 1)	94.74571 (100, 1)
353900.0 /	87.45223 (112, 1)	84.14348 (100, 1)	79.41867 (100, 1)
353800.0 /	51.46952 (112, 1)	51.91042 (112, 1)	51.65077 (112, 1)
353700.0 /	32.96146 (180, 1)	31.54786 (100, 1)	31.69147 (100, 1)
353600.0 /	26.13291 (112, 1)	27.05941 (180, 1)	24.43216 (180, 1)
353500.0 /	17.11813 (112, 1)	21.24628 (112, 1)	23.98945 (180, 1)
353400.0 /	16.19486 (273, 1)	17.67223 (273, 1)	18.84827 (273, 1)
353300.0 /	16.09801 (273, 1)	17.47373 (273, 1)	18.55301 (273, 1)
353200.0 /	16.57531 (110, 1)	17.26696 (273, 1)	18.25534 (273, 1)
353100.0 /	22.57887 (110, 1)	17.48405 (110, 1)	17.96141 (273, 1)
353000.0 /	27.76752 (110, 1)	22.57194 (110, 1)	17.89651 (110, 1)
352900.0 /	32.01390 (110, 1)	27.30954 (110, 1)	22.47474 (110, 1)
352800.0 /	32.55748 (180, 1)	31.49787 (110, 1)	27.05429 (110, 1)
352700.0 /	29.02245 (180, 1)	30.65561 (180, 1)	31.21928 (110, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* 50 MAXIMUM 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *

* FROM ALL SOURCES *

RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y(METERS) OR DIRECTION (DEGREES)	RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y(METERS) OR DIRECTION (DEGREES)
1	129.67303	1	112	439200.0	354100.0	26	110.89085	1	100	438700.0	354100.0
2	128.91029	1	112	439100.0	354100.0	27	110.31721	1	100	438800.0	354100.0
3	127.69781	1	100	438600.0	354000.0	28	109.96690	1	273	437900.0	352800.0
4	125.65123	1	100	438500.0	354000.0	29	108.42615	1	273	437900.0	353000.0
5	125.28198	1	112	439000.0	354100.0	30	107.74702	1	100	438600.0	354100.0
6	124.87182	1	100	438700.0	354000.0	31	107.49860	1	100	438900.0	354100.0
7	122.99385	1	273	438100.0	352800.0	32	107.44366	1	112	439200.0	354200.0
8	122.89373	1	273	438100.0	352700.0	33	106.78339	1	100	439000.0	354000.0
9	122.21223	1	273	438000.0	352900.0	34	106.32381	1	112	438800.0	354100.0
10	122.17374	1	112	438900.0	354000.0	35	105.81990	1	100	438600.0	353900.0
11	121.70303	1	273	438000.0	352800.0	36	105.32964	1	273	437900.0	352700.0
12	121.46926	1	112	439000.0	354000.0	37	103.79082	1	100	438500.0	353900.0
13	120.20494	1	112	438800.0	354000.0	38	103.70300	1	100	438700.0	353900.0
14	119.57732	1	100	438800.0	354000.0	39	103.50940	1	100	439000.0	354100.0
15	118.96524	1	112	439100.0	354000.0	40	103.26687	1	273	438200.0	352800.0
16	117.97655	1	112	438900.0	354100.0	41	102.31380	1	112	438600.0	354000.0
17	116.78649	1	273	438000.0	352700.0	42	101.40851	1	207	438500.0	354300.0
18	115.39519	1	273	438100.0	352900.0	43	100.82488	1	207	438600.0	354400.0
19	115.31093	1	112	439200.0	354000.0	44	100.54407	1	100	439100.0	354000.0
20	115.23077	1	273	438000.0	353000.0	45	99.64541	1	207	438700.0	354400.0
21	114.86919	1	100	438400.0	354000.0	46	99.50558	1	100	438800.0	353900.0
22	114.46118	1	112	438700.0	354000.0	47	99.12209	1	100	438500.0	354100.0
23	113.36034	1	273	438200.0	352700.0	48	99.04882	1	100	439100.0	354100.0
24	113.27099	1	100	438900.0	354000.0	49	97.84726	1	273	438100.0	353000.0
25	111.72247	1	273	437900.0	352900.0	50	97.74953	1	273	438000.0	353100.0

ISCST FINE GRID ANALYSIS
PRODUCING HIGHEST AND
SECOND-HIGHEST 24-HOUR AVERAGES

Best Available Copy

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

CALCULATE (CONCENTRATION=1,DEPOSITION=2)
RECEPTOR GRID SYSTEM (RECTANGULAR=1 OR 3, POLAR=2 OR 4)
DISCRETE RECEPTOR SYSTEM (RECTANGULAR=1,POLAR=2)
TERRAIN ELEVATIONS ARE READ (YES=1,NO=0)
CALCULATIONS ARE WRITTEN TO TAPE (YES=1,NO=0)
LIST ALL INPUT DATA (NO=0,YES=1,MET DATA ALSO=2)

ISW(1) = 1
ISW(2) = 3
ISW(3) = 1
ISW(4) = 0
ISW(5) = 0
ISW(6) = 1

COMPUTE AVERAGE CONCENTRATION (OR TOTAL DEPOSITION)
WITH THE FOLLOWING TIME PERIODS:

HOURLY (YES=1,NO=0)
2-HOUR (YES=1,NO=0)
3-HOUR (YES=1,NO=0)
4-HOUR (YES=1,NO=0)
6-HOUR (YES=1,NO=0)
8-HOUR (YES=1,NO=0)
12-HOUR (YES=1,NO=0)
24-HOUR (YES=1,NO=0)

ISW(7) = 0
ISW(8) = 0
ISW(9) = 1
ISW(10) = 0
ISW(11) = 0
ISW(12) = 0
ISW(13) = 0
ISW(14) = 1
ISW(15) = 0

PRINT 'N'-DAY TABLE(S) (YES=1,NO=0)

PRINT THE FOLLOWING TYPES OF TABLES WHOSE TIME PERIODS ARE
SPECIFIED BY ISW(7) THROUGH ISW(14):

DAILY TABLES (YES=1,NO=0)
HIGHEST & SECOND HIGHEST TABLES (YES=1,NO=0)
MAXIMUM 50 TABLES (YES=1,NO=0)

ISW(16) = 0
ISW(17) = 1
ISW(18) = 1
ISW(19) = 1
ISW(20) = 0
ISW(21) = 1
ISW(22) = 1
ISW(23) = 0
ISW(24) = 1
ISW(25) = 1

METEOROLOGICAL DATA INPUT METHOD (PRE-PROCESSED=1,CARD=2)
RURAL-URBAN OPTION (RURAL=0,URBAN MODE 1=1,URBAN MODE 2=2)
WIND PROFILE EXPONENT VALUES (DEFAULTS=1,USER ENTERS=2,3)
VERTICAL POT. TEMP. GRADIENT VALUES (DEFAULTS=1,USER ENTERS=2,3)
SCALE EMISSION RATES FOR ALL SOURCES (NO=0,YES>0)
PROGRAM CALCULATES FINAL PLUME RISE ONLY (YES=1,NO=2)
PROGRAM ADJUSTS ALL STACK HEIGHTS FOR DOWNWASH (YES=2,NO=1)

NUMBER OF INPUT SOURCES
NUMBER OF SOURCE GROUPS (=0,ALL SOURCES)
TIME PERIOD INTERVAL TO BE PRINTED (=0,ALL INTERVALS)
NUMBER OF X (RANGE) GRID VALUES
NUMBER OF Y (THETA) GRID VALUES
NUMBER OF DISCRETE RECEPTORS
SOURCE EMISSION RATE UNITS CONVERSION FACTOR
ENTRAINMENT COEFFICIENT FOR UNSTABLE ATMOSPHERE
ENTRAINMENT COEFFICIENT FOR STABLE ATMOSPHERE
HEIGHT ABOVE GROUND AT WHICH WIND SPEED WAS MEASURED
LOGICAL UNIT NUMBER OF METEOROLOGICAL DATA
DECAY COEFFICIENT FOR PHYSICAL OR CHEMICAL DEPLETION
SURFACE STATION NO.
YEAR OF SURFACE DATA
UPPER AIR STATION NO.
YEAR OF UPPER AIR DATA
ALLOCATED DATA STORAGE
REQUIRED DATA STORAGE FOR THIS PROBLEM RUN

NSOURC = 17
NGROUP = 0
IPERD = 0
NXPNTS = 21
NYPNTS = 21
NXWYPT = 0
TK = .10000E+07
BETA1 = 0.600
BETA2 = 0.600
ZR = 7.00 METERS
IMET = 9
DECAY = 0.000000E+00
ISS = 13889
ISY = 71
IUS = 13861
IUY = 71
LIMIT = 43500 WORDS
MIMIT = 9391 WORDS

Joint 7 RC

1971

*File end
A 64 h
271 24 h*

*** SOURCE DATA ***

SOURCE NUMBER	T W Y A P K E E	PART. CATS.	EMISSION RATE		X (METERS)	Y (METERS)	BASE ELEV. (METERS)	HEIGHT (METERS)	TEMP.	EXIT VEL.		BLDG. HEIGHT (METERS)	BLDG. LENGTH (METERS)	BLDG. WIDTH (METERS)
			TYPE=0,1 (GRAMS/SEC)	TYPE=2 (GRAMS/SEC)					TYPE=0 (DEG.K); VERT.DIM (METERS)	TYPE=0 (M/SEC); HORZ.DIM (METERS)	TYPE=0 (METERS)			
1	0	0	0	0.11766E+04	446900.0	366300.0	0.0	194.20	327.60	18.29	10.13	0.00	0.00	0.00
2	0	0	0	0.70570E+03	446900.0	364900.0	0.0	76.20	401.00	20.10	5.03	0.00	0.00	0.00
3	0	0	0	0.70570E+03	446900.0	364900.0	0.0	91.40	408.20	8.50	5.33	0.00	0.00	0.00
4	0	0	0	0.12556E+04	446900.0	364900.0	0.0	106.70	438.80	19.20	7.01	0.00	0.00	0.00
5	0	0	0	0.23160E+03	446900.0	364900.0	0.0	10.10	779.80	18.30	6.56	0.00	0.00	0.00
6	0	0	0	0.13180E+03	437670.0	353900.0	0.0	40.70	433.20	11.70	2.44	0.00	0.00	0.00
7	0	0	0	0.90600E+02	437670.0	353900.0	0.0	40.70	406.50	10.30	3.05	0.00	0.00	0.00
8	0	0	0	0.11030E+03	437670.0	353900.0	0.0	43.70	422.10	11.80	3.35	0.00	0.00	0.00
9	0	0	0	0.20970E+03	437670.0	353900.0	0.0	44.20	416.50	13.70	3.05	0.00	0.00	0.00
10	0	0	0	0.16520E+03	440080.0	359150.0	0.0	45.70	414.30	7.80	3.20	0.00	0.00	0.00
11	0	0	0	0.20480E+03	440080.0	359150.0	0.0	41.50	405.40	15.50	2.74	0.00	0.00	0.00
12	0	0	0	0.19120E+03	440080.0	359150.0	0.0	13.70	714.30	8.80	5.84	0.00	0.00	0.00
13	0	0	0	0.13800E+02	440080.0	359150.0	0.0	6.30	766.50	11.80	3.13	0.00	0.00	0.00
14	0	0	0	0.20840E+03	441800.0	365600.0	0.0	32.30	433.00	16.10	2.13	0.00	0.00	0.00
15	0	0	0	0.82200E+02	437900.0	366800.0	0.0	15.90	505.00	8.60	1.37	0.00	0.00	0.00
16	0	0	0	0.54400E+02	439900.0	359300.0	0.0	76.20	477.00	9.20	3.78	0.00	0.00	0.00
17	0	0	0	0.25600E+02	447040.0	366570.0	0.0	85.40	441.00	12.20	2.08	0.00	0.00	0.00

Source NO.

Source Name

- 1 SJRPP Units 1 & 2
- 2 Northside Unit 1
- 3 Northside Unit 2
- 4 Northside Unit 3
- 5 Northside CT 3, 4, 5, 6
- 6 Southside Units 1 & 2
- 7 Southside Unit 3
- 8 Southside Unit 4
- 9 Southside Unit 5
- 10 Kennedy Units 8 & 9
- 11 Kennedy Unit 10
- 12 Kennedy CT 3, 4, 5, 6
- 13 Kennedy CT 1
- 14 St. Regis (All major sources)
- 15 Anheuser Busch (All major sources)
- 16 Alton Box Board (All major sources)
- 17 SJRPP Aux. Boiler

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 670.38708 AND OCCURRED AT (436400.0, 352200.0) *

Y-AXIS / (METERS) /	X-AXIS (METERS)				
	435200.0	435300.0	435400.0	435500.0	435600.0
352700.0 /	297.96158 (101, 6)	323.44562 (101, 6)	326.37604 (101, 6)	327.35077 (101, 4)	405.31613 (101, 4)
352600.0 /	327.19434 (101, 6)	321.25342 (302, 6)	351.91077 (101, 4)	420.71216 (101, 4)	484.86630 (101, 4)
352500.0 /	323.03223 (302, 6)	366.20724 (101, 4)	424.52136 (101, 4)	474.67126 (101, 4)	508.12640 (101, 4)
352400.0 /	371.61227 (101, 4)	419.27032 (101, 4)	456.62341 (101, 4)	476.82477 (101, 4)	473.65338 (101, 4)
352300.0 /	407.36945 (101, 4)	433.60022 (101, 4)	443.20847 (101, 4)	431.97491 (101, 4)	398.12762 (101, 4)
352200.0 /	407.81271 (101, 4)	409.22482 (101, 4)	392.45532 (101, 4)	357.03650 (101, 4)	305.45844 (101, 4)
352100.0 /	376.13226 (101, 4)	355.77570 (101, 4)	320.17792 (101, 4)	280.75784 (356, 6)	364.07727 (356, 6)
352000.0 /	322.21036 (101, 4)	287.35760 (101, 4)	291.79568 (356, 6)	372.62384 (356, 6)	470.05963 (356, 6)
351900.0 /	258.26056 (101, 4)	301.36420 (356, 6)	379.13788 (356, 6)	469.62555 (356, 6)	545.09717 (356, 6)
351800.0 /	309.57809 (356, 6)	383.76648 (356, 6)	467.52814 (356, 6)	536.11060 (356, 6)	558.51453 (356, 6)
351700.0 /	386.96960 (356, 6)	464.25635 (356, 6)	526.35559 (356, 6)	546.72968 (356, 6)	507.83331 (356, 6)
351600.0 /	460.17761 (356, 6)	516.41864 (356, 6)	534.77026 (356, 6)	500.03259 (356, 6)	450.86261 (302, 8)
351500.0 /	506.44012 (356, 6)	522.92749 (356, 6)	491.73737 (356, 6)	444.44443 (302, 8)	503.58820 (302, 8)
351400.0 /	511.29587 (356, 6)	483.13864 (356, 6)	437.95996 (302, 8)	495.47202 (302, 8)	539.40533 (302, 8)
351300.0 /	474.38428 (356, 6)	431.51181 (302, 8)	487.09802 (302, 8)	531.89771 (302, 8)	554.82190 (302, 8)
351200.0 /	425.17078 (302, 8)	478.64941 (302, 8)	523.63318 (302, 8)	550.15643 (302, 8)	571.40918 (356, 7)
351100.0 /	470.25742 (302, 8)	514.90973 (302, 8)	544.03137 (302, 8)	550.67926 (356, 7)	578.84338 (356, 7)
351000.0 /	505.95288 (302, 8)	536.85907 (302, 8)	547.65314 (302, 8)	566.29559 (356, 7)	558.36230 (356, 7)
350900.0 /	528.96796 (302, 8)	543.54810 (302, 8)	551.37482 (356, 7)	555.77063 (356, 7)	517.74927 (356, 7)
350800.0 /	538.14490 (302, 8)	535.96790 (302, 8)	549.41016 (356, 7)	524.50574 (356, 7)	466.64429 (356, 7)
350700.0 /	534.05408 (302, 8)	540.14679 (356, 7)	526.91553 (356, 7)	480.40845 (356, 7)	413.74963 (356, 7)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 670.38708 AND OCCURRED AT (436400.0, 352200.0) *

Y-AXIS (METERS) /	X-AXIS (METERS)				
	435700.0	435800.0	435900.0	436000.0	436100.0
352700.0 /	483.70203 (101, 4)	551.28442 (101, 4)	593.41656 (101, 4)	595.13806 (101, 4)	546.82062 (101, 4)
352600.0 /	534.26190 (101, 4)	557.29407 (101, 4)	543.77081 (101, 4)	489.12167 (101, 4)	398.40356 (101, 4)
352500.0 /	516.17773 (101, 4)	492.36658 (101, 4)	435.43076 (101, 4)	351.56906 (101, 4)	433.48676 (356, 6)
352400.0 /	443.40207 (101, 4)	386.83911 (101, 4)	323.81036 (356, 6)	447.92145 (356, 6)	568.10870 (356, 6)
352300.0 /	343.58533 (101, 4)	339.90521 (356, 6)	458.13434 (356, 6)	568.27142 (356, 6)	602.66675 (356, 6)
352200.0 /	353.25665 (356, 6)	464.82208 (356, 6)	565.34662 (356, 6)	597.23297 (356, 6)	523.27936 (356, 6)
352100.0 /	468.61414 (356, 6)	560.11938 (356, 6)	589.49402 (356, 6)	524.89001 (356, 6)	468.85498 (302, 8)
352000.0 /	553.20819 (356, 6)	580.13330 (356, 6)	523.51727 (356, 6)	468.17953 (302, 8)	522.52472 (302, 8)
351900.0 /	569.67419 (356, 6)	519.86646 (356, 6)	465.61224 (302, 8)	523.43591 (302, 8)	611.15942 (356, 7)
351800.0 /	514.50513 (356, 6)	461.68039 (302, 8)	521.38873 (302, 8)	582.29504 (356, 7)	646.96948 (356, 7)
351700.0 /	456.79712 (302, 8)	517.15436 (302, 8)	552.71265 (356, 7)	630.28571 (356, 7)	625.52161 (356, 7)
351600.0 /	511.19696 (302, 8)	550.21216 (302, 8)	608.86224 (356, 7)	626.93658 (356, 7)	563.25824 (356, 7)
351500.0 /	545.76849 (302, 8)	584.61627 (356, 7)	620.35016 (356, 7)	581.58691 (356, 7)	483.72800 (356, 7)
351400.0 /	559.01544 (356, 7)	607.55920 (356, 7)	590.85748 (356, 7)	512.76001 (356, 7)	428.20227 (357, 5)
351300.0 /	590.74585 (356, 7)	592.43298 (356, 7)	534.18384 (356, 7)	438.88080 (356, 7)	480.59705 (357, 5)
351200.0 /	587.96790 (356, 7)	548.47351 (356, 7)	466.57751 (356, 7)	439.56390 (357, 5)	516.75696 (357, 5)
351100.0 /	556.24677 (356, 7)	489.06378 (356, 7)	401.61780 (302, 1)	482.43433 (357, 5)	533.08557 (357, 5)
351000.0 /	506.07379 (356, 7)	426.74170 (356, 7)	445.21811 (357, 5)	509.85822 (357, 5)	529.54608 (357, 5)
350900.0 /	448.70786 (356, 7)	407.98935 (357, 5)	479.83539 (357, 5)	519.77795 (357, 5)	508.91101 (357, 5)
350800.0 /	393.19104 (356, 7)	446.46136 (357, 5)	500.12817 (357, 5)	512.87402 (357, 5)	475.48215 (357, 5)
350700.0 /	412.29303 (357, 5)	474.00964 (357, 5)	505.13440 (357, 5)	491.77673 (357, 5)	433.93890 (357, 5)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 670.38708 AND OCCURRED AT (436400.0, 352200.0) *

Y-AXIS / (METERS) /	X-AXIS (METERS)				
	436200.0	436300.0	436400.0	436500.0	436600.0
352700.0 /	450.76157 (101, 4)	389.10828 (356, 6)	538.14240 (356, 6)	579.70868 (356, 6)	434.55042 (356, 6)
352600.0 /	414.10583 (356, 6)	554.36774 (356, 6)	595.01746 (356, 6)	467.16284 (356, 6)	531.07361 (356, 7)
352500.0 /	563.87659 (356, 6)	602.83661 (356, 6)	491.02979 (356, 6)	506.48996 (356, 7)	648.11353 (356, 7)
352400.0 /	604.91168 (356, 6)	507.47247 (356, 6)	479.36093 (356, 7)	635.73938 (356, 7)	648.15332 (356, 7)
352300.0 /	517.81989 (356, 6)	461.75665 (302, 8)	612.58630 (356, 7)	668.72845 (356, 7)	557.37231 (356, 7)
352200.0 /	466.98010 (302, 8)	583.65027 (356, 7)	670.38708 (356, 7)	608.19312 (356, 7)	445.84332 (357, 4)
352100.0 /	552.36572 (356, 7)	658.39880 (356, 7)	640.20959 (356, 7)	501.88840 (356, 7)	520.09998 (357, 5)
352000.0 /	637.42865 (356, 7)	655.20514 (356, 7)	552.64185 (356, 7)	477.26709 (357, 5)	564.70679 (357, 5)
351900.0 /	656.31812 (356, 7)	590.03900 (356, 7)	450.29562 (356, 7)	541.09558 (357, 5)	566.41553 (357, 5)
351800.0 /	613.89685 (356, 7)	497.07867 (356, 7)	501.46790 (357, 5)	570.45483 (357, 5)	531.74329 (357, 5)
351700.0 /	535.12134 (356, 7)	455.47787 (357, 5)	550.00684 (357, 5)	563.47455 (357, 5)	473.79025 (357, 5)
351600.0 /	447.87909 (356, 7)	514.55328 (357, 5)	567.38843 (357, 5)	527.09332 (357, 5)	405.86484 (357, 5)
351500.0 /	472.06659 (357, 5)	550.10095 (357, 5)	554.47290 (357, 5)	472.05585 (357, 5)	381.23627 (357, 6)
351400.0 /	519.04285 (357, 5)	558.40051 (357, 5)	517.79553 (357, 5)	408.83533 (357, 5)	386.75592 (302, 2)
351300.0 /	544.02826 (357, 5)	541.61127 (357, 5)	466.08777 (357, 5)	380.29767 (302, 2)	388.59955 (302, 2)
351200.0 /	545.29718 (357, 5)	505.44061 (357, 5)	407.63318 (357, 5)	395.46277 (302, 2)	381.82407 (302, 2)
351100.0 /	525.82562 (357, 5)	456.89474 (357, 5)	383.44843 (302, 2)	399.23401 (302, 2)	370.02158 (302, 2)
351000.0 /	490.74359 (357, 5)	402.87714 (357, 5)	399.98389 (302, 2)	393.57758 (302, 2)	356.24069 (302, 2)
350900.0 /	445.80453 (357, 5)	383.48199 (302, 2)	405.76022 (302, 2)	381.73093 (302, 2)	359.57013 (357, 7)
350800.0 /	396.28772 (357, 5)	401.40594 (302, 2)	402.11163 (302, 2)	366.80676 (302, 2)	365.35162 (357, 7)
350700.0 /	381.48486 (302, 2)	409.25592 (302, 2)	391.45432 (302, 2)	351.34579 (302, 2)	367.79938 (357, 7)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 670.38708 AND OCCURRED AT (436400.0, 352200.0) *

Y-AXIS (METERS) /	X-AXIS (METERS)				
	436700.0	436800.0	436900.0	437000.0	437100.0
352700.0 /	549.15820 (356, 7)	612.86145 (356, 7)	443.20825 (356, 7)	444.53656 (357, 5)	364.65424 (357, 6)
352600.0 /	643.04645 (356, 7)	534.10455 (356, 7)	454.59967 (357, 5)	445.29938 (357, 5)	383.07117 (357, 6)
352500.0 /	603.91473 (356, 7)	432.43976 (357, 4)	503.88510 (357, 5)	392.46167 (357, 5)	373.22351 (357, 6)
352400.0 /	488.93726 (356, 7)	511.02893 (357, 5)	490.22437 (357, 5)	396.97189 (357, 6)	345.87683 (357, 6)
352300.0 /	483.49130 (357, 5)	540.99884 (357, 5)	431.71860 (357, 5)	390.21649 (357, 6)	374.72739 (357, 7)
352200.0 /	546.37744 (357, 5)	516.85553 (357, 5)	400.81342 (357, 6)	365.80322 (357, 6)	395.08469 (357, 7)
352100.0 /	560.25647 (357, 5)	456.34833 (357, 5)	396.84787 (357, 6)	375.73584 (357, 7)	402.78766 (357, 7)
352000.0 /	529.38336 (357, 5)	397.85559 (357, 6)	376.40732 (357, 6)	397.46228 (357, 7)	398.01294 (357, 7)
351900.0 /	469.37973 (357, 5)	396.01453 (357, 6)	366.30597 (357, 7)	410.96588 (357, 7)	383.20142 (357, 7)
351800.0 /	397.18616 (357, 5)	379.45160 (357, 6)	386.16754 (357, 7)	414.53973 (357, 7)	361.66345 (357, 7)
351700.0 /	390.19952 (357, 6)	355.90817 (302, 2)	401.67477 (357, 7)	408.53467 (357, 7)	336.58328 (357, 7)
351600.0 /	376.96521 (357, 6)	368.76556 (357, 7)	410.48291 (357, 7)	394.66144 (357, 7)	310.52090 (357, 7)
351500.0 /	374.06793 (302, 2)	383.71698 (357, 7)	411.65039 (357, 7)	375.20819 (357, 7)	285.28000 (357, 7)
351400.0 /	366.86423 (302, 2)	394.80902 (357, 7)	405.50806 (357, 7)	352.45862 (357, 7)	263.13489 (302, 2)
351300.0 /	362.49457 (357, 7)	400.56323 (357, 7)	393.23227 (357, 7)	328.36224 (357, 7)	245.92682 (302, 2)
351200.0 /	373.82062 (357, 7)	400.43881 (357, 7)	376.39447 (357, 7)	304.40710 (357, 7)	247.88611 (357, 8)
351100.0 /	381.86420 (357, 7)	394.70184 (357, 7)	356.61279 (357, 7)	281.61874 (357, 7)	257.74323 (357, 8)
351000.0 /	385.51251 (357, 7)	384.08212 (357, 7)	335.33594 (357, 7)	260.62518 (357, 7)	266.60291 (357, 8)
350900.0 /	384.52707 (357, 7)	369.58823 (357, 7)	313.53973 (357, 7)	241.65268 (357, 7)	274.05685 (357, 8)
350800.0 /	379.24042 (357, 7)	352.59970 (357, 7)	292.37231 (357, 7)	245.90062 (357, 8)	279.90573 (357, 8)
350700.0 /	370.21588 (357, 7)	334.17535 (357, 7)	272.42062 (357, 7)	252.99597 (357, 8)	284.16730 (357, 8)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 670.38708 AND OCCURRED AT (436400.0, 352200.0) *

Y-AXIS /
(METERS) /

437200.0

X-AXIS (METERS)

352700.0 /	343.78488 (357, 6)
352600.0 /	324.55502 (357, 7)
352500.0 /	353.59839 (357, 7)
352400.0 /	367.59698 (357, 7)
352300.0 /	365.92368 (357, 7)
352200.0 /	351.82419 (357, 7)
352100.0 /	329.91248 (357, 7)
352000.0 /	304.44775 (357, 7)
351900.0 /	278.60565 (357, 7)
351800.0 /	259.92560 (302, 2)
351700.0 /	243.64072 (302, 2)
351600.0 /	243.04227 (357, 8)
351500.0 /	255.38251 (357, 8)
351400.0 /	266.63892 (357, 8)
351300.0 /	276.44153 (357, 8)
351200.0 /	284.51920 (357, 8)
351100.0 /	290.69958 (357, 8)
351000.0 /	294.90158 (357, 8)
350900.0 /	296.98999 (357, 8)
350800.0 /	296.94748 (357, 8)
350700.0 /	295.12610 (357, 8)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 557.62488 AND OCCURRED AT (435800.0, 351500.0) *

Y-AXIS / (METERS) /	X-AXIS (METERS)				
	435200.0	435300.0	435400.0	435500.0	435600.0
352700.0 /	257.38110 (356, 6)	269.83545 (302, 6)	306.38959 (302, 6)	326.67334 (302, 6)	323.73511 (302, 6)
352600.0 /	296.95343 (302, 6)	309.32526 (101, 6)	326.87329 (302, 6)	310.33496 (302, 6)	273.27676 (302, 6)
352500.0 /	306.64484 (101, 4)	315.64716 (302, 6)	289.21655 (302, 6)	247.85368 (302, 6)	267.06714 (302, 4)
352400.0 /	296.68976 (302, 6)	264.11005 (302, 6)	258.10321 (302, 4)	279.61057 (302, 4)	288.39166 (302, 4)
352300.0 /	248.02184 (302, 8)	271.37039 (302, 4)	287.33408 (302, 4)	289.59485 (302, 4)	277.60773 (302, 4)
352200.0 /	280.58807 (302, 4)	290.93964 (302, 4)	287.80786 (302, 4)	273.10352 (302, 4)	268.32455 (356, 6)
352100.0 /	291.14642 (302, 4)	283.97119 (302, 4)	267.88544 (302, 4)	272.03580 (101, 4)	260.74234 (356, 8)
352000.0 /	278.65027 (302, 4)	262.33765 (302, 4)	248.60289 (357, 2)	262.36481 (356, 8)	282.90686 (356, 8)
351900.0 /	256.66632 (302, 4)	244.54192 (302, 4)	263.14233 (356, 8)	280.43079 (356, 8)	292.67807 (302, 5)
351800.0 /	241.81511 (356, 8)	263.20605 (356, 8)	277.64624 (356, 8)	295.16034 (302, 5)	330.09235 (302, 5)
351700.0 /	262.77615 (356, 8)	274.71381 (356, 8)	296.94998 (302, 5)	329.41351 (302, 5)	389.01520 (302, 8)
351600.0 /	271.73639 (356, 8)	298.32608 (302, 5)	329.37405 (302, 8)	385.91864 (302, 8)	415.42905 (356, 6)
351500.0 /	299.33389 (302, 5)	329.29532 (302, 8)	382.67029 (302, 8)	414.98373 (356, 6)	410.88925 (302, 5)
351400.0 /	328.97910 (302, 8)	379.33990 (302, 8)	413.34888 (356, 6)	402.37057 (302, 5)	469.51349 (356, 7)
351300.0 /	375.97519 (302, 8)	410.76978 (356, 6)	394.38098 (302, 5)	445.37216 (356, 7)	533.40070 (356, 7)
351200.0 /	407.45026 (356, 6)	386.91626 (302, 5)	423.30527 (356, 7)	508.46555 (356, 7)	550.26062 (302, 8)
351100.0 /	379.95514 (302, 5)	405.08957 (302, 5)	484.65363 (356, 7)	550.05249 (302, 8)	528.80170 (302, 8)
351000.0 /	395.99927 (302, 5)	462.22714 (356, 7)	529.40912 (356, 7)	533.80255 (302, 8)	494.90515 (302, 8)
350900.0 /	441.31821 (356, 7)	508.22046 (356, 7)	536.02911 (302, 8)	504.99265 (302, 8)	453.42953 (302, 8)
350800.0 /	487.55054 (356, 7)	534.94122 (356, 7)	512.00684 (302, 8)	467.75217 (302, 8)	408.93658 (302, 8)
350700.0 /	517.67725 (356, 7)	516.35120 (302, 8)	479.05365 (302, 8)	426.15915 (302, 8)	377.23581 (356, 4)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 557.62488 AND OCCURRED AT (435800.0, 351500.0) *

Y-AXIS (METERS) /	X-AXIS (METERS)				
	435700.0	435800.0	435900.0	436000.0	436100.0
352700.0 /	295.40997 (302, 6)	246.83720 (302, 6)	255.83875 (302, 4)	278.98029 (302, 3)	295.65442 (302, 3)
352600.0 /	249.33653 (302, 4)	272.55960 (302, 4)	284.65146 (302, 3)	289.94284 (302, 3)	283.07697 (356, 6)
352500.0 /	283.09589 (302, 4)	284.79218 (302, 3)	280.71741 (302, 3)	304.85291 (356, 6)	284.98187 (356, 8)
352400.0 /	280.75623 (302, 3)	269.46725 (302, 3)	310.36322 (101, 4)	286.87268 (356, 8)	306.34421 (356, 8)
352300.0 /	261.12897 (357, 2)	274.43985 (101, 4)	287.25629 (356, 8)	303.43765 (356, 8)	323.98505 (302, 5)
352200.0 /	261.43427 (357, 2)	286.52853 (356, 8)	299.82733 (356, 8)	326.94870 (302, 5)	392.67566 (302, 8)
352100.0 /	284.99933 (356, 8)	295.78387 (356, 8)	328.81924 (302, 5)	394.02267 (302, 8)	413.23010 (302, 5)
352000.0 /	291.50543 (356, 8)	329.84402 (302, 5)	394.04440 (302, 8)	408.79883 (302, 5)	520.94312 (356, 7)
351900.0 /	330.21802 (302, 5)	393.06403 (302, 8)	405.33563 (356, 6)	490.71664 (356, 7)	543.04877 (302, 8)
351800.0 /	391.33905 (302, 8)	410.99860 (356, 6)	462.42548 (356, 7)	549.39240 (302, 8)	530.95410 (302, 8)
351700.0 /	414.27716 (356, 6)	436.42197 (356, 7)	551.46735 (302, 8)	544.92920 (302, 8)	496.25842 (302, 5)
351600.0 /	419.91693 (302, 5)	523.65149 (356, 7)	553.61597 (302, 8)	515.64001 (302, 8)	454.91901 (302, 5)
351500.0 /	495.69492 (356, 7)	557.62488 (302, 8)	531.57416 (302, 8)	472.37036 (302, 5)	421.02826 (356, 4)
351400.0 /	557.51764 (302, 8)	541.76196 (302, 8)	491.91000 (302, 8)	431.97253 (356, 4)	421.12433 (357, 4)
351300.0 /	547.71075 (302, 8)	508.36987 (302, 8)	442.81561 (302, 8)	400.06427 (356, 4)	444.12598 (302, 1)
351200.0 /	520.50220 (302, 8)	464.05969 (302, 8)	410.94138 (356, 4)	422.48544 (302, 1)	468.52280 (302, 1)
351100.0 /	481.36450 (302, 8)	418.18542 (356, 4)	401.22070 (356, 7)	450.13400 (302, 1)	479.42282 (302, 1)
351000.0 /	435.92355 (302, 8)	389.56052 (356, 4)	428.92792 (302, 1)	469.34424 (302, 1)	473.97424 (302, 1)
350900.0 /	397.54636 (356, 4)	407.60559 (302, 1)	452.58270 (302, 1)	475.39230 (302, 1)	453.01270 (302, 1)
350800.0 /	387.83838 (302, 1)	432.46210 (302, 1)	467.01221 (302, 1)	466.75336 (302, 1)	419.90088 (302, 1)
350700.0 /	411.49152 (302, 1)	452.05478 (302, 1)	469.01270 (302, 1)	444.68832 (302, 1)	379.11676 (302, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 557.62488 AND OCCURRED AT (435800.0, 351500.0) *

Y-AXIS / (METERS) /	X-AXIS (METERS)				
	436200.0	436300.0	436400.0	436500.0	436600.0
352700.0 /	278.76801 (357, 2)	324.73328 (101, 4)	306.60168 (356, 8)	314.30670 (356, 8)	359.83752 (357, 1)
352600.0 /	287.44843 (101, 4)	308.47632 (356, 8)	316.09064 (356, 8)	365.09262 (302, 8)	434.55450 (357, 6)
352500.0 /	308.18378 (356, 8)	315.39423 (356, 8)	376.36984 (302, 8)	437.46729 (302, 8)	470.21811 (357, 6)
352400.0 /	319.62305 (302, 5)	384.35211 (302, 8)	452.25531 (302, 8)	484.88513 (357, 6)	456.38031 (302, 5)
352300.0 /	389.60886 (302, 8)	452.09433 (356, 7)	492.02319 (302, 8)	482.20737 (302, 5)	415.96054 (356, 4)
352200.0 /	426.05408 (356, 7)	507.94751 (302, 8)	495.98969 (302, 5)	450.61414 (302, 5)	440.35291 (356, 7)
352100.0 /	517.72284 (302, 8)	513.31598 (302, 8)	480.79230 (302, 5)	413.92578 (356, 4)	482.30746 (357, 4)
352000.0 /	531.38568 (302, 8)	499.28818 (302, 5)	436.66223 (356, 4)	464.50424 (357, 4)	484.45044 (357, 4)
351900.0 /	510.83002 (302, 8)	459.91220 (302, 5)	436.20004 (357, 4)	483.79050 (357, 4)	462.39145 (357, 4)
351800.0 /	482.67609 (302, 5)	423.60388 (356, 4)	469.68750 (357, 4)	475.96225 (357, 4)	427.18759 (357, 4)
351700.0 /	439.45563 (356, 4)	445.90060 (357, 4)	476.46118 (357, 4)	458.18710 (302, 1)	386.42755 (357, 4)
351600.0 /	416.33261 (357, 4)	465.69492 (357, 4)	475.57587 (302, 1)	428.03415 (302, 1)	380.71765 (357, 6)
351500.0 /	446.28345 (357, 4)	475.38092 (302, 1)	463.38718 (302, 1)	382.57101 (302, 1)	373.48129 (302, 2)
351400.0 /	463.13452 (302, 1)	479.81296 (302, 1)	431.38303 (302, 1)	369.38361 (357, 6)	370.67856 (357, 6)
351300.0 /	480.21490 (302, 1)	463.80048 (302, 1)	386.43781 (302, 1)	370.39230 (357, 6)	351.77173 (357, 6)
351200.0 /	478.95078 (302, 1)	430.69891 (302, 1)	357.31073 (357, 6)	361.90683 (357, 6)	330.15924 (357, 7)
351100.0 /	459.73334 (302, 1)	386.45038 (302, 1)	358.44672 (357, 6)	345.82700 (357, 6)	340.90143 (357, 7)
351000.0 /	426.21783 (302, 1)	356.14709 (302, 2)	351.46497 (357, 6)	324.60355 (357, 6)	351.07849 (357, 7)
350900.0 /	383.62994 (302, 1)	348.57733 (357, 5)	337.75519 (357, 6)	319.91742 (357, 7)	343.04089 (302, 2)
350800.0 /	354.09375 (302, 2)	340.19794 (357, 6)	319.17682 (357, 6)	328.68250 (357, 7)	331.64435 (302, 2)
350700.0 /	346.39758 (357, 5)	328.46057 (357, 6)	300.70731 (357, 7)	336.90234 (357, 7)	322.31915 (302, 2)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 557.62488 AND OCCURRED AT (435800.0, 351500.0) *

Y-AXIS / (METERS) /	X-AXIS (METERS)				
	436700.0	436800.0	436900.0	437000.0	437100.0
352700.0 /	427.28748 (357, 6)	405.82458 (356, 8)	372.94397 (357, 4)	427.79498 (357, 1)	336.84961 (357, 5)
352600.0 /	443.64008 (357, 6)	367.32050 (356, 4)	437.41357 (357, 1)	403.07788 (357, 4)	287.92111 (357, 4)
352500.0 /	416.44589 (302, 5)	428.64325 (357, 5)	459.15338 (357, 1)	378.76147 (357, 6)	311.55286 (357, 7)
352400.0 /	408.95712 (357, 4)	470.33798 (357, 4)	427.36865 (357, 4)	318.29193 (357, 4)	344.91269 (357, 7)
352300.0 /	467.16846 (357, 4)	471.18402 (357, 1)	386.07562 (357, 4)	323.16748 (357, 7)	313.28665 (357, 6)
352200.0 /	484.28647 (357, 4)	436.25800 (357, 4)	355.14355 (357, 5)	349.54221 (357, 7)	295.58301 (302, 2)
352100.0 /	470.09662 (357, 1)	393.10059 (357, 4)	326.63745 (302, 2)	333.58167 (357, 6)	302.59766 (302, 2)
352000.0 /	434.91577 (357, 4)	380.94662 (357, 5)	345.27914 (357, 7)	313.17410 (302, 2)	308.32660 (302, 2)
351900.0 /	392.27780 (357, 4)	347.11667 (302, 2)	346.89801 (357, 6)	315.24042 (302, 2)	310.94086 (302, 2)
351800.0 /	390.58514 (357, 6)	356.50864 (302, 2)	331.37848 (302, 2)	318.11041 (302, 2)	309.29047 (302, 2)
351700.0 /	362.59702 (302, 2)	353.54828 (357, 6)	328.00491 (302, 2)	320.44324 (302, 2)	303.07697 (302, 2)
351600.0 /	373.86273 (302, 2)	349.69431 (302, 2)	326.07236 (302, 2)	320.73343 (302, 2)	292.71741 (302, 2)
351500.0 /	354.72717 (357, 6)	341.87518 (302, 2)	325.31799 (302, 2)	317.92151 (302, 2)	279.06378 (302, 2)
351400.0 /	349.41452 (357, 7)	334.96350 (302, 2)	324.64105 (302, 2)	311.58218 (302, 2)	261.97479 (357, 7)
351300.0 /	356.23621 (302, 2)	329.83209 (302, 2)	322.81589 (302, 2)	301.85376 (302, 2)	241.17717 (357, 7)
351200.0 /	345.30188 (302, 2)	326.16101 (302, 2)	318.91489 (302, 2)	289.25952 (302, 2)	228.30463 (302, 2)
351100.0 /	335.82700 (302, 2)	323.04172 (302, 2)	312.46112 (302, 2)	274.52148 (302, 2)	210.95683 (302, 2)
351000.0 /	328.18457 (302, 2)	319.39267 (302, 2)	303.40158 (302, 2)	258.41168 (302, 2)	194.56223 (357, 7)
350900.0 /	322.06500 (302, 2)	314.27301 (302, 2)	291.71848 (302, 2)	241.47571 (302, 2)	186.03940 (356, 7)
350800.0 /	316.84760 (302, 2)	307.45572 (302, 2)	278.23001 (302, 2)	224.89383 (357, 7)	178.27664 (356, 7)
350700.0 /	311.70935 (302, 2)	298.78613 (302, 2)	263.49304 (302, 2)	210.32536 (357, 7)	170.26424 (356, 7)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 557.62488 AND OCCURRED AT (435800.0, 351500.0) *

Y-AXIS / X-AXIS (METERS)
(METERS) / 437200.0

352700.0 / 286.49789 (357, 7)
352600.0 / 316.67456 (357, 6)
352500.0 / 287.94739 (357, 6)
352400.0 / 278.01697 (302, 2)
352300.0 / 286.67786 (302, 2)
352200.0 / 291.35559 (302, 2)
352100.0 / 290.74316 (302, 2)
352000.0 / 284.72018 (302, 2)
351900.0 / 274.04724 (302, 2)
351800.0 / 254.39655 (357, 7)
351700.0 / 232.87767 (357, 7)
351600.0 / 226.34612 (302, 2)
351500.0 / 217.57654 (356, 7)
351400.0 / 211.91380 (356, 7)
351300.0 / 205.62393 (356, 7)
351200.0 / 198.78674 (356, 7)
351100.0 / 191.48412 (356, 7)
351000.0 / 183.79820 (356, 7)
350900.0 / 175.81029 (356, 7)
350800.0 / 174.67789 (357, 3)
350700.0 / 178.67668 (357, 3)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* 50 MAXIMUM 3-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *

* FROM ALL SOURCES *

RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y(METERS) OR DIRECTION (DEGREES)	RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y(METERS) OR DIRECTION (DEGREES)
1	670.38708	7	356	436400.0	352200.0	26	602.83661	6	356	436300.0	352500.0
2	668.72845	7	356	436500.0	352300.0	27	602.66675	6	356	436100.0	352300.0
3	658.39880	7	356	436300.0	352100.0	28	597.23297	6	356	436000.0	352200.0
4	656.31812	7	356	436200.0	351900.0	29	595.13806	4	101	436000.0	352700.0
5	655.20514	7	356	436300.0	352000.0	30	595.01746	6	356	436400.0	352600.0
6	648.15332	7	356	436600.0	352400.0	31	593.41656	4	101	435900.0	352700.0
7	648.11353	7	356	436600.0	352500.0	32	592.43298	7	356	435800.0	351300.0
8	646.96948	7	356	436100.0	351800.0	33	590.85748	7	356	435900.0	351400.0
9	643.04645	7	356	436700.0	352600.0	34	590.74585	7	356	435700.0	351300.0
10	640.20959	7	356	436400.0	352100.0	35	590.03900	7	356	436300.0	351900.0
11	637.42865	7	356	436200.0	352000.0	36	589.49402	6	356	435900.0	352100.0
12	635.73938	7	356	436500.0	352400.0	37	587.96790	7	356	435700.0	351200.0
13	630.28571	7	356	436000.0	351700.0	38	584.61627	7	356	435800.0	351500.0
14	626.93658	7	356	436000.0	351600.0	39	583.65027	7	356	436300.0	352200.0
15	625.52161	7	356	436100.0	351700.0	40	582.29504	7	356	436000.0	351800.0
16	620.35016	7	356	435900.0	351500.0	41	581.58691	7	356	436000.0	351500.0
17	613.89685	7	356	436200.0	351800.0	42	580.13330	6	356	435800.0	352000.0
18	612.86145	7	356	436800.0	352700.0	43	579.70868	6	356	436500.0	352700.0
19	612.58630	7	356	436400.0	352300.0	44	578.84338	7	356	435600.0	351100.0
20	611.15942	7	356	436100.0	351900.0	45	571.40918	7	356	435600.0	351200.0
21	608.86224	7	356	435900.0	351600.0	46	570.45483	5	357	436500.0	351800.0
22	608.19312	7	356	436500.0	352200.0	47	569.67419	6	356	435700.0	351900.0
23	607.55920	7	356	435800.0	351400.0	48	568.27142	6	356	436000.0	352300.0
24	604.91168	6	356	436200.0	352400.0	49	568.10870	6	356	436100.0	352400.0
25	603.91473	7	356	436700.0	352500.0	50	567.38843	5	357	436400.0	351600.0

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 331.04660 AND OCCURRED AT (436700.0, 352100.0) *

Y-AXIS (METERS) /	X-AXIS (METERS)				
	435200.0	435300.0	435400.0	435500.0	435600.0
352700.0 /	173.02234 (302, 1)	180.18176 (302, 1)	184.70370 (302, 1)	186.17941 (302, 1)	185.03830 (302, 1)
352600.0 /	183.62991 (302, 1)	186.54588 (302, 1)	186.73654 (302, 1)	185.08850 (302, 1)	183.02628 (302, 1)
352500.0 /	186.46841 (302, 1)	185.99094 (302, 1)	184.42694 (302, 1)	182.91960 (302, 1)	181.97021 (302, 1)
352400.0 /	184.51608 (302, 1)	183.37112 (302, 1)	182.40520 (302, 1)	181.56628 (302, 1)	179.91008 (302, 1)
352300.0 /	182.05675 (302, 1)	181.48859 (302, 1)	180.54492 (302, 1)	178.29681 (302, 1)	174.24173 (302, 1)
352200.0 /	180.17343 (302, 1)	178.99016 (302, 1)	176.22147 (302, 1)	171.86444 (302, 1)	173.46600 (356, 1)
352100.0 /	176.97778 (302, 1)	173.84573 (302, 1)	169.42126 (302, 1)	174.65239 (356, 1)	187.64838 (356, 1)
352000.0 /	171.25299 (302, 1)	166.98981 (302, 1)	175.33374 (356, 1)	187.82639 (356, 1)	202.39633 (356, 1)
351900.0 /	165.91713 (356, 1)	175.53537 (356, 1)	187.53392 (356, 1)	201.19067 (356, 1)	214.42938 (356, 1)
351800.0 /	175.35483 (356, 1)	186.81210 (356, 1)	199.61505 (356, 1)	211.92783 (356, 1)	221.88208 (356, 1)
351700.0 /	185.79581 (356, 1)	197.77869 (356, 1)	209.19864 (356, 1)	218.52196 (356, 1)	230.57907 (302, 1)
351600.0 /	195.76700 (356, 1)	206.38086 (356, 1)	215.08780 (356, 1)	226.51268 (302, 1)	250.74707 (302, 1)
351500.0 /	203.50931 (356, 1)	211.65393 (356, 1)	222.47319 (302, 1)	245.56625 (302, 1)	267.75082 (302, 1)
351400.0 /	208.24307 (356, 1)	218.50116 (302, 1)	240.44534 (302, 1)	261.91101 (302, 1)	280.16382 (302, 1)
351300.0 /	214.62427 (302, 1)	235.43260 (302, 1)	256.09280 (302, 1)	274.30713 (302, 1)	286.86475 (302, 1)
351200.0 /	230.56145 (302, 1)	250.36453 (302, 1)	268.33618 (302, 1)	281.73596 (302, 1)	287.38586 (302, 1)
351100.0 /	244.77434 (302, 1)	262.35416 (302, 1)	276.26166 (302, 1)	283.64215 (302, 1)	282.23480 (302, 1)
351000.0 /	256.43747 (302, 1)	270.58887 (302, 1)	279.28210 (302, 1)	280.22867 (302, 1)	272.85455 (302, 1)
350900.0 /	264.83148 (302, 1)	274.48474 (302, 1)	277.38983 (302, 1)	272.51483 (302, 1)	261.21420 (302, 1)
350800.0 /	269.39709 (302, 1)	273.89478 (302, 1)	271.26700 (302, 1)	262.09006 (302, 1)	249.25591 (302, 1)
350700.0 /	269.90045 (302, 1)	269.24051 (302, 1)	262.15680 (302, 1)	250.69141 (302, 1)	238.44754 (302, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 331.04660 AND OCCURRED AT (436700.0, 352100.0) *

Y-AXIS (METERS) /	X-AXIS (METERS)				
	435700.0	435800.0	435900.0	436000.0	436100.0
352700.0 /	182.66093 (302, 1)	180.78488 (302, 1)	180.16373 (302, 1)	179.48718 (302, 1)	176.53038 (302, 1)
352600.0 /	181.71057 (302, 1)	181.01138 (302, 1)	179.31931 (302, 1)	175.35233 (302, 1)	176.34436 (356, 1)
352500.0 /	180.87686 (302, 1)	178.19409 (302, 1)	173.64714 (302, 1)	180.36392 (356, 1)	199.71539 (356, 1)
352400.0 /	176.41638 (302, 1)	171.68402 (302, 1)	183.39148 (356, 1)	201.88969 (356, 1)	221.21262 (356, 1)
352300.0 /	171.70651 (356, 1)	185.53789 (356, 1)	203.07683 (356, 1)	221.03809 (356, 1)	234.82120 (356, 1)
352200.0 /	186.91959 (356, 1)	203.45789 (356, 1)	220.11383 (356, 1)	233.08232 (356, 1)	246.38312 (302, 1)
352100.0 /	203.18781 (356, 1)	218.61601 (356, 1)	230.77713 (356, 1)	244.17937 (302, 1)	271.84393 (302, 1)
352000.0 /	216.68439 (356, 1)	228.06549 (356, 1)	241.32536 (302, 1)	268.77042 (302, 1)	290.43549 (302, 1)
351900.0 /	225.06949 (356, 1)	238.01511 (302, 1)	264.92029 (302, 1)	287.50241 (302, 1)	299.31189 (302, 1)
351800.0 /	234.40118 (302, 1)	260.53894 (302, 1)	283.51349 (302, 1)	297.85056 (302, 1)	297.61530 (302, 1)
351700.0 /	255.81696 (302, 1)	278.78723 (302, 1)	294.89380 (302, 1)	298.64624 (302, 1)	287.40921 (302, 1)
351600.0 /	273.51810 (302, 1)	290.83649 (302, 1)	297.77176 (302, 1)	290.98938 (302, 1)	272.83859 (302, 1)
351500.0 /	285.76813 (302, 1)	295.29068 (302, 1)	292.56854 (302, 1)	277.99655 (302, 1)	263.73438 (357, 1)
351400.0 /	291.46094 (302, 1)	292.13806 (302, 1)	281.36157 (302, 1)	263.44748 (302, 1)	275.31229 (357, 1)
351300.0 /	290.29999 (302, 1)	282.98608 (302, 1)	267.46048 (302, 1)	262.16968 (357, 1)	286.14606 (357, 1)
351200.0 /	283.21817 (302, 1)	270.38297 (302, 1)	253.87979 (302, 1)	272.36386 (357, 1)	293.59116 (357, 1)
351100.0 /	272.17148 (302, 1)	257.03763 (302, 1)	259.38831 (357, 1)	281.04190 (357, 1)	296.06290 (357, 1)
351000.0 /	259.51688 (302, 1)	247.62732 (357, 1)	268.16925 (357, 1)	286.27521 (357, 1)	293.11603 (357, 1)
350900.0 /	247.32791 (302, 1)	255.75522 (357, 1)	274.95538 (357, 1)	287.01447 (357, 1)	285.29456 (357, 1)
350800.0 /	244.24632 (357, 1)	263.10583 (357, 1)	278.37610 (357, 1)	283.13431 (357, 1)	273.73117 (357, 1)
350700.0 /	251.43652 (357, 1)	268.23303 (357, 1)	277.80200 (357, 1)	275.20847 (357, 1)	259.77490 (357, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 331.04660 AND OCCURRED AT (436700.0, 352100.0) *

Y-AXIS / (METERS) /	X-AXIS (METERS)				
	436200.0	436300.0	436400.0	436500.0	436600.0
352700.0 /	172.12891 (302, 1)	191.57758 (356, 1)	214.80194 (356, 1)	231.00896 (356, 1)	240.80144 (356, 1)
352600.0 /	196.35010 (356, 1)	218.38754 (356, 1)	234.25883 (356, 1)	244.59850 (356, 1)	261.96738 (302, 1)
352500.0 /	220.41833 (356, 1)	235.71182 (356, 1)	246.38837 (302, 1)	268.98730 (302, 1)	277.72626 (356, 1)
352400.0 /	235.78659 (356, 1)	247.81458 (302, 1)	272.91171 (302, 1)	282.22693 (302, 1)	278.47366 (356, 1)
352300.0 /	247.69414 (302, 1)	274.34296 (302, 1)	288.42902 (302, 1)	286.29065 (356, 1)	273.48529 (357, 1)
352200.0 /	273.83044 (302, 1)	291.43835 (302, 1)	289.69092 (302, 1)	275.90149 (356, 1)	296.00656 (357, 1)
352100.0 /	291.91180 (302, 1)	295.78909 (302, 1)	284.48810 (356, 1)	283.26178 (357, 1)	317.05835 (357, 1)
352000.0 /	298.80496 (302, 1)	288.46848 (356, 1)	271.97937 (357, 1)	303.20560 (357, 1)	329.10919 (357, 1)
351900.0 /	294.25598 (302, 1)	276.90332 (356, 1)	288.73694 (357, 1)	319.24158 (357, 1)	328.79962 (357, 1)
351800.0 /	281.90509 (356, 1)	275.41986 (357, 1)	305.42236 (357, 1)	326.32556 (357, 1)	317.35089 (357, 1)
351700.0 /	266.95972 (356, 1)	290.56464 (357, 1)	316.99274 (357, 1)	322.96124 (357, 1)	298.50076 (357, 1)
351600.0 /	276.40247 (357, 1)	303.90408 (357, 1)	320.30627 (357, 1)	310.70807 (357, 1)	276.41733 (357, 1)
351500.0 /	289.48102 (357, 1)	311.75867 (357, 1)	314.92825 (357, 1)	292.64243 (357, 1)	254.47665 (357, 1)
351400.0 /	299.72723 (357, 1)	312.29443 (357, 1)	302.44147 (357, 1)	272.01678 (357, 1)	234.83191 (357, 1)
351300.0 /	304.60913 (357, 1)	305.64746 (357, 1)	285.35144 (357, 1)	251.48997 (357, 1)	218.46025 (357, 1)
351200.0 /	303.03976 (357, 1)	293.24954 (357, 1)	266.21475 (357, 1)	232.83952 (357, 1)	205.43576 (357, 1)
351100.0 /	295.54694 (357, 1)	277.10724 (357, 1)	247.06668 (357, 1)	216.94794 (357, 1)	195.27112 (357, 1)
351000.0 /	283.46420 (357, 1)	259.35153 (357, 1)	229.46213 (357, 1)	204.00049 (357, 1)	187.17407 (357, 1)
350900.0 /	268.44550 (357, 1)	241.66400 (357, 1)	214.23766 (357, 1)	193.77310 (357, 1)	180.47038 (357, 1)
350800.0 /	252.10612 (357, 1)	225.25174 (357, 1)	201.65268 (357, 1)	185.70956 (357, 1)	174.55418 (357, 1)
350700.0 /	235.80302 (357, 1)	210.83673 (357, 1)	191.56146 (357, 1)	179.18088 (357, 1)	169.00543 (357, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 331.04660 AND OCCURRED AT (436700.0, 352100.0) *

Y-AXIS (METERS) /	X-AXIS (METERS)				
	436700.0	436800.0	436900.0	437000.0	437100.0
352700.0 /	255.71121 (356, 1)	256.34564 (356, 1)	265.57858 (357, 1)	293.10657 (357, 1)	260.25427 (357, 1)
352600.0 /	270.35638 (356, 1)	262.28201 (357, 1)	297.77576 (357, 1)	297.91559 (357, 1)	240.16283 (357, 1)
352500.0 /	264.35110 (356, 1)	291.93182 (357, 1)	316.10052 (357, 1)	283.34348 (357, 1)	220.15845 (357, 1)
352400.0 /	282.61066 (357, 1)	317.36685 (357, 1)	314.05212 (357, 1)	260.10791 (357, 1)	204.58984 (357, 1)
352300.0 /	308.61804 (357, 1)	327.70630 (357, 1)	296.44827 (357, 1)	237.11411 (357, 1)	193.22440 (357, 1)
352200.0 /	326.90131 (357, 1)	320.91077 (357, 1)	272.04492 (357, 1)	218.49878 (357, 1)	184.26859 (357, 1)
352100.0 /	331.04660 (357, 1)	301.93060 (357, 1)	247.92172 (357, 1)	204.65219 (357, 1)	176.19690 (357, 1)
352000.0 /	321.27893 (357, 1)	277.66171 (357, 1)	227.72720 (357, 1)	194.20288 (357, 1)	168.28494 (357, 1)
351900.0 /	302.02545 (357, 1)	253.63614 (357, 1)	212.21497 (357, 1)	185.50995 (357, 1)	160.43170 (357, 1)
351800.0 /	278.65082 (357, 1)	232.96439 (357, 1)	200.52861 (357, 1)	177.50439 (357, 1)	152.90730 (357, 1)
351700.0 /	255.46976 (357, 1)	216.60040 (357, 1)	191.29393 (357, 1)	169.69070 (357, 1)	146.02066 (357, 1)
351600.0 /	235.08206 (357, 1)	204.10449 (357, 1)	183.31169 (357, 1)	162.01376 (357, 1)	140.00008 (357, 1)
351500.0 /	218.49321 (357, 1)	194.41869 (357, 1)	175.82217 (357, 1)	154.64081 (357, 1)	134.96013 (357, 1)
351400.0 /	205.57227 (357, 1)	186.43295 (357, 1)	168.49551 (357, 1)	147.79465 (357, 1)	130.91144 (357, 1)
351300.0 /	195.57126 (357, 1)	179.29092 (357, 1)	161.30197 (357, 1)	141.66013 (357, 1)	127.78921 (357, 1)
351200.0 /	187.55719 (357, 1)	172.47922 (357, 1)	154.36737 (357, 1)	136.34851 (357, 1)	125.48314 (357, 1)
351100.0 /	180.69638 (357, 1)	165.78586 (357, 1)	147.86256 (357, 1)	131.89618 (357, 1)	123.86195 (357, 1)
351000.0 /	174.35466 (357, 1)	159.19022 (357, 1)	141.93793 (357, 1)	128.27908 (357, 1)	122.79128 (357, 1)
350900.0 /	168.20947 (357, 1)	152.77722 (357, 1)	136.65532 (357, 1)	125.40446 (357, 1)	122.12164 (357, 1)
350800.0 /	162.15726 (357, 1)	146.72784 (357, 1)	132.10800 (357, 1)	123.19957 (357, 1)	121.74014 (357, 1)
350700.0 /	156.20558 (357, 1)	141.16248 (357, 1)	128.29498 (357, 1)	121.57744 (357, 1)	121.57851 (357, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 331.04660 AND OCCURRED AT (436700.0, 352100.0) *

Y-AXIS / X-AXIS (METERS)
(METERS) / 437200.0

352700.0 /	196.74554 (357, 1)
352600.0 /	185.72491 (357, 1)
352500.0 /	177.46097 (357, 1)
352400.0 /	170.12601 (357, 1)
352300.0 /	162.77202 (357, 1)
352200.0 /	155.35628 (357, 1)
352100.0 /	148.26128 (357, 1)
352000.0 /	141.90631 (357, 1)
351900.0 /	136.56546 (357, 1)
351800.0 /	132.34282 (357, 1)
351700.0 /	129.20213 (357, 1)
351600.0 /	127.01522 (357, 1)
351500.0 /	125.61194 (357, 1)
351400.0 /	124.81313 (357, 1)
351300.0 /	124.45083 (357, 1)
351200.0 /	124.37939 (357, 1)
351100.0 /	124.47951 (357, 1)
351000.0 /	124.65831 (357, 1)
350900.0 /	124.82699 (357, 1)
350800.0 /	124.92245 (357, 1)
350700.0 /	124.95572 (357, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 289.04456 AND OCCURRED AT (436400.0, 352200.0) *

Y-AXIS / (METERS) /	435200.0	435300.0	X-AXIS (METERS) 435400.0	435500.0	435600.0
352700.0 /	131.40512 (356, 1)	134.12534 (356, 1)	136.12143 (356, 1)	137.45479 (356, 1)	138.38834 (356, 1)
352600.0 /	132.38419 (356, 1)	134.72701 (356, 1)	136.59357 (356, 1)	138.27449 (356, 1)	140.24463 (356, 1)
352500.0 /	133.46794 (356, 1)	135.91000 (356, 1)	138.36098 (356, 1)	141.23755 (356, 1)	144.97638 (356, 1)
352400.0 /	135.40326 (356, 1)	138.60002 (356, 1)	142.28688 (356, 1)	146.76964 (356, 1)	152.32985 (356, 1)
352300.0 /	138.92667 (356, 1)	143.29602 (356, 1)	148.35040 (356, 1)	154.31815 (356, 1)	161.73273 (356, 1)
352200.0 /	144.18613 (356, 1)	149.65717 (356, 1)	155.89771 (356, 1)	163.47736 (356, 1)	167.62378 (302, 1)
352100.0 /	150.64426 (356, 1)	157.07246 (356, 1)	164.73718 (356, 1)	165.69266 (302, 1)	166.00668 (302, 1)
352000.0 /	157.82542 (356, 1)	165.54172 (356, 1)	163.87326 (302, 1)	164.97440 (302, 1)	173.20532 (302, 1)
351900.0 /	164.60385 (302, 1)	162.14130 (302, 1)	163.96051 (302, 1)	172.46928 (302, 1)	188.64136 (302, 1)
351800.0 /	160.51651 (302, 1)	162.92081 (302, 1)	171.58885 (302, 1)	187.27147 (302, 1)	208.97159 (302, 1)
351700.0 /	161.90617 (302, 1)	170.60759 (302, 1)	185.68442 (302, 1)	206.31723 (302, 1)	226.02011 (356, 1)
351600.0 /	169.57379 (302, 1)	184.02716 (302, 1)	203.55121 (302, 1)	222.13150 (356, 1)	230.07414 (356, 1)
351500.0 /	182.32602 (302, 1)	200.78024 (302, 1)	218.27539 (356, 1)	225.56670 (356, 1)	236.66081 (356, 1)
351400.0 /	198.03125 (302, 1)	214.47466 (356, 1)	221.18871 (356, 1)	231.19724 (356, 1)	245.89810 (356, 1)
351300.0 /	210.74449 (356, 1)	216.94675 (356, 1)	225.99063 (356, 1)	239.43028 (356, 1)	255.63501 (356, 1)
351200.0 /	212.84320 (356, 1)	221.03384 (356, 1)	233.27994 (356, 1)	248.67383 (356, 1)	262.96265 (356, 1)
351100.0 /	216.31534 (356, 1)	227.45378 (356, 1)	241.91772 (356, 1)	256.43164 (356, 1)	265.76453 (356, 1)
351000.0 /	221.94597 (356, 1)	235.42949 (356, 1)	249.80542 (356, 1)	260.60281 (356, 1)	263.45642 (356, 1)
350900.0 /	229.24225 (356, 1)	243.22739 (356, 1)	254.94943 (356, 1)	260.26013 (356, 1)	256.82544 (356, 1)
350800.0 /	236.79544 (356, 1)	249.01477 (356, 1)	256.21515 (356, 1)	255.71115 (356, 1)	247.37564 (356, 1)
350700.0 /	242.96039 (356, 1)	251.55444 (356, 1)	253.53105 (356, 1)	248.06743 (356, 1)	236.65042 (356, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 289.04456 AND OCCURRED AT (436400.0, 352200.0) *

Y-AXIS (METERS) /	X-AXIS (METERS)				
	435700.0	435800.0	435900.0	436000.0	436100.0
352700.0 /	139.40959 (356, 1)	141.17448 (356, 1)	144.35422 (356, 1)	149.56926 (356, 1)	157.82912 (356, 1)
352600.0 /	143.06761 (356, 1)	147.25951 (356, 1)	153.34750 (356, 1)	162.38411 (356, 1)	171.32555 (302, 1)
352500.0 /	149.95605 (356, 1)	156.66866 (356, 1)	166.21190 (356, 1)	170.32672 (302, 1)	174.34811 (302, 1)
352400.0 /	159.46867 (356, 1)	169.30751 (356, 1)	169.24734 (302, 1)	174.57562 (302, 1)	191.32903 (302, 1)
352300.0 /	169.64040 (302, 1)	168.15018 (302, 1)	174.53445 (302, 1)	191.60741 (302, 1)	217.77916 (302, 1)
352200.0 /	167.06595 (302, 1)	174.26805 (302, 1)	191.38327 (302, 1)	216.92731 (302, 1)	242.84033 (356, 1)
352100.0 /	173.81418 (302, 1)	190.75870 (302, 1)	215.48405 (302, 1)	240.09673 (356, 1)	252.28070 (356, 1)
352000.0 /	189.82054 (302, 1)	213.59982 (302, 1)	236.91753 (356, 1)	248.09930 (356, 1)	265.84454 (356, 1)
351900.0 /	211.39658 (302, 1)	233.44666 (356, 1)	243.69342 (356, 1)	260.04294 (356, 1)	279.30807 (356, 1)
351800.0 /	229.79150 (356, 1)	239.18158 (356, 1)	254.10526 (356, 1)	273.12637 (356, 1)	286.29306 (356, 1)
351700.0 /	234.64549 (356, 1)	248.19232 (356, 1)	266.44476 (356, 1)	281.88428 (356, 1)	283.58942 (356, 1)
351600.0 /	242.38042 (356, 1)	259.58636 (356, 1)	276.19855 (356, 1)	282.59473 (356, 1)	272.45993 (356, 1)
351500.0 /	252.65562 (356, 1)	269.69177 (356, 1)	279.55396 (356, 1)	275.16095 (356, 1)	258.15848 (302, 1)
351400.0 /	262.69586 (356, 1)	274.86017 (356, 1)	275.35080 (356, 1)	262.15088 (356, 1)	246.12981 (302, 1)
351300.0 /	269.19678 (356, 1)	273.49127 (356, 1)	265.17511 (356, 1)	250.21196 (302, 1)	237.49960 (302, 1)
351200.0 /	270.16898 (356, 1)	266.21008 (356, 1)	251.72720 (356, 1)	239.96762 (302, 1)	231.58493 (302, 1)
351100.0 /	265.53717 (356, 1)	255.02026 (356, 1)	242.51984 (302, 1)	232.75182 (302, 1)	227.21796 (302, 1)
351000.0 /	256.66254 (356, 1)	245.02959 (302, 1)	234.01068 (302, 1)	227.70621 (302, 1)	223.18170 (302, 1)
350900.0 /	245.43457 (356, 1)	235.42809 (302, 1)	227.98981 (302, 1)	223.70819 (302, 1)	218.66771 (302, 1)
350800.0 /	236.94656 (302, 1)	228.34209 (302, 1)	223.58672 (302, 1)	219.80846 (302, 1)	213.31071 (302, 1)
350700.0 /	228.87254 (302, 1)	223.23596 (302, 1)	219.86374 (302, 1)	215.41272 (302, 1)	207.06090 (302, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 289.04456 AND OCCURRED AT (436400.0, 352200.0) *

Y-AXIS (METERS) /	X-AXIS (METERS)				
	436700.0	436800.0	436900.0	437000.0	437100.0
352700.0 /	251.26927 (302, 1)	239.13562 (357, 1)	216.02856 (356, 1)	182.78935 (302, 1)	163.55821 (302, 1)
352600.0 /	257.75320 (302, 1)	243.28589 (356, 1)	199.56732 (302, 1)	180.95824 (302, 1)	158.24083 (302, 1)
352500.0 /	258.93219 (357, 1)	219.17668 (356, 1)	196.67422 (302, 1)	176.63022 (302, 1)	151.97104 (302, 1)
352400.0 /	242.81989 (356, 1)	210.87363 (302, 1)	193.69144 (302, 1)	169.71526 (302, 1)	146.21632 (302, 1)
352300.0 /	224.56932 (302, 1)	207.64801 (302, 1)	188.12041 (302, 1)	161.68562 (302, 1)	141.68408 (302, 1)
352200.0 /	219.12390 (302, 1)	203.67700 (302, 1)	180.11530 (302, 1)	153.95500 (302, 1)	138.39246 (302, 1)
352100.0 /	215.51563 (302, 1)	197.26749 (302, 1)	170.92932 (302, 1)	147.36716 (302, 1)	135.95096 (302, 1)
352000.0 /	210.80034 (302, 1)	188.62590 (302, 1)	161.76030 (302, 1)	142.18739 (302, 1)	133.84842 (302, 1)
351900.0 /	203.86560 (302, 1)	178.77910 (302, 1)	153.46857 (302, 1)	138.24686 (302, 1)	131.64989 (302, 1)
351800.0 /	194.98444 (302, 1)	168.75687 (302, 1)	146.51834 (302, 1)	135.17737 (302, 1)	129.08627 (302, 1)
351700.0 /	184.95453 (302, 1)	159.35031 (302, 1)	140.96747 (302, 1)	132.52969 (302, 1)	126.04832 (302, 1)
351600.0 /	174.59581 (302, 1)	151.05818 (302, 1)	136.60042 (302, 1)	129.92760 (302, 1)	122.54834 (302, 1)
351500.0 /	164.58409 (302, 1)	144.08824 (302, 1)	133.06354 (302, 1)	127.12091 (302, 1)	118.67187 (302, 1)
351400.0 /	155.41032 (302, 1)	138.39835 (302, 1)	129.98503 (302, 1)	123.98650 (302, 1)	114.53625 (302, 1)
351300.0 /	147.36371 (302, 1)	133.77380 (302, 1)	127.05294 (302, 1)	120.50155 (302, 1)	110.26238 (302, 1)
351200.0 /	140.53302 (302, 1)	129.91843 (302, 1)	124.04937 (302, 1)	116.70996 (302, 1)	105.95886 (302, 1)
351100.0 /	134.83881 (302, 1)	126.53197 (302, 1)	120.85190 (302, 1)	112.69167 (302, 1)	101.71463 (302, 1)
351000.0 /	130.07031 (302, 1)	123.35083 (302, 1)	117.41692 (302, 1)	108.53951 (302, 1)	97.59776 (302, 1)
350900.0 /	125.99026 (302, 1)	120.17212 (302, 1)	113.72162 (302, 1)	104.32226 (302, 1)	93.64801 (302, 1)
350800.0 /	122.37881 (302, 1)	116.91507 (302, 1)	109.85823 (302, 1)	100.14211 (302, 1)	89.90155 (302, 1)
350700.0 /	119.03000 (302, 1)	113.52767 (302, 1)	105.89272 (302, 1)	96.07271 (302, 1)	86.46465 (356, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 289.04456 AND OCCURRED AT (436400.0, 352200.0) *

Y-AXIS / X-AXIS (METERS)
(METERS) / 437200.0

352700.0 / 143.09602 (302, 1)
352600.0 / 139.55420 (302, 1)
352500.0 / 137.02605 (302, 1)
352400.0 / 135.25446 (302, 1)
352300.0 / 133.71313 (302, 1)
352200.0 / 131.92772 (302, 1)
352100.0 / 129.61954 (302, 1)
352000.0 / 126.70943 (302, 1)
351900.0 / 123.25778 (302, 1)
351800.0 / 119.39635 (302, 1)
351700.0 / 115.27638 (302, 1)
351600.0 / 111.03809 (302, 1)
351500.0 / 106.79678 (302, 1)
351400.0 / 102.63980 (302, 1)
351300.0 / 98.62844 (302, 1)
351200.0 / 94.80288 (302, 1)
351100.0 / 91.18676 (302, 1)
351000.0 / 88.51833 (356, 1)
350900.0 / 86.83888 (356, 1)
350800.0 / 85.11970 (356, 1)
350700.0 / 83.37201 (356, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* SECOND HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE RECEPTOR GRID *

* MAXIMUM VALUE EQUALS 289.04456 AND OCCURRED AT (436400.0, 352200.0) *

Y-AXIS / (METERS) /	X-AXIS (METERS)				
	436200.0	436300.0	436400.0	436500.0	436600.0
352700.0 /	171.24693 (356, 1)	172.88058 (302, 1)	186.27263 (302, 1)	211.17416 (302, 1)	237.23216 (302, 1)
352600.0 /	173.80225 (302, 1)	188.78990 (302, 1)	214.80832 (302, 1)	243.00693 (302, 1)	260.45355 (356, 1)
352500.0 /	190.43213 (302, 1)	216.94896 (302, 1)	246.21603 (356, 1)	262.01141 (356, 1)	272.17252 (302, 1)
352400.0 /	217.85791 (302, 1)	246.19275 (356, 1)	261.36053 (356, 1)	280.14194 (356, 1)	266.34711 (302, 1)
352300.0 /	244.95685 (356, 1)	259.21100 (356, 1)	279.12961 (356, 1)	279.98596 (302, 1)	262.03577 (356, 1)
352200.0 /	256.06665 (356, 1)	275.88071 (356, 1)	289.04456 (356, 1)	266.87250 (302, 1)	238.23514 (356, 1)
352100.0 /	271.25507 (356, 1)	288.06433 (356, 1)	279.06375 (302, 1)	255.09256 (356, 1)	229.39456 (302, 1)
352000.0 /	284.51309 (356, 1)	288.16959 (302, 1)	268.05206 (356, 1)	239.27814 (302, 1)	224.51129 (302, 1)
351900.0 /	288.76053 (356, 1)	273.54248 (302, 1)	248.91319 (302, 1)	231.97903 (302, 1)	220.55028 (302, 1)
351800.0 /	281.61938 (302, 1)	258.39758 (356, 1)	238.87268 (302, 1)	227.45667 (302, 1)	215.34843 (302, 1)
351700.0 /	266.09814 (302, 1)	245.59215 (302, 1)	232.73026 (302, 1)	223.23288 (302, 1)	208.19853 (302, 1)
351600.0 /	252.10501 (302, 1)	237.32047 (302, 1)	228.43500 (302, 1)	217.76462 (302, 1)	199.36174 (302, 1)
351500.0 /	241.74199 (302, 1)	232.02928 (302, 1)	224.04578 (302, 1)	210.61090 (302, 1)	189.45543 (302, 1)
351400.0 /	234.89037 (302, 1)	227.88554 (302, 1)	218.47806 (302, 1)	202.00339 (302, 1)	179.11896 (302, 1)
351300.0 /	230.21074 (302, 1)	223.41795 (302, 1)	211.46140 (302, 1)	192.41551 (302, 1)	168.90747 (302, 1)
351200.0 /	226.05370 (302, 1)	217.82486 (302, 1)	203.19322 (302, 1)	182.33946 (302, 1)	159.26677 (302, 1)
351100.0 /	221.44243 (302, 1)	210.90045 (302, 1)	193.94531 (302, 1)	172.19376 (302, 1)	150.51352 (302, 1)
351000.0 /	215.88809 (302, 1)	202.93736 (302, 1)	184.19727 (302, 1)	162.35367 (302, 1)	142.77890 (302, 1)
350900.0 /	209.29901 (302, 1)	194.20976 (302, 1)	174.32083 (302, 1)	153.19049 (302, 1)	136.13866 (302, 1)
350800.0 /	201.80984 (302, 1)	184.99774 (302, 1)	164.62672 (302, 1)	144.90607 (302, 1)	130.50581 (302, 1)
350700.0 /	193.62877 (302, 1)	175.56607 (302, 1)	155.38773 (302, 1)	137.59438 (302, 1)	125.71307 (302, 1)

*** ISC RUN FOR JAX ELEC. AUTH. SHORT STACKS (GLC, OCT 2, 1981) ***

* 50 MAXIMUM 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *

* FROM ALL SOURCES *

RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y(METERS) OR DIRECTION (DEGREES)	RANK	CON.	PER.	DAY	X OR RANGE (METERS)	Y(METERS) OR DIRECTION (DEGREES)
1	331.04660	1	357	436700.0	352100.0	26	303.90408	1	357	436300.0	351600.0
2	329.10919	1	357	436600.0	352000.0	27	303.20560	1	357	436500.0	352000.0
3	328.79962	1	357	436600.0	351900.0	28	303.03976	1	357	436200.0	351200.0
4	327.70630	1	357	436800.0	352300.0	29	302.44147	1	357	436400.0	351400.0
5	326.90131	1	357	436700.0	352200.0	30	302.02545	1	357	436700.0	351900.0
6	326.32556	1	357	436500.0	351800.0	31	301.93060	1	357	436800.0	352100.0
7	322.96124	1	357	436500.0	351700.0	32	299.72723	1	357	436200.0	351400.0
8	321.27893	1	357	436700.0	352000.0	33	299.31189	1	302	436100.0	351900.0
9	320.91077	1	357	436800.0	352200.0	34	298.80496	1	302	436200.0	352000.0
10	320.30627	1	357	436400.0	351600.0	35	298.64624	1	302	436000.0	351700.0
11	319.24158	1	357	436500.0	351900.0	36	298.50076	1	357	436600.0	351700.0
12	317.36685	1	357	436800.0	352400.0	37	297.91559	1	357	437000.0	352600.0
13	317.35089	1	357	436600.0	351800.0	38	297.85056	1	302	436000.0	351800.0
14	317.05835	1	357	436600.0	352100.0	39	297.77576	1	357	436900.0	352600.0
15	316.99274	1	357	436400.0	351700.0	40	297.77176	1	302	435900.0	351600.0
16	316.10052	1	357	436900.0	352500.0	41	297.61530	1	302	436100.0	351800.0
17	314.92825	1	357	436400.0	351500.0	42	296.44827	1	357	436900.0	352300.0
18	314.05212	1	357	436900.0	352400.0	43	296.06290	1	357	436100.0	351100.0
19	312.29443	1	357	436300.0	351400.0	44	296.00656	1	357	436600.0	352200.0
20	311.75867	1	357	436300.0	351500.0	45	295.78909	1	302	436300.0	352100.0
21	310.70807	1	357	436500.0	351600.0	46	295.54694	1	357	436200.0	351100.0
22	308.61804	1	357	436700.0	352300.0	47	295.29068	1	302	435800.0	351500.0
23	305.64746	1	357	436300.0	351300.0	48	294.89380	1	302	435900.0	351700.0
24	305.42236	1	357	436400.0	351800.0	49	294.25598	1	302	436200.0	351900.0
25	304.60913	1	357	436200.0	351300.0	50	293.59116	1	357	436100.0	351200.0

ATTACHMENT 2

TOTAL SUSPENDED PARTICULATES

The issue evaluated with respect to compliance with the NAAQS for TSP involved the predicted impact of SJRPP in the vicinity of Southside and Kennedy. The question of the impacts in the vicinities of Southside and Kennedy due to lower than originally modelled stack heights at those two sources is only relevant to SJRPP licensing if SJRPP has a significant effect on TSP concentrations in those vicinities.

Downtown Jacksonville is currently designated as nonattainment for TSP. Specifically, that portion of the downtown area bordered on the east and south by the St. Johns River, on the west by Interstate 95 and on the north by the Trout River is the nonattainment area. The Kennedy Plant is contained within this area and the Southside Plant is located just across the St. Johns River to the south of this area. SJRPP is located to the northeast of the nonattainment area and is 9.4 km away from the closest boundary.

The impacts of SJRPP in the vicinity of Southside and Kennedy can be inferred from the modelling of TSP impacts already conducted. The short-term modelling results, which were attached to a letter from D. A. Moehle to K. Williams dated October 21, 1981, indicated a maximum TSP 24-hour average impact on the boundary of the nonattainment area closest to SJRPP of 4.3 ug/m^3 (see attached ISCST printout reproduced from the October 21, 1981 letter). Since both Southside and Kennedy are farther from SJRPP than the boundary of the nonattainment area, it can be concluded that the 24-hour average TSP impact from SJRPP is also below the significance level of 5 ug/m^3 in their vicinities. The long-term modelling results, which were described in the PSD application, indicated a maximum annual TSP impact at the nonattainment area boundary of less than the 1 ug/m^3 significance level (see attached CRSTER printout). Thus, the TSP impact at Southside and Kennedy is also expected to be below the annual significance level.

Since SJRPP impacts on TSP concentrations will not be significant around Southside and Kennedy, the stack height question is not relevant to the SJRPP PSD permit with respect to TSP.

ISCST ANALYSIS
OF MAXIMUM 24-HOUR AVERAGE
TSP IMPACT ON NONATTAINMENT AREA

CALCULATE (CONCENTRATION=1, DEPOSITION=2)	ISW(1) = 1
RECEPTOR GRID SYSTEM (RECTANGULAR=1 OR 3, POLAR=2 OR 4)	ISW(2) = 1
DISCRETE RECEPTOR SYSTEM (RECTANGULAR=1, POLAR=2)	ISW(3) = 1
TERRAIN ELEVATIONS ARE READ (YES=1, NO=0)	ISW(4) = 0
CALCULATIONS ARE WRITTEN TO TAPE (YES=1, NO=0)	ISW(5) = 0
LIST ALL INPUT DATA (NO=0, YES=1, MET DATA ALSO=2)	ISW(6) = 1

COMPUTE AVERAGE CONCENTRATION (OR TOTAL DEPOSITION) WITH THE FOLLOWING TIME PERIODS:	
HOURLY (YES=1, NO=0)	ISW(7) = 0
2-HOUR (YES=1, NO=0)	ISW(8) = 0
3-HOUR (YES=1, NO=0)	ISW(9) = 0
4-HOUR (YES=1, NO=0)	ISW(10) = 0
6-HOUR (YES=1, NO=0)	ISW(11) = 0
8-HOUR (YES=1, NO=0)	ISW(12) = 0
12-HOUR (YES=1, NO=0)	ISW(13) = 0
24-HOUR (YES=1, NO=0)	ISW(14) = 1
PRINT *N*-DAY TABLE(S) (YES=1, NO=0)	ISW(15) = 1

PRINT THE FOLLOWING TYPES OF TABLES WHOSE TIME PERIODS ARE SPECIFIED BY ISW(7) THROUGH ISW(14):	
DAILY TABLES (YES=1, NO=0)	ISW(16) = 0
HIGHEST & SECOND HIGHEST TABLES (YES=1, NO=0)	ISW(17) = 1
MAXIMUM 50 TABLES (YES=1, NO=0)	ISW(18) = 1
METEOROLOGICAL DATA INPUT METHOD (PRE-PROCESSED=1, CARD=2)	ISW(19) = 1
RURAL-URBAN OPTION (RURAL=0, URBAN MODF 1=1, URBAN MODE 2=2)	ISW(20) = 0
WIND PROFILE EXPONENT VALUES (DEFAULTS=1, USER ENTERS=2, 3)	ISW(21) = 1
VERTICAL POT. TEMP. GRADIENT VALUES (DEFAULTS=1, USER ENTERS=2, 3)	ISW(22) = 1
SCALE EMISSION RATES FOR ALL SOURCES (NO=0, YES=1)	ISW(23) = 0
PROGRAM CALCULATES FINAL PLUME RISE ONLY (YES=1, NO=2)	ISW(24) = 1
PROGRAM ADJUSTS ALL STACK HEIGHTS FOR DOWNWASH (YES=2, NO=1)	ISW(25) = 1

NUMBER OF INPUT SOURCES	NSOURC = 14
NUMBER OF SOURCE GROUPS (=0, ALL SOURCES)	NGROUP = 0
TIME PERIOD INTERVAL TO BE PRINTED (=0, ALL INTERVALS)	IPERD = 0
NUMBER OF X (RANGE) GRID VALUES	NXPNTS = 0
NUMBER OF Y (THETA) GRID VALUES	NYPNTS = 0
NUMBER OF DISCRETE RECEPTORS	NXWYPT = 22
SOURCE EMISSION RATE UNITS CONVERSION FACTOR	TK = .10000E+07
ENTRAINMENT COEFFICIENT FOR UNSTABLE ATMOSPHERE	BETA1 = 0.600
ENTRAINMENT COEFFICIENT FOR STABLE ATMOSPHERE	BETA2 = 0.600
HEIGHT ABOVE GROUND AT WHICH WIND SPEED WAS MEASURED	ZR = 10.00 METERS
LOGICAL UNIT NUMBER OF METEOROLOGICAL DATA	IMET = 9
DECAY COEFFICIENT FOR PHYSICAL OR CHEMICAL DEPLETION	DECAY = 0.
SURFACE STATION NO.	ISS = 13889
YEAR OF SURFACE DATA	ISY = 73
UPPER AIR STATION NO.	IUS = 13861
YEAR OF UPPER AIR DATA	IUY = 73
ALLOCATED DATA STORAGE	LIMIT = 43500 WORDS
REQUIRED DATA STORAGE FOR THIS PROBLEM RUN	MIMIT = 3431 WORDS

PSP TSP
18 weeks
now out → 43
14/10

*** ISC RUN FOR JAX ELEC. AUTH. PARTICULATES (GLC, SEPT 25, 1981) ***

*** X,Y COORDINATES OF DISCRETE RECEPTORS ***
(METERS)

(47200.0, 68400.0),	(48000.0, 68300.0),	(48500.0, 67800.0),	(49000.0, 67100.0),	(49200.0, 66400.0),
(49000.0, 65600.0),	(48600.0, 65000.0),	(48000.0, 64600.0),	(47300.0, 64300.0),	(46500.0, 64500.0),
(45600.0, 64800.0),	(46300.0, 65900.0),	(46100.0, 66400.0),	(46300.0, 66700.0),	(46400.0, 67100.0),
(46800.0, 67300.0),	(51000.0, 61000.0),	(37900.0, 62300.0),	(39000.0, 61600.0),	(39500.0, 59300.0),
(40600.0, 58500.0),	(39800.0, 55000.0),	(

*** SOURCE DATA ***

FORM 511

SOURCE NUMBER	T W	Y A NUMBER	PART. CATS.	EMISSION RATE		X (METERS)	Y (METERS)	BASE ELEV. (METERS)	HEIGHT (METERS)	TEMP.	EXIT VEL.	BLDG. HEIGHT (METERS)	BLDG. LENGTH (METERS)	BLDG. WIDTH (METERS)	
				TYPE=0,1 (GRAMS/SEC)	TYPE=2 (GRAMS/SEC)					(DEG.K); VERT.DIM TYPE=1 (METERS)	(M/SEC); HORZ.DIM TYPE=1,2 (METERS)				DIAMETER TYPE=0 (METERS)
1	0 0	0		.46400E+02		47140.0	66270.0	0.0	194.20	327.60	18.29	10.13	0.00	0.00	0.00
2	0 0	R		.21000E+00		47140.0	66270.0	0.0	10.00	325.00	0.00	0.00	0.00	0.00	0.00
3	0 0	R		.40000E-02		47380.0	65930.0	0.0	10.00	325.00	0.00	0.00	0.00	0.00	0.00
4	0 0	R		.48000E+00		47140.0	65870.0	0.0	10.00	325.00	0.00	0.00	0.00	0.00	0.00
5	0 0	E		.40000E-02		47630.0	65970.0	0.0	10.00	325.00	0.00	0.00	0.00	0.00	0.00
6	0 0	R		.63000E+00		47630.0	65900.0	0.0	10.00	325.00	0.00	0.00	0.00	0.00	0.00
7	0 0	R		.10700E+01		49100.0	61900.0	0.0	10.00	325.00	0.00	0.00	0.00	0.00	0.00
8	2 0	R		.17000E-05		49400.0	62300.0	0.0	0.00	0.00	348.00	0.00	0.00	0.00	0.00
9	0 0	R		.63300E+01		46900.0	67140.0	0.0	130.00	310.00	1.00	66.00	0.00	0.00	0.00
10	0 0	R		.63300E+01		47140.0	67130.0	0.0	130.00	310.00	1.00	66.00	0.00	0.00	0.00
11	2 0	E		.10000E-06		47080.0	65370.0	0.0	0.00	0.00	246.00	0.00	0.00	0.00	0.00
12	2 0	P		.10000E-06		47350.0	65390.0	0.0	0.00	0.00	246.00	0.00	0.00	0.00	0.00
13	2 0	R		.15000E-05		47230.0	65400.0	0.0	0.00	0.00	179.00	0.00	0.00	0.00	0.00
14	2 0	R		.17000E-05		48000.0	67000.0	0.0	10.00	0.00	200.00	0.00	0.00	0.00	0.00

*** ISC RUN FOR JAX ELEC. AUTH. PARTICULATES (GLC, SEPT 25, 1981) ***

*** SOURCE PARTICULATE DATA ***

*** SOURCE NUMBER = 2 ***

MASS FRACTION =
0.00330, 0.01040, 0.02480, 0.06590, 0.12340, 0.17850, 0.21240, 0.38130,

SETTLING VELOCITY (METERS/SEC) =
0.0006, 0.0011, 0.0023, 0.0045, 0.0091, 0.0181, 0.0362, 0.0724,

SURFACE REFLECTION COEFFICIENT =
0.98000, 0.96000, 0.92000, 0.85000, 0.79000, 0.72000, 0.65000, 0.55000,

*** SOURCE NUMBER = 3 ***

MASS FRACTION =
0.00330, 0.01040, 0.02480, 0.06590, 0.12340, 0.17850, 0.21240, 0.38130,

SETTLING VELOCITY (METERS/SEC) =
0.0006, 0.0011, 0.0023, 0.0045, 0.0091, 0.0181, 0.0362, 0.0724,

SURFACE REFLECTION COEFFICIENT =
0.98000, 0.96000, 0.92000, 0.85000, 0.79000, 0.72000, 0.65000, 0.55000,

*** SOURCE NUMBER = 4 ***

MASS FRACTION =
0.00330, 0.01040, 0.02480, 0.06590, 0.12340, 0.17850, 0.21240, 0.38130,

SETTLING VELOCITY (METERS/SEC) =
0.0006, 0.0011, 0.0023, 0.0045, 0.0091, 0.0181, 0.0362, 0.0724,

SURFACE REFLECTION COEFFICIENT =
0.98000, 0.96000, 0.92000, 0.85000, 0.79000, 0.72000, 0.65000, 0.55000,

*** ISC RUN FOR JAX ELEC. AUTH. PARTICULATES (GLC, SEPT 25, 1981) ***

*** SOURCE PARTICULATE DATA ***

*** SOURCE NUMBER = 5 ***

MASS FRACTION =
0.00330, 0.01040, 0.02480, 0.06590, 0.12340, 0.17850, 0.21240, 0.38130,

SETTLING VELOCITY (METERS/SEC) =
0.0006, 0.0011, 0.0023, 0.0045, 0.0091, 0.0181, 0.0362, 0.0724,

SURFACE REFLECTION COEFFICIENT =
0.98000, 0.96000, 0.92000, 0.85000, 0.79000, 0.72000, 0.65000, 0.55000,

*** SOURCE NUMBER = 6 ***

MASS FRACTION =
0.00330, 0.01040, 0.02480, 0.06590, 0.12340, 0.17850, 0.21240, 0.38130,

SETTLING VELOCITY (METERS/SEC) =
0.0006, 0.0011, 0.0023, 0.0045, 0.0091, 0.0181, 0.0362, 0.0724,

SURFACE REFLECTION COEFFICIENT =
0.98000, 0.96000, 0.92000, 0.85000, 0.79000, 0.72000, 0.65000, 0.55000,

*** SOURCE NUMBER = 7 ***

MASS FRACTION =
0.00330, 0.01040, 0.02480, 0.06590, 0.12340, 0.17850, 0.21240, 0.38130,

SETTLING VELOCITY (METERS/SEC) =
0.0006, 0.0011, 0.0023, 0.0045, 0.0091, 0.0181, 0.0362, 0.0724,

SURFACE REFLECTION COEFFICIENT =
0.98000, 0.96000, 0.92000, 0.85000, 0.79000, 0.72000, 0.65000, 0.55000,

*** ISC RUN FOR JAX FLEC. AUTH. PARTICULATES (GLC, SEPT 25, 1981) ***

*** SOURCE PARTICULATE DATA ***

*** SOURCE NUMBER = 8 ***

MASS FRACTION =

0.00330, 0.01040, 0.02480, 0.06590, 0.12340, 0.17850, 0.21240, 0.38130,

SETTLING VELOCITY (METERS/SEC) =

0.0006, 0.0011, 0.0023, 0.0045, 0.0091, 0.0181, 0.0362, 0.0724,

SURFACE REFLECTION COEFFICIENT =

0.98000, 0.95000, 0.92000, 0.85000, 0.79000, 0.72000, 0.65000, 0.55000,

*** SOURCE NUMBER = 9 ***

MASS FRACTION =

0.00330, 0.01040, 0.02480, 0.06590, 0.12340, 0.17850, 0.21240, 0.38130,

SETTLING VELOCITY (METERS/SEC) =

0.0006, 0.0011, 0.0023, 0.0045, 0.0091, 0.0181, 0.0362, 0.0724,

SURFACE REFLECTION COEFFICIENT =

0.98000, 0.95000, 0.92000, 0.85000, 0.79000, 0.72000, 0.65000, 0.55000,

*** SOURCE NUMBER = 10 ***

MASS FRACTION =

0.00330, 0.01040, 0.02480, 0.06590, 0.12340, 0.17850, 0.21240, 0.38130,

SETTLING VELOCITY (METERS/SEC) =

0.0006, 0.0011, 0.0023, 0.0045, 0.0091, 0.0181, 0.0362, 0.0724,

SURFACE REFLECTION COEFFICIENT =

0.98000, 0.95000, 0.92000, 0.85000, 0.79000, 0.72000, 0.65000, 0.55000,

*** ISC RUN FOR JAX ELEC. AUTH. PARTICULATES (GLC, SEPT 25, 1981) ***

*** SOURCE PARTICULATE DATA ***

*** SOURCE NUMBER = 11 ***

MASS FRACTION =
0.00330, 0.01040, 0.02480, 0.06590, 0.12340, 0.17850, 0.21240, 0.38130,

SETTLING VELOCITY (METERS/SEC) =
0.0006, 0.0011, 0.0023, 0.0045, 0.0091, 0.0181, 0.0362, 0.0724,

SURFACE REFLECTION COEFFICIENT =
0.98000, 0.96000, 0.92000, 0.85000, 0.79000, 0.72000, 0.65000, 0.55000,

*** SOURCE NUMBER = 12 ***

MASS FRACTION =
0.00330, 0.01040, 0.02480, 0.06590, 0.12340, 0.17850, 0.21240, 0.38130,

SETTLING VELOCITY (METERS/SEC) =
0.0006, 0.0011, 0.0023, 0.0045, 0.0091, 0.0181, 0.0362, 0.0724,

SURFACE REFLECTION COEFFICIENT =
0.98000, 0.95000, 0.92000, 0.85000, 0.79000, 0.72000, 0.65000, 0.55000,

*** SOURCE NUMBER = 13 ***

MASS FRACTION =
0.00330, 0.01040, 0.02480, 0.06590, 0.12340, 0.17850, 0.21240, 0.38130,

SETTLING VELOCITY (METERS/SEC) =
0.0006, 0.0011, 0.0023, 0.0045, 0.0091, 0.0181, 0.0362, 0.0724,

SURFACE REFLECTION COEFFICIENT =
0.98000, 0.96000, 0.92000, 0.85000, 0.79000, 0.72000, 0.65000, 0.55000,

*** ISC RUN FOR JAX ELEC. AUTH. PARTICULATES (GLC, SEPT 25, 1981) ***

*** SOURCE PARTICULATE DATA ***

*** SOURCE NUMBR = 14 ***

MASS FRACTION =

0.00330, 0.01040, 0.02480, 0.06590, 0.12340, 0.17950, 0.21240, 0.38130,

SETTLING VELOCITY (METERS/SEC) =

0.0006, 0.0011, 0.0023, 0.0045, 0.0091, 0.0181, 0.0362, 0.0724,

SURFACE REFLECTION COEFFICIENT =

0.98000, 0.96000, 0.92000, 0.85000, 0.79000, 0.72000, 0.65000, 0.55000,

DEPARTMENT OF ENVIRONMENTAL PERMITTING

JUN 21 1982

RECEIVED

*** ISC RUN FOR JAX ELEC. AUTH. PARTICULATES (GLC, SEPT 25, 1981) ***

* 18-DAY AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *

• FROM ALL SOURCES •

* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	- X -	- Y -	CON.	- X -	- Y -	CON.
47200.0	68400.0	0.72262	48000.0	68300.0	0.75808	48500.0	67800.0	0.39901
49000.0	67100.0	0.90147	49200.0	66400.0	0.47970	49000.0	65600.0	0.59714
48600.0	65000.0	0.65926	48000.0	64600.0	0.87226	47300.0	64300.0	0.89888
46500.0	64500.0	1.07234	45600.0	64800.0	1.68711	46300.0	65900.0	2.03987
46100.0	66400.0	2.89385	46300.0	66700.0	2.44220	46400.0	67100.0	0.78968
46800.0	67300.0	0.75551	51000.0	61000.0	0.47116	37900.0	62300.0	0.45811
39000.0	61600.0	0.49725	39500.0	59300.0	0.22694	40600.0	58500.0	0.22293
39800.0	55000.0	0.13952						

*** ISC RUN FOR JAX ELEC. AUTH. PARTICULATES (GLC, SEPT 25, 1981) ***

* HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY, PER.)	- X -	- Y -	CON.	(DAY, PER.)
47200.0	68400.0	3.05084	(216, 1)	48000.0	68300.0	4.00553	(115, 1)
48500.0	67800.0	2.78763	(115, 1)	49000.0	67100.0	7.05195	(239, 1)
49200.0	66400.0	3.12212	(133, 1)	49000.0	65600.0	3.64947	(216, 1)
48600.0	65000.0	3.05299	(170, 1)	48000.0	64600.0	4.73998	(287, 1)
47300.0	64300.0	3.43581	(170, 1)	46500.0	64500.0	6.65648	(259, 1)
45600.0	64800.0	6.86032	(120, 1)	46300.0	65900.0	4.84719	(239, 1)
46100.0	66400.0	14.22257	(236, 1)	46300.0	66700.0	13.84013	(236, 1)
46400.0	67100.0	3.12955	(324, 1)	46800.0	67300.0	4.26695	(224, 1)
51000.0	61000.0	2.87974	(170, 1)	57900.0	62300.0	1.97250	(120, 1)
39000.0	61600.0	4.34710	(120, 1)	39500.0	59300.0	1.07832	(246, 1)
40600.0	58500.0	1.26228	(1, 1)	39800.0	55000.0	1.00417	(287, 1)

MAXIMUM NONATTAINMENT AREA IMPACT

*** ISC RUN FOR JAX ELEC. AUTH. PARTICULATES (GLC, SEPT 25, 1981) ***

* SECOND HIGHEST 24-HOUR AVERAGE CONCENTRATION (MICROGRAMS/CUBIC METER) *
* FROM ALL SOURCES *
* FOR THE DISCRETE RECEPTOR POINTS *

- X -	- Y -	CON.	(DAY, PER.)	- X -	- Y -	CON.	(DAY, PER.)
47200.0	68400.0	2.70067	(115, 1)	48000.0	68300.0	2.95198	(161, 1)
48500.0	67800.0	1.59984	(161, 1)	49000.0	67100.0	2.29166	(161, 1)
49200.0	66400.0	1.43156	(216, 1)	49000.0	65600.0	1.93643	(115, 1)
48600.0	65000.0	1.48832	(133, 1)	48000.0	64600.0	2.84347	(184, 1)
47300.0	64300.0	2.81172	(1, 1)	46500.0	64500.0	5.83002	(1, 1)
45600.0	64800.0	6.83174	(246, 1)	46300.0	65900.0	4.55330	(246, 1)
46100.0	66400.0	9.52086	(63, 1)	46300.0	66700.0	7.27261	(324, 1)
45400.0	67100.0	2.92305	(224, 1)	46800.0	67300.0	2.63270	(161, 1)
51000.0	61000.0	2.27637	(287, 1)	37900.0	62300.0	1.79747	(239, 1)
39000.0	61600.0	1.41777	(246, 1)	39500.0	59300.0	0.87491	(1, 1)
49600.0	58500.0	0.78503	(287, 1)	39800.0	55000.0	0.48020	(170, 1)

CRSTER ANALYSIS
OF MAXIMUM ANNUAL TSP
IMPACT ON NONATTAINMENT AREA

STACK # 1--JEA EASTPORT UNITS 1 AND 2

SOURCE LOCATION FROM CENTER OF RECEPTOR GRID (DIR,DIST(KM)) 0.00 0.00

STACK # 2--COOLING TOWERS

SOURCE LOCATION FROM CENTER OF RECEPTOR GRID (DIR,DIST(KM)) 350.00 0.84

STACK # 3--COAL HANDLING

SOURCE LOCATION FROM CENTER OF RECEPTOR GRID (DIR,DIST(KM)) 150.00 0.12

STACK # 4--SHIP UNLOADING

SOURCE LOCATION FROM CENTER OF RECEPTOR GRID (DIR,DIST(KM)) 154.00 4.92

STACK	MONTH	EMISSION RATE (GMS/SEC)	HEIGHT (METERS)	DIAMETER (METERS)	EXIT VELOCITY (M/SEC)	TEMP (DEG.K)	VOLUMETRIC FLOW (M**3/SEC)
1	ALL	46.4000	194.16	10.13	18.29	327.60	1474.08
2	ALL	12.6600	130.00	66.00	1.00	300.00	3421.19
3	ALL	1.4500	20.00	1.00	0.00	300.00	0.00
4	ALL	1.3200	20.00	1.00	0.00	300.00	0.00

PLANT NAME: JACKSONVILLE ELECTRIC AU POLLUTANT: THORITY EMISSION UNITS: GM/SEC AIR QUALITY UNITS: GM/M**3

MAXIMUM MEAN CONC= 3.4499E-06 DIRECTION= 16 DISTANCE= 5.0 KM

ANNUAL MEAN CONCENTRATION AT EACH RECEPTOR

DIR	RANGE	2.0 KM	3.0 KM	4.0 KM	5.0 KM	9.4 KM
15		8.06348E-07	7.93508E-07	1.29475E-06	1.99765E-06	2.82520E-07
16		9.81685E-07	1.06227E-06	1.82127E-06	3.44986E-06	2.79578E-07
17		1.14592E-06	1.06719E-06	8.24039E-07	1.46155E-06	2.56927E-07
20		9.01172E-07	8.08744E-07	4.25114E-07	3.94385E-07	2.18795E-07
21		7.21049E-07	5.73824E-07	2.67818E-07	2.00968E-07	3.02257E-07
22		1.03688E-06	8.12116E-07	4.84560E-07	3.72883E-07	2.47169E-07
23		1.02465E-06	6.83630E-07	3.99290E-07	2.93910E-07	1.79647E-07
24		1.53115E-06	1.09321E-06	7.89594E-07	6.05765E-07	3.05318E-07
25		8.86917E-07	6.49159E-07	5.48026E-07	3.68069E-07	1.89528E-07

~ MAXIMUM ANNUAL AVERAGE
NONATTAINMENT AREA
IMPACT

ATTACHMENT 3

OTHER CRITERIA POLLUTANTS

As indicated in the PSD Permit, the criteria pollutants relevant to this analysis other than SO₂ and TSP are NO₂ and CO. Since detailed emission inventory data are not available for these pollutants in the Jacksonville area, it is not possible to explicitly model the effects of lower stack heights at Southside and Kennedy in combination with the impacts of other sources in the same manner as was done for SO₂. However, if the assumption is made that NO_x and CO emissions from major point sources are proportional to SO₂ emissions in the same ratio as for the main units of SJRPP, then estimates can be made of maximum impacts by simply scaling the results of the SO₂ modelling. This same approach was used for NO₂ in the PSD application and for CO in supplemental information regarding the application submitted with a July 8, 1980 letter from D. A. Moehle to K. Williams.

NO_x emissions from the main units of SJRPP are expected to be .6 lb/mm Btu versus SO₂ emissions of .76 lb/mm Btu. CO emissions are expected to be on the order of .05 lb/mm Btu. Thus, SO₂ modelling results must be scaled by a factor of .79 (.6/.76) to yield NO₂ estimates and by a factor of .07 (.05/.76) to yield CO estimates. Monitored background values are added to these estimated impacts to produce totals which can be compared with ambient standards.

The maximum annual average SO₂ impact in the Southside and Kennedy areas was predicted to be 25 ug/m³ (see Table 3 of Attachment 1). Maximum annual NO₂ impacts are about 20 ug/m³ using this scaling approach. Including the monitored background concentration of 10 ug/m³ (see Table 3 of the PSD Permit) produces a total NO₂ concentration of 30 ug/m³, which is well below the annual NAAQS of 100 ug/m³.

Based on the highest predicted 3-hour average SO₂ impact in the Southside and Kennedy vicinities of 828 ug/m³, and the scaling factors above, one can infer a maximum 3-hour average CO impact from major point sources of 58 ug/m³. By using the averaging time scaling factors in the Workbook for Atmospheric Dispersion Estimates, 1-hour and 8-hour averages are roughly estimated to be 69 ug/m³ and 48 ug/m³, respectively. When added to the monitored background values of 5200 ug/m³ (1-hour) and 4500 ug/m³ (8-hour), the resulting totals are very small in comparison with the NAAQS of 40,000 ug/m³ and 10,000 ug/m³ for the 1-hour and 8-hour averaging times respectively.



UNITED STATES ENVIRONMENTAL PROTECTION AGENCY

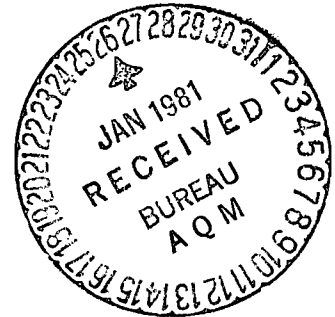
REGION IV

345 COURTLAND STREET
ATLANTA, GEORGIA 30365

JAN 14 1981

REF: 4AH-AF

Mr. Steve Smallwood, Chief
Bureau of Air Quality Management
Division of Environmental Programs
Twin Towers Office Building
2600 Blair Stone Road
Tallahassee, Florida 32301



RE: Jacksonville Electric Authority
New Power Generating Station
PSD-FL-010

Dear Mr. Smallwood:

Enclosed for your review and comment are the Public Notice and Preliminary PSD Determination for the reference source located near Jacksonville, Florida. The public notice will appear in a local newspaper, Florida Times Journal, in the near future.

Please let my office know if you have comments or questions regarding this determination. You may contact Mr. Kent Williams, Chief, New Source Review, 404/881-4552 or Mr. Jeffrey Shumaker of TRW Inc. at 919/541-9100. TRW Inc. is under contract to EPA, and TRW personnel are acting as authorized representatives of the Agency in providing aid to the Region IV PSD review program.

Sincerely yours,

Tommie A. Gibbs

Tommie A. Gibbs, Chief
Air Facilities Branch

TAB:JLS:cg

Enclosure



UNITED STATES ENVIRONMENTAL PROTECTION AGENCY

REGION IV

Best Available Copy

345 COURTLAND STREET
ATLANTA, GEORGIA 30365

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JAN 20 1981

JAN 14 1981

REF: 4AH-AF

Mr. Dale A. Moehle
Division Chief
Jacksonville Electric Authority
Post Office Box 53015
Jacksonville, Florida 32201

DIVISION CHIEF
NEW FOSSIL GENERATION
EXPANSION PROJECTS

DIVISION CHIEF
NEW FOSSIL GENERATION
EXPANSION PROJECTS

RE: New Power Generating Station
PSD-FL-010

Dear Mr. Moehle:

EPA Region IV has reviewed your application to construct the reference source under the provisions of Prevention of Significant Deterioration Regulations (40 CFR 52.21) and has made a preliminary determination of approval with conditions. Please find enclosed two copies of the Preliminary Determination.

A public notice will be run in the near future in a local newspaper, Florida Times Journal. A copy of the summary and your application will be open to public review and comment for a period of 30 days. The public can also request a public hearing to review and discuss specific issues. At the end of this period, EPA will evaluate the comments received and make a final determination regarding the proposed construction.

Should you have questions regarding this information, please contact Mr. Kent Williams, Chief, New Source Review, at 404/881-4552 or Mr. Jeffrey Shumaker of TRW Inc. at 919/541-9100. TRW is under contract to EPA, and its personnel are acting as authorized representatives of the Agency in providing aid to the Region IV PSD program.

Sincerely yours,

Tommie A. Gibbs

Tommie A. Gibbs, Chief
Air Facilities Branch

TAG:JLS:cg

Enclosure

cc. D FULW
J JACKSON
C ALVIN

FILE 9.7.4

R HARMAN
W O RYAN
R. HARRISON
D FINE

1/31/81
D. Fine

ENVIROPSHERE COMPANY
ATLANTA OFFICE
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RECEIVED
JEA PROJECT

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PUBLIC NOTICE

A new air pollution source is proposed for construction by the Jacksonville Electric Authority near the town of Jacksonville in Duval County, Florida. The source is a new power generating complex that will increase emissions of air pollutants by the following amounts in tons per year:

<u>Sulfur Dioxide</u>	<u>Particulate Matter</u>	<u>Nitrogen Oxides</u>	<u>Carbon Monoxide</u>	<u>Volatile Organic Compounds</u>
9015	377	7117	593	29

The maximum increment consumed by the proposed new source is as follows:

	<u>Annual</u>	<u>24-Hour</u>	<u>3-Hour</u>
Sulfur Dioxide			
Class I	50%	80%	72%
Class II	10%	46%	65%
Particulate Matter			
Class I	10%	20%	--
Class II	12%	46%	--

Note that no allowable 3-hour increments have been established for particulate matter.

The proposed construction has been reviewed by the U.S. Environmental Protection Agency (EPA) under Federal Prevention of Significant Deterioration (PSD) Regulations (40 CFR 52.21), and EPA has made a preliminary determination that the construction can be approved provided certain conditions are met. A summary of the basis for this determination and the application for a permit submitted by the Jacksonville Electric Authority are available for public review in the Information Services Division, City Hall, 200 E. Bay Street, Jacksonville, Florida.

Any person may submit written comments to EPA regarding the proposed modification. All comments, postmarked not later than 30 days from the date of this notice, will be considered by EPA in making a final determination regarding approval for construction of this source. These comments will be made available for public review at the above location. Furthermore, a public hearing can be requested by any person. Such requests should be submitted within 15 days of the date of this notice. Letters should be addressed to:

Mr. Tommie A. Gibbs, Chief
Air Facilities Branch
U.S. Environmental Protection Agency
345 Courtland Street, NE
Atlanta, Georgia 30365

Preliminary Determination
Jacksonville Electric Authority
PSD-FL-010

I. Applicant

Jacksonville Electric Authority
P. O. Box 53015
233 W. Duval Street
Jacksonville, Florida 32201

II. Location

The Jacksonville Electric Authority (JEA), in cooperation with the Florida Power and Light Company (FPL), proposes to construct a new power generating facility consisting of two 600 megawatt (MW) coal-fired steam generating units in Duval County, Florida. The construction site, known as the Eastport site, is located adjacent to the existing JEA Northside Generating Station, approximately 15 kilometers northeast of downtown Jacksonville, Florida. The UTM coordinates of the proposed source are 446.9 kilometers north and 366.3 kilometers east.

III. Project Description

The applicant proposes to construct a new power generating station consisting of two 600 MW turbine-generator units powered by two pulverized coal-fired steam generators (boilers), an auxiliary boiler, and coal, limestone, and fly ash handling facilities. The two proposed steam generators will fire a maximum of 5928 million Btus per hour (MM Btu/hr) each or approximately 282.3 tons per hour each of a medium bituminous coal having a maximum higher heating value of 10,500 Btu/lb. Of the coals under consideration, the maximum sulfur content coal has 4.0 percent sulfur by weight.

A 200 MMBtu/hr auxiliary boiler will be utilized to provide start-up and shut-down capability for the two turbine-generating units. The auxiliary boiler will be fired with No. 2 fuel oil having a maximum sulfur content of .76 percent by weight (wt. %) and a maximum higher heating value of 19,000 Btu/lb.

The cooling system will consist of two counterflow natural draft cooling towers located at the north end of the plant.

The coal handling facility provides for water delivery of coal by ocean-going barge or ship to a marine terminal located on Blount Island, Florida where a 30-acre coal surge pile will be operated. The coal will be transferred from the marine terminal to the proposed plant site by a shuttle train. The coal handling equipment at the proposed plant site includes a rotary car dumper, yard area coal storage, transfer system, coal silos, and tripper floor distribution system. Approximately 10,000 tons per day of coal will be unloaded at the proposed source.

Limestone will be delivered to the proposed source by truck and stored in long-term silos or day storage silos.

IV. Source Impact Analysis

PSD regulations amended in the August 7, 1980 Federal Register require that a new fossil fuel fired steam electric plant with potential emissions of 100 or more tons per year of any pollutant regulated under the Act undergo a PSD review for each pollutant regulated under the Act which results in a significant net increase in emissions. Table 1 presents an emissions summary for the proposed new source. The proposed new source has potential emission increases of sulfur dioxide (SO₂) and other pollutants of greater than 100 tons per year and significant increases in particulate matter (PM), nitrogen oxides (NO_x), carbon monoxide (CO) and SO₂. Therefore, a PSD review is required for SO₂, NO_x, PM, and CO. A full PSD review consists of the following:

- A. A demonstration that Best Available Control Technology (BACT) is being applied to all facilities emitting SO₂, PM, NO_x, and CO;
- B. An analysis of existing air quality;
- C. A demonstration that the source will not cause or contribute to any NAAQS violations;

- D. A PSD increment analysis;
- E. A growth analysis;
- F. An analysis of impacts on soils, vegetation, and visibility;
and
- G. A Class I area analysis.

The proposed new source will be located in an area considered attainment for all pollutants under review. Non-attainment areas for PM and ozone are located in the vicinity of Jacksonville, Florida, approximately 10 to 15 kilometers from the proposed new source.

The JEA's application was considered complete prior to August 7, 1980.

A. Best Available Control Technology (BACT)

Paragraph (i)(9) of the August 7, 1980 PSD regulations exempts this source from paragraph (j) of the regulations. Instead, paragraph (j) of the June 19, 1978 PSD regulations applies. Therefore, BACT must be applied to all emission units emitting SO₂, PM, NO_x, and CO because allowable emissions of these pollutants are greater than 50 tons per year.

Sulfur Dioxide

BACT must be applied to the two proposed steam generators (boilers) and the auxiliary boiler to control SO₂ emissions.

The applicant proposes to install a lime/limestone flue gas desulfurization (FGD) system on each of the proposed steam generators as BACT for SO₂. The SO₂ removal efficiency of a single FGD system is 90 percent (.76 lb/MM Btu SO₂ emissions).

Two other emissions control systems, a lime/limestone FGD with a 95 percent SO₂ removal efficiency and a lime spray drying FGD with a 90 percent SO₂ removal efficiency, were examined. The incremental cost of the higher efficiency lime/limestone FGD system was determined not to be cost effective with respect to the resulting improvement in air quality.

The lime spray drying FGD system was determined to be neither reliable nor cost effective. These alternate control systems were rejected based upon the above economic and potential environmental impact considerations. The New Source Performance Standard (NSPS) for electric utility steam generation was promulgated June 11, 1979. The NSPS limits SO₂ emissions to 10 percent of potential SO₂ emissions and a maximum emission rate of 1.2 lb/MMBtu heat input except when the emissions are less than 0.6 lb/MMBtu. At the later emission rate, a minimum of 70 percent reduction (30 percent of potential emitted) in potential SO₂ emissions is required. The percentage reduction in potential SO₂ emissions is dependent upon the sulfur content of the coal. The proposed SO₂ control system meets all requirements of the NSPS for electric utility steam generation stations for the control of SO₂ emissions. A continuous monitor for sulfur dioxide emissions will be installed in the flue of both steam generators in accordance with 40 CFR 60.47a. The above emissions control system represents BACT for SO₂ emissions from the two proposed steam generators.

The auxiliary boiler will be fired with .76 wt.% sulfur fuel oil. The SO₂ emissions from the auxiliary boiler are small when compared to those from the main units. Also, the auxiliary boiler will be operated on an intermittent basis (annual capacity factor of 5 percent) and will not operate simultaneously with the main power generating boilers. Therefore, the air quality impacts due to operation of the auxiliary boiler will be much less than those resulting from the operation of the main boilers. Based on the above analysis, BACT for SO₂ emissions from auxiliary boiler has been determined to be the firing of .76 wt.% sulfur fuel oil.

Particulate Matter

Application of BACT is required for the emissions of PM from the two steam generators (boilers), auxiliary boiler and coal, flyash, and limestone handling facilities.

BACT for PM emissions from the two steam generators has been determined to be the installation of an electrostatic precipitator with a PM removal efficiency of 99.78 percent (.03 lb/MM Btu). Two alternative systems, a electrostatic precipitator with a PM removal efficiency of 99.85 percent (.02 lb/MM Btu) and a fabric filter with a PM removal efficiency of 99.78 percent (.03 lb/MM Btu), were examined in the BACT analysis. The higher efficiency electrostatic precipitator was determined not to be cost effective with respect to the resulting improvement in ambient air quality. The fabric filter system was considered neither reliable nor cost effective. These alternative control systems were rejected on the basis of the above economic and environmental impact considerations. The NSPS for electric utility steam generation limits PM emissions to .03 lb/MM Btu heat input. The proposed PM emissions control system meets the NSPS requirements for control of PM emissions. A continuous monitor for opacity emissions will be installed in the flue of both steam generators in accordance with 40 CFR 60.47a. The above system has been determined to be BACT for PM emissions from the two steam generators.

Control and collection of particulate matter emissions from the coal handling system will be accomplished by several different methods including totally enclosed conveying systems, water spray dust collection systems, and dust collection systems utilizing fabric filters.

Control of fugitive dust from limestone handling will be accomplished by the use of totally enclosed conveyors and fabric filter dust collectors.

Fugitive fly ash emissions will be controlled at all transfer and discharge locations by fabric filters. Pneumatic conveyors are

utilized to transfer fly ash to and from ash storage silos, and to mixers which prepare the fly ash and FGD wastes for disposal.

Fugitive dissolved and suspended particulate emissions from the cooling tower will be controlled by high efficiency drift eliminators. Additionally, a circumferential drift eliminator wall will be provided at the base of the hyperbolic shell to mitigate the potential effects of blow-through. Table 2 presents a fugitive emissions and controls summary.

The above emission control systems represent BACT for fugitive emissions.

BACT for PM emissions from the auxiliary boiler has been determined to be the firing of No. 2 fuel oil with an ash content of 0.1 wt.%. The auxiliary boiler will not operate simultaneously with the main steam generating unit and the air quality impact from the auxiliary boiler is small when compared to the emissions from the main units. Therefore, no air pollution control equipment for the purpose of PM reduction is warranted.

Nitrogen Oxides and Carbon Monoxide

BACT must be applied to the two steam generators and the auxiliary boiler to control NO_x and CO emissions. Emissions of NO_x and CO resulting from the combustion of coal is dependent on such factors of boiler design as the amount of excess air in the combustion chamber, flame temperature, burner spacing and burner design.

The applicant proposes to use combustion controls and modern boiler design to guarantee a maximum NO_x emission rate of 0.6 lb/MM Btu and CO emission rate of 0.05 lb/MM Btu in the two steam generators (boilers). This is in agreement with the NO_x emission limit required in the NSPS for steam electric generating stations. Control of NO_x and CO emissions will be accomplished by a flue gas oxygen monitoring system to control the air/fuel ratio in accordance with the attached "Use of Flue Gas Oxygen Meter as BACT for Combustion Controls." In addition, a continuous nitrogen oxides meter will be installed in the flue at both steam generators in accordance with 40 CFR 60.47a.

BACT for NO_x and CO emissions from the auxiliary boiler will be accomplished by a flue gas oxygen monitoring system in accordance with the attached "Use of Flue Gas Oxygen Meter as BACT for Combustion Controls."

The above emissions control system represents BACT for NO_x and CO emissions from the two steam generators and the auxiliary boiler.

B. Analysis of Existing Air Quality

Paragraph (i)(9) of the August 7, 1980 PSD regulations exempts this source from paragraph (m)(1) of the regulations. Instead, paragraph (n) of the June 19, 1978 PSD regulations apply. Therefore, an analysis of existing air quality for SO_2 , PM, NO_x , and CO is required as deemed necessary by the Administrator because the allowable emissions increases of these pollutants are greater than 50 tons per year.

Monitoring data for SO_2 , NO_x , and PM were obtained from the New Berlin monitoring site near Jacksonville, Florida for the year 1977. Monitoring data for CO was not available; however, the area surrounding the proposed new source has been classified attainment or unclassified for CO and therefore no NAAQS violations for CO are expected.

An air quality analysis using meteorological data from the Jacksonville International Airport was used to determine the maximum pollutant concentrations at the monitoring site when the contributions from large existing sources of pollution were negligible. These sources were the JEA Northside plant and the St. Regis Paper Company. These maximum background pollutant concentrations were determined to be representative of the existing air quality in the region of the proposed source. All monitoring, data collection procedures, and modeling analyses were conducted using EPA-approved techniques. The monitoring data was utilized in the NAAQS analysis in projecting the maximum ambient air concentrations of each pollutant under review. The results are shown in Table 3.

C. NAAQS ANALYSIS

The EPA-approved dispersion models CRSTER (modified for use with multiple point sources of emissions) PTMPT and PAL were utilized to assess the total ambient air concentrations of SO₂, PM, NO_x and CO within 50 km of the proposed plant site. Meteorological data for the years 1970-1974 were obtained from weather stations located at Jacksonville International Airport (surface data) and Waycross, Georgia (upper air observations). The meteorological data was determined to be representative of the weather conditions at the proposed construction site.

An emissions inventory of all increment consuming and other sources within 50 km of the proposed plant, and new sources within 100 km of the nearest Class I area was compiled. For the purpose of the modeling analysis, the main steam generating units were considered to operate continuously. This is a conservative assumption because the plant capability factor is expected to be no greater than 74 percent.

An initial modeling analysis determined that the 1973 meteorological data represented the "worst-case" year assuming a 100 percent plant load. Additional modeling at 75 percent and 50 percent load showed that a 100 percent continuous operating load resulted in the highest ground level concentrations. Therefore, the more detailed analyses were conducted using the emission parameters for the 100 percent load level. All modeling was conducted using EPA-approved modeling techniques. All stacks were modeled at Good Engineering Practice (GEP) stack height. No effects on the projected ambient air concentrations of pollutants were expected to occur as a result of turbulent building wake effects (downwash) because all stacks met GEP stack height.

The maximum ambient air concentrations for the pollutants under review were determined by modeling emissions from the proposed new source along with emissions from the JEA Northside plant and St. Regis Paper Company. The maximum concentrations obtained from the modeling analysis were added to the maximum monitored concentrations (which did not include contributions from the St. Regis Paper Company or the JEA Northside Plant) to obtain the

maximum ambient air concentrations of each pollutant under review. This analysis is considered conservative because both the maximum monitored and modeled concentrations were not located at the same geographical point. The results of the NAAQS analysis are presented in Table 3.

A modeling analysis was conducted to determine the impact of PM emissions (including fugitive PM emissions) from the proposed new source on the PM non-attainment area located in the downtown Jacksonville, Florida area. The maximum impacts were projected to be below 1 ug/m³ on a 24-hr average. These values are below the PSD modeling significance levels as defined in the June 19, 1978 PSD regulations, 43FR26358. Therefore, the proposed new source will not significantly impact the PM non-attainment area which is in compliance with the August 7, 1980 PSD regulations paragraph (f)(4)(a).

The VOC emissions from the proposed new source are not expected to impact the ozone non-attainment area located near Jacksonville, Florida. Presently, no EPA-approved dispersion models exist with which to model ozone emissions (of which VOC is a precursor). The VOC emission levels from the proposed new source are small and therefore are not expected to significantly impact the ozone non-attainment area under any meteorological conditions.

D. Increment Analysis

The models and meteorology for determination of PM and SO₂ increment consumption were the same as those discussed in the NAAQS analysis (above). All increment consuming sources potentially affecting the ambient air quality in the area of the proposed new source were included in the modeling analysis. No violations of the Class II increment standards were predicted. The results are presented in Table 4.

E. Growth Analysis

The proposed new source is expected to directly employ 200 people. Most of these workers will come from the local work force. No air quality impacts resulting from industrial, commercial, or residential growth associated with the proposed new source are expected.

F. Soils, Vegetation and Visibility Analysis

No soils vegetation or visibility impacts are expected to occur due to emissions from the proposed new source because of the relatively small increase in ambient pollutant concentrations.

G. Class I Area Analysis

The nearest Class I area to the proposed new source is the Okefenokee Swamp whose borders are located between 61 and 73 kilometers in a northwesterly direction. The models and meteorology used in the increment and NAAQS analyses were utilized to predict the maximum SO₂ and PM increment consumption at the borders of the Class I area. All increment consuming sources potentially impacting the Class I area were included in the modeling analysis. Five years of meteorological data were modeled. No violations of the Class I increments were predicted. The results are presented in Table 5.

No impacts on Class I area soils, vegetation or visibility are expected due to the low level of ambient air concentrations projected in the Class I area for any pollutant under review. The results of this analysis will be forwarded to the Federal Land Managers responsible for this Class I area for comment on the significance of the Class I impacts.

V. Conclusion

EPA proposes a preliminary determination of approval with conditions for construction of the steam electric generating station proposed by the Jacksonville Electric Authority. This determination is based upon the application received May 28, 1980 and additional information dated July 8, 1980 and November 26, 1980 (application determined complete as of July 9, 1980). The determination of approval is contingent upon the following specific conditions:

1. The proposed steam generating station will be constructed and operated in accordance with the capabilities and specifications of the application including the 600 megawatt generating capacity and the 5928 MMBtu/hr heat input rate for each steam generator.

2. Emissions will not exceed the allowable emissions listed in Table 6 for SO₂, PM, NO_x, and CO.
3. Compliance with the allowable emission limits for emission points 1, 2, and 3 in Table 6 will be demonstrated with performance tests conducted in accordance with the provisions of 40 CFR 60.46a, 48a and 49a, including applicable test methods, sampling procedures, sample volumes, sampling periods, etc.

Compliance with the emission limitations of all emission points in Table 6 will be in accordance with 40 CFR 60, Appendix A; Method 5, Determination of Particulate Emissions from Stationary Sources; Method 6, Determination of Sulfur Dioxide Emissions from Stationary Sources; Method 7, Determination of Nitrogen Oxide Emissions from Stationary Sources; Method 9, Determination of the Opacity of Emissions from Stationary Sources; and Method 10, Determination of Carbon Monoxide Emissions from Stationary Sources.

Emission points 4 thru 13 of Table 6 are exempted from mass emission rate compliance tests unless opacity limits are exceeded or the Administrator (or his representative) otherwise determines that such performance testing is required. All facilities will operate within 10 percent of maximum operating opacity during performance testing.

4. A flue gas oxygen meter shall be installed in emission points 1, 2, and 3 of Table 6 to continuously monitor a representative sample of the flue gas. The oxygen monitor shall be used with automatic feedback or manual controls to continuously maintain low excess air (LEA) air/fuel ratio parameters. Performance tests shall be conducted and operating procedures established in accordance with the attached "Use of Flue Gas Oxygen Meter as BACT for Combustion Controls."

The applicant will install and maintain a continuous monitoring and recording opacity meter, as well as sulfur dioxide and nitrogen oxide analyzers for each steam generator (emissions units 1 and 2 of Table 6) in accordance with the provisions of 40 CFR 60.47a.

5. Emission points 1 and 2 of Table 6 shall fire coal with an ash content not to exceed 18% and a sulfur content not to exceed 4% by weight. Coal sulfur content shall be determined and recorded in accordance with 40 CFR 60.47a.

Emission point 3 of Table 6 shall fire No. 2 fuel oil with a maximum sulfur content of .7 percent by weight and a maximum ash content of .01 percent by weight. Samples of fuel oil shall be taken and analyzed for sulfur and ash content once per day or whenever new supplies are received, whichever time period is shortest. Records of the analyses shall be recorded and kept for public inspection for a minimum of two years after the data is recorded.

6. The following requirements will be met to minimize fugitive emissions of particulate from the coal storage and handling facilities, the limestone storage and handling facilities, haul roads and general plant operations:
 - a. All conveyors and conveyor transfer points will be enclosed to preclude PM emissions.
 - b. Coal storage piles will be shaped, compacted and oriented to minimize wind erosion;
 - c. Water sprays for storage piles, handling equipment etc., will be applied during dry periods and as necessary to all facilities to maintain an opacity of "no visible emissions";
 - d. The limestone handling receiving hopper, transfer conveyors and day silos will be maintained at negative pressures with the exhaust vented to a control system; and
 - e. The fly ash handling system (including transfer and silo storage) will be maintained at negative pressures and vented to the control system.

7. Within 90 days of commencement of operations, the applicant will determine and submit to EPA the pH level in the scrubber effluent that will ensure 90% removal of the SO₂ in the flue gas. Moreover, the applicant is required to operate a continuous pH meter equipped with an upset alarm to ensure that the pH level of the scrubber effluent does not fall below this level. The minimum value pH may be revised at a later date provided notification to EPA is made demonstrating the minimum percent removal will be achieved on a continuous basis. Further, if compliance data show that higher FGD performance is necessary to maintain an overall system reduction of greater than or equal to 90%, a higher minimum pH value will be determined and maintained consistent with the required more stringent removal efficiency.
8. Emission point 3 of Table 6 shall not operate simultaneously with emission point 1 or 2 of Table 6.
9. The applicant will comply with all requirements and provisions of the New Source Performance Standard for electric utility steam generating units (40 CFR 60 Part Da). In addition, the applicant must comply with the provisions and the requirements of the attached General Conditions.
10. As a requirement of this specific condition, the applicant will comply with all emissions limits and enforceable restrictions required by the State of Florida Department of Environmental Regulation which are more restrictive, that is lower emissions limits or more strict operating requirements and equipment specifications, than the requirements of specific conditions 1- 9 of this permit.

Table 1. EMISSIONS SUMMARY OF THE PROPOSED JEA
POWER GENERATING PLANT

Pollutant	Potential emissions ^a	PSD significance levels
SO ₂	9,015	40
PM	377	25
NO _x	7,117	40
CO	593	100
VOC	29	40

^aPotential emissions calculations are based on a continuous maximum operating capacity.

Table 2. FUGITIVE EMISSIONS AND CONTROL SUMMARY

Process	Type	Amount	Factor	Control	Technique	Emissions (Grams/Sec)
Ship Unloading	Grab Bucket	10,000 Tons/Day	.4LB/Ton ^a	(99.9%) ^b	Dry Collection on Hoppers	.04
Ship Unloading Transfer Points	6 Points	10,000 Tons/Day	.2LB/Ton ^a	(99.9%) ^b	Dry Collection	.06
Ship Unloading Transfer Points	3 Points	10,000 Tons/Day	.2LB/Ton ^a	(97%) ^b	Wet Suppression	.95
Ship Unloading Facility Train	Loading Shed	10,000 Tons/Day	.4LB/Ton ^a	(99.9%) ^b	Dry Collection	.02
Ship Unloading Facility Coal Surge Pile	Active	30 Acres	13LB/Acre/Day ^a	(90%) ^a	Wetting Agents	.20
Rail Car Unloading	Rotary Dumper	10,000 Tons/Day	.4LB/Ton ^a	(97%) ^b	Wet Suppression	.63
Coal Handling Transfer Points	2 Points	10,000 Tons/Day	.2LB/Ton ^a	(99.9%) ^b	Dry Collection	.02
Coal Handling Transfer Points	2 Points	3,300 Tons/Day	.2LB/Ton ^a	(99.9%) ^b	Dry Collection	.01
Coal Handling Transfer Points	6 Points	3,300 Tons/Day	.2LB/Ton ^a	(97%) ^b	Wet Suppression	.62
Coal Handling Transfer Points	7 Points	5,000 Tons/Day	.2LB/Ton ^a	(99.9%) ^b	Dry Collection	.04
Coal Storage at Plant	Active	8 Acres	13LB/Acre/Day ^a	(90%) ^a	Wetting Agents	.05
Coal Storage at Plant	2 Inactive Piles	15 Acres Each	3.5LB/Acre/Day ^a	(99%) ^b	Wetting Agents	.01
Limestone Unloading	Rail Dumper	750 Tons/Day	.4LB/Ton ^a	(99.9%) ^b	Dry Collection	.002
Limestone Transfer Point	1 Point	750 Tons/Day	.2LB/Ton ^a	(99.9%) ^b	Dry Collection	.001
Cooling Towers	Drift	2x603 Grams/Sec	32,963 ppm Solids	21% < 50 Microns	Drift Eliminators	8.4

a (Pedco, 1977)

b (Stoughton, 1980)

Table 3. NAAQS ANALYSIS

Pollutant/ averaging time	Monitored ^a background concentration (ug/m ³)	Maximum ^b projected concentration (ug/m ³)	Total concentration (ug/m ³)	NAAQS (ug/m ³)
SO ₂				
3-hour	123	987	1,110	1,300
24-hour	45	187	232	365
annual	11	13	24	80
PM				
24-hour	79	27	106	150
annual	37	3	40	75
NO ₂				
annual	15	10	25	100
CO				
1-hour	-- ^c	108 ^d		40,000
8-hour	-- ^c	<100 ^d		20,000

^aThese values do not include contributions from the JEA Northside Plant and the St. Regis Paper Co.

^bThese concentrations include contributions from the proposed JEA steam electric generating station, the existing JEA Northside Plant and the existing St. Regis Paper Co.

^cCO monitoring data was not available. However, because of the low ambient air concentrations of CO projected, no violations of the NAAQS for CO is expected.

^dThese values were estimated from the projected SO₂ ambient air concentrations based on worst-case operating load and meteorological conditions.

Table 4. CLASS II INCREMENT ANALYSIS

Pollutant/ averaging time	Maximum ^a Class II increment consumption (ug/m ³)	PSD Class II increment (ug/m ³)
SO ₂		
3-hour	334	512
24-hour	42	91
annual	2	20
PM		
24-hour	17	37
annual	2.3	19

^aThese values include contributions from all increment consuming sources impacting the ambient air quality within 50 kilometers of the proposed new source, including the proposed JEA steam electric generating station. Five years of meteorological data was used in the analysis; therefore, these values represent the highest, second highest concentrations.

Table 5. CLASS I INCREMENT ANALYSIS

Pollutant/ averaging time	Maximum ^a Class I increment consumption (ug/m ³)	PSD Class I increment (ug/m ³)
SO ₂		
3-hour	18	25
24-hour	4	5
annual	<1	2
PM		
24-hour	<1	5
annual	<1	10

^aThese values include contributions from all increment consuming sources within 100 kilometers of the Class I area including the proposed JEA electric steam generating station. Five years of meteorological data was used in the analysis; therefore, these values represent the highest, second highest concentrations.

Table 6. ALLOWABLE EMISSION LIMITS
(lb/hour; lb/MM Btu)

Emission unit	SO ₂	NO _x	PM	CO	Opacity (Percent)
1. Steam generating boiler no. 1 (5,928 MM Btu/hr maximum heat input)	4,502; 0.76 (30 day rolling average)	3,559; 0.6	178; 0.03	296; 0.05	20
2. Steam generating boiler no. 2 (5,928 MM Btu/hr maximum heat input)	4,502; 0.76 (30 day rolling average)	3,559; 0.6	178; 0.03	296; 0.05	20
3. Auxiliary boiler (200 MM Btu/hr maximum heat input)	160; 0.8	60; 0.3	2; 0.01	1; 0.005	10
4. Ship unloading			0.32		no visible emissions
5. Ship unloading transfer points			0.5 (each)		no visible emissions
6. Ship unloading facility train			0.2		no visible emissions
7. Ship unloading facility coal storage pile			1.5		no visible emissions

(continued)

Table 6. (continued)

Emission unit	SO ₂	NO _x	PM	CO	Opacity (Percent)
8. Rail car unloading			5		no visible emissions
9. All coal handling transfer points			5 (each)		no visible emissions
10. Coal storage at plant			0.4 (each pile)		no visible emissions
11. Limestone unloading			0.1		no visible emissions
12. Limestone transfer points			0.1 (each)		no visible emissions
13. Cooling towers			67 (each tower)		20

USE OF FLUE GAS OXYGEN METER AS BACT FOR
COMBUSTION CONTROLS

Within the time limits specified in General Condition 3 of this permit, the permittee shall determine the emissions of nitrogen oxides and carbon monoxide from the permitted combustion device in accordance with test methods and procedures set out in 40 CFR Part 60, Appendix A, Methods 7 and 10, respectively. These emission determinations shall be made at:

- 1) Maximum design capacity; and
- 2) Normal operational load.

The permittee shall install a continuous oxygen monitor in the flue of the permitted combustion device which meets the requirements of 40 CFR Part 60, Appendix B, Performance Specification 3. Results of emission determinations shall be correlated to the flue gas oxygen content to define:

- 1) The point at which Nitrogen Oxides (NO_x) emissions (lb/MMBtu) equals the allowable NO_x emission rate contained in the permit.
- 2) The point at which carbon monoxide (CO) emissions exceed the allowable CO emission rate contained in the permit.

The flue gas oxygen content shall be maintained between these points and alarms shall be set to sound when flue gas oxygen levels exceed either side of this range. Any operation outside of this range will constitute noncompliance with this specific condition, shall be recorded in accordance with General Condition 4 of this permit, and will be reported quarterly along with excess emissions in accordance with 40 CFR 60.7 (c).

Should any combustion equipment modifications be made such as different type burners, combustion air relocation, fuel conversion, tube removal or addition, etc., emissions correlations as described above shall be conducted within 90 days of attaining full operation after such modification. Results of all emission determinations shall be sent to the permitting authority within 90 days after completion of the tests.

GENERAL CONDITIONS

1. The permittee shall notify the permitting authority in writing of the beginning of construction of the permitted source within 30 days of such action and the estimated date of start-up of operation.
2. The permittee shall notify the permitting authority in writing of the actual start-up of the permitted source within 30 days of such action and the estimated date of demonstration of compliance as required in the specific conditions.
3. Each emission point for which an emission test method is established in this permit shall be tested in order to determine compliance with the emission limitations contained herein within sixty (60) days of achieving the maximum production rate, but in no event later than 180 days after initial start-up of the permitted source. The permittee shall notify the permitting authority of the scheduled date of compliance testing at least thirty (30) days in advance of such test. Compliance test results shall be submitted to the permitting authority within forty-five (45) days after the complete testing. The permittee shall provide (1) sampling ports adequate for test methods applicable to such facility, (2) safe sampling platforms, (3) safe access to sampling platforms, and (4) utilities for sampling and testing equipment.
4. The permittee shall retain records of all information resulting from monitoring activities and information indicating operating parameters as specified in the specific conditions of this permit for a minimum of two (2) years from the date of recording.
5. If, for any reason, the permittee does not comply with or will not be able to comply with the emission limitations specified in this permit, the permittee shall provide the permitting authority with the following information in writing within five (5) days of such conditions:
 - (a) description of noncomplying emission(s),
 - (b) cause of noncompliance,
 - (c) anticipated time the noncompliance is expected to continue or, if corrected, the duration of the period of noncompliance,
 - (d) steps taken by the permittee to reduce and eliminate the noncomplying emission,and
 - (e) steps taken by the permittee to prevent recurrence of the noncomplying emission.

Failure to provide the above information when appropriate shall constitute a violation of the terms and conditions of this permit. Submittal of this report does not constitute a waiver of the emission limitations contained within this permit.

6. Any change in the information submitted in the application regarding facility emissions or changes in the quantity or quality of materials processed that will result in new or increased emissions must be reported to the permitting authority. If appropriate, modifications to the permit may then be made by the permitting authority to reflect any necessary changes in the permit conditions. In no case are any new or increased emissions allowed that will cause violation of the emission limitations specified herein.
7. In the event of any change in control or ownership of the source described in the permit, the permittee shall notify the succeeding owner of the existence of this permit by letter and forward a copy of such letter to the permitting authority.
8. The permittee shall allow representatives of the State environmental control agency and/or representatives of the Environmental Protection Agency, upon the the presentation of credentials:
 - (a) to enter upon the permittee's premises, or other premises under the control of the permittee, where an air pollutant source is located or in which any records are required to be kept under the terms and conditions of the permit;
 - (b) to have access to and copy at reasonable times any records required to be kept under the terms and conditions of this permit, or the Act;
 - (c) to inspect at reasonable times any monitoring equipment or monitoring method required in this permit;
 - (d) to sample at reasonable times any emission of pollutants;and
 - (e) to perform at reasonable times an operation and maintenance inspection of the permitted source.
9. All correspondence required to be submitted by this permit to the permitting agency shall be mailed to the:

Chief, Air Facilities Branch
Air and Hazardous Materials Division
U.S. Environmental Protection Agency
Region IV
345 Courtland Street
Atlanta, Georgia 30365
10. The conditions of this permit are severable, and if any provision of this permit, or the application of any provision of this permit to any circumstance, is held invalid, the application of such provision to other circumstances, and the remainder of this permit, shall not be affected thereby.

The emission of any pollutant more frequently or at a level in excess of that authorized by this permit shall constitute a violation of the terms and conditions of this permit.

MEMORANDUM



DATE: June 9, 1987

To: Tom Rogers, JEA

From: Marion G. DeGrove, Associate Engineer

Re: **SO₂ Modeling**

Thanks for sending me your file. I copied it, and am returning the original. It will take me a while to digest all of the information.

Marion De Grove
Marion G. DeGrove, Associate Engineer

Enclosures

cc: BESD File, Air Monitoring 1987

MGD/bgm

State of Florida
DEPARTMENT OF ENVIRONMENTAL REGULATION



Interoffice Memorandum

To: Buck Oven

From: John Brown ^{JB}
Clair Fancy ^{CF}

Subject: St. Johns River Power Park Operating Restrictions Proposal

Date: October 31, 1986

FOR ROUTING TO OTHER THAN THE ADDRESSEE	
To: <u>Clair Fancy</u>	LOCN: _____
To: _____	LOCN: _____
To: _____	LOCN: _____
FROM: _____	DATE: _____

The following comments are submitted in reference to Jacksonville Electric Authority's proposal for meeting the requirements of Part IE, Conditions of Certification of the St. John's River Power Plant.

It appears that JEA did not meet the requirement of condition IE2 since they did not file the operating plan by June 1, 1986 as required.

Their proposal seems to otherwise meet the requirements of condition IE. Paragraph 3 of the JEA letter should state that "JEA will not start up Southside units 1 or 2 until the department reviews and approves the operating plan to offset emissions equivalent to those from Southside units 1 and 2."

The plan to leave SJRPP in operation during an episode seems reasonable subsequent to demonstrating full compliance. Until then there needs to be a contingency plan.

If you have additional information or questions on the above, please contact Jim Pennington at 904-488-1344.

JB:JP:ht

July 17, 1986

DER

JUL 21 1986

BAQM



Mr. Hamilton S. Oven, Jr., P.E.
Administrator
Siting Coordination Section
Fla. Dept. of Env. Regulation
2600 Blair Stone Road
Tallahassee, Florida 32301

Dear Mr. Oven:

Subject: Jacksonville Electric Authority
St. Johns River Coal Terminal
Response to BESD Letter

The Jacksonville Electric Authority (JEA) has received a copy of the Bio-Environmental Services Division (BESD) letter dated July 1, 1986, concerning the modification of the St. Johns River Coal Terminal's PSD permit. The purpose of this letter is to discuss BESD's comments, many of which JEA feels are based on information which has been taken out of context and are therefore not representative of expected operating conditions at the coal unloader and conveyor system. Listed below are JEA's responses to BESD's comments.

1. BESD supports the design change from rail coal conveying to an enclosed belt conveyor.

JEA appreciates BESD's support of the conveyor design. JEA maintains that the transport of coal by an enclosed conveyor represents an improved design, resulting in reduced environmental impacts over the original rail transport design.

2. Dust control on the ship unloader

JEA shares BESD's concern for potential deposition on the import car facilities; however, BESD's statement that emissions at the ship unloading point would be over 330% of the original value is based on an analysis taken out of context. It is true that the emissions from the ship unloading point will increase; however, in absolute terms, BESD has compared two very small numbers. The increase at the ship unloading point is from approximately 0.3 lb/hr to 1.0 lb/hr. In addition, a major point which seems to have been overlooked by BESD is that the current design modification will in fact result in a significant decrease in particulate emissions on Blount Island of approximately 5.1 lb/hr, not a "substantial increase" as indicated by BESD.

(CONT.)

JEA proposes to use wet dust suppression in addition to containment to meet the emission limits presented in the PSD modification. The vendor supplying the ship unloader (which will include the particulate control equipment) will be required per his contract to guarantee that the 10% opacity standard will be met.

3. Separate BACT determinations

The total emissions resulting from the modification of the PSD permit results in a net decrease in particulate emissions. Thus, re-addressing BACT (Best Available Control Technology) is not warranted by the proposed PSD modification.

4. Lower the visible emission standard

BESD asserts without supporting information that the visible emission standard should be reduced from 10% to 5% opacity. The initial licensing process for the Power Park and the coal unloading facility established a 10% standard. During this licensing process, analyses were conducted to determine the effect on ambient air quality and appropriate standards were set by the agencies. Since that time, ambient particulate levels have improved in Duval County resulting in a reduction in the size of the particulate non-attainment area. For this reason, there has been an increase in the distance between the non-attainment area boundary and the project site. This improvement along with the fact that the total emissions are slightly less than the original PSD permit levels would seem to justify the current 10% opacity level.

5. Installation and operation of deposition monitoring station

BESD has recommended that JEA install a particulate deposition monitor on Blount Island. In light of the proposed impact reduction in particulate emissions, JEA does not feel that a deposition monitoring program is necessary as part of the PSD permit. If this program is deemed necessary for some other regulatory purpose, JEA would be willing to discuss this matter further.

(CONT.)

Mr. Hamilton S. Oven
July 17, 1986
Page 3.

If you have any questions or require any additional information,
please feel free to contact me at (904) 633-4517.

Very truly yours,



Richard Breitmoser, P.E.
Division Chief
Research & Environmental
Affairs Division

RB/AJT/lwr

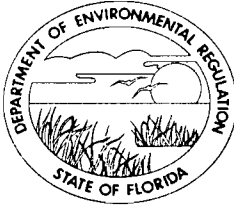
cc: Royce Lyles, JEA
Bill Stewart, DER
Clair Fancy, DER
Henry Colson, JPA
Paul deMariano, JPA
Bruce Miller, EPA
Ted Bisterfeld, EPA
Mike Branden, EPA
Ed Svec, FDER

ST. JOHNS RIVER COAL TERMINAL

Submittal Title	Licensing Procedure	JEA Sub. Date	Agency Review	Exp. Response Date	Next Agency Action	Comments
Blount Island Well	Amend SCA/EID Modif. Cond. of Cert. III	3/26/86	N/A	N/A	Issue Final Order of Modification	- FDER sent out Notice to parties on 3/27/86 - FAW Notice May 2, 1986
FDER Dredge and Fill Modification	Approval Under Cond. of Cert. XXXII	3/24/86	90 days	6/24/86	Publish Notice of Decision in FAW	- FDER sent out Notice to parties on 3/27/86 - FDER questions 5/30/86 / JEA response 6/18/86 - Dredge and Fill approval for FDNR lease and fee waiver
Amendment to Fugitive Emissions Control Summary	Approval Under Cond. of Cert. XXXII	5/15/86	90 days	8/15/86	Publish Notice of Decision in FAW	- FDER sent out Notice to parties on 6/2/86 - FDER questions 5/30/86 / JEA response 6/18/86
Condition of Certification XXXII	Approval Under Cond. of Cert. XXXII	4/25/86	90 days	7/28/86	Publish Notice of Decision in FAW	- FDER sent out Notice to parties 5/14/86 - Need FDER approval for FDNR Use Approval - Approval should include Water Quality Cert. for conveyor and State concurrence with JEA's CZM statement. WQC and CZM necessary for U.S. Coast Guard Bridge Permit
PSD Revision	FDER to provide tech. review	⁵ 8/12/86/EPA 6/15/86/FDER	N/A	8/15/86	FDER Technical Comments to EPA	- FDER to provide JEA with information for Public Notice (Ed Svec-FDER)
Particulate Emission Control Equipment Data	Compliance w/ Cond. of Cert. I.A.3.b.	Exp. 7/21/86	30 days	Exp. 8/21/86		- Submittal currently being prepared by JEA

STATE OF FLORIDA
DEPARTMENT OF ENVIRONMENTAL REGULATION

TWIN TOWERS OFFICE BUILDING
2600 BLAIR STONE ROAD
TALLAHASSEE, FLORIDA 32301-8241



BOB GRAHAM
GOVERNOR
VICTORIA J. TSCHINKEL
SECRETARY

December 9, 1985

Mr. Richard Breitmoser, Chief
Research & Environmental Affairs Division
Jacksonville Electric Authority
233 West Duval Steet
Jacksonville, Florida 32202

Dear Mr. Breitmoser:

The second ambient air monitoring site for the St. Johns River Power Park that you proposed in your November 27, 1985, letter is acceptable to us at this time. All EPA siting and instrumentation criteria must be met, and all necessary SAROAD forms must be filed with the department as soon as possible.

Our acceptance of this site at this time does not preclude you from relocating the site in the future, provided such relocation would also have to be approved. We understand that the Jacksonville Bio-Environmental Services Division is concerned that construction in the area may someday adversely affect this location.

Please direct all future correspondence on this subject to Mr. Bill Blommel, Environmental Administrator, Air Monitoring Section.

Sincerely,

Lawrence A. George
Environmental Administrator
Bureau of Air Quality
Management

LG/ps

cc: M. DeGrove, Jacksonville BESD
B. Blommel
F. Watkins

SJRMISC-85-525
November 27, 1985



Mr. Larry George
Florida Department of
Environmental Regulation
2600 Blair Stone Rd.
Tallahassee, Florida 32301

Dear Mr. George:

Subject: **St. Johns River Power Park, Units 1 & 2
AMBIENT AIR MONITORING STATIONS
SITE SELECTION**

The SJRPP is required by our Conditions of Certification to site and operate two ambient air monitors for SO₂ and particulate matter (each). One site has been selected to the north of the plant off of Cedar Point Road. This site was previously approved by your office and the Jacksonville Bio-Environmental Services Division (BESD). The other site which we are now proposing is located south and west of the plant adjacent to August Drive. This site is located as close to a predicted location of maximum concentration as possible; it conforms to EPA siting criteria, and was identified in cooperation with the BESD.

Thus, we request that you review the site location as necessary and notify me of its acceptability. Following the approval we plan to begin installation of the shelter and equipment with Start-up by early January, 1986. Bio-Environmental Services will then operate the stations as part of a cooperative agreement.

DER

DEC 02 1985

BAQM

AMBIENT AIR MONITORING
Page Two

If you have any questions please call Mr. Stan Stokes
at 757-2866. Your prompt review will be appreciated.

Sincerely,



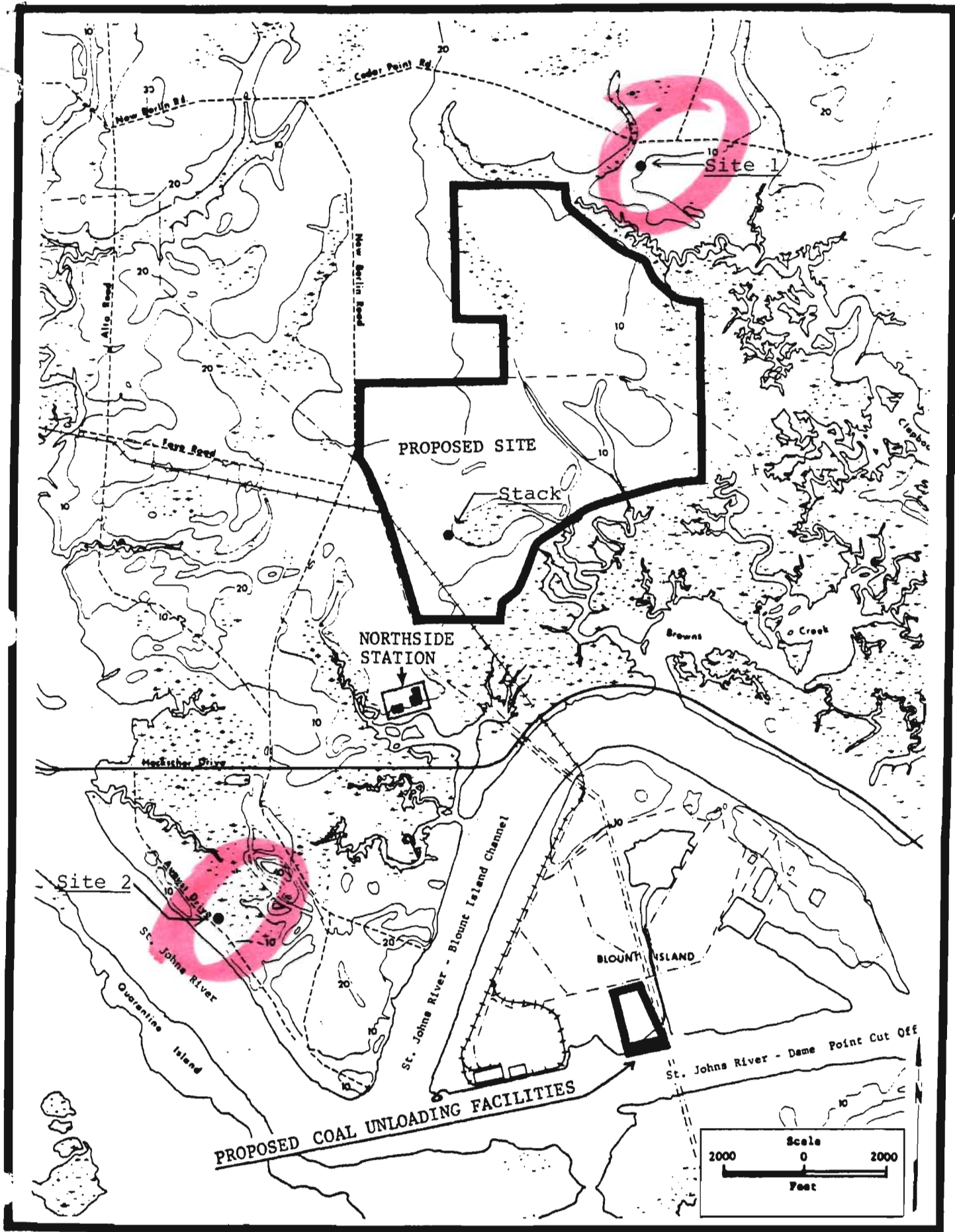
Richard Breitmoser, Chief
Research & Environmental
Affairs Division

RB/STS/pmh

cc: R. Lyles
W. Fries
R. Donatelli (2)
R. Bloor
B. Wirz
A. Bavington
C. Slepow
J. Herman
J. Clark
C. French
R. Kermitz
F. Fuerst
F. Bold
J. Rutledge
W. Ondler
J. Weitzel
S. Stokes
C. Pait
M. DeGrove
B. Blommel, FDER
F. Watkins, FDER

Attachment: Map of Selected Monitoring Sites

wp: STS/Env.



AIR MONITORING SITES 1 AND 2

copy: district } sent
 Jax BES } 10/20/83 PA
 file permit file



UNITED STATES ENVIRONMENTAL PROTECTION AGENCY

REGION IV

345 COURTLAND STREET
ATLANTA, GEORGIA 30365

OCT 3 1983

4AW-AM

Mr. Richard Breitmoser, P.E.
Division Chief
Research & Environmental Affairs Division
Jacksonville Electric Authority
233 W. Duval Street
Jacksonville, Florida 32201

RE: St. Johns River Power Park - Auxiliary Boiler Design and
Conveyor Gallery Design

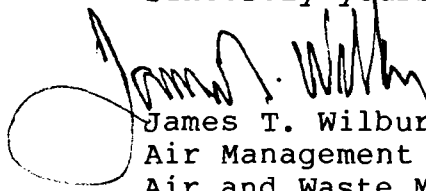
Dear Mr. Breitmoser:

This letter is in response to your letters of August 29, 1983 and August 22, 1983, regarding the increase in steam pressure and temperature and BTU input for the auxiliary boilers and conveyor gallery design and control efficiency considerations.

In regard to the conveyor gallery design, we generally concur with the information provided, with the exception of the control efficiency for water spray dust suppression on the stacker/reclaimer conveyor discharges. Literature indicates efficiencies of 30-40% for wet suppression on conveyors. In conjunction with partial enclosures with estimated efficiency of 70% to 80%, the estimated total efficiency will be 91% ($1 - [(1 - .75) \times .35]$). In addition, the face velocity at the ventilation system vents within the galleries should be held well below 100 ft. per second per ft.² to prevent entrainment of dust particles.

If you should have any questions or comments regarding this letter please contact Mr. Michael Brandon at 404/881-7654.

Sincerely yours,


James T. Wilburn, Chief
Air Management Branch
Air and Waste Management Division

cc: Steve Smallwood, Chief
Bureau of Air Quality Management

Received DER
AUG 23 1983
PPSS

SJRFDER 83-8
August 18, 1983

DER
st/jr
johns
river
1984
OWER
APK

Mr. Hamilton S. Oven, Jr., P.E.
Administrator - Power Plant Siting Section
Florida Department of Environmental Regulation
2600 Blair Stone Road
Tallahassee, Fl 32301

Dear Mr. Oven:

Subject: St. Johns River Power Park Units 1 & 2
Change in Project Construction Schedule

The purpose of this letter is to inform you of the change in the Project Construction Schedule as required by Section I.A.8 of the Conditions of Certification.

The Project Construction Schedule contained in the PSD application and the SCA/EID indicated Project Certification (commercial operation) for Unit 1 in December 1985 and for Unit 2 in July 1987. Although construction has already commenced (December 1, 1982), the present schedule calls for Project Certification for Unit 1 in April 1987 and for Unit 2 in October 1988.

The Conditions of Certification which associate the SJRPP Units 1 & 2 Project Certification Dates with the submittal date of a particular condition will be changed accordingly.

Further, submittal dates for some other conditions should be changed appropriately to reflect the revised commercial operation dates.

These changes include the following:

<u>Section</u>	<u>Existing Date</u>	<u>Revised Date</u>
I.B.6 - Salt Drift Monitoring Program Implementation (1 yr before project cert.)	Dec. 1, 1984	April 1, 1986
I.E.2 - Proposed System Operating Plan (6 mo. before proj. cert.)	June 1, 1984	Oct. 1, 1985

Mr. Hamilton S. Oven
August 18, 1983
Page 2 -

<u>Section</u>	<u>Existing Date</u>	<u>Revised Date</u>
I.E.4 - Schedule of Implementation (date of proj. cert.)	Dec. 1, 1985	April 1, 1987
II.A.15 Submittal of Bioassay Test Program (2 yrs. before proj. cert.)	Dec. 1, 1983	April 1, 1985

If you have any questions, please contact me at (904)633-4517.

Sincerely,



Richard Breitmoser
Environmental Supervisor

RB:PEJ:cb

cc: D. Dutton, FDER
P. Gaboury, JEA
L. Leskovjan, FPL
P. Jennings, FPL
J. Jackson, ESI

File: 1.6.10.1(2)
1.6.10.13(2)
NG
Chrono

BEST AVAILABLE COPY

cc Clair Fancy
Devy Dutton
JACKSONVILLE ELECTRIC AUTHORITY
P.O. BOX 53015
250 W. DUVAL STREET
JACKSONVILLE, FL 32201

SJRFDER 83-7

August 16, 1983



DER
AUG 19 1983
BAOM
Received DER

Mr. Hamilton S. Oven, Jr., P.E.
Administrator - Power Plant Siting Section
Florida Department of Environmental Regulation
2600 Blair Stone Road
Tallahassee, Florida 32301

AUG 18 1983

Dear Mr. Oven:

Subject: St. Johns River Power Park
Units 1 & 2
Revised Chimney Location

R P S

This is to provide a change in the coordinates of the main chimney of the proposed St. Johns River Power Park. The revised chimney coordinates are:

N	Latitude:	30° 25' 51"
W	Longitude:	81° 33' 03"
UTM N-S		3366.42 km
UTM E-W		447.07 km

This new chimney location is .12 km north of the original location presented in the 1980 Prevention of Significant Deterioration (PSD) Report for the Jacksonville Electric Authority and the 1981 St. Johns River Power Park Site Certification Application/Environmental Information Document.

This chimney relocation is small relative to the downwind distances (ranging between 1 km and 5 km) at which maximum ground level air quality impacts resulting from the main boiler operation were predicted by dispersion modelling. Therefore, the changes in location and magnitude of the calculated maximum ground level impacts for PSD increment consumption and compliance with National and Florida Ambient Air Quality Standards will be insignificant.

(CONT.)

Mr. Hamilton S. Oven, Jr.
August 16, 1983
Page 2.

If you have any questions regarding the new chimney location, please call me at (904) 633-4517 at your earliest convenience.

Very truly yours,



Richard Breitmoser, P.E.
Division Chief
Research & Environmental
Affairs Division

RB/lwr

cc: D. Bayly, BES
P. Gaboury, JEA
L. Leskovjan, FPL
P. Jennings, FPL
J. Jackson, ESI
File 1.6.9.14
1.6.10.3 (2)
NG
Chrono

cc Clair Fancy

Jacksonville Electric Authority

233 WEST DUVAL STREET • P. O. BOX 53015 • JACKSONVILLE, FLORIDA 32201



November 13, 1981

Mr. Kent Williams, Chief
New Source Review Section
Air Facilities Branch
Environmental Protection Agency
Region IV
345 Courtland Street, N.E.
Atlanta, Georgia 30308

RECEIVED
NOV 19 1981
DIV. ENVIRONMENTAL
PERMITTING

Dear Mr. Williams:

Subject: JACKSONVILLE ELECTRIC AUTHORITY
ST. JOHNS RIVER POWER PARK UNITS 1 & 2
PSD APPLICATION (PSD-FL-010)
COMMENTS ON REVISED PRELIMINARY DETERMINATION

Attached please find our comments on the Revised Preliminary Determination as it was presented in the Draft Environmental Impact Statement/State Analysis Report, dated October 1981. Although many of our comments are editorial in nature, several are substantive and may require further discussion before an appropriate resolution can be made. Please review these comments as soon as possible and let us know if you feel that a meeting will be necessary to resolve any of the issues identified. If possible, we would like to see these issues resolved prior to the public hearings which are scheduled to begin on 12/1/81.

Thank you for your immediate attention to this matter.

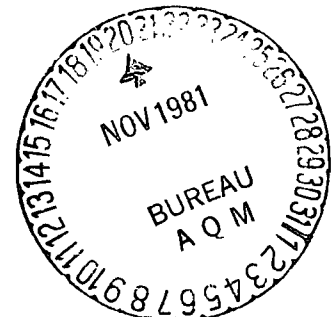
Sincerely,

Richard Breitmoser DTF

Richard Breitmoser
Division Chief
Research and Environmental Affairs

RB/pag
Att.

- cc: D. Lucas
- D. Fulle
- D. A. Moehle
- R. Lyles
- L. Leskovjan
- J. E. Hagan (EPA)
- ~~H. Owen~~ (FDER)
- File



COMMENTS ON PSD REVISED PRELIMINARY DETERMINATION (RPD)

Page 1, Section III

Issue: A maximum heating value for the No. 2 fuel oil to be burned in the auxiliary boilers is specified.

Resolution: The words "a maximum higher heating value of 19,567 Btu/lb" should be changed to "an approximate heating value of 19,500 Btu/lb" to allow for fluctuations in oil heating value that are normally expected and to make the condition consistent with a similar condition in FDER's Conditions of Certification.

Page 2, Section III

Issue: "Coal will be transferred from the marine terminal to the proposed plant site by shuttle train."

Resolution: The words "or other means of coal transport" should be added to the above sentence because alternate means of coal transfer are still under investigation and may ultimately be chosen. The method of coal transport chosen should have no measurable effect on air quality.

Page 2, Section III

Issue: "Dry" storage silos for limestone.

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DIV. ENVIRONMENTAL
PERMITTING

Resolution: This should be changed to "day" storage silos.

Page 5, First Paragraph

Issue: Reference to the No. 2 fuel oil which will be used to fire the auxiliary boilers. It is indicated in two places that the oil will have a sulfur content of 0.76% by weight.

Resolution: The words "a maximum" should be inserted before 0.76 wt % sulfur fuel oil in both places to allow for normal fluctuations in fuel oil sulfur content.

Page 5, Third Paragraph

Issue: Typo in third paragraph.

Resolution: The word "fo" should be changed to "to" on the 12th line of that paragraph.

Page 5, Sixth Paragraph

Issue: Reference to sealed trucks for fly ash transport to landfills.

Resolution: Sealed trucks will be used for transport of fly ash for sale. However, since fly ash to be transported to the landfills will be wetted prior to loading into trucks, the use of sealed trucks is unnecessary and is not planned.

RECEIVED
NOV 19 1981

DIV. ENVIRONMENTAL
PERMITTING

Therefore, the sentence should be modified to read: "Transfer of fly ash for sale will be by sealed trucks and of fly ash for disposal by dump trucks."

Page 6, First Paragraph

Issue: A fuel oil ash content of 0.01 wt. % is specified.

Resolution: The words "an ash content of 0.01 wt. %" should be changed to "a maximum ash content of 0.01 wt. %" to allow for normal fluctuations in fuel oil ash content.

Page 6, Third Paragraph

Issue: The requirement for setting a CO emission limitation during NO_x performance testing as well as the requirement for controlling NO_x and CO emissions using a flue gas oxygen meter are unnecessary.

Resolution: As indicated in our comment on Specific Condition 7 on Page 13 of the RPD, a specific emission limit for CO is not feasible. Also, although a flue gas oxygen meter will be used, it will be only one of several means for controlling CO and NO_x emissions and, in practice, can only be used as a guideline. Therefore the second, third, and fourth sentences of the third paragraph on page 6 should be deleted.

RECEIVED

NOV 19 1981

DIV. ENVIRONMENTAL
PERMITTING

Issue: The RPD discusses the analysis of existing air quality based on historical data obtained from the New Berlin monitoring site. The results of the on-site monitoring program are now available.

Resolution: The second paragraph of Section IV-B on Page 6 should be replaced with the following:

"Monitoring data for SO₂, NO_x, CO, O₃ and PM were obtained for a site about 0.5 km north of the northeast boundary of the proposed plant site during the period from December 1979 to December 1980. The results of the monitoring program were presented in four quarterly reports which were submitted to EPA as addenda to the PSD application."

The words "Jacksonville International Airport" in the first paragraph on page 7 of the RPD should be changed to "on-site monitoring program."

The second paragraph on page 7 of the RPD should be eliminated.

These changes are based on information submitted to EPA in a letter from D. Moehle to K. Williams dated 10/21/81.

RECEIVED
NOV 19 1981

DIV. ENVIRONMENTAL
PERMITTING

Issue: Various dispersion models which were used in the NAAQS analysis are referred to in this section. Since reanalyses have been conducted for a variety of reasons, the list of models utilized is no longer correct.

Resolution: The first sentence of the first paragraph of the above referenced section should be modified to begin as follows:
"The EPA - approved dispersion models CRSTER (modified for use with multiple sources) and ISC were utilized.." This change was described in a letter from D. Moehle to K. Williams dated 10/21/81, as it relates to a revised fugitive dust analysis.

Page 10

Issue: The conclusion on page 10 of the RPD refers to dates on which information was provided to EPA regarding the application. Additional information has been provided since the dates indicated.

Resolution: The dates of the letters providing additional information to EPA regarding the PSD application should be added. These include July 30, 1981; September 8, 1981; and October 21, 1981.

RECEIVED
NOV 19 1981

DIV. ENVIRONMENTAL
PERMITTING

Page 11, Condition 3

Issue: Performance test requirements refer to emission point 3 (auxiliary boilers) and to CO emission test methods.

Resolution: Condition 3 should be modified to refer to performance tests for only emission points 1 and 2 in Table 6 rather than for emission points 1, 2, and 3. Reference to Method 10 should be deleted since a CO emission limit is infeasible. Also the third paragraph of this condition should be modified to refer to emission points 3 through 13 of Table 6 rather than emission points 4 through 13 of Table 6 since the auxiliary boilers should also be exempted from mass emission rate compliance tests.

Page 11, Condition 4

Issue: Requirement for flue gas oxygen meter, as described in an attachment following the general conditions of the RPD.

Resolution: Although the use of flue gas oxygen meters is planned as one of several methods of controlling CO and NO_x emissions, we feel that the requirement as described in the above referenced attachment is not feasible and is unnecessary as indicated in our response to specific Condition 7 on Page 13 of the RPD. CO and NO_x emissions will be monitored directly in the main units and are very small in the case of the auxiliary boilers.

.Therefore, the first paragraph of Condition 4 and the attachment regarding use of the flue gas oxygen meter should be deleted.

Page 12

Issue: Typo in second paragraph.

Resolution: Change .7 to .76 in the second line of that paragraph.

Page 12, Condition 6.d

Issue: Typo in condition 6.d on page 12.

Resolution: Change "Dry" storage silos to "day" storage silos in the second line of that condition.

Page 13, Condition 7

Issue: Carbon monoxide emission limitation.

Resolution: Boilers are designed for optimum combustion efficiency and this design inherently minimizes the production of carbon monoxide. It is in the best interest of the utility to minimize CO emissions for both economic (combustion efficiency) and safety reasons. Therefore, JEA will make every attempt to limit CO emissions. However, since the

boiler vendor cannot and will not guarantee a CO emission level, it is not feasible for JEA to comply with a specific CO emission limitation.

The boiler vendor has indicated that optimum boiler operation can be achieved by maintaining minimum excess O_2 while simultaneously keeping CO emissions as low as practicable. This will also be the condition at which NO_x is minimum for normal boiler operation. However, the parametric relationship between NO_x , O_2 and CO will change with:

- . boiler load,
- . number of ball mills in service
- . coal characteristics (volatility, moisture, grindability, etc.)
- . coal nitrogen content and heating value.

Consequently, the excess O_2 range suggested by EPA (between the 0.6 NO_x point and max. CO point) may limit boiler flexibility since this range will change as boiler operating mode changes. Since compliance tests are performed at full load, the O_2 end points thus developed may not be valid during other operating conditions.

The design of the steam generators and their combustion systems is such that the NO_x limit will not be exceeded during normal steam generator operation. But if the EPA recommended method based on a specified O₂ range is to govern boiler operation, JEA's flexibility may be unduly limited.

If, instead, monitoring flue gas O₂ is used only as guideline, we would expect no operational limitations to result. We do not agree that the use of O₂ monitoring alone is BACT for NO_x or CO control.

In light of the above, we request that BACT for CO be expressed as follows:

"JEA will utilize boiler combustion controls and burner settings in order that NO_x emission limits may be observed while maintaining CO emissions at the minimum practicable level."

Page 13, Condition 10

Issue: Typo in Condition 10 on page 13.

Resolution: Change Southside (Units 1-4) to Southside (Units 1-5) in the second line of that condition.

Table 1

Issue: The potential emissions from the project, in tons per year, presented in Table 1 are incorrect.

Resolution: The potential emissions should be as follows:

SO ₂	41,800
PM	1,670
NO _x	32,700
CO	2,870
VOC	28

These are based on continuous full load operation of the main units and auxiliary boilers and assume worst case fuel conditions.

Table 2

Issue: The fugitive emission and control summary (Table 2) in the RPD has been updated by information submitted in a letter from D. Moehle to K. Williams dated 10/21/81.

Resolution: Replace Table 2 with the updated information attached to the referenced 10/21/81 letter.

Tables 3,4 and 5

Issue The numbers presented in the NAAQS Analysis Summary (Table 3), the Class II Increment Analysis (Table 4), and the Class I Increment Analysis (Table 5) in the RPD have been updated by information submitted in a letter from D. Moehle to K. Williams dated 10/21/81.

Resolution: Revise Tables 3,4 and 5 based on Exhibits 4,2, and 3, respectively, attached to the referenced 10/21/81 letter. The changes result from (1) use of on-site monitoring data for background instead of historical data from the New Berlin Site, (2) the increase in unit heat input from 5928 to 6144 MMBtu/hr, (3) consideration of the auxiliary boilers, and (4) revisions in the fugitive dust calculations.

Table 6

Issue: Some of the numbers presented in Table 6 (allowable emission limits) of the RPD need to be revised for various reasons.

Resolution: The following revisions to Table 6 should be made for the following reasons:

- a. The numerical emission limits for the auxiliary boilers (emission Unit 3) are not appropriate since they are estimated emissions rather than guaranteed values. The

potential boiler vendors have indicated that they do not guarantee specific emission rates. We believe that BACT for the auxiliary boilers is the use of low sulfur, low ash fuel rather than any specific control technology. Hence, given the use of a specific fuel as BACT (as required in Specific Condition 5) and the fact that no control technology is used, there is no need for specific emission limitations, especially if one considers that the auxiliary boilers will only be operated about 5% of the year.

- b. The ship unloading facility storage pile emission limit should be 1.6 lbs/hr rather than 1.5 lbs/hr; this difference is apparently due to a rounding error.
- c. The emission limits for Emission Units 10 and 11 should be modified so that one refers to points where control is by wet suppression and the other refers to points where control is by dry collection. It is suggested that Emission Unit 11 refer to the 11 dry dust collection points and that the emission limits be 0.1 lbs/hr (each). It is suggested that Emission Unit 10 refer to the six wet dust suppression points and that the emission limits be 5 lbs/hr (each).

d. The emission limit for Emission Point 14 (Limestone Rail Dumper) should be changed to 0.4 lbs/hr from 0.1 lbs/hr in accordance with the information submitted to EPA regarding this system in the 7/30/81 letter from D. Moehle to K. Williams.

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RESPONSES TO FDER INTERROGATORIES (APRIL 28, 1981)

Question 1: JEA used tall stacks at Kennedy and Southside Generating stations for modeling, however, at this time (4/20/81) JEA is not taking steps to construct said tall stacks. Please explain.

Response: The only analysis in the Site Certification Application which explicitly included the Kennedy and Southside Generating Stations is the worst-case year analysis, the results of which are presented in Table 5.3-1. Tall stacks were used in the analysis since at that time it was assumed that they would definitely be built. However, in accordance with recommendations from EPA Region IV, the detailed analysis for determination of compliance with ambient standards did not explicitly consider these sources. Kennedy and Southside (at their existing stack heights) were implicitly considered in these analyses through the background air quality concentrations determined from the on-site monitoring program; only the proposed source, Northside, and St. Regis were explicitly modelled.

The JEA has entered into contract with the Southern Company to purchase 600 MW of coal generated electric power. Transmission lines to bring this power into Florida are currently under construction. The first of two 500 kv transmission lines will be in service by August, 1982. The second line will be in service by January, 1983. The effect of this large block of purchased power is to reduce the need for power generation from the Southside and Kennedy Generation Stations. The exact degree of reduced generation, however, is unknown at this time.

If the Kennedy and Southside units are removed from service or greatly reduced in output, the JEA will recommend that tall stacks not be constructed.

A rigorous study of the import power operating mode is currently underway. The results of that study will be made available immediately upon completion.

Question 2: JEA should specifically define the operational state of the Kennedy and Southside Generating Stations, and model accordingly. These operational states should be clearly expressed as permit conditions for the Coal Fired Units.

Response: Suggested by FPL. The operational stations of Kennedy and Southside should not be expressed as permit conditions for SJRPP. They already have approved permits; we do not wish to limit their capabilities and affect system reliability. Please see the response to Question 1.

Question 3: JEA has used differing input data for the modeling efforts presented in this application and their PSD application. Please explain.

Response: The differing input includes differences in background concentrations and emissions inventories. Because the on-site monitoring program was not completed at the time of the May, 1980 PSD application, the background estimates were based on regional air quality monitoring data supplied by the Jacksonville Bio-Environmental Services Division (BESD). The background values presented in the SCA/EID in January, 1981 were based on the results of the on-site monitoring program and were submitted to EPA as an addendum to the PSD application in November, 1980.

The original emissions inventory for PSD increment consuming sources and ambient emissions sources was performed in March, 1980, by canvassing the various DER offices and the BESD. This inventory was included in modeling runs that were used to develop ground-level pollutant concentrations estimates for the May, 1980 PSD submittal. Pursuant to requests by EPA during the initial review of the PSD application, an additional inquiry was made of the regulatory agencies in June of 1980 regarding the inventory of increment consuming sources. This inquiry resulted in some changes to the emission inventory modeling input. The resulting re-analysis was submitted to EPA on July 8, 1980. Correspondence with the Department of Environmental Regulation personnel in November, 1980 regarding the baseline date indicated that an additional PSD increment consuming source existed outside the Jacksonville area which had not been considered in the earlier analyses. The latest inventory was used for modeling input for the SCA/EID submittal in January, 1981. Although the emissions inventories vary somewhat, the resultant differences in ground-level concentrations are not significant.

Question 4: JEA expresses that PAL was used to model fugitive emissions, however, results are not presented. Please provide results.

Response:

The following pages present the PAL computer output used to estimate the highest and second highest fugitive emission impacts for comparison to PSD and NAAQS standards. As indicated in Section 5.3.1.2 of the SCA/EID, PAL was run on 18 "worst case" days of meteorological data which were selected based on a CRSTER run using the entire year of 1973 as meteorological input. Because of the relatively large TSP emission rate from the main boilers and the low release heights of the fugitive emissions, the other more distant TSP sources in the emissions inventory were not included in the PAL modeling. The relative impacts from these other sources are very small due to their relatively small emission rates, high release heights and exit velocities, and greater distances from the receptor points which are located in the vicinity of the plant property boundary.

Question 5:

In order to better evaluate the isopleths presented throughout the text, please identify the computer run used to generate the specified.

Response:

The attached computer printouts were used to generate the air quality isopleths presented in the text:

Figure 5.3-2 - Predicted Annual Average SO₂ PSD Increment Consumption

Figure 5.3-3 - Predicted Annual Average TSP PSD Increment Consumption

Figure 5.3-4 - Predicted Highest, Second-Highest 24-Hour Average SO₂ PSD Increment Consumption

Figure 5.3-5 - Predicted Highest, Second-Highest 3-Hour Average SO₂ PSD Increment Consumption

Figure 5.3-6 - Predicted Highest, Second-Highest 24-Hour Average TSP PSD Increment Consumption

Figure 5.3-7 - Predicted Annual Average SO₂ Ambient Impacts

Figure 5.3-8 - Predicted Highest, Second-Highest 24-Hour Average SO₂ Ambient Impacts

Figure 5.3-9 - Predicted Highest, Second-Highest 3-Hour Average SO₂ Ambient Impacts

Figure 5.3-10- Predicted Annual Average TSP Ambient Impacts

Figure 5.3-11- Predicted Highest, Second-Highest 24-Hour Average TSP Ambient Impacts

Figure 5.3-12- Predicted Annual Average NO₂ Ambient Impacts

Question 6: The dispersion modeling output needs to be received in order to determine correct use of the models and proper interpretation. Many other questions concerning the modeling can be answered when by looking at this output.

Response: Copies of dispersion modeling output are attached for the following analyses:

- a. Worst-Case Load Analysis-Plant by Itself
- b. Five-Year Analysis-Major Sources
- c. Highest and Second-Highest PSD Class II SO₂ Concentrations
- d. Highest and Second-Highest PSD Class II TSP Concentrations
- e. Highest and Second-Highest PSD Class I SO₂ Concentrations
- f. Highest and Second-Highest Ambient SO₂ Concentrations
- g. Highest and Second-Highest Ambient TSP Concentrations

Question 7: The baseline date used, November 25, 1977, is incorrect. The correct dates are December 27, 1977 for particulate matter and July 9, 1980 for SO₂.

Response: After discussing the question of baseline date with L. George of FDER and A. Lee of EPA Region IV, we were directed to Bill Wagner of EPA Region IV on December 9, 1980. Mr. Wagner indicated to us in a telephone conversation on that date that the baseline date was set for both SO₂ and TSP statewide (except for nonattainment areas) on November 25, 1977 when the Occidental Chemical White Springs PSD application was deemed "complete".

However, even if this information is not correct, and the baseline dates are in fact December 27, 1977, and July 9, 1980, for SO₂ and TSP, respectively, the emission inventories modelled are correct since Occidental Chemical would be the only source subject to possible deletion, and it appears to be a "major" source which must be modelled regardless of the baseline date.

Question 8: The JEA conducted a noise survey of the area in and around the project site. Please advise whether the noise meter was operated in the "slow" or "fast" response mode.

Response: It was operated in the "slow" response mode.

Question 9: The JEA noise survey reflects that exceedances of the EPA 55dB(A) guideline will occur. What provisions will JEA use to resolve noise complaints?

Response: Many noise control measures are being taken in the design and construction of the plant to minimize noise levels in plant and off site. Because the EPA guideline of 55dB(A) may be exceeded, does not necessarily mean that complaints will occur at and above that level.

Complaints will be investigated on a case-by-case basis in accordance with existing JEA policy. If the situation warrants, a noise survey will be conducted at the location of the complaint, first to verify the validity of the complaint, and second to determine the exact source of the noise. If feasible, appropriate corrective actions will be taken.

Question 10: Since annoyance and perceived loudness are a function of frequency, did JEA perform any spectrum analysis, and if so, please provide such data.

Response: No spectral analyses of the existing ambient noise were performed, primarily because of the character of the existing noise. The existing noise can be described as "white" noise. That is, the power per-unit of frequency is substantially independent of frequency over the audible range of the human ear. No pure tones were noted by the monitoring personnel. A spectral analysis would be more appropriate after the plant is in operation.

Question 11: In projecting the noise from the construction of the power plant, was the noise contribution from the concurrent construction of the coal handling facility at Blount Island included?

Response: Yes, but its contribution was insignificant because of the spatial separation and the more dominant noise levels from construction of the main plant, which is between the nearest residence and Blount Island.

Question 12: The projected noise levels as shown in Figure 4.1-6 do not agree with noise levels already measured at one mile from the site. Please explain.

Response: The projected ambient levels shown in Figure 4.1-6 show only the contribution of plant construction activities to the noise level at one mile. Existing ambient noise levels are not included. As a rule-of-thumb, if the existing level is equal to the projected plant contribution, the combined level will be three decibels higher than the existing ambient. If the difference in decibel levels is about two decibels, add two decibels to the higher level to obtain the combined noise level. If the difference is six decibels, add one decibel to the higher level, and if the difference is greater than ten decibels, the lower level can be ignored entirely. Thus, as indicated in the text of the SCA/EID, the maximum noise level predicted is 57dB(A) which is a result of combining the existing noise level and the construction impact.

Cooling Tower Drift

Question 1: JEA addresses biological effects of salt deposition, but does not reflect impact as a result of corrosion. JEA should comment on this aspect.

Response: A number of corrosion tests have been performed on a variety of materials. Those materials of particular interest in the area of the proposed plant site include steel, aluminum and aluminum alloys, tin, and concrete.

Cast carbon steels tested at a marine location and an industrial location exhibited a corrosion rate of 0.5 mils per year (mpy) at both locations. (One mil is equivalent to one thousandth of an inch.) Steels alloyed with nickel, chromium, or copper will corrode at a lower rate. The maximum annual average salt deposition rate from the cooling towers outside the site boundary is predicted to be 0.5 mg/m²/hr in the site vicinity. Combining this with a reported natural deposition rate of 0.42 mg/m² yields a total deposition rate of 0.92 mg/m²/hr. This rate is 18.4 percent of that recorded at the shoreline. Thus, the corrosion rate of steel exposed to the 0.92 mg/m²/hr should be less than the 0.5 mpy observed at the shoreline where a deposition rate approaching 5 mg/m²/hr was recorded. The exact rate is difficult to predict since it is affected by local weather conditions, proximity of industry, and other factors. The corrosion rate of steel in the vicinity of the proposed site should not increase by more than 0.1 or 0.2 mpy as a result of any increase in salt deposition (0.2-0.5 mg/m²/hr) due to cooling tower operation.

Corrosion tests on various aluminum alloys have shown that the rate of weathering for both wrought and cast aluminum alloys decreases drastically with time. After one or two years, the maximum rate of attack does not exceed 0.11 mpy for the most severe seacoast conditions and may approach 0.03 mpy for less severe atmospheres. The average corrosion rate does not exceed 0.04 mpy for atmospheric exposure. The addition of 0.5 mg/m²hr or less of salt to the atmosphere would have a negligible effect on the existing aluminum corrosion rate in the vicinity of the proposed plant.

The corrosion rate of tin, based on ten years of exposure tests conducted by ASTM, ranges from 0.02 mpy in rural atmospheres to 0.09 mpy in marine atmospheres. The addition of 0.5 mg/m²/hr to the background of 0.42 mg/m²/hr yields a total rate which is only 18.4 percent of the deposition recorded at the seacoast and would therefore not significantly affect the atmospheric corrosion rate of tin in the vicinity of the site. What are commonly referred to as tin roofs are often galvanized steel. Zinc coatings are unaffected by changes in salt content, corroding at the rate of 0.1-0.3 mpy in most atmospheres.

Concrete has widespread use in marine environments, including seawater immersion. This widespread use attests to its excellent resistance to attack by aqueous chlorides (salt). Due to the resistant properties of concrete, the low concentration of salt deposited as a result of cooling tower drift would not pose a problem.

Question 2: JEA should comment on the deposition of other material, other than salt, as a result of the emissions from the cooling tower.

Response: The salt deposition values presented include a number of elements other than the major components, chlorides and sulfates. The salt concentration value used in the dispersion modeling was the total dissolved solids (TDS) as determined by the water quality analyses of the recirculating cooling water source. A water quality analysis was conducted for a number of the elements which comprise the TDS. The selection of elements for analysis was based on engineering, environmental, and human health factors. The predicted deposition of these elements, keeping in mind that they are a fraction of the salt deposition numbers, can be determined by computing a ratio of the elemental concentration in the recirculating water to the TDS concentration used in the dispersion modeling. The element deposition rate is the product of this ratio and the salt deposition isopleths. A list of the elements analyzed for, the corresponding ratios, and the annual deposition values are presented in Table 1.

The background soil concentrations, estimated soil concentration increase, and percent increase are presented in Table 2. It should be noted that the annual deposition values presented in Table 2 are a fraction of the salt deposition numbers and should not be added to the salt deposition numbers presented in the SCA/EID.

None of the elements analyzed for would be deposited in an amount greater than $1 \text{ mg/m}^2/\text{yr}$, with the exception of bromine. The percent increase of bromine over the 40-year plant life, assuming all the bromine deposited remains in the top 25 cm of the soil, is only 3 percent at the $0.2 \text{ mg/m}^2/\text{hr}$ isopleth and 7.5 percent at the $0.5 \text{ mg/m}^2/\text{hr}$ isopleth. In the existing saline environment, these predicted percent increases are considered to be insignificant. Given the small percent increases from the other trace elements analyzed, no significant impact from trace elements in cooling tower drift is anticipated.

Question 3: What impact from the cooling towers emissions and the project site itself, can be expected on the new cars stored at Blount Island?

Response: Cars are typically stored for five to eight days at Blount Island, with five being the typical time, before being shipped to dealers or distributors. Based on the response to Question 1 above (Cooling Tower Emissions) no adverse effects are anticipated on the cars stored at the Blount Island facility due to the low predicted salt deposition rates, the short storage period, and the rust preventative techniques applied to the cars.

Sulfur oxides and particulate matter are two of the projected emissions from the proposed plant with the potential for damaging the new car finishes. Sulfur oxides accelerate the corrosion of metals and the erosion of building stone, while airborne particles soil fibers and structures. Corrosion products were observed on untreated iron surfaces after exposure to $260 \text{ ug/m}^3 \text{ SO}_2$ for six to eight weeks, while corrosion was evident after a few hours exposure to $4 \times 10^5 \text{ ug/m}^3 \text{ SO}_2$. For particulates, a concentration of 45 ug/m^3 is thought to be that concentration below which soiling would not increase the cost of cleaning activities.

The predicted SO_2 concentration for the new car storage area on Blount Island ranges from $13\text{-}15 \text{ ug/m}^3$ as an annual average. Maximum predicted SO_2 concentration for all sources including the proposed plant is $600\text{-}900 \text{ ug/m}^3$ for a 3-hour average. The total suspended particulate (TSP) concentration predicted to occur in the vicinity of the Blount Island car storage area is 31 ug/m^3 on an annual average.

TABLE 1
 POTENTIAL DEPOSITION OF TRACE ELEMENTS
 FROM COOLING TOWER DRIFT

Element	Maximum Concentration After 1.5 Cycles of Concentration ^a (mg/l)	Element to Total Dissolved Solids Ratio	Annual Deposition (mg/m ² /yr) ^b	
			0.2 mg/m ² /hr Salt Deposition Isopleth	0.5 mg/m ² /hr Salt Deposition Isopleth
Arsenic	0.0015	3.1 x 10 ⁻⁸	5.4 x 10 ⁻⁵	1.3 x 10 ⁻⁴
Beryllium	0.00029	5.9 x 10 ⁻⁹	1.0 x 10 ⁻⁵	2.5 x 10 ⁻⁵
Boron	6.9	1.4 x 10 ⁻⁴	2.4 x 10 ⁻¹	6.1 x 10 ⁻¹
Bromine	78	1.6 x 10 ⁻³	2.8	7.0
Cadmium	0.0033	6.8 x 10 ⁻⁸	1.2 x 10 ⁻⁴	2.9 x 10 ⁻⁴
Chromium	0.0075	1.5 x 10 ⁻⁷	2.6 x 10 ⁻⁴	6.5 x 10 ⁻⁴
Copper	0.36	7.4 x 10 ⁻⁶	1.3 x 10 ⁻²	3.2 x 10 ⁻²
Fluorine	0.84	1.7 x 10 ⁻⁵	2.9 x 10 ⁻²	7.4 x 10 ⁻²
Lead	0.14	2.9 x 10 ⁻⁶	5.1 x 10 ⁻³	1.3 x 10 ⁻²
Manganese	0.132	2.7 x 10 ⁻⁶	4.7 x 10 ⁻³	1.2 x 10 ⁻²
Mercury	0.009	1.8 x 10 ⁻⁷	3.1 x 10 ⁻⁴	7.8 x 10 ⁻⁴
Nickel	0.18	3.7 x 10 ⁻⁶	6.5 x 10 ⁻³	1.6 x 10 ⁻²
Selenium	0.0015	3.1 x 10 ⁻⁸	5.4 x 10 ⁻⁵	1.3 x 10 ⁻⁴
Tin	1.4	2.8 x 10 ⁻⁵	4.9 x 10 ⁻²	1.2 x 10 ⁻¹
Zinc	0.29	5.9 x 10 ⁻⁶	1.0 x 10 ⁻²	2.6 x 10 ⁻²

^a EnviroSphere Water Quality Analysis

^b Refer to Figures 5.4-9 Through 5.4-12

TABLE 2
ESTIMATED TRACE ELEMENT CONCENTRATIONS IN THE SOIL
FROM COOLING TOWER DRIFT

Element	Average Background Soil Concentration ^a (ppm)	Percent Increase Due To Emissions From The Proposed Cooling Towers ^e					
		Estimated Soil Conc. Increase ^d (mg/kg/yr)		Per Annum		40 Year Plant Life	
		0.2 mg/m ² /hr Salt Deposition Isopleth	0.5 mg/m ² /hr Salt Deposition Isopleth	0.2 mg/m ² /hr Salt Deposition Isopleth	0.5 mg/m ² /hr Salt Deposition Isopleth	0.2 mg/m ² /hr Salt Deposition Isopleth	0.5 mg/m ² /hr Salt Deposition Isopleth
Arsenic	6	1.44 x 10 ⁻⁷	3.46 x 10 ⁻⁷	2.4 x 10 ⁻⁶	5.76 x 10 ⁻⁶	9.6 x 10 ⁻⁵	2.3 x 10 ⁻⁴
Beryllium	6	2.67 x 10 ⁻⁸	6.67 x 10 ⁻⁸	4.4 x 10 ⁻⁷	1.11 x 10 ⁻⁶	1.78 x 10 ⁻⁵	4.4 x 10 ⁻⁵
Boron	10	6.4 x 10 ⁻⁴	1.62 x 10 ⁻³	6.4 x 10 ⁻³	1.62 x 10 ⁻²	2.5 x 10 ⁻¹	6.5 x 10 ⁻¹
Bromine	10 ^b	7.47 x 10 ⁻³	1.87 x 10 ⁻²	7.46 x 10 ⁻²	1.86 x 10 ⁻¹	2.98	7.5
Cadmium	0.06	3.2 x 10 ⁻⁷	7.73 x 10 ⁻⁷	5.3 x 10 ⁻⁴	1.28 x 10 ⁻³	2.13 x 10 ⁻²	5.15 x 10 ⁻²
Chromium	100	6.93 x 10 ⁻⁷	1.73 x 10 ⁻⁶	6.9 x 10 ⁻⁷	1.73 x 10 ⁻⁶	2.77 x 10 ⁻⁵	6.9 x 10 ⁻⁵
Copper	20	3.46 x 10 ⁻⁵	8.53 x 10 ⁻⁵	1.73 x 10 ⁻⁴	4.26 x 10 ⁻⁴	6.9 x 10 ⁻³	1.70 x 10 ⁻²
Fluorine	200	7.73 x 10 ⁻⁵	1.97 x 10 ⁻⁴	3.86 x 10 ⁻⁵	9.85 x 10 ⁻⁵	1.5 x 10 ⁻³	3.93 x 10 ⁻³
Lead	10	1.36 x 10 ⁻⁵	3.44 x 10 ⁻⁵	1.35 x 10 ⁻⁴	3.43 x 10 ⁻⁴	5.44 x 10 ⁻³	1.37 x 10 ⁻²
Manganese	850	1.25 x 10 ⁻⁵	3.2 x 10 ⁻⁵	1.47 x 10 ⁻⁶	3.76 x 10 ⁻⁶	5.88 x 10 ⁻⁵	1.5 x 10 ⁻⁴
Mercury	0.1	8.26 x 10 ⁻⁷	2.08 x 10 ⁻⁶	8.25 x 10 ⁻⁴	2.08 x 10 ⁻³	3.3 x 10 ⁻²	8.3 x 10 ⁻²
Nickel	40	1.73 x 10 ⁻⁵	4.26 x 10 ⁻⁵	4.32 x 10 ⁻⁵	1.06 x 10 ⁻⁴	1.72 x 10 ⁻³	4.25 x 10 ⁻³
Selenium	0.5	1.44 x 10 ⁻⁷	3.46 x 10 ⁻⁷	2.88 x 10 ⁻⁵	6.92 x 10 ⁻⁵	1.15 x 10 ⁻³	2.76 x 10 ⁻³
Tin	200 ^c	1.31 x 10 ⁻⁴	3.2 x 10 ⁻⁴	6.5 x 10 ⁻⁵	1.59 x 10 ⁻⁴	2.6 x 10 ⁻³	6.4 x 10 ⁻³
Zinc	50	2.67 x 10 ⁻⁵	6.9 x 10 ⁻⁵	5.3 x 10 ⁻⁵	1.38 x 10 ⁻⁴	2.14 x 10 ⁻³	5.5 x 10 ⁻³

^a U.S. Fish and Wildlife Service, 1978

^b Horton et al., 1977

^c Environmental Research and Technology, 1978

^d Refer to Appendix A - Table A-30 for soil concentration increase formula

^e Refer to Table 5.3-18

Since the predicted long-term SO₂ concentration (13-15 ug/m³) is below that where corrosion products were observed (260 ug/m³) and the maximum short-term concentration of 600-900 ug/m³ is below that where corrosion products were observed (4 x 10⁵ ug/m³), and considering the short time period that the cars would be exposed to these low SO₂ concentrations, no adverse effects to the car finishes due to SO₂ are anticipated.

The predicted TSP concentration (31 ug/m³) is below the concentration reported as the threshold above which additional cleaning costs due to soiling would be incurred. However, the highest 24-hour TSP concentration observed during the on-site monitoring (61 ug/m³ exceeds this 45 ug/m³ threshold), which suggests that a soiling problem may exist. However, no problems with car finishes were reported by representatives of the companies operating the car unloading facilities at Blount Island. Thus, it is not anticipated that any adverse soiling effects would occur due to the small increment to be added by the proposed project.

Coal Unloading Facility Blount Island

Question 1: Does JEA recognize the potential problems from locating their coal unloading facility immediately next to a new car storage facility?

Response: The potential for damage to new car finishes exists at the Blount Island coal unloading facility as it would be at or near any industrialized area.

It has been reported that iron particles from industrial operations resulted in the staining and pitting of auto finishes. Cars parked near brick buildings being demolished have been damaged by alkali mortar dust during humid weather. A sticky material emitted from oil-fired power plants, termed acid smut, has also been linked to the damage of automotive finishes.

The only atmospheric emission from the coal unloading facility with the potential to damage automotive finishes is the coal dust. Without knowing the chemical composition of the coal, it is difficult to predict what the actual effect of coal dust will be on automotive finishes. However, there have been no reports of coal dust affecting new car finishes from the auto manufacturing representatives questioned.

Coal Blending

Question 1: Will coal blending be utilized at this project to reduce potential SO₂ emissions? If so, what type of blending system will be used?

Response: Coal blending has been considered for the SJRPP project. Plans are now being made to incorporate the capability to readily retrofit coal blending at the Blount Island coal unloading facility for water-borne transport. Retrofit of coal blending capability would be implemented should it be shown to be cost-effective in the future. Currently, the capability of the boiler and AQCS to use a wide range of coal from the eastern U.S. makes blending unnecessary, and current economics do not justify its incorporation.

Plans are currently being made to provide the capability to retrofit a blending system capability based on a bucket-wheel reclaimer and a slewing stacker, mounted on common rail system.

Coal Piles

Question 1: What means will be used, or available to prevent or fight fires within the coal pile?

Response: Fires within the coal may occur due to spontaneous combustion of loose coal left undisturbed for extended periods. The coal stored in the active storage system will be cycled in and out over a relatively short period (one to three days) and should not present a serious problem. The coal in inactive storage will be compacted carefully to control spontaneous combustion. Recommendations in the Coal Handling System Study call for two bulldozers and a front-end loader to support coal operations. Should a coal fire occur, this equipment may be used to dig it out and extinguish it. Once the burning coal is dug out and the fire extinguished, the smoldering coals may be quenched using the fireplugs and hoses provided with Fire Protection System. Fireplugs are located every 500 ft. around the periphery of the coal storage area.

FGD

Questions 1 &

2: Does JEA intend to effect HCL removal ahead of the SO₂ removal system in order to minimize chemical consumption and purge requirements?

Has JEA defined the parameters of the purge system necessary to prevent the accumulation of chlorides and magnesium in the circulating solution?

Response:

The conceptual arrangement of the FGDS uses a purge flow of water to maintain the chloride level below 3,500 ppm. This purge flow will also produce low magnesium concentrations. Use of a separate chloride stripper ahead of the FGDS was considered. The design of such a stripper leads to a situation where extremely corrosive conditions (pH less than or equal to 1.0, chloride in excess of 100,000 ppm) would exist. To date, we know of no FGDS chloride stripper operating under such severe conditions. We feel that the chloride stripper would produce a considerably less reliable system than our current FGDS conceptual arrangement.

RESPONSES TO BESD INTERROGATORIES (MARCH 25, 1981)
TRANSMITTED THROUGH FDER (MARCH 30, 1981)

Question A: ESP - which of the following instruments will be provided with the ESP?

1. Primary voltage
2. Primary current
3. Secondary current
4. Secondary voltage
5. Gas temperature (outlet)
6. Fan motor current
7. Fan inlet and outlet static pressure taps
8. Hopper level indicator
9. Rapper activation indicator board

What is the size and slope of the hopper?

What type discharge equipment is on the hopper?

What provisions for gas distribution through the ESP has been made?

What explosion and fire protection in the ESP is provided?

What type of rappers will be used?

What degree of accessibility to the ESP is provided? i.e., number, size and location of hatches?

What type of hatch gaskets are proposed?

What construction materials will be used for the ESP?

What type of electrodes are proposed?

What will be the plate spacing?

Show assumptions and calculations used in sizing the ESP, including particle resistivity, particle size distribution, etc.

Response: The control system for the electrostatic precipitator utilizes a microprocessor to monitor primary voltage and current, secondary voltage and current, hopper level, the status of the rapping system and the flue gas temperature in the precipitator. Additional instrumentation such as induced draft fan motor current, and inlet and outlet static pressures will be monitored by other plant systems.

The hoppers are sized for a 12 hour storage capacity when firing coal with maximum ash and minimum heating value, at full load. The hoppers will have a minimum of a 60 degree slope. Fly ash removal from the hoppers will be effected using a pressurized pneumatic conveying system which will be controlled by a microprocessor. This system would be capable of removing fly ash on an hourly basis from each hopper.

To assure that proper flue gas distribution to the precipitator is established, the precipitator manufacturer will conduct a model study to determine the type, size and location of such distribution devices as required. In addition, the manufacturer will conduct air flow tests on the installed precipitator to assure that proper gas distribution can be achieved. Furthermore, emergency flue gas balancing dampers are provided to correct gross deviations in gas flow distribution and would be employed until such time that the manufacturer can make corrections to gas distribution devices.

A fire protection system is provided for the precipitator control room and electrical power supplies.

Precipitator rappers can either be the mechanical drive type or the electromagnetic impulse type depending upon the precipitator manufacturer selected.

Access to the precipitator and associated ductwork will be provided to facilitate inspection and maintenance. Since the location, type and size of the access hatches is dependent upon a particular manufacturer's design, the exact nature of these facilities cannot be determined until a manufacturer is selected. However, design specifications do require the use of four precipitator casings for each steam generator. Further, each casing will be provided with man-safe isolation devices to facilitate on-line maintenance.

The precipitator casing and hoppers along with associated ductwork will be constructed of ASTM A-242 material. Collecting and discharge electrodes will be constructed of mild steel.

The centerline to centerline distance between electrodes will be 12 inches on a nominal basis.

Rigid type discharge electrodes will be the only type considered for this project.

Due to the broad range of fuels to be fired and the lack of coal specific data, a conservative sizing approach based on field experience of various precipitator manufacturers was used to develop a minimum precipitator size based on 0.5 percent sulfur content coal. Further, the selected manufacturer will have to demonstrate using the EPA precipitator computer program, that the sizing is sufficient. Further, a design margin of 20 percent will be added to the base precipitator size.

Question B: FGD Scrubber - which of the following instruments are provided on the FGD, and where will they be located?

1. Static pressure taps/meters
2. Gas temperature
3. pH of absorber
4. Liquid pressure to nozzle header
5. Fan motor current
6. Liquid temperature
7. Liquid flow rates
8. Other

What is the schematic flow configuration of the FGD?
What construction materials are to be used?
What is the recycle tank capacity?
What is the size, type and location of nozzles?
What type mist eliminator is proposed?
What provisions are made for accessibility to the FGD System?
What method is proposed for solids removal?
Will a thickener tank be employed?
If a thickener is to be used, what are the dimensions and the detention time?

Response: The conceptual flow diagrams (SK-ACE-FGD-3, 4, 5 and 6) are attached hereto. These diagrams also show all required process control instrumentation labeled (AECNTRL). The nature of these diagrams is such that minor modifications will be required to reflect the experience and technology of the selected FGDS manufacturer.

FGDS materials of construction will consist of high nickel alloys such as 904L alloy, Hastelloy G and C-276 and Inconel 625. Specific material selection will be dependent upon the type of service, pH and chloride concentrations.

The absorber recycle tank will have a minimum retention time of ten minutes to allow for chemical reactions to equilibrate.

FGDS nozzles will be constructed of silicon carbide and located as appropriate to provide for uniform flow patterns, complete and intimate mixing and contact between the flue gas and slurry droplets.

Mist eliminators will be of the open, multipass type located horizontally. Accessibility to the FGDS will be provided via access hatches with the use of man-safe isolation devices to permit on-line maintenance. A spare module will be provided to permit full load operation while maintaining any module.

Calcium sulfate solids will be removed from the FGDS through the use of hydrocyclones and vacuum filters to produce a stable material in cake form. It is not planned to use thickeners.

Question C: Fabric Filters for Coal Handling System

What are the sizes and configurations, including gas flows, A/C ratios, number of bags, bag materials to be utilized?
What type of bag cleaning will be used?
Which of the following instruments will be used?

1. Baghouse inlet and outlet static pressure taps/meters
2. Fan inlet and outlet static pressure taps/meters
3. Temperature
4. Fan motor current

What is the size and shape of hoppers?
What type discharge equipment will be used on the hoppers?
What is the ultimate means of dust disposal?
What fire and explosion protection is provided?
What construction materials will be used?
What is the number, size and shape of blast plates?
What type of bag hanger and thimble arrangements are proposed?

Response: Dust collection shall be provided for the following facilities (see attached flow diagrams, M-022260-01/02):

COLLECTOR

- | | |
|------|---|
| I. | a - Plant coal storage silos |
| | b - Belt conveyors C-7/C-9 transfer |
| | c - Belt conveyors C-8/C-10 transfer |
| II. | d - Crusher CR-A to Belt Conveyor C-7 transfer including crusher discharge |
| | e - Crusher CR-B to Belt Conveyor C-8 transfer including crusher discharge |
| III. | f - Surge Bins (for ventilation) |
| | g - Belt Conveyors C-2 and C-4 Coal Handling Building discharges and C-4 loading chutes and skirt |
| | h - Belt Conveyor C-3 discharge chute |
| IV. | i - Belt Conveyor C-1/C-2 transfer |
| V. | j - Belt Feeder F-CD to Belt Conveyor C-1 transfer |
| | k - Bin CD Hoppers to Belt Feeder F-CD |
| VI. | l - Bin LD hoppers to belt Feeder F-LD |
| | m - Belt Feeder F-LD to Belt Conveyor L-1 |

- VII. n - Belt Conveyor L-1/L-2 transfer
- VIII. o - Main Coal Handling Systems control and electrical equipment room HVAC unit - separate collector for outdoor air intake

* All points under a given Roman Numeral are collected by that collector.

The requested information for each installation if available, is given below according to the respective collector for the above designated facilities.

<u>Item</u>	<u>Resolution</u>
1. Bag House Size	Not available - to be determined by Vendor per spec. 20-80-JEA criteria
2. Total Air Flow	50,800 CFM for Collector 1 Resolution for remaining collectors same as for Item No. 1
3. Air to Cloth Ratio	G to 1
4. No. of Bags	Per Item 1 resolution
5. Bag Material	16 oz. polypropylene or Dacron, fire resistant, grounded
6. Bag Cleaning Method	Reverse air pulse
7. Instrumentation	Dust level switch with remote indication and alarm Differential pressure across the collecto-gage and switch for alarm
8. Hopper Size	10 hours dust holding capacity, 60° slopes, Item 1 resolution applicable
9. Hopper Shape	Conical or Pyramid per Item 1 resolution

Discharge Equipment	Rotary Discharge valve with antispark end seals, cast iron casing. Totally enclosed dust and ignition proof motor. Valve designed for 150% expected maximum load
Ultimate Disposal	Discharged material is pneumatically conveyed to coal silos from Collector 1 Discharged material is gravity chuted back into process from remaining collectors. The process fires the coal dust into the boilers. The lime dust is discharged into the FGDS solution.
10. Protection	
Fire	Automatic shutdown when process fire protection system is activated, except for underground service where the collector is bypassed, but the fans kept running
Explosion	Blast doors on housings. Electrical equipment designed for NFPA Std. 70, Class II, Div. 1, Group F Application
11. Construction Material	Housings, Hoppers, and tube sheets are of 10 gage ASTM A570 material, suitably reinforced to assure parallel bag alignment and (-) 20 in. hg. internal pressure
12. Blast Gates	1 sq.ft. of gate per 30 to 40 ft ³ of collector volume
13. Bag Hanger and Thimble Arrangement	Item No. 1 Resolution is applicable

Question D: Continuous Emission Monitors

Regarding the Ebasco memo of October 27, 1980: Is this the total number of Continuous Monitoring Devices (CMD) or the monitors per generating unit?

What is the degree of accessibility of each CMD location for servicing and calibration, inspection, and provision of data acquisition in case of instrument outage?

Response:

The information in Ebasco memo dated October 27, 1980, (JEA-IC-147) has been revised. The following are the number of CMDs which will now be provided for each generating unit. The locations and services of the CMDs are given in Figure 1, attached.

1. Two (2) combination NO_x and CO_2 control monitors will be located in the ducts between the air heaters and each pair of precipitators (one in each duct). Performance test ports will be provided for manual measurement of NO_x in each duct between the precipitator and air heater outlet.
2. Eight control transmissometers will be located in the ducts between the precipitators and the induced draft fans. Each of the four precipitator outlet ducts will have two transmissometers. Both transmissometers will be used in conjunction with the precipitator control system. One will be used for backup, but they both will be operating continuously. The Operator selectable signal of each pair of transmissometers will be used in the precipitator control system to optimize control of the precipitator and to provide an alarm to the AQCS Control Room Operator.
3. One EPA approved transmissometer will be located in the duct between the induced draft fan discharge header and the scrubber system inlet header. This transmissometer will be used to monitor opacity for EPA reporting and to provide an alarm to the AQCS Control Room Operator.
4. One combination SO_2/CO_2 EPA approved analyzer and two (2) SO_2 control analyzers will be located in the duct between the induced draft fan discharge header and the scrubber system inlet header.

The combination SO₂/CO₂ analyzer will be used for EPA reporting and to provide an alarm to the AQCS Control Room Operator. The two SO₂ analyzers will be used for scrubber control. One control analyzer will be used as a backup but both control analyzers will be operating continuously. The Operator selectable signal from the two control analyzers will be used for the following:

- a. Control of the limestone slurry feed.
- b. Calculation of the percentage removal of SO₂.
- c. Calculation of inlet pounds SO₂ /MBtu.

Performance test ports will be provided for manual measurement of SO₂ in the duct between the induced draft fan discharge header and the scrubber system inlet header.

5. Eight SO₂ control analyzers will be located in the absorber tower outlet ducts. Each of the four absorber tower outlet ducts will have two control analyzers; one will be used as backup but both will be operating continuously. The Operator selectable signal from each pair of control analyzers will be used for the following:

- a. Absorber tower diagnostic.
- b. Alarm to AQCS Control Room Operator.
- c. Calculation of the percentage SO₂ removed.
- d. Calculation of outlet pounds SO₂ /MBtu.
- e. Fine tune control on limestone slurry feed.

6. The chimney liner will contain one combination SO₂/NO_x/CO₂ EPA approved monitor. Its signals will be used for EPA reporting and to provide alarms to the AQCS Control Room Operator. A diagram of the chimney cross-section at the measurement point is given in Figure 2, attached.

Performance test ports will be provided in the chimney liner for manual measurement of stack emissions.

The chimney is provided with an inside elevator and platforms for access to the CMDs and the performance test ports. The CMDs and performance test ports located on the flue gas ducts will also be provided with access platforms for servicing and calibration purposes.

In the event of an instrument outage, data may be collected manually through performance test ports which will be located near all EPA monitoring ports. Another alternative which may be used for data acquisition is the microprocessor based control system. On an extraordinary basis, the control system may be used as a backup to gather, store and print emissions data. The control system will be designed with the ability to calculate this data using various correlation factors.

Question E: NO_x and CO Emissions

What are the specific contract arrangements with the boiler manufacturer to guarantee that the coal fired units and the auxilliary boiler will meet NO_x and CO emission limits? More specifically, what contractual assurances are there that a repeat of the Northside Unit #3 problems with NO_x and subsequent extensive and expensive boiler reconfiguration will be avoided?

Resonse: Coal-Fired Boilers

Foster Wheeler has guaranteed that NO_x emissions will not exceed 0.6 lb/MBtu at economizer outlet when firing performance fuel. The boiler will have special Low NO_x burners. The only other contractual obligations are expressed in paragraphs 3.1.2.4 and 3.1.2.5 of the Steam Generator contract which is attached.

Auxiliary Boilers

It is our understanding that boilers with maximum inputs of less than 250 MBtu/HR do not have to comply with the NO_x limits of the Clean Air Act. However, the boiler manufacturers will be encouraged to guarantee maximum NO_x emissions of .3 lb/MKB and maximum CO emissions of .05 lbs/MBtu through the specifications in the Bid Package. We understand that these guarantees were recommended by you.

Comparison of this case to Northside No. 3 is not valid because the boiler configuration, boiler manufacturers, and boiler fuel are different.

FDER (3/30) Question B

FDER (3/30) Question D

6'-0" WIDE X 8'-0" ±
EXTERIOR BALCONY
(TYP)

FULL PLATF
@ EL 439.00

ACCESS DOOR
(TYP)

MONITORING
PORT
(2 REQD/LINER)
@ EL 443.50
180° APART (TYP)

STACK

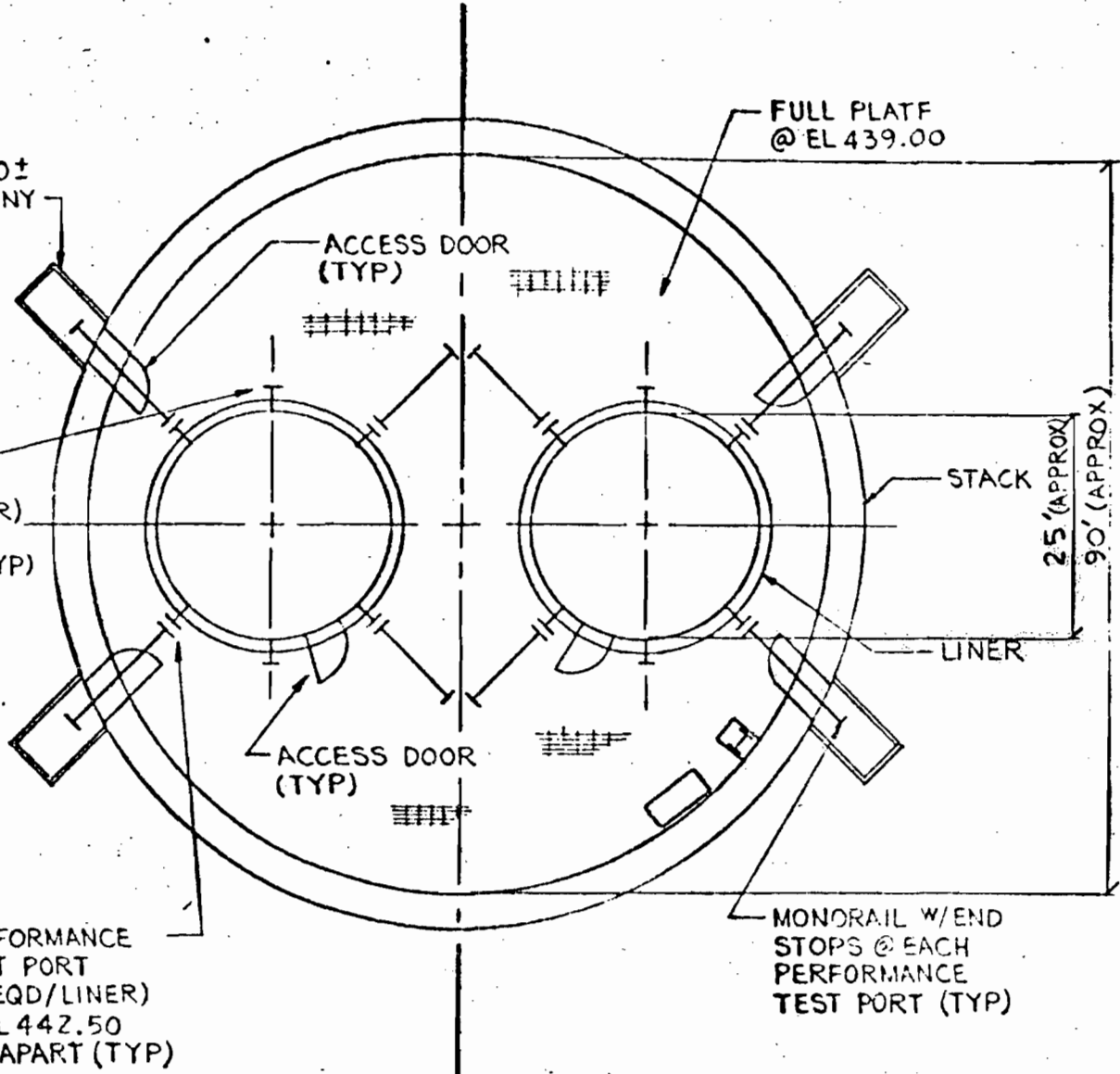
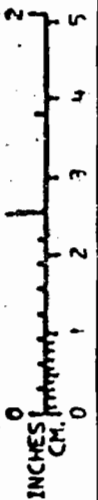
25' (APPROX)
90' (APPROX)

LINER

ACCESS DOOR
(TYP)

PERFORMANCE
TEST PORT
(4 REQD/LINER)
@ EL 442.50
90° APART (TYP)

MONORAIL W/END
STOPS @ EACH
PERFORMANCE
TEST PORT (TYP)



EBASCO SERVICES INCORPORATED		JACKSONVILLE ELECTRIC AUTHORITY		Question D FIGURE 2
DIV. I & C DR. <i>sk</i>		600MW COAL FIRE PLANT		
DATE _____ CH _____		EMISSION MONITORING AND TESTING EQUIPMENT LOCATIONS		
SCALE _____		APPROVED _____		

FDER (3/30) Question E

DEA 3/30
Question E
Ebasco Specification 57-78-JEA
Fossil Steam Generating Unit

Project Identification
No. JEA 3332-001400

Revision No. 1

- b - Expected sound pressure level measured under "free field" conditions at a distance of 5 ft. from the outline of equipment shown in decibels at the octave band center frequencies ranging from 31.5 to 16,000 Hz, either eight or ten bands, or:
- c - Calculated sound power level of the equipment shown in decibels at eight or ten octave band center frequencies ranging from 31.5 to 16,000 Hz and referred to a base of 10^{-12} watts.

3.1.2.1.2 Sound level data shall be provided at maximum capacity rating and at start-up operating conditions of the steam generating unit(s) and all Seller furnished auxiliary equipment.

3.1.2.1.3 In the event that the normal sound level of equipment exceeds the allowable level, at a distance of 5 ft, acoustical treatment features, subject to Purchaser review and acceptance, shall be utilized to achieve the sound level limit specified.

3.1.2.2 No asbestos or asbestos bearing material shall be used as part of the Seller furnished equipment covered by this Specification.

3.1.2.3 No PCB compounds shall be used as part of the Seller furnished equipment covered by this Specification.

3.1.2.4 The equipment furnished under this specification shall, under all normal operating conditions, including start-up, shutdown, load changes and soot blower operation, comply with the New Source Performance Standards for nitrogen oxides as adopted by the United States Environmental Protection Agency in 40CFR Part 60, Subpart Da, Paragraph 60.44a and published in the Federal Register, Volume 44, Number 113, on June 11, 1979. Further, performance testing shall be in accordance with Paragraph 7.1.3.7.

3.1.2.5 Emissions of nitrogen oxides as well as emissions of all other air pollutants regulated under the Clean Air Act (such as, but not limited to, hydrocarbons and carbon monoxide) shall be limited using "Best Available Control Technology" of Contractor's design and manufacture for items of equipment within Contractor's scope.

3.1.3 Guaranteed Performance

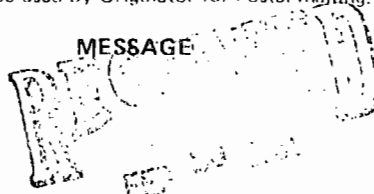
3.1.3.1 Guarantee shall be as stated in Bid Item 3: Technical Data, Category 2.0 of the Technical Proposal Form.

3.1.4 Seismic Design Requirements

2/20/81

SPEED LETTER

INSTRUCTIONS: Originator - Send White and Yellow copies intact to Addressee. Retain Pink copy and destroy when White copy is returned.
Addressee - Prepare reply in duplicate, retain Yellow copy for file, return White copy to Originator
NOTE: Window envelope (E21201 or E21202) may be used by Originator for Postal mailing.



TO Buck Owen

FDEP

Tallahassee, Florida

FROM Doug Fulle

ENVIRONMENTAL

Norcross, Georgia

DIV. ENVIRONMENTAL PERMITTING

SUBJECT

DATE FEBRUARY 18 1981

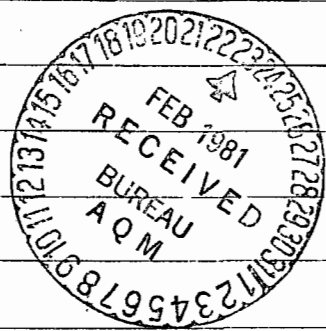
FOR YOUR DISCUSSION WITH DON LUCAS OF THIS DATE, ATTACHED PLEASE FIND ONE COPY OF THE PRELIMINARY DETERMINATION REGARDING IEA'S PSD APPLICATION WHICH WAS TRANSMITTED FROM EPA ON JANUARY 14, 1981.

cc D. Lucas

SIGNED Doug Fulle

REPLY

DATE _____ 19 ____



SIGNED _____



UNITED STATES ENVIRONMENTAL PROTECTION AGENCY

REGION IV

345 COURTLAND STREET
ATLANTA, GEORGIA 30308

JUL 16 1980

REF: 4AH-AF

Mr. Richard Breitmoser
Jacksonville Electric Authority
P. O. Box 53015
233 W. Duval Street
Jacksonville, Florida 32201

RECEIVED

JUL 21 1980

DEPT. OF
ENVIRONMENTAL REGULATION

Re: PSD Permit Application
PSD-FL-010

Dear Mr. Breitmoser:

EPA received on May 28, 1980 your latest application submittal for construction of two power generating units (600 MW) near the city of Jacksonville, Florida. Review of this application under the Federal Prevention of Significant Deterioration (PSD) Regulations (40 CFR 52.21) and the partial stay of these regulations published February 5, 1980 (45FR7800) has shown it to be complete for the purposes of determining increment rights. However, certain additional technical information is required to allow review of the application to continue.

Please submit information on the following items:

1. Explain the criteria and data sources used in selection of increment consuming sources included in your increment analyses. It is not clear that all increment consuming sources have been identified. In general, increment consuming sources are identified as follows:
 - a. The area of impact of the proposed project should be defined and shown on maps (circular area with radius equal to furthest distance at which proposed source has a significant impact).
 - b. An inventory of all major sources constructed since January 6, 1975 within the impact area of the proposed project, and all major sources within 50 km which could significantly impact the proposed source's impact area should be established.
 - c. An inventory of all minor sources constructed since August 7, 1977 within the impact area of the proposed project should be established.

- d. These sources should be considered in the Class II increment analysis. Although not all increment consuming sources need to be modeled, all should be considered for significance. Any arbitrary determination of insignificance should be justified.
- e. The Class I area increment analysis must consider all increment consuming sources within 100 km as your analysis has indicated. Minor sources beyond 50 km need not be modeled.

Two sources have been identified which may consume increment and effect the results of your Class I and Class II increment analyses. These areas are as follows:

Union Camp	Boiler (77 MM Btu/hr)	FDER Permit # AC 16-11888
ITT Rayonier	Sulfite Recovery Boiler	FDER permit # AC 45-2601

In addition, the SO₂ increment consuming emission rates for Container Corporation facilities are as follows:

Boiler 4 & 5 50.8 g/s Recovery Boiler 35.3 g/s

Reevaluating previous increment consumption may require additional increment analysis.

2. Additional air quality analysis is required to demonstrate protection of the NAAQS. The "background" concentrations developed in your application through analysis of 95th percentile concentrations at monitors not located near major sources is unacceptable. Given the large number of sources in the Jacksonville urban area, the quantity of existing monitoring data and the small number of sources outside the Jacksonville urban area, the most appropriate analysis technique likely is to establish urban "background" from highest or highest, second highest monitoring data and model outlying sources along with the proposed new source to estimate maximum interaction impacts.
3. Copies of input and output to pertinent computer runs.
4. The technical basis for the conclusion that CO emissions impacts are insignificant (i.e. through comparison with TSP modeling results from the boilers considering a ratio of CO to TSP emission rates or by what other means).

5. Did the 3-hour and 24-hour maximums and highest, second highest concentration during the 5 years of meteorological data screened by CRSTER (multisource) occur in the "worst" year selected for use in the remaining analysis?
6. Parameters used to calculate HC emissions from storage tanks, which serve as the basis for your assumption of negligible source emissions. Example parameters are tank capacity, roof type, number of turnovers expected, fuel vapor pressure, type of control technology, etc.
7. Design parameters proposed as BACT for NO_x and CO from the main boilers, and SO₂, CO, TSP and NO_x from the auxiliary boiler.
8. The basis for compliance with minimum GEP stack height.

EPA met with your consultant, Environsphere, on July 9, 1980 and they submitted the information requested on items 1, 3, 4, 5, 6, 8 and submitted partial information on item 7. You are encouraged to submit the remaining information on items 2 and 7 as soon as possible. Please also be aware that the United States Court of Appeals for the DC Circuit has issued a ruling in the case of Alabama Power Co. vs. Douglas M. Costle (78-1006 and consolidated cases) which will have significant impacts on the EPA Prevention of Significant Deterioration (PSD) program. You are advised that review requirements of your application may be subject to reevaluation as a result of the final court decision and its ultimate effect. In addition, EPA has issued a "partial stay" of regulations (published February 5, 1980, 45 FR 7800) affecting applicability of sources proposed for construction prior to affecting applicability of sources proposed for construction prior to promulgation of the final PSD regulations. Your application has been reviewed under the provisions of the Stay and the proposed source remains subject to PSD review.

Sincerely yours,

Tommy A. Gibbs

Tommy A. Gibbs
Chief
Air Facilities Branch

cc: FL DER