

**TAMPA ELECTRIC COMPANY  
F.J. GANNON STATION  
UNIT NUMBER THREE  
TAMPA, FLORIDA**

**REQUEST FOR PERMIT AMENDMENT  
AIR OPERATION PERMIT NO. A029-172179  
TIRE DERIVED FUEL TEST BURN**

**RECEIVED**  
**AUG 23 1996**  
**BUREAU OF  
AIR REGULATION**

**AUGUST 1996**

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# Department of Environmental Protection

## DIVISION OF AIR RESOURCES MANAGEMENT

### APPLICATION FOR AIR PERMIT - LONG FORM

See Instructions for Form No. 62-210.900(1)

#### I. APPLICATION INFORMATION

This section of the Application for Air Permit form identifies the facility and provides general information on the scope and purpose of this application. This section also includes information on the owner or authorized representative of the facility (or the responsible official in the case of a Title V source) and the necessary statements for the applicant and professional engineer, where required, to sign and date for formal submittal of the Application for Air Permit to the Department. If the application form is submitted to the Department using ELSA, this section of the Application for Air Permit must also be submitted in hard-copy.

#### Identification of Facility Addressed in This Application

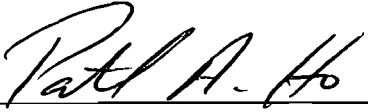
Enter the name of the corporation, business, governmental entity, or individual that has ownership or control of the facility; the facility site name, if any; and the facility's physical location. If known, also enter the facility identification number.

1. Facility Owner/Company Name: <b>Tampa Electric Company</b>	
2. Site Name: <b>F.J. Gannon Station</b>	
3. Facility Identification Number: <span style="float: right;">[ ] Unknown</span> <b>0570040</b>	
4. Facility Location: Street Address or Other Locator: <b>Port Sutton Road</b> City: <b>Tampa</b> County: <b>Hillsborough</b> Zip Code: <b>33619</b>	
5. Relocatable Facility? [ ] Yes [ <b>X</b> ] No	6. Existing Permitted Facility? [ <b>X</b> ] Yes [ ] No

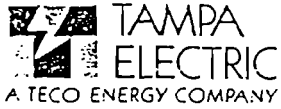
#### Application Processing Information (DEP Use)

1. Date of Receipt of Application:	
2. Permit Number:	
3. PSD Number (if applicable):	
4. Siting Number (if applicable):	

**Owner/Authorized Representative or Responsible Official**

1. Name and Title of Owner/Authorized Representative or Responsible Official: <b>Patrick A. Ho, P.E.</b> <b>Manager, Environmental Planning</b>
2. Owner/Authorized Representative or Responsible Official Mailing Address:  Organization/Firm: <b>Tampa Electric Company</b> Street Address: <b>702 North Franklin Street</b> City: <b>Tampa</b> State: <b>Florida</b> Zip Code: <b>33602</b>
3. Owner/Authorized Representative or Responsible Official Telephone Numbers: Telephone: <b>(813) 228-4844</b> Fax: <b>(813) 228-4881</b>
4. Owner/Authorized Representative or Responsible Official Statement:  <i>I, the undersigned, am the owner or authorized representative* of the non-Title V source addressed in this Application for Air Permit or the responsible official, as defined in Rule 62-210.200, F.A.C., of the Title V source addressed in this application, whichever is applicable. I hereby certify, based on information and belief formed after reasonable inquiry, that the statements made in this application are true, accurate and complete and that, to the best of my knowledge, any estimates of emissions reported in this application are based upon reasonable techniques for calculating emissions. The air pollutant emissions units and air pollution control equipment described in this application will be operated and maintained so as to comply with all applicable standards for control of air pollutant emissions found in the statutes of the State of Florida and rules of the Department of Environmental Protection and revisions thereof. I understand that a permit, if granted by the Department, cannot be transferred without authorization from the Department, and I will promptly notify the Department upon sale or legal transfer of any permitted emissions unit.</i>  <p style="text-align: center;"> _____</p> <p>Signature _____ Date <u>8/8/96</u></p>

\* Attach letter of authorization if not currently on file.



TO WHOM IT MAY CONCERN:

Please be advised that Patrick A. Ho, Manager, Environmental Planning, is the authorized representative of Tampa Electric Company concerning matters with which this permit application deals.

Very truly yours,

William N. Cantrell  
Vice President  
Energy Supply

WNC\gm\ADMIN\AUTH.LTR

**Scope of Application**

This Application for Air Permit addresses the following emissions unit(s) at the facility. An Emissions Unit Information Section (a Section III of the form) must be included for each emissions unit listed.

Emissions Unit ID	Description of Emissions Unit	Permit Type
<b>003</b>	<b>Unit No. 3, Solid Fuel Steam Generator</b>	<b>AC1B</b>

**Purpose of Application and Category**

Check one (except as otherwise indicated):

**Category I: All Air Operation Permit Applications Subject to Processing Under Chapter 62-213, F.A.C.**

This Application for Air Permit is submitted to obtain:

- Initial air operation permit under Chapter 62-213, F.A.C., for an existing facility which is classified as a Title V source.
- Initial air operation permit under Chapter 62-213, F.A.C., for a facility which, upon start up of one or more newly constructed or modified emissions units addressed in this application, would become classified as a Title V source.

Current construction permit number: \_\_\_\_\_

- Air operation permit renewal under Chapter 62-213, F.A.C., for a Title V source.

Operation permit to be renewed: \_\_\_\_\_

- Air operation permit revision for a Title V source to address one or more newly constructed or modified emissions units addressed in this application.

Current construction permit number: \_\_\_\_\_

Operation permit to be revised: \_\_\_\_\_

- Air operation permit revision or administrative correction for a Title V source to address one or more proposed new or modified emissions units and to be processed concurrently with the air construction permit application. Also check Category III.

Operation permit to be revised/corrected: \_\_\_\_\_

- Air operation permit revision for a Title V source for reasons other than construction or modification of an emissions unit. Give reason for the revision; e.g., to comply with a new applicable requirement or to request approval of an "Early Reductions" proposal.

Operation permit to be revised: A029-172179

Reason for revision: Amendment to allow combustion of coal/tire-derived

fuel blend.

**Category II: All Air Operation Permit Applications Subject to Processing Under Rule 62-210.300(2)(b), F.A.C.**

This Application for Air Permit is submitted to obtain:

- Initial air operation permit under Rule 62-210.300(2)(b), F.A.C., for an existing facility seeking classification as a synthetic non-Title V source.

Current operation/construction permit number(s): \_\_\_\_\_

- Renewal air operation permit under Rule 62-210.300(2)(b), F.A.C., for a synthetic non-Title V source.

Operation permit to be renewed: \_\_\_\_\_

- Air operation permit revision for a synthetic non-Title V source. Give reason for revision; e.g., to address one or more newly constructed or modified emissions units.

Operation permit to be revised: \_\_\_\_\_

Reason for revision: \_\_\_\_\_

**Category III: All Air Construction Permit Applications for All Facilities and Emissions Units**

This Application for Air Permit is submitted to obtain:

- Air construction permit to construct or modify one or more emissions units within a facility (including any facility classified as a Title V source).

Current operation permit number(s), if any: \_\_\_\_\_

- Air construction permit to make federally enforceable an assumed restriction on the potential emissions of one or more existing, permitted emissions units.

Current operation permit number(s): \_\_\_\_\_

- Air construction permit for one or more existing, but unpermitted, emissions units.



**Application Processing Fee**

Check one:

Attached - Amount: \$ \_\_\_\_\_

Not Applicable.

**Construction/Modification Information**

1. Description of Proposed Project or Alterations:

Tampa Electric Company (TEC) was authorized by FDEP to conduct a test burn of an 80-percent coal/20-percent tire-derived fuel (TDF) fuel blend for comparison to baseline coal emissions (see Attachment A for a copy of the FDEP test burn letters of authorization). TEC conducted the test burn from February 28 through April 29, 1996.

The results from the test burn enabled TEC to conduct a screening analysis to determine whether future long-term firing of coal/TDF blends would constitute a modification subject to Prevention of Significant Deterioration (PSD) review pursuant to Chapter 62-212.400, Florida Administrative Code (F.A.C.). The analysis of PSD applicability as shown in Attachment B was conducted by comparing the fuel blend test results with the 100-percent coal baseline emission test data in accordance with the FDEP authorization letter dated March 3, 1996. This comparison shows that PSD review is not applicable to this permit amendment request.

Based on the test burn results, TEC requests the F.J. Gannon Station Unit No. 3 permit be modified to allow for the combustion of coal and TDF blends on a permanent basis as an alternative method of operation to the currently approved use of 100-percent coal. Specifically, approval to combust blends of coal and TDF containing up to 20 weight percent TDF is requested.

As indicated, an analysis of PSD applicability along with the complete test burn report are provided in Attachments B and D, respectively. In addition, a no-threat-level guidance analysis is provided in Attachment C for those metals cited in FDEP's test burn approval.

2. Projected or Actual Date of Commencement of Construction:

N/A

3. Projected Date of Completion of Construction:

N/A

**Professional Engineer Certification**

1. Professional Engineer Name: **Douglas A. Dean**

Registration Number: **40094**

2. Professional Engineer Mailing Address:

Organization/Firm: **Environmental Consulting & Technology, Inc.**

Street Address: **3701 Northwest 98th Street**

City: **Gainesville** State: **Florida** Zip Code: **33606**

3. Professional Engineer Telephone Numbers:

Telephone: **(352) 332-0444**

Fax: **(352) 332-6722**

4. Professional Engineer Statement:

*I, the undersigned, hereby certify, except as particularly noted herein\*, that:*

*(1) To the best of my knowledge, there is reasonable assurance that the air pollutant emissions unit(s) and the air pollution control equipment described in this Application for Air Permit, when properly operated and maintained, will comply with all applicable standards for control of air pollutant emissions found in the Florida Statutes and rules of the Department of Environmental Protection; and*

*(2) To the best of my knowledge, any emission estimates reported or relied on in this application are true, accurate, and complete and are either based upon reasonable techniques available for calculating emissions or, for emission estimates of hazardous air pollutants not regulated for an emissions unit addressed in this application, based solely upon the materials, information and calculations submitted with this application.*

*If the purpose of this application is to obtain a Title V source air operation permit (check here [ ] if so), I further certify that each emissions unit described in this Application for Air Permit, when properly operated and maintained, will comply with the applicable requirements identified in this application to which the unit is subject, except those emissions units for which a compliance schedule is submitted with this application.*

*If the purpose of this application is to obtain an air construction permit for one or more proposed new or modified emissions units (check here [ ] if so), I further certify that the engineering features of each such emissions unit described in this application have been designed or examined by me or individuals under my direct supervision and found to be in conformity with sound engineering principles applicable to the control of emissions of the air pollutants characterized in this application.*

*If the purpose of this application is to obtain an initial air operation permit or operation permit revision for one or more newly constructed or modified emissions units (check here [ ] if so), I further certify that, with the exception of any changes detailed as part of this application, each such emissions unit has been constructed or modified in substantial accordance with the information given in the corresponding application for air construction permit and with all provisions contained in such permit.*

*Douglas Dean*  
\_\_\_\_\_  
Signature

08/07/96  
\_\_\_\_\_  
Date

Attach any exception to certification statement.



**Application Contact**

1. Name and Title of Application Contact:  <b>Janice Taylor</b> <b>Senior Engineer, Environmental Planning</b>
2. Application Contact Mailing Address:  Organization/Firm: <b>Tampa Electric Company</b> Street Address: <b>702 North Franklin Street</b> City: <b>Tampa</b> State: <b>Florida</b> Zip Code: <b>33602</b>
3. Application Contact Telephone Numbers: Telephone: <b>(813) 228-4939</b> Fax: <b>(813) 228-4881</b>

**Application Comment**

N/A
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## II. FACILITY INFORMATION

### A. GENERAL FACILITY INFORMATION

#### Facility Location and Type

1. Facility UTM Coordinates: Zone: <b>17</b> East (km): <b>360.0</b> North (km): <b>3,087.5</b>			
2. Facility Latitude/Longitude: Latitude (DD/MM/SS): Longitude (DD/MM/SS):			
3. Governmental Facility Code: <b>0</b>	4. Facility Status Code: <b>A</b>	5. Facility Major Group SIC Code: <b>49</b>	6. Facility SIC(s): <b>4911</b>
7. Facility Comment (limit to 500 characters):          <b>N/A</b>			

#### Facility Contact

1. Name and Title of Facility Contact: <b>Cindy Barringer</b>			
2. Facility Contact Mailing Address: Organization/Firm: <b>Tampa Electric Company</b> Street Address: <b>Port Sutton Road</b> City: <b>Tampa</b> State: <b>Florida</b> Zip Code: <b>33619</b>			
3. Facility Contact Telephone Numbers: Telephone: <b>(813) 228-1896</b> Fax: <b>(813) 228-1905</b>			

**Facility Regulatory Classifications**

1. Small Business Stationary Source? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No <input type="checkbox"/> Unknown
2. Title V Source? <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No
3. Synthetic Non-Title V Source? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No
4. Major Source of Pollutants Other than Hazardous Air Pollutants (HAPs)? <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No
5. Synthetic Minor Source of Pollutants Other than HAPs? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No
6. Major Source of Hazardous Air Pollutants (HAPs)? <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No
7. Synthetic Minor Source of HAPs? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No
8. One or More Emissions Units Subject to NSPS? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No
9. One or More Emission Units Subject to NESHAP? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No
10. Title V Source by EPA Designation? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No
11. Facility Regulatory Classifications Comment (limit to 200 characters):          <p style="text-align: center;">N/A</p>

## B. FACILITY REGULATIONS

**Rule Applicability Analysis** (Required for Category II applications and Category III applications involving non Title-V sources. See Instructions.)

**A complete listing of all federal and state applicable requirements has been submitted with the initial F.J. Gannon Station Title V permit application.**

**List of Applicable Regulations** (Required for Category I applications and Category III applications involving Title-V sources. See Instructions.)

N/A	

**C. FACILITY POLLUTANTS**

**Facility Pollutant Information**

1. Pollutant Emitted	2. Pollutant Classification
<b>Provided with the initial F.J. Gannon Station Title V permit application.</b>	



**D. FACILITY POLLUTANT DETAIL INFORMATION**

**Facility Pollutant Detail Information:** Pollutant   1   of   1  

1. Pollutant Emitted: <b>SO2</b>		
2. Requested Emissions Cap:	(lb/hour) <b>21,200</b>	(tons/year) <b>N/A</b>
3. Basis for Emissions Cap Code: <b>FDEP Rule 62-296.405(1)(c)2.a, F.A.C.</b>		
4. Facility Pollutant Comment (limit to 400 characters):  <b>Hourly emissions cap represents total sulfur dioxide emissions from F.J. Gannon Station Unit No. 1 through Unit No. 6 for a weekly average period. This is an existing requirement per FDEP Rule 62-296.405(1)(c)2.a, F.A.C.</b>		

**Facility Pollutant Detail Information:** Pollutant \_\_\_\_\_ of \_\_\_\_\_

1. Pollutant Emitted:		
2. Requested Emissions Cap:	(lb/hour)	(tons/year)
3. Basis for Emissions Cap Code:		
4. Facility Pollutant Comment (limit to 400 characters):		

## E. FACILITY SUPPLEMENTAL INFORMATION

### Supplemental Requirements for All Applications

1. Area Map Showing Facility Location: <input checked="" type="checkbox"/> Attached, Document ID: <u>II.D.1.1</u> [ ] Not Applicable [ ] Waiver Requested <b>Attachment E</b>
2. Facility Plot Plan: <input checked="" type="checkbox"/> Attached, Document ID: <u>II.D.2.4</u> [ ] Not Applicable [ ] Waiver Requested <b>Attachment E</b>
3. Process Flow Diagram(s): [ ] Attached, Document ID: _____ [ <input checked="" type="checkbox"/> ] Not Applicable [ ] Waiver Requested
4. Precautions to Prevent Emissions of Unconfined Particulate Matter: [ ] Attached, Document ID: _____ [ <input checked="" type="checkbox"/> ] Not Applicable [ ] Waiver Requested
5. Fugitive Emissions Identification: [ ] Attached, Document ID: _____ [ <input checked="" type="checkbox"/> ] Not Applicable [ ] Waiver Requested
6. Supplemental Information for Construction Permit Application: [ ] Attached, Document ID: _____ [ <input checked="" type="checkbox"/> ] Not Applicable

### Additional Supplemental Requirements for Category I Applications Only

7. List of Proposed Exempt Activities: [ ] Attached, Document ID: _____ [ ] Not Applicable
8. List of Equipment/Activities Regulated under Title VI:  [ ] Attached, Document ID: _____  [ ] Equipment/Activities On site but Not Required to be Individually Listed  [ ] Not Applicable
9. Alternative Methods of Operation: [ ] Attached, Document ID: _____ [ ] Not Applicable
10. Alternative Modes of Operation (Emissions Trading): [ ] Attached, Document ID: _____ [ ] Not Applicable

<p>11. Identification of Additional Applicable Requirements:  <input type="checkbox"/> Attached, Document ID: _____ <input type="checkbox"/> Not Applicable</p>
<p>12. Compliance Assurance Monitoring Plan:  <input type="checkbox"/> Attached, Document ID: _____ <input type="checkbox"/> Not Applicable</p>
<p>13. Risk Management Plan Verification:</p> <p><input type="checkbox"/> Plan Submitted to Implementing Agency - Verification Attached,  Document ID: _____</p> <p><input type="checkbox"/> Plan to be Submitted to Implementing Agency by Required Date</p> <p><input type="checkbox"/> Not Applicable</p>
<p>14. Compliance Report and Plan:  <input type="checkbox"/> Attached, Document ID: _____ <input type="checkbox"/> Not Applicable</p>
<p>15. Compliance Certification (Hard-copy Required):  <input type="checkbox"/> Attached, Document ID: _____ <input type="checkbox"/> Not Applicable</p>

### III. EMISSIONS UNIT INFORMATION

A separate Emissions Unit Information Section (including subsections A through L as required) must be completed for each emissions unit addressed in this Application for Air Permit. If submitting the application form in hard copy, indicate, in the space provided at the top of each page, the number of this Emissions Unit Information Section and the total number of Emissions Unit Information Sections submitted as part of this application. Some of the subsections comprising the Emissions Unit Information Section of the form are intended for regulated emissions units only. Others are intended for both regulated and unregulated emissions units. Each subsection is appropriately marked.

#### A. TYPE OF EMISSIONS UNIT (Regulated and Unregulated Emissions Units)

##### Type of Emissions Unit Addressed in This Section

1. Regulated or Unregulated Emissions Unit? Check one:

[ X ] The emissions unit addressed in this Emissions Unit Information Section is a regulated emissions unit.

[ ] The emissions unit addressed in this Emissions Unit Information Section is an unregulated emissions unit.

2. Single Process, Group of Processes, or Fugitive Only? Check one:

[ X ] This Emissions Unit Information Section addresses, as a single emissions unit, a single process or production unit, or activity, which produces one or more air pollutants and which has at least one definable emission point (stack or vent).

[ ] This Emissions Unit Information Section addresses, as a single emissions unit, a group of process or production units and activities which has at least one definable emission point (stack or vent) but may also produce fugitive emissions.

[ ] This Emissions Unit Information Section addresses, as a single emissions unit, one or more process or production units and activities which produce fugitive emissions only.

**B. GENERAL EMISSIONS UNIT INFORMATION  
(Regulated and Unregulated Emissions Units)**

**Emissions Unit Description and Status**

1. Description of Emissions Unit Addressed in This Section (limit to 60 characters):  <b>Unit No. 3, Solid Fuel Steam Generator</b>		
2. Emissions Unit Identification Number: [ ] No Corresponding ID [ ] Unknown <b>003</b>		
3. Emissions Unit Status Code: <b>A</b>	4. Acid Rain Unit? [ X ] Yes [ ] No	5. Emissions Unit Major Group SIC Code: <b>49</b>
6. Emissions Unit Comment (limit to 500 characters):          <b>N/A</b>		

**Emissions Unit Control Equipment**

**A.**

1. Description (limit to 200 characters):  <b>Electrostatic precipitator system</b>
2. Control Device or Method Code: <b>010</b>

Emissions Unit Information Section  1  of  1

B.

<p>1. Description (limit to 200 characters):</p>          <p style="text-align: center;">N/A</p>
--

<p>2. Control Device or Method Code:</p>
--

C.

<p>1. Description (limit to 200 characters):</p>          <p style="text-align: center;">N/A</p>
--

<p>2. Control Device or Method Code:</p>
--

**C. EMISSIONS UNIT DETAIL INFORMATION  
(Regulated Emissions Units Only)**

**Emissions Unit Details**

1. Initial Startup Date: N/A			
2. Long-term Reserve Shutdown Date: N/A			
3. Package Unit: N/A		Model Number:	
Manufacturer:			
4. Generator Nameplate Rating:	180	MW	
5. Incinerator Information: N/A			
	Dwell Temperature:		°F
	Dwell Time:		seconds
	Incinerator Afterburner Temperature:		°F

**Emissions Unit Operating Capacity**

1. Maximum Heat Input Rate:	1,599	mmBtu/hr
2. Maximum Incineration Rate:	lb/hr	tons/day
N/A		
3. Maximum Process or Throughput Rate: N/A		
4. Maximum Production Rate: N/A		
5. Operating Capacity Comment (limit to 200 characters):		
<p><b>Maximum fuel heat input rate of 1,599 MMBtu/hr is on a monthly average basis.</b></p>		

**Emissions Unit Operating Schedule**

Requested Maximum Operating Schedule:			
24	hours/day	7	days/week
52	weeks/year	8,760	hours/year

**D. EMISSIONS UNIT REGULATIONS  
(Regulated Emissions Units Only)**

**Rule Applicability Analysis** (Required for Category II applications and Category III applications involving non Title-V sources. See Instructions.)

**A complete listing of all federal and state applicable requirements for Unit No. 3 has been submitted with the initial F.J. Gannon Station Title V permit application.**



**List of Applicable Regulations** (Required for Category I applications and Category III applications involving Title-V sources. See Instructions.)

N/A	

### E. EMISSION POINT (STACK/VENT) INFORMATION (Regulated Emissions Units Only)

**Emission Point Description and Type**

1. Identification of Point on Plot Plan or Flow Diagram:	
2. Emission Point Type Code: [ X ] 1            [   ] 2            [   ] 3            [   ] 4	
3. Descriptions of Emissions Points Comprising this Emissions Unit for VE Tracking (limit to 100 characters per point):  <p style="text-align: center; margin-top: 40px;">N/A</p>	
4. ID Numbers or Descriptions of Emission Units with this Emission Point in Common:  <p style="text-align: center; margin-top: 40px;">N/A</p>	
5. Discharge Type Code: [   ] D            [   ] F            [   ] H            [   ] P [   ] R            [ X ] V            [   ] W	
6. Stack Height:	315 feet
7. Exit Diameter:	10.6 feet
8. Exit Temperature:	290 °F

Emissions Unit Information Section  1  of  1

9. Actual Volumetric Flow Rate:	<b>537,259</b>	acfm
10. Percent Water Vapor : N/A		%
11. Maximum Dry Standard Flow Rate: N/A		dscfm
12. Nonstack Emission Point Height: N/A		feet
13. Emission Point UTM Coordinates: Zone: <b>17</b>	East (km): <b>360.0</b>	North (km): <b>3,087.5</b>
14. Emission Point Comment (limit to 200 characters):		

**F. SEGMENT (PROCESS/FUEL) INFORMATION  
(Regulated and Unregulated Emissions Units)**

**Segment Description and Rate:** Segment  1  of  1

1. Segment Description (Process/Fuel Type and Associated Operating Method/Mode) (limit to 500 characters):	
<b>Coal and coal/TDF blends in Unit No. 3.</b>	
2. Source Classification Code (SCC): <b>1-01-002-03</b>	
3. SCC Units: <b>Tons burned (all solid fuels)</b>	
4. Maximum Hourly Rate: <b>65.0</b>	5. Maximum Annual Rate: <b>569,400</b>
6. Estimated Annual Activity Factor:	
7. Maximum Percent Sulfur: <b>1.3</b>	8. Maximum Percent Ash: <b>8.2</b>
9. Million Btu per SCC Unit: <b>25</b>	
10. Segment Comment (limit to 200 characters):	
<p><b>No. 2 fuel oil used for ignition during startups. Fluxing agents may be added to fuel. Maximum hourly rate (Field 4), maximum annual rate (Field 5), and Btu/SCC unit (Field 9) based on average heat content of 12,300 Btu/hr. Fuel sulfur content based on 100-percent coal blend. Ash content based on 80/20 percent coal/TDF blend. Solid fuel blend may be supplemented with up to 48 gal/min used oil combustion, including liquid oil and oil-contaminated solids (i.e., oil absorbant, oily soil, etc.). Up to 50 gal/min of nonhazardous boiler cleaning waste may be injected into boiler during firing as a routine maintenance activity.</b></p>	

**G. EMISSIONS UNIT POLLUTANTS  
(Regulated and Unregulated Emissions Units)**

1. Pollutant Emitted	2. Primary Control Device Code	3. Secondary Control Device Code	4. Pollutant Regulatory Code
SO2			EL
NOx			NS
PM	010		EL
PM10	010		NS
CO			NS
VOC			NS
Pb	010		NS
H106 HCl			NS
H107 HF			NS
SAM			NS

**H. EMISSIONS UNIT POLLUTANT DETAIL INFORMATION  
(Regulated Emissions Units Only - Emissions Limited Pollutants Only)**

**Pollutant Detail Information:**

1. Pollutant Emitted: <b>SO2</b>	
2. Total Percent Efficiency of Control:	<b>0.0 %</b>
3. Potential Emissions:	<b>3,837.6 lb/hour                      16,808.7 tons/year</b>
4. Synthetically Limited? <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No	
5. Range of Estimated Fugitive/Other Emissions: <input type="checkbox"/> 1 <input type="checkbox"/> 2 <input type="checkbox"/> 3                      _____ to _____ tons/year	
6. Emission Factor: N/A Reference:	
7. Emissions Method Code: <input checked="" type="checkbox"/> 0 <input type="checkbox"/> 1 <input type="checkbox"/> 2 <input type="checkbox"/> 3 <input type="checkbox"/> 4 <input type="checkbox"/> 5	
8. Calculation of Emissions (limit to 600 characters):  <p align="center"><b>Potential hourly and annual emission rates set equal to equivalent allowable emission rates.</b></p>	
9. Pollutant Potential/Estimated Emissions Comment (limit to 200 characters):  <p align="center">N/A</p>	

**Allowable Emissions** (Pollutant identified on front of page)

**A.**

1. Basis for Allowable Emissions Code: <b>RULE</b>		
2. Future Effective Date of Allowable Emissions: <b>N/A</b>		
3. Requested Allowable Emissions and Units: <b>2.4 lb/MMBtu</b>		
4. Equivalent Allowable Emissions:	lb/hour <b>3,837.6</b>	tons/year <b>16,808.7</b>
5. Method of Compliance (limit to 60 characters): <b>Weekly composite fuel sampling and analysis or continuous emissions monitoring, per FDEP Rule 62-296.405(1)(f)1.b, F.A.C.</b>		
6. Pollutant Allowable Emissions Comment (Desc. of Related Operating Method/Mode) (limit to 200 characters):  <b>Requested allowable emissions represent a weekly average, per Specific Condition No. 4 of Permit A029-172179 and FDEP Rule 62-296.405(1)(c)2.a, F.A.C.</b>		

**B.**

1. Basis for Allowable Emissions Code:		
2. Future Effective Date of Allowable Emissions:		
3. Requested Allowable Emissions and Units:		
4. Equivalent Allowable Emissions:	lb/hr	tons/year
5. Method of Compliance (limit to 60 characters):		
6. Pollutant Allowable Emissions Comment (Desc. of Related Operating Method/Mode) (limit to 200 characters):		

**H. EMISSIONS UNIT POLLUTANT DETAIL INFORMATION  
(Regulated Emissions Units Only - Emissions Limited Pollutants Only)**

**Pollutant Detail Information:**

1. Pollutant Emitted: <b>PM/PM10</b>	
2. Total Percent Efficiency of Control:	<b>99.7 %</b>
3. Potential Emissions:	<b>479.7 lb/hour      875.5 tons/year</b>
4. Synthetically Limited? [ ] Yes      [X] No	
5. Range of Estimated Fugitive/Other Emissions: [ ] 1      [ ] 2      [ ] 3      _____ to _____ tons/year	
6. Emission Factor: N/A Reference:	
7. Emissions Method Code: [X] 0      [ ] 1      [ ] 2      [ ] 3      [ ] 4      [ ] 5	
8. Calculation of Emissions (limit to 600 characters):  <b>Potential hourly and annual emission rates set equal to equivalent allowable emission rates.</b>	
9. Pollutant Potential/Estimated Emissions Comment (limit to 200 characters):	



**Allowable Emissions** (Pollutant identified on front of page)

A.

1. Basis for Allowable Emissions Code: <b>RULE</b>		
2. Future Effective Date of Allowable Emissions: <b>N/A</b>		
3. Requested Allowable Emissions and Units: <b>0.3 lb/MMBtu</b>		
4. Equivalent Allowable Emissions:	<b>479.7 lb/hour</b>	<b>875.5 tons/year</b>
5. Method of Compliance (limit to 60 characters): <b>Annual testing using EPA Reference Method 5, 5B, or 17. As an option, three soot-blowing test runs will be used to demonstrate compliance with the nonsoot-blowing standard.</b>		
6. Pollutant Allowable Emissions Comment (Desc. of Related Operating Method/Mode) (limit to 200 characters): <b>0.3 lb/MMBtu applicable during soot-blowing (3 hours per day [hr/day]). 0.1 lb/MMBtu applicable during nonsoot-blowing. Per FDEP Rules 62-210.700(3) and 62-296.405(1)(b), F.A.C.</b>		
<b>Hourly equivalent allowable emissions based on 0.3 lb/MMBtu. Annual equivalent allowable emissions based on 3 hr/day at 0.3 lb/MMBtu and 21 hr/day at 0.1 lb/MMBtu.</b>		

B.

1. Basis for Allowable Emissions Code:		
2. Future Effective Date of Allowable Emissions:		
3. Requested Allowable Emissions and Units:		
4. Equivalent Allowable Emissions:	<b>lb/hr</b>	<b>tons/year</b>
5. Method of Compliance (limit to 60 characters):		
6. Pollutant Allowable Emissions Comment (Desc. of Related Operating Method/Mode) (limit to 200 characters):		

I. VISIBLE EMISSIONS INFORMATION  
(Regulated Emissions Units Only)

**Visible Emissions Limitation:** Visible Emissions Limitation  1  of  5

1. Visible Emissions Subtype: <b>VE20</b>	
2. Basis for Allowable Opacity:	<input checked="" type="checkbox"/> Rule <input type="checkbox"/> Other
3. Requested Allowable Opacity:	Normal Conditions: <b>20</b> %      Exceptional Conditions: <b>27</b> % Maximum Period of Excess Opacity Allowed: <b>6</b> min/hour
4. Method of Compliance:	<b>Continuous emissions monitoring</b>
5. Visible Emissions Comment (limit to 200 characters):  <b>FDEP Rule 62-296.405(1)(a), F.A.C.</b>	

**Visible Emissions Limitation:** Visible Emissions Limitation  2  of  5

1. Visible Emissions Subtype: <b>VE60</b>	
2. Basis for Allowable Opacity:	<input checked="" type="checkbox"/> Rule <input type="checkbox"/> Other
3. Requested Allowable Opacity:	Normal Conditions:      %      Exceptional Conditions: <b>60</b> % Maximum Period of Excess Opacity Allowed: <b>60</b> min/hour
4. Method of Compliance:	<b>Continuous emissions monitoring</b>
5. Visible Emissions Comment (limit to 200 characters):  <b>Maximum period of excess opacity allowed for 3 hours in any 24-hour period during soot blowing and load change. FDEP Rule 62-210.700(3), F.A.C.</b>	

**I. VISIBLE EMISSIONS INFORMATION  
(Regulated Emissions Units Only)**

**Visible Emissions Limitation:** Visible Emissions Limitation  3  of  5

1. Visible Emissions Subtype: <b>VE100</b>			
2. Basis for Allowable Opacity:		<input checked="" type="checkbox"/> Rule	<input type="checkbox"/> Other
3. Requested Allowable Opacity:			
Normal Conditions:	%	Exceptional Conditions:	<b>100</b> %
Maximum Period of Excess Opacity Allowed:			<b>24</b> min/hour
4. Method of Compliance: <b>Continuous emissions monitoring</b>			
5. Visible Emissions Comment (limit to 200 characters):  <b>Excess emission resulting from boiler cleaning and load change. Maximum period of excess opacity allowed is four 6-minute periods during a single 3-hour period. FDEP Rule 62-210.700(3), F.A.C.</b>			

**Visible Emissions Limitation:** Visible Emissions Limitation  4  of  5

1. Visible Emissions Subtype: <b>VE100</b>			
2. Basis for Allowable Opacity:		<input checked="" type="checkbox"/> Rule	<input type="checkbox"/> Other
3. Requested Allowable Opacity:			
Normal Conditions:	%	Exceptional Conditions:	<b>100</b> %
Maximum Period of Excess Opacity Allowed:			<b>60</b> min/hour
4. Method of Compliance: <b>Continuous emissions monitoring</b>			
5. Visible Emissions Comment (limit to 200 characters):  <b>Excess emission resulting from boiler startup and shutdown. FDEP Rule 62-210.700(2), F.A.C.</b>			

**I. VISIBLE EMISSIONS INFORMATION  
(Regulated Emissions Units Only)**

**Visible Emissions Limitation:** Visible Emissions Limitation  5  of  5

1. Visible Emissions Subtype: <b>VE100</b>			
2. Basis for Allowable Opacity:		<input checked="" type="checkbox"/> Rule	<input type="checkbox"/> Other
3. Requested Allowable Opacity:		Normal Conditions:	% Exceptional Conditions: <b>100</b> %
		Maximum Period of Excess Opacity Allowed:	<b>60</b> min/hour
4. Method of Compliance: <b>Continuous emissions monitoring</b>			
5. Visible Emissions Comment (limit to 200 characters):  <b>Excess emission resulting from startup, shutdown, and malfunction. Maximum period of excess opacity allowed is 2 hours during any 24-hour period. FDEP Rule 62-210.700(1), F.A.C.</b>			

**Visible Emissions Limitation:** Visible Emissions Limitation \_\_\_\_\_ of \_\_\_\_\_

1. Visible Emissions Subtype:			
2. Basis for Allowable Opacity:		<input type="checkbox"/> Rule	<input type="checkbox"/> Other
3. Requested Allowable Opacity:		Normal Conditions:	% Exceptional Conditions: %
		Maximum Period of Excess Opacity Allowed:	min/hour
4. Method of Compliance:			
5. Visible Emissions Comment (limit to 200 characters):			

**J. CONTINUOUS MONITOR INFORMATION  
(Regulated Emissions Units Only)**

**Continuous Monitoring System:** Continuous Monitor  1  of  5

1. Parameter Code: <b>VE</b>	2. Pollutant(s): <b>N/A</b>
3. CMS Requirement: <input checked="" type="checkbox"/> Rule <input type="checkbox"/> Other	
4. Monitor Information: Manufacturer: <b>Thermo Environmental Corporation</b> Model Number: <b>M400</b> Serial Number: <b>400B-3500</b>	
5. Installation Date: <b>10/01/93</b>	
6. Performance Specification Test Date:	
7. Continuous Monitor Comment (limit to 200 characters):  <b>Required by FDEP Rule 62-296.405(1)(f)1.a, F.A.C., and 40 CFR 75. System includes one opacity monitor.</b>	

**Continuous Monitoring System:** Continuous Monitor  2  of  5

1. Parameter Code: <b>EM</b>	2. Pollutant(s): <b>SO2</b>
3. CMS Requirement: <input checked="" type="checkbox"/> Rule <input type="checkbox"/> Other	
4. Monitor Information: Manufacturer: <b>Thermo Environmental Corporation</b> Model Number: <b>43B</b> Serial Number: <b>43B-48171-279</b>	
5. Installation Date: <b>07/01/94</b>	
6. Performance Specification Test Date:	
7. Continuous Monitor Comment (limit to 200 characters):  <b>Required by FDEP Rule 62-296.405(1)(f)1.b, F.A.C., and 40 CFR 75. System includes one SO<sub>2</sub> monitor with a backup system shared among Emission Unit Nos. 1, 2, and 3.</b>	

**J. CONTINUOUS MONITOR INFORMATION  
(Regulated Emissions Units Only)**

**Continuous Monitoring System:** Continuous Monitor  3  of  5

1. Parameter Code: <b>EM</b>	2. Pollutant(s): <b>NOx</b>
3. CMS Requirement: <input checked="" type="checkbox"/> Rule <input type="checkbox"/> Other	
4. Monitor Information: Manufacturer: <b>Thermo Environmental Corporation</b> Model Number: <b>42D</b> Serial Number: <b>42D-47872-279</b>	
5. Installation Date: <b>07/01/94</b>	
6. Performance Specification Test Date:	
7. Continuous Monitor Comment (limit to 200 characters):  <b>Required by 40 CFR 75. System includes one NO<sub>x</sub> monitor with a backup system shared among Emission Unit Nos. 1, 2, and 3.</b>	

**Continuous Monitoring System:** Continuous Monitor  4  of  5

1. Parameter Code: <b>FLOW</b>	2. Pollutant(s): <b>N/A</b>
3. CMS Requirement: <input checked="" type="checkbox"/> Rule <input type="checkbox"/> Other	
4. Monitor Information: Manufacturer: <b>USI</b> Model Number: <b>Ultraflow 100</b> Serial Number: <b>9401629</b>	
5. Installation Date: <b>07/01/94</b>	
6. Performance Specification Test Date:	
7. Continuous Monitor Comment (limit to 200 characters):  <b>Required by 40 CFR 75. System includes one flow monitor.</b>	

**J. CONTINUOUS MONITOR INFORMATION  
(Regulated Emissions Units Only)**

**Continuous Monitoring System:** Continuous Monitor  5  of  5

1. Parameter Code: <b>CO2</b>	2. Pollutant(s): <b>N/A</b>
3. CMS Requirement:	<input checked="" type="checkbox"/> Rule <input type="checkbox"/> Other
4. Monitor Information: Manufacturer: <b>Siemens</b> Model Number: <b>Ultramat 5E</b> Serial Number: <b>E3-727</b>	
5. Installation Date: <b>07/01/94</b>	
6. Performance Specification Test Date:	
7. Continuous Monitor Comment (limit to 200 characters):  <b>Required by 40 CFR 75. System includes one CO<sub>2</sub> monitor with a backup system shared among Emission Unit Nos. 1, 2, and 3.</b>	

**Continuous Monitoring System:** Continuous Monitor \_\_\_\_\_ of \_\_\_\_\_

1. Parameter Code:	2. Pollutant(s):
3. CMS Requirement:	<input type="checkbox"/> Rule <input type="checkbox"/> Other
4. Monitor Information: Manufacturer: Model Number:      Serial Number:	
5. Installation Date:	
6. Performance Specification Test Date:	
7. Continuous Monitor Comment (limit to 200 characters):	

**K. PREVENTION OF SIGNIFICANT DETERIORATION (PSD) INCREMENT  
TRACKING INFORMATION  
(Regulated and Unregulated Emissions Units)**

**PSD Increment Consumption Determination**

1. Increment Consuming for Particulate Matter or Sulfur Dioxide?

If the emissions unit addressed in this section emits particulate matter or sulfur dioxide, answer the following series of questions to make a preliminary determination as to whether or not the emissions unit consumes PSD increment for particulate matter or sulfur dioxide. Check the first statement, if any, that applies and skip remaining statements.

- ] The emissions unit is undergoing PSD review as part of this application, or has undergone PSD review previously, for particulate matter or sulfur dioxide. If so, emissions unit consumes increment.
  
- ] The facility addressed in this application is classified as an EPA major source pursuant to paragraph (c) of the definition of "major source of air pollution" in Chapter 62-213, F.A.C., and the emissions unit addressed in this section commenced (or will commence) construction after January 6, 1975. If so, baseline emissions are zero, and emissions unit consumes increment.
  
- ] The facility addressed in this application is classified as an EPA major source, and the emissions unit began initial operation after January 6, 1975, but before December 27, 1977. If so, baseline emissions are zero, and emissions unit consumes increment.
  
- ] For any facility, the emissions unit began (or will begin) initial operation after December 27, 1977. If so, baseline emissions are zero, and emissions unit consumes increment.
  
- ] None of the above apply. If so, the baseline emissions of the emissions unit are nonzero. In such case, additional analysis, beyond the scope of this application, is needed to determine whether changes in emissions have occurred (or will occur) after the baseline date that may consume or expand increment.



2. Increment Consuming for Nitrogen Dioxide?

If the emissions unit addressed in this section emits nitrogen oxides, answer the following series of questions to make a preliminary determination as to whether or not the emissions unit consumes PSD increment for nitrogen dioxide. Check first statement, if any, that applies and skip remaining statements.

- ] The emissions unit addressed in this section is undergoing PSD review as part of this application, or has undergone PSD review previously, for nitrogen dioxide. If so, emissions unit consumes increment.
- ] The facility addressed in this application is classified as an EPA major source pursuant to paragraph (c) of the definition of "major source of air pollution" in Chapter 62-213, F.A.C., and the emissions unit addressed in this section commenced (or will commence) construction after February 8, 1988. If so, baseline emissions are zero, and emissions unit consumes increment.
- ] The facility addressed in this application is classified as an EPA major source, and the emissions unit began initial operation after February 8, 1988, but before March 28, 1988. If so, baseline emissions are zero, and emissions unit consumes increment.
- ] For any facility, the emissions unit began (or will begin) initial operation after March 28, 1988. If so, baseline emissions are zero, and emissions unit consumes increment.
- ] None of the above apply. If so, the baseline emissions of the emissions unit are nonzero. In such case, additional analysis, beyond the scope of this application, is needed to determine whether changes in emissions have occurred (or will occur) after the baseline date that may consume or expand increment.

3. Increment Consuming/Expanding Code:			
PM	<input type="checkbox"/> ] C	<input type="checkbox"/> ] E	<input type="checkbox"/> ] Unknown
SO2	<input type="checkbox"/> ] C	<input type="checkbox"/> ] E	<input type="checkbox"/> ] Unknown
NO2	<input type="checkbox"/> ] C	<input type="checkbox"/> ] E	<input type="checkbox"/> ] Unknown
4. Baseline Emissions:			
PM	lb/hour		tons/year
SO2	lb/hour		tons/year
NO2			tons/year
5. PSD Comment (limit to 200 characters):			
<b>Emission unit is part of baseline PSD emission inventory. Use of coal/TDF blends will result in a net decrease in emissions in comparison to 100-percent baseline coal.</b>			

**L. EMISSIONS UNIT SUPPLEMENTAL INFORMATION  
(Regulated Emissions Units Only)**

**Supplemental Requirements for All Applications**

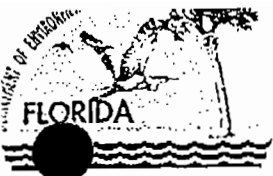
1. Process Flow Diagram <input checked="" type="checkbox"/> Attached, Document ID: <u>II.D.3.6</u> <input type="checkbox"/> Not Applicable <input type="checkbox"/> Waiver Requested <b>Attachment E</b>
2. Fuel Analysis or Specification <input type="checkbox"/> Attached, Document ID: _____ <input checked="" type="checkbox"/> Not Applicable <input type="checkbox"/> Waiver Requested
3. Detailed Description of Control Equipment <input type="checkbox"/> Attached, Document ID: _____ <input checked="" type="checkbox"/> Not Applicable <input type="checkbox"/> Waiver Requested
4. Description of Stack Sampling Facilities <input type="checkbox"/> Attached, Document ID: _____ <input checked="" type="checkbox"/> Not Applicable <input type="checkbox"/> Waiver Requested
5. Compliance Test Report <input type="checkbox"/> Attached, Document ID: _____  <input type="checkbox"/> Previously submitted, Date: _____  <input checked="" type="checkbox"/> Not Applicable
6. Procedures for Startup and Shutdown <input type="checkbox"/> Attached, Document ID: _____ <input checked="" type="checkbox"/> Not Applicable
7. Operation and Maintenance Plan <input type="checkbox"/> Attached, Document ID: _____ <input checked="" type="checkbox"/> Not Applicable
8. Supplemental Information for Construction Permit Application <input type="checkbox"/> Attached, Document ID: _____ <input checked="" type="checkbox"/> Not Applicable
9. Other Information Required by Rule or Statute <input type="checkbox"/> Attached, Document ID: _____ <input checked="" type="checkbox"/> Not Applicable

**Additional Supplemental Requirements for Category I Applications Only**

10. Alternative Methods of Operation <input type="checkbox"/> Attached, Document ID: _____ <input checked="" type="checkbox"/> Not Applicable
11. Alternative Modes of Operation (Emissions Trading) <input type="checkbox"/> Attached, Document ID: _____ <input checked="" type="checkbox"/> Not Applicable
12. Identification of Additional Applicable Requirements <input type="checkbox"/> Attached, Document ID: _____ <input checked="" type="checkbox"/> Not Applicable
13. Compliance Assurance Monitoring Plan <input type="checkbox"/> Attached, Document ID: _____ <input checked="" type="checkbox"/> Not Applicable
14. Acid Rain Application (Hard-copy Required)  <input type="checkbox"/> Acid Rain Part - Phase II (Form No. 62-210.900(1)(a)) Attached, Document ID: _____  <input type="checkbox"/> Repowering Extension Plan (Form No. 62-210.900(1)(a)1.) Attached, Document ID: _____  <input type="checkbox"/> New Unit Exemption (Form No. 62-210.900(1)(a)2.) Attached, Document ID: _____  <input type="checkbox"/> Retired Unit Exemption (Form No. 62-210.900(1)(a)3.) Attached, Document ID: _____  <input checked="" type="checkbox"/> Not Applicable

**ATTACHMENT A**

**FDEP TEST BURN AUTHORIZATION LETTER**



# Department of Environmental Protection

Lawton Chiles  
Governor

Southwest District  
3804 Coconut Palm Drive  
Tampa, Florida 33619

Virginia B. Wetherell  
Secretary

## NOTICE OF TDF TEST AUTHORIZATION

Mr. Philip J. Matonte, P.E.  
Tampa Electric Company  
P.O. Box 111  
Tampa, FL 33601-0111

RECEIVED

MAY 7 1996

ENVIRONMENTAL  
PLANNING

Dear Mr. Matonte:

Re: Letters dated 10/20/95 & 12/8/95  
Reference Permit No. A029-172179

Pursuant to Rule 62-4.210(1)(b)6., F.A.C., the Department authorizes your request to conduct a trial test burn of a coal/tire-derived fuel (TDF) mix containing a maximum of 20% TDF by weight at your Gannon Unit 3 facility as proposed. The authorization is granted with the following stipulations:

1. The Tampa Electric Company (TEC) shall notify in writing this office and the Environmental Protection of Commission of Hillsborough County at least 15 days prior to the date on which each formal compliance emission test is to begin of the date, time, and place of each such test, and the test contact person who will be responsible for coordinating and having such test conducted.
2. TEC shall notify this office and the EPCHC of the date initial testing of the baseline test, which uses coal only, within 5 days after that date.
3. TEC shall notify this office and the EPCHC of the date of first introducing TDF in Unit 3, within 5 days after that date.
4. The baseline testing shall be conducted for no less than 7 days and no more than 10 days.
6. Trial test burn testing when using TDF shall be conducted for a maximum of 21 days.
7. All testing shall be conducted within 60 days after the date TDF is first introduced into Unit 3.

8. The maximum total amount of TDF that may be used is 13 tons/hr. and 5,000 tons for up to 60 days from the date of first introducing TDF in Unit 3.
9. Only TDF that has a nominal 1 square inch size may be used.
10. Coal used for the baseline tests and trial burn test shall be conducted with coal that has the same typical heat content.
11. No TDF shall be used after 60 days from the date of first introducing TDF in Unit 3. This limitation is applicable even if all testing has been completed before the end of the 60th day of when TDF was first introduced into Unit 3, provided the emission limitations of permit AO29-172179 are not exceeded.
12. Testing during each operating scenario shall be in accordance with the following:
  - A. During each of the baseline and trial burn test periods when stack emission testing is conducted, sulfur dioxide, nitrogen oxides, carbon dioxide, and opacity emissions data shall be reported using continuous emission monitors (CEMS) that are located in the stack. The monitoring systems will be quality assured pursuant to 40 CFR 75, Appendix B. The data assessment report from 40 CFR 60, Appendix F, for the most recent relative accuracy test audit (RATA) and most recent cylinder gas audit (CGA), will be submitted with the test report(s).
  - B. During the baseline test period that only uses coal (steady-state & soot blowing conditions), EPA reference method emission testing shall be performed for particulate matter, visible emissions, and sulfuric acid mist. The EPA Method 17 test for particulates shall include EPA Methods 1, 2, 3, and 4. During these tests Unit 3 shall be operating within 90%-100% of maximum capacity (159 MW output & 65 tons/hr. total fuel input rate).
  - C. During each trial burn test that uses coal and TDF (steady-state & soot blowing conditions), EPA reference method emission testing shall be performed for particulate matter, visible emissions, and sulfuric acid mist. During these tests Unit 3 shall be operating with 90%-100% of maximum capacity (159 MW output & 65 tons/hr. total fuel input rate).

- D. Particulate testing and visible emissions testing shall be conducted when fly ash collected by the ESP is being re-injected into the boiler.
- E. Sulfuric acid mist emission testing shall be conducted when fly ash collected by the ESP is being re-injected into the boiler.
- F. All fuel testing shall be done on coal alone prior to blending with tires.
- G. Composite weekly coal fuel analysis results shall be supplied for the baseline test and the trial burn test. A single representative TDF fuel analysis results shall be supplied for each time the fuel bunker is charged for use during each CEM/stack tested operating scenario. The fuel analysis shall include the following:

Fuel Analysis

Trace Metal Analysis

Sulfur, wt. %	Beryllium
Volatiles, content, wt. %	Chromium
Nitrogen, wt. %	Lead
Ash, wt. %	Mercury
Calorific Value, BTU/lb.	Nickel
Carbon, wt. %	Vanadium
Moisture, wt. %	Zinc
TDF square inch size	
Coal origin (i.e., Eastern Kentucky, Blue Gem, etc.)	

- H. Records of the following operating parameters during each CEM/stack tested operating scenario shall be submitted with the associated test report:
  - 1. Fuel input rates (tons/hr.)
  - 2. Fuel ratio(s) on an hourly basis
  - 3. Opacity, CO, NOx, and SO2 CEM data, (The SO<sub>2</sub> and NO<sub>x</sub> CEM data shall be reported in lbs./MMBTU on an hourly average basis)
  - 4. Operating temperatures (degrees F)
  - 5. Operating conditions (soot blowing, load changes, normal operations, fuel additives, etc.)
  - 6. Power output (MW)
  - 7. Air to fuel ratio(s)

13. TEC shall comply with the emission limitations of permit A029-172179 at all times during the CEM/stack tests, operating scenarios, and operating modes approved by this authorization.
14. TEC shall notify this office and the EPCHC of the date the last test run is conducted within 5 days of that date.
15. All test reports/results shall be submitted to this office and the EPCHC within 45 days of the date of the last test run.
16. If at any time during the use of TDF the emission limitations of permit A029-172179 are exceeded, TEC shall immediately cease using TDF. Performance testing or continued operation when using TDF shall not resume until the appropriate measures to correct the problem have been corrected and approved by the Department in writing.
17. The trial test burn and other related testing, requested to be conducted, shall be conducted under the supervision of a Florida registered professional engineer. The professional engineer shall sign and seal each copy of the stack test reports and other related information.
18. The use of TDF shall not result in the release of objectionable odors.
19. This authorization expires on June 30, 1996.
20. If additional time is needed to conduct the tests, TEC shall request in writing to this office and the EPCHC an extension of time. The request shall have attached documentation of the progress to date and shall identify what is left to be done to complete the tests.

Any party to this Order (authorization) has the right to seek judicial review of the permit pursuant to Section 120.68, Florida Statutes, by the filing of a Notice of Appeal pursuant to Rule 9.110, Florida Rules of Appellate Procedure, with the Clerk of the Department in the Office of General Counsel, 2600 Blair Stone Road, Tallahassee, Florida 32399-2400; and by filing a copy of the Notice of Appeal accompanied by the applicable filing fees with the appropriate District Court of Appeal. The Notice of Appeal must be filed within 30 days from the date this Notice is filed with the Clerk of the Department.

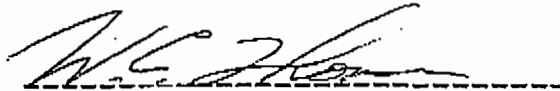
Executed in Tampa, Florida.



Tampa Electric Company  
Reference Permit No. AO29-172179  
Tire-Derived Fuel Test Authorization

Page 5 of 5

STATE OF FLORIDA DEPARTMENT  
OF ENVIRONMENTAL PROTECTION



W.C. Thomas, P.E.  
District Air Program Administrator

cc: EPCHC

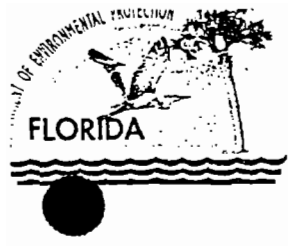
CERTIFICATE OF SERVICE

The undersigned duly designated deputy agency clerk hereby certifies that this NOTICE OF TDF TEST AUTHORIZATION and all copies were mailed before the close of business on 3/5/96 to the listed persons.

Clerk Stamp

FILING AND ACKNOWLEDGEMENT FILED, on this date, pursuant to Section 120.52(11), Florida Statutes, with the designated Department Clerk, receipt of which is hereby acknowledged.

Carol S. Moore 3/5/96  
(Clerk) (Date)



# Department of Environmental Protection

Lawton Chiles  
Governor

Southwest District  
3804 Coconut Palm Drive  
Tampa, Florida 33619

Virginia B. Wetherell  
Secretary

## NOTICE OF AMENDED TDF TEST AUTHORIZATION

Mr. Philip J. Matonte, P.E.  
Tampa Electric Company  
P.O. Box 111  
Tampa, FL 33601-0111

Dear Mr. Matonte:

Re: Letter dated 05/01/96  
Reference Permit No. A029-255208

Pursuant to Rule 62-4.210(1)(b)6., F.A.C., the Department authorizes your request to conduct a trial test burn of a coal/tire-derived fuel (TDF) mix containing a maximum of 20% TDF by weight at your Gannon Unit 4 instead of Gannon Unit 3 facility as proposed. The authorization is granted with the following stipulations:

1. The Tampa Electric Company (TEC) shall notify in writing this office and the Environmental Protection of Commission of Hillsborough County at least 15 days prior to the date on which each formal compliance emission test is to begin of the date, time, and place of each such test, and the test contact person who will be responsible for coordinating and having such test conducted.
2. TEC shall notify this office and the EPCHC of the date initial testing of the baseline test, which uses coal only, within 5 days after that date.
3. TEC shall notify this office and the EPCHC of the date of first introducing TDF in Unit 4, within 5 days after that date.
4. The baseline testing shall be conducted for no less than 7 days and no more than 10 days.
6. Trial test burn testing when using TDF shall be conducted for a maximum of 21 days.
7. All testing shall be conducted within 60 days after the date TDF is first introduced into Unit 4.

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8. The maximum total amount of TDF that may be used is 16 tons/hr. and 5,000 tons for up to 60 days from the date of first introducing TDF in Unit 4.
9. Only TDF that has a nominal 1 square inch size may be used.
10. Coal used for the baseline tests and trial burn test shall be conducted with coal that has the same typical heat content.
11. No TDF shall be used after 60 days from the date of first introducing TDF in Unit 4. This limitation is applicable even if all testing has been completed before the end of the 60th day of when TDF was first introduced into Unit 4, provided the emission limitations of permit AO29-255208 are not exceeded.
12. Testing during each operating scenario shall be in accordance with the following:
  - A. During each of the baseline and trial burn test periods when stack emission testing is conducted, sulfur dioxide, nitrogen oxides, carbon dioxide, and opacity emissions data shall be reported using continuous emission monitors (CEMS) that are located in each stack. The monitoring systems will be quality assured pursuant to 40 CFR 75, Appendix B. The data assessment report from 40 CFR 60, Appendix F, for the most recent relative accuracy test audit (RATA) and most recent cylinder gas audit (CGA), will be submitted with the test report(s).
  - B. During the baseline test period that only uses coal (steady-state & soot blowing conditions), EPA reference method emission testing shall be performed for particulate matter, visible emissions, and sulfuric acid mist. The EPA Method 17 test for particulates shall include EPA Methods 1, 2, 3, and 4. During these tests Unit 4 shall be operating within 90%-100% of maximum capacity (187.5 MW output & 80 tons/hr. total fuel input rate - corresponds to 1,876 MMBTU/hr. max.).
  - C. During each trial burn test that uses coal and TDF (steady-state & soot blowing conditions), EPA reference method emission testing shall be performed for particulate matter, visible emissions, and sulfuric acid mist. During these tests Unit 4 shall be operating with 90%-100% of maximum capacity (187.5 MW output & 80 tons/hr. total fuel input rate - corresponds to 1,876 MMBTU/hr. max.).

- D. Particulate testing and visible emissions testing shall be conducted when fly ash collected by the ESP is being re-injected into the boiler.
- E. Sulfuric acid mist emission testing shall be conducted when fly ash collected by the ESP is being re-injected into the boiler.
- F. All fuel testing shall be done on coal alone prior to blending with tires.
- G. Composite weekly coal fuel analysis results shall be supplied for the baseline test and the trial burn test. A single representative TDF fuel analysis results shall be supplied for each time the fuel bunker is charged for use during each CEM/stack tested operating scenario. The fuel analysis shall include the following:

Fuel Analysis

Trace Metal Analysis

Sulfur, wt. %	Beryllium
Volatiles, content, wt. %	Chromium
Nitrogen, wt. %	Lead
Ash, wt. %	Mercury
Calorific Value, BTU/lb.	Nickel
Carbon, wt. %	Vanadium
Moisture, wt. %	Zinc
TDF square inch size	
Coal origin (i.e., Eastern Kentucky, Blue Gem, etc.)	

- H. Records of the following operating parameters during each CEM/stack tested operating scenario shall be submitted with the associated test report:
  - 1. Fuel input rates (tons/hr.)
  - 2. Fuel ratio(s) on an hourly basis
  - 3. Opacity, CO, NOx, and SO2 CEM data, (The SO<sub>2</sub> and NO<sub>x</sub> CEM data shall be reported in lbs./MMBTU on an hourly average basis)
  - 4. Operating temperatures (degrees F)
  - 5. Operating conditions (soot blowing, load changes, normal operations, fuel additives, etc.)
  - 6. Power output (MW)
  - 7. Air to fuel ratio(s)

13. TEC shall comply with the emission limitations of permit A029-255208 at all times during the CEM/stack tests, operating scenarios, and operating modes approved by this authorization.
14. TEC shall notify this office and the EPCHC of the date the last test run is conducted within 5 days of that date.
15. All test reports/results shall be submitted to this office and the EPCHC within 45 days of the date of the last test run.
16. If at any time during the use of TDF the emission limitations of permit A029-255208 are exceeded, TEC shall immediately cease using TDF. Performance testing or continued operation when using TDF shall not resume until the appropriate measures to correct the problem have been corrected and approved by the Department in writing.
17. The trial test burn and other related testing, requested to be conducted, shall be conducted under the supervision of a Florida registered professional engineer. The professional engineer shall sign and seal each copy of the stack test reports and other related information.
18. The use of TDF shall not result in the release of objectionable odors.
19. This authorization expires on August 30, 1996.
20. If additional time is needed to conduct the tests, TEC shall request in writing to this office and the EPCHC an extension of time. The request shall have attached documentation of the progress to date and shall identify what is left to be done to complete the tests.
21. The Notice of TDF Test Authorization dated March 5, 1996, regarding Gannon Unit No. 3 is null and void.
22. Since the emissions from Cannon No. 4 are exhausted through 2 stacks, both stacks shall be tested simultaneously for emissions.

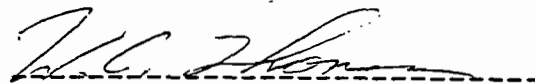
Persons whose substantial interests are affected by this authorization have a right, pursuant to Section 120.57, Florida Statutes, to petition for an administrative determination (hearing) in the Department's Office of General Counsel, 3900 Commonwealth Boulevard, Tallahassee, Florida 32399-3000, within fourteen (14)

days of receipt of this notice. Failure to file a petition within the fourteen (14) days constitutes a waiver of any right such person has to an administrative determination (hearing) pursuant to Section 120.57 Florida Statutes. This authorization is final and effective on the date filed with the Clerk of the Department unless a petition is filed in accordance with this paragraph or unless a request for extension of time in which to file a petition is filed within the time specified for filing a petition and conforms to Rule 62-103.70, F.A.C. Upon timely filing of a petition or a request for an extension of time, this authorization will not be effective until further Order of the Department.

When the Order (authorization) is final, any party to the Order has the right to seek judicial review of the Order pursuant to Section 120.68. Florida Statutes, by the filing of a Notice of Appeal pursuant to Rule 9.110, Florida Rules of Appellate Procedure, with the Clerk of the Department in the Office of General Counsel, 3900 Commonwealth Boulevard, Tallahassee, Florida 32399-3000; and by filing a copy of the Notice of Appeal accompanied by the applicable filing fees with the appropriate District Court of Appeal. The Notice of Appeal must be filed within 30 days from the date the Final Order is filed with the Clerk of the Department.

Executed in Tampa, Florida.

STATE OF FLORIDA DEPARTMENT  
OF ENVIRONMENTAL PROTECTION



W.C. Thomas, P.E.  
District Air Program Administrator

cc: EPCHC

CERTIFICATE OF SERVICE

The undersigned duly designated deputy agency clerk hereby certifies that this NOTICE OF AMENDED TDF TEST AUTHORIZATION and all copies were mailed before the close of business on 5/14/96 to the listed persons.

Clerk Stamp

FILING AND ACKNOWLEDGEMENT FILED, on this date, pursuant to Section 120.52(11), Florida Statutes, with the designated Department Clerk, receipt of which is hereby acknowledged.

Carol S. Moore      5/14/96  
(Clerk)                      (Date)

**ATTACHMENT B**

**ANALYSIS OF PSD APPLICABILITY**



## ATTACHMENT B

### Baseline and Coal/TDF Blend Test Burn Results Comparison

BASELINE COAL TEST BURN DATA					
Pollutant	Emission Rate (lb/MMBtu)	Load (MMBtu/hr)	Emission Rate (lb/hr)	Annual Utilization* (hr/yr)	Annual Emission (tpy)
SO <sub>2</sub>	2.0	1,527.3	3,054.6	5,875	8,972.9
NO <sub>x</sub>	1.32	1,527.3	2,016.0	5,875	5,922.1
PM	0.026	1,527.3	39.7	5,875	116.6
Pb	2.9E-07	1,527.3	4.4E-04	5,875	1.3E-03
H <sub>2</sub> SO <sub>4</sub>	0.012	1,527.3	18.3	5,875	53.8

COAL/TDF BLEND TEST BURN DATA					
Pollutant	Emission Rate (lb/MMBtu)	Load (MMBtu/hr)	Emission Rate (lb/hr)	Annual Utilization* (hr/yr)	Annual Emission (tpy)
SO <sub>2</sub>	2.0	1,379.4	2,758.8	5,875	8,104.0
NO <sub>x</sub>	1.16	1,379.4	1,600.1	5,875	4,700.3
PM	0.026	1,379.4	35.9	5,875	105.4
Pb	2.1E-07	1,379.4	2.9E-04	5,875	8.4E-04
H <sub>2</sub> SO <sub>4</sub>	0.009	1,379.4	12.4	5,875	36.5

EMISSION RATE CHANGE (COAL/TDF BLEND TEST BURN - COAL TEST BURN)				
Pollutant		Emission Rate (lb/hr)	Annual Utilization* (lb/yr)	Annual Emission (tpy)
SO <sub>2</sub>		-295.8	5,875	-868.9
NO <sub>x</sub>		-415.9	5,875	-1221.8
PM		-3.8	5,875	-11.3
Pb		-1.5E-04	5,875	-4.6E-04
H <sub>2</sub> SO <sub>4</sub>		-5.9	5,875	-17.4

\*From 1994 Annual Operating Report (AOR).

Source: TEC, 1996.

**ATTACHMENT C**

**NO-THREAT-LEVEL GUIDANCE ANALYSIS**

## ATTACHMENT C

### Coal/TDF Blend Test Burn Metals Emissions Comparison to No-Threat Levels

Metal	Metal Concentration (µg/g)*	PM Emission Rate (lb/hr)	PM Emission Rate (g/hr)	Metal Emission Rate (g/hr)	Stack Gas Flow (dsft <sup>3</sup> /min)	Stack Gas Flow (dsm <sup>3</sup> /hr)	Metal Concentration Emission Rate (µg/m <sup>3</sup> )†	No-Threat Level		
								8-hr (µg/m <sup>3</sup> )	24-hr (µg/m <sup>3</sup> )	Annual (µg/m <sup>3</sup> )
Beryllium	0.3	35.9	16,284.24	0.005	310,054	527,793	0.01	0.02	0.0048	0.00042
Chromium	6	35.9	16,284.24	0.098	310,054	527,793	0.19	5	1.2	None
Mercury	0.08	35.9	16,284.24	0.001	310,054	527,793	0.002	1	0.24	None
Nickel	6	35.9	16,284.24	0.098	310,054	527,793	0.19	10	2.4	0.0042
Vanadium	19	35.9	16,284.24	0.309	310,054	527,793	0.59	0.5	0.12	20

\*Weighed average, coal/TDF blend.

†Worst-case scenario.

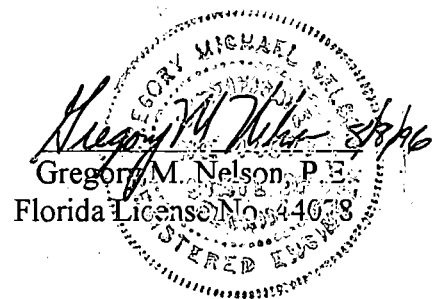
**ATTACHMENT D**

**TEST BURN REPORT**

**Tire Derived Fuel Emissions Test  
F. J. Gannon Generating Station  
Boiler No. 3  
February 26, 1996 Thru April 28, 1996  
Particulate, Sulfuric Acid Mist  
Visible Emissions, Sulfur Dioxide, Opacity  
Oxides of Nitrogen and Fuel Analysis**

Tampa Electric Company

August 8, 1996



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### **I. PROJECT PARTICIPANTS**



## **1.0 INTRODUCTION**

---

Tampa Electric Company's (TEC) Corporate Environmental Services(CES) performed a series of emission tests on Unit No. 3 at the F.J. Gannon Generating Station located in Hillsborough County on Port Sutton Road, in Tampa, Florida. The tests performed were used to determine the effects on emissions of supplementing the normal fuel for the facility (bituminous coal) with tire derived fuel (TDF) . The authorized test conditions for this test were:

1. Baseline firing with no TDF.
2. 20% TDF with 80% normal fuels

The Florida Department of Environmental Protection issued a letter of authorization to Tampa Electric Company allowing for these tests relating to F. J. Gannon Unit No. 3, operating permit No. AO29-172179. The Baseline testing period began on February 26 and was completed March 3, 1996. The TDF Fuel blend began March 7, 1996 and ended April 28, 1996. TDF was not bunkered continuously during this blend period. Fuel blend stack testing was performed on April 23, 1996.

Unit No. 3 is a steam-generating boiler which is normally fired with coal. Tests for particulate matter, sulfuric acid mist and visible emissions were performed on the boiler during sootblowing conditions. Sulfur dioxide, nitrogen oxides and opacity data were recorded using continuous emission monitors (CEMS) during the baseline and trial burn tests.

All testing was performed following the procedures and quality control guidelines given in 40 CFR 60 Appendix A - Test Methods.

Section 2.0 presents a brief source description and diagram of the sample point locations.

Section 3.0 outlines the procedures and test methods used along with diagrams of sampling trains used.

Section 4.0 presents the test results and comparison tables.

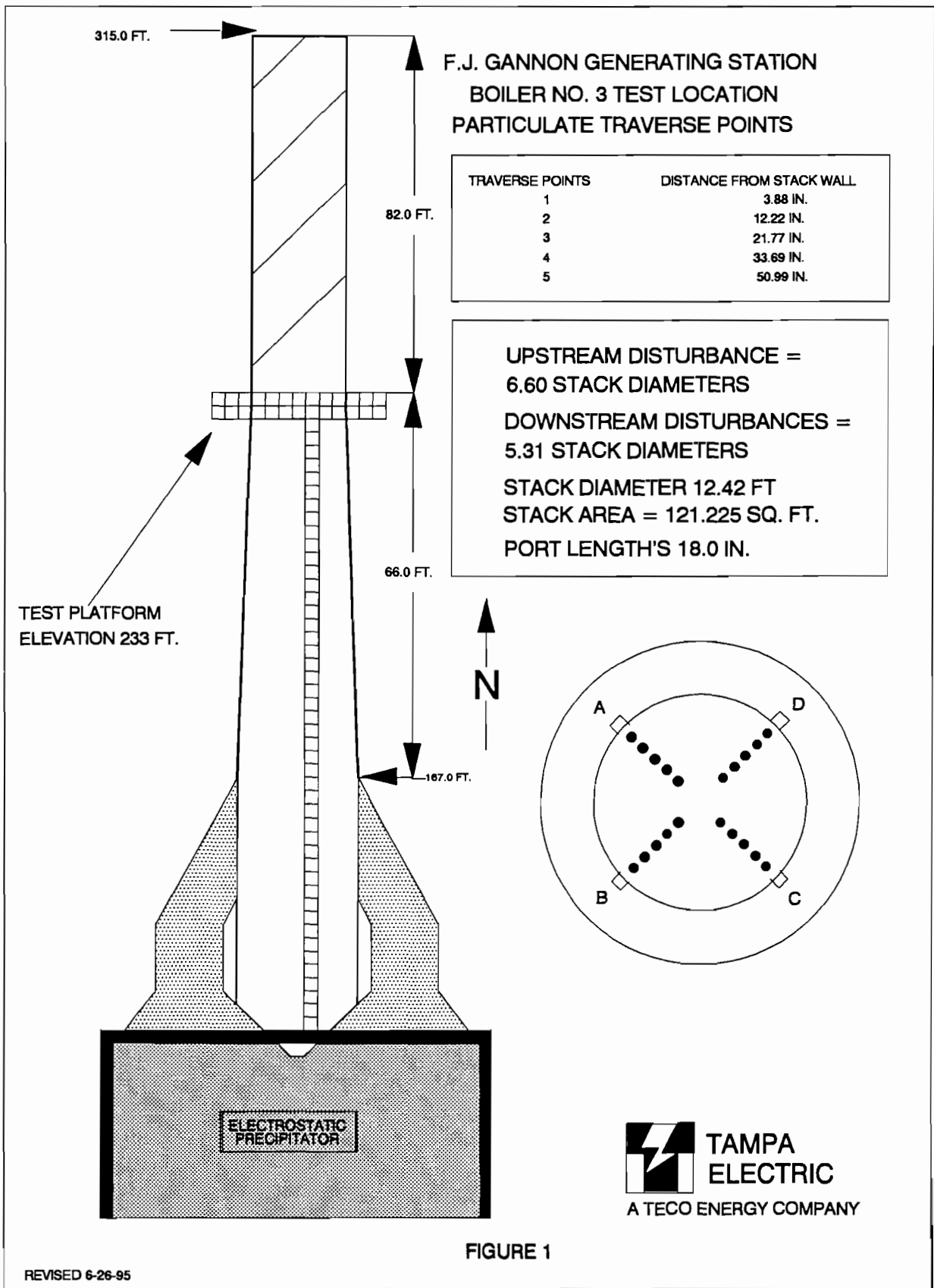
All supporting documentation, field data sheets, laboratory data, sample calculations, calibration data, quality assurance/quality control measures are included in the Appendices to this report.

## **2.0 SOURCE DESCRIPTION**

---

F.J. Gannon Generating Station is a coal-fired steam electric generating facility located in Hillsborough County on Port Sutton Road, in Tampa, Florida at UTM coordinates East 360.0 North 3087.5. The Unit No. 3 source sampling location consists of four sample ports located 90° apart on the circumference of the 12 ft. diameter circular stack, which is 315 ft in height. Upstream and downstream gas flow disturbances were determined to be 6.60 and 5.31 stack diameters away from the test ports, respectively. Using these criteria, a total of 20 sampling points were chosen for particulate sampling and sulfuric acid mist sampling, as stipulated in the U.S. EPA Method 1 test procedure. A diagram of the stack sampling location is included in Figure 1 along with other pertinent information on the test site.

Unit No. 3 is equipped with an electrostatic precipitator for the control of flyash emissions. Appendix C details the operational parameters of the electrostatic precipitator during the test period.



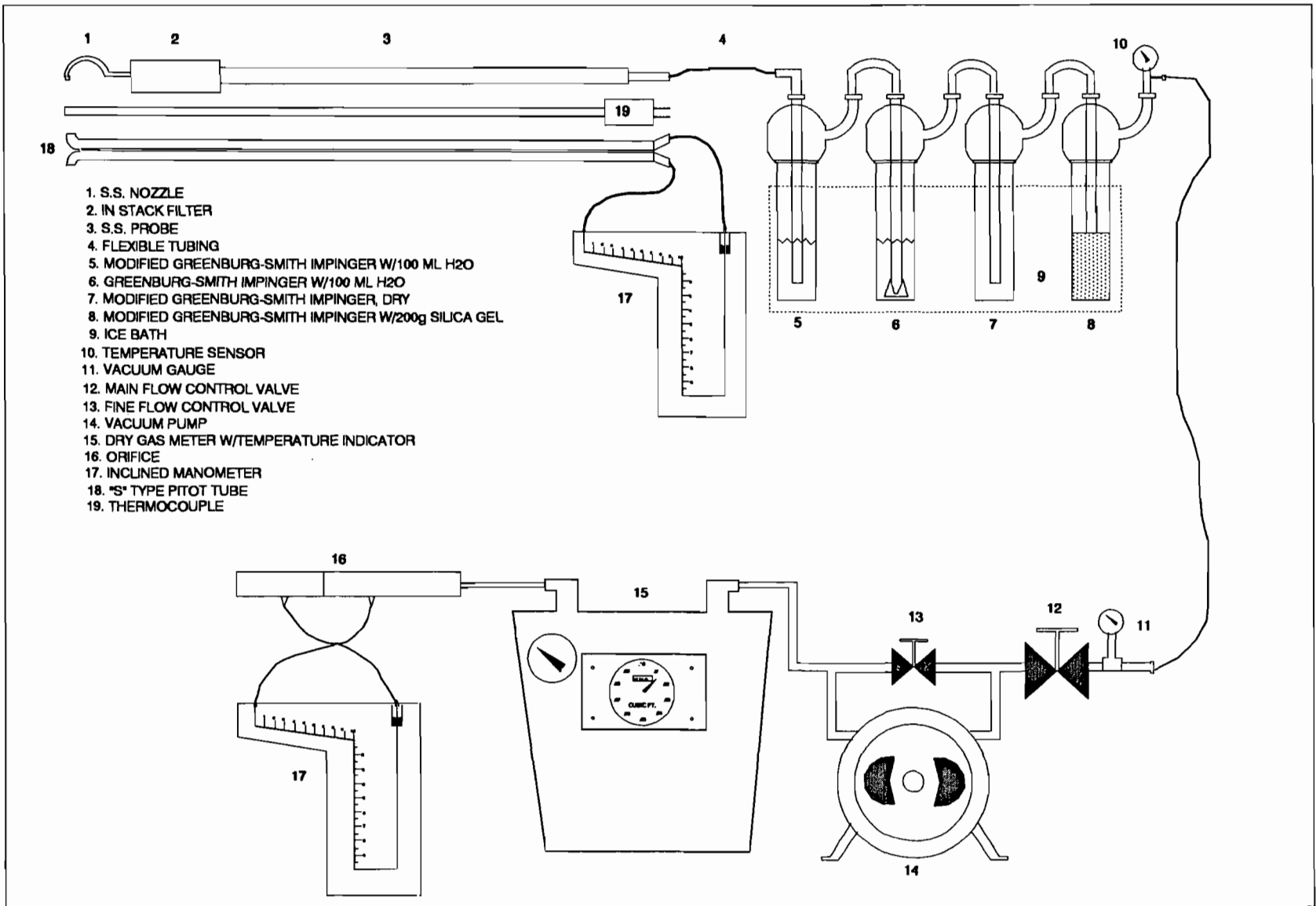
### **3.0 TEST PROCEDURES/SAMPLING TRAIN DIAGRAMS**

All particulate, sulfuric acid mist, oxygen, and visible emission testing followed the procedures and quality assurance/quality control guidelines given in 40 CFR 60 Appendix A.

Fuel analysis was performed on weekly composite coal samples taken during the baseline test and trial burn test period. Fuel analysis was also performed on a tire derived fuel sample collected during fuel bunkering for trial burn stack tests. Fuel sampling and analysis was performed following ASTM procedures and EPA methods. Fuel analysis of the composite coal samples for concentration of chromium, lead, nickel, beryllium, vanadium and zinc was prepared using ASTM 3683-78 (Re-approved 1989), "Standard Test Method for Trace Elements in Coal and Coke Ash by Atomic Absorption" and performed by EPA Method 200.7 "Determination of Metals and Trace Elements in Water and Wastes by Inductively Coupled Plasma-Atomic Emission Spectrometry." Fuel analysis on tire derived fuel for concentration of chromium, lead, nickel, beryllium, vanadium and zinc was performed using ASTM procedure D-3683, "Standard Test Method for Trace Elements in Coal and Coke Ash by Atomic Absorption." Trace metal analysis on all samples for concentration of mercury was prepared and analyzed using ASTM 3684-94 "Total Mercury in Coal by Oxygen Bomb Combustion/Atomic Absorption Method." Appendix E details the results of the coal and TDF analysis.

Particulate matter sampling was performed according to U.S. EPA Method 17, "Determination of Particulate Matter from Stationary Sources." Sampling was performed using the equipment depicted in Figure 2. Particulate matter was collected on a high purity glass micro fiber thimble measuring 19 X 90 mm. Sulfuric acid mist sampling was performed according to U.S. EPA Method 8 "Determination of Sulfuric Acid Mist and Sulfur Dioxide Emissions from Stationary Sources." Sampling was performed using the equipment depicted in Figure 3.

Diluent sampling and analysis was performed according to U.S. EPA Method 3 "Gas Analysis for Determination of Emission Rate Correction Factor, or Excess Air." Sampling was performed using the equipment depicted in Figure 4. Diluent analysis was performed using the equipment depicted in Figure 5.



**FIGURE 2**  
**PARTICULATE SAMPLING TRAIN**  
**USEPA METHOD 17**

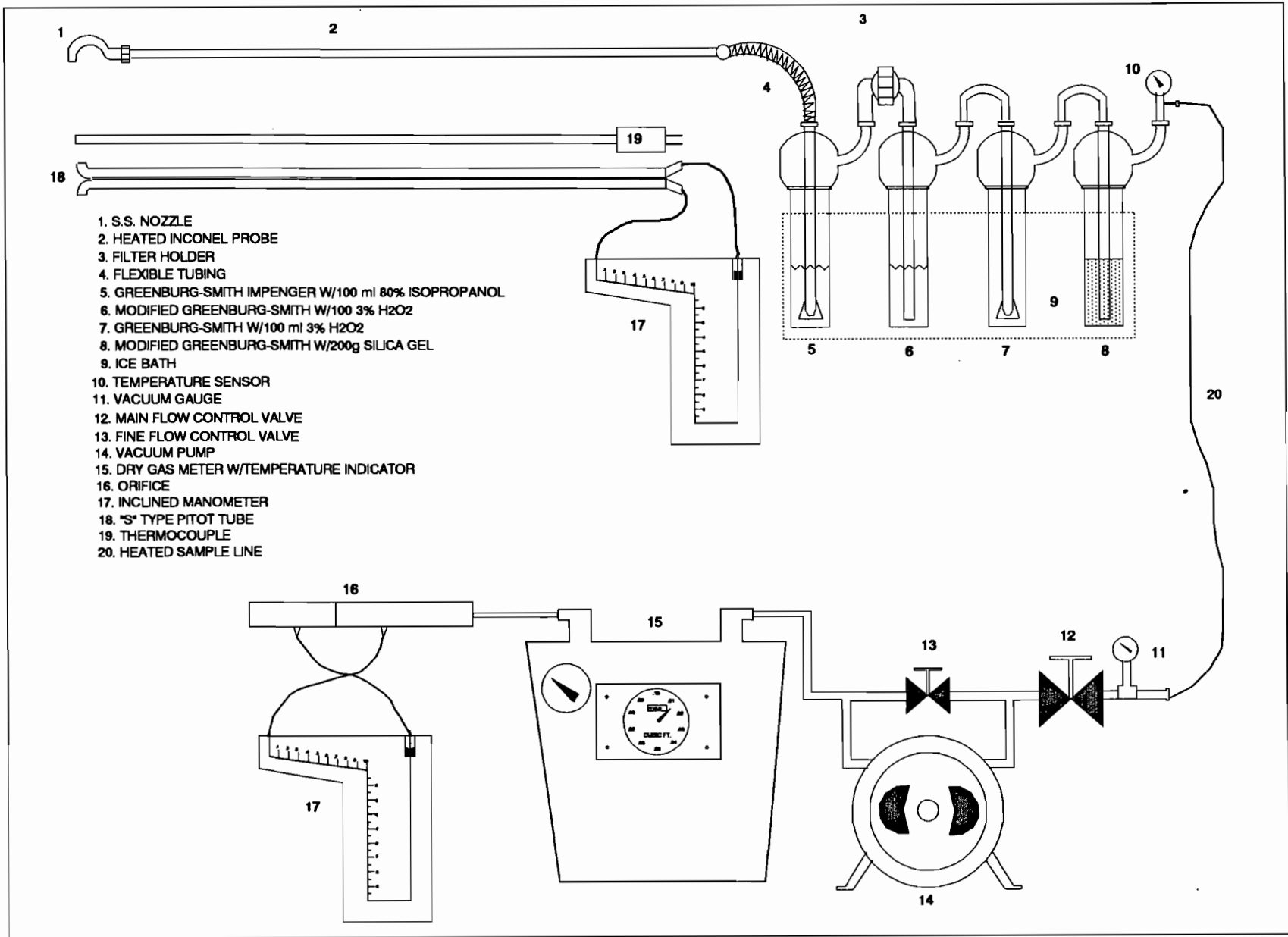


FIGURE 3  
 SULFURIC ACID MIST SAMPLING TRAIN  
 USEPA METHOD 8



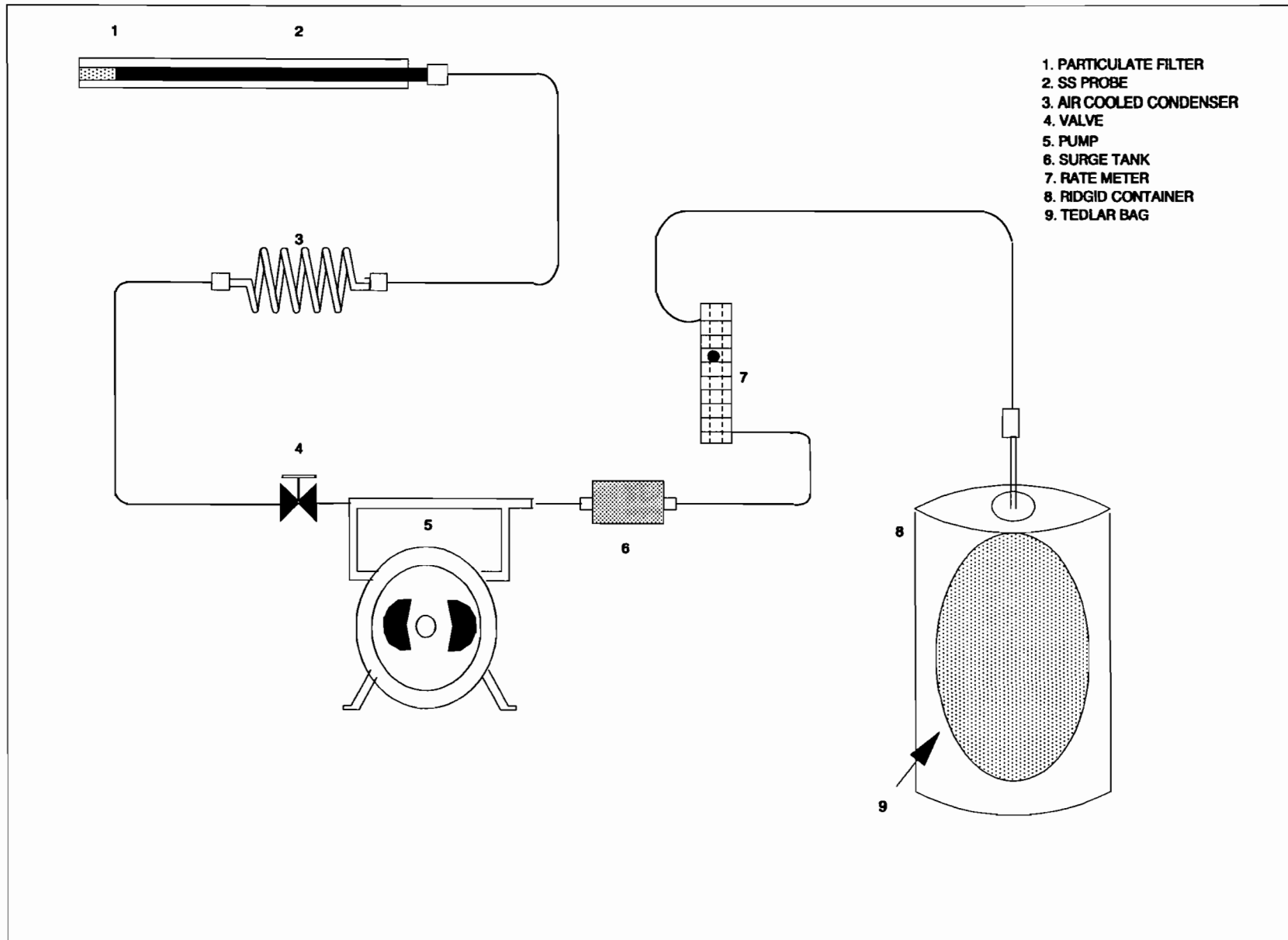


FIGURE 4  
INTEGRATED GAS SAMPLING TRAIN  
USEPA METHOD 3-B

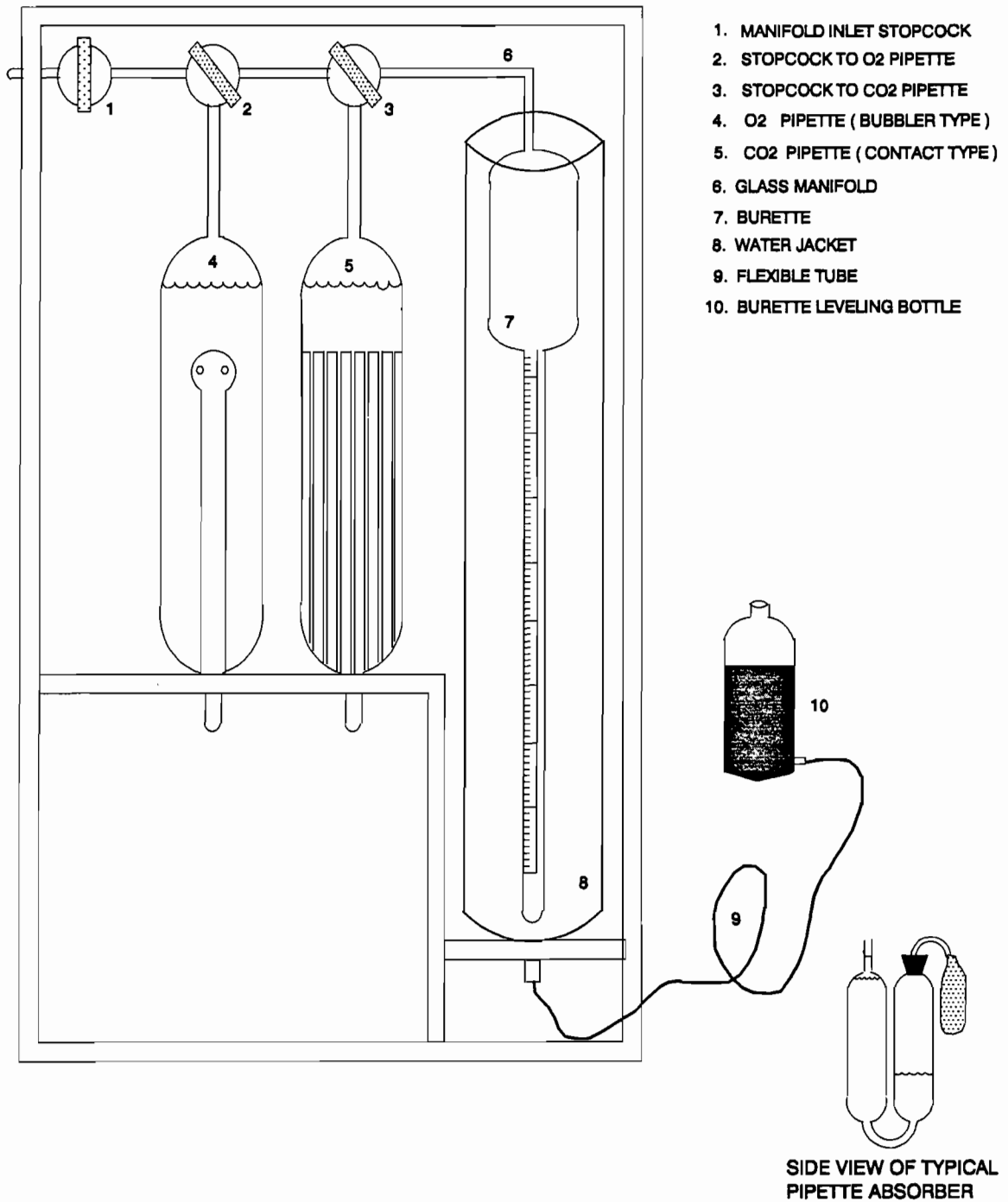


FIGURE 5  
 ORSAT ANALYZER  
 USEPA METHOD 3B

**TAMPA**  
**ELECTRIC**  
 A TECO ENERGY COMPANY

## 4.0 SUMMARY OF RESULTS

Section 4.1 presents the Continuous Emission Monitor Data from the baseline stack test and the fuel blend stack test. Data is presented comparing opacity, SO<sub>2</sub>, NO<sub>x</sub>, during baseline and fuel blend burn stack tests. The test data is summarized below.

F.J. GANNON STATION UNIT NO. 3 CONTINUOUS EMISSION MONITOR DATA			
PARAMETER	BASELINE	TIRE DERIVED FUEL	EMISSION RATE
Opacity	5	3	(%)
SO <sub>2</sub>	2.0	2.0	(LB/MMBtu)
NO <sub>x</sub>	1.32	1.16	(LB/MMBtu)

Section 4.2 presents stack test data from the baseline test and the fuel blend test burn. Data is presented comparing particulate, sulfuric acid mist, and visible emissions test data.

F.J. GANNON STATION UNIT NO. 3 STACK TEST DATA			
PARAMETER	BASELINE	TIRE DERIVED FUEL	EMISSION RATE
Particulate	0.03	0.03	(LB/MMBtu)
H <sub>2</sub> SO <sub>4</sub>	0.01	0.01	(LB/MMBtu)
V.E.	5	0	(%)

Section 4.3 presents the fuel sampling and analysis of weekly coal composites taken during the baseline and TDF blend test burn. Analysis of TDF samples taken during fuel bunkering for each stack test day is also included.

## 4.1 CEM DATA

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F.J. GANNON STATION UNIT NO. 3  
CONTINUOUS EMISSION MONITOR DATA DURING STACK TESTS\*  
BASELINE TEST BURN  
FEBRUARY 28, 1996  
TIRE DERIVED FUEL BLEND  
APRIL 23, 1996

**SO2 (lb/MMBtu)**

BASELINE VS FUEL BLEND

	DATE	TIME	AVG
BASELINE TESTS	02/28/96	0700-1800	2.0

	DATE	TIME	AVG
TIRE DERIVED FUEL BLEND	04/23/96	0800-1700	2.0

\* CONTINUOUS EMISSION MONITOR DATA CORRESPONDS TO STACK TEST DAYS AND TIME

TABLE 4.1.1

**F.J. GANNON STATION UNIT NO. 3**  
**CONTINUOUS EMISSION MONITOR DATA DURING STACK TESTS\***  
**BASELINE TEST BURN**  
**FEBRUARY 28, 1996**  
**TIRE DERIVED FUEL BLEND**  
**APRIL 23, 1996**

**NO<sub>x</sub> (lb/MMBtu)**

BASELINE VS FUEL BLEND

	DATE	TIME	AVG
BASELINE TESTS	02/28/96	0700-1800	1.32
	DATE	TIME	AVG
TIRE DERIVED FUEL BLEND	04/23/96	0800-1700	1.16

\* CONTINUOUS EMISSION MONITOR DATA CORRESPONDS TO STACK TEST DAYS AND TIME

TABLE 4.1.2

**F.J. GANNON STATION UNIT NO. 3**  
**CONTINUOUS EMISSION MONITOR DATA DURING STACK TESTS\***  
**BASELINE TEST BURN**  
**FEBRUARY 28, 1996**  
**TIRE DERIVED FUEL BLEND**  
**APRIL 23, 1996**

**OPACITY (%)**

BASELINE VS FUEL BLEND

	DATE	TIME	AVG
BASELINE TESTS	02/28/96	0700-1800	5

	DATE	TIME	AVG
TIRE DERIVED FUEL BLEND	04/23/96	0800-1700	3

\* CONTINUOUS EMISSION MONITOR DATA CORRESPONDS TO STACK TEST DAYS AND TIME

TABLE 4.1.3

## 4.2 STACK TEST DATA

---



F.J. GANNON STATION UNIT NO. 3  
 STACK TEST DATA  
 BASELINE TEST BURN  
 FEBRUARY 28, 1996  
 TIRE DERIVED FUEL BLEND  
 APRIL 23, 1996

<b>PARTICULATE (Lb/MMBtu)</b> U.S. EPA METHOD 17		BASELINE VS FUEL BLEND			
RUN	1	2	3	AVG.	
BASELINE TESTS	0.027	0.026	0.025	0.026	
TIRE DERIVED FUEL BLEND	0.023	0.030	0.024	0.026	

<b>SULFURIC ACID MIST (Lb/MMBtu)</b> U.S. EPA METHOD 8		BASELINE VS FUEL BLEND			
RUN	1	2	3	AVG.	
BASELINE TESTS	0.015	0.012	0.010	0.012	
TIRE DERIVED FUEL BLEND	0.012	0.008	0.006	0.009	

TABLE 4.2.1

F.J. GANNON STATION UNIT NO. 3  
STACK TEST DATA  
BASELINE TEST BURN  
FEBRUARY 28, 1996  
TIRE DERIVED FUEL BLEND  
APRIL 23, 1996

<b>VISIBLE EMISSIONS (%)</b>		BASELINE VS FUEL BLEND
U.S. EPA METHOD 9		
60 MINUTE TEST		AVG.
BASELINE TESTS		5
TIRE DERIVED FUEL BLEND		0

TABLE 4.2.2

### 4.3 FUEL ANALYSIS DATA

---

**F. J. GANNON STA UNIT NO. 3**  
**TRACE METALS FUEL ANALYSIS**  
**WEEKLY COMPOSITE BASELINE**  
**FEBRUARY 26, 1996 THRU MARCH 3, 1996**  
**WEEKLY COMPOSITE FUEL BLEND**  
**APRIL 22, 1996 THRU APRIL 28, 1996**  
**TIRE DERIVED FUEL STACK TEST BUNKERING**  
**APRIL 22, 1996**

**VANADIUM (ug/g)**  
**ASTM D 3683-78 (REAPPROVED 1989)**  
**EPA 200.7**

SAMPLE DESCRIPTION	SAMPLE DATES	RESULTS
BASELINE TESTS PERIOD / WEEKLY COAL COMPOSITE (BLWCC)	02-26-96 THRU 03-03-96	17 ug/g
FUEL BLEND TEST PERIOD / WEEKLY COAL COMPOSITE (FBWCC)	04-22-96 THRU 04-28-96	17 ug/g
TIRE DERIVED FUEL / TDF DURING BUNKERING (TDF)	04-22-96	9 ug/g
CALCULATED FUEL BLEND = ((ug/g) * 80%(FBWCC)) + ((ug/g * 20%(TDF))		15 ug/g

**NICKEL (ug/g)**  
**ASTM D 3683-78 (REAPPROVED 1989)**  
**EPA 200.7**

SAMPLE DESCRIPTION	SAMPLE DATES	RESULTS
BASELINE TESTS PERIOD / WEEKLY COAL COMPOSITE (BLWCC)	02-26-96 THRU 03-03-96	9 ug/g
FUEL BLEND TEST PERIOD / WEEKLY COAL COMPOSITE (FBWCC)	04-22-96 THRU 04-28-96	9 ug/g
TIRE DERIVED FUEL / TDF DURING BUNKERING (TDF)	04-22-96	19 ug/g
CALCULATED FUEL BLEND = ((ug/g) * 80%(FBWCC)) + ((ug/g * 20%(TDF))		11 ug/g

(BLWCC)=BASELINE WEEKLY COAL COMPOSITE  
 (FBWCC) = FUEL BLEND WEEKLY COAL COMPOSITE - COAL ONLY  
 (TDF) = TIRE DERIVED FUEL

TABLE 4.3.1

**F. J. GANNON STATION UNIT NO. 3**  
**TRACE METALS FUEL ANALYSIS**  
**WEEKLY COMPOSITE BASELINE**  
**FEBRUARY 26, 1996 THRU MARCH 3, 1996**  
**WEEKLY COMPOSITE FUEL BLEND**  
**APRIL 22, 1996 THRU APRIL 28, 1996**  
**TIRE DERIVED FUEL STACK TEST BUNKERING**  
**APRIL 22, 1996**

**BERYLLIUM (ug/g)**  
**ASTM D 3683-78 (REAPPROVED 1989)**  
**EPA 200.7**

SAMPLE DESCRIPTION	SAMPLE DATES	RESULTS
BASELINE TESTS PERIOD / WEEKLY COAL COMPOSITE (BLWCC)	02-26-96 THRU 03-03-96	1 ug/g
FUEL BLEND TEST PERIOD / WEEKLY COAL COMPOSITE (FBWCC)	04-22-96 THRU 04-28-96	1 ug/g
TIRE DERIVED FUEL / TDF DURING BUNKERING (TDF)	04-22-96	3 ug/g
CALCULATED FUEL BLEND = ((ug/g) * 80%(FBWCC)) + ((ug/g * 20%(TDF))		1 ug/g

**LEAD (ug/g)**  
**ASTM D 3683-78 (REAPPROVED 1989)**  
**EPA 200.7**

SAMPLE DESCRIPTION	SAMPLE DATES	RESULTS
BASELINE TESTS PERIOD / WEEKLY COAL COMPOSITE (BLWCC)	02-26-96 THRU 03-03-96	13 ug/g
FUEL BLEND TEST PERIOD / WEEKLY COAL COMPOSITE (FBWCC)	04-22-96 THRU 04-28-96	6 ug/g
TIRE DERIVED FUEL / TDF DURING BUNKERING (TDF)	04-22-96	21 ug/g
CALCULATED FUEL BLEND = ((ug/g) * 80%(FBWCC)) + ((ug/g * 20%(TDF))		9 ug/g

(BLWCC)=BASELINE WEEKLY COAL COMPOSITE  
 (FBWCC) = FUEL BLEND WEEKLY COAL COMPOSITE - COAL ONLY  
 (TDF) = TIRE DERIVED FUEL

TABLE 4.3.2

**F. J. GANNON STA UNIT NO. 3**  
**TRACE METALS FUEL ANALYSIS**  
**WEEKLY COMPOSITE BASELINE**  
**FEBRUARY 26, 1996 THRU MARCH 3, 1996**  
**WEEKLY COMPOSITE FUEL BLEND**  
**APRIL 22, 1996 THRU APRIL 28, 1996**  
**TIRE DERIVED FUEL STACK TEST BUNKERING**  
**APRIL 22, 1996**

**MERCURY (ug/g)**  
**ASTM D 3684-94 (REAPPROVED 1994) (COAL)**  
**DOUBLE GOLD AMALGAMATION, COLD VAPOR ATOMIC ABSORPTION (TDF)**

SAMPLE DESCRIPTION	SAMPLE DATES	RESULTS
BASELINE TESTS PERIOD / WEEKLY COAL COMPOSITE (BLWCC)	02-26-96 THRU 03-03-96	0.09 ug/g
FUEL BLEND TEST PERIOD / WEEKLY COAL COMPOSITE (FBWCC)	04-22-96 THRU 04-28-96	0.10 ug/g
TIRE DERIVED FUEL / TDF DURING BUNKERING (TDF)	04-22-96	0.04 ug/g
CALCULATED FUEL BLEND = ((ug/g) * 80%(FBWCC)) + ((ug/g * 20%(TDF))		0.09 ug/g

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(BLWCC)=BASELINE WEEKLY COAL COMPOSITE  
 (FBWCC) = FUEL BLEND WEEKLY COAL COMPOSITE - COAL ONLY  
 (TDF) = TIRE DERIVED FUEL

TABLE 4.3.4

**F. J. GANNON STA UNIT NO. 3**  
**TRACE METALS FULL ANALYSIS**  
**WEEKLY COMPOSITE BASELINE**  
**FEBRUARY 26, 1996 THRU MARCH 3, 1996**  
**WEEKLY COMPOSITE FUEL BLEND**  
**APRIL 22, 1996 THRU APRIL 28, 1996**  
**TIRE DERIVED FUEL STACK TEST BUNKERING**  
**APRIL 22, 1996**

**CHROMIUM (ug/g)**  
**ASTM D 3683-78 (REAPPROVED 1989)**  
**EPA 200.7**

SAMPLE DESCRIPTION	SAMPLE DATES	RESULTS
BASELINE TESTS PERIOD / WEEKLY COAL COMPOSITE (BLWCC)	02-26-96 THRU 03-03-96	8 ug/g
FUEL BLEND TEST PERIOD / WEEKLY COAL COMPOSITE (FBWCC)	04-22-96 THRU 04-28-96	7 ug/g
TIRE DERIVED FUEL / TDF DURING BUNKERING (TDF)	04-22-96	9 ug/g
CALCULATED FUEL BLEND = ((ug/g) * 80%(FBWCC)) + ((ug/g * 20%(TDF))		7 ug/g

**ZINC (ug/g)**  
**ASTM D 3683-78 (REAPPROVED 1989)**  
**EPA 200.7**

SAMPLE DESCRIPTION	SAMPLE DATES	RESULTS
BASELINE TESTS PERIOD / WEEKLY COAL COMPOSITE (BLWCC)	02-26-96 THRU 03-03-96	25 ug/g
FUEL BLEND TEST PERIOD / WEEKLY COAL COMPOSITE (FBWCC)	04-22-96 THRU 04-28-96	25 ug/g
TIRE DERIVED FUEL / TDF DURING BUNKERING (TDF)	04-22-96	4327 ug/g
CALCULATED FUEL BLEND = ((ug/g) * 80%(FBWCC)) + ((ug/g * 20%(TDF))		886 ug/g

(BLWCC)=BASELINE WEEKLY COAL COMPOSITE  
 (FBWCC) = FUEL BLEND WEEKLY COAL COMPOSITE - COAL ONLY  
 (TDF) = TIRE DERIVED FUEL

TABLE 4.3.3

#### **4.4 UNIT OPERATIONS SUMMARY**

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Boiler performance was not noticeably affected by the TDF blend. No measurable differences were observed in overall boiler operation. Extensive daily records exist for the baseline and TDF test burn. The records are available for inspection at the station but are not included because of the quantity of the material. Appendix C - Boiler Precipitator Operation data shows records from all stack tests performed during the test burn. These records include unit load, fuel ratio, and operating conditions.



## **APPENDIX A**

### **SOURCE TEST CALCULATIONS**

- A-1 BASELINE PARTICULATE CALCULATIONS**
- A-2 BASELINE SULFURIC ACID MIST CALCULATIONS**
- A-3 FUEL BLEND BURN PARTICULATE CALCULATIONS**
- A-4 FUEL BLEND BURN SULFURIC ACID MIST CALCULATIONS**
- A-5 NOMENCLATURE**

## **A-1 BASELINE PARTICULATE CALCULATIONS**

U.S. EPA  
PARTICULATE CALCULATIONS  
RUN NO. 1

PLANT : F. J. GANNON STATION  
DATE : 2-28-96  
SAMP. LOCATION : BOILER NO. 3  
OPERATING COND.: BASELINE /SOOTBLOWING

SAMPLE TIME =	60.0 min.		NOZZLE DIA. =	0.198 in.
BAR. PRESSURE =	29.80 in.Hg		NOZZLE AREA =	0.000214 Sq.Ft.
STK. PRESSURE =	29.80 in.Hg		METER ORIFICE =	1.064 in. H2O
EFF. STACK AREA =	121.23 Sq.Ft.		METER VOLUME =	33.249 Cu.Ft.
Cp =	0.84		METER TEMP. =	80.2 DEG. F
GAS ANALYSIS =	13.8 % CO2		STACK TEMP. =	279.6 DEG. F
	5.0 % O2		SQ.RT. dP =	1.007 in. H2O
	0.0 % CO		CONDENSATE VOL.=	57.7 ml
	81.2 % N2		METER Y =	1.013
LAB ANALYSIS =	0.03080 grams		F-FACTOR =	9780 dscf/MMBtu
*****				

Vw(std) = 0.04714 x Vic	=	2.720	scf
Vm(std) = 17.647 x Vm x Y x (Pb + (dH / 13.6)) / (Tm + 460)	=	32.861	scf
Bws = Vw(std) / (Vm(std) + Vw(std))	=	0.076	%
FDA = 1.0 - Bws	=	0.924	%
Md = (.44 x %CO2) + (.32 x %O2) + [.28 x (%N2 + %CO)]	=	30.41	lb\lb-mole
Ms = (Md x FDA) + (18.0 x Bws)	=	29.47	lb\lb-mole
vs = 85.49 x CP x (Sq.Rt.dP) x [Sq.Rt.(Ts+460) / (Ms x Ps)]	=	66.4	ft/sec
Qs = vs x As x 60	=	482960	acf/min
Qs(std) = Qs x FDA x (528 / (Ts + 460)) x (Ps / 29.92)	=	317325	dscf/min
I = (Ts + 460) x [(0.00267 x Vic) + (Vm(std) / 17.647)] x 100 / (Time x Ps x An x vs x 60)	=	97.9	%
*****			
cs = 15.432 x grams / Vm(std)	=	0.0145	grains/dscf
grains/acf = cs x 17.647 x Ps x FDA / (Ts + 460)	=	0.0095	grains/acf
C = cs / 7000	=	2.07E-06	lbs/dscf
EM = C x Qs(std) x 60	=	39.4	lbs/hr
E = C x F x (20.9 / 20.9 - %O2) F-Factor method	=	0.027	lbs/MM Btu

U.S. EPA  
PARTICULATE CALCULATIONS  
RUN NO. 2

PLANT : F. J. GANNON STATION  
DATE : 2-28-96  
SAMP. LOCATION : BOILER NO. 3  
OPERATING COND.: BASELINE /SOOTBLOWING

SAMPLE TIME =	60.0 min.	NOZZLE DIA. =	0.198 in.
BAR. PRESSURE =	29.80 in.Hg	NOZZLE AREA =	0.000214 Sq.Ft.
STK. PRESSURE =	29.80 in.Hg	METER ORIFICE =	1.079 in. H2O
EFF. STACK AREA =	121.23 Sq.Ft.	METER VOLUME =	33.369 Cu.Ft.
Cp =	0.84	METER TEMP. =	81.5 DEG. F
GAS ANALYSIS =	13.8 % CO2	STACK TEMP. =	281.3 DEG. F
	5.2 % O2	SQ.RT. dP =	1.014 in. H2O
	0.0 % CO	CONDENSATE VOL.=	67.7 ml
	81.0 % N2	METER Y =	1.013
LAB ANALYSIS =	0.02980 grams	F-FACTOR =	9780 dscf/MMBtu
*****	*****	*****	*****

Vw(std) = 0.04714 x Vic	=	3.191	scf
Vm(std) = 17.647 x Vm x Y x (Pb + (dH / 13.6)) / (Tm + 460)	=	32.902	scf
Bws = Vw(std) / (Vm(std) + Vw(std))	=	0.088	%
FDA = 1.0 - Bws	=	0.912	%
Md = (.44 x %CO2) + (.32 x %O2) + [.28 x (%N2 + %CO)]	=	30.42	lb\lb-mole
Ms = (Md x FDA) + (18.0 x Bws)	=	29.33	lb\lb-mole
vs = 85.49 x CP x (Sq.Rt.dP) x [Sq.Rt.(Ts+460)] / (Ms x Ps)	=	67.0	ft/sec
Qs = vs x As x 60	=	487325	acf/min
Qs(std)=Qs x FDA x (528/(Ts + 460)) x (Ps/29.92)	=	315288	dscf/min
I = (Ts + 460) x [(0.00267 x Vic) + (Vm(std) / 17.647)] x 100 / (Time x Ps x An x vs x 60)	=	98.6	%
*****	*****	*****	*****
cs = 15.432 x grams / Vm(std)	=	0.0140	grains/dscf
grains/acf = cs x 17.647 x Ps x FDA / (Ts + 460)	=	0.0091	grains/acf
C = cs / 7000	=	2.00E-06	lbs/dscf
EM = C x Qs(std) x 60	=	37.8	lbs/hr
E = C x F x (20.9 / 20.9 - %O2) F-Factor method	=	0.026	lbs/MM Btu

U.S. EPA  
PARTICULATE CALCULATIONS  
RUN NO. 3

PLANT : F. J. GANNON STATION  
DATE : 2-28-96  
SAMP. LOCATION : BOILER NO. 3  
OPERATING COND.: BASELINE /SOOTBLOWING

SAMPLE TIME =	60.0 min.	NOZZLE DIA. =	0.198 in.
BAR. PRESSURE =	29.80 in.Hg	NOZZLE AREA =	0.000214 Sq.Ft.
STK. PRESSURE =	29.80 in.Hg	METER ORIFICE =	1.027 in. H2O
EFF. STACK AREA =	121.23 Sq.Ft.	METER VOLUME =	32.980 Cu.Ft.
Cp =	0.84	METER TEMP. =	82.3 DEG. F
GAS ANALYSIS =	13.2 % CO2	STACK TEMP. =	279.7 DEG. F
	5.6 % O2	SQ.RT. dP =	0.989 in. H2O
	0.0 % CO	CONDENSATE VOL.=	67.7 ml
	81.2 % N2	METER Y =	1.013
LAB ANALYSIS =	0.02785 grams	F-FACTOR =	9780 dscf/MMBtu
*****	*****	*****	*****

$V_w(\text{std}) = 0.04714 \times V_{ic}$	=	3.191	scf
$V_m(\text{std}) = 17.647 \times V_m \times Y \times (P_b + (dH / 13.6)) / (T_m + 460)$	=	32.469	scf
$B_{ws} = V_w(\text{std}) / (V_m(\text{std}) + V_w(\text{std}))$	=	0.089	%
$FDA = 1.0 - B_{ws}$	=	0.911	%
$M_d = (.44 \times \%CO_2) + (.32 \times \%O_2) + [.28 \times (\%N_2 + \%CO)]$	=	30.34	lb\lb-mole
$M_s = (M_d \times FDA) + (18.0 \times B_{ws})$	=	29.24	lb\lb-mole
$v_s = 85.49 \times CP \times (Sq.Rt.dP) \times [Sq.Rt.(T_s+460) / (M_s \times P_s)]$	=	65.4	ft/sec
$Q_s = v_s \times A_s \times 60$	=	475687	acf/min
$Q_s(\text{std}) = Q_s \times FDA \times (528 / (T_s + 460)) \times (P_s / 29.92)$	=	308107	dscf/min
$I = (T_s + 460) \times [(0.00267 \times V_{ic}) + (V_m(\text{std}) / 17.647)] \times 100 / (Time \times P_s \times A_n \times v_s \times 60)$	=	99.6	%
*****	*****	*****	*****
$cs = 15.432 \times \text{grams} / V_m(\text{std})$	=	0.0132	grains/dscf
$\text{grains/acf} = cs \times 17.647 \times P_s \times FDA / (T_s + 460)$	=	0.0085	grains/acf
$C = cs / 7000$	=	1.89E-06	lbs/dscf
$EM = C \times Q_s(\text{std}) \times 60$	=	34.9	lbs/hr
$E = C \times F \times (20.9 / 20.9 - \%O_2)$ F-Factor method	=	0.025	lbs/MM Btu

## A-2 BASELINE SULFURIC ACID MIST CALCULATIONS

U.S. EPA METHOD EIGHT  
SULFURIC ACID MIST TEST CALCULATIONS  
RUN NO. 1-S

PLANT : F.J. GANNON STATION  
DATE : 2-28-96  
SAMP. LOCATION : BOILER NO. 3  
OPERATING COND.: BASELINE /SOOTBLOWING

SAMPLE TIME =	60.0 min.	NOZZLE DIA. =	0.198 in.
BAR. PRESSURE =	29.80 in.Hg	NOZZLE AREA =	0.00021382 Sq.Ft.
STK. PRESSURE =	29.80 in.Hg	METER ORIFICE =	0.971 in. H2O
EFF. STACK AREA =	121.23 Sq.Ft.	METER VOLUME =	33.416 Cu.Ft.
Cp =	0.84	METER TEMP. =	78.3 DEG. F
GAS ANALYSIS =	12.8 % CO2	STACK TEMP. =	263.6 DEG. F
	6.0 % O2	SQ.RT. dP =	1.000 in. H2O
	0.0 % CO	CONDENSATE VOL.=	75.5 ml
	81.2 % N2	METER Y =	1.000
LAB ANALYSIS =	0.00000 grams	HEAT INPUT =	*** MM Btu/hr
		F-FACTOR =	9780 dscf/MMBtu

\*\*\*\*\*

$V_w(\text{std}) = 0.04714 \times V_{ic}$	=	3.559	scf
$V_m(\text{std}) = 17.647 \times V_m \times Y \times (P_b + (dH / 13.6)) / (T_m + 460)$	=	32.710	scf
$B_{ws} = V_w(\text{std}) / (V_m(\text{std}) + V_w(\text{std}))$	=	0.098	%
$FDA = 1.0 - B_{ws}$	=	0.902	%
$M_d = (.44 \times \%CO_2) + (.32 \times \%O_2) + [.28 \times (\%N_2 + \%CO)]$	=	30.29	lb/lb mole
$M_s = (M_d \times FDA) + (18.0 \times B_{ws})$	=	29.09	lb/lb mole
$v_s = 85.49 \times CP \times (Sq.Rt.dP) \times [Sq.Rt.(T_s+460) / (M_s \times P_s)]$	=	65.6	ft/sec
$Q_s = v_s \times A_s \times 60$	=	477142	acf/min
$Q_s(\text{std}) = Q_s \times FDA \times (528 / (T_s + 460)) \times (P_s / 29.92)$	=	312784	dscf/min
$I = (T_s + 460) \times [(0.00267 \times V_{ic}) + (V_m(\text{std}) / 17.647)] \times 100 / (Time \times P_s \times A_n \times v_s \times 60)$	=	98.8	%
*****			
$N = \text{NORMALITY OF BaBI}_2 \cdot 2H_2O$	=	0.0103	
$T_b = \text{TITRANT BLANK}$	=	0.0600	milliliters
$V_s = \text{VOLUME SOLUTION}$	=	5.05E+02	milliliters
$V_a = \text{VOLUME ALIQUOT}$	=	100.0	milliliters
$T = \text{TITRANT}$	=	6.32	milliliters
$H_2SO_4 \text{ (lb/dscf)} = 0.0001081 \times (N \times (T - T_b) \times V_s / V_a) / V_m$	=	0.00000108	lb/dscf
$H_2SO_4 \text{ (g/dscm)} = 0.04904 \times (N \times (T - T_b) \times V_s / V_a) / V_m$	=	0.0172	g/dscm
$H_2SO_4 \text{ (lb/MMBtu)}$	=	0.0148	lb/MMBtu

U.S. EPA METHOD EIGHT  
SULFURIC ACID MIST TEST CALCULATIONS  
RUN NO. 2-S

PLANT : F.J. GANNON STATION  
DATE : 2-28-96  
SAMP. LOCATION : BOILER NO. 3  
OPERATING COND.: BASELINE /SOOTBLOWING

SAMPLE TIME =	60.0 min.	NOZZLE DIA. =	0.198 in.
BAR. PRESSURE =	29.80 in.Hg	NOZZLE AREA =	0.00021382 Sq.Ft.
STK. PRESSURE =	29.80 in.Hg	METER ORIFICE =	0.983 in. H2O
EFF. STACK AREA =	121.23 Sq.Ft.	METER VOLUME =	33.923 Cu.Ft.
Cp =	0.84	METER TEMP. =	80.5 DEG. F
GAS ANALYSIS =	13.8 % CO2	STACK TEMP. =	267.4 DEG. F
	5.3 % O2	SQ.RT. dP =	0.989 in. H2O
	0.0 % CO	CONDENSATE VOL.=	72.3 ml
	80.9 % N2	METER Y =	1.000
LAB ANALYSIS =	0.00000 grams	HEAT INPUT =	*** MM Btu/hr
		F-FACTOR =	9780 dscf/MMBtu
*****	*****	*****	*****

$V_w(\text{std}) = 0.04714 \times V_{ic}$	=	3.408	scf
$V_m(\text{std}) = 17.647 \times V_m \times Y \times (P_b + (dH / 13.6)) / (T_m + 460)$	=	33.075	scf
		0.937	scm
$B_{ws} = V_w(\text{std}) / (V_m(\text{std}) + V_w(\text{std}))$	=	0.093	%
$FDA = 1.0 - B_{ws}$	=	0.907	%
$M_d = (.44 \times \%CO_2) + (.32 \times \%O_2) + [.28 \times (\%N_2 + \%CO)] =$		30.42	lb/lb mole
$M_s = (M_d \times FDA) + (18.0 \times B_{ws})$	=	29.26	lb/lb mole
$v_s = 85.49 \times CP \times (Sq.Rt.dP) \times [Sq.Rt.(T_s+460) / (M_s \times P_s)]$	=	64.9	ft/sec
$Q_s = v_s \times A_s \times 60$	=	472050	acf/min
$Q_s(\text{std}) = Q_s \times FDA \times (528 / (T_s + 460)) \times (P_s / 29.92) =$		309536	dscf/min
$I = (T_s + 460) \times [(0.00267 \times V_{ic}) + (V_m(\text{std}) / 17.647)] \times 100 / (Time \times P_s \times A_n \times v_s \times 60)$	=	101.0	%
*****	*****	*****	*****

$N = \text{NORMALITY OF BaBI2} \cdot 2H_2O$	=	0.0103	
$T_b = \text{TITRANT BLANK}$	=	0.0600	milliliters
$V_s = \text{VOLUME SOLUTION}$	=	5.60E+02	milliliters
$V_a = \text{VOLUME ALIQUOT}$	=	100.0	milliliters
$T = \text{TITRANT}$	=	4.08	milliliters
$H_2SO_4 \text{ (lb/dscf)} = 0.0001081 \times (N \times (T - T_b) \times V_s / V_a) / V_m$	=	0.00000076	lb/dscf
$H_2SO_4 \text{ (g/dscm)} = 0.04904 \times (N \times (T - T_b) \times V_s / V_a) / V_m$	=	0.0121	g/dscm
$H_2SO_4 \text{ (lb/MMBtu)}$		0.0099	lb/MMBtu



U.S. EPA METHOD EIGHT  
SULFURIC ACID MIST TEST CALCULATIONS  
RUN NO. 3-S

PLANT : F.J. GANNON STATION  
DATE : 2-28-96  
SAMP. LOCATION : BOILER NO. 3  
OPERATING COND.: BASELINE /SOOTBLOWING

SAMPLE TIME =	60.0 min.	NOZZLE DIA. =	0.198 in.
BAR. PRESSURE =	29.80 in.Hg	NOZZLE AREA =	0.00021382 Sq.Ft.
STK. PRESSURE =	29.80 in.Hg	METER ORIFICE =	0.983 in. H2O
EFF. STACK AREA =	121.23 Sq.Ft.	METER VOLUME =	33.756 Cu.Ft.
Cp =	0.84	METER TEMP. =	89.4 DEG. F
GAS ANALYSIS =	13.2 % CO2	STACK TEMP. =	267.5 DEG. F
	5.2 % O2	SQ.RT. dP =	0.991 in. H2O
	0.0 % CO	CONDENSATE VOL.=	71.6 ml
	81.6 % N2	METER Y =	1.000
LAB ANALYSIS =	0.00000 grams	HEAT INPUT =	*** MM Btu/hr
		F-FACTOR =	9780 dscf/MMBtu

Vw(std) = 0.04714 x Vic	=	3.375	scf
Vm(std) = 17.647 x Vm x Y x (Pb + (dH / 13.6)) / (Tm + 460)	=	32.379	scf
Bws = Vw(std) / (Vm(std) + Vw(std))	=	0.094	%
FDA = 1.0 - Bws	=	0.906	%
Md = (.44 x %CO2)+(.32 x %O2)+[.28 x (%N2 + %CO)] =	=	30.32	lb/lb mole
Ms = (Md x FDA) + (18.0 x Bws)	=	29.16	lb/lb mole
vs = 85.49 x CP x (Sq.Rt.dP) x [Sq.Rt.(Ts+460) / (Ms x Ps)]	=	65.1	ft/sec
Qs = vs x As x 60	=	473505	acf/min
Qs(std)=Qs x FDA x (528/(Ts + 460)) x (Ps/29.92) =	=	310126	dscf/min
I = (Ts + 460) x [(0.00267 x Vic) + (Vm(std) / 17.647)] x 100 / (Time x Ps x An x vs x 60)	=	98.7	%

N = NORMALITY OF BaBi2 * 2H2O	=	0.0103	
Tb = TITRANT BLANK	=	0.0600	milliliters
Vs = VOLUME SOLUTION	=	6.69E+02	milliliters
Va = VOLUME ALIQUOT	=	100.0	milliliters
T = TITRANT	=	3.25	milliliters
H2SO4 (lb/dscf) = 0.0001081 x (N x (T-Tb) x Vs/Va)/Vm	=	0.00000073	lb/dscf
H2SO4 (g/dscm) = 0.04904 x (N x (T-Tb) x Vs/Va)/Vm	=	0.0118	g/dscm
H2SO4 (lb/MMBtu)	=	0.0096	lb/MMBtu

**A-3 FUEL BLEND BURN PARTICULATE CALCULATIONS**

U.S. EPA  
PARTICULATE CALCULATIONS  
RUN NO. 1-S

PLANT : F. J. GANNON  
DATE : 4-23-96  
SAMP. LOCATION : BOILER NO. 3  
OPERATING COND.: TDF TEST BLEND/ SOOTBLOWING

SAMPLE TIME = 60.0 min.	NOZZLE DIA. = 0.212 in.
BAR. PRESSURE = 30.05 in.Hg	NOZZLE AREA = 0.000245 Sq.Ft.
STK. PRESSURE = 30.05 in.Hg	METER ORIFICE = 1.265 in. H2O
EFF. STACK AREA = 122.72 Sq.Ft.	METER VOLUME = 38.748 Cu.Ft.
Cp = 0.84	METER TEMP. = 89.3 DEG. F
GAS ANALYSIS = 12.6 % CO2	STACK TEMP. = 279.2 DEG. F
5.9 % O2	SQ.RT. dP = 0.972 in. H2O
0.0 % CO	CONDENSATE VOL.= 64.2 ml
81.8 % N2	METER Y = 1.000
LAB ANALYSIS = 0.02825 grams	F-FACTOR = 9780 dscf/MMBtu
*****	

Vw(std) = 0.04714 x Vic	=	3.026	scf
Vm(std) = 17.647 x Vm x Y x (Pb + (dH / 13.6)) / (Tm + 460)	=	37.512	scf
Bws = Vw(std) / (Vm(std) + Vw(std))	=	0.075	%
FDA = 1.0 - Bws	=	0.925	%
Md = (.44 x %CO2) + (.32 x %O2) + [.28 x (%N2 + %CO)]	=	30.34	lb\lb-mole
Ms = (Md x FDA) + (18.0 x Bws)	=	29.41	lb\lb-mole
vs = 85.49 x CP x (Sq.Rt.dP) x [Sq.Rt.(Ts+460)] / (Ms x Ps)	=	63.8	ft/sec
Qs = vs x As x 60	=	469765	acf/min
Qs(std)=Qs x FDA x (528/(Ts + 460)) x (Ps/29.92)	=	311750	dscf/min
I = (Ts + 460) x [(0.00267 x Vic) + (Vm(std) / 17.647)] x 100 / (Time x Ps x An x vs x 60)	=	100.4	%
*****			
cs = 15.432 x grams / Vm(std)	=	0.0116	grains/dscf
grains/acf = cs x 17.647 x Ps x FDA / (Ts + 460)	=	0.0077	grains/acf
C = cs / 7000	=	1.66E-06	lbs/dscf
EM = C x Qs(std) x 60	=	31.0	lbs/hr
E = C x F x (20.9 / 20.9 - %O2) F-Factor method	=	0.023	lbs/MM Btu

U.S. EPA  
PARTICULATE CALCULATIONS  
RUN NO. 2-S

PLANT : F. J. GANNON  
DATE : 4-23-96  
SAMP. LOCATION : BOILER NO. 3  
OPERATING COND.: TDF TEST BLEND/ SOOTBLOWING

SAMPLE TIME =	60.0 min.		NOZZLE DIA. =	0.212 in.
BAR. PRESSURE =	29.98 in.Hg		NOZZLE AREA =	0.000245 Sq.Ft.
STK. PRESSURE =	29.98 in.Hg		METER ORIFICE =	1.258 in. H2O
EFF. STACK AREA =	122.72 Sq.Ft.		METER VOLUME =	38.450 Cu.Ft.
Cp =	0.84		METER TEMP. =	87.2 DEG. F
GAS ANALYSIS =	12.3 % CO2		STACK TEMP. =	278.1 DEG. F
	6.3 % O2		SQ.RT. dP =	0.968 in. H2O
	0.0 % CO		CONDENSATE VOL.=	70.2 ml
	81.4 % N2		METER Y =	1.000
LAB ANALYSIS =	0.03595 grams		F-FACTOR =	9780 dscf/MMBtu
*****				

Vw(std) = 0.04714 x Vic	=	3.309	scf
Vm(std) = 17.647 x Vm x Y x (Pb + (dH / 13.6)) / (Tm + 460)	=	37.278	scf
Bws = Vw(std) / (Vm(std) + Vw(std))	=	0.082	%
FDA = 1.0 - Bws	=	0.918	%
Md = (.44 x %CO2) + (.32 x %O2) + [.28 x (%N2 + %CO)]	=	30.22	lb\lb-mole
Ms = (Md x FDA) + (18.0 x Bws)	=	29.22	lb\lb-mole
vs = 85.49 x CP x (Sq.Rt.dP) x [Sq.Rt.(Ts+460)] / (Ms x Ps)	=	63.8	ft/sec
Qs = vs x As x 60	=	469765	acf/min
Qs(std) = Qs x FDA x (528 / (Ts + 460)) x (Ps / 29.92)	=	309130	dscf/min
I = (Ts + 460) x [(0.00267 x Vic) + (Vm(std) / 17.647)] x 100 / (Time x Ps x An x vs x 60)	=	100.6	%
*****			
cs = 15.432 x grams / Vm(std)	=	0.0149	grains/dscf
grains/acf = cs x 17.647 x Ps x FDA / (Ts + 460)	=	0.0098	grains/acf
C = cs / 7000	=	2.13E-06	lbs/dscf
EM = C x Qs(std) x 60	=	39.5	lbs/hr
E = C x F x (20.9 / 20.9 - %O2) F-Factor method	=	0.030	lbs/MM Btu

U.S. EPA  
PARTICULATE CALCULATIONS  
RUN NO. 3-S

PLANT : F. J. GANNON  
DATE : 4-23-96  
SAMP. LOCATION : BOILER NO. 3  
OPERATING COND.: TDF TEST BLEND/ SOOTBLOWING

SAMPLE TIME =	60.0 min.		NOZZLE DIA. =	0.212 in.
BAR. PRESSURE =	30.05 in.Hg		NOZZLE AREA =	0.000245 Sq.Ft.
STK. PRESSURE =	30.05 in.Hg		METER ORIFICE =	1.841 in. H2O
EFF. STACK AREA =	122.72 Sq.Ft.		METER VOLUME =	39.301 Cu.Ft.
Cp =	0.84		METER TEMP. =	87.6 DEG. F
GAS ANALYSIS =	12.6 % CO2		STACK TEMP. =	278.3 DEG. F
	5.8 % O2		SQ.RT. dP =	0.967 in. H2O
	0.0 % CO		CONDENSATE VOL.=	72.4 ml
	81.6 % N2		METER Y =	1.000
LAB ANALYSIS =	0.03075 grams		F-FACTOR =	9780 dscf/MMBtu
*****	*****	*****	*****	*****

Vw(std) = 0.04714 x Vic	=	3.413	scf
Vm(std) = 17.647 x Vm x Y x (Pb + (dH / 13.6)) / (Tm + 460)	=	38.215	scf
Bws = Vw(std) / (Vm(std) + Vw(std))	=	0.082	%
FDA = 1.0 - Bws	=	0.918	%
Md = (.44 x %CO2) + (.32 x %O2) + [.28 x (%N2 + %CO)]	=	30.25	lb/lb-mole
Ms = (Md x FDA) + (18.0 x Bws)	=	29.25	lb/lb-mole
vs = 85.49 x CP x (Sq.Rt.dP) x [Sq.Rt.(Ts+460)] / (Ms x Ps)]	=	63.7	ft/sec
Qs = vs x As x 60	=	469028	acf/min
Qs(std) = Qs x FDA x (528 / (Ts + 460)) x (Ps / 29.92)	=	309282	dscf/min
I = (Ts + 460) x [(0.00267 x Vic) + (Vm(std) / 17.647)] x 100 / (Time x Ps x An x vs x 60)	=	103.1	%
*****	*****	*****	*****
cs = 15.432 x grams / Vm(std)	=	0.0124	grains/dscf
grains/acf = cs x 17.647 x Ps x FDA / (Ts + 460)	=	0.0082	grains/acf
C = cs / 7000	=	1.77E-06	lbs/dscf
EM = C x Qs(std) x 60	=	32.9	lbs/hr
E = C x F x (20.9 / 20.9 - %O2) F-Factor method	=	0.024	lbs/MM Btu

**A-4 FUEL BLEND BURN SULFURIC ACID MIST CALCULATIONS**

U.S. EPA METHOD EIGHT  
SULFURIC ACID MIST TEST CALCULATIONS  
RUN NO. 1-S

PLANT : F. J. GANNON  
DATE : 4-23-96  
SAMP. LOCATION : BOILER NO. 3  
OPERATING COND.: TDF TEST BLEND/ SOOTBLOWING

SAMPLE TIME =	60.0 min.	NOZZLE DIA. =	0.197 in.
BAR. PRESSURE =	30.00 in.Hg	NOZZLE AREA =	0.00021167 Sq.Ft.
STK. PRESSURE =	30.00 in.Hg	METER ORIFICE =	0.838 in. H2O
EFF. STACK AREA =	122.72 Sq.Ft.	METER VOLUME =	31.075 Cu.Ft.
Cp =	0.84	METER TEMP. =	81.1 DEG. F
GAS ANALYSIS =	10.4 % CO2	STACK TEMP. =	266.9 DEG. F
	5.1 % O2	SQ.RT. dP =	0.932 in. H2O
	0.0 % CO	CONDENSATE VOL.=	50.4 ml
	84.5 % N2	METER Y =	1.000
LAB ANALYSIS =	0.00000 grams	F-FACTOR =	9780 dscf/MMBtu
*****	*****	*****	*****

Vw(std) = 0.04714 x Vic	=	2.376	scf
Vm(std) = 17.647 x Vm x Y x (Pb + (dH / 13.6)) / (Tm + 460)	=	30.457	scf
Bws = Vw(std) / (Vm(std) + Vw(std))	=	0.863	scm
FDA = 1.0 - Bws	=	0.072	%
Md = (.44 x %CO2) + (.32 x %O2) + [.28 x (%N2 + %CO)] =	=	0.928	%
Ms = (Md x FDA) + (18.0 x Bws)	=	29.87	lb/lb mole
vs = 85.49 x CP x (Sq.Rt.dP) x [Sq.Rt.(Ts+460)] / (Ms x Ps)]	=	29.02	lb/lb mole
Qs = vs x As x 60	=	61.2	ft/sec
Qs(std)=Qs x FDA x (528/(Ts + 460)) x (Ps/29.92) =	=	450620	acf/min
I = (Ts + 460) x [(0.00267 x Vic) + (Vm(std) / 17.647)] x 100 / (Time x Ps x An x vs x 60)	=	304584	dscf/min
*****	*****	*****	*****
N = NORMALITY OF BaI2 * 2H2O	=	96.7	%
Tb = TITRANT BLANK	=	0.0102	
Vs = VOLUME SOLUTION	=	0.0400	milliliters
Va = VOLUME ALIQUOT	=	5.35E+02	milliliters
T = TITRANT	=	100.0	milliliters
H2SO4 (lb/dscf) = 0.0001081 x (N x (T-Tb) x Vs/Va)/Vm	=	4.66	milliliters
H2SO4 (g/dscm) = 0.04904 x (N x (T-Tb) x Vs/Va)/Vm	=	0.0000089	lb/dscf
H2SO4 (lb/MMBtu)	=	0.0143	g/dscm
	=	0.0116	lb/MMBtu

U.S. EPA METHOD EIGHT  
SULFURIC ACID MIST TEST CALCULATIONS  
RUN NO. 2-S

PLANT : F. J. GANNON  
DATE : 4-23-96  
SAMP. LOCATION : BOILER NO. 3  
OPERATING COND.: TDF TEST BLEND/ SOOTBLOWING

SAMPLE TIME =	60.0 min.	NOZZLE DIA. =	0.212 in.
BAR. PRESSURE =	30.00 in.Hg	NOZZLE AREA =	0.00024513 Sq.Ft.
STK. PRESSURE =	30.00 in.Hg	METER ORIFICE =	1.182 in. H2O
EFF. STACK AREA =	122.72 Sq.Ft.	METER VOLUME =	37.130 Cu.Ft.
Cp =	0.84	METER TEMP. =	88.4 DEG. F
GAS ANALYSIS =	11.6 % CO2	STACK TEMP. =	270.3 DEG. F
	5.1 % O2	SQ.RT. dP =	0.940 in. H2O
	0.0 % CO	CONDENSATE VOL.=	79.2 ml
	84.5 % N2	METER Y =	1.000
LAB ANALYSIS =	0.00000 grams	HEAT INPUT =	*** MM Btu/hr
		F-FACTOR =	9780 dscf/MMBtu
*****	*****	*****	*****

$V_w(\text{std}) = 0.04714 \times V_{ic}$	=	3.733	scf
$V_m(\text{std}) = 17.647 \times V_m \times Y \times (P_b + (dH / 13.6)) / (T_m + 460)$	=	35.937	scf
		1.018	scm
$B_{ws} = V_w(\text{std}) / (V_m(\text{std}) + V_w(\text{std}))$	=	0.094	%
$FDA = 1.0 - B_{ws}$	=	0.906	%
$M_d = (.44 \times \%CO_2) + (.32 \times \%O_2) + [.28 \times (\%N_2 + \%CO)]$	=	30.40	lb/lb mole
$M_s = (M_d \times FDA) + (18.0 \times B_{ws})$	=	29.23	lb/lb mole
$v_s = 85.49 \times CP \times (Sq.Rt.dP) \times [Sq.Rt.(T_s+460) / (M_s \times P_s)]$	=	61.6	ft/sec
$Q_s = v_s \times A_s \times 60$	=	453566	acf/min
$Q_s(\text{std}) = Q_s \times FDA \times (528 / (T_s + 460)) \times (P_s / 29.92)$	=	297914	dscf/min
$I = (T_s + 460) \times [(0.00267 \times V_{ic}) + (V_m(\text{std}) / 17.647)] \times 100 / (Time \times P_s \times A_n \times v_s \times 60)$	=	100.7	%
*****	*****	*****	*****

N = NORMALITY OF BaBI2 * 2H2O	=	0.0102	
Tb = TITRANT BLANK	=	0.0400	milliliters
Vs = VOLUME SOLUTION	=	6.40E+02	milliliters
Va = VOLUME ALIQUOT	=	100.0	milliliters
T = TITRANT	=	2.66	milliliters
$H_2SO_4 \text{ (lb/dscf)} = 0.0001081 \times (N \times (T - T_b) \times V_s / V_a) / V_m$	=	0.00000051	lb/dscf
$H_2SO_4 \text{ (g/dscm)} = 0.04904 \times (N \times (T - T_b) \times V_s / V_a) / V_m$	=	0.0082	g/dscm
$H_2SO_4 \text{ (lb/MMBtu)}$	=	0.0067	lb/MMBtu



U.S. EPA METHOD EIGHT  
SULFURIC ACID MIST TEST CALCULATIONS  
RUN NO. 3-S

PLANT : F. J. GANNON  
DATE : 4-23-96  
SAMP. LOCATION : BOILER NO. 3  
OPERATING COND.: TDF TEST BLEND/ SOOTBLOWING

SAMPLE TIME =	60.0 min.		NOZZLE DIA. =	0.212 in.
BAR. PRESSURE =	30.06 in.Hg		NOZZLE AREA =	0.00024513 Sq.Ft.
STK. PRESSURE =	30.06 in.Hg		METER ORIFICE =	1.149 in. H2O
EFF. STACK AREA =	122.72 Sq.Ft.		METER VOLUME =	36.481 Cu.Ft.
Cp =	0.84		METER TEMP. =	90.0 DEG. F
GAS ANALYSIS =	11.7 % CO2		STACK TEMP. =	269.2 DEG. F
	5.1 % O2		SQ.RT. dP =	0.926 in. H2O
	0.0 % CO		CONDENSATE VOL.=	74.6 ml
	85.6 % N2		METER Y =	1.000
LAB ANALYSIS =	0.00000 grams		HEAT INPUT =	*** MM Btu/hr
			F-FACTOR =	9780 dscf/MMBtu
*****	*****	*****	*****	*****

$Vw(std) = 0.04714 \times Vic$	=	3.517	scf
$Vm(std) = 17.647 \times Vm \times Y \times (Pb + (dH / 13.6)) / (Tm + 460)$	=	35.270	scf
	=	0.999	scm
$Bws = Vw(std) / (Vm(std) + Vw(std))$	=	0.091	%
$FDA = 1.0 - Bws$	=	0.909	%
$Md = (.44 \times \%CO2) + (.32 \times \%O2) + [.28 \times (\%N2 + \%CO)] =$	=	30.75	lb/lb mole
$Ms = (Md \times FDA) + (18.0 \times Bws)$	=	29.59	lb/lb mole
$vs = 85.49 \times CP \times (Sq.Rt.dP) \times [Sq.Rt.(Ts+460) / (Ms \times Ps)]$	=	60.2	ft/sec
$Qs = vs \times As \times 60$	=	443257	acf/min
$Qs(std) = Qs \times FDA \times (528 / (Ts + 460)) \times (Ps / 29.92) =$	=	293112	dscf/min
$I = (Ts + 460) \times [(0.00267 \times Vic) + (Vm(std) / 17.647)] \times 100 / (Time \times Ps \times An \times vs \times 60)$	=	100.4	%
*****	*****	*****	*****

N = NORMALITY OF BaBi2 * 2H2O	=	0.0102	
Tb = TITRANT BLANK	=	0.0400	milliliters
Vs = VOLUME SOLUTION	=	5.58E+02	milliliters
Va = VOLUME ALIQUOT	=	100.0	milliliters
T = TITRANT	=	2.65	milliliters
$H2SO4 (lb/dscf) = 0.0001081 \times (N \times (T-Tb) \times Vs/Va)/Vm$	=	0.00000046	lb/dscf
$H2SO4 (g/dscm) = 0.04904 \times (N \times (T-Tb) \times Vs/Va)/Vm$	=	0.0073	g/dscm
$H2SO4 (lb/MMBtu)$	=	0.0059	lb/MMBtu

**A-5 NOMENCLATURE**

## SOURCE SAMPLING NOMENCLATURE

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- A** = Absorbance of sample.  
**A<sub>n</sub>** = Cross-sectional area of nozzle, m<sup>2</sup> (ft<sup>2</sup>).  
**A<sub>s</sub>** = Cross-sectional area of stack, m<sup>2</sup> (ft<sup>2</sup>).  
**B<sub>ws</sub>** = Water vapor in the gas steam, proportion by volume.  
**C** = Concentration of particulate matter, (lbs/dscf), Method 5,17.  
**C** = Concentration of NO<sub>x</sub>, as NQ<sub>2</sub>, basis, corrected to standard conditions, mg/dscm (lbs/dscf), Method 7.  
**C<sub>a</sub>** = Concentration of acetone blank residue, mg/g.  
**CH<sub>2</sub> SO<sub>4</sub>** = Sulfuric acid (including SO<sub>3</sub>) concentration, g/dscm (lbs/dscf).  
**C<sub>p</sub>** = Pitot tube coefficient, dimensionless.  
**cs** = Concentration of stack gas particulates, dry basis corrected to standard conditions, g/dscm (lbs/dscf).  
**CSO<sub>2</sub>** = Sulfur dioxide concentration, mg/dscm (lbs/dscf).  
**E** = Pollutant emissions, lbs/106 Btu.  
**EM** = Particulate emission rate, lbs/hr.  
**F** = Factor ratio of generated flue gases to calorific value of fuel, Method 5,17.  
**F** = Dilution factor (i.e., 25/5, 25/10, etc.) required only if sample dilution was needed to reduce the absorbance to the range of calibration, Method 7.  
**FDA** = Fraction of dry air.  
**I** = Percent of isokinetic sampling, %.  
**K<sub>c</sub>** = Spectrophotometer calibration factor.  
**K<sub>p</sub>** = Pitot tube constant,

### Metric

$$34.97 \text{ m/sec} \left[ \frac{(g/g\text{-mole}) (mmHg)}{(\text{°K}) (mmH2O)} \right]^{1/2}$$

## English

$$85.49 \text{ ft/sec} \left[ \frac{(\text{lb/lb-mole}) (\text{''Hg})}{(^{\circ}\text{K}) (\text{mmH}_2\text{O})} \right]^{1/2}$$

- $L_a$  = Maximum acceptable leakage rate for either a pretest leak check or a leak check following a component change; equal to 0.00057 m<sup>3</sup>/min (0.02 ft<sup>3</sup>/min) or 4% of the average sampling rate, whichever is less.
- $L_i$  = Individual leakage rate observed during the leak check conducted prior to the "ith" component change (i = 1, 2, 3,...n), m<sup>3</sup>/min (ft<sup>3</sup>/min).
- $L_p$  = Leakage rate observed during the post test leak check, m<sup>3</sup>/min (ft<sup>3</sup>/min).
- $m$  = Mass of NO<sub>x</sub> as NO<sub>2</sub> in gas sample, μg.
- $m_a$  = Mass of acetone residue after evaporation, mg.
- $M_d$  = Molecular weight of stack gas, dry basis, g/g-mole (lb/lb-mole).
- $m_f$  = Filter weight gain, mg.
- $m_n$  = Total amount of particulates collected, mg.
- $M_s$  = Molecular weight of stack gas, wet basis, g/g-mole (lb/lb-mole), or  $M_d(1 - B_{ws}) = 18.0 B_{ws}$ .
- $M_w$  = Molecular weight of water, 18.0 g/g-mole (18.0 lb/lb-mole).
- $N$  = Normality of Ba(C10<sub>4</sub>)<sub>2</sub> titrant, g-eg/l.
- $N$  = Normality of barium perchlorate titrant, meq/ml.
- $P_a$  = Density of acetone, mg/ml (see bottle label).
- $P_{bar}$  = Barometric pressure at sampling site, mm Hg (in. Hg).
- $P_f$  = Final absolute pressure of flask, mm Hg (in. Hg).
- $P_g$  = Stack static pressure, mm Hg (in. Hg).
- $P_i$  = Initial absolute pressure of flask, mm Hg (in. Hg).
- $P_s$  = Absolute stack pressure, 760 mm Hg (29.92 in. Hg).
- $P_w$  = Density of water, 0.9982 g/ml (0.0022 lb/ml).
- $Q_s$  = Volumetric flow rate, actual cubic feet per min, acf/min.
- $Q_{std}$  = Dry volumetric stack gas flow rate corrected to standard conditions dsm<sup>3</sup>/hr (dscf/hr).
- $R$  = Ideal gas constant, 0.06236 (mm Hg - m<sup>3</sup>)/(°K - g - mole) for metric units and 21.85 (in. Hg - ft<sup>3</sup>)(°R - 1b - mole) for English units.

- S.V.P. = Saturated vapor pressure of water at average stack temperature mm Hg (in. Hg).
- $T_f$  = Final absolute temperature of flask, K ( $^{\circ}$ R).
- $T_i$  = Initial absolute temperature of flask, K ( $^{\circ}$ R).
- $T_m$  = Absolute average dry gas meter temperature, K ( $^{\circ}$ R).
- $t_s$  = Stack temperature,  $^{\circ}$ C ( $^{\circ}$ F).
- $T_s$  = Absolute stack temperature, K ( $^{\circ}$ R), or  $273 + t_s$  for metric system or  $460 + t_s$  for English system.
- $T_{std}$  = Standard absolute temperature, 293K ( $528^{\circ}$ R).
- $V_a$  = Volume of acetone blank, ml, (Method 5,17).
- $V_a$  = Volume of sample aliquot titrated, ml, (Method 6).
- $V_a$  = Volume of absorbing solution, 25 ml, (Method 7).
- $V_a$  = Volume of sample aliquot titrated, 100 ml for  $H_2SO_4$  and 10ml for  $SO_2$  (Method 8).
- $V_{aw}$  = Volume of acetone used in wash, ml.
- $V_f$  = Final volume of condenser water, ml.
- $V_f$  = Volume of flask and valve, ml.
- $V_i$  = Initial volume of condenser water, ml.
- $V_{ic}$  = Total volumes of liquid and silica gel collected in impingers, ml.
- $V_m$  = Dry gas volume measured by dry gas meter, scm (dcf).
- $V_{m(std)}$  = Volume of gas sample measured by the dry gas meter and corrected to standard condition, dscm (dscf).
- vs = Average stack gas velocity calculated by Method 2, m/sec (ft/sec).
- $V_{sc}$  = Sample volume at standard conditions (dry basis), ml.
- $V_{soln}$  = Total volume of solution in which the sulfur dioxide sample is contained, 100 ml, (method 6).
- $V_{soln}$  = Total volume of solution in which the  $H_2SO_4$  or  $SO_2$  sample is contained, 250 ml or 1000 ml, respectively, (Method 8).
- $V_t$  = Volume of  $Ba(CIO_4)_2$  titrant used for the sample, ml, (Method 8).
- $V_t$  = Volume of barium perchlorate titrant used for the sample (average of replicate titrations), ml, (Method 6).
- $V_{tb}$  = Volume of barium perchlorate titrant used for the blank, ml.
- $V_{w(std)}$  = Volume of water vapor in the gas sample, corrected to standard conditions, scm (scf).

- $V_{wc(std)}$  = Volume of condensed water vapor, corrected to standard conditions,  $sm^3(scf)$ .
- $V_{wsg(std)}$  = Volume of water vapor collected in silica gel, corrected to standard conditions,  $sm^3(scf)$ .
- $W_a$  = Weight of acetone wash residue, mg.
- $W_f$  = Final weight of silica gel or silica gel plus impinger, g.
- $W_i$  = Initial weight of silica gel or silica gel plus impinger, g.
- $Y$  = Dry gas meter calibration factor.
- $\Delta H$  = Average pressure differential across the orifice meter, mm (in.)  $H_2O$ .
- $\Delta H@i$  = Measurement of pressure differential across the orifice meter, mm (in.)  $H_2O$ .
- $\Delta p$  = Average velocity head of stack gas, mm (in.)  $H_2O$ .
- $\Delta V_m$  = Incremental volume measured by dry gas meter at each traverse point,  $dm^3(dcf)$ .
- $\%CO$  = Percent CO by volume (dry basis), average of three CO values.
- $\%CO_2$  = Percent  $CO_2$  by volume (dry basis), average of three analyses.
- $\%EA$  = Percent excess air, %.
- $\%N_2$  = Percent  $N_2$  by volume (dry basis), average of three  $N_2$  values.
- $\%O_2$  = Percent  $O_2$  by volume (dry basis), average of three  $O_2$  values.
- 0.262 = Ratio of  $O_2$  to  $N_2$  in air, v/v.
- 2 = 50/25, the aliquot factor, (Method 7).
- 13.6 = Specific gravity of mercury (Hg).
- 18.0 = Molecular weight of water, g/g-mole (lb/lb-mole).
- 32.03 = Equivalent weight of sulfur dioxide.
- 60 = Seconds per minute (sec/min).
- 100 = Conversion to percent, %.
- 3600 = Conversion factor, (sec/hr).
- $\theta$  = Total sampling time, min.
- $\theta_1$  = Interval of sampling time from beginning of a run until first component change, min.
- $\theta_i$  = Interval of sampling time between two successive component changes, beginning with first and second changes, min.
- $\theta_p$  = Interval of sampling time from final (nth) component change until the end of the sampling run, min.

## **APPENDIX B**

### **LABORATORY ANALYTICAL DATA**

- B-1 BASELINE PARTICULATE LABORATORY DATA**
- B-2 BASELINE SULFURIC ACID MIST LABORATORY DATA**
- B-3 FUEL BLEND BURN PARTICULATE LABORATORY  
DATA**
- B-4 FUEL BLEND BURN SULFURIC ACID MIST  
LABORATORY DATA**

**B-1 BASELINE PARTICULATE LABORATORY DATA**



# SAMPLE ANALYTICAL DATA FORM

Plant F.D. GANNON STATION Run number RUN 15  
 Sample location Boiler No. 3  
 Relative humidity 37%

Sample Type	Sample Identifiable	Liquid Level Marked and/or Container Sealed
Acetone Rinse	YES	YES
Filters	YES	YES

Acetone rinse container number Air-13  
 Acetone rinse volume ( $V_{aw}$ ) 150 ml  
 Acetone blank residue weight ( $M_{ab}$ ) 0.8 mg

Date and time of wt 3.5.96 7:00 32% Gross wt 104609.3 mg  
 Date and time of wt 3.5.96 15:00 37% Gross wt 104609.3 mg  
 Date and time of wt \_\_\_\_\_ Gross wt \_\_\_\_\_ mg

Average gross wt 104609.3 mg  
 Tare wt 104606.2 mg

Less acetone blank wt ( $M_{ab}$ ) 0.8 mg

Weight of particulate in acetone rinse ( $m_a$ ) 2.3 mg

Filter/Thimble Number 001093

Date and time of wt 3.4.96 7:15 39% Gross wt 1666.8 mg  
 Date and time of wt 3.4.96 14:15 35% Gross wt 1666.7 mg  
 Date and time of wt \_\_\_\_\_ Gross wt \_\_\_\_\_ mg

Average gross wt 1666.75 mg  
 Tare wt 1638.25 mg

Weight of particulate on filter(s) ( $m_f$ ) 28.5 mg

Weight of particulate in acetone rinse ( $m_a$ ) 2.3 mg

Total weight of particulate ( $m_n$ ) 30.8 mg

**Note:** In no case should a blank residue >0.01 mg/g or 0.001% of the weight of acetone used be subtracted from the sample weight.

Remarks \_\_\_\_\_

Signature of analyst *[Signature]*  
 Signature of reviewer *[Signature]* 3/6/96

# SAMPLE ANALYTICAL DATA FORM

Plant ED. GANNON STATION Run number RUN 25  
 Sample location Boiler No. 3  
 Relative humidity 37%

Sample Type	Sample Identifiable	Liquid Level Marked and/or Container Sealed
Acetone Rinse	YES	YES
Filters	YES	YES

Acetone rinse container number AIR-14  
 Acetone rinse volume ( $V_{aw}$ ) 150 ml  
 Acetone blank residue weight ( $M_{ab}$ ) 0.8 mg

Date and time of wt 3.5.96 7:00 32% Gross wt 107543.0 mg  
 Date and time of wt 3.5.96 15:00 37% Gross wt 107542.9 mg  
 Date and time of wt \_\_\_\_\_ Gross wt \_\_\_\_\_ mg

Average gross wt 107542.95 mg  
 Tare wt 107540.6 mg

Less acetone blank wt ( $M_{ab}$ ) 0.8 mg

Weight of particulate in acetone rinse ( $m_a$ ) 1.55 mg

Filter/Thimble Number 001094

Date and time of wt 3.4.96 7:15 39% Gross wt 1759.1 mg  
 Date and time of wt 3.4.96 14:15 35% Gross wt 1759.2 mg  
 Date and time of wt \_\_\_\_\_ Gross wt \_\_\_\_\_ mg

Average gross wt 1759.15 mg  
 Tare wt 1730.85 mg

Weight of particulate on filter(s) ( $m_f$ ) 28.3 mg  
 Weight of particulate in acetone rinse ( $m_a$ ) 1.55 mg  
 Total weight of particulate ( $m_n$ ) 29.85 mg

**Note:** In no case should a blank residue >0.01 mg/g or 0.001% of the weight of acetone used be subtracted from the sample weight.

Remarks \_\_\_\_\_

Signature of analyst *Belgian Alton*

Signature of reviewer *Ken Parby 3/6/96*



# BLANK ANALYTICAL DATA FORM

Plant F.D. GANNON STATION

Sample location BOILER No. 3

Relative humidity 37%

Liquid level marked and container sealed YES APR-16

Blank volume ( $V_a$ ) 150 ml

Date and time of wt 3.5.96 7:00 32% Gross wt 109294.4 mg

Date and time of wt 3.5.96 15:00 37% Gross wt 109294.2 mg

Date and time of wt \_\_\_\_\_ Gross wt \_\_\_\_\_ mg

Average Gross wt 109294.3 mg

Tare wt 109293.5 mg

Weight of blank ( $m_{ab}$ ) 0.8 mg

Note: In no case should a blank residue greater than 0.001% of the blank weight be subtracted from the sample weight.

Filters Filter number 001097

Date and time of wt 3.4.96 7:15 39% Gross wt 1495.8 mg

Date and time of wt 3.4.96 14:15 35% Gross wt 1495.8 mg

Date and time of wt \_\_\_\_\_ Gross wt \_\_\_\_\_ mg

Average gross wt 1495.8 mg

Tare wt 1494.4 mg

Note: Average difference must be less than  $\pm 5$  mg or 2% of total sample weight whichever is greater.

Remarks \_\_\_\_\_

Signature of analyst [Signature]

Signature of reviewer [Signature] 3/6/96

**B-2 BASELINE SULFURIC ACID MIST LABORATORY DATA**

# TAMPA ELECTRIC COMPANY

Corporate Environmental Services  
Laboratory Services

To: Stack Test Coordinator, CES

**Laboratory Number: AA28439**

Location Description: Gannon Unit #3 - SO3 Testing

Collection Date: 02/28/96

Report Date: 03/05/96

Analysis Date: 03/04/96

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Parameter	Result	Units
Normality of BaCl <sub>2</sub> * 2H <sub>2</sub> O	0.0103	
SO <sub>3</sub> , Volume of Sample Aliquot	100	milliliters
<b>Sample Titration Results</b>		
SO <sub>3</sub> , Avg. of Blank Titrations	0.06	milliliters
SO <sub>3</sub> , Run #1, Avg. of Titrations	6.32	milliliters
SO <sub>3</sub> , Run #2, Avg. of Titrations	4.08	milliliters
SO <sub>3</sub> , Run #3, Avg. of Titrations	3.25	milliliters

**Sample Comments:**

Total volume of solution in which the sample is contained.

Run #1 = 505 mls.

Run #2 = 560 mls.

Run #3 = 669 mls.

Frank Sandley  
Analyst

3-5-96  
Date

Bret A. Nicholas  
Quality Assurance Specialist

3/5/96  
Date

**B-3 FUEL BLEND BURN PARTICULATE LABORATORY DATA**









BLANK ANALYTICAL DATA FORM

Plant F. D. GANNON STATION

Sample location BOILER No. 3

Relative humidity 40%

Liquid level marked and container sealed YES AIR-20

Blank volume (V<sub>a</sub>) 200 ml

Date and time of wt 4-26-96 7:13 37% Gross wt 109968.5 mg

Date and time of wt 4-26-96 13:24 39% Gross wt 109968.5 mg

Date and time of wt \_\_\_\_\_ Gross wt \_\_\_\_\_ mg

Average Gross wt 109968.5 mg

Tare wt 109968.3 mg

Weight of blank (m<sub>ab</sub>) 0.2 mg

Note: In no case should a blank residue greater than 0.001% of the blank weight be subtracted from the sample weight.

Filters Filter number 001092

Date and time of wt 4-25-96 14:53 42% Gross wt 1015.0 mg

Date and time of wt 4-26-96 7:13 37% Gross wt 1015.0 mg

Date and time of wt \_\_\_\_\_ Gross wt \_\_\_\_\_ mg

Average gross wt 1015.0 mg

Tare wt 1013.8 mg

Note: Average difference must be less than ±5 mg or 2% of total sample weight whichever is greater.

Remarks \_\_\_\_\_

Signature of analyst [Signature]

Signature of reviewer [Signature] 4/30/96

**B-4 FUEL BLEND BURN SULFURIC ACID MIST LABORATORY DATA**

# TAMPA ELECTRIC COMPANY

Corporate Environmental Services

Laboratory Services

To: Stack Test Coordinator, CES

**Laboratory Number:** AA29423

Location Description: Gannon Unit #3 - SO3 Testing

Collection Date: 04/23/96

Report Date: 04/26/96

Analysis Date: 04/25/96

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Parameter	Result	Units
Normality of BaCl <sub>2</sub> * 2H <sub>2</sub> O	0.0102	
SO <sub>3</sub> , Volume of Sample Aliquot	100	milliliters
<b>Sample Titration Results</b>		
SO <sub>3</sub> , Avg. of Blank Titrations	0.04	milliliters
SO <sub>3</sub> , Run #1, Avg. of Titrations	4.66	milliliters
SO <sub>3</sub> , Run #2, Avg. of Titrations	2.66	milliliters
SO <sub>3</sub> , Run #3, Avg. of Titrations	2.65	milliliters

**Sample Comments:**

Total volume of solution in which the sample is contained:

Run #1 = 535 ml

Run #2 = 640 ml

Run #3 = 558 ml

Frank Hardy  
Analyst

4-26-96  
Date

Bret A. Nicholas  
Quality Assurance Specialist

4/26/96  
Date

**APPENDIX C**

**BOILER/PRECIPITATOR OPERATION DATA**

**C-1 BASELINE OPERATIONAL DATA**

**C-2 FUEL BLEND BURN OPERATIONAL DATA**

**C-1 BASELINE OPERATIONAL DATA**

**F.J. GANNON GENERATING STATION  
HEAT INPUT CALCULATIONS**

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<b>F.J. GANNON STATION BOILER NO. 3 BASELINE SULFURIC ACID MIST TEST FEBRUARY 28, 1996</b>	
January Gross Heat Rate =	10.337 x 10 <sup>6</sup> Btu/MWH
<b>BOILER NO. 3 SOURCE TEST HEAT INPUT CALCULATIONS</b>	
Final MWH (746152) - Initial MWH (745428) =	724 MWH
Time =	4.90 Hrs
Average MW = 724 MWH ÷ 4.90 H =	147.8 MW
10.337 x 10 <sup>6</sup> Btu/MWH x 724 MWH ÷ 4.90 H =	1527.3 x 10 <sup>6</sup> Btu/H



# COMPLIANCE TEST DATA

F. J. GANNON STATION

BOILER NO. 3 TEST DATE 2/28/90

UNIT LOAD (MN) 145 MW

BASE LOADED (TIME) 4:30

**TEST DATA**

MEGAWATTS INTEGRATOR	INITIALS
BEGIN MWH <u>0728</u> BEGIN SAMPLING <u>745428</u>	<u>CRB</u>
END MWH <u>1222</u> END SAMPLING <u>746152</u>	<u>CRB</u>

**SOOTBLOWING**

RUN	BEGIN TIME	END TIME	INITIALS
<u>1 SO3</u>	<u>0728</u>	<u>0836</u>	<u>CRB / J.M.C.</u>
<u>2 SO3</u>	<u>0921</u>	<u>1029</u>	<u>CRB / J.M.C.</u>
<u>3 SO3</u>	<u>1114</u>	<u>1232</u>	<u>CRB / J.M.C.</u>

**FLYASH REINJECTION**

RUN	REINJECTION (Y/N)	% REINJECTION	INITIALS
<u>1 SO3</u>	<u>Y</u>	<u>100%</u>	<u>CRB / LRJ</u>
<u>2 SO3</u>	<u>Y</u>	<u>100%</u>	<u>CRB / LRJ</u>
<u>3 SO3</u>	<u>Y</u>	<u>100%</u>	<u>CRB / LRJ</u>

COMPLIANCE TEST DATA  
F. J. GANNON STATION

INTEGRATOR DATA

RUN NUMBER	START TIME	STOP TIME	INTEGRATOR START	INTEGRATOR STOP
1 SO3	0728	0836	745428	745597
2 SO3	0921	1029	745708	745874
3 SO3	1114	1222	745986	746152

STACK

- \* B cyclone tripped  $\approx$  1040; between run 2 & 3. Operator was able to return cyclone to service promptly - no MW drop.
- \* B cyclone tripped  $\approx$  1119; start of run 3. Operator was able to return cyclone to service promptly - no MW drop.

GANNON STACK TEST PRECIPITATOR LOG - UNIT 3

DATE : 2/20/90

TIME : 1503

RUN NO. : 0735

INITIALS: CEB

T/R	PRIMARY VOLTS	SECONDARY VOLTS (DC)	PRIMARY AMPS	SECONDARY AMPS (DC)
A1	<u>290</u>	<u>40</u>	<u>50</u>	<u>325</u>
A2	<u>300</u>	<u>30</u>	<u>75</u>	<u>475</u>
A3	<u>350</u>	<u>22</u>	<u>85</u>	<u>550</u>
A4	<u>350</u>	<u>40</u>	<u>70</u>	<u>400</u>
B1	<u>300</u>	<u>46</u>	<u>60</u>	<u>350</u>
B2	<u>290</u>	<u>44</u>	<u>50</u>	<u>325</u>
B3	<u>290</u>	<u>44</u>	<u>50</u>	<u>325</u>
B4	<u>*</u>	<u>*</u>	<u>*</u>	<u>*</u>
C1	<u>330</u>	<u>52</u>	<u>55</u>	<u>300</u>
C2	<u>290</u>	<u>50</u>	<u>45</u>	<u>250</u>
C3	<u>300</u>	<u>52</u>	<u>45</u>	<u>250</u>
C4	<u>280</u>	<u>50</u>	<u>45</u>	<u>225</u>
D1	<u>260</u>	<u>44</u>	<u>35</u>	<u>250</u>
D2	<u>180</u>	<u>30</u>	<u>17</u>	<u>75</u>
D3	<u>280</u>	<u>46</u>	<u>45</u>	<u>250</u>
D4	<u>280</u>	<u>44</u>	<u>40</u>	<u>225</u>

GANNON STACK TEST PRECIPITATOR LOG - UNIT 3

DATE : 2/28/96

TIME : 0925

RUN NO. : 2 503

INITIALS: CRB

T/R	PRIMARY VOLTS	SECONDARY VOLTS (DC)	PRIMARY AMPS	SECONDARY AMPS (DC)
A1	<u>290</u>	<u>38</u>	<u>50</u>	<u>350</u>
A2	<u>320</u>	<u>30</u>	<u>75</u>	<u>475</u>
A3	<u>350</u>	<u>24</u>	<u>80</u>	<u>550</u>
A4	<u>350</u>	<u>40</u>	<u>65</u>	<u>375</u>
B1	<u>300</u>	<u>46</u>	<u>120</u>	<u>350</u>
B2	<u>290</u>	<u>44</u>	<u>50</u>	<u>325</u>
B3	<u>290</u>	<u>44</u>	<u>50</u>	<u>325</u>
B4	<u>*</u>	<u>*</u>	<u>*</u>	<u>*</u>
C1	<u>300</u>	<u>52</u>	<u>55</u>	<u>325</u>
C2	<u>270</u>	<u>50</u>	<u>45</u>	<u>225</u>
C3	<u>300</u>	<u>52</u>	<u>45</u>	<u>250</u>
C4	<u>280</u>	<u>50</u>	<u>45</u>	<u>225</u>
D1	<u>240</u>	<u>44</u>	<u>40</u>	<u>250</u>
D2	<u>170</u>	<u>30</u>	<u>17</u>	<u>75</u>
D3	<u>280</u>	<u>46</u>	<u>45</u>	<u>250</u>
D4	<u>270</u>	<u>44</u>	<u>40</u>	<u>250</u>

GANNON STACK TEST PRECIPITATOR LOG - UNIT 3

DATE : 2/28/94  
 TIME : 1125  
 RUN NO. : 3 503  
 INITIALS: CEB

T/R	PRIMARY VOLTS	SECONDARY VOLTS (DC)	PRIMARY AMPS	SECONDARY AMPS (DC)
A1	<u>270</u>	<u>38</u>	<u>50</u>	<u>300</u>
A2	<u>320</u>	<u>30</u>	<u>65</u>	<u>475</u>
A3	<u>350</u>	<u>22</u>	<u>85</u>	<u>550</u>
A4	<u>340</u>	<u>40</u>	<u>65</u>	<u>400</u>
B1	<u>300</u>	<u>40</u>	<u>60</u>	<u>350</u>
B2	<u>290</u>	<u>44</u>	<u>50</u>	<u>325</u>
B3	<u>290</u>	<u>44</u>	<u>50</u>	<u>325</u>
B4	<u>*</u>	<u>*</u>	<u>*</u>	<u>*</u>
C1	<u>330</u>	<u>52</u>	<u>50</u>	<u>350</u>
C2	<u>270</u>	<u>50</u>	<u>45</u>	<u>250</u>
C3	<u>300</u>	<u>52</u>	<u>45</u>	<u>250</u>
C4	<u>280</u>	<u>50</u>	<u>45</u>	<u>225</u>
D1	<u>250</u>	<u>44</u>	<u>40</u>	<u>275</u>
D2	<u>170</u>	<u>30</u>	<u>17</u>	<u>75</u>
D3	<u>280</u>	<u>46</u>	<u>50</u>	<u>275</u>
D4	<u>280</u>	<u>44</u>	<u>40</u>	<u>250</u>

**F.J. GANNON GENERATING STATION  
HEAT INPUT CALCULATIONS**

F.J. GANNON STATION BOILER NO. 3 BASELINE PARTICULATE TEST February 28, 1996	
January Gross Heat Rate =	10.337 x 10 <sup>6</sup> Btu/MWH
<b>BOILER NO. 3 SOURCE TEST HEAT INPUT CALCULATIONS</b>	
Final MWH (746932) - Initial MWH (746308) =	624 MWH
Time =	4.22 Hrs
Average MW = 624 MWH ÷ 4.22 H =	147.9 MW
10.337 x 10 <sup>6</sup> Btu/MWH x 624 MWH ÷ 4.22 H =	1528.5 x 10 <sup>6</sup> Btu/H

**COMPLIANCE TEST DATA**  
**F. J. GANNON STATION**

BOILER NO. 3 TEST DATE 2/28/96  
 UNIT LOAD (MN) 148  
 BASE LOADED (TIME) 0430

**TEST DATA**

MEGAWATTS INTEGRATOR	INITIALS
BEGIN MWH <u>1324</u> BEGIN SAMPLING <u>746308</u>	<u>CRB</u>
END MWH <u>1737</u> END SAMPLING <u>746932</u>	<u>CRB</u>

**SOOTBLOWING**

RUN	BEGIN TIME	END TIME	INITIALS
1 particulate	1324	1433	CRB / J.M.E.
2 particulate	1510	1615	CRB / J.M.E.
3 particulate	1633	1737	CRB / J.M.E.

**FLYASH REINJECTION**

RUN	REINJECTION (Y/N)	% REINJECTION	INITIALS
1 particulate	yes	100%	CRB / LRJ
2 particulate	yes	100%	CRB / LRJ
3 particulate	yes	100%	CRB / LRJ

COMPLIANCE TEST DATA  
F. J. GANNON STATION

INTEGRATOR DATA

RUN NUMBER	START TIME	STOP TIME	INTEGRATOR START	INTEGRATOR STOP
1 particulate	1324	1433	746308	746479
2 particulate	1510	1615	746567	746730
3 particulate	1633	1737	746776	746932

STACK



UNIT: 3DATE: 2/28/96

HOUR	MW	FUEL RATIO	TEMP	AIR/FUEL RATIO	OPERATING CONDITIONS
0700	145	100% Coal	290°	58% / 50%	Sootblowing, reinjection, Steady State
0800	147	100% Coal	290°	60% / 50%	Sootblowing, reinjection, Steady State
0900	147	100% Coal	295°	58% / 50%	Sootblowing, reinjection, Steady State
1000	146	100% Coal	290°	60% / 52%	Sootblowing, reinjection, Steady State
1100	148	100% Coal	285°	58% / 51%	Sootblowing, reinjection, Steady State
1200	147	100% Coal	280°	60% / 55%	Sootblowing, reinjection, Steady State
1300	147	100% Coal	290°	60% / 55%	Sootblowing, reinjection, Steady State
1400	147	100% Coal	290°	60% / 56%	Sootblowing, reinjection, Steady State
1500	147	100% Coal	290°	60% / 56%	Sootblowing, reinjection, Steady State
1600	147	100% Coal	295°	58% / 50%	Sootblowing, reinjection, Steady State
1700	146	100% Coal	290°	60% / 55%	Sootblowing, reinjection, Steady

GANNON STACK TEST PRECIPITATOR LOG - UNIT 3

DATE : 2-28-96

TIME : 1330

RUN NO. : 1 Particulate

INITIALS: LRJ

T/R	PRIMARY VOLTS	SECONDARY VOLTS (DC)	PRIMARY AMPS	SECONDARY AMPS (DC)
A1	<u>270</u>	<u>39</u>	<u>50</u>	<u>300</u>
A2	<u>320</u>	<u>31</u>	<u>75</u>	<u>500</u>
A3	<u>350</u>	<u>23</u>	<u>85</u>	<u>575</u>
A4	<u>345</u>	<u>41</u>	<u>70</u>	<u>400</u>
B1	<u>290</u>	<u>46</u>	<u>60</u>	<u>350</u>
B2	<u>285</u>	<u>44</u>	<u>45</u>	<u>300</u>
B3	<u>285</u>	<u>45</u>	<u>50</u>	<u>300</u>
B4	<u>★</u>	<u>★</u>	<u>★</u>	<u>★</u>
C1	<u>310</u>	<u>51</u>	<u>60</u>	<u>350</u>
C2	<u>270</u>	<u>49</u>	<u>40</u>	<u>225</u>
C3	<u>300</u>	<u>52</u>	<u>45</u>	<u>250</u>
C4	<u>275</u>	<u>50</u>	<u>45</u>	<u>225</u>
D1	<u>250</u>	<u>43</u>	<u>40</u>	<u>275</u>
D2	<u>160</u>	<u>31</u>	<u>15</u>	<u>50</u>
D3	<u>280</u>	<u>46</u>	<u>45</u>	<u>250</u>
D4	<u>270</u>	<u>44</u>	<u>45</u>	<u>250</u>

GANNON STACK TEST PRECIPITATOR LOG - UNIT 3

DATE : 2-28-96

TIME : 1520

RUN NO. : #2 Particulate

INITIALS: LRJ

T/R	PRIMARY VOLTS	SECONDARY VOLTS (DC)	PRIMARY AMPS	SECONDARY AMPS (DC)
A1	<u>260</u>	<u>38</u>	<u>50</u>	<u>300</u>
A2	<u>340</u>	<u>31</u>	<u>75</u>	<u>500</u>
A3	<u>355</u>	<u>26</u>	<u>85</u>	<u>575</u>
A4	<u>345</u>	<u>41</u>	<u>65</u>	<u>400</u>
B1	<u>300</u>	<u>46</u>	<u>60</u>	<u>325</u>
B2	<u>285</u>	<u>44</u>	<u>45</u>	<u>300</u>
B3	<u>290</u>	<u>45</u>	<u>50</u>	<u>325</u>
B4	<u>*</u>	<u>*</u>	<u>*</u>	<u>*</u>
C1	<u>320</u>	<u>50</u>	<u>65</u>	<u>375</u>
C2	<u>270</u>	<u>49</u>	<u>45</u>	<u>225</u>
C3	<u>300</u>	<u>52</u>	<u>45</u>	<u>250</u>
C4	<u>265</u>	<u>50</u>	<u>40</u>	<u>200</u>
D1	<u>260</u>	<u>44</u>	<u>40</u>	<u>250</u>
D2	<u>165</u>	<u>30</u>	<u>15</u>	<u>50</u>
D3	<u>280</u>	<u>45</u>	<u>50</u>	<u>275</u>
D4	<u>275</u>	<u>44</u>	<u>45</u>	<u>275</u>

GANNON STACK TEST PRECIPITATOR LOG - UNIT 3

DATE : 2/28/90

TIME : 1645

RUN NO. : 3 Particulate

INITIALS: LCJ

T/R	PRIMARY VOLTS	SECONDARY VOLTS (DC)	PRIMARY AMPS	SECONDARY AMPS (DC)
A1	<u>270</u>	<u>39</u>	<u>50</u>	<u>350</u>
A2	<u>330</u>	<u>32</u>	<u>75</u>	<u>500</u>
A3	<u>380</u>	<u>22</u>	<u>80</u>	<u>575</u>
A4	<u>350</u>	<u>41</u>	<u>70</u>	<u>400</u>
B1	<u>300</u>	<u>47</u>	<u>55</u>	<u>325</u>
B2	<u>285</u>	<u>44</u>	<u>50</u>	<u>300</u>
B3	<u>290</u>	<u>46</u>	<u>50</u>	<u>325</u>
B4	<u>★</u>	<u>★</u>	<u>★</u>	<u>★</u>
C1	<u>300</u>	<u>52</u>	<u>55</u>	<u>300</u>
C2	<u>260</u>	<u>50</u>	<u>40</u>	<u>200</u>
C3	<u>290</u>	<u>52</u>	<u>45</u>	<u>250</u>
C4	<u>260</u>	<u>49</u>	<u>40</u>	<u>200</u>
D1	<u>240</u>	<u>44</u>	<u>40</u>	<u>250</u>
D2	<u>170</u>	<u>31</u>	<u>15</u>	<u>60</u>
D3	<u>280</u>	<u>46</u>	<u>50</u>	<u>250</u>
D4	<u>270</u>	<u>44</u>	<u>40</u>	<u>250</u>

**C-2 FUEL BLEND BURN OPERATIONAL DATA**

# F. J. GANNON GENERATING STATION HEAT INPUT CALCULATIONS

F. J. GANNON STATION BOILER NO. 3 FUEL BLEND H2SO4 TEST APRIL 23, 1996	
March Gross Heat Rate =	10.233 X 10 <sup>6</sup> Btu/MWH
<b>BOILER NO. 3 SOURCE TEST HEAT INPUT CALCULATIONS</b>	
Final MWH (873599) - Initial MWH( 872956) =	643 MWH
Time =	4.77 Hours
Average MW = 643 MWH ÷ 4.77 H =	134.8 MW
10.233 X 10 <sup>6</sup> Btu/MWH X 643 MWH ÷ 4.77 H =	1379.4 X 10 <sup>6</sup> MMBtu/H

# COMPLIANCE TEST DATA

F. J. GANNON STATION

BOILER NO. 3 TDF/Coal Burn TEST DATE 4/23/96

UNIT LOAD (MN) 133 MW

BASE LOADED (TIME) 5:00 a.m.

**TEST DATA**

MEGAWATTS INTEGRATOR	INITIALS
BEGIN MWH <u>0747</u> BEGIN SAMPLING <u>872956</u>	<u>CRB</u>
END MWH <u>1233</u> END SAMPLING <u>873599</u>	<u>CRB</u>

**SOOTBLOWING**

RUN	BEGIN TIME	END TIME	INITIALS
1 SO3	0747	0853	CRB / <i>[Signature]</i>
2 SO3	0940	1046	CRB / <i>[Signature]</i>
3 SO3	1129	1233	CRB / <i>[Signature]</i>

**FLYASH REINJECTION**

RUN	REINJECTION (Y/N)	% REINJECTION	INITIALS
1 SO3	yes	100%	CRB / F.D.
2 SO3	yes	100%	CRB / F.D.
3 SO3	yes	100%	CRB / F.D.

COMPLIANCE TEST DATA  
F. J. GANNON STATION

INTEGRATOR DATA

RUN NUMBER	START TIME	STOP TIME	INTEGRATOR START	INTEGRATOR STOP
1 SO <sub>3</sub>	0747	0853	872954	873102
2 SO <sub>3</sub>	0940	1046	873210	873360
3 SO <sub>3</sub>	1129	1233	873454	873599

STACK



UNIT: 3DATE: 4/23/96

HOUR	MW	FUEL * RATIO	TEMP	AIR/FUEL RATIO	OPERATING CONDITIONS
0700	133	18% tires	290°	54% / 53%	sootblowing, reinjection steady state
0800	133	18% tires	300°	54% / 52%	sootblowing, reinjection steady state
0900	133	18% tires	300°	54% / 52%	sootblowing, reinjection steady state
1000	134	18% tires	300°	54% / 54%	sootblowing, reinjection steady state
1100	135	18% tires	300°	55% / 53%	sootblowing, reinjection steady state
1200	134	18% tires	300°	54% / 53%	sootblowing, reinjection steady state
1300	133	18% tires	305°	52% / 51%	sootblowing, reinjection steady state
1400	134	18% tires	309°	54% / 51%	sootblowing, reinjection steady state
1500	133	18% tires	310°	54% / 51%	sootblowing, reinjection steady state
1600	134	18% tires	310°	54% / 52%	sootblowing, reinjection steady state
1700	133	18% tires	305°	55% / 52%	sootblowing, reinjection steady state

\* Based on 4/22/96 bunkering

UNIT 3 TDF / COAL BUNKERING WORKSHEET

BUNKER DATE 4/22/96

BURN DATE 4/23/96

NUMBER OF PAYLOADS OF TIRES 152

TOTAL TONS TIRES 245  
(CONVERSION 3226 LBS TIRES /PAYLOAD)

CONVEYOR H1 START 116289

CONVEYOR H1 STOP 117123

DIFFERENCE 834

CONVEYOR H2 START 934265

CONVEYOR H2 STOP 934784

DIFFERENCE 519

TONS MIX 1353

PERCENT TIRES = TONS TIRES / TONS MIX x 100

PERCENT TIRES = 18%

GANNON STACK TEST PRECIPITATOR LOG - UNIT 3

DATE : 4/23/90

TIME : 0751

RUN NO. : 1 503

INITIALS: CRB

T/R	PRIMARY VOLTS	SECONDARY VOLTS (DC)	PRIMARY AMPS	SECONDARY AMPS (DC)
A1	<u>300</u>	<u>38</u>	<u>45</u>	<u>375</u>
A2	<u>310</u>	<u>30</u>	<u>75</u>	<u>450</u>
A3	<u>330</u>	<u>22</u>	<u>100</u>	<u>575</u>
A4	<u>350</u>	<u>40</u>	<u>75</u>	<u>450</u>
B1	<u>290</u>	<u>44</u>	<u>100</u>	<u>375</u>
B2	<u>290</u>	<u>42</u>	<u>55</u>	<u>350</u>
B3	<u>290</u>	<u>44</u>	<u>55</u>	<u>375</u>
B4	<u>*</u>	<u>*</u>	<u>*</u>	<u>*</u>
C1	<u>310</u>	<u>50</u>	<u>55</u>	<u>375</u>
C2	<u>260</u>	<u>40</u>	<u>45</u>	<u>250</u>
C3	<u>270</u>	<u>40</u>	<u>45</u>	<u>250</u>
C4	<u>250</u>	<u>48</u>	<u>45</u>	<u>225</u>
D1	<u>240</u>	<u>44</u>	<u>40</u>	<u>275</u>
D2	<u>190</u>	<u>30</u>	<u>17</u>	<u>125</u>
D3	<u>280</u>	<u>44</u>	<u>55</u>	<u>325</u>
D4	<u>250</u>	<u>42</u>	<u>45</u>	<u>275</u>

GANNON STACK TEST PRECIPITATOR LOG - UNIT 3

DATE : 4/23/90

TIME : 0945

RUN NO. : 2503

INITIALS: CRB

T/R	PRIMARY VOLTS	SECONDARY VOLTS (DC)	PRIMARY AMPS	SECONDARY AMPS (DC)
A1	<u>290</u>	<u>38</u>	<u>60</u>	<u>375</u>
A2	<u>310</u>	<u>30</u>	<u>70</u>	<u>475</u>
A3	<u>330</u>	<u>20</u>	<u>85</u>	<u>575</u>
A4	<u>350</u>	<u>40</u>	<u>75</u>	<u>450</u>
B1	<u>300</u>	<u>40</u>	<u>65</u>	<u>375</u>
B2	<u>290</u>	<u>42</u>	<u>55</u>	<u>350</u>
B3	<u>290</u>	<u>44</u>	<u>55</u>	<u>350</u>
B4	<u>*</u>	<u>*</u>	<u>*</u>	<u>*</u>
C1	<u>310</u>	<u>48</u>	<u>65</u>	<u>350</u>
C2	<u>270</u>	<u>46</u>	<u>50</u>	<u>250</u>
C3	<u>270</u>	<u>48</u>	<u>45</u>	<u>250</u>
C4	<u>270</u>	<u>48</u>	<u>45</u>	<u>225</u>
D1	<u>200</u>	<u>44</u>	<u>40</u>	<u>275</u>
D2	<u>200</u>	<u>30</u>	<u>17</u>	<u>100</u>
D3	<u>280</u>	<u>42</u>	<u>55</u>	<u>275</u>
D4	<u>240</u>	<u>42</u>	<u>45</u>	<u>275</u>

GANNON STACK TEST PRECIPITATOR LOG - UNIT 3

DATE : 4/23/94

TIME : 1200

RUN NO. : 3 503

INITIALS: CRB

T/R	PRIMARY VOLTS	SECONDARY VOLTS (DC)	PRIMARY AMPS	SECONDARY AMPS (DC)
A1	<u>280</u>	<u>36</u>	<u>50</u>	<u>375</u>
A2	<u>310</u>	<u>32</u>	<u>75</u>	<u>500</u>
A3	<u>330</u>	<u>22</u>	<u>85</u>	<u>575</u>
A4	<u>350</u>	<u>40</u>	<u>75</u>	<u>450</u>
B1	<u>300</u>	<u>46</u>	<u>65</u>	<u>375</u>
B2	<u>290</u>	<u>44</u>	<u>50</u>	<u>325</u>
B3	<u>290</u>	<u>44</u>	<u>55</u>	<u>350</u>
B4	<u>*</u>	<u>*</u>	<u>*</u>	<u>*</u>
C1	<u>250</u>	<u>48</u>	<u>70</u>	<u>250</u>
C2	<u>210</u>	<u>76</u>	<u>45</u>	<u>250</u>
C3	<u>270</u>	<u>48</u>	<u>45</u>	<u>250</u>
C4	<u>270</u>	<u>46</u>	<u>45</u>	<u>250</u>
D1	<u>240</u>	<u>42</u>	<u>50</u>	<u>250</u>
D2	<u>190</u>	<u>30</u>	<u>17</u>	<u>125</u>
D3	<u>280</u>	<u>44</u>	<u>60</u>	<u>325</u>
D4	<u>270</u>	<u>40</u>	<u>50</u>	<u>250</u>

**F. J. GANNON GENERATING STATION  
HEAT INPUT CALCULATIONS**

---

F. J. GANNON STATION BOILER NO. 3 FUEL BLEND PARTICULATE TEST APRIL 23, 1996	
March Gross Heat Rate =	10.233 X 10 <sup>6</sup> Btu/MWH
<b>BOILER NO. 3 SOURCE TEST HEAT INPUT CALCULATIONS</b>	
Final MWH (874224) - Initial MWH( 873721) =	503 MWH
Time =	3.75 Hours
Average MW = 503 MWH ÷ 3.75 H =	134.1 MW
10.233 X 10 <sup>6</sup> Btu/MWH X 503 MWH ÷ 3.75 H =	1372.6 X 10 <sup>6</sup> MMBtu/H

# COMPLIANCE TEST DATA

F. J. GANNON STATION

BOILER NO. 3 TDF/Coal Burn TEST DATE 4/23/96

UNIT LOAD (MN) 133

BASE LOADED (TIME) 5:00 a.m.

**TEST DATA**

MEGAWATTS INTEGRATOR	INITIALS
BEGIN MWH <u>1328</u> BEGIN SAMPLING <u>873721</u>	<u>CRB</u>
END MWH <u>1713</u> END SAMPLING <u>874224</u>	<u>CRB</u>

**SOOTBLOWING**

RUN	BEGIN TIME	END TIME	INITIALS
1 particulate	1328	1423	CRB / JHF
2 particulate	1453	1554	CRB / JHF
3 particulate	1610	1713	CRB / JHF

**FLYASH REINJECTION**

RUN	REINJECTION (Y/N)	% REINJECTION	INITIALS
1 particulate	yes	100%	CRB / JHF
2 particulate	yes	100%	CRB / JHF
3 particulate	yes	100%	CRB / JHF

COMPLIANCE TEST DATA  
F. J. GANNON STATION

INTEGRATOR DATA

RUN NUMBER	START TIME	STOP TIME	INTEGRATOR START	INTEGRATOR STOP
1 particulate	1328	1433	873721	873868
2 particulate	1453	1554	873912	874052
3 particulate	1610	1713	874084	874224

STACK



GANNON STACK TEST PRECIPITATOR LOG - UNIT 3

DATE : 4/23/96

TIME : 1338

RUN NO. : 1 particulate

INITIALS: CRB

T/R	PRIMARY VOLTS	SECONDARY VOLTS (DC)	PRIMARY AMPS	SECONDARY AMPS (DC)
A1	<u>300</u>	<u>36</u>	<u>60</u>	<u>450</u>
A2	<u>320</u>	<u>30</u>	<u>75</u>	<u>475</u>
A3	<u>330</u>	<u>26</u>	<u>85</u>	<u>575</u>
A4	<u>350</u>	<u>40</u>	<u>75</u>	<u>450</u>
B1	<u>300</u>	<u>46</u>	<u>65</u>	<u>375</u>
B2	<u>290</u>	<u>42</u>	<u>50</u>	<u>350</u>
B3	<u>290</u>	<u>44</u>	<u>55</u>	<u>350</u>
B4	<u>*</u>	<u>*</u>	<u>*</u>	<u>*</u>
C1	<u>310</u>	<u>46</u>	<u>75</u>	<u>475</u>
C2	<u>260</u>	<u>46</u>	<u>45</u>	<u>275</u>
C3	<u>270</u>	<u>48</u>	<u>45</u>	<u>250</u>
C4	<u>250</u>	<u>46</u>	<u>50</u>	<u>225</u>
D1	<u>200</u>	<u>42</u>	<u>25</u>	<u>250</u>
D2	<u>190</u>	<u>30</u>	<u>17</u>	<u>125</u>
D3	<u>280</u>	<u>44</u>	<u>50</u>	<u>300</u>
D4	<u>260</u>	<u>44</u>	<u>45</u>	<u>225</u>

GANNON STACK TEST PRECIPITATOR LOG - UNIT 3

DATE : 4/23/94

TIME : 1500

RUN NO. : 2 Particulate

INITIALS: CDB

T/R	PRIMARY VOLTS	SECONDARY VOLTS (DC)	PRIMARY AMPS	SECONDARY AMPS (DC)
A1	<u>300</u>	<u>38</u>	<u>60</u>	<u>400</u>
A2	<u>320</u>	<u>30</u>	<u>75</u>	<u>475</u>
A3	<u>330</u>	<u>24</u>	<u>85</u>	<u>575</u>
A4	<u>350</u>	<u>40</u>	<u>75</u>	<u>450</u>
B1	<u>300</u>	<u>40</u>	<u>65</u>	<u>375</u>
B2	<u>290</u>	<u>44</u>	<u>50</u>	<u>350</u>
B3	<u>290</u>	<u>44</u>	<u>55</u>	<u>350</u>
B4	<u>*</u>	<u>*</u>	<u>*</u>	<u>*</u>
C1	<u>300</u>	<u>48</u>	<u>75</u>	<u>475</u>
C2	<u>260</u>	<u>46</u>	<u>50</u>	<u>275</u>
C3	<u>270</u>	<u>48</u>	<u>40</u>	<u>250</u>
C4	<u>250</u>	<u>48</u>	<u>45</u>	<u>200</u>
D1	<u>240</u>	<u>42</u>	<u>45</u>	<u>250</u>
D2	<u>190</u>	<u>30</u>	<u>17</u>	<u>100</u>
D3	<u>280</u>	<u>44</u>	<u>50</u>	<u>275</u>
D4	<u>240</u>	<u>44</u>	<u>40</u>	<u>250</u>

GANNON STACK TEST PRECIPITATOR LOG - UNIT 3

DATE : 4/23/90

TIME : 1017

RUN NO. : 3 Particulate

INITIALS: CRB

T/R	PRIMARY VOLTS	SECONDARY VOLTS (DC)	PRIMARY AMPS	SECONDARY AMPS (DC)
A1	<u>280</u>	<u>38</u>	<u>70</u>	<u>400</u>
A2	<u>310</u>	<u>30</u>	<u>75</u>	<u>475</u>
A3	<u>330</u>	<u>26</u>	<u>85</u>	<u>575</u>
A4	<u>350</u>	<u>40</u>	<u>80</u>	<u>450</u>
B1	<u>300</u>	<u>76</u>	<u>65</u>	<u>375</u>
B2	<u>290</u>	<u>44</u>	<u>50</u>	<u>350</u>
B3	<u>290</u>	<u>44</u>	<u>55</u>	<u>350</u>
B4	<u>*</u>	<u>*</u>	<u>*</u>	<u>*</u>
C1	<u>300</u>	<u>50</u>	<u>75</u>	<u>475</u>
C2	<u>260</u>	<u>46</u>	<u>50</u>	<u>275</u>
C3	<u>260</u>	<u>46</u>	<u>45</u>	<u>250</u>
C4	<u>250</u>	<u>46</u>	<u>45</u>	<u>225</u>
D1	<u>240</u>	<u>44</u>	<u>45</u>	<u>250</u>
D2	<u>180</u>	<u>30</u>	<u>17</u>	<u>125</u>
D3	<u>280</u>	<u>44</u>	<u>55</u>	<u>250</u>
D4	<u>270</u>	<u>40</u>	<u>45</u>	<u>250</u>

**APPENDIX D**

**CONTINUOUS EMISSION MONITORING DATA**

- D-1 BASELINE CEMS STACK TEST LOGS**
- D-2 FUEL BLEND BURN CEMS STACK TEST LOGS**
- D-3 CONTINUOUS EMISSION MONITOR RELATIVE  
ACCURACY TEST AUDIT RESULTS 1995**
- D-4 CONTINUOUS EMISSION MONITOR QUALITY  
ASSURANCE LINEARITY CHECKS - QUARTER 1  
1996**

**D-1 BASELINE CEMS STACK TESTS LOGS**

=====  
Gannon Station  
Unit 3  
Tampa  
=====

Today's Date: 03/04/96  
Time: 13:23:28

Reporting Period  
Day: 02/28/96

DAILY EPA CEM SUMMARY

Time	CO2 %	SO2 lb/mmBtu	NOX lb/mmBtu	OPACITY %
700	12.1	2.1	1.32	5
800	12.2	2.1	1.26	5
900	12.1	2.1	1.27	5
1000	12.0	2.0	1.30	5
1100	11.7	2.0	1.31	5
1200	11.8	2.0	1.34	5
1300	11.9	2.0	1.37	5
1400	11.2	1.9	1.36	5
1500	10.6	1.9	1.35	5
1600	10.9	1.9	1.33	5
1700	11.1	2.0	1.30	5
1800	11.4	2.0	1.31	5
	11.6	2.0	1.32	5

**D-2 FUEL BLEND BURN CEMS STACK TEST LOGS**

=====  
Gannon Station  
Unit 3  
Tampa  
=====

Today's Date: 04/24/96  
Time: 10:03:52

Reporting Period  
Day: 04/23/96

DAILY EPA CEM SUMMARY

Time	CO2 %	SO2 lb/mmBtu	NOX lb/mmBtu	OPACITY %
800	10.8	2.1	1.10	4
900	10.8	2.0	1.13	4
1000	11.0	2.0	1.14	4
1100	11.2	2.0	1.15	3
1200	11.2	2.0	1.16	3
1300	11.2	2.0	1.14	3
1400	10.3	1.9	1.20	3
1500	9.9	1.9	1.20	3
1600	10.0	2.0	1.13	3
1700	9.5	1.9	1.21	3
	10.6	2.0	1.16	3



**D-3 CONTINUOUS EMISSION MONITOR RELATIVE  
ACCURACY TEST AUDIT RESULTS - 1995**



TAMPA  
ELECTRIC  
A TECO ENERGY COMPANY

**CORPORATE ENVIRONMENTAL SERVICES  
MEMORANDUM**

**SUBJECT:** Continuous Emissions Monitoring (CEM) Systems  
Relative Accuracy Test Audit Results - 1995  
F. J. Gannon Station Boiler No.3

**DATE:** 25, January, 1996

**FROM:** Martin Duff

**TO:** Cindy Barringer

Corporate Environmental Services, Air Programs group, performed a Relative Accuracy Test Audit (RATA) on Boiler No. 3 (GB03), on October 30 thru November 1, 1995. This audit was conducted in accordance with the system supplier's directions, and meet the requirements of 40 CFR 75, Appendix B.

All results were deemed acceptable, meeting the performance specifications of 40 CFR 75, Appendix A, Performance Specification 3.31,3.32,3.33,3.34.

Attached to this memorandum, you will find data summary sheets for each system tested. All testing was performed under my direction, and the results are certified as true and accurate.

These records should be maintained at your facility for a period of three (3) years to comply with 40 CFR 75, Appendix F, Recordingkeeping Requirements. Corporate Environmental Services will maintain all supporting information for this test for the same time period.

Should you have any questions regarding this information, feel free to contact me at extension 38285.

Martin C. Duff  
Technician  
Corporate Environmental Services  
Air Programs

ratarpt.wpd

cc: L.F. Robinson

RELATIVE ACCURACY TEST AUDIT

DATA SUMMARY

PLANT: F.J. GANNON STATION

DATE: 11/01/95

UNIT: UNIT NO.3

MONITOR: SPECTRUM SYSTEMS PRIMARY

COMPARISON: ppm SO2 (wet basis)

OPERATING LEVEL: HIGH

GROSS SOURCE LOAD: 160

VALID OR INVALID RUN	RUN	TIME	RM ppm SO2	CEMS ppm SO2	DIFF ppm SO2
V	1	0845-0906	756.9	770.4	-13.5
V	2	0932-0953	754.9	757.4	-2.5
V	3	1032-1053	751.2	772.1	-20.9
V	4	1129-1150	738.9	742.6	-3.7
V	5	1220-1241	736.9	739.7	-2.8
V	6	1313-1334	725.0	732.0	-7.0
V	7	1421-1442	726.7	698.3	28.4
V	8	1508-1529	727.7	736.1	-8.4
v	9	1615-1636	730.7	738.9	-8.2
I	10	00:00 - 00:00	0.0	0.0	0.0
I	11	00:00 - 00:00	0.0	0.0	0.0
I	12	00:00 - 00:00	0.0	0.0	0.0
I	13	00:00 - 00:00	0.0	0.0	0.0
I	14	00:00 - 00:00	0.0	0.0	0.0
I	15	00:00 - 00:00	0.0	0.0	0.0

REFERENCE MEAN: 738.767 MD: -4.291  
 MEAN CEM: 743.057 STD DEV: 13.582  
 CC: 10.440

NUMBER OF RUNS: 9  
 T-VALUE: 2.306

REL ACCY: 1.99%

BIAS TEST: PASSED  
 BIAS ADJ. (BAF) 1.000

RELATIVE ACCURACY TEST AUDIT

DATA SUMMARY

PLANT: F. J. GANNON STATION

DATE: 11/01/95

UNIT: UNIT NO. 3

MONITOR: SPECTRUM SYSTEMS PRIMARY

COMPARISON: lb NOx/MMBTU

OPERATING LEVEL: HIGH

GROSS SOURCE LOAD:

160

VALID OR INVALID RUN	RUN	TIME	RM lbNOx/ MMBTU	CEMS lbNOx/ MMBTU	DIFF lbNOx/ MMBTU
V	1	0845-0906	1.482	1.497	-0.015
V	2	0932-0953	1.503	1.519	-0.016
V	3	1032-1053	1.443	1.466	-0.023
V	4	1129-1150	1.499	1.509	-0.010
V	5	1220-1241	1.537	1.546	-0.009
V	6	1313-1343	1.626	1.626	0.000
V	7	1421-1442	1.653	1.649	0.004
V	8	1508-1529	1.648	1.672	-0.024
V	9	1615-1636	1.631	1.657	-0.026
I	10	00:00 - 00:00	0.000	0.000	0.000
I	11	00:00 - 00:00	0.000	0.000	0.000
I	12	00:00 - 00:00	0.000	0.000	0.000
I	13	00:00 - 00:00	0.000	0.000	0.000
I	14	00:00 - 00:00	0.000	0.000	0.000
I	15	00:00 - 00:00	0.000	0.000	0.000

REFERENCE MEAN:	1.558	MD:	-0.013
MEAN CEM:	1.571	STD DEV:	0.011
		CC:	0.008

NUMBER OF RUNS: 9  
T-VALUE: 2.306

REL ACCY: 1.37%

BIAS TEST: PASSED  
BIAS ADJ. (BAF) 1.000

RELATIVE ACCURACY TEST AUDIT

DATA SUMMARY

PLANT: F. J. GANNON STATION

DATE: 11/01/95

UNIT: UNIT NO. 3

MONITOR: SPECTRUM SYSTEMS PRIMARY

COMPARISON: Percent CO2 (wet basis)

OPERATING LEVEL: HIGH

GROSS SOURCE LOAD:

160

VALID OR INVALID RUN	RUN	TIME	RM % CO2	CEMS % CO2	DIFF % CO2
V	1	0845-0906	12.26	12.4	-0.2
V	2	0932-0953	12.47	12.5	-0.0
V	3	1032-1053	12.28	12.5	-0.2
V	4	1129-1150	12.47	12.5	0.0
V	5	1220-1241	12.52	12.5	0.0
V	6	1313-1334	12.50	12.5	-0.0
V	7	1421-1442	12.43	12.0	0.4
V	8	1508-1529	12.46	12.5	-0.1
V	9	1615-1636	12.51	12.5	-0.0
I	10	00:00 - 00:00	0.00	0.0	0.0
I	11	00:00 - 00:00	0.00	0.0	0.0
I	12	00:00 - 00:00	0.00	0.0	0.0
I	13	00:00 - 00:00	0.00	0.0	0.0
I	14	00:00 - 00:00	0.00	0.0	0.0
I	15	00:00 - 00:00	0.00	0.0	0.0

REFERENCE MEAN:	12.433	MD:	-0.008
MEAN CEM:	12.441	STD DEV:	0.190
		CC:	0.146
NUMBER OF RUNS:	9		
T-VALUE:	2.306		
		REL ACCY:	1.24%
BIAS TEST:	PASSED		
BIAS ADJ. (BAF)	1.000		

RELATIVE ACCURACY TEST AUDIT

DATA SUMMARY

PLANT: F.J.GANNON

DATE: 11/01/95

UNIT: UNIT NO. 3

MONITOR: SPECTRUM SYSTEMS USI PRIMARY

COMPARISON: STACK FLOW

OPERATING LEVEL: HIGH

GROSS SOURCE LOAD: 160

VALID OR INVALID RUN	RUN	TIME	RM FLOW WSCFH	CEMS FLOW WSCFH	DIFF FLOW WSCFH
V	1	0845-0906	394583	370195	24388
V	2	0932-0953	392482	370907	21575
V	3	1032-1053	391217	370679	20538
V	4	1129-1150	390320	367960	22360
V	5	1220-1241	388726	366795	21931
V	6	1313-1334	388913	367109	21804
V	7	1421-1442	386245	363730	22515
V	8	1508-1529	388064	364937	23127
v	9	1615-1636	384020	361965	22055
i	10	00:00 - 00:00	0	0	0
i	11	00:00 - 00:00	0	0	0
i	12	00:00 - 00:00	0	0	0
i	13	00:00 - 00:00	0	0	0
i	14	00:00 - 00:00	0	0	0
i	15	00:00 - 00:00	0	0	0

REFERENCE MEAN:	389397	MD:	22255
MEAN CEM:	367142	STD DEV:	1069
		CC:	822
NUMBER OF RUNS:	9		
T-VALUE:	2.306		
		REL ACCY:	5.93%
BIAS TEST:	NOT PASSED		
BIAS ADJ. (BAF)	1.061		

RELATIVE ACCURACY TEST AUDIT

DATA SUMMARY

PLANT: F.J.GANNON

DATE: 10/30/95

UNIT: UNIT NO. 3

MONITOR: SPECTRUM SYSTEMS USI

COMPARISON: STACK FLOW

OPERATING LEVEL: MID

GROSS SOURCE LOAD: 125

VALID OR INVALID RUN	RUN	TIME	RM FLOW WSCFH	CEMS FLOW WSCFH	DIFF FLOW WSCFH
I	1	1950-1958	317115	309429	7686
V	2	1959-2007	314989	308465	6524
V	3	2008-2016	316068	309476	6592
I	4	2029-2036	320665	311920	8745
V	5	2037-2045	318395	312024	6371
V	6	2046-2053	318454	313300	5154
V	7	2102-2110	316741	313788	2953
V	8	2111-2118	316373	313673	2700
V	9	2119-2126	317040	312580	4460
V	10	2136-2143	316816	311307	5509
V	11	2144-2151	316663	310000	6663
I	12	2152-2159	319967	310329	9638
I	13	00:00 - 00:00	0	0	0
I	14	00:00 - 00:00	0	0	0
I	15	00:00 - 00:00	0	0	0

REFERENCE MEAN:	316838	MD:	5214
MEAN CEM:	311624	STD DEV:	1547
		CC:	1189
NUMBER OF RUNS:	9		
T-VALUE:	2.306		
		REL ACCY:	2.02%
BIAS TEST:	NOT PASSED		
BIAS ADJ. (BAF)	1.017		

RELATIVE ACCURACY TEST AUDIT

DATA SUMMARY

PLANT: F.J.GANNON

DATE: 10/31/95

UNIT: UNIT NO. 3

MONITOR: SPECTRUM SYSTEMS USI PRIMARY

COMPARISON: STACK FLOW

OPERATING LEVEL: LOW

GROSS SOURCE LOAD: 85

VALID OR INVALID RUN	RUN	TIME	RM FLOW WSCFH	CEMS FLOW WSCFH	DIFF FLOW WSCFH
I	1	2136-2144	277887	266894	10993
V	2	2145-2151	275313	266977	8336
I	3	2152-2159	280308	269187	11121
V	4	2214-2222	275386	267288	8098
V	5	2223-2231	276380	267365	9015
I	6	2232-2238	277878	266269	11609
V	7	2245-2252	277287	267027	10260
V	8	2253-2300	277540	268227	9313
V	9	2301-2308	278215	269633	8582
V	10	2315-2324	275919	266247	9672
V	11	2325-2332	275461	265540	9921
V	12	2333-2340	277154	267547	9607
I	13	00:00 - 00:00	0	0	0
I	14	00:00 - 00:00	0	0	0
I	15	00:00 - 00:00	0	0	0

REFERENCE MEAN:	276517	MD:	9200
MEAN CEM:	267317	STD DEV:	743
		CC:	571

NUMBER OF RUNS: 9  
T-VALUE: 2.306

REL ACCY: 3.53%

BIAS TEST: NOT PASSED  
BIAS ADJ. (BAF) 1.034



RELATIVE ACCURACY TEST AUDIT

DATA SUMMARY

PLANT: F.J. GANNON STATION

DATE: 11/01/95

UNIT: UNIT NO.3

MONITOR: SPECTRUM SYSTEMS BACKUP

COMPARISON: ppm SO2 (wet basis)

OPERATING LEVEL: HIGH

GROSS SOURCE LOAD: 160

VALID OR INVALID RUN	RUN	TIME	RM ppm SO2	CEMS ppm SO2	DIFF ppm SO2
V	1	0845-0906	756.9	769.4	-12.5
V	2	0932-0953	754.9	757.6	-2.7
V	3	1032-1053	751.2	772.1	-20.9
V	4	1129-1150	738.9	743.2	-4.3
V	5	1220-1241	736.9	740.2	-3.3
V	6	1313-1334	725.0	733.4	-8.4
V	7	1421-1442	726.7	698.6	28.1
V	8	1508-1529	727.7	736.1	-8.4
V	9	1615-1636	730.7	738.3	-7.6
I	10	00:00 - 00:00	0.0	0.0	0.0
I	11	00:00 - 00:00	0.0	0.0	0.0
I	12	00:00 - 00:00	0.0	0.0	0.0
I	13	00:00 - 00:00	0.0	0.0	0.0
I	14	00:00 - 00:00	0.0	0.0	0.0
I	15	00:00 - 00:00	0.0	0.0	0.0

REFERENCE MEAN:	738.767	MD:	-4.457
MEAN CEM:	743.224	STD DEV:	13.433
		CC:	10.325

NUMBER OF RUNS: 9  
T-VALUE: 2.306

REL ACCY: 2.00%

BIAS TEST: PASSED  
BIAS ADJ. (BAF) 1.000

RELATIVE ACCURACY TEST AUDIT

DATA SUMMARY

PLANT: F. J. GANNON STATION

DATE: 11/01/95

UNIT: UNIT NO. 3

MONITOR: SPECTRUM SYSTEMS BACKUP

COMPARISON: lb NO<sub>x</sub>/MMBTU

OPERATING LEVEL: HIGH

GROSS SOURCE LOAD:

160

VALID OR INVALID RUN	RUN	TIME	RM lbNO <sub>x</sub> / MMBTU	CEMS lbNO <sub>x</sub> / MMBTU	DIFF lbNO <sub>x</sub> / MMBTU
V	1	0845-0906	1.482	1.463	0.019
V	2	0932-0953	1.503	1.487	0.016
V	3	1032-1053	1.443	1.433	0.010
V	4	1129-1150	1.499	1.476	0.023
V	5	1220-1241	1.537	1.513	0.024
V	6	1313-1334	1.626	1.590	0.036
V	7	1421-1442	1.653	1.606	0.047
V	8	1508-1529	1.648	1.637	0.011
V	9	1615-1636	1.631	1.626	0.005
I	10	00:00 - 00:00	0.000	0.000	0.000
I	11	00:00 - 00:00	0.000	0.000	0.000
I	12	00:00 - 00:00	0.000	0.000	0.000
I	13	00:00 - 00:00	0.000	0.000	0.000
I	14	00:00 - 00:00	0.000	0.000	0.000
I	15	00:00 - 00:00	0.000	0.000	0.000

REFERENCE MEAN:	1.558	MD:	0.021
MEAN CEM:	1.537	STD DEV:	0.013
		CC:	0.010
NUMBER OF RUNS:	9		
T-VALUE:	2.306		
		REL ACCY:	2.02%
BIAS TEST:	NOT PASSED		
BIAS ADJ. (BAF)	1.014		

RELATIVE ACCURACY TEST AUDIT

DATA SUMMARY

PLANT: F. J. GANNON STATION

DATE: 11/01/95

UNIT: UNIT NO. 3

MONITOR: SPECTRUM SYSTEMS BACKUP

COMPARISON: Percent CO2 (wet basis)

OPERATING LEVEL: HIGH

GROSS SOURCE LOAD: 160

VALID OR INVALID RUN	RUN	TIME	RM % CO2	CEMS % CO2	DIFF % CO2
V	1	0845-0906	12.26	12.7	-0.4
V	2	0932-0953	12.47	12.7	-0.2
V	3	1032-1053	12.28	12.8	-0.5
V	4	1129-1150	12.47	12.7	-0.2
V	5	1220-1241	12.52	12.7	-0.2
V	6	1313-1334	12.50	12.7	-0.2
V	7	1421-1442	12.43	12.2	0.2
V	8	1508-1529	12.46	12.8	-0.3
V	9	1615-1636	12.51	12.7	-0.2
I	10	00:00 - 00:00	0.00	0.0	0.0
I	11	00:00 - 00:00	0.00	0.0	0.0
I	12	00:00 - 00:00	0.00	0.0	0.0
I	13	00:00 - 00:00	0.00	0.0	0.0
I	14	00:00 - 00:00	0.00	0.0	0.0
I	15	00:00 - 00:00	0.00	0.0	0.0

REFERENCE MEAN:	12.433	MD:	-0.240
MEAN CEM:	12.674	STD DEV:	0.194
		CC:	0.149

NUMBER OF RUNS: 9  
T-VALUE: 2.306

REL ACCY: 3.13%

BIAS TEST: PASSED  
BIAS ADJ. (BAF) 1.000

RELATIVE ACCURACY TEST AUDIT

DATA SUMMARY

PLANT: F.J.GANNON

DATE: 11/01/95

UNIT: UNIT NO. 3

MONITOR: SPECTRUM SYSTEMS USI BACKUP

COMPARISON: STACK FLOW

OPERATING LEVEL: HIGH

GROSS SOURCE LOAD: 160

VALID OR INVALID RUN	RUN	TIME	RM FLOW WSCFH	CEMS FLOW WSCFH	DIFF FLOW WSCFH
V	1	0845-0906	394583	369491	25092
V	2	0932-0953	392482	370216	22266
V	3	1032-1053	391217	369979	21238
V	4	1129-1150	390320	367251	23069
V	5	1220-1241	388726	367251	21475
V	6	1313-1334	388913	366074	22839
V	7	1421-1442	386245	362898	23347
V	8	1508-1529	388064	364095	23969
v	9	1615-1636	384020	361107	22913
I	10	00:00 - 00:00	0	0	0
I	11	00:00 - 00:00	0	0	0
I	12	00:00 - 00:00	0	0	0
I	13	00:00 - 00:00	0	0	0
I	14	00:00 - 00:00	0	0	0
I	15	00:00 - 00:00	0	0	0

REFERENCE MEAN:	389397	MD:	22912
MEAN CEM:	366485	STD DEV:	1192
		CC:	917

NUMBER OF RUNS: 9  
T-VALUE: 2.306

REL ACCY: 6.12%

BIAS TEST: NOT PASSED  
BIAS ADJ. (BAF) 1.063

RELATIVE ACCURACY TEST AUDIT

DATA SUMMARY

PLANT: F.J.GANNON

DATE: 10/30/95

UNIT: UNIT NO. 3

MONITOR: SPECTRUM SYSTEMS USI BACKUP

COMPARISON: STACK FLOW

OPERATING LEVEL: MID

GROSS SOURCE LOAD:

125

VALID OR INVALID RUN	RUN	TIME	RM FLOW WSCFH	CEMS FLOW WSCFH	DIFF FLOW WSCFH
I	1	1950-1958	317115	308759	8356
V	2	1959-2007	314989	307800	7189
V	3	2008-2016	316068	308800	7268
I	4	2029-2036	320665	311233	9432
V	5	2037-2045	318395	311365	7030
V	6	2046-2053	318454	312627	5827
V	7	2102-2110	316741	313082	3659
V	8	2111-2118	316373	313000	3373
V	9	2119-2126	317040	311920	5120
V	10	2136-2143	316816	310620	6196
V	11	2144-2151	316663	309327	7336
I	12	2152-2159	319967	309648	10319
I	13	00:00 - 00:00	0	0	0
I	14	00:00 - 00:00	0	0	0
I	15	00:00 - 00:00	0	0	0

REFERENCE MEAN:	316838	MD:	5889
MEAN CEM:	310949	STD DEV:	1541
		CC:	1184
NUMBER OF RUNS:	9		
T-VALUE:	2.306		
		REL ACCY:	2.23%
BIAS TEST:	NOT PASSED		
BIAS ADJ. (BAF)	1.019		

DATA SUMMARY

PLANT: F.J.GANNON

DATE: 10/31/95

UNIT: UNIT NO. 3

MONITOR: SPECTRUM SYSTEMS USI BACKUP

COMPARISON: STACK FLOW

OPERATING LEVEL: LOW

GROSS SOURCE LOAD: 85

VALID OR INVALID RUN	RUN	TIME	RM FLOW WSCFH	CEMS FLOW WSCFH	DIFF FLOW WSCFH
I	1	2136-2144	277887	266253	11634
V	2	2145-2151	275313	266277	9036
I	3	2152-2159	280308	268520	11788
V	4	2214-2222	275386	266635	8751
V	5	2223-2231	276380	266682	9698
I	6	2232-2238	277878	265600	12278
V	7	2245-2252	277287	266347	10940
V	8	2253-2300	277540	267587	9953
V	9	2301-2308	278215	268960	9255
V	10	2315-2324	275919	265579	10340
V	11	2325-2332	275461	264847	10614
V	12	2333-2340	277154	267547	9607
I	13	00:00 - 00:00	0	0	0
I	14	00:00 - 00:00	0	0	0
I	15	00:00 - 00:00	0	0	0

REFERENCE MEAN:	276517	MD:	9799
MEAN CEM:	266718	STD DEV:	734
		CC:	564
NUMBER OF RUNS:	9		
T-VALUE:	2.306		
		REL ACCY:	3.75%
BIAS TEST:	NOT PASSED		
BIAS ADJ. (BAF)	1.037		

**D-4 CONTINUOUS EMISSION MONITOR QUALITY  
ASSURANCE LINEARITY CHECKS - QUARTER 1 1996**



TAMPA  
ELECTRIC  
A TECO ENERGY COMPANY

**CORPORATE ENVIRONMENTAL SERVICES  
MEMORANDUM**

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**SUBJECT:** Continuous Emissions Monitoring (CEM) Systems  
Quality Assurance Linearity Checks  
Quarter 1, 1996  
Gannon Unit 3, Primary and Backup

**DATE:** 27, March, 1996

**FROM:** R. A. Mc Darby

**TO:** Cindy Barringer

Corporate Environmental Services, Air Programs group, performed linearity checks on Gannon Unit 3, on March 25, 1996. These checks were conducted in accordance with the system supplier's directions, and meet the requirements of 40 CFR 75, Appendix B, Quality Assurance and Quality Control Procedures.

Linearity checks were performed on the primary and backup systems sequentially. Primary system linearity checks were performed from 13:41 through 15:28. Backup system linearity checks were performed from 16:06 through 17:34. A concerted effort was made to avoid causing any missing data periods during these tests. All final results were deemed acceptable, meeting the performance specifications of 40 CFR 75, Appendix A, section 3.2.

Attached to this memorandum, you will find data summary sheets for each analyzer tested. All testing was performed under my direction, and the results are certified as true and accurate. These records should be maintained at your facility for a period of three (3) years to comply with 40 CFR 75, Appendix F, Recordingkeeping Requirements. Corporate Environmental Services will maintain all supporting information for this test for the same time period.

Should you have any questions regarding this information, feel free to contact me at extension 38306.

Raymond A. Mc Darby  
Quality Assurance Specialist  
Corporate Environmental Services  
Air Programs



**40 CFR 75 Appendix B  
Linearity Check Data**

Unit Under Test Gannon Unit 3  
 Monitor SO2 Test Date 03/25/96  
 Manufacturer Thermo Environmental  
 Serial Number 43B-48171-279  
 Unit ID # GB03 Component ID # 001  
 Monitoring Plan System ID # 311  
 Low-level Bottle Number ALM - 054552  
 Mid-level Bottle Number ALM - 040737  
 High-level Bottle Number ALM - 022399

Protocol  
Expiration Dates  
03/05/98  
03/05/98  
09/11/97

Linearity Check Point	Reading Number & Time of Day	Reference Value (R)	Monitor Response
Low-level	#1 13:51	347.0	345.0
	#2 14:54		353.9
	#3 15:14		354.9
Average Monitor Response (A)			351.267
Linearity Error (LE)			1.2
Linearity Check Point	Reading Number & Time of Day	Reference Value (R)	Monitor Response
Mid-level	#1 14:11	762.0	784.8
	#2 15:01		759.8
	#3 15:20		763.1
Average Monitor Response (A)			769.233
Linearity Error (LE)			0.9
Linearity Check Point	Reading Number & Time of Day	Reference Value (R)	Monitor Response
High-level	#1 14:19	1234.0	1222.1
	#2 15:07		1232.5
	#3 15:28		1233.4
Average Monitor Response (A)			1229.333
Linearity Error (LE)			0.4

**LE = (|R-A|/R)\*100**

**NOTE:**  
 LE must not exceed 5%, or the absolute difference of R - A must be less than or equal to 5 ppm for SO<sub>2</sub> and NO<sub>x</sub> analyzers. For CO<sub>2</sub> analyzers, LE must not exceed 5%, or the absolute difference of R - A must be less than or equal to 0.5% by volume.

**The analyzers must pass at all three levels.**

<b><u>Monitor Summary</u></b>	
Level	
Low	1.2 %
Mid	0.9 %
High	0.4 %

Comments: \_\_\_\_\_

Signature: \_\_\_\_\_

40 CFR 75 Appendix B  
 Linearity Check Data

Unit Under Test Gannon Unit 3  
 Monitor NOx Test Date 03/25/96  
 Manufacturer Thermo Environmental  
 Serial Number 42D-47872-279  
 Unit ID # GB03 Component ID # 003  
 Monitoring Plan System ID # 313  
 Low-level Bottle Number ALM - 054552  
 Mid-level Bottle Number ALM - 040737  
 High-level Bottle Number ALM - 022399

Protocol  
Expiration Dates  
03/05/98  
03/05/98  
09/11/97

Linearity Check Point	Reading Number & Time of Day	Reference Value (R)	Monitor Response
Low-level	#1 13:51	368.0	383.8
	#2 14:54		384.7
	#3 15:14		385.3
Average Monitor Response (A)			384.600
Linearity Error (LE)			4.5
Linearity Check Point	Reading Number & Time of Day	Reference Value (R)	Monitor Response
Mid-level	#1 14:11	825.0	797.1
	#2 15:01		861.6
	#3 15:20		854.0
Average Monitor Response (A)			837.567
Linearity Error (LE)			1.5
Linearity Check Point	Reading Number & Time of Day	Reference Value (R)	Monitor Response
High-level	#1 14:19	1431.0	1461.5
	#2 15:07		1444.8
	#3 15:28		1445.3
Average Monitor Response (A)			1450.533
Linearity Error (LE)			1.4

$LE = (|R-A|/R)*100$

**NOTE:**

LE must not exceed 5%, or the absolute difference of R - A must be less than or equal to 5 ppm for SO<sub>2</sub> and NO<sub>x</sub> analyzers. For CO<sub>2</sub> analyzers, LE must not exceed 5%, or the absolute difference of R - A must be less than or equal to 0.5% by volume.

**The analyzers must pass at all three levels.**

**Monitor Summary**

Level	
Low	4.5 %
Mid	1.5 %
High	1.4 %

Comments: \_\_\_\_\_

Signature: \_\_\_\_\_

40 CFR 75 Appendix B  
Linearity Check Data

Unit Under Test Gannon Unit 3  
 Monitor CO2 Test Date 03/25/96  
 Manufacturer Siemens  
 Serial Number E3-727  
 Unit ID # GB03 Component ID # 005  
 Monitoring Plan System ID # 315  
 Low-level Bottle Number ALM - 054552  
 Mid-level Bottle Number ALM - 040737  
 High-level Bottle Number ALM - 022399

Protocol  
Expiration Dates  
03/05/98  
03/05/98  
09/11/97

Linearity Check Point	Reading Number & Time of Day	Reference Value (R)	Monitor Response
Low-level	#1 13:51	5.00	5.1
	#2 14:54		5.3
	#3 15:14		5.3
Average Monitor Response (A)			5.233
Linearity Error (LE), percent volume			0.2
Linearity Check Point	Reading Number & Time of Day	Reference Value (R)	Monitor Response
Mid-level	#1 14:11	10.90	11.4
	#2 15:01		11.1
	#3 15:20		11.1
Average Monitor Response (A)			11.200
Linearity Error (LE)			2.8
Linearity Check Point	Reading Number & Time of Day	Reference Value (R)	Monitor Response
High-level	#1 14:19	17.94	18.1
	#2 15:07		18.1
	#3 15:28		18.1
Average Monitor Response (A)			18.100
Linearity Error (LE)			0.9

$LE = (|R-A|/R)*100$

**NOTE:**

LE must not exceed 5%, or the absolute difference of R - A must be less than or equal to 5 ppm for SO<sub>2</sub> and NO<sub>x</sub> analyzers. For CO<sub>2</sub> analyzers, LE must not exceed 5%, or the absolute difference of R - A must be less than or equal to 0.5% by volume.

**The analyzers must pass at all three levels.**

**Monitor Summary**

Level	
Low	0.2 %
Mid	2.8 %
High	0.9 %

Comments: \_\_\_\_\_

Signature: \_\_\_\_\_

40 CFR 75 Appendix B  
Linearity Check Data

Unit Under Test Gannon Unit 3 BACKUP  
 Monitor SO2 Test Date 03/25/96  
 Manufacturer Thermo Environmental  
 Serial Number 43B-47950-281  
 Unit ID # GB03 Component ID # 002  
 Monitoring Plan System ID # 312  
 Low-level Bottle Number ALM - 054552  
 Mid-level Bottle Number ALM - 040737  
 High-level Bottle Number ALM - 022399

Protocol  
Expiration Dates  
03/05/98  
03/05/98  
09/11/97

Linearity Check Point	Reading Number & Time of Day	Reference Value (R)	Monitor Response
Low-level	#1 16:13	347.0	353.1
	#2 17:01		353.9
	#3 17:21		360.3
Average Monitor Response (A)			355.767
Linearity Error (LE)			2.5
Linearity Check Point	Reading Number & Time of Day	Reference Value (R)	Monitor Response
Mid-level	#1 16:20	762.0	766.5
	#2 17:07		765.3
	#3 17:28		769.1
Average Monitor Response (A)			766.967
Linearity Error (LE)			0.7
Linearity Check Point	Reading Number & Time of Day	Reference Value (R)	Monitor Response
High-level	#1 16:28	1234.0	1229.1
	#2 17:15		1236.4
	#3 17:34		1235.3
Average Monitor Response (A)			1233.600
Linearity Error (LE)			0.0

$LE = (|R-A|/R) * 100$

**NOTE:**

LE must not exceed 5%, or the absolute difference of R - A must be less than or equal to 5 ppm for SO<sub>2</sub> and NO<sub>x</sub> analyzers. For CO<sub>2</sub> analyzers, LE must not exceed 5%, or the absolute difference of R - A must be less than or equal to 0.5% by volume.

**The analyzers must pass at all three levels.**

**Monitor Summary**

**Level**

Low	2.5 %
Mid	0.7 %
High	0.0 %

Comments: \_\_\_\_\_

Signature: \_\_\_\_\_

40 CFR 75 Appendix B  
Linearity Check Data

Unit Under Test Gannon Unit 3 BACKUP  
 Monitor NOx Test Date 03/25/96  
 Manufacturer Thermo Environmental  
 Serial Number 42D-47871-279  
 Unit ID # GB03 Component ID # 004  
 Monitoring Plan System ID # 314  
 Low-level Bottle Number ALM - 054552  
 Mid-level Bottle Number ALM - 040737  
 High-level Bottle Number ALM - 022399

Protocol  
Expiration Dates  
03/05/98  
03/05/98  
09/11/97

Linearity Check Point	Reading Number & Time of Day	Reference Value (R)	Monitor Response
Low-level	#1 16:13	368.0	384.2
	#2 17:01		383.6
	#3 17:21		381.8
Average Monitor Response (A)			383.200
Linearity Error (LE)			4.1
Linearity Check Point	Reading Number & Time of Day	Reference Value (R)	Monitor Response
Mid-level	#1 16:20	825.0	857.5
	#2 17:07		855.0
	#3 17:28		854.0
Average Monitor Response (A)			855.500
Linearity Error (LE)			3.7
Linearity Check Point	Reading Number & Time of Day	Reference Value (R)	Monitor Response
High-level	#1 16:28	1431.0	1441.4
	#2 17:15		1445.5
	#3 17:34		1441.7
Average Monitor Response (A)			1442.867
Linearity Error (LE)			0.8

$$LE = (|R-A|/R) * 100$$

**NOTE:**

LE must not exceed 5%, or the absolute difference of R - A must be less than or equal to 5 ppm for SO<sub>2</sub> and NO<sub>x</sub> analyzers. For CO<sub>2</sub> analyzers, LE must not exceed 5%, or the absolute difference of R - A must be less than or equal to 0.5% by volume.

**The analyzers must pass at all three levels.**

**Monitor Summary**

Level	
Low	4.1 %
Mid	3.7 %
High	0.8 %

Comments: \_\_\_\_\_

Signature: \_\_\_\_\_

40 CFR 75 Appendix B  
Linearity Check Data

Unit Under Test Gannon Unit 3 BACKUP  
 Monitor CO2 Test Date 03/25/96  
 Manufacturer Siemens  
 Serial Number E2-786  
 Unit ID # GB03 Component ID # 006  
 Monitoring Plan System ID # 316  
 Low-level Bottle Number ALM - 054552  
 Mid-level Bottle Number ALM - 040737  
 High-level Bottle Number ALM - 022399

Protocol  
Expiration Dates  
03/05/98  
03/05/98  
09/11/97

Linearity Check Point	Reading Number & Time of Day	Reference Value (R)	Monitor Response
Low-level	#1 16:13	5.00	5.2
	#2 17:01		5.2
	#3 17:21		5.3
Average Monitor Response (A)			5.233
Linearity Error (LE), percent volume			0.2
Linearity Check Point	Reading Number & Time of Day	Reference Value (R)	Monitor Response
Mid-level	#1 16:20	10.90	11.1
	#2 17:07		11.1
	#3 17:28		11.1
Average Monitor Response (A)			11.100
Linearity Error (LE)			1.8
Linearity Check Point	Reading Number & Time of Day	Reference Value (R)	Monitor Response
High-level	#1 16:28	17.94	17.8
	#2 17:15		17.9
	#3 17:34		17.8
Average Monitor Response (A)			17.833
Linearity Error (LE)			0.6

$LE = (|R-A|/R) * 100$

**NOTE:**

LE must not exceed 5%, or the absolute difference of R - A must be less than or equal to 5 ppm for SO<sub>2</sub> and NO<sub>x</sub> analyzers. For CO<sub>2</sub> analyzers, LE must not exceed 5%, or the absolute difference of R - A must be less than or equal to 0.5% by volume.

**The analyzers must pass at all three levels.**

**Monitor Summary**

Level	
Low	0.2 %
Mid	1.8 %
High	0.6 %

Comments: \_\_\_\_\_

Signature: \_\_\_\_\_

**APPENDIX E**

**FUEL ANALYSIS**

- E-1 BASELINE WEEKLY COMPOSITE**
- E-2 FUEL BLEND BURN WEEKLY COMPOSITES**
- E-3 TIRE DERIVED FUEL ANALYSIS**

**E-1 BASELINE WEEKLY COMPOSITE**





Data for Trace Elements in Coal by ICP:

Trace Metals in Coal and Coke by Inductively Coupled Plasma  
Digestion Method: ASTM D-3683  
Analysis Method: Inductively Coupled Plasma

Beryllium by ICP.....	0.96	ug/g
Chromium by ICP.....	7.53	ug/g
Nickel by ICP.....	9.32	ug/g
Lead by ICP.....	12.8	ug/g
Vanadium by ICP.....	17.2	ug/g
Zinc by ICP.....	25.4	ug/g

Note: All results reported represent concentrations in coal on a DRY BASIS.

Sample comments:

Trace Metal analysis request added 05/08/96

If there are any questions regarding this data, please call.

Robert L. Dorey  
Supervisor of Laboratory Services

**E-2 FUEL BLEND BURN WEEKLY COMPOSITES**



Data for Trace Elements in Coal by ICP:

Trace Metals in Coal and Coke by Inductively Coupled Plasma  
Digestion Method: ASTM D-3683  
Analysis Method: Inductively Coupled Plasma

Beryllium by ICP.....	1.22	ug/g
Chromium by ICP.....	6.97	ug/g
Nickel by ICP.....	9.45	ug/g
Lead by ICP.....	5.71	ug/g
Vanadium by ICP.....	17.4	ug/g
Zinc by ICP.....	25.3	ug/g

Note: All results reported represent concentrations in coal on a DRY BASIS.

Sample comments:

Trace Metals analysis request added 05/08/96

If there are any questions regarding this data, please call.

Robert L. Dorey  
Supervisor of Laboratory Services

**E-3 TIRE DERIVED FUEL ANALYSIS**



# COMMERCIAL TESTING & ENGINEERING CO.

GENERAL OFFICES: 1819 SOUTH HIGHLAND AVE., SUITE 210-B, LOMBARD, ILLINOIS 60148 • TEL: 708-953-9300 FAX: 708-953-9306

Member of the SGS Group (Société Générale de Surveillance)

PLEASE ADDRESS ALL CORRESPONDENCE TO:  
18130 VAN DRUENEN RD.  
SOUTH HOLLAND, IL 60473  
TEL: (708) 331-2900  
FAX: (708) 333-3060

May 13, 1996

TAMPA ELECTRIC  
Corporate Environmental Svcs.  
5010 Causeway Blvd.  
Tampa, FL 33619  
Attn: Robert L. Dorey

Sample identification by  
Tampa Electric

Kind of sample reported to us TDF

Sample ID: TDF

Sample taken at -----

Sample taken by -----

Date sampled -----

P.O. No. EN35816

Date received May 1, 1996

REVISED REPORT 5/13/96

Analysis Report No. 71-24828

Page 1 of 2

### PROXIMATE ANALYSIS

	<u>As Received</u>	<u>Dry Basis</u>	
% Moisture	5.57	XXXXXX	
% Ash	12.54	13.28	
% Volatile	45.31	47.98	
% Fixed Carbon	<u>36.58</u>	<u>38.74</u>	
	100.00	100.00	
Btu/lb	13697	14505	MAF 16726
% Sulfur	1.52	1.61	
% CARBON	57.87	61.28	
% NITROGEN	0.72	0.76	

### METHODS

Moisture: ASTM D 3302; Ash: ASTM D 3174; Volatile: ASTM D 3175; Fixed Carbon: Calculated Value; ASTM D 3172  
Btu/lb: ASTM D 3286; Sulfur: ASTM D 4239 (Method C); Carbon & Nitrogen: ASTM D 5375

Respectfully submitted,  
COMMERCIAL TESTING & ENGINEERING CO.

Manager, South Holland Laboratory



OVER 40 BRANCH LABORATORIES STRATEGICALLY LOCATED IN PRINCIPAL COAL MINING AREAS, TIDEWATER AND GREAT LAKES PORTS, AND RIVER LOADING FACILITIES



# COMMERCIAL TESTING & ENGINEERING CO.

GENERAL OFFICES: 1919 SOUTH HIGHLAND AVE., SUITE 210-B, LOMBARD, ILLINOIS 60148 • TEL. 708-953-9300 FAX: 708-953-9306

Member of the SGS Group (Société Générale de Surveillance)

PLEASE ADDRESS ALL CORRESPONDENCE TO:  
16130 VAN DRUNEN RD.  
SOUTH HOLLAND, IL 60473  
TEL: (708) 331-2900  
FAX: (708) 333-3060

May 13, 1996

TAMPA ELECTRIC  
Corporate Environmental Svcs.  
5010 Causeway Blvd.  
Tampa, FL 33619  
Attn: Robert L. Dorey

Sample identification by  
Tampa Electric

Kind of sample reported to us TDF

Sample ID: TDF

Sample taken at -----

Sample taken by -----

Date sampled -----

P.O. No. SN35816

Date received May 1, 1996

REVISED REPORT 5/13/96

Analysis Report No. 71-24828

Page 2 of 2

Dry Basis, ug/g

Beryllium, Be	3
Chromium, Cr	9
Lead, Pb	21
Nickel, Ni	19
Mercury, Hg	0.04
Vanadium, V	9
Zinc, Zn	4327

METHOD

Mercury: Double Gold Amalgamation, Cold Vapor Atomic Absorption; Remaining Parameters: ASTM D 3683

Respectfully submitted,  
COMMERCIAL TESTING & ENGINEERING CO.



Manager, South Holland Laboratory

OVER 40 BRANCH LABORATORIES STRATEGICALLY LOCATED IN PRINCIPAL COAL MINING AREAS, TIDEWATER AND GREAT LAKES PORTS, AND RIVER LOADING FACILITIES



## **APPENDIX F**

### **FIELD DATA SHEETS**

- F-1 BASELINE PARTICULATE DATA SHEETS**
- F-2 BASELINE SULFURIC ACID DATA SHEETS**
- F-3 BASELINE ORSAT DATA SHEETS**
- F-4 BASELINE VISIBLE EMISSIONS DATA SHEETS**
- F-5 FUEL BLEND BURN PARTICULATE DATA SHEETS**
- F-6 FUEL BLEND BURN SULFURIC ACID MIST DATA SHEETS**
- F-7 FUEL BLEND BURN ORSAT DATA SHEETS**
- F-8 FUEL BLEND VISIBLE EMISSIONS DATA SHEETS**

**F-1 BASELINE PARTICULATE DATA SHEETS**















**F-2 BASELINE SULFURIC ACID DATA SHEETS**

H.S. of  
PARTICULATE FIELD DATA FORM

Plant F.J. Gannon Station  
 Location Boiler No. 3  
 Method US EPA Method 8  
 Operator Mantiduff/ROS/RAS  
 Date February 28 1996  
 Run Number 1  
 Min./Pt. 3  
 Stack Area ft<sup>2</sup> 121.225  
 Sample Box Number N/A  
 Meter Box Number 6  
 Meter ΔH@ 1.706  
 Meter Calibration (Y) 1.006  
 Nozzle I.D. No. 16 (0.198)  
 Nozzle Diameter (0.194)

Pitot Tube (C.) 0.84  
 Probe Length 8'  
 Probe Liner Material GLASS  
 Probe Heater Setting 250°  
 Ambient Temperature 65°  
 Barometric Pressure (P<sub>b</sub>) 29.80 in. Hg  
 Assumed Moisture 9.0%  
 Static Pressure (P<sub>s</sub>) 2.12 in. Hg  
 Time - Start 0728 End 0834  
 Total Sample Time 60 Min.  
 Gas Analysis CO<sub>2</sub> \_\_\_\_\_ % O<sub>2</sub> \_\_\_\_\_ %  
 CO<sub>2</sub> \_\_\_\_\_ % O<sub>2</sub> \_\_\_\_\_ %  
 Comments \_\_\_\_\_

Dry Gas Meter Volume  
 Final 637.812 Ft<sup>3</sup>  
 Initial 604.396 Ft<sup>3</sup>  
 Net 33.416 Ft<sup>3</sup>

Equipment Leak Checks  
 Initial 0.00 CFM@ 15"Hg  
 Final 0.00 CFM@ 8"Hg  
 Pitot Tube OK 0.00 7" H<sub>2</sub>O

Moisture Determination  
 Impinger 58 ml  
 Silica Gel 17.5 gm  
 Total 75.5 ml

Traverse Point Number	Clock Time	Gas Sample Volume (Ft <sup>3</sup> )	ΔP (In. H <sub>2</sub> O)	ΔH (In. H <sub>2</sub> O)	Stack Temp. Ts (°F)	Meter Temp. Tm (°F)	Unbilled Sample Box Temp. (°F)	Probe Temp. (°F)	Last Imp. Temp. (°F)	Vacuum (In. Hg.)
1	0728	606.7	1.20	1.13	264	72	255	303	58	7
2		607.8	1.00	0.94	265	74	256	308	55	6
3		609.3	0.95 +1.15 NO	0.87 +1.08 NO	265 256 NO	75	256 265 NO	307	57	5
4		611.0	0.93	0.87	265 257 NO	76	251	308	59	5
5	0743	612.4	0.83	0.78	263	76	250	306	61	5

Traverse Point Number	Clock Time	Gas Sample Volume (Ft <sup>3</sup> )	$\Delta P$ (In. H <sub>2</sub> O)	$\Delta H$ (In. H <sub>2</sub> O)	Stack Temp. Ts (°F)	Meter Temp. Tm (°F)	<sup>Umbilical</sup> Sample Box Temp. (°F)	Probe Temp. (°F)	Last Imp. Temp. (°F)	Vacuum (In. Hg.)
1	0744	614.5	1.10	1.03	264	77	254	300	61	6
2		615.8	0.92	0.86	264	78	251	300	61	6
3		617.5	0.96	0.90	264	79	252	300	61	6
4		619.3	0.95	0.90	262	80	250	299	60	6
5	0759	620.6	0.82	0.82	260	80	255	291	62	6
1	0802	622.5	1.20	1.19	260	76	255	306	61	7
2		623.6	0.98	0.97	264	80	254	306	59	7
3		625.9	1.05	1.05	264	81	255	306	59	7
4		627.6	1.10	<del>1.10</del> 1.09	<del>263</del> 263	81	255	307	60	7
5	0817	629.3	0.90	0.89	262	82	253	308	61	7
1	0821	631.9	0.97	0.94	265	78	255	308	62	7
2		633.0	1.10	1.09	265	80	255	308	58	6
3		635.3	1.10	1.09	265	80	255	308	58	6
4		636.3	1.10	1.09	265	80	251	302	59	6
5	0834	637.812	0.88	0.87	263	81	256	294	59	6

H2564  
**PARTICULATE FIELD DATA FORM**

Plant F. J. Cannon  
 Location Oiler No 3  
 Method Method RPA 8  
 Operator M. D. A. / KAS / JOS  
 Date February 29, 1994  
 Run Number 2  
 Min./Pt. 3  
 Stack Area ft<sup>2</sup> 121.225  
 Sample Box Number W/A  
 Meter Box Number 6  
 Meter ΔH@ 1.704  
 Meter Calibration (Y) 1.000  
 Nozzle I.D. No. 16  
 Nozzle Diameter (0.198)

Pitot Tube (C.) 0.84  
 Probe Length 8'  
 Probe Liner Material Celco 55  
 Probe Heater Setting 300° 250°  
 Ambient Temperature 70  
 Barometric Pressure (P<sub>b</sub>) 29.80 in. Hg  
 Assumed Moisture 8.0%  
 Static Pressure (P<sub>s</sub>) 29.80 in. Hg  
 Time - Start 0921<sup>a</sup> End 1028  
 Total Sample Time 60 Min.  
 Gas Analysis CO<sub>2</sub> \_\_\_\_\_ % O<sub>2</sub> \_\_\_\_\_ %  
                   CO<sub>2</sub> \_\_\_\_\_ % O<sub>2</sub> \_\_\_\_\_ %  
 Comments \_\_\_\_\_

Dry Gas Meter Volume  
 Final 679.230 Ft<sup>3</sup>  
 Initial 645.307 Ft<sup>3</sup>  
 Net 33.923 Ft<sup>3</sup>

Equipment Leak Checks  
 Initial 0.00 CFM@ 15 "Hg  
 Final 0.00 CFM@ 7 "Hg  
 Pitot Tube OK

Moisture Determination  
 Impinger 59 ml  
 Silica Gel 13.3 gm  
 Total 72.3 ml

Traverse Point Number	Clock Time	Gas Sample Volume (Ft <sup>3</sup> )	ΔP (In. H <sub>2</sub> O)	ΔH (In. H <sub>2</sub> O)	Stack Temp. Ts (°F)	Meter Temp. Tm (°F)	<sup>Unofficial</sup> Sample Box Temp. (°F)	Probe Temp. (°F)	Last Imp. Temp. (°F)	Vacuum (In. Hg.)
1	921	646.9	1.10	1.09	266	74	250	281	60	5
2		649.2	1.05	1.05	268	78	250	272	56	5
3		651.3	1.10	1.09	270	79	250	268	56	5
4		652.2	1.10	1.09	267	79	251	269	56	5
5	0936	654.1	0.85	0.85	265	70	252	269	57	5

Traverse Point Number	Clock Time	Gas Sample Volume (Ft <sup>3</sup> )	ΔP (In. H <sub>2</sub> O)	ΔH (In. H <sub>2</sub> O)	Stack Temp. Ts (°F)	Meter Temp. Tm (°F)	Sample Box Temp. (°F)	Probe Temp. (°F)	Last Imp. Temp. (°F)	Vacuum (In. Hg.)
1	09:37	655.8	1.10	1.10	269	79	253	268	58	4
2		657.7	1.10	1.10	268	80	253	268	57	4
3		659.4	1.05	1.05	268	80	252	267	57	4
4		661.1	1.05	1.05	267	80	252	268	58	4
5	09:52	662.8	0.90	0.90	266	82	253	267	58	4
1	09:54	664.5	1.10	1.10	267	81	256	265	59	4
2		666.3	1.00	1.00	267	82	253	264	57	4
3		667.9	0.95	0.95	267	82	256	264	57	4
4		669.5	0.90	0.90	266	83	257	264	58	4
5	10:09	670.8	0.50	0.50	264	82	256	265	59	2
1	10:13	672.9	1.15	1.14	269	81	256	271	60	4
2		674.4	<del>0.94</del> 0.82	<del>0.94</del> 0.82	269	80	256	272	60	4
3		677.1	0.96	0.96	269	82	252	274	59	4
4		677.7	0.96	0.96	269	82	252	274	59	4
5	10:28	677.2 <sup>30</sup>	0.84	0.84	267	83	254	273	60	4

H<sub>2</sub>Sed  
PARTICULATE FIELD DATA FORM

Plant F. J. Gannett  
 Location Boiler No. 3  
 Method USEPA 8  
 Operator M. Duff RAB POS  
 Date 2/28/96  
 Run Number 3  
 Min./Pt. 3  
 Stack Area ft<sup>2</sup> 122.121.225  
 Sample Box Number N/A  
 Meter Box Number 6  
 Meter ΔH@ 1.704  
 Meter Calibration (Y) 1,000  
 Nozzle I.D. No. 14  
 Nozzle Diameter (0.198)

Pitot Tube (C.) 0.84  
 Probe Length 8'  
 Probe Liner Material Cl<sub>2</sub>  
 Probe Heater Setting 250° F  
 Ambient Temperature 76  
 Barometric Pressure (P<sub>b</sub>) 29.85 in. Hg  
 Assumed Moisture 9.0  
 Static Pressure (P<sub>a</sub>) 29.85 in. Hg  
 Time - Start 1114 End 1129 1220  
 Total Sample Time 60 min Min.  
 Gas Analysis CO<sub>2</sub> \_\_\_\_\_ % O<sub>2</sub> \_\_\_\_\_ %  
 CO<sub>2</sub> \_\_\_\_\_ % O<sub>2</sub> \_\_\_\_\_ %  
 Comments \_\_\_\_\_

Dry Gas Meter Volume  
 Final 720.856 Ft<sup>3</sup>  
 Initial 687.100 Ft<sup>3</sup>  
 Net 33.756 Ft<sup>3</sup>

Equipment Leak Checks  
 Initial 0.00 CFM@ 15 "Hg  
 Final 6.00 CFM@ 7 "Hg  
 Pitot Tube OR

Moisture Determination  
 Impinger 39 ml  
 Silica Gel 12.6 gm  
 Total 71.6 ml

Traverse Point Number	Clock Time	Gas Sample Volume (Ft <sup>3</sup> )	ΔP (In. H <sub>2</sub> O)	ΔH (In. H <sub>2</sub> O)	Stack Temp. Ts (°F)	Meter Temp. Tm (°F)	Duplicate Sample Box Temp. (°F)	Probe Temp. (°F)	Last Imp. Temp. (°F)	Vacuum (In. Hg.)
1	1114	689.2	1.10	1.09	269	84	255	268	62	5
2		690.2	0.96	0.958	268	85	252	270	61	5
3		692.1	1.10	1.09	268	85	251	270	61	5
4		693.8	0.88	0.88	269	87	256	269	61	5
5	1129	695.4	0.78	0.78	267	88	256	270	61	5

*M. Duff RAB*

Traverse Point Number	Clock Time	Gas Sample Volume (Ft <sup>3</sup> )	$\Delta P$ (In. H <sub>2</sub> O)	$\Delta H$ (In. H <sub>2</sub> O)	Stack Temp. Ts (°F)	Meter Temp. Tm (°F)	Umbil Sample Box Temp. (°F)	Probe Temp. (°F)	Last Imp. Temp. (°F)	Vacuum (In. Hg.)
1	1230	697.1	1.05	1.05	268	88	253	265	62	5
2		699.1	1.05	1.05	268	88	253	265	62	5
3		701.1	1.08	1.08	265	90	258	265	62	5
4		702.6	0.92	0.92	267	91	258	264	61	5
5	1245	703.9	0.95	0.95	265	91	258	264	62	5
1	1247	705.8	1.03	1.03	268	88	252	268	<sup>62</sup> 68	5
2		707.7	1.00	1.00	268	90	258	272	59	5
3		709.4	1.08	1.08	268	90	254	269	60	5
4		711.4	1.10	1.10	266	91	255	270	62	6
5	1202	712.5	0.86	0.86	269	91	253	270	63	5
1	1205	714.5	0.99	0.99	268	91	253	264	63	5
2		716.9	0.98	0.98	269	92	256	266	63	5
3		718.4	0.94	0.96	268	92	252	266	63	5
4		719.5	0.97	0.97	267	93	252	265	65	5
5	1220	720.856	0.83	0.83	264	92	252	264	64	5

**F-3 BASELINE ORSAT DATA SHEETS**



## ORSAT DATA AND CALCULATION SHEET

Source Gannon station

Location Boiler No. 3

Run No.	Date	Gas	Orsat Analysis, Dry Basis (% Volume)				Remarks
			1	2	3	Avg.	
1-5	2-28-94	CO <sub>2</sub>	13.8	13.8	13.8	13.8	ND
		O <sub>2</sub>	5.0	5.0	5.0	5.0	
		CO	0.0	0.0	0.0	0.0	
		N <sub>2</sub>	81.2	81.2	81.2	81.2	
2-5	2-28-94	CO <sub>2</sub>	13.8	13.8	13.8	13.8	ND
		O <sub>2</sub>	5.2	5.2	5.2	5.2	
		CO	0.0	0.0	0.0	0.0	
		N <sub>2</sub>	81.0	81.0	81.0	81.0	
3-5	2-28-94	CO <sub>2</sub>	13.2	13.2	13.2	13.2	ND
		O <sub>2</sub>	5.4	5.4	5.4	5.6	
		CO	0.0	0.0	0.0	0.0	
		N <sub>2</sub>	81.2	81.2	81.2	81.2	

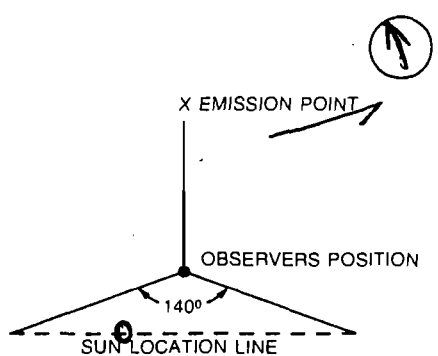

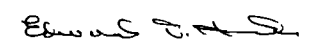
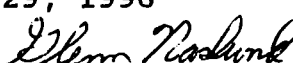
# ORSAT DATA AND CALCULATION SHEET

Source Boiler No. 3

Location Garage Station

Run No.	Date	Gas	Orsat Analysis, Dry Basis (% Volume)				Remarks
			1	2	3	Avg.	
1	2/28/94	CO <sub>2</sub>	12.8	12.8	12.8	12.8	Method 8 Sulphur Acid M. st ND
		O <sub>2</sub>	6.0	6.0	6.0	6.0	
		CO	0.0	0.0	0.0	0.0	
		N <sub>2</sub>	81.2	81.2	81.2	81.2	
2	2/28/94	CO <sub>2</sub>	13.8	13.8	13.8	13.8	Method 8 H <sub>2</sub> Soy ND
		O <sub>2</sub>	5.4	5.2	5.3	5.3	
		CO	0.0	0.0	0.0	0.0	
		N <sub>2</sub>	80.8	81.0	80.9	80.9	
3	2/28/94	CO <sub>2</sub>	13.2	13.2	13.2	13.2	Method 8 H <sub>2</sub> Soy ND
		O <sub>2</sub>	5.2	5.2	5.2	5.2	
		CO	0.0	0.0	0.0	0.0	
		N <sub>2</sub>	81.6	81.6	81.6	81.6	

**F-4 BASELINE VISIBLE EMISSIONS DATA SHEETS**

SOURCE NAME <b>Boiler #3</b>		SOURCE LOCATION <b>Gannon Station</b>		OBSERVATION DATE <b>2/28/96</b>		START TIME <b>1634</b>		STOP TIME <b>1734</b>	
TYPE OF FACILITY <b>Coal Fired Boiler</b>		SEC.		MIN		SEC		MIN	
DISTANCE FROM OBSERVER <b>1000'</b>		MIN		0		15		30	
SKY CONDITIONS/PLUME BACKGROUND <b>Partly Cloudy to Blue Skies</b>		MIN		45		0		15	
SOURCE LAYOUT SKETCH      DRAW NORTH ARROW 		MIN		30		45		0	
		MIN		0		15		30	
		MIN		45		0		15	
		MIN		30		45		0	
		MIN		0		15		30	
		MIN		45		0		15	
		MIN		30		45		0	
		MIN		0		15		30	
		MIN		45		0		15	
		MIN		30		45		0	
AVERAGE OPACITY <b>5.0 %</b>		MIN		0		15		30	
WIND SPEED (EST.) <b>5-10 mph</b>		MIN		45		0		15	
WIND DIRECTION (EST.) <b>West</b>		MIN		30		45		0	
OBSERVER'S NAME (PRINT) <b>Glenn Naslund</b>		MIN		0		15		30	
OBSERVER'S SIGNATURE <i>Glenn Naslund</i>		MIN		45		0		15	
DATE <b>2/28/96</b>		MIN		30		45		0	
COMMENTS <b>Soot-Blowing Run</b>		MIN		0		15		30	
COPY OF VISIBLE EMISSIONS CERTIFICATION CARD		MIN		45		0		15	
STATE OF FLORIDA DEPARTMENT OF ENVIRONMENTAL REGULATION  THIS IS TO CERTIFY THAT <b>GLENN NASLUND</b> has completed the STATE OF FLORIDA visible emissions evaluation training and is a qualified observer of visible emissions as specified by EPA reference method 9. THIS CERTIFICATE EXPIRES <b>Feb 29, 1996</b>  CERTIFICATE OFFICER  BEARER'S SIGNATURE		MIN		30		45		0	
		MIN		0		15		30	
		MIN		45		0		15	
		MIN		30		45		0	
		MIN		0		15		30	
		MIN		45		0		15	
		MIN		30		45		0	
		MIN		0		15		30	
		MIN		45		0		15	
		MIN		30		45		0	

**F5 FUEL BLEND BURN PARTICULATE DATA SHEETS**















**F6 FUEL BLEND BURN SULFURIC ACID MIST DATA SHEETS**

**Sulfuric Acid Mist Field Data Form**

Plant F. J. GANNON  
 Location Boiler No. 3  
 Method USEPA Method 8  
 Operator DAVID SMITH  
 Date 4-23-96  
 Run No. 1-5  
 Min. | Pt. 3  
 Stack Area Ft.<sup>2</sup> 122.718  
 Sample Box No. N/A  
 Meter Box No. 6  
 Meter ΔH 1.681  
 Meter Cal. (M) 1,000  
 Nozzle I.D. No. 6  
 Nozzle Diameter 0.197

Pitot Tube (C) 0.84  
 Probe Length 10  
 Probe Liner Material inconel  
 Probe Heater Setting 250  
 Ambient Temperature 76  
 Barometric Pressure (P<sub>b</sub>) 30.00 in. Hg  
 Static Pressure (P<sub>s</sub>) 30.00 in. Hg  
 Assumed Moisture (%) 8.0%  
 Time - Start 0747 End 0853  
 Total Sampling Time 60 min. Min.  
 Comments So blowing this run  
TDI Test Blend

Dry Gas Meter Volume  
 Final 576.941 Ft.<sup>3</sup>  
 Initial 545.866 Ft.<sup>3</sup>  
 Net 31.075 Ft.<sup>3</sup>

Equipment Leak Checks  
 Initial 0.0 CFM@ 15 "Hg  
 Final 0.0 CFM@ 2 "Hg  
 Pitot Tube 0.0 @ 7.5 "H<sub>2</sub>O

Moisture Determination  
 Impinger 30 ml  
 Silica Gel 20.4 gm  
 Total 50.4

Traverse Point No.	Clock Time	Gas Sample Volume (Ft. <sup>3</sup> )	ΔP (In. H <sub>2</sub> O)	ΔH (In. H <sub>2</sub> O)	Probe Temp. (°F)	Stack Temp. Ts (°F)	Umbilical Temp (°F)	Meter Temp. Tm (°F)	Last Imp. Temp. (°F)	Vacuum (In. Hg.)
1	0747	547.2	0.96	0.92	263	265	267	77	68	7
2		548.8	0.92	0.88	268	268	257	80	68	6.5
3		550.6	0.92	0.88	257	268	256	81	68	6.5
4		552.0	0.90	0.87	256	268	255	81	68	6
5	0802	553.4	0.82	0.79	255	265	257	82	68	6
1	0804	555.2	0.99	0.95	253	269	258	81	65	6.5
2		556.7	0.91	0.87	251	268	256	81	65	6
3		558.4	0.95	0.91	248	267	256	82	65	6.5
4		560.0	0.95	0.91	249	266	258	82	65	6.5
5	0819	561.5	0.84	0.81	247	264	257	82	66	6



**Sulfuric Acid Mist Field Data Form**

Plant F. S. GANNON  
 Location Boiler No. 3  
 Method USEPA Method 8  
 Operator David Smith  
 Date 4-23-96  
 Run No. 2-5  
 Min. 1 Pt. 3  
 Stack Area Ft.<sup>2</sup> 122.718  
 Sample Box No. N/A  
 Meter Box No. 6  
 Meter ΔH 1.681  
 Meter Cal. (Y) 1.000  
 Nozzle I.D. No. 37  
 Nozzle Diameter .212

Pitot Tube (C<sub>p</sub>) 0.84  
 Probe Length 10  
 Probe Liner Material neave  
 Probe Heater Setting 250  
 Ambient Temperature 86  
 Barometric Pressure (P<sub>b</sub>) 30.00 in. Hg  
 Static Pressure (P<sub>s</sub>) 30.00 in. Hg  
 Assumed Moisture (%) 8.0  
 Time - Start 0941 End 1046  
 Total Sampling Time 60 min Min.  
 Comments Subsiding this Run  
TDI: test Blend

Dry Gas Meter Volume  
 Final 622.755 Ft.<sup>3</sup>  
 Initial 585.625 Ft.<sup>3</sup>  
 Net 37.130 Ft.<sup>3</sup>

Equipment Leak Checks  
 Initial 0.0 CFM@ 15 \*Hg  
 Final 0.0 CFM@ 8.5 \*Hg  
 Pitot Tube 0.0 @ 2.5 \*H<sub>2</sub>O

Moisture Determination  
 Impinger 62 ml  
 Silica Gel 17.2 gm  
 Total 79.2

Traverse Point No.	Clock Time	Gas Sample Volume (Ft <sup>3</sup> )	ΔP (In. H <sub>2</sub> O)	ΔH (In. H <sub>2</sub> O)	Probe Temp. (°F)	Stack Temp. Ts (°F)	Umbilical Temp (°F)	Meter Temp. Tm (°F)	Last Imp. Temp. (°F)	Vacuum (In. Hg.)
1	0941	587.5	0.92	1.23	215	267	248	80	64	6
2	}	589.4	0.92	1.23	235	272	253	83	61	6
3		591.2	0.89	1.19	249	272	254	85	62	6
4		593.1	0.85	1.14	250	272	248	86	65	6
5		0956	594.7	0.72	0.96	246	270	249	87	66
1	0957	596.6	0.87	1.16	246	271	245	87	65	8.5
2	}	598.3	0.87	1.16	247	270	246	87	65	7
3		600.2	0.87	1.16	247	270	250	88	67	7
4		602.0	0.85	1.14	246	269	251	88	67	7
5		1013	603.8	0.83	1.11	245	268	247	89	65

Sulfuric Acid Mist Field Data Form (Continued)

Traverse Point No.	Clock Time	Gas Sample Volume (Ft <sup>3</sup> )	$\Delta P$ (In. H <sub>2</sub> O)	$\Delta H$ (In. H <sub>2</sub> O)	Probe Temp. (°F)	Stack Temp. Ts (°F)	Umbilical Temp (°F)	Meter Temp. Tm (°F)	Last Imp. Temp. (°F)	Vacuum (In. Hg.)
1	1014	605.8	0.98	1.31	246	271	247	89	65	6.5
2	}	607.7	0.96	1.28	248	271	251	90	65	6
3		609.5	0.90	1.20	248	271	246	90	65	6
4		611.4	0.96	1.28	246	270	252	91	65	6
5	1029	613.4	0.83	1.11	246	262	251	91	66	6
<del>X</del>										
1	1031	615.4	0.71	1.22	250	272	247	90	65	6
2	}	617.1	0.92	1.23	254	271	247	91	64	6
3		619.0	0.95	1.27	254	271	247	91	65	6
4		620.9	0.94	1.26	254	271	250	92	66	6
5	1046	622.7	0.75	1.00	254	268	248	92	68	6
<del>X</del>										



Sulfuric Acid Mist Field Data Form

Plant F. J. GANNON  
 Location Boiler No. 3  
 Method USEPA Method B  
 Operator David Smith  
 Date 4-23-96  
 Run No. 3-5  
 Min. 1 Pt. 3  
 Stack Area Ft.<sup>2</sup> 122.718  
 Sample Box No. N/A  
 Meter Box No. 6  
 Meter ΔH 1.681  
 Meter Cal. (Y) 1.000  
 Nozzle I.D. No. 37  
 Nozzle Diameter 0.212

Pitot Tube (C) 0.84  
 Probe Length 10  
 Probe Liner Material incone 1  
 Probe Heater Setting 250  
 Ambient Temperature 80  
 Barometric Pressure (P<sub>b</sub>) 30.04 in. Hg  
 Static Pressure (P<sub>s</sub>) 30.04 in. Hg  
 Assumed Moisture (%) 8.0 %  
 Time - Start 1129 End 1233  
 Total Sampling Time 60 min. Min.  
 Comments Spilling this run  
TDI Test Blend

Dry Gas Meter Volume  
 Final 668.525 Ft.<sup>3</sup>  
 Initial 632.044 Ft.<sup>3</sup>  
 Net 36.481 Ft.<sup>3</sup>

Equipment Leak Checks  
 Initial 0.0 CFM@ 15 "Hg  
 Final 0.0 CFM@ 8 "Hg  
 Pitot Tube 0.0 @ 7.5 "H<sub>2</sub>O

Moisture Determination  
 Impinger 60 ml  
 Silica Gel 14.6 gm  
 Total 74.6

Traverse Point No.	Clock Time	Gas Sample Volume (Ft <sup>3</sup> )	ΔP (In. H <sub>2</sub> O)	ΔH (In. H <sub>2</sub> O)	Probe Temp. (°F)	Stack Temp. Ts (°F)	Umbilical Temp (°F)	Meter Temp. Tm (°F)	Last Imp. Temp. (°F)	Vacuum (In. Hg.)
1	1129	634.4	0.98	1.31	220	270	244	83	59	6
2	}	636.3	0.89	1.19	252	270	249	86	57	6
3		638.1	0.91	1.22	254	270	249	87	59	6
4		640.0	0.91	1.22	251	269	247	89	60	6
5	1144	641.8	0.75	1.00	252	266	248	89	60	5
1	1146	643.3	0.91	1.22	252	269	251	89	62	7
2	}	645.1	0.89	1.19	252	269	247	90	61	6
3		647.0	0.89	1.19	251	268	252	90	61	6
4		648.8	0.84	1.12	249	268	253	90	62	5.5
5	1201	650.5	0.79	1.06	248	266	253	91	63	5

Sulfuric Acid Mist Field Data Form ( Continued )

Traverse Point No.	Clock Time	Gas Sample Volume ( Ft <sup>3</sup> )	ΔP (In. H <sub>2</sub> O)	ΔH (In. H <sub>2</sub> O)	Probe Temp. (°F)	Stack Temp. Ts (°F)	Umbilical Temp (°F)	Meter Temp. Tm (°F)	Last Imp. Temp. (°F)	Vacuum (In. Hg.)
1	1202	652.4	0.89	1.19	246	269	247	90	63	5.5
2	}	654.1	0.81	1.08	247	269	252	91	62	6
3		655.9	0.88	1.18	249	269	247	91	62	6
4		657.8	0.85	1.14	249	268	252	91	63	6
5		1217	659.6	0.81	1.08	248	268	250	91	63
1	1218	661.4	0.87	1.16	254	270	250	91	66	5.5
2	}	663.2	0.85	1.14	260	271	250	92	67	5.5
3		665.0	0.85	1.14	256	272	254	93	67	5.5
4		666.8	0.87	1.16	256	272	248	93	68	5.5
5		1233	668.5	0.73	0.98	256	271	252	93	68

**F-7 FUEL BLEND BURN ORSAT DATA SHEETS**

# ORSAT DATA AND CALCULATION SHEET

Source Boiler No. 3

Location F.J. GANNON

Run No.	Date	Gas	Orsat Analysis, Dry Basis (% Volume)				Remarks
			1	2	3	Avg.	
1-5	4-23-94 DAS	CO <sub>2</sub>	10.4	10.4	10.4	10.4	Method B TDF $F_o = 1.519$
		O <sub>2</sub>	6.2	4.4	7.8	5.1	
		CO	0	0	0	0	
		N <sub>2</sub>	83.4	85.2	84.8	84.5	
2-5	4-23-94 DAS	CO <sub>2</sub>	11.7	11.4	11.7	11.6	TDF Blend $F_o = 1.466$
		O <sub>2</sub>	4.1	3.4	4.1	3.9	
		CO	0	0	0	0	
		N <sub>2</sub>	84.2	85.2	84.2	84.5	
3-5	4-23-94 Allison	CO <sub>2</sub>	11.7	11.7	11.7	11.7	TDF Blend $F_o = 1.556$
		O <sub>2</sub>	2.7	2.7	2.7	2.7	
		CO	0	0	0	0	
		N <sub>2</sub>	85.6	85.6	85.6	85.6	

Note: Suspect a problem with the orsat analyzer in Run 2-5 and 3-5.

DAS

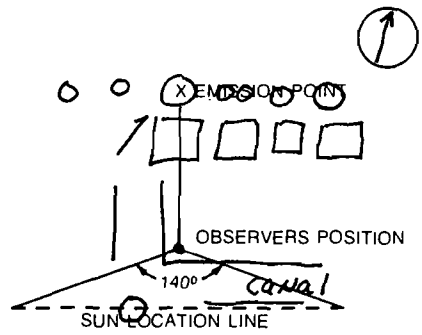
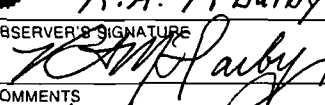

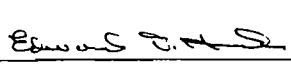
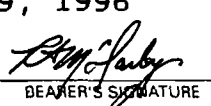
## ORSAT DATA AND CALCULATION SHEET

Source Boiler NO. 3

Location F. J. GANNON

Run No.	Date	Gas	Orsat Analysis, Dry Basis (% Volume)				Remarks
			1	2	3	Avg.	
1-S PART.	4-23-96 DAS	CO <sub>2</sub>	12.6	12.6	12.6	12.6	TDF Blend Method 17  $F_o = 1.190$
		O <sub>2</sub>	6	5.6	6	5.9	
		CO	0	0	0	0	
		N <sub>2</sub>	81.4	81.8	81.4	81.5	
2-S PART.	4-23-96 DAS	CO <sub>2</sub>	12.3	12.3	12.3	12.3	TDF Blend  $F_o = 1.187$
		O <sub>2</sub>	6.3	6.3	6.3	6.3	
		CO	0	0	0	0	
		N <sub>2</sub>	81.4	81.4	81.4	81.4	
3-S PART.	4-23-96 DAS	CO <sub>2</sub>	12.6	12.6	12.6	12.6	TDF Blend  $F_o = 1.198$
		O <sub>2</sub>	5.8	5.8	5.8	5.8	
		CO	0	0	0	0	
		N <sub>2</sub>	81.6	81.6	81.6	81.6	

**F-8 FUEL BLEND VISIBLE EMISSIONS DATA SHEETS**

SOURCE NAME <b>J Gannon Unit #3</b>		SOURCE LOCATION <b>Tampa FL</b>		OBSERVATION DATE <b>4/23/96</b>		START TIME <b>13:29</b>		STOP TIME <b>14:29</b>	
TYPE OF FACILITY <b>Coal Fired boiler</b>		SEC.		MIN		SEC		MIN	
DISTANCE FROM OBSERVER <b>~750'</b>		MIN		0		15		30	
SKY CONDITIONS/PLUME BACKGROUND <b>Scattered / blue</b>		MIN		45		MIN		0	
SOURCE LAYOUT SKETCH DRAW NORTH ARROW 		MIN		0		15		30	
		MIN		45		MIN		0	
AVERAGE OPACITY <b>0.29</b>		MIN		0		15		30	
WIND SPEED (EST.) <b>15-18 mph</b>		MIN		0		15		30	
WIND DIRECTION (EST.) <b>WSW</b>		MIN		45		MIN		0	
OBSERVER'S NAME (PRINT) <b>R.A. McDarby</b>		MIN		0		15		30	
OBSERVER'S SIGNATURE 		MIN		45		MIN		0	
DATE <b>4/23/96</b>		MIN		0		15		30	
COMMENTS <b>sight angle ~21°</b>		MIN		0		15		30	
<b>TDF test burn</b>		MIN		45		MIN		0	
COPY OF VISIBLE EMISSIONS CERTIFICATION CARD		MIN		0		15		30	
 <b>STATE OF FLORIDA</b> <b>DEPARTMENT OF ENVIRONMENTAL REGULATION</b>  THIS IS TO CERTIFY THAT <b>RAY MCDARBY</b> has completed the STATE OF FLORIDA visible emissions evaluation training and is a qualified observer of visible emissions as specified by EPA reference method 9. THIS CERTIFICATE EXPIRES <b>Aug 29, 1996</b>   CERTIFICATE OFFICER   BEARER'S SIGNATURE		MIN		0		15		30	
		MIN		45		MIN		0	
		MIN		0		15		30	
		MIN		45		MIN		0	
		MIN		0		15		30	
		MIN		45		MIN		0	
		MIN		0		15		30	
		MIN		45		MIN		0	
		MIN		0		15		30	
		MIN		45		MIN		0	

**APPENDIX G**

**SAMPLE EQUIPMENT CALIBRATIONS**

**G-1 BASELINE EQUIPMENT CALIBRATIONS**

**G-2 FUEL BLEND BURN EQUIPMENT CALIBRATIONS**



**G-1 BASELINE EQUIPMENT CALIBRATIONS**

## SUMMARY OF EQUIPMENT CALIBRATIONS

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EQUIPMENT	CALIBRATION DATE	LOCATION	METHOD	RESULTS
Method 17 Console 4 Initial Test Post Test	1-2-96 3-4-96	CES CES	Wet Test Meter Wet Test Meter	Y = 1.013 Y = 1.019
Nozzle #16 Initial Measurement Post Test	1-2-96 3-5-96	CES CES	3 Measurements w/calipers	DN= 0.198 DN= 0.198
Pyrometer No. 5	1-12-96	CES	Comparison to ASTM Thermometer	Correct to ± 2°F
Pitot Tube 00107	1-4-96	CES	EPA Method	CP = 0.84
Wet Test Meter Serial No. 12-AH-4	1-9-96	CES	Liquid Displacement	CF= 1.007
Barometer SN 00224	1-3-96	CES	Comparison to National Weather Services	Correct to ± 0.04" Hg

**INITIAL DRY GAS METER AND ORIFICE CALIBRATION**

CONTROL BOX NO. 4 BAROMETRIC PRESS. 29.90 IN. HG.

DATE 1-2-96 PERFORMED BY *J.P.O.*

	RUN 1	RUN 2	RUN 3	RUN 4
VACUUM ("Hg)	3.0	3.0	3.0	3.0
dHw ("H2O)	0.65	1.10	1.30	2.00
dHd ("H2O)	0.50	1.00	1.50	2.00
INITIAL WTM	0.0000	0.0000	0.0000	0.0000
FINAL WTM	6.0038	8.3573	7.3038	7.6165
INITIAL DGM	810.306	816.907	826.221	834.414
FINAL DGM	816.260	825.338	833.687	842.297
TEMP. WTM (F)	71.5	72.0	72.5	72.5
TEMP. DGM (F)	85.0	88.0	89.0	91.0
TEST TIME (MIN.)	15.0	15.0	11.0	10.0

NET VOLUME WTM	6.0038	8.3573	7.3038	7.6165
NET VOLUME DGM	5.954	8.431	7.466	7.883
Y	1.033	1.019	1.005	0.995
dH@	1.715	1.764	1.863	1.881

AVERAGE Y = 1.013

ACCEPTABLE Y RANGE = 0.993 TO 1.033

AVERAGE dH@ = 1.806

ACCEPTABLE dH@ RANGE = 1.656 TO 1.956

$$Y = (V_w (P_b) \times (T_d + 460)) / (V_d (P_b + (dH_d / 13.6)) \times (T_w + 460))$$

$$dH@ = 0.0317 \times dH_d / (P_b (T_d + 460)) \times ((T_w + 460) \times \text{time}) / V_w \wedge 2$$

*JAM*  
1/2/96

**RECHECK OF ORIFICE AND DGM CALIBRATION**

CONTROL BOX NO. 4 BAROMETRIC PRESS. 30.40 IN. HG.

DATE 3-04-96 PERFORMED BY *[Signature]*

LEAK CHECK OF METER SYSTEM ok @ 7" Hg. PRIOR Y = 1.013

	RUN 1	RUN 2	RUN 3
VACUUM ("Hg)	7.0	7.0	7.0
dHw ("H2O)	1.10	1.10	1.10
dHd ("H2O)	1.00	1.00	1.00
INITIAL WTM	0.0000	8.3770	16.7378
FINAL WTM	8.3770	16.7378	25.0900
INITIAL DGM	593.522	601.924	610.392
FINAL DGM	601.924	610.392	618.883
TEMP. WTM (F)	68.0	68.0	68.5
TEMP. DGM (F)	83.0	86.0	87.0
TEST TIME (MIN.)	15.0	15.0	15.0

NET VOLUME WTM	8.3770	8.3608	8.3522
NET VOLUME DGM	8.402	8.468	8.491
Y	1.023	1.019	1.016
dH@	1.717	1.714	1.717

PRIOR Y = 1.013  
 RECHECK Y = 1.019  
 % DIFFERENCE = 0.592  
  
 AVERAGE dH@ = 1.716

*[Signature]*  
 3/6/96

$$Y = (Vw (Pb) x (Td + 460)) / (Vd (Pb + (dHd / 13.6)) x (Tw + 460))$$

$$dH@ = 0.0317 x dHd / (Pb (Td + 460)) x ((Tw + 460) x time) / Vw ^ 2$$

**NOZZLE CALIBRATION DATA FORM**

NOZZLE SET NO. 1

DATE: 1-2-96

CALIBRATED BY: *[Signature]*

NOZZLE IDENTIFICATION	NOZZLE DIAMETER (IN.)			ΔD	D avg
	D1	D2	D3		
1	.111	.111	.111	0.000	0.111
4	.125	.125	.125	0.000	0.125
5	.150	.150	.150	0.000	0.150
6	.197	.197	.197	0.000	0.197
9	.276	.276	.276	0.0000	0.276 *
10	.295	.296	.296	0.001	0.296
12	.388	.388	.388	0.000	0.388
15	.164	.164	.164	0.000	0.164
16	.198	.198	.198	0.000	0.198
19	.274	.274	.274	0.000	0.274
22	.365	.364	.364	0.001	0.364
30	.314	.314	.314	0.000	0.314
36	.185	.185	.185	0.000	0.185
37	.211	.211	.212	<del>0.000</del> <sup>0.001</sup>	0.211 *
38	.244	.244	.245	0.001	0.244
46	.192	.192	.192	0.000	0.192
48	.249	.249	.249	0.000	0.249
47	.200	.200	.201	0.001	0.200 *
50	.314	.314	.314	0.000	0.314 *
58	.236	.236	.236	0.000	0.236

where:

D1,2,3 = three different nozzle diameters, (in); each diameter must be measured to the nearest 0.001 in.

ΔD = maximum difference between any two diameters, (in.)  
 ΔD ≤ 0.004 in.

D Avg = average of D1, D2, and D3.

*\* changed since last cal.*  
*[Signature]*  
 1/10/96

**FINAL NOZZLE CALIBRATION DATA FORM**

NOZZLE NO 16

DATE: 3-5-96

CALIBRATED BY: *[Signature]*

NOZZLE IDENTIFICATION	NOZZLE DIAMETER			$\Delta D$ (IN.)	D AVG
	D1 (IN.)	D2 (IN.)	D3 (IN.)		
#16	0.198	0.198	0.198	0.000	0.198

**where:**

$D_{1,2,3}$  = three different nozzle diameters, (in); each diameter must be measured to the nearest 0.001 in.

$\Delta D$  = maximum difference between any two diameters, (in.).  
 $\Delta D \leq 0.004$  in.

$D_{AVG}$  = average of  $D_1, D_2$  and  $D_3$ .

*AM*  
3/6/96

PYROMETER CALIBRATION

PYROMETER NO. 5 REFERENCE THERMOMETER

CTL SERIAL NO. 5 SERIAL NO. E2735

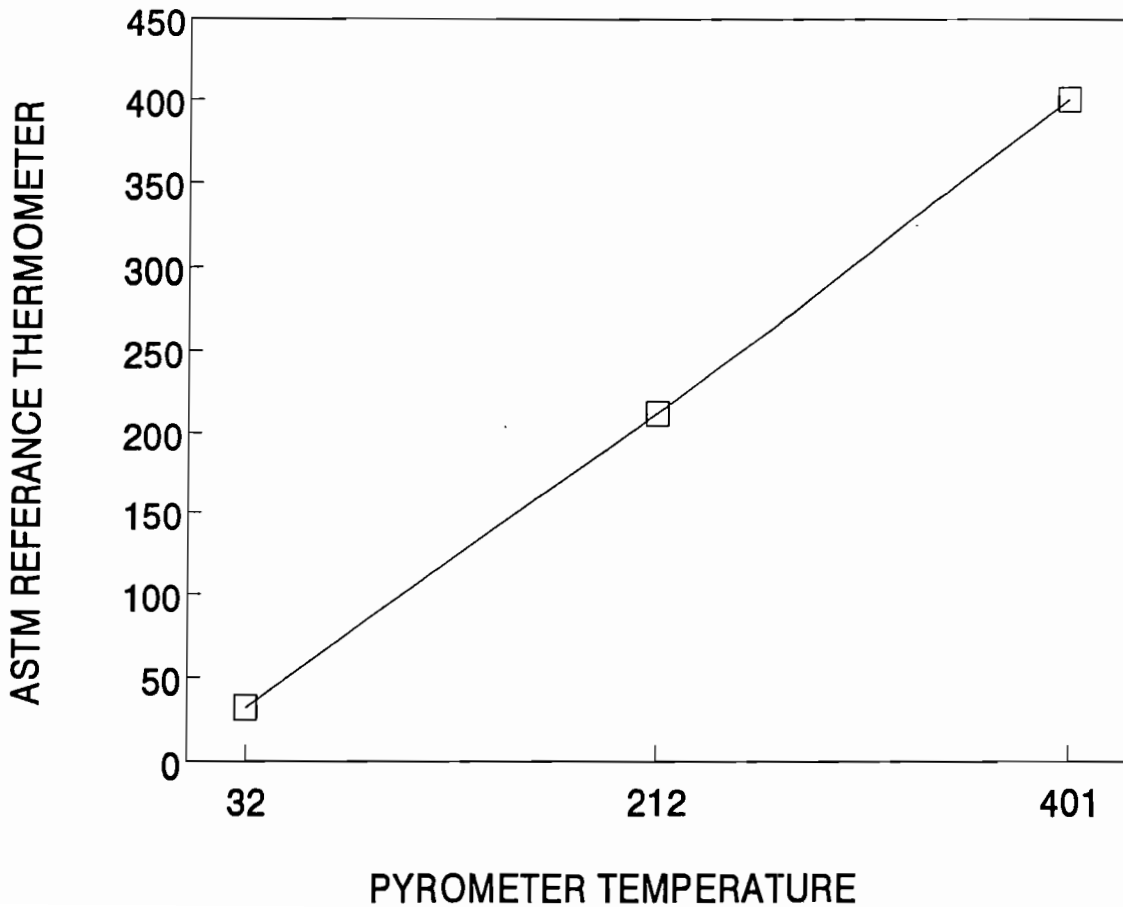
DATE 1-12-96

CALIBRATOR *[Signature]*

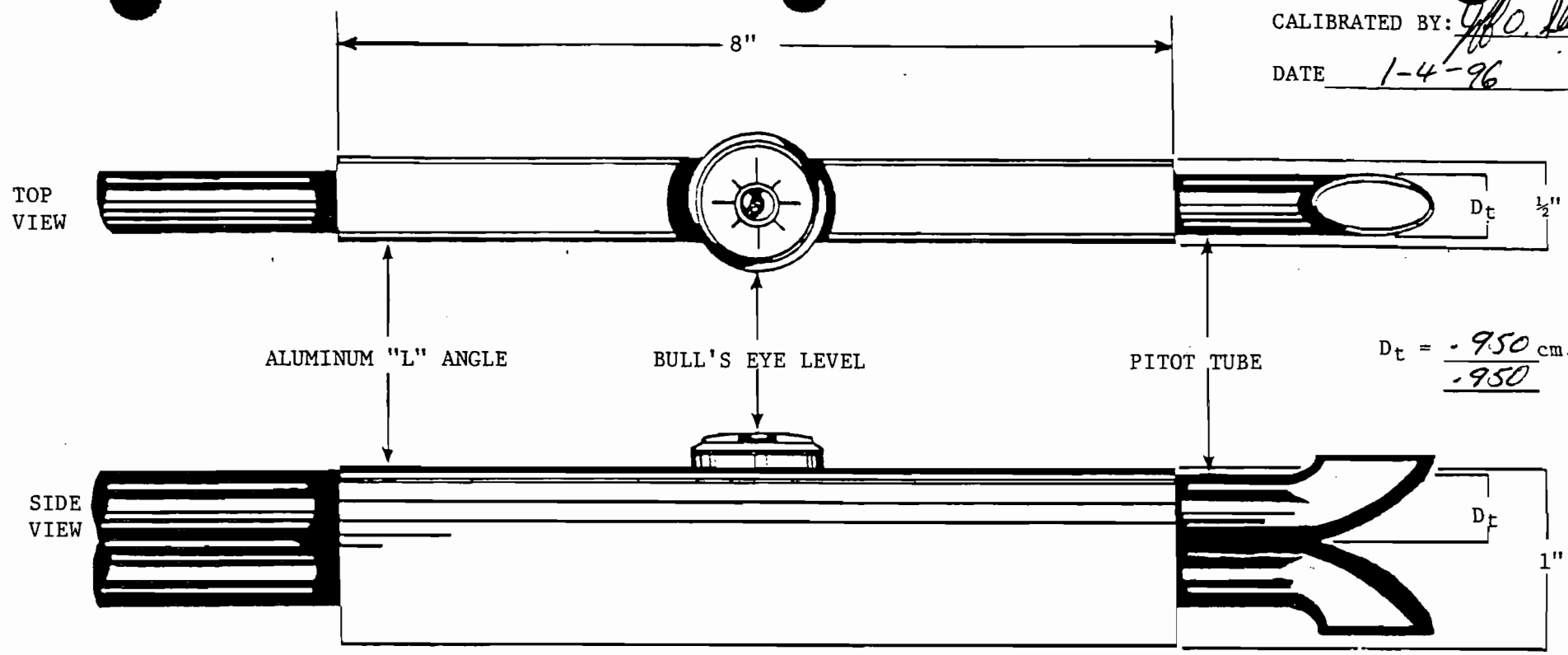
REFERENCE TEMP. (F)	PYROMETER INDICATION
32	32
212	212
400	401

*[Signature]*  
1/31/96

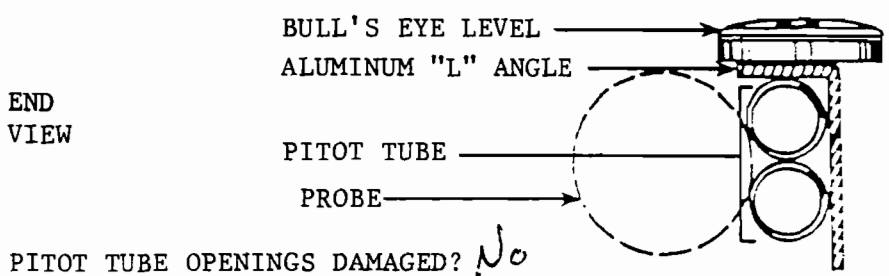
PYROMETER TEMPERATURE CALIBRATION



SERIAL NO. 0007  
 CALIBRATED BY: [Signature]  
 DATE 1-4-96



$$D_t = \frac{-950 \text{ cm.}}{-950}$$

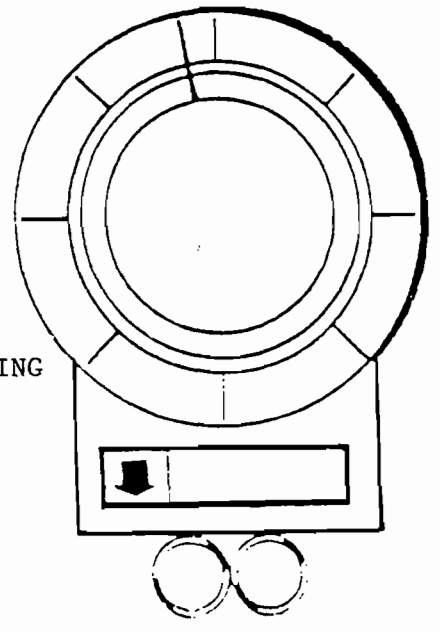


PITOT TUBE OPENINGS DAMAGED? No

COMMENTS: \_\_\_\_\_  
 \_\_\_\_\_  
 \_\_\_\_\_

[Signature]  
 1/19/96

DEGREE INDICATING LEVEL



PITOT TUBE CALIBRATION SET-UP POSITION



SERIAL NO. 0017

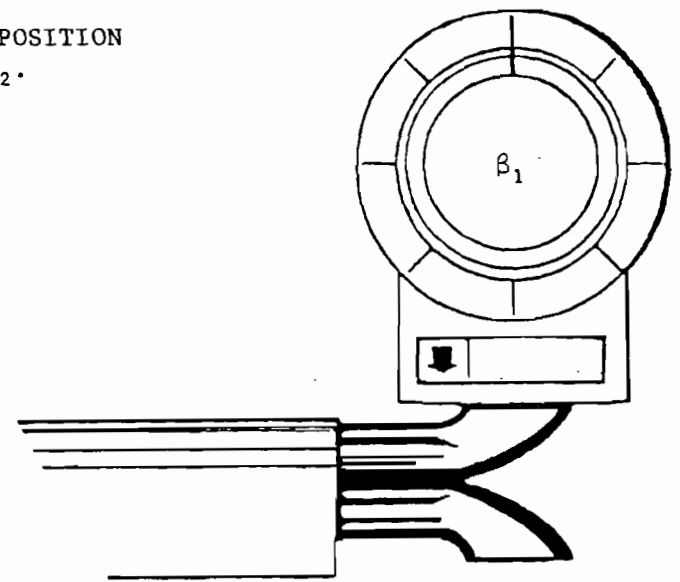
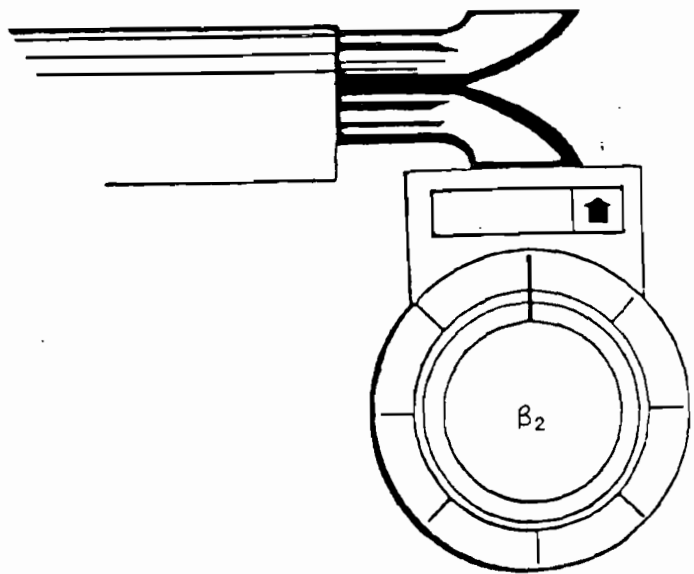
CALIBRATED BY J.F.O. R.

DATE 1-4-96

DEGREE INDICATING LEVEL POSITION FOR DETERMINING  $\beta_1$  and  $\beta_2$ .

$$\beta_1 = \underline{2.0}^\circ (<5^\circ)$$

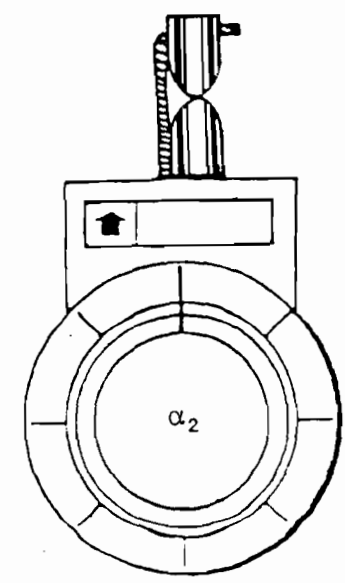
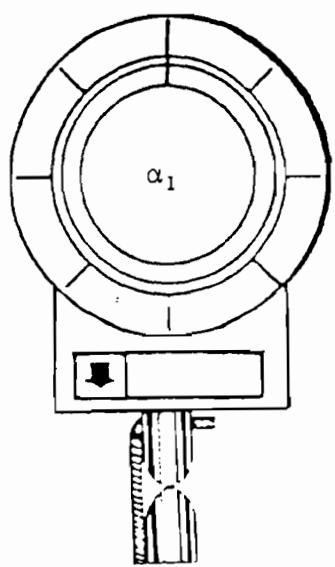
$$\beta_2 = \underline{2.0}^\circ (<5^\circ)$$



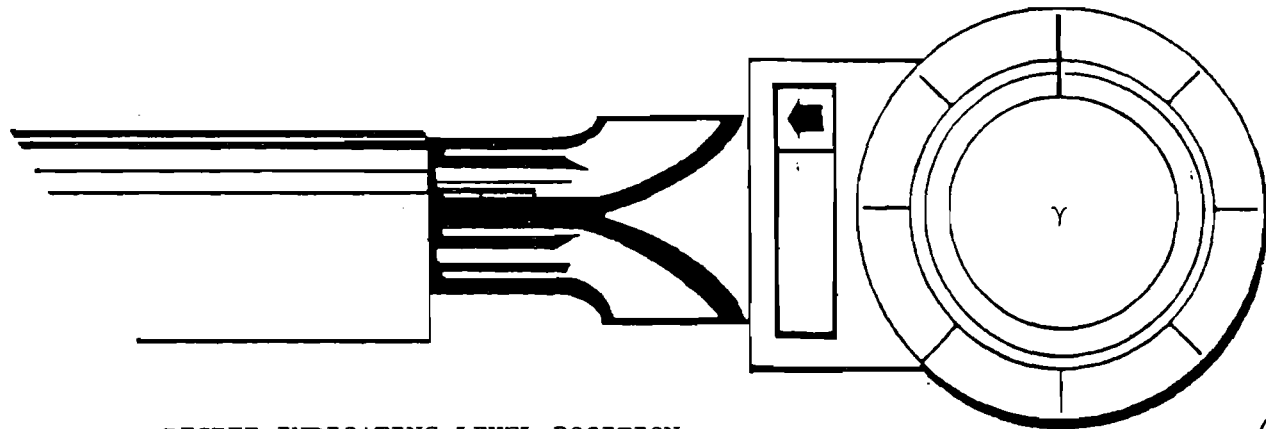
DEGREE INDICATING LEVEL POSITION FOR DETERMINING  $\alpha_1$  and  $\alpha_2$ .

$$\alpha_1 = \underline{1.0}^\circ (<10^\circ)$$

$$\alpha_2 = \underline{1.0}^\circ (<10^\circ)$$



SERIAL NO. 00107  
 CALIBRATED BY J.P.O. [Signature]  
 DATE 1-4-96



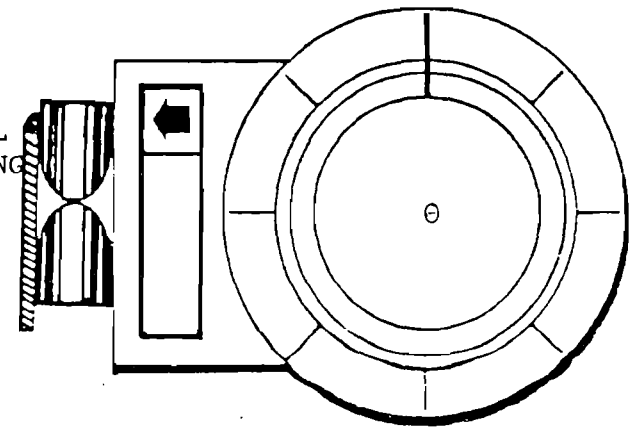
DEGREE INDICATING LEVEL POSITION  
 FOR DETERMINING  $\gamma$ , THEN CALCULATING Z.

$\gamma = \underline{0.5}^\circ$

A = DISTANCE BETWEEN TIPS, ( $P_a + P_b$ ), cm. = 2.220.

Z = A sin  $\gamma$  = 0.02 cm; (<0.32 cm).

DEGREE INDICATING LEVEL  
 POSITION FOR DETERMINING  
 $\Theta$ , THEN CALCULATING W.



$\Theta = \underline{1.0}^\circ$

W = A sin  $\Theta$  = 0.04 cm; (<0.08 cm).

**WET TEST METER CALIBRATION DATA SHEET**

DATE 1-9-96

BAROMETRIC PRESSURE 30.32

WET TEST METER

NAME [Signature]

AMBIENT TEMPERATURE 71.0°F

SERIAL NUMBER  
12-AH-4

RUN NO.	VOLUME OF WATER DISPLACED (LITERS) $V_a$	INITIAL METER READING (FT <sup>3</sup> )	FINAL METER READING (FT <sup>3</sup> )	NET METER VOLUME (FT <sup>3</sup> )	NET METER VOLUME $V_w$ (LITERS) $V_m$	ERROR
1	3.360	0.0000	0.1180	0.1180	3.342	-0.00535714
2	3.360	0.1180	0.2355	0.1175	3.328	-0.00952381
3	3.360	0.2355	0.3534	0.1179	3.339	-0.00625000
4	3.360	0.3534	0.4712	0.1178	3.336	-0.00714286
CALCULATIONS:						AVG. ERROR = -0.00706846

$ERROR = (V_w - V_a) / V_a$

$CORRECTION FACTOR = 1 / (1 + AVG. ERROR)$

\*CONVERSION FACTOR, FT<sup>3</sup> TO LITERS = 28.32 x FT<sup>3</sup>

C. F. =  $\frac{1.007118779}{0.992981152}$   
(1.000 +/- 0.010)

WHEN USING THE WET TEST METER, THE ACTUAL VOLUME OF AIR CAN BE DETERMINED BY THE EQUATION:

$V_a = V_w \times C. F.$

WHERE:

$V_a$  = ACTUAL VOLUME OF AIR PASSED THROUGH THE WET TEST METER.

$V_w$  = VOLUME OF AIR INDICATED BY THE WET TEST METER.

C. F. = CORRECTION FACTOR FOR THE METER.

*[Signature]*  
1/10/96

**BAROMETER CALIBRATION DATA FORM**

DATE 1-3-96

CALIBRATOR *[Signature]*

COMMENTS

#00224

Time between readings due to weather Service shutdown.

TIME	BAROMETER READING (HG")	REFERENCE STANDARD READING (HG")	DIFFERENCE (HG")
1-3-96 2:16 pm	29.85"	29.81"	0.04"
1-7-96 9:15 am	<i>9:15</i> 34.30" 30.30	<i>9:15</i> 34.34" 30.34	0.04"

*[Signature]*  
1/10/96

**\*NOTE: BAROMETRIC READINGS MUST AGREE WITHIN 0.1 INCHES HG OF READINGS OBTAINED FROM THE REFERENCE STANDARD, THE NATIONAL WEATHER SERVICE, RUSKIN FL. TO BE DEEMED ACCEPTABLE.**

## **G-2 FUEL BLEND BURN EQUIPMENT CALIBRATIONS**

## SUMMARY OF EQUIPMENT CALIBRATIONS

EQUIPMENT	CALIBRATION DATE	LOCATION	METHOD	RESULTS
Method 17 Console #6 Initial Test Post Test	4-19-96 4-25-96	CES CES	Wet Test Meter Wet Test Meter	Y = 1.000 Y = 1.004
Nozzle #37 Initial Measurement Post Test Measurement	4-4-96 4-25-96	CES CES	3 Measurements w/calipers	DN= 0.212 DN= 0.211
Nozzle #16 Initial Measurement Post Test Measurement	4-4-96 4-5-96	CES	3 Measurements w/calipers	DN= 0.197 DN= 0.197
Pyrometer No. 12	4-12-96	CES	Comparison to ASTM Thermometer	Correct to $\pm 2^{\circ}\text{F}$
Pitot Tube 00112	4-12-96	CES	EPA Method	CP = 0.84
Wet Test Meter Serial No. 12-AH-4	4-3-96	CES	Liquid Displacement	CF= 1.004
Barometer SN 00224	4-16-96	CES	Comparison to National Weather Services	Correct to $\pm 0.03''\text{Hg}$

**INITIAL DRY GAS METER AND ORIFICE CALIBRATION**

CONTROL BOX NO. **6** BAROMETRIC PRESS. **30.13** IN. HG.

DATE **4-16-96** PERFORMED BY *[Signature]*

	RUN 1	RUN 2	RUN 3	RUN 4
VACUUM ("Hg)	3.0	3.0	3.0	3.0
dHw ("H2O)	0.65	1.10	1.60	2.05
dHd ("H2O)	0.50	1.00	1.50	2.00
INITIAL WTM	0.0000	0.0000	0.0000	0.0000
FINAL WTM	6.1698	8.5264	6.8275	7.8093
INITIAL DGM	513.704	520.238	529.578	537.149
FINAL DGM	519.943	529.027	536.725	545.425
TEMP. WTM (F)	69.5	70.0	69.5	69.5
TEMP. DGM (F)	87.0	91.0	92.0	93.0
TEST TIME (MIN.)	15.0	15.0	10.0	10.0

NET VOLUME WTM	6.1698	8.5264	6.8275	7.8093
NET VOLUME DGM	6.239	8.789	7.147	8.276
Y	1.020	1.006	0.992	0.981
dH@	1.594	1.660	1.720	1.749

AVERAGE Y = 1.000

ACCEPTABLE Y RANGE = 0.980 TO 1.020

AVERAGE dH@ = 1.681

ACCEPTABLE dH@ RANGE = 1.531 TO 1.831

$$Y = (V_w (P_b) \times (T_d + 460)) / (V_d (P_b + (dH_d / 13.6)) \times (T_w + 460))$$

$$dH@ = 0.0317 \times dH_d / (P_b (T_d + 460)) \times ((T_w + 460) \times \text{time}) / V_w^2$$

*[Signature]*  
4/16/96

RECHECK OF ORIFICE AND DGM CALIBRATION

CONTROL BOX NO: 6 BAROMETRIC PRESS. 30.10 IN. HG.

DATE 4.25.96 PERFORMED BY Amir Aliog

LEAK CHECK OF METER SYSTEM 0.000 @ 15" Hg PRIOR Y = 1.000

	RUN 1	RUN 2	RUN 3
VACUUM ("Hg)	11.0	11.0	11.0
dHw ("H2O)	1.10	1.15	1.15
dHd ("H2O)	1.00	1.00	1.00
INITIAL WTM	0.0000	8.5414	17.0636
FINAL WTM	8.5414	17.0636	25.5678
INITIAL DGM	829.325	838.066	846.824
FINAL DGM	838.066	846.824	855.610
TEMP. WTM (F)	71.0	71.0	70.5
TEMP. DGM (F)	87.0	89.5	90.5
TEST TIME (MIN.)	15.0	15.0	15.0

NET VOLUME WTM	<del>8.5414</del>	8.5222	8.5092
NET VOLUME DGM	8.741	8.758	8.786
Y	1.004	1.005	1.002
dH@	1.674	1.674	1.675

PRIOR Y = 1.000  
 RECHECK Y = 1.004  
 % DIFFERENCE = 0.4%

AVERAGE dH@ = 1.674

$$Y = (V_w (P_b) \times (T_d + 460)) / (V_d (P_b + (dH_d / 13.6)) \times (T_w + 460))$$

$$dH@ = 0.0317 \times dH_d / (P_b (T_d + 460)) \times ((T_w + 460) \times \text{time}) / V_w^2$$

*Am*  
4/30/96



**NOZZLE CALIBRATION DATA FORM**

NOZZLE SET NO. 1

DATE: 4-4-96

CALIBRATED BY: [Signature]

NOZZLE IDENTIFICATION	NOZZLE DIAMETER (IN.)			ΔD	D avg
	D1	D2	D3		
1	0.111	0.111	0.111	0.000	0.111
4	0.125	0.125	0.125	0.000	0.125
5	0.149	0.149	0.149	0.000	0.149
6	0.197	0.197	0.197	0.000	0.197
9	0.276	0.276	0.276	0.000	0.276
10	0.289	0.290	0.289	0.001	0.289
12	0.388	0.388	0.388	0.000	0.388
15	0.164	0.164	0.164	0.000	0.164
16	0.198	0.198	0.198	0.000	0.198
19	0.275	0.275	0.275	0.000	0.275
22	0.364	0.364	0.364	0.000	0.364
30	0.314	0.314	0.314	0.000	0.314
36	0.185	0.185	0.185	0.000	0.185
37	0.212	0.213	0.212	0.001	0.212
38	0.244	0.245	0.244	0.001	0.244
46	0.192	0.192	0.192	0.000	0.192
47	0.200	0.200	0.200	0.000	0.200
48	0.249	0.249	0.249	0.000	0.249
50	0.314	0.314	0.314	0.000	0.314
58	0.237	0.237	0.237	0.000	0.237

where:

D1,2,3 = three different nozzle diameters, (in); each diameter must be measured to the nearest 0.001 in.

ΔD = maximum difference between any two diameters, (in.)  
 ΔD ≤ 0.004 in.

D Avg = average of D1, D2, and D3.

*[Signature]*  
5/7/96

FINAL NOZZLE CALIBRATION DATA FORM

NOZZLE NO. 37

DATE: 4-25-96

CALIBRATED BY: *William H. King*

NOZZLE IDENTIFICATION	NOZZLE DIAMETER			$\Delta D$ (IN.)	D AVG
	D1 (IN.)	D2 (IN.)	D3 (IN.)		
37	0.212	0.210	0.211	0.002	0.211

where:

*D1,2,3* = three different nozzle diameters, (in.); each diameter must be measured to the nearest 0.001 in.

$\Delta D$  = maximum difference between any two diameters, (in.).  
 $\Delta D \leq 0.004$  in.

*D AVG* = average of *D1, D2* and *D3*.

*W.H.K.*  
4/30/96

**FINAL NOZZLE CALIBRATION DATA FORM**

NOZZLE NO 6

DATE: 4.25.96

CALIBRATED BY: *Adrian King*

NOZZLE IDENTIFICATION	NOZZLE DIAMETER			$\Delta D$ (IN.)	D AVG
	D1 (IN.)	D2 (IN.)	D3 (IN.)		
# <u>6</u>	<u>0.197</u>	<u>0.196</u>	<u>0.197</u>	<u>0.001</u>	<u>0.197</u>

where:

*D1,2,3= three different nozzle diameters,(in); each diameter must be measured to the nearest 0.001 in.*

*$\Delta D$ = maximum difference between any two diameters,(in.).*  
 *$\Delta D \leq 0.004$  in.*

*D AVG= average of D1,D2 and D3.*

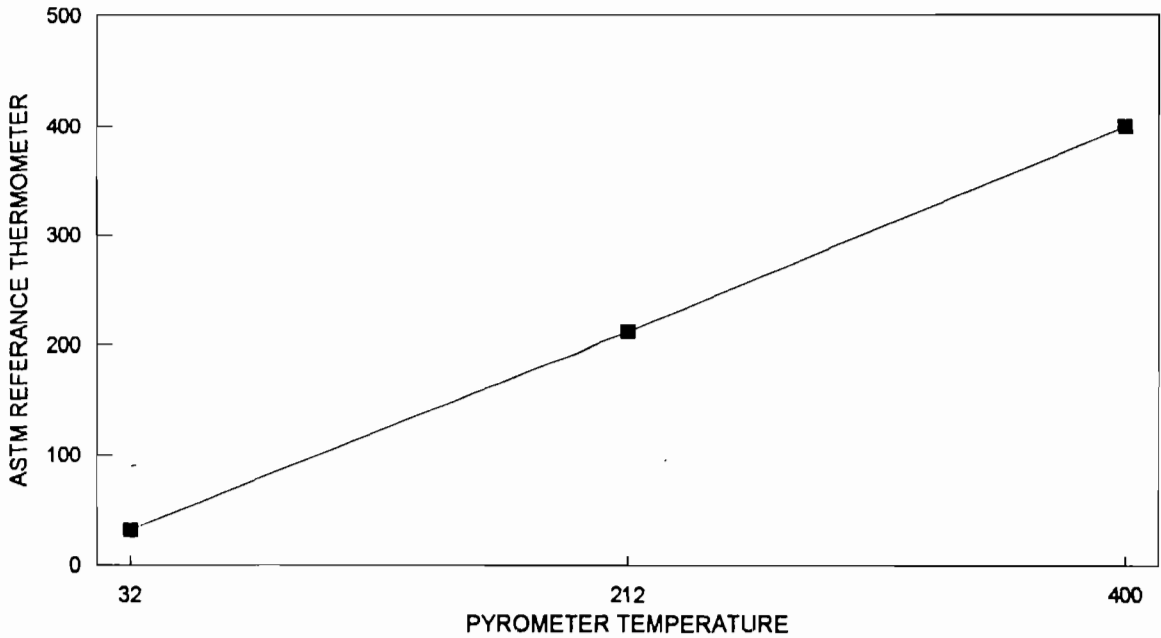
*AKM*  
4/30/96

PYROMETER CALIBRATION

PYROMETER NO. 12 REFERENCE THERMOMETER  
CTL SERIAL NO. 12 SERIAL NO. 1E2735  
DATE 4-12-96 CALIBRATOR *[Signature]*

REFERENCE TEMP. (F)	PYROMETER INDICATION
32	32
212	212
400	400

**PYROMETER TEMPERATURE CALIBRATION**



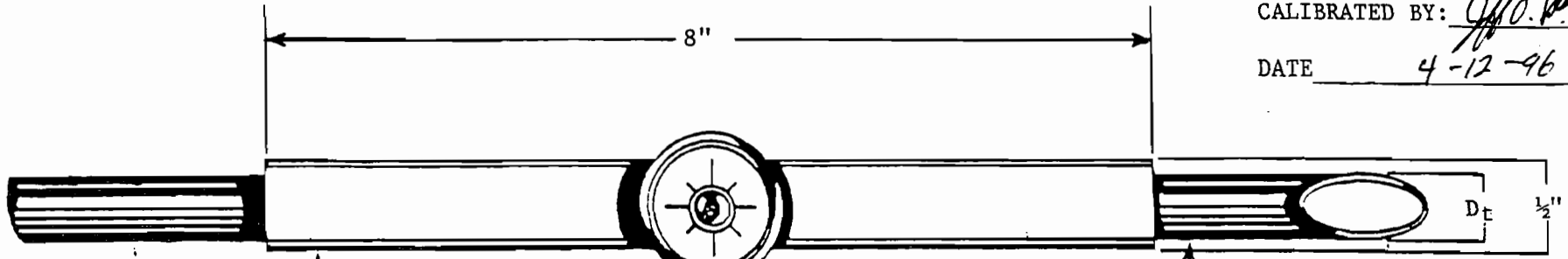
*[Signature]*  
4/15/96

SERIAL NO. 002

CALIBRATED BY: J.H.P.

DATE 4-12-96

TOP  
VIEW



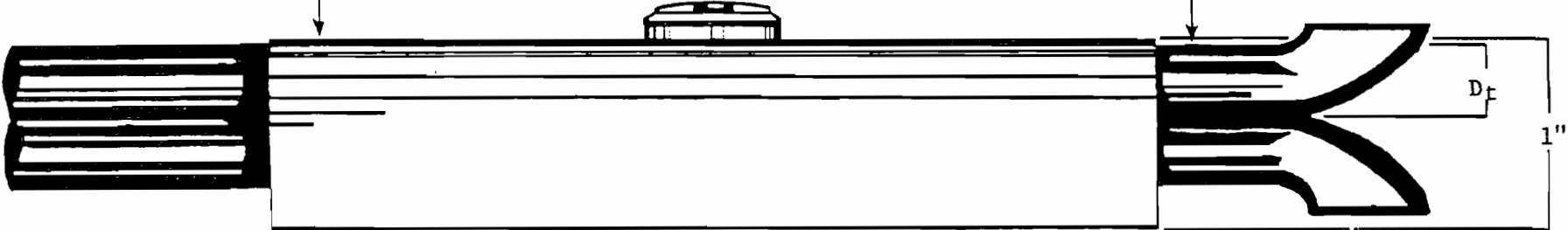
ALUMINUM "L" ANGLE

BULL'S EYE LEVEL

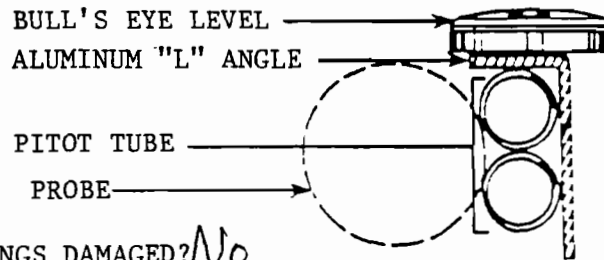
PITOT TUBE

$$D_t = \frac{.950 \text{ cm.}}{.950}$$

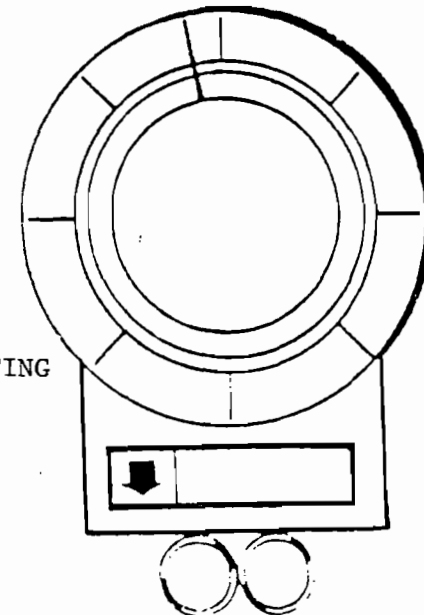
SIDE  
VIEW



END  
VIEW



DEGREE INDICATING  
LEVEL



PITOT TUBE OPENINGS DAMAGED? No

COMMENTS: - Not permanently attached.

*RAM*  
4/19/96  
4/15/94

SERIAL NO. 001

CALIBRATED BY J.O. [Signature]

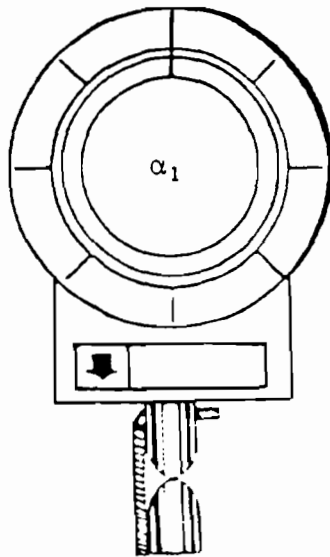
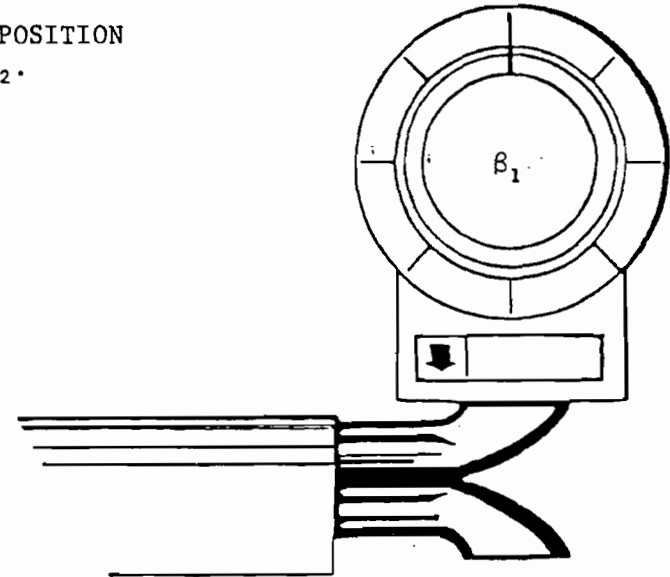
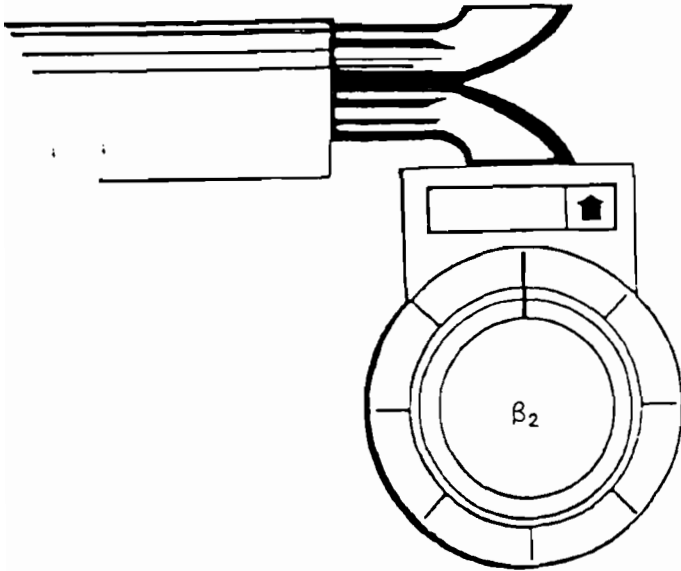
DATE

4-12-96

DEGREE INDICATING LEVEL POSITION  
FOR DETERMINING  $\beta_1$  and  $\beta_2$ .

$$\beta_1 = 1.5^\circ (<5^\circ)$$

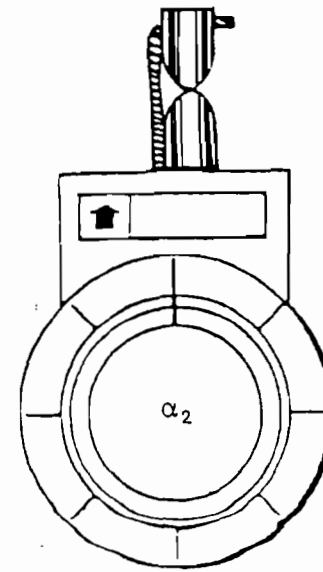
$$\beta_2 = 1.5^\circ (<5^\circ)$$



DEGREE INDICATING LEVEL  
POSITION FOR DETERMINING  
 $\alpha_1$  and  $\alpha_2$ .

$$\alpha_1 = 1.5^\circ (<10^\circ)$$

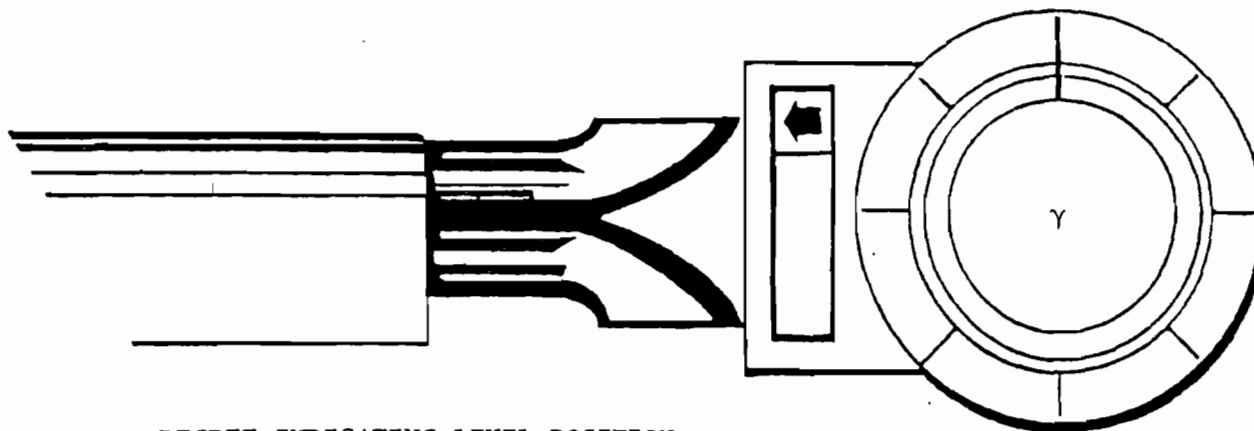
$$\alpha_2 = 1.5^\circ (<10^\circ)$$



SERIAL NO. 00112

CALIBRATED BY J. O. R.

DATE 4-12-96



$\gamma = \underline{.5}^\circ$

DEGREE INDICATING LEVEL POSITION  
FOR DETERMINING  $\gamma$ , THEN CALCULATING Z.

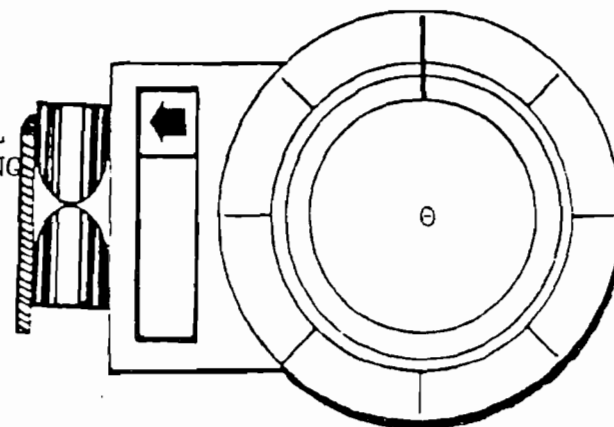
A = DISTANCE BETWEEN TIPS, ( $P_a + P_b$ ), cm. = 2.530.

Z = A sin  $\gamma$  = 0.02 cm; (<0.32 cm).

DEGREE INDICATING LEVEL  
POSITION FOR DETERMINING  
 $\theta$ , THEN CALCULATING W.

$\theta = \underline{1.0}^\circ$

W = A sin  $\theta$  = 0.04 cm; (<0.08 cm).



**WET TEST METER CALIBRATION DATA SHEET**

DATE 4-3-96

BAROMETRIC PRESSURE 30.30

WET TEST METER

NAME [Signature]

AMBIENT TEMPERATURE 72°F

SERIAL NUMBER  
12-AH-4

RUN NO.	VOLUME OF WATER DISPLACED (LITERS) $V_w$	INITIAL METER READING (FT3)	FINAL METER READING (FT3)	NET METER VOLUME (FT3)	NET METER VOLUME (LITERS) $V_w$	ERROR
1	3.360	0.0000	0.1175	0.1175	3.3276	-0.009642857
2	3.360	0.1175	0.2353	0.1178	3.3361	-0.007113095
3	3.360	0.2353	0.3538	0.1185	3.3559	-0.001220238
4	3.360	0.3538	0.4728	0.1190	3.3701	+0.003005952
CALCULATIONS:						AVG. ERROR = -0.00374256

$ERROR = (V_w - V_a) / V_a$

$CORRECTION FACTOR = 1 / (1 + AVG. ERROR)$

\*CONVERSION FACTOR, FT3 TO LITERS = 28.32 x FT3

$C.F. = \frac{1.003756619}{(1.000 +/- 0.010)}$

WHEN USING THE WET TEST METER, THE ACTUAL VOLUME OF AIR CAN BE DETERMINED BY THE EQUATION:

$V_a = V_w \times C.F.$

WHERE:

$V_a$  = ACTUAL VOLUME OF AIR PASSED THROUGH THE WET TEST METER.

$V_w$  = VOLUME OF AIR INDICATED BY THE WET TEST METER.

C.F. = CORRECTION FACTOR FOR THE METER.

[Signature]  
4/15/96



**BAROMETER CALIBRATION DATA FORM**

DATE 4-16-96 CALIBRATOR *[Signature]*

COMMENTS #00224

TIME	BAROMETER READING (HG")	REFERENCE STANDARD READING (HG")	DIFFERENCE (HG")
9:05am	30.18"	30.12"	0.06"
11:10am	30.20"	30.15"	0.05"
2:15pm	30.17"	30.14"	0.03"
			<i>[Signature]</i>
			4/16/96

**\*NOTE: BAROMETRIC READINGS MUST AGREE WITHIN 0.1 INCHES HG OF READINGS OBTAINED FROM THE REFERENCE STANDARD, THE NATIONAL WEATHER SERVICE, RUSKIN FL. TO BE DEEMED ACCEPTABLE.**

**APPENDIX H**

**CHAIN OF CUSTODY**

**H-1 BASELINE CHAIN OF CUSTODY**

**H-2 FUEL BLEND BURN CHAIN OF CUSTODY**

**H-1 BASELINE CHAIN OF CUSTODY**

TAMPA ELECTRIC COMPANY  
SAMPLE CHAIN OF CUSTODY

GENERATING STATION F.D. GANNON STATION  
 SOURCE IDENTIFICATION BOILER No. 3  
 DATE OF TEST FEBRUARY 28, 1996  
 POLLUTANT SAMPLED PARTICULATE (SOOT BLOWING)

SAMPLE RECOVERY

LOCATION CENTRAL TESTING LABORATORY  
 DATE / TIME FEBRUARY 29, 1996 @ 08:00  
 SIGNATURE *Bruce Polyz*  
 TITLE SR. TECHNICAL ASSISTANT

SAMPLE ANALYSIS

LOCATION CENTRAL TESTING LABORATORY  
 DATES FEBRUARY 29 - MARCH 5, 1996  
 SIGNATURE *William Hoag*  
 TITLE SR. TECHNICAL ASSISTANT

CONTAINER CODE	SAMPLE IDENTIFICATION	ANALYTICAL METHOD
THIMBLE No.	19x90mm GLASS MICROPIPER THIMBLE	USEPA
001093	RUN 1S	METHOD
001094	RUN 2S	17
001095	RUN 3S	<div style="font-size: 2em;">}</div> <div style="text-align: right; margin-top: -20px;"> <i>AWM</i>                      3/6/96                 </div>
001097	BLANK	
BEAKER No.	ACETONE WASH SAMPLES	
AIR-13	ACETONE WASH - RUN 1S	
AIR-14	ACETONE WASH - RUN 2S	
AIR-15	ACETONE WASH - RUN 3S	
AIR-16	ACETONE WASH - BLANK	↓

## SAMPLE RECOVERY AND INTEGRITY DATA

Plant F. J. GANNON

Sample location Boiler No. 3

### Field Data Checks

Sample recovery personnel Robert Baerhette

Person with direct responsibility for recovered samples Martin Duff

Sample Number	Sample Identification Number	Date and Time of Recovery	Liquid Level Marked	Stored in refrigerated Container
1	Run 1 isopropanol	2-28-96	~400 ml	✓
2	Run 1 H <sub>2</sub> O <sub>2</sub>	2-28-96	~400 ml	✓
3	Run 2 isopropanol	2-28-96	~400 ml	✓
4	Run 2 H <sub>2</sub> O <sub>2</sub>	2-28-96	~400 ml	✓
5	Run 3 isopropanol	2-28-96	~500 ml	✓
6	Run 3 H <sub>2</sub> O <sub>2</sub>	2-28-96	~300 ml	✓
Blank				

Remarks For Method B Sulfuric Acid Mist Testing.

Signature of field sample trustee David A. Smith

### Laboratory Data Checks

Lab person with direct responsibility for recovered samples FRANK SARDUY

Date recovered samples received 2-28-96

Analyst Frank Sarduy

Sample Number	Sample Identification Number	Date and Time of Recovery	Liquid Level Marked	Stored in refrigerated Container
1	AA28439	2-28-96	YES	YES
2	AA28439	2-28-96	YES	YES
3	AA28439	2-28-96	YES	YES
4				
5				
6				
Blank	AA28439		YES	YES

Remarks \_\_\_\_\_

Signature of lab sample trustee Frank Sarduy

**H-2 FUEL BLEND BURN CHAIN OF CUSTODY**

TAMPA ELECTRIC COMPANY  
SAMPLE CHAIN OF CUSTODY

GENERATING STATION F.D. GANNON STATION  
 SOURCE IDENTIFICATION BOILER No. 3  
 DATE OF TEST APRIL 23, 1996  
 POLLUTANT SAMPLED TDF PARTICULATE

SAMPLE RECOVERY

LOCATION CENTRAL TESTING LABORATORY  
 DATE / TIME APRIL 24, 1996 @ 7:30  
 SIGNATURE *Michael P. [Signature]*  
 TITLE SR. TECHNICAL ASSISTANT

SAMPLE ANALYSIS

LOCATION CENTRAL TESTING LABORATORY  
 DATES APRIL 24-26, 1996  
 SIGNATURE *Michael P. [Signature]*  
 TITLE SR. TECHNICAL ASSISTANT

CONTAINER CODE	SAMPLE IDENTIFICATION	ANALYTICAL METHOD
----------------	-----------------------	-------------------

THIMBLE NO.	19x90mm GLASS MICROFIBER THIMBLE	USEPA
001098	RUN 1S	METHOD
001099	RUN 2S	17
001100	RUN 3S	
001092	BLANK	
BEAKER NO.	ACETONE WASH SAMPLES	
AIR-17	ACETONE WASH - RUN 1S	
AIR-18	ACETONE WASH - RUN 2S	
AIR-19	ACETONE WASH - RUN 3S	
AIR-20	ACETONE WASH - BLANK	

*[Signature]*  
4/30/96

## SAMPLE RECOVERY AND INTEGRITY DATA

Plant EMMON Sample location BOILER #3

### Field Data Checks

Sample recovery personnel BRUCE RODRIGUEZ

Person with direct responsibility for recovered samples \_\_\_\_\_

Sample Number	Sample Identification Number	Date and Time of Recovery	Liquid Level Marked	Stored in refrigerated Container
1	1S, ISOPROPANOL	4-23-96 0920	✓	✓
2	1S, PEROXIDE	4-23-96 0930	✓	✓
3	2S, ISOPROPANOL	4-23-96 1115	✓	✓
4	2S, PEROXIDE	4-23-96 1125	✓	✓
5	3S, ISOPROPANOL	4-23-96 1300	✓	✓
6	3S, PEROXIDE	4-23-96 1310	✓	✓
Blank	80% ISOPROPANOL	4-23-96 1310	✓	✓
	BLANK 3% H <sub>2</sub> O <sub>2</sub>	4-23-96 1310	✓	✓

Remarks \_\_\_\_\_

Signature of field sample trustee Bruce Rodriguez

### Laboratory Data Checks

Lab person with direct responsibility for recovered samples FRANK SARDUJ

Date recovered samples received 4-23-96

Analyst Frank Sarduj

Sample Number	Sample Identification Number	Date and Time of Recovery	Liquid Level Marked	Stored in refrigerated Container
1	AA29423	4-25-96 / 0900	YES	✓ YES
2				
3				
4				
5				
6				
Blank				

Remarks \_\_\_\_\_

Signature of lab sample trustee Frank Sarduj



**APPENDIX I**

**PROJECT PARTICIPANTS**

## **PROJECT PARTICIPANTS**

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### **Corporate Environmental Services**

Lynn F. Robinson, P.E.	Supervisor- Air Programs
Gregory M. Nelson, P.E.	Environmental Compliance Coordinator
Martin Duff	Test Project Leader Senior Environmental Technician
David Smith	Test Team Leader Environmental Technician
Robert Barthelette	Sr. Technical Assistant
Adriano Alcoz	Sr. Technical Assistant
Ray McDarby	Quality Assurance Specialist - CES
Frank Sarduy	Technician - CES
Tom Toombs	Technician-CES
Glenn Naslund	Technician - CES
Bruce Rodriguez	Sr. Technical Assistant
Jeff Sellars	Sr. Technical Assistant

### **F. J. Gannon Station**

Cindy Barringer	Environmental Specialist
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**ATTACHMENT E**

**SUPPLEMENTAL INFORMATION**

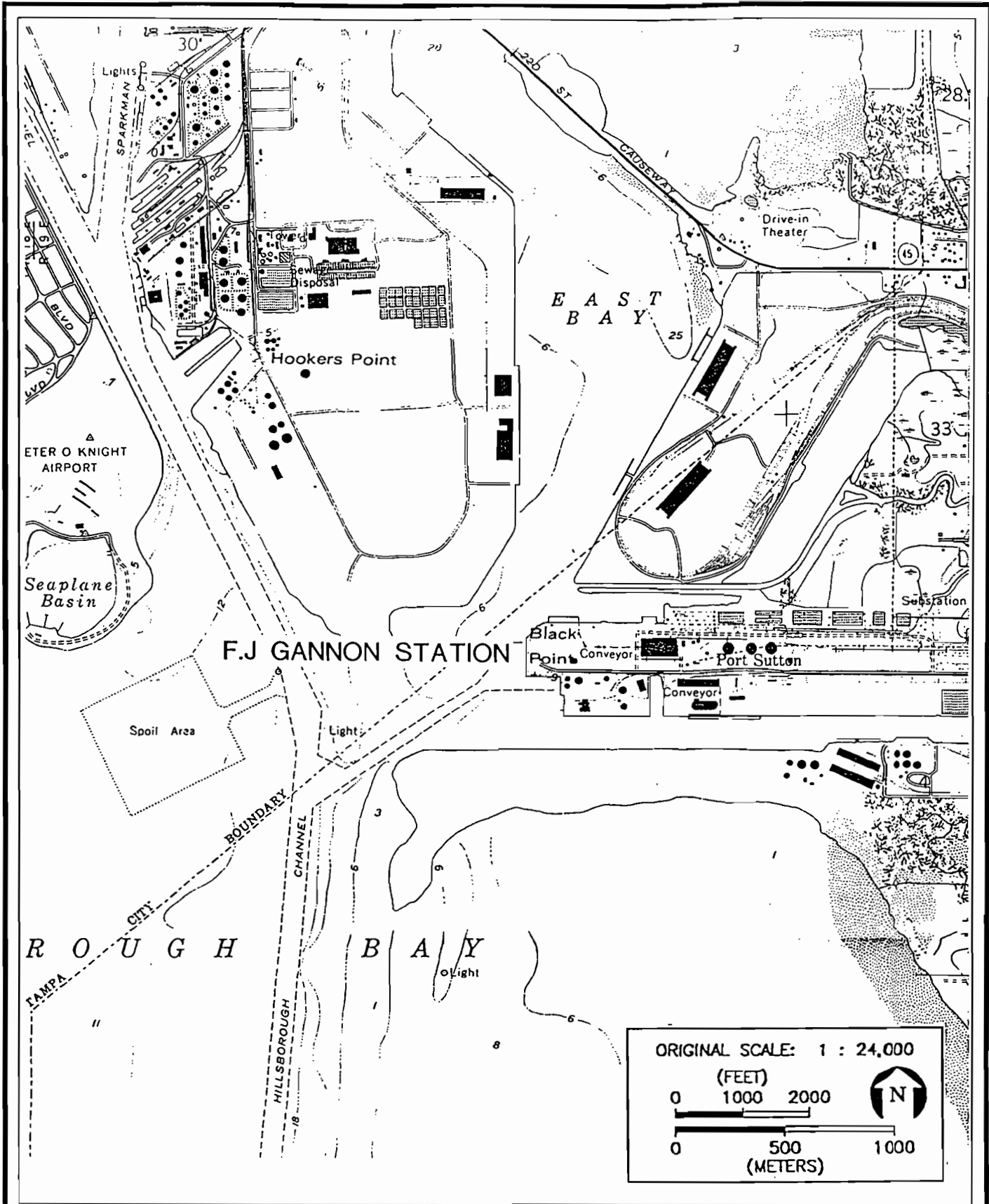
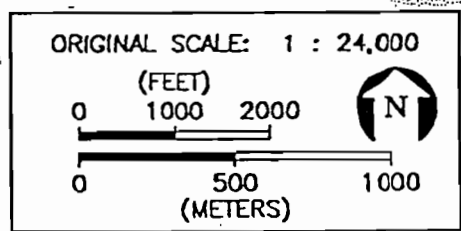


FIGURE II.D.11.  
 F.J. GANNON STATION AREA MAP

Sources: USGS Quad, Tampa, FL 1981.



**ECT**

Environmental Consulting & Technology, Inc.



SCALE: 1"=250'

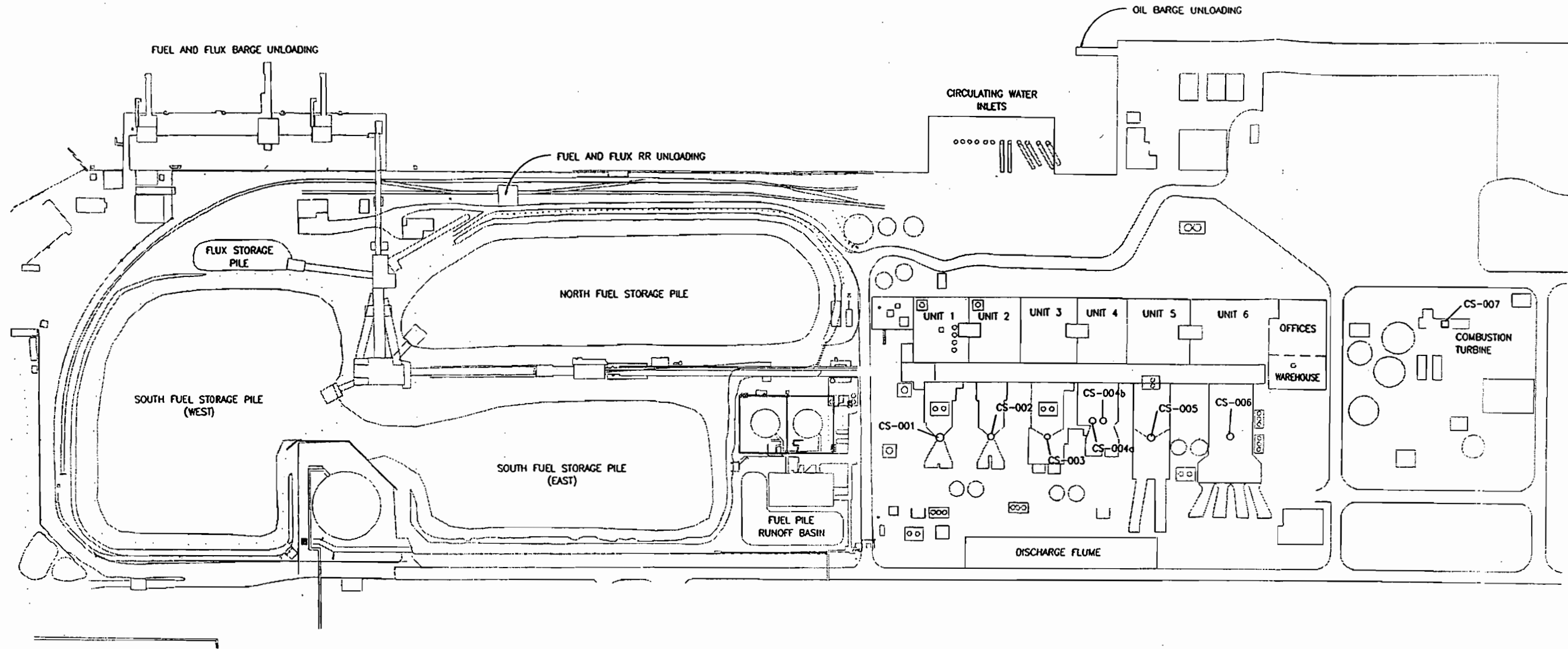


FIGURE II.D.2.4.

F.J. GANNON STATION  
COMBUSTION EMISSION SOURCES

Source: TEC; ECT, 1996.

**ECT**  
Environmental Consulting & Technology, Inc.

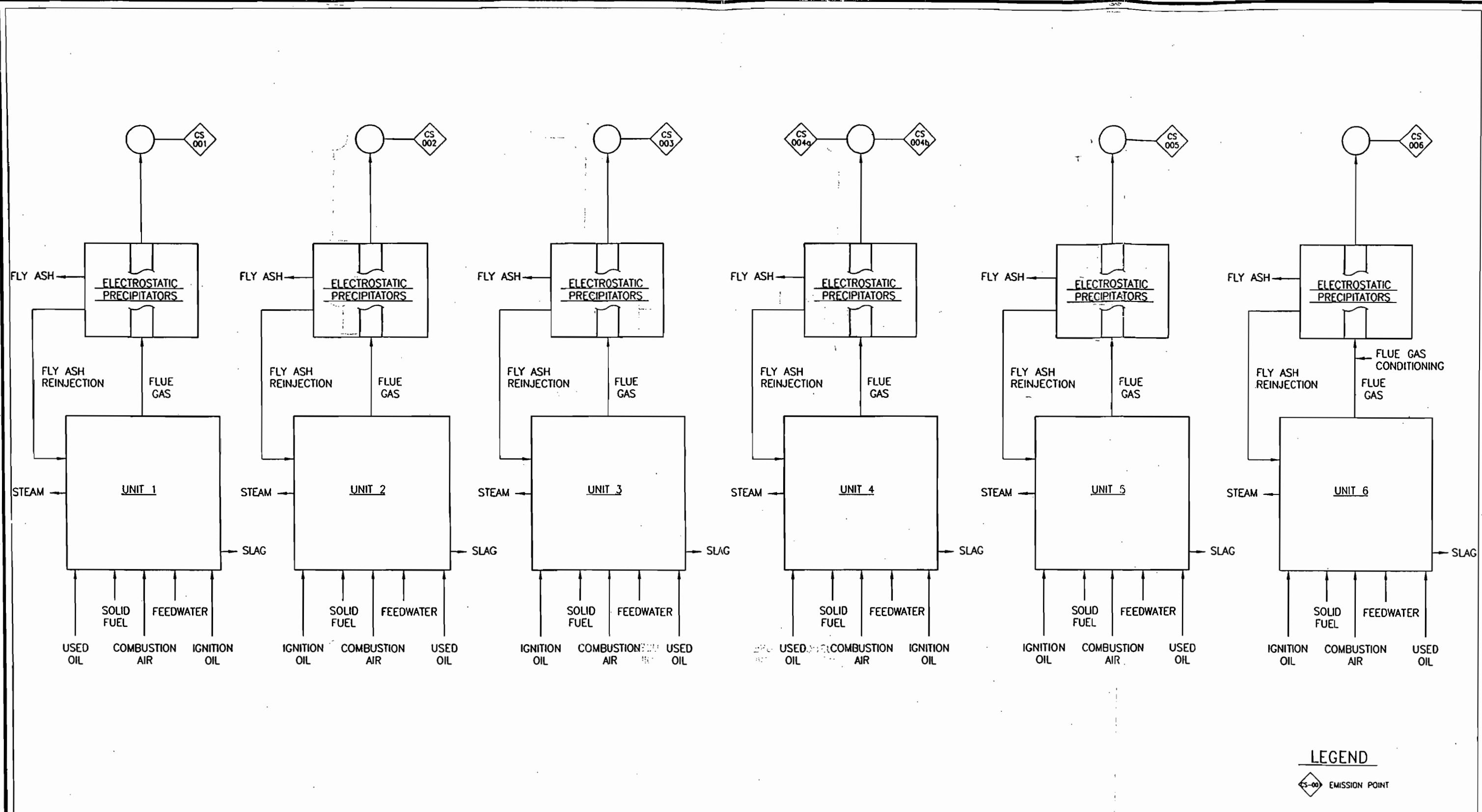


FIGURE I.D.3.6.  
 F.J. GANNON STATION  
 BOILER PROCESS FLOW DIAGRAM  
 Source: ECT, 1996.

