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CleanAir Engineering 500 W. Wood Street Palatine, IL 60067-4975 800-627-0033 www.cleanair.com



Wheelabrator North Broward, Inc. 2600 NW 48th Street Pompano Beach, FL 33073

RECEIVED

APR 27 2010 BUREAU OF AIR REGULATION

REPORT ON COMPLIANCE TESTING

Performed for: WHEELABRATOR NORTH BROWARD, INC. ASH HANDLING SYSTEM, LIME SILO VENTS, UNITS 1, 2 AND 3 SDA INLETS, FF OUTLETS AND STACKS POMPANO BEACH, FL VOLUME I OF II

> CleanAir Project No: 10955-2 Revision 0: April 23, 2010

To the best of our knowledge, the data presented in this report are accurate, complete, error free, legible and representative of the actual emissions during the test program.

Submitted by,

Scott Brown Project Manager sbrown@cleanair.com (800) 627-0033 ext. 4544 Reviewed by,

Kevin O'Halloren, P.E. Project Manager kohalloren@cleanair.com (800) 627-0033 ext. 4661

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Wheelabrator North Broward Inc.

A Waste Management Company

2600 Wiles Road Pompano Beach, FL 33073 (954) 971-8701 Tel (954) 971-8703 Fax

April 27, 2010

UPS# 1Z26X1500394865542

Mr. Lennon Anderson Air Program Administrator Florida Department of Environmental Protection Southeast District 400 North Congress Ave., Suite 200 West Palm Beach, FL 33401 APR 27 2010 BUREAU OF AIR REGULATION

Re: Wheelabrator North Broward 2010 Annual Compliance Stack Test and RATA Reports

Dear Mr. Anderson:

Please find enclosed a copy of the final compliance stack test report and the continuous emissions monitoring system certification RATA report for testing conducted on March 16-18 of this year by Clean Air Engineering, Inc.

1, the undersigned, am a responsible official, as defined in Rule 62-210.200, F.A.C., of the Title V source addressed in this submittal. I hereby certify, based on information and belief formed after reasonable inquiry, that the statements and information in this document are true, accurate and complete.

If there are any questions, please contact this office at (954) 971-8701.

Sincerely,

Scott McIlvaine Plant Manager

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cc: USEPA, Region IV, Pesticides and Toxics Management Division, Air & EPCRA Enforcement Branch, Air Enforcement Section (with) UPS# 1Z26X1500390744304
 FDEP, Tallahassee, Bureau of Air Regulation, New Source Review Section, (with) UPS# 1Z26X1500394730124
 Broward County Department of Planning and Environmental Protection, Air Quality Division (with) UPS# 1Z26X1500393811511

Chuck Faller (with) Ram Tewari – BCWRS (without) Tim Porter (without) Rob French – MPI (with) UPS# 1Z26X1500392976131



Client Reference No: CleanAir Project No: 10955-2

REVISION HISTORY

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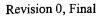
REPORT ON COMPLIANCE TESTING

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PROJECT OVERVIEW

INTRODUCTION

Wheelabrator North Broward, Inc. operates a Refuse-to-Energy facility, located in Pompano Beach, Florida. The facility's emission levels are regulated by the Florida Department of Environmental Protection (FDEP). Wheelabrator North Broward, Inc. contracted Clean Air Engineering (CleanAir) to perform a compliance test program. The lime silo fabric filter vent was observed for visual emissions (VEs) and the ash handling system was observed for fugitive emissions.

The VEs were determined by the facility's continuous opacity monitor system (COMS) data, as allowed under Title V Conditions A.36 (6), A.53 and A.54. The lime silo fabric filter vent was observed for VEs and the ash handling system was observed for fugitive emissions. Testing was conducted in accordance with the Wheelabrator North and South Broward Protocol on Compliance, dated February 8, 2010, 40 CFR 60 Subpart Cb, and applicable sections of the facility's Title V Permit number 0112120-009-AV.

All testing was conducted in accordance with the regulations set-forth by the United States Environmental Protection Agency (EPA) and the Florida Department of Environmental Protection (FDEP).

Key Project Participants

Individuals responsible for coordinating and conducting the test program were:

C. Faller – Wheelabrator North Broward S. Brown - CleanAir

Lee Hoefert of the FDEP was present for portions of the test program.

The CleanAir test crew consisted of the following individuals:

B. Wiltse R. Vicere P. Bihun N. Hitchins A. Obuchowski B. Arnold

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Test Program Parameters

PROJECT OVERVIEW

The sampling was conducted at the Units 1, 2 and 3 Spray Dry Absorption (SDA) Inlet, Fabric Filter (FF) Outlets, Ash Handling System and Lime Silo FF Outlet from March 16 through 18, 2010, and included the following emissions measurements:

- beryllium (Be);
- cadmium (Cd);
- lead (Pb);
- mercury (Hg);
- polychlorinated dibenzo-p-dioxins and polychlorinated dibenzofurans (PCDD/PCDF); Unit 2 only;
- total suspended particulate (TSP);
- hydrogen chloride (HCl);
- total fluoride;
- fugitive emissions (FE);
- visual emissions (VE).

PROJECT OVERVIEW

TEST PROGRAM SYNOPSIS

Test Schedule

The on-site schedule followed during the test program is outlined in Table 1-1.

| Table 1-1: | | | | | | | |
|---------------|-----------------------------------|-------------------|--------------------|----------|-------|-------|--|
| | | Schedule of A | ctivities | | | | |
| Run Number | nber Location Method Analyte Date | | | | | | |
| 1 | Unit 3 SDA Inlet/FF Outlet | USEPA Method 26A | HCI | 03/16/10 | 07:17 | 08:17 | |
| 1 | Unit 1 FF Outlet | USEPA Method 5/29 | Particulate/Metals | 03/16/10 | 07:21 | 09:32 | |
| 1 | Unit 2 FF Outlet | USEPA Method 23 | PCDD/F | 03/16/10 | 08:44 | 13:36 | |
| 2 | Unit 3 SDA Inlet/FF Outlet | USEPA Method 26A | HCI | 03/16/10 | 09:04 | 10:04 | |
| 2 | Unit 1 FF Outlet | USEPA Method 5/29 | Particulate/Metals | 03/16/10 | 10:00 | 12:14 | |
| 3 | Unit 3 SDA Inlet/FF Outlet | USEPA Method 26A | HCI | 03/16/10 | 10:32 | 11:32 | |
| 1 | Unit 3 FF Outlet | USEPA Method 13B | Total Fluorides | 03/16/10 | 11:49 | 13:07 | |
| 3 | Unit 1 FF Outlet | USEPA Method 5/29 | Particulate/Metals | 03/16/10 | 12:36 | 14:47 | |
| 3 2 3 | Unit 3 FF Outlet | USEPA Method 13B | Total Fluorides | 03/16/10 | 13:33 | 14:44 | |
| 3 | Unit 3 FF Outlet | USEPA Method 13B | Total Fluorides | 03/16/10 | 15:07 | 16:16 | |
| 1 | Unit 3 FF Outlet | USEPA Method 5/29 | Particulate/Metals | 03/17/10 | 06:50 | 09:03 | |
| 1 | Unit 2 SDA Inlet/FF Outlet | USEPA Method 26A | HCI | 03/17/10 | 06:54 | 07:54 | |
| 2 | Unit 2 FF Outlet | USEPA Method 23 | PCDD/F | 03/17/10 | 06:54 | 12:19 | |
| 2 | Unit 2 SDA Inlet/FF Outlet | USEPA Method 26A | HCI | 03/17/10 | 09:02 | 10:02 | |
| 2 | Unit 3 FF Outlet | USEPA Method 5/29 | Particulate/Metals | 03/17/10 | 09:26 | 11:38 | |
| 3 | Unit 2 SDA Inlet/FF Outlet | USEPA Method 26A | HCI | 03/17/10 | 10:25 | 11:25 | |
| 1 | Lime Silo | USEPA Method 9 | Opacity | 03/17/10 | 10:26 | 11:45 | |
| 1 | Unit 1 FF Outlet | USEPA Method 13B | Total Fluorides | 03/17/10 | 11:46 | 12:56 | |
| 3 | Unit 3 FF Outlet | USEPA Method 5/29 | Particulate/Metals | 03/17/10 | 11:59 | 14:11 | |
| 3 3 2 | Unit 2 FF Outlet | USEPA Method 23 | PCDD/F | 03/17/10 | 12:53 | 17:26 | |
| 2 | Unit 1 FF Outlet | USEPA Method 13B | Total Fluorides | 03/17/10 | 13:15 | 14:27 | |
| 3 | Unit 1 FF Outlet | USEPA Method 13B | Total Fluorides | 03/17/10 | 14:45 | 15:53 | |
| 1 | Unit 1 SDA Inlet/FF Outlet | USEPA Method 26A | HCI | 03/18/10 | 07:02 | 08:02 | |
| 1 | Unit 2 FF Outlet | USEPA Method 13B | Total Fluorides | 03/18/10 | 07:09 | 08:24 | |
| 1 | Unit 2 FF Outlet | USEPA Method 5/29 | Particulate/Metals | 03/18/10 | 07:09 | 09:22 | |
| · 1 | Ash Handling System | USEPA Method 22 | Fugitive Emissions | 03/18/10 | 07:22 | 12:20 | |
| 2 | Unit 2 FF Outlet | USEPA Method 13B | Total Fluorides | 03/18/10 | 08:56 | 10:10 | |
| 2 | Unit 1 SDA Inlet/FF Outlet | USEPA Method 26A | HCI | 03/18/10 | 09:26 | 10:37 | |
| 2 | Unit 2 FF Outlet | USEPA Method 5/29 | Particulate/Metals | 03/18/10 | 09:49 | 12:02 | |
| 2 3 | Unit 2 FF Outlet | USEPA Method 13B | Total Fluorides | 03/18/10 | 10:45 | 12:05 | |
| 3 | Unit 1 SDA Inlet/FF Outlet | USEPA Method 26A | HCI | 03/18/10 | 11:49 | 12:49 | |
| 3 | Unit 2 FF Outlet | USEPA Method 5/29 | Particulate/Metals | 03/18/10 | 12:27 | 14:39 | |

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PROJECT OVERVIEW

TEST PROGRAM SYNOPSIS (CONTINUED)

Results Summary

Table 1-2 summarizes the results of the test program. A more detailed presentation of the test conditions and results of analysis are shown in Tables 2-1 through 2-20 on pages 2-1 through 2-18. Subpart Cb-required operating data is summarized in Table 1-3, and opacity and fugitive emission results are presented in Table 1-4, both on page 1-5.

| Table 1-2: Summary of Test Results | | | | | | |
|---|-------------------|-------------------|-------------------|------------------------------|--|--|
| Source | Average Unit 1 | Average Unit 2 | Average Unit 3 | Permit Limit ¹ | | |
| Constituent | | | | | | |
| Particulate (mg/dscm @7% O₂) | <0.54 | 1.6 | 0.84 | 25 | | |
| Visual Emissions (%, by COMS) ² | 2 | 0 | 2 | 10 | | |
| Fluoride (lb/MMBtu as HF) ³ | <0.000036 | <0.000038 | <0.000038 | 0.0040 | | |
| Total PCCD/PCDF (ng/dscm @ 7% O₂) | NA | 0.41 | NA | 30 | | |
| Hydrogen Chloride (ppmdv @ 7% O₂) <u>or</u> | 20 | 18 | 18 | 29 | | |
| Hydrogen Chloride Removal (%) ^⁴ | 97% | 96% | 97% | >95 | | |
| Beryllium (mg/dscm @ 7% O₂) | <0.00003 | <0.00003 | <0.00003 | 0.001 | | |
| Cadmium (mg/dscm @ 7% O₂) | <0.00011 | <0.00016 | <0.00011 | 0.035 | | |
| Lead (mg/dscm @ 7% O ₂) | 0.00062 | <0.00051 | 0.00016 | 0.40 | | |
| Mercury (µg/dscm @ 7% O₂) | 4.7 | 5.2 | 4.6 | 50 | | |
| Average Steam Flow (Klbs/hr)⁵ | 183.8 | 184.0 | 184.1 | 186 | | |
| Average FF Inlet Temperature (^o F) ⁵ | 318 | 320 | 312 | NA | | |

¹ Limits obtained from facilities Title V Permit 0112119-009-AV.

²Visual Emissions (opacity) was obtained from the facilities COMS data as allowed under Title V Conditions B.53(6), B.76 and B.81. ³Ib/MMBtu calculations used Fd of 9,570 for MSW as per Method 19.

⁴ Removal for hydrogen chloride calculated in the unit of its standard (ppmdv @ 7% O₂). The hydrogen chloride limit is

29 ppmd v @ 7% O2 or 95% removal, which ever is less stringent.

⁵ From all compliance test runs.

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| | Tał Subpart Cb-requ | ole 1-3: lired Operati | ng Data | | |
|---|---|---|---|---|---|
| Proc | ess Condition | | | | |
| Unit | 1 Maximum Demonstrated Combustor | ·Load (Klbs/h | r) ¹ | 184.5 ² | |
| Unit 2 | 2 Maximum Demonstrated Combustor | ·Load (Klbs/h | r) ¹ | 184.3 | |
| Unit 3 | 3 Maximum Demonstrated Combustor | Load (Klbs/h | r) ¹ | 184.1 ³ | |
| Unit ' | 1 Maximum Particulate Control Device | Inlet Tempe | rature (°F) ⁴ | 322 ² | |
| Unit 2 Maximum Particulate Control Device Inlet Temperature (°F) ⁴ 321 | | | | | |
| Unit 2 | 2 Maximum Particulate Control Device | iniet i empei | rature (***) | 321 | |
| Unit 3 ¹ From ² From ³ From | 2 Maximum Particulate Control Device 3 Maximum Particulate Control Device 40CFR60.58b (i) (8) the maximum demonstrat CleanAir Cb test report dated April 22, 2009 (F CleanAir Cb test report dated April 30, 2008 (F 40CFR60.58b (i) (9) the highest four hour aver | ed load during P Project 10735). Project 10455). | CDD/PCDF test | 325 ³ | - |
| Unit 3 ¹ From ² From ³ From | 3 Maximum Particulate Control Device 40CFR60.58b (i) (8) the maximum demonstrat CleanAir Cb test report dated April 22, 2009 (F CleanAir Cb test report dated April 30, 2008 (F 40CFR60.58b (i) (9) the highest four hour aver Tab | Inlet Temper ed load during P Project 10735). Project 10455). rage during PCD | CDD/PCDF test | 325 ³ | - |
| Unit 3 ¹ From ² From ³ From | 3 Maximum Particulate Control Device 40CFR60.58b (i) (8) the maximum demonstrat CleanAir Cb test report dated April 22, 2009 (F CleanAir Cb test report dated April 30, 2008 (F 40CFR60.58b (i) (9) the highest four hour aver | Inlet Temper ed load during P Project 10735). Project 10455). rage during PCD | CDD/PCDF test | 325 ³ | |
| Unit : ¹ From ² From ³ From ⁴ From <u>urce</u> | 3 Maximum Particulate Control Device 40CFR60.58b (i) (8) the maximum demonstrat CleanAir Cb test report dated April 22, 2009 (F CleanAir Cb test report dated April 30, 2008 (F 40CFR60.58b (i) (9) the highest four hour aver Tab Opacity and Fugitive | Inlet Temper ed load during P Project 10735). Project 10455). rage during PCD Ile 1-4: Emission Te Sampling | CDD/PCDF test D/PCDF testing. | 325 ³ ing, four hour average. Permit | |
| Unit : ¹ From ² From ³ From ⁴ From <u>urce</u> | 3 Maximum Particulate Control Device 40CFR60.58b (i) (8) the maximum demonstrat CleanAir Cb test report dated April 22, 2009 (F CleanAir Cb test report dated April 30, 2008 (F 40CFR60.58b (i) (9) the highest four hour aver Tab Opacity and Fugitive Constituent ing System ² Fugitive Emissions (% of obseravtion time) | Inlet Temper ed load during P Project 10735). Project 10455). rage during PCD Ile 1-4: Emission Te Sampling | rature (°F) ⁴ CDD/PCDF test D/PCDF testing. est Results Results 0 | 325 ³ ing, four hour average. Permit Limit ³ 5% | |
| Unit : ¹ From ² From ³ From ⁴ From <u>urce</u> | 3 Maximum Particulate Control Device 40CFR60.58b (i) (8) the maximum demonstrat CleanAir Cb test report dated April 22, 2009 (F CleanAir Cb test report dated April 30, 2008 (F 40CFR60.58b (i) (9) the highest four hour aver Tab Opacity and Fugitive Constituent ing System ² | Inlet Temper ed load during P Project 10735). Project 10455). age during PCD Ile 1-4: Emission Tr Sampling Method | rature (°F) ⁴ CDD/PCDF test D/PCDF testing. est Results Results | 325 ³ ing, four hour average. Permit Limit ¹ | |

³ The Lime Silo was observed for one complete truck unloading.

Discussion of Test Program

All test methods were done in triplicate. All data that is reported in the units of lb/MMBTU utilized the Fd of 9,570 as per EPA Method 19.

All equipment utilized for compliance testing was manufactured by Clean Air Engineering, except for the Servomex O_2/CO_2 analyzer utilized for all of the integrated gas sample bag analysis.

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PROJECT OVERVIEW TEST PROGRAM SYNOPSIS (CONTINUED)

During the compliance testing, all three (3) boilers were operated within 10% of the 186,000 lb/hr maximum steam flow rating. The result tables present each boiler's steam output for every test run.

Raina Vicere performed the fugitive emission readings (per EPA Method 22) on the Ash Handling System and conducted the VE readings (per EPA Method 9) on the Lime Silo during one (1) entire truck unloading. Ms. Vicere's VE evaluation certificate is presented in Appendix J.

Any fractions of the mercury analysis that were reported as not detected were summed as zero if there was at least one (1) fraction detected in that run. The beryllium, cadmium and lead front- and back-half fractions were combined proportionately for analysis, per EPA Method 29, Section 5.4.

Field blanks were collected for the Method 23 and 29 testing by assembling a used set of glassware, taking the complete train to the outlet location and performing a leakcheck. These samples were treated exactly as the other samples. The results for the Method and Field Blanks are presented in Table 2-19 on page 2-17, as well as Appendix I. The results of the Method 29 reagent blank analysis were used to correct any data, as outlined in Method 29.

All Method 23 samples were analyzed with the DB-5S column with modified calibration and additional quality assurance procedures as a direct substitute for the DB-5 and DB-225 columns. Confirmation of the 2,3,7,8 TCDF and TCDD 2,3,7,8 isomers was performed on the DB-5S column. The DB-5S column and modified calibration procedures meet the column separation requirement and can be used as a direct substitute for the DB-5 and DB-225 columns, in accordance with Method 23 as approved by the EPA. All QA/QC data (spikes and recoveries) for Method 23, as well as the EPA Audit Sample results, are presented in Appendix I.

The Method 23 results for all three (3) runs contained at least one (1) estimated maximum possible concentration (EMPC) value. EMPC results do not meet all the identification criteria required by Method 23 to be positively identified as a dioxin or furan. Specifically, the integrated ion abundance ratios were not within 15% of the theoretical value limits specified in Method 23, Section 5.3.2.5, Table 4. The laboratory reports EMPC results as zero and, for this reason, all EMPC results are enclosed in brackets and are considered zero when calculating total dioxin/furans.

Chuck Faller of Wheelabrator North Broward, Inc. provided the process (operating) data. This data is presented in its entirety in Appendix C. All process data and CleanAir run times are based on facility CEM and Bailey Computer Time, which is 70 minutes earlier than actual Eastern Standard Time (EST). The Lime Silo opacity start and stop times are based on CEM time; however, the initial and final truck weights were recorded using EST.

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PROJECT OVERVIEW

TEST PROGRAM SYNOPSIS (CONTINUED)

Integrated gas samples (IGS) were collected in a vinyl sample bag from every sample train. The contents of the bag were then analyzed for oxygen (O_2) and carbon dioxide (CO_2) concentrations using an O_2/CO_2 continuous monitoring analyzer calibrated with EPA Protocol gases. A linearity and bias check was performed on the analyzers before each set of bags was analyzed, and then a post bias check was performed after each set of bags was analyzed. All data was recorded using CleanAir's data acquisition system. The results of the IGS bag analyses are presented in Appendix G.

Metals and particulate matter sampling were combined during this test program, per the Method 29, Section 1.2 principle, "This method may be used to determine particulate emissions in addition to the metals emissions if the prescribed procedures and precautions are followed".

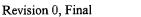
Sixty-minute Method 26A sample trains at the SDA Inlets and FF Outlets were utilized to exhibit compliance with each unit's HCl limit(s). The Method 26A was modified to a single-point constant sampling rate at all test locations.

The FDEP supplied audit samples for PCDD/PCDF, metals and HCl to CleanAir. The analytical results of these samples are presented in Appendix I, along with each respective lab report.

The initial reporting of the high HCl audit sample was not within the required 5% of actual concentration. The lab reanalyzed all of the samples, including the audits after concluding that erroneously contaminated glassware created the high audit result. The results of the reanalysis are presented in this report and an explanation of the failed audit is presented, along with the laboratory report, in Appendix I. The reanalyzed audit was within 5% of the audit samples value.

At the request of Wheelabrator North Broward, Inc., the Unit 2 Method 23 Run 2 was paused for 42 minutes in order to accommodate a soot blow. During the delay, the probe was removed from the FF Outlet and the XAD trap was kept cold. Once the soot blow was complete, the probe was placed back in the duct and the test run was resumed.

End of Section 1 – Project Overview



Client Reference No: CleanAir Project No: 10955-2

| RES | ULTS | e 2-1: | | | |
|-------------------------------------|---|------------|------------|------------|------------|
| | Unit 1 FF Outlet – Particu | | and Mercu | rv | |
| Run N | | 1 | 2 | 3 | Average |
| Date (2 | 2010) | Mar 16 | Mar 16 | Mar 16 | |
| Start T | ime (approx.) | 07:21 | 10:00 | 12:36 | |
| Stop T | ime (approx.) | 09:32 | 12:14 | 14:47 | |
| | ss Conditions | | | | |
| R _P | Steam Production Rate (Klbs/hr) | 183.9 | 184.4 | 183.4 | 183.9 |
| P ₁ | Fabric Filter Inlet Temperature (°F) | 310 | 313 | 320 | 314 |
| | | 0.5 | 0.5 | 0.7 | • • |
| O₂ CO₂ | Oxygen (dry volume %) Carbon dioxide (dry volume %) | 9.5 9.9 | 9.5 9.9 | 9.7 9.8 | 9.6 9.9 |
| T _s | Sample temperature (°F) | 293 | 295 | 301 | 296 |
| Bw | Actual water vapor in gas (% by volume) | 20.1 | 20.0 | 19.7 | 20.0 |
| Gas Fle | ow Rate | | | | |
| Qa | Volumetric flow rate, actual (acfm) | 191,586 | 191,421 | 193,814 | 192,274 |
| \mathbf{Q}_{std} | Volumetric flow rate, dry standard (dscfm) | 105,082 | 104,870 | 105,806 | 105,252 |
| Sampli | ng Data | | | | |
| V_{mstd} | Volume metered, standard (dscf) | 80.55 | 81.15 | 81.55 | 81.09 |
| %I | Isokinetic sampling (%) | 98.8 | 99.7 | 99.3 | 99.3 |
| | tory Data | - | | | |
| m" | Net matter collected (g) | 0.00049 | 0.00218 | <0.00020 | |
| | ble Particulate Results | | | | |
| C _{sd} | Particulate Concentration (mg/dscm) | 0.22 | 0.95 | <0.087 | <0.42 |
| C _{sd7} | Particulate Concentration @7% O ₂ (mg/dscm) | 0.26 | 1.2 | <0.11 | <0.51 |
| | y Laboratory Data | 7 7000 | 0.0454 | 0 75 40 | |
| mn | Total matter corrected for allowable blanks (µg) | 7.7629 | 8.8151 | 9.7549 | |
| - ' | y Results - Total | 2.4 | 2.0 | 4.0 | 3.8 |
| C _{sd} C _{sd7} | Concentration (µg/dscm) Concentration @7% O₂ (µg/dscm) | 3.4 4.2 | 3.8 4.7 | 4.2 5.3 | 3.8 4.7 |
| | m Laboratory Data | | | 0.0 | |
| m _n | Total matter corrected for allowable blanks (µg) | <0.0500 | <0.0500 | <0.0500 | |
| | m Results - Total | | | 0.0000 | |
| | Concentration (mg/dscm) | <0.00002 | <0.00002 | <0.00002 | <0.00002 |
| | Concentration @7% O ₂ (mg/dscm) | < 0.00003 | < 0.00003 | < 0.00003 | <0.00003 |
| | m Laboratory Data | | | | |
| mn | Total matter corrected for allowable blanks (µg) | <0.2000 | 0.2093 | <0.2000 | |
| Cadmiu | m Results - Total | | | | |
| C _{sd} | Concentration (mg/dscm) | <0.000088 | 0.000091 | <0.000087 | <0.00088 |
| C_{sd7} | Concentration @7% O_2 (mg/dscm) | <0.00011 | 0.00011 | <0.00011 | <0.00011 |
| Lead La | boratory Data | | | | |
| m" | Total matter corrected for allowable blanks (µg) | 1.0847 | 1.1424 | 1.2738 | |
| Lead Re | esults - Total | | | | |
| C_{sd} | Concentration (mg/dscm) | 0.00048 | 0.00050 | 0.00055 | 0.00051 |
| C_{sd7} | Concentration @7% O_2 (mg/dscm) | 0.00058 | 0.00060 | 0.00069 | 0.00062 |

Client Reference No: CleanAir Project No: 10955-2



2-2

RESULTS Table 2-2: Unit 1 FF Outlet - Fluorides 2 Run No. 3 Average 1 Mar 17 Mar 17 Mar 17 Date (2010) 11:46 13:15 14:45 Start Time (approx.) 12:56 14:27 15:53 Stop Time (approx.) **Process Conditions** 184.0 184.0 184.1 184.0 R_P Steam Production Rate (Klbs/hr) 320 P₁ Fabric Filter Inlet Temperature (°F) 320 320 320 Gas Conditions Oxygen (dry volume %) 10.6 10.1 10.0 10.2 O2 CO2. 9.1 9.6 9.8 9.5 Carbon dioxide (dry volume %) 303 302 302 T, Sample temperature (°F) 303 В" Actual water vapor in gas (% by volume) 19.9 20.5 21.0 20.5 Gas Flow Rate 207,433 205,926 198,952 204,104 Volumetric flow rate, actual (acfm) Qa Qstd Volumetric flow rate, dry standard (dscfm) 111,627 111,678 106,345 109,883 Sampling Data 42.7316 42.4517 41.1525 42.1120 V_{mstd} Volume metered, standard (dscf) 100.2534 100.1239 99.4233 101.2130 %I Isokinetic sampling (%) Laboratory Data < 0.03681 < 0.03385 < 0.03889 Total HF collected (mg) m Hydrogen Fluoride (HF) Results < 0.034 < 0.037 <0.040 < 0.037 C_{sd} HF Concentration (ppmdv) C_{sd7} HF Concentration @7% O₂ (ppmdv) <0.049 < 0.044 <0.051 <0.048 <0.030 < 0.028 < 0.033 <0.031 HF Concentration (mg/dscm) C_{sd} HF Concentration @7% O2 (mg/dscm) < 0.041 < 0.036 < 0.042 <0.040 C_{sd7} Elb/hr HF Rate (lb/hr) < 0.013 < 0.012 <0.013 <0.013 E_{Fď} HF Rate - Fd-based (lb/MMBtu) < 0.000037 < 0.000033 < 0.000038 < 0.000036

Client Reference No: CleanAir Project No: 10955-2

| RES | JLTS | | | | |
|-------------------|--|----------------|--------------------|----------|---------|
| | | le 2-3: | | | |
| · | Unit 1 FF Outlet and SDA | Inlet - Hydrog | en Chloride | <u> </u> | |
| Run N | D. | 1 | 2 | 3 | Average |
| Date (2 | 2010) | Mar 18 | Mar 18 | Mar 18 | |
| Start Ti | me (approx.) | 07:02 | 09:26 | 11:49 | |
| Stop Ti | me (approx.) | 08:02 | 10:37 [°] | 12:49 | |
| Proces | s Conditions | | | | |
| R _P | Steam Production Rate (Klbs/hr) | 183.5 | 1 8 4.1 | 182.8 | 183.5 |
| P ₁ | Fabric Filter Inlet Temperature (°F) | 320 | 320 | 320 | 320 |
| SDA In | let Gas Conditions | | | | |
| O ₂ | Oxygen (dry volume %) | 9.1 | 9.0 | 9.7 | 9.3 |
| CO2 | Carbon dioxide (dry volume %) | 10.2 | 10.4 | 9.8 | 10.1 |
| Τs | Sample temperature (°F) | 489 | 489 | 497 | 492 |
| B _w | Actual water vapor in gas (% by volume) | 17.5 | 16.9 | 16.6 | 17.0 |
| SDA In | let Sampling Data | | | | |
| V _{mstd} | Volume metered, standard (dscf) | 38.19 | 36.42 | 35.65 | 36.76 |
| SDA In | let Laboratory Data | | | | |
| m | Total HCI collected (mg) | 789.381 | 879.513 | 662.680 | |
| SDA In | let Hydrogen Chloride (HCI) Results | | | | |
| \mathbf{C}_{sd} | HCI Concentration (ppmdv) | 482 | 563 | 433 | 493 |
| C_{sd7} | HCI Concentration @7% O ₂ (ppmdv) | 568 | 658 | 538 | 588 |
| FF Outl | et Gas Conditions | | | | |
| O ₂ | Oxygen (dry volume %) | 9.9 | 9.7 | 10.1 | 9.9 |
| CO2 | Carbon dioxide (dry volume %) | 9.5 | 9.7 | 9.4 | 9.5 |
| Тs | Sample temperature (°F) | 308 | 309 | 310 | 309 |
| Bw | Actual water vapor in gas (% by volume) | 19.9 | 21.4 | 19.6 | 20.3 |
| FF Outl | et Sampling Data | | | | |
| V _{mstd} | Volume metered, standard (dscf) | 41.10 | 40.79 | 40.64 | 40.85 |
| FF Outl | et Laboratory Data | | | | |
| m | Total HCI collected (mg) | 30.484 | 25.143 | 26.450 | |
| FF Outb | et Hydrogen Chloride (HCI) Results | | | | |
| C _{sd} | HCl Concentration (ppmdv) | 17 | 14 | 15 | 16 |
| C _{sd7} | HCI Concentration @7% O ₂ (ppmdv) | 22 | 18 | 19 | 20 |
| RE | Reduction Efficiency (% Removal) | 96% | 97% | 96% | 97% |

Client Reference No: CleanAir Project No: 10955-2

2-4

| RESI | JLTS | | | | |
|---------------------------|---|--------------|--------------|--------------|--------------|
| | Table Unit 2 FF Outlet – Particul | | and Mercur | TV. | |
| Run No | | 1 1 | 2 | 3 | Average |
| Date (2 | 010) | Mar 18 | Mar 18 | Mar 18 | |
| | me (approx.) | 07:09 | 09:49 | 12:27 | |
| | me (approx.) | 09:22 | 12:02 | 14:39 | |
| | s Conditions | 192.0 | 192.0 | 1920 | 400.0 |
| R _P P₁ | Steam Production Rate (Klbs/hr) Fabric Filter Inlet Temperature (°F) | 183.9 320 | 182.9 320 | 183.9 321 | 183.6 320 |
| | nditions | 020 | 520 | 021 | ULU |
| 02 | Oxygen (dry volume %) | 10.1 | 9.8 | 9.9 | 9.9 |
| CO₂ | Carbon dioxide (dry volume %) | 9.3 | 9.6 | 9.6 | 9.5 |
| T _s | Sample temperature (°F) | 307 | 308 | 308 | 308 |
| Bw | Actual water vapor in gas (% by volume) | 20.4 | 20.5 | 21.0 | 20.6 |
| Gas Flo | ow Rate | | | | |
| Qa | Volumetric flow rate, actual (acfm) | 201,928 | 193,105 | 199,217 | 198,083 |
| Q_{std} | Volumetric flow rate, dry standard (dscfm) | 108,134 | 103,333 | 105,868 | 105,778 |
| Sampli | ng Data | | | | |
| V _{mstd} | Volume metered, standard (dscf) | 84.18 | 79.34 | 82.11 | 81.88 |
| %1 | Isokinetic sampling (%) | 100.3 | 98.9 | 99.9 | 99.7 |
| | tory Data | 0.00404 | 0.00004 | 0.00050 | |
| m, | Net matter collected (g) | 0.00404 | 0.00231 | 0.00252 | |
| _ | ole Particulate Results | 4 7 | 4.0 | | |
| C _{sd} | Particulate Concentration (mg/dscm) Particulate Concentration @7% O₂ (mg/dscm) | 1.7 2.2 | 1.0 1.3 | 1.1 1.4 | 1.3 1.6 |
| C _{sd7} | | ۷.۷ | 1.5 | 1.4 | 1.0 |
| m _n | y Laboratory Data Total matter corrected for allowable blanks (µg) | 9.1977 | 9.2740 | 10.1318 | |
| | | 5.1577 | 5.2140 | 10.1318 | |
| Wercur C _{sd} | y Results - Total Concentration (µg/dscm) | 3.9 | 4.1 | 4.4 | 4.1 |
| C _{sd} | Concentration ($\mu g/dscm$) Concentration ($\pi g/dscm$) | 5.0 | 5.1 | 5.5 | 5.2 |
| | Im Laboratory Data | | | | |
| m _n | Total matter corrected for allowable blanks (µg) | < 0.0500 | <0.0500 | < 0.0500 | |
| | Im Results - Total | | | | |
| C _{sd} | Concentration (mg/dscm) | < 0.00002 | < 0.00002 | < 0.00002 | <0.00002 |
| C _{sd7} | Concentration @7% O2 (mg/dscm) | < 0.00 003 | < 0.00003 | < 0.00003 | <0.00003 |
| Cadmiu | Im Laboratory Data | | | | |
| m" | Total matter corrected for allowable blanks (µg) | 0.4679 | <0.2000 | <0.2000 | |
| Cadmiu | um Results - Total | | | | |
| C_{sd} | Concentration (mg/dscm) | 0.00020 | <0.000089 | <0.000086 | <0.00012 |
| C_{sd7} | Concentration @7% O2 (mg/dscm) | 0.00025 | <0.00011 | <0.00011 | <0.00016 |
| Lead La | aboratory Data | | | | |
| mn | Total matter corrected for allowable blanks (μg) | 2.4408 | <0.2000 | <0.2000 | |
| Lead R | esults - Total | | | | |
| C _{sd} | Concentration (mg/dscm) | 0.0010 | < 0.000089 | <0.000086 | <0.00040 |
| C _{sd7} | Concentration @7% O ₂ (mg/dscm) | 0.0013 | <0.00011 | <0.00011 | <0.00051 |

Client Reference No: CleanAir Project No: 10955-2

| RES | ULTS | | | | |
|-------------------|---|------------------|---|------------|---|
| | | ole 2-5: | an san ang kanang ka | | In the second second second second second second second second second second second second second second second |
| | | utlet - Fluoride | · | | |
| Run N | 0. | 1 | 2 | 3 | Average |
| Date (2 | 2010) | Mar 18 | Mar 18 | Mar 18 | |
| Start Ti | me (approx.) | 07:09 | 08:56 | 10:45 | |
| Stop Ti | me (approx.) | 08:24 | 10:10 | 12:05 | |
| Proces | s Conditions | | | | |
| RP | Steam Production Rate (Klbs/hr) | 183.9 | 184.2 | 183.0 | 183.7 |
| Ρı | Fabric Filter Inlet Temperature (°F) | 321 | 320 | 320 | 320 |
| Gas Co | onditions | | | | |
| O ₂ | Oxygen (dry volume %) | 10.0 | 9.6 | 10.2 | 9.9 |
| CO2 | Carbon dioxide (dry volume %) | 9.3 | 9.6 | 9.1 | 9.3 |
| Τs | Sample temperature (°F) | 306 | 305 | 306 | 306 |
| B, | Actual water vapor in gas (% by volume) | 20.7 | 21.1 | 20.3 | 20.7 |
| Gas Flo | ow Rate | | | | |
| Qa | Volumetric flow rate, actual (acfm) | 190,226 | 182,805 | 185,088 | 186,040 |
| Q_{std} | Volumetric flow rate, dry standard (dscfm) | 101,644 | 9 7 ,309 | 99,545 | 99,499 |
| Sampli | ng Data | | | | |
| V _{mstd} | Volume metered, standard (dscf) | 38.2069 | 36.8944 | 37.3103 | 37.4705 |
| %1 | Isokinetic sampling (%) | 98.3144 | 99.1667 | 98.0324 | 98.5045 |
| Labora | tory Data | | | | |
| mn | Total HF collected (mg) | <0.03601 | < 0.03449 | <0.03537 | |
| Hydrog | en Fluoride (HF) Results | | | | |
| C _{sd} | HF Concentration (ppmdv) | <0.040 | <0.040 | <0.040 | <0.040 |
| C_{sd7} | HF Concentration @7% O ₂ (ppmdv) | <0.051 | <0.049 | <0.052 | <0.051 |
| C_{sd} | HF Concentration (mg/dscm) | <0.033 | <0.033 | <0.033 | <0.033 |
| C_{sd7} | HF Concentration @7% O ₂ (mg/dscm) | <0.043 | <0.041 | <0.043 | <0.042 |
| Elb/hr | HF Rate (lb/hr) | <0.013 | <0.012 | <0.012 | <0.012 |
| EFd | HF Rate - Fd-based (lb/MMBtu) | <0.000038 | < 0.000037 | < 0.000039 | <0.00038 |

Client Reference No: CleanAir Project No: 10955-2

| RESU | LTS | | | | |
|----------------------|--|--------------------|--------------------|--------------------|--------------------|
| | Table 2-6 Unit 2 FF Outlet - PC | | 5 | | |
| Run No. | | 1 | 2 | 3 | Average |
| Date (201 | 0) | Mar 16 | Mar 17 | Mar 17 | |
| Start Time | | 08:44 | 06:54 | 12:53 | |
| Stop Time | (approx.) | 13:36 | 12:19 | 17:26 | |
| Process (| Conditions | | | | |
| R _P | Steam Production Rate (Klbs/hr) | 184.1 | 184.3 | 183.9 | 184.1 |
| P ₁ | Fabric Filter Inlet Temperature (°F) | 314 | 321 | 320 | 319 |
| Gas Cond | litions | | | | |
| O₂ | Oxygen (dry volume %) | 9.7 | 9.7 | 10.3 | 9.9 |
| CO₂ | Carbon dioxide (dry volume %) | 9.7 | 9.8 | 9.5 | 9.7 |
| Ts | Sample temperature (°F) | 301 | 307 | 308 | 305 |
| B _w | Actual water vapor in gas (% by volume) | 20.1 | 20.8 | 20.5 | 20.5 |
| Gas Flow | | | | | |
| Q, | Volumetric flow rate, actual (acfm) | 198,967 | 214,211 | 203,730 | 205,636 |
| Q _{std} | Volumetric flow rate, dry standard (dscfm) | 107,335 | 113,400 | 108,891 | 109,875 |
| Sampling | | | | | |
| V _{mstd} | Volume metered, standard (dscf) | 156.06 | 168.82 | 164.13 | 163.00 |
| %1 | Is okinetic sampling (%) | 98.0 | 100.3 | 101.6 | 100.0 |
| <u>Results (N</u> | ID and EMPC = 0) | | | | |
| Laborator | y Data from USEPA Method 23 | | | | |
| m'n | Total PCDDs & PCDFs (ng) | 1.2600 | 1.5100 | 1.6700 | |
| m _{n_teq} | Total TEQ PCDDs & PCDFs (ng) | 0.0168 | 0.0227 | 0.0270 | |
| | D/F Results (TEF=1) | | | | |
| C _{sd} | PCDD/F Concentration (ng/dscm) | 0.29 | 0.32 | 0.36 | 0.32 |
| C _{sd7} | PCDD/F Concentration @7% O ₂ (ng/dscm) | 0.35 | 0.39 | 0.47 | 0.41 |
| | PCDD/F Rate (lb/hr) | 1.15E-07 | 1.34E-07 | 1.47E-07 | 1.32E-07 |
| E _{Fd} | PCDD/F Rate - F _d based (Ib/MMBtu) | 3.17E-10 | 3.53E-10 | 4.24E-10 | 3.65E-10 |
| | D/F TEQ Results (using USEPA/INTL 1989 TEFs) | 0.0030 | 0.0047 | 0.0050 | |
| C _{sdTEQ} | TEQ Concentration (ng/dscm) | 0.0038 | 0.0047 | 0.0058 | 0.0048 |
| Csd7TEQ Elb/hrTEQ | TEQ Concentration @7% O ₂ (ng/dscm) TEQ Rate (lb/hr) | 0.0047 1.53E-09 | 0.0059 2.02E-09 | 0.0076 2.37E-09 | 0.0061 1.97E-09 |
| E _{FdTEQ} | TEQ Rate - F _d -based (lb/MMBtu) | 4.23E-12 | 5.31E-12 | 6.85E-12 | 5.47E-12 |
| | ID and EMPC = actual value) | _ | | | |
| | y Data from USEPA Method 23, including NDs and EMPCs | i | | | |
| mn | Total PCDDs & PCDFs (ng) | 1.3600 | 1.7700 | 1.8600 | |
| m _{n_TEQ} | Total TEQ PCDDs & PCDFs (ng) | 0.0211 | 0.0275 | 0.0305 | |
| _ | D/F Results (TEF=1) | | | | |
| C _{sd} | PCDD/F Concentration (ng/dscm) | 0.31 | 0.37 | 0.40 | 0.36 |
| C _{sd7} | PCDD/F Concentration @7% O ₂ (ng/dscm) | 0.38 | 0.46 | 0.53 | 0.46 |
| E _{lb/hr} | PCDD/F Rate (lb/hr) | 1.24E-07 | 1.57E-0 7 | 1.63 E -07 | 1.48E-07 |
| EFd | PCDD/F Rate - Fd-based (Ib/MMBtu) | 3.43E-10 | 4.14E-10 | 4.72E-10 | 4.10E-10 |
| Total PCD | D/F TEQ Results (using USEPA/INTL 1989 TEFs) | | | | |
| C_{sdTEQ} | TEQ Concentration (ng/dscm) | 0.0048 | 0.0058 | 0.0066 | 0.0057 |
| C_{sd7TEQ} | TEQ Concentration @7% O_2 (ng/dscm) | 0.0059 | 0.0072 | 0.0086 | 0.0072 |
| | TEQ Rate (lb/hr) | 1.92E-09 | 2.44E-09 | 2.68E-09 | 2.35E-09 |
| EFUTEQ | TEQ Rate - F _d -based (lb/MMBtu) | 5.31E-12 | 6.44E-12 | 7.74E-12 | 6.50E-12 |

Client Reference No: CleanAir Project No: 10955-2

| RES | ULTS | a an an an an an an an an an an an an an | | | |
|-------------------|--|--|---------|-----------------|---------------|
| | | le 2-7: | | | |
| | Unit 2 FF Outlet and SD | <u> A Inlet - Hydrog</u> | | | |
| Run N | 0. | 1 | 2 | 3 | Average |
| Date (2 | 2010) | Mar 17 | Mar 17 | Mar 17 | |
| Start Ti | ime (approx.) | 06:54 | 09:02 | 10:25 | |
| Stop Ti | me (approx.) | 07:54 | 10:02 | 11:25 | |
| Proces | ss Conditions | | | | |
| R _P | Steam Production Rate (Klbs/hr) | 184.7 | 184.2 | 184.9 | 1 84.6 |
| P1 | Fabric Filter Inlet Temperature (°F) | 323 | 320 | 319 | 321 |
| SDA In | let Gas Conditions | | | | |
| O ₂ | Oxygen (dry volume %) | 8.4 | 9.3 | 8.7 | 8.8 |
| CO₂ | Carbon dioxide (dry volume %) | 10.9 | 10.2 | 10.7 | 10.6 |
| Τs | Sample temperature (°F) | 510 | 504 | 502 | 505 |
| B, | Actual water vapor in gas (% by volume) | 17.5 | 16.3 | 17.6 | 17.1 |
| SDA In | let Sampling Data | | | | |
| V _{mstd} | Volume metered, standard (dscf) | 35.88 | 36.43 | 36.20 | 36.17 |
| SDA In | let Laboratory Data | | | | |
| m'n | Total HCI collected (mg) | 680.971 | 649.597 | 646.92 7 | |
| SDA In | let Hydrogen Chloride (HCI) Results | | | | |
| C_{sd} | HCI Concentration (ppmdv) | 442 | 416 | 417 | 425 |
| C_{sd7} | HCI Concentration @7% O ₂ (ppmdv) | 492 | 498 | 474 | 488 |
| FF Out | let Gas Conditions | | | | |
| O ₂ | Oxygen (dry volume %) | 9.7 | 10.4 | 9.5 | 9.9 |
| CO₂ | Carbon dioxide (dry volume %) | 9.7 | 9.1 | 10.0 | 9.6 |
| Τs | Sample temperature (°F) | 309 | 308 | 307 | 308 |
| Bw | Actual water vapor in gas (% by volume) | 21.1 | 20.3 | 21.5 | 21.0 |
| FF Out | et Sampling Data | | | | |
| V _{mstd} | Volume metered, standard (dscf) | 41.24 | 41.01 | 40.73 | 40.99 |
| FF Out | et Laboratory Data | | | | |
| m _n | Total HCI collected (mg) | 29.747 | 21.278 | 23.228 | |
| FF Out | et Hydrogen Chloride (HCI) Results | | | | |
| C _{sd} | HCI Concentration (ppmdv) | 17 | 12 | 13 | 14 |
| C _{sd7} | HCI Concentration @7% O ₂ (ppmdv) | 21 | 16 | 16 | 18 |
| RE | Reduction Efficiency (% Removal) | 96% | 97% | 97% | 96% |

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WHEELABRATOR NORTH BROWARD, INC. POMPANO BEACH, FL

Client Reference No: CleanAir Project No: 10955-2

2

| RESULTS | | | | |
|--|--------------|--------------|-------------|--------------|
| Table Unit 3 FF Outlet – Particu | | and Mercu | rv. | |
| Run No. | 1 1 | 2 2 | 3 | Average |
| Date (2010) | Mar 17 | Mar 17 | Mar 17 | |
| Start Time (approx.) | 06:50 | 09:26 | 11:59 | |
| Stop Time (approx.) | 09:03 | 11:38 | 14:11 | |
| Process Conditions | | | | |
| R _P Steam Production Rate (Klbs/hr) P1 Fabric Filter Inlet Temperature (°F) | 184.2 | 184.2 | 183.5 | 184.0 |
| · · · · · · · · · · · · · · · · · · · | 315 | 315 | 315 | 315 |
| Gas Conditions O ₂ Oxygen (dry volume %) | 8.7 | 8.3 | 8.7 | 8.6 |
| CO_2 Carbon dioxide (dry volume %) | 10.5 | 0.3 10.9 | 0.7 10.8 | 10.7 |
| T_s Sample temperature (°F) | 303 | 304 | 304 | 304 |
| B _w Actual water vapor in gas (% by volume) | 22.7 | 22.9 | 22.6 | 22.7 |
| Gas Flow Rate | | | | |
| Q _a Volumetric flow rate, actual (acfm) | 174,264 | 186,885 | 184,323 | 181,824 |
| Q _{std} Volumetric flow rate, dry standard (dscfm) | 90,897 | 97,143 | 96,346 | 94,795 |
| Sampling Data | | | | |
| V _{mstd} Volume metered, standard (dscf) | 70.86 | 75.80 | 74.78 | 73.81 |
| %I Isokinetic sampling (%) | 100.4 | 100.5 | 100.0 | 100.3 |
| Laboratory Data | | | | |
| m _n Net matter collected (g) | 0.00115 | 0.00130 | 0.00223 | |
| Filterable Particulate Results | 0.67 | 0.00 | | |
| C_{sd} Particulate Concentration (mg/dscm) C_{sd7} Particulate Concentration @7% O ₂ (mg/dscm) | 0.57 0.65 | 0.60 0.67 | 1.1 1.2 | 0.74 0.84 |
| | 0.05 | 0.07 | 1.2 | 0.04 |
| Mercury Laboratory Data m n Total matter corrected for allowable blanks (µg) | 8.8257 | 8.9307 | 7.6261 | |
| | 0.0207 | 0.5507 | 7.0201 | |
| Mercury Results - Total C₅d Concentration (µg/dscm) | 4.4 | 4.2 | 3.6 | 4.1 |
| C_{sd7} Concentration @7% O ₂ (µg/dscm) | 5.0 | 4.6 | 4.1 | 4.6 |
| Beryllium Laboratory Data | | | | |
| m_n Total matter corrected for allowable blanks (µg) | <0.0500 | <0.0500 | <0.0500 | |
| Beryllium Results - Total | | | | |
| C _{sd} Concentration (mg/dscm) | <0.00002 | <0.00002 | <0.00002 | <0.00002 |
| C_{sd7} Concentration @7% O ₂ (mg/dscm) | <0.00003 | <0.00003 | <0.00003 | <0.00003 |
| Cadmium Laboratory Data | | | | |
| m _n Total matter corrected for allowable blanks (µg) | <0.2000 | <0.2000 | <0.2000 | |
| Cadmium Results - Total | | | | |
| C _{sd} Concentration (mg/dscm) | <0.00010 | < 0.000093 | < 0.000094 | <0.000096 |
| C _{sd7} Concentration @7% O ₂ (mg/dscm) | <0.00011 | <0.00010 | <0.00011 | <0.00011 |
| Lead Laboratory Data | | | | |
| m _n Total matter corrected for allowable blanks (µg) | 0.2760 | 0.2230 | 0.3748 | |
| Lead Results - Total | | | | |
| C_{sd} Concentration (mg/dscm) | 0.00014 | 0.00010 | 0.00018 | 0.00014 |
| C_{sd7} Concentration @7% O_2 (mg/dscm) | 0.00016 | 0.00011 | 0.00020 | 0.00016 |

Client Reference No: CleanAir Project No: 10955-2

RESULTS Table 2-9: **Unit 3 FF Outlet - Fluorides** 2 Run No. 3 Average 1 Date (2010) Mar 16 Mar 16 Mar 16 Start Time (approx.) 11:49 13:33 15:07 Stop Time (approx.) 13:07 14:44 16:16 **Process** Conditions RP Steam Production Rate (Klbs/hr) 183.7 183.9 184.2 183.9 P₁ Fabric Filter Inlet Temperature (°F) 310 310 310 310 **Gas Conditions** 9.9 9.5 Oxygen (dry volume %) 9.7 9.7 02 CO Carbon dioxide (dry volume %) 9.7 10.0 10.0 9.9 Т, Sample temperature (°F) 298 299 299 299 Actual water vapor in gas (% by volume) B, 20.9 21.4 21.6 21.3 Gas Flow Rate Qa Volumetric flow rate, actual (acfm) 173,798 179,576 173,781 175,718 Q_{std} Volumetric flow rate, dry standard (dscfm) 93.705 96,031 92,736 94,158 Sampling Data Volume metered, standard (dscf) 36.4042 36.9891 35.7340 36.3758 V_{mstd} %I Isokinetic sampling (%) 101.6122 100.7446 100.7835 101.0467 Laboratory Data < 0.03589 Total HF collected (mg) < 0.03481 < 0.03261 m'n Hydrogen Fluoride (HF) Results < 0.042 C_{sd} HF Concentration (ppmdv) < 0.040 < 0.039 <0.040 HF Concentration @7% O₂ (ppmdv) < 0.053 C_{sd7} < 0.049 <0.048 <0.050 C_{sd} HF Concentration (mg/dscm) < 0.035 < 0.033 < 0.032 <0.033 C_{sd7} HF Concentration @7% O2 (mg/dscm) <0.044 < 0.041 < 0.040 <0.042 HF Rate (lb/hr) < 0.012 < 0.012 < 0.011 <0.012 E_{lb/hr} HF Rate - Fd-based (lb/MMBtu) < 0.000040 < 0.000037 < 0.000036 < 0.000037 E_{Ed}



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| | | e 2-10: | | | |
|-------------------|--|------------------|-------------|---------|--------|
| | Unit 3 FF Outlet and SDA | A Inlet - Hydrog | en Chloride | | |
| Run No | 0. | 1 | 2 | 3 | Averag |
| Date (2 | 010) | Mar 16 | Mar 16 | Mar 16 | |
| Start Ti | me(approx.) | 07:17 | 09:04 | 10:32 | |
| Stop Ti | me (approx.) | 08:17 | 10:04 | 11:32 | |
| roces | s Conditions | | | | |
| R _P | Steam Production Rate (Klbs/hr) | 184.6 | 184.1 | 184.3 | 184. |
| P1 | Fabric Filter Inlet Temperature (°F) | 310 | 310 | 310 | 31 |
| DA In | let Gas Conditions | | | | |
| O2 | Oxygen (dry volume %) | 8.6 | 8.2 | 8.1 | 8. |
| CO2 | Carbon dioxide (dry volume %) | 10.7 | 11.1 | 11.2 | 11. |
| Ts | Sample temperature (°F) | 503 | 510 | 508 | 50 |
| В" | Actual water vapor in gas (% by volume) | 17.5 | 17.5 | 16.7 | 17.: |
| SDA In | let Sampling Data | | | | |
| V _{mstd} | Volume metered, standard (dscf) | 35.39 | 35.83 | 34.78 | 35.33 |
| SDA In | let Laboratory Data | | | | |
| m'n | Total HCI collected (mg) | 860.248 | 813.798 | 910.786 | |
| SDA In | let Hydrogen Chloride (HCI) Results | | | | |
| C _{ad} | HCI Concentration (ppmdv) | 567 | 529 | 611 | 56 |
| C_{sd7} | HCI Concentration @7% O ₂ (ppmdv) | 640 | 580 | 661 | 627 |
| F Out | let Gas Conditions | | | | |
| O ₂ | Oxygen (dry volume %) | 9.0 | 9.1 | 8.9 | 9.0 |
| CO₂ | Carbon dioxide (dry volume %) | 10.3 | 10.2 | 10.4 | 10.3 |
| T, | Sample temperature (°F) | 299 | 300 | 299 | 300 |
| Bw | Actual water vapor in gas (% by volume) | 20.8 | 21.3 | 21.8 | 21.3 |
| F Out | let Sampling Data | | | | |
| Vrnstd | Volume metered, standard (dscf) | 42.13 | 41.78 | 41.67 | 41.86 |
| F Out | let Laboratory Data | | | | |
| m _n | Total HCl collected (mg) | 26.091 | 32.864 | 23.884 | |
| | let Hydrogen Chloride (HCI) Results | | | | |
| C _{sd} | HCI Concentration (ppmdv) | 14 | 18 | 13 | 15 |
| C _{sd} | HCI Concentration $@7\% O_2$ (ppmdv) | 17 | 22 | 16 | 18 |
| | | | | | |
| RE | Reduction Efficiency (% Removal) | 97% | 96% | 98% | 97% |

Client Reference No: CleanAir Project No: 10955-2

2-11

| RESULTS | | | | |
|------------------------------------|------------------------------------|--------------|--------|---------|
| Units 1.2 a | Table 2-11: nd 3 FF Outlets – O | pacity by CO | MS | |
| Run No. | 1 | 2 | 3 | Average |
| <u>Unit 1</u> | | | | • |
| Date (2010) | Mar 16 | Mar 16 | Mar 16 | |
| Start Time (approx.) | 07:18 | 10:00 | 12:36 | |
| Stop Time (approx.) | 09:30 | 12:06 | 14:42 | |
| Visible Emissions (%) ¹ | | | | |
| Average Opacity | 2 | 2 | 2 | 2 |
| Maximum Reading | 2 | 2 | 2 | 2 |
| Minimum Reading | 2 | 2 | 2 | 2 |
| Unit 2 | | | | |
| Date (2010) | Mar 18 | Mar 18 | Mar 18 | |
| Start Time (approx.) | 07:06 | 09:48 | 12:24 | |
| Stop Time (approx.) | 09:18 | 12:00 | 14:36 | |
| Visible Emissions (%) ¹ | | | | |
| Average Opacity | 0 | 0 | 0 | 0 |
| Maximum Reading | 0 | 0 | 0 | 0 |
| Minimum Reading | 0 | 0 | 0 | 0 |
| Unit 3 | | | | |
| Date (2010) | Mar 17 | Mar 17 | Mar 17 | |
| Start Time (approx.) | 06:48 | 09:24 | 11:54 | |
| Stop Time (approx.) | 09:00 | 11:36 | 14:06 | |
| /isible Emissions (%) ¹ | | | | |
| Average Opacity | 1 | 1 | 3 | 2 |
| Maximum Reading | 2 | 2 | 4 | 3 |
| Minimum Reading | 0 | 0. | 3 | 1 |

¹ Reading obtained from facility's continuous opacity monitoring system (COMS) as provided under 40 CFR 60.11(e) and Title V Conditions A.36(6), A.53 and A.54 and coincide with Method 5/29 test run Manager Courses and Stratter Strat

COLUMN STATES

WHEELABRATOR NORTH BROWARD, INC. POMPANO BEACH, FL

Client Reference No: CleanAir Project No: 10955-2

| | | | | e 2-12: | | |
|---|--|--|--|---|---|-------------------------------|
| | | | | n - Fugitive | | |
| <u>Source</u> Constituent | Date (2009) | | Stop Time (approx.) | Observation Duration (minutes) | Accumulated Emission Duration (seconds) | |
| Ash Conveyor/Doors to Visual Opacity (%) | Baghouse March 12 | 7:22 | 8:32 | 60 | 0 | |
| Ash Unloading/Convey Visual Opacity (%) | <u>or</u> March 12 | 8:43 | 9:54 | 60 | 0 | |
| Rolling Door/Door to Ba Visual Opacity (%) | aghouse March 12 | 11:10 | 12:20 | 60 | 0 | Permit Limit |
| ` | | | Tot | al (% of observa | tion time) = 0 | - < 5% of observation Time |
| | | | | Total (minute | es) = 0 | < 9 minutes |
| | | | | | | |
| | | | | e 2-13: | | |
| | Lime | Silo Fabr | | | ole Emissions | - |
| | Lime S Run No | | | | ole Emissions 1 | - |
| | | | | | | - |
| | Run No. Date (20 | | ic Filter (| | 1 | - |
| | Run No. Date (20 Start Tin | 910) | ic Filter (x.) | | 1 Mar 17 | - |
| | Run No. Date (20 Start Tin Stop Tin <u>Process</u> | 10) ne (appro ne (appro Conditior | <u>ic Filter (</u> x.) x.) <u>1s</u> | <u>Dutlet - Visik</u> | 1 Mar 17 10:26 11:45 | - |
| | Run No. Date (20 Start Tin Stop Tin <u>Process</u> | 10) ne (appro ne (appro Conditior | <u>ic Filter (</u> x.) x.) | <u>Dutlet - Visik</u> | 1 Mar 17 10:26 | - |
| | Run No. Date (20 Start Tin Stop Tin <u>Process</u> To | 10) ne (appro ne (appro <u>Conditior</u> tal lime u | <u>ic Filter (</u> x.) x.) <u>1s</u> | <u>Outlet - Visik</u> ons) | 1 Mar 17 10:26 11:45 | - |
| | Run No. Date (20 Start Tin Stop Tin <u>Process</u> To Ra <u>Visible E</u> | 110) ne (appro ne (appro <u>Conditior</u> tal lime un tal lime un te of unlo | <u>ic Filter (</u> x.) x.) nloaded (t ading (tor | <u>Outlet - Visik</u> ons) ns/hr) | 1 Mar 17 10:26 11:45 25.36 | - |
| | Run No. Date (20 Start Tin Stop Tin <u>Process</u> To Ra <u>Visible E</u> | 110) ne (appro ne (appro <u>Conditior</u> tal lime un tal lime un te of unlo | <u>ic Filter (</u> x.) x.) nloaded (t | <u>Outlet - Visik</u> ons) ns/hr) | 1 Mar 17 10:26 11:45 25.36 | _ |

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| | | | | Ta | ble 2-14 | l: | | | | | |
|-------------|-----------|-------------|----------------------------|---------------------------|------------------|------------------|-------------------|-----------------------------------|-----------------------|--------------------|---|
| | | | | Air Flo | ow Sum | mary | | | | | |
| Run Number | Run Date | Run Time | Steam Flow Klbs/hour | Flue Gas Temp Deg F | Air Flow ACFM | O ₂ % | CO ₂ % | CO ₂ Sample Rate | Stack Flow 2RSD | Air Flow, DSCFM | Air Flow, DSCFM@ 7%O ₂ |
| | | | Ribarriour | Dog. | | | | (ipm) ¹ | (%) | | 17002 |
| 1-0-M5/29-1 | 3/16/2010 | 07:21-09:32 | 183.9 | 293 | 191,586 | 9.5 | 9,9 | 0.2 | 11.6% | 105.082 | 85.956 |
| 1-O-M5/29-2 | 3/16/2010 | 10:00-12:14 | 184.4 | 295 | 191,421 | 9.5 | 9.9 | 0.2 | 12.2% | 104,870 | 86,310 |
| 1-O-M5/29-3 | 3/16/2010 | 12:36-14:47 | 183.4 | 301 | 193,814 | 9.7 | 9.8 | 0.2 | 15.3% | 105,806 | 84,949 |
| 1-0-M13B-1 | 3/17/2010 | 11:46-12:56 | 184.0 | 303 | 205,926 | 10.6 | 9.1 | 0.4 | 12.1% | 111,627 | 83,118 |
| 1-0-M13B-2 | 3/17/2010 | 13:15-14:27 | 1 <u>84</u> .0 | 302 | 207,433 | 10.1 | 9.6 | 0.4 | 12.9% | 111.678 | 86,530 |
| 1-O-M13B-3 | 3/17/2010 | 14:45-15:53 | 184.1 | 303 | 198,952 | 10.0 | 9.8 | 0.4 | 11.0% | 106,345 | 83,699 |
| | | Average | | 299 | _ 198,189] | 9.9 | 97 | NA < | 12.5% | 107.568 | 85.094 |
| 2-O-M5/29-1 | 3/18/2010 | 07:09-09:22 | 183.9 | 307 | 201,928 | 10.1 | 9.3 | 0.2 | 13.9% | 108,134 | 84.251 |
| 2-O-M5/29-2 | 3/18/2010 | 9:49-12:02 | 182.9 | 308 | 193,105 | 9.8 | 9.6 | 0.2 | 10.0% | 103.333 | 82,890 |
| 2-O-M5/29-3 | 3/18/2010 | 12:27-14:39 | 183.9 | 308 | 199,217 | 9.9 | 9.6 | 0.2 | 16.8% | 105,806 | 83,856 |
| 2-0-M13B-1 | 3/18/2010 | 07:09-08:24 | 183.9 | 306 | 190,226 | 10.0 | 9.3 | 0.4 | 14.3% | 101.644 | 79,560 |
| 2-0-M13B-2 | 3/18/2010 | 08:56-10:10 | 184.2 | 305 | 182,805 | 9.6 | 9.6 | 0.4 | 10.0% | 97,309 | 78,827 |
| 2-O-M13B-3 | 3/18/2010 | 10:45-12:05 | 183.0 | 306 | 185,088 | 10.2 | 9.1 | 0.4 | 13.4% | 99,545 | 76,986 |
| 2-O-M23-1 | 3/16/2010 | 0B:44-13:36 | 184.1 | 301 | 198,967 | 9.7 | 9.7 | 0.1 | 8.7% | 107,335 | 86,640 |
| 2-O-M23-2 | 3/17/2010 | 06:54-12:19 | 184.3 | 307 | 214,211 | 9.7 | 9.8 | 0.1 | 7.0% | 113,400 | 91,046 |
| 2-O-M23-3 | | 12:53-17:26 | 183.9 | 308 | 203,730 | 10.3 | 9.5 | 0.1 | 8.8% | 108.891 | 82,961 |
| | | Average | 183.8 | 306 | 196,586 | 9.9 | 9.5 | | 11.4% | _105,044 | 83.002 |
| 3-0-M5/29-1 | | 06:50-09:03 | 184.2 | 303 | 174,264 | 8.7 | 10.5 | 0.2 | 16.1% | 90,897 | 79,715 |
| 3-O-M5/29-2 | | 09:26-11:38 | 184.2 | 304 | 186,885 | 8.3 | 10.9 | 0.2 | 9.4% | 97,143 | 88.057 |
| 3-O-M5/29-3 | | 11:59-14:11 | 183.5 | 304 | 184.323 | 8.7 | 10.8 | 0.2 | 12.1% | 105,806 | 84,424 |
| 3-O-M13B-1 | | 11:49-13:07 | 183.7 | 298 | 173,798 | 9.9 | 9.7 | 0.4 | 8.5% | 101,644 | 74,155 |
| 3-O-M13B-2 | | 13:33-14:44 | 183.9 | 299 | 179,576 | 9.5 | 10.0 | 0.4 | 11.4% | 96.031 | 78,552 |
| 3-O-M13B-3 | | 15:07-16:16 | 184.2 | 299 | 173,781 | 9.7 | 10.0 | 0.4 | 11.0% | 92,736 | 74,589 |
| <u></u> | 0.10.2010 | Average | 184.0 | 301 | 178.771 | 9.1 | 10.3 | NA | 11.4% | 97,376 | 79,915 |

 1 COz gas sample flow rate was within 10% of initial flow rate throughout all test runs.

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| Table 2-15: | | | | | | | | |
|------------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|--|
| Q | uality C | ontrol a | nd Qual | ity Assu | Irance | | | |
| PCDD/PC | DF - Ext | raction | Standar | d Perce | nt Reco | veries | | |
| | | Extrac | tion Stand | ard Perce | nt Recove | ries, % | | |
| Sample Number | ¹³ C- | ¹³ C- | ¹³ C- | ¹³ C- | ¹³ C- | ¹³ C- | ¹³ C- | |
| | TCDD | PeCDD | HxCDD | HxCDD | HxCDD | HpCDD | OCDD | |
| | | | | | | | | |
| 0_7679_MB001 | 88.6 | 88.9 | 91.1 | 92.8 | 94.1 | 91.2 | 89.2 | |
| Field Blank | 86.3 | 89.5 | 90.9 | 96.6 | 94.6 | 92.4 | 91.7 | |
| Unit 2 FF Outlet Run 1 | 83.1 | 88.6 | 82.5 | 86.2 | 82.9 | 85.3 | 84.7 | |
| Unit 2 FF Outlet Run 2 | 86.3 | 82.9 | 82.1 | 84.3 | 84.4 | 84.1 | 82.8 | |
| Unit 2 FF Outlet Run 3 | 85.6 | 82.5 | 80 | 85.5 | 86 | 82.8 | 81.9 | |
| Reagent Blank | 94.3 | 97.8 | 97.3 | 98.7 | 100 | 96.9 | 92.6 | |
| | | | | | | | | |
| Average | 87 | 88 | 87 | 91 | 90 | 89 | 87 | |
| SD | 4 | 6 | 7 | 6 | 7 | 6 | 5 | |
| Min | 83.1 | 82.5 | 80 | 84.3 | 82.9 | 82.8 | 81.9 | |
| Max | 94.3 | 97.8 | 97.3 | 98.7 | 100 | 96.9 | 92.6 | |
| Within M23 QC | TRUE | |

| | | | E | xtraction S | Standard P | ercent Re | coveries, ' | | | |
|------------------------|------|-------|-------|-------------|------------|-----------|-------------|-------|-------|------|
| Sample Number | | -0°C- | '°C- | -1°C- | -3°' | "°C- | -3°' | -3°C- | -3°- | |
| | TCDF | PeCDF | PeCDF | HxCDF | HxCDF | HxCDF | HxCDF | HpCDF | HpCDF | OCDF |
| | | | | | | | | | | |
| 0_7679_MB001 | 89.1 | 91.1 | 91.7 | 95.6 | 94.2 | 92.9 | 83.4 | 89.9 | 86.2 | 86.9 |
| Field Blank | 88.6 | 92.4 | 93.6 | 94.2 | 92.7 | 91.2 | 83.1 | 91.2 | 88.6 | 89.9 |
| Unit 2 FF Outlet Run 1 | 84.6 | 89.3 | 92.7 | 86.9 | 84.3 | 82.6 | 78.4 | 82.9 | 82.6 | 84.2 |
| Unit 2 FF Outlet Run 2 | 88.6 | 85.4 | 85.2 | 84.3 | 82.7 | 84.9 | 77.9 | 79.7 | 81.6 | 80.2 |
| Unit 2 FF Outlet Run 3 | 87.7 | 87.3 | 85.3 | 81.6 | 81.9 | 83.6 | 77.3 | 79.1 | 80 | 79.4 |
| Reagent Blank | 95.4 | 97.3 | 97.3 | 99.9 | 98 | 98.2 | 91.1 | 95.9 | 92.7 | 91 |
| | | | | | | | | | | |
| Average | 89 | 90 | 91 | 90 | 89 | 89 | 82 | 86 | 85 | 85 |
| SD | 4 | 4 | 5 | 7 | 7 | 6 | 5 | 7 | 5 | 5 |
| Min | 84.6 | 85.4 | 85.2 | 81.6 | 81.9 | 82.6 | 77.3 | 79.1 | 80 | 79.4 |
| Max | 95.4 | 97.3 | 97.3 | 99.9 | 98 | 98.2 | 91.1 | 95.9 | 92.7 | 91 |
| Within M23 QC | TRUE | TRUE | TRUE | TRUE | TRUE | TRUE | TRUE | TRUE | TRUE | TRUE |

Table 2-16: Quality Control and Quality Assurance PCDD/PCDF – CS/SS Percent Recoveries

| | | | | Overica | |
|------------------------|-------------------|------------------|------------------|------------------|------------------|
| | | CS/SS Pe | rœnt Rea | ovenies,% | |
| Sample Number | ³⁷ Cl- | ¹³ C- | ¹³ C- | ¹³ C- | ¹³ C- |
| | TCDD | PeCDD | PeCDF | HxCDF | HpCDF |
| | | | | | |
| 0_7679_MB001 | 98.5 | 101 | 94.8 | 98.9 | 100 |
| Field Blank | 98.1 | 97.9 | 90.9 | 97.6 | 98 |
| Unit 2 FF Outlet Run 1 | 98.1 | 98.3 | 97.8 | 101 | 103 |
| Unit 2 FF Outlet Run 2 | 98.4 | 101 | 100 | 101 | 98.7 |
| Unit 2 FF Outlet Run 3 | 96.1 | 99.1 | 93 | 100 | 102 |
| Reagent Blank | | | | | |
| | | | | | |
| Average | 98 | 99 | 95 | 100 | 100 |
| SD | 30 | 35 | 95 | 100 | 2 |
| Min | 96.1 | 97.9 | 90.9 | 97.6 | 2 98 |
| win | 90.1 | 97.9 | 90.9 | 97.0 | 90 |

101

TRUE

100

98.5

TRUE

103

TRUE

101

TRUE TRUE

| 2-1 | 4 |
|-----|---|
| | |

Max

Min within M23 QC

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| Table 2-17: Quality Control and Quality Assurance - Metals | | | | | | | | |
|---|-------------|------------|------------|------------|-----|--|--|--|
| | Quality Col | RPD RES | | wethis | | | | |
| Mercury | FH | BH | Α | В | с | | | |
| • | | | Empty | | | | | |
| Run Number | Front Half | H₂O₂/HNO₄ | Impinger | KMnO₄ | НСІ | | | |
| U1 FF Outlet R1 | NA | 0.8% | NA | NA | NA | | | |
| U1 FF Outlet R2 | NA | 2.5% | NA | NA | NA | | | |
| U1 FF Outlet R3 | NA | 0.3% | NA | · NA | NA | | | |
| U2 FF Outlet R1 | NA | 1.2% | NA | NA | NA | | | |
| U2 FF Outlet R2 | NA | 0.1% | NA | NA | NA | | | |
| U2 FF Outlet R3 | NA | 0.6% | NA | NA | NA | | | |
| U3 FF Outlet R1 | NA | 0.6% | NA | NA | NA | | | |
| U3 FF Outlet R2 | NA | 0.8% | NA | NA | NA | | | |
| U3 FF Outlet R3 | NA | 0.5% | NA | NA | NA | | | |
| Field Blank | NA | NA | NA | NA | NA | | | |
| Reagent Blank | NA | NA | NA | NA | NA | | | |
| 3/17 Reagent Blank | NA | NA | NA | NA | NA | | | |
| 3/18 Reagent Blank | NA | NA | NA | NA | NA | | | |
| | | U1-FF-O-R2 | U2-FF-O-R2 | U3-FF-O-R2 | | | | |
| | Element | RPD | RPD | RPD | | | | |
| | Beryllium | NA | NA | NA | | | | |
| | Cadmium | 1.3% | NA | NA | | | | |
| | Lead | 0.1% | 3.1% | 6.8% | | | | |

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| | | Sample | Spike and Re | ecoverv | | |
|-----------------|--------|-------------|----------------|--------------|------------|----------|
| Mercury | | FH | BH | A | В | С |
| | | | | Empty | | |
| Run Number | | Front half | H_2O_2/HNO_4 | Impinger | KMnO₄ | HCI |
| U1 FF Outlet R3 | #1 | 102% | 98% | 93% | 106% | 102% |
| | #2 | 102% | 96% | 94% | 106% | 102% |
| U2 FF Outlet R3 | #1 | 102% | 99% | 103% | 88% | 101% |
| | #2 | 102% | 98% | 102% | 86% | 99% |
| U3 FF Outlet R3 | #1 | 103% | 94% | 103% | 89% | 96% |
| | #2 | 103% | 92% | 96% | 91% | 95% |
| | | | U1-FF-O-R3 | U2-FF-O-R3 | U3-FF-O-R3 | |
| | | Element | Recovery | Recovery | Recovery | |
| | | Beryllium | 85% | 85% | 87% | |
| | | Cadmium | 86% | 87% | 88% | |
| | | Lead | 97% | 100% | 102% | |
| | | Second Sour | ce Calibration | Verification | | |
| Element | | .25 ppb | 1 ppb | 50 ppb | 100 ppb | 250 ppb |
| | | QC Std 8 | QC Std 2 | QC Std 5 | QC Std 4 | QC Std 3 |
| Beryllium | | 98% | 97% | 98% | 101% | 97% |
| Cadmium | | | 97% | 95% | 99% | 94% |
| | | | | | | |

92%

97%

100%

94%

Lead

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| | | | | e 2-19: | | | |
|--------------------|----------------|---------------------------|------------|---|-------------------------|----------------|----------|
| يوا | uanty | Control and | Guanty Ass | Urance - IVI BH | | I Field Blanks | |
| Method 29 | | Average Total Catch ug | Front half | H ₂ O ₂ /HNO ₄ | A Empty Impinger | B KMnO₄ | C HCI |
| Field Blank | #1 | < 0.5 | < 0.1 | < 0.3 | < 0.2 | < 0.5 | < 0.4 |
| | #2 | | < 0.1 | < 0.3 | < 0.2 | < 0.5 | < 0.4 |
| Reagent Blank | #1 | < 0.5 | < 0.1 | < 0.2 | < 0.2 | < 0.5 | < 0.4 |
| | #2 | | < 0.1 | < 0.2 | < 0.2 | < 0.5 | < 0.4 |
| 3/17 Reagent Blan | | < 0.5 | NA | NA | NA | < 0.5 | NA |
| 3/18 Reagent Blan | #2 k #1 | < 0.5 | NA NA | NA NA | NA NA | < 0.5 | NA |
| of to Reagent Dian | * #1 #2 | < 0.5 | NA | NA | NA | < 0.5 < 0.5 | NA NA |
| | | | Element | Field Blank Total µg | Reagent Bla Total µg | ınk | |
| | | | | 14211-10 | 14211-11 | - | |
| | | | Beryllium | < 0.05 | < 0.05 | | |
| | | | Cadmium | < 0.2 | < 0.2 | | |
| | | | Lead | 0.290 | 0.454 | | |
| Me | thod 2 | 3 | | 0_7679 | 9_MB001 | Field Blank | |
| | | | | | pg | pg | |
| 2.2 | 7,8-TCD | D | | (1 | .46) | (1.39) | |
| | 3,7,8-Pe | | | | .79) | (1.82) | |
| | 3,4,7,8-H | | | | | | |
| | | | | · · · | 2.66) | (1.83) | |
| | 8,6,7,8-H | | | | .48) | (1.93) | |
| J | 3,7,8,9-H | | | | 79) | (2.08) 4.71 | |
| 1,2,0 OCE | | -HpCDD | | | 4.1 | 4.71 | |
| | | _ | | | | | |
| | ,8-TCDI | | | | .07) | (0.973) | |
| | ,7,8-Pe | | | | .09) | (1.07) | |
| | ,7,8-Pe | | | | .03) | (1.02) | |
| | ,4,7,8-H | | | | .78) | (1.44) | |
| 1 | 6,7,8-H | | | | .66) | (1.36) | |
| | ,6,7,8-H | | | | .78) | (1.44) | |
| 1 | ,7,8,9-H | | | | .42) | (1.93) | |
| | ,4,6,7,8- | - | | | .69) | 3.19 | |
| | ,4,7,8,9- - | HPCDF | | · · | .53) | (2.05) | |
| | | | | | .41) | 6.16 | |
| | • | D=0; EMPC=0) | | |)141 | 0.0999 | |
| • | • | D=0; EMPC=EMF | , | J | 0141 | 0.0999 | |
| | • | D=DL/2; EMPC=0 | | | .34 | 2.19 | |
| [ITEF | TEQ (N | D=DL/2; EMPC=E | EMPC) | 2. | .34 | 2.19 | |
| | | D=DL; EMPC=EN | (PC) | 4 | 67 | 4.28 | |

Client Reference No: CleanAir Project No: 10955-2

2-18



| RESULTS | | | |
|---------|---|------------------------|-----------------|
| | Quality Control and Quality | e 2-20: V Assurance | - Miscellaneous |
| | Blanks | Result | misochanebus |
| | Acetone (g) | 0.0008 | |
| | HCI DI H ₂ O (mg/l) | <0.077 | |
| | HCI 0.1 N H ₂ SO ₄ (mg/l) | <0.077 | |
| | HF DI H ₂ O (mg/l) | <0.038 | |
| | Meters - Post Cal | Result | Limit |
| | 61-6 | -0.6% | ≤ ± 5% |
| | 61-8 | -0.4% | ≤ ± 5% |
| | 61-11 | -0.6% | ≤ ± 5% |
| | 66-6 | -0.4% | ≤ ± 5% |
| | 66-14 | 0.3% | ≤±5% |
| | 66-24 | -0.4% | ≤ ± 5% |
| | 85-2 | 1.2% | ≤ ± 5% |
| | 85-4 | -0.2% | ≤ ± 5% |

End of Section 2 – Results

DESCRIPTION OF INSTALLATION

PROCESS DESCRIPTION

The North Broward Resource Recovery facility operates three (3) 750-tons-per-day municipal refuse-fired, water-wall boiler trains. The trains were manufactured by Babcock and Wilcox to produce electricity for sale to a local utility company. The boilers are rated at a maximum steam flow of 186,000 lbs/hr. Each boiler is equipped with an SDA for acid gas removal, followed by an FF baghouse for the control of particulate emissions and selective non-catalytic reduction for nitrogen oxide (NO_X) control. The control equipment is manufactured by Wheelabrator Air Pollution Control, Inc. Each FF baghouse is followed by an induced draft fan that directs the flue gas to a dedicated flue in a common stack.

Figure 3-1 shows a general schematic of the facility. The general sampling locations for the Units 1, 2 and 3 SDA Inlets and FF Outlets are shown in Figure 3-2 on page 3-2.

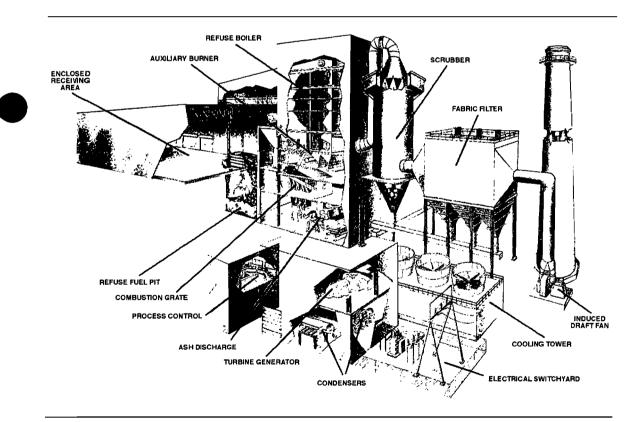
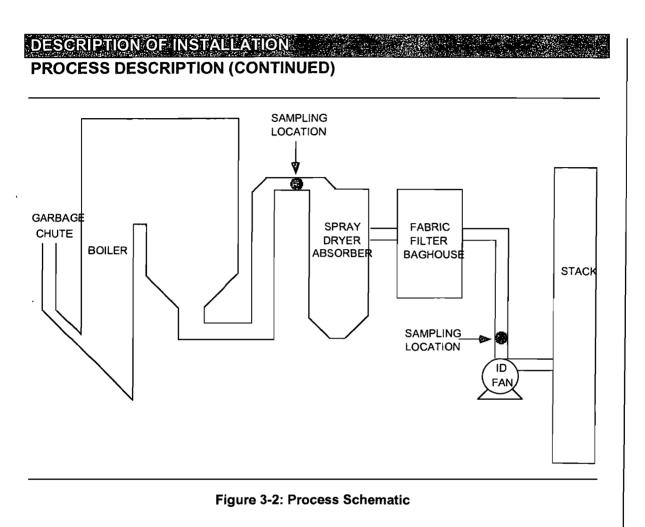


Figure 3-1: General Process Schematic

Clean Air Project No: 10955-2

Clean Air Project No: 10955-2

3-2



Revision 0, Final

DESCRIPTION OF INSTALLATION

PROCESS DESCRIPTION (CONTINUED)

4

| | | | | | | | | | Table 3 | | - | | | | | | |
|----------|----------|-----|-----------|-------|-------|---------|----------|-----------------------|---------|-------|---------|--------|--------|----------|------------|--------|--------------------|
| PLANT NA | | | | | | | | Complia ta from DC | | | ocess | | ulated | 1.1- | ne Feed Ra | -4- | 1 |
| 2010 | WE: NO | | KU WARD | | | | | Fabric | SDA | Total | Diluton | Calci | llated | L)r | Slurry | ite | |
| | | | | | _ | Steam | FF Inlet | Filter | inlet | SDA | H2O | Slurry | Slurry | Slurry | CaO | CaO | |
| | Unit | Run | | Ti | me | Flow | Temp | Delta | Temp | Flow | flow | Flow | Conc. | Specific | Density | Flow | |
| Test | No. | No. | Date | Start | Stop | klbs/hr | deg F | In. H2O | deg F | gpm | gpm | gpm | % | Gravity | lb/gal | lbs/hr | Test Run Comments |
| M-26A | 1 | 1 | 3/18/2010 | 07:02 | 08:02 | 183.5 | 320.2 | 6.6 | 510.8 | 38.0 | 30.1 | 7.9 | 13.5 | 1.129 | 1.357 | 641.6 | |
| нсі | 1 | 2 | 3/18/2010 | 09:26 | 10:37 | 184.1 | 320.4 | 5.3 | 510.8 | 37.8 | 28.5 | 9.4 | 15.2 | 1.129 | 1.363 | 765.5 | All times based on |
| | | 3 | 3/18/2010 | 11:49 | 12:49 | 182.8 | 320.1 | 6.4 | 520.1 | 40.7 | 29.9 | 10.8 | 14.2 | 1.129 | 1.357 | 880.2 | CEMS time |
| | | | | | Avg | 183.4 | 320.2 | 6.1 | 513.9 | 38.8 | 29.5 | 9.4 | 14.3 | 1.129 | 1.359 | 762.4 | |
| | | | | | | | | | | | _ | | | | | | |
| M-29/5 | 1 | 1 | 3/16/2010 | 07:21 | 09:32 | 183.9 | 310.4 | 6.3 | 521.3 | 39.2 | 29.5 | 9.8 | 14.9 | 1.104 | 1.095 | 640.6 | |
| Metals | | 2 | 3/16/2010 | 10:00 | 12:11 | 184.4 | 312.5 | 6.1 | 524.0 | 39.3 | 28.8 | 10.5 | 15.1 | 1.101 | 1.061 | 671.0 | All times based on |
| РМ | | 3 | 3/16/2010 | 12:36 | 14:47 | 183.4 | 320.2 | 6.3 | 529.0 | 40.0 | 32.9 | 7.2 | 14.5 | 1.104 | 1.091 | 468.0 | CEMS time |
| | | | | | Avg | 183.9 | 314.4 | 6.2 | 524.8 | 39.5 | 30.4 | 9.1 | 14.8 | 1.103 | 1.082 | 593.2 | |
| | | | | | | | | | | | | | | | | | |
| M-13B | 1 | 1 | 3/17/2010 | 11:46 | 12:56 | 184.0 | 320.1 | 6.4 | 543.7 | 47.4 | 42.5 | 4.9 | 11.2 | 1.117 | 1.232 | 362.2 | |
| HF | | 2 | 3/17/2010 | 13:15 | 14:27 | 184.0 | 319.9 | 6.4 | 541.6 | 46.7 | 41.0 | 5.7 | 11.3 | 1.116 | 1.228 | 416.3 | All times based on |
| l | \ | 3 | 3/17/2010 | 14:45 | 15:53 | 184.1 | 319.8 | 6.3 | 539.4 | 45.2 | 39.4 | 5.8 | 11.7 | 1.117 | 1.230 | 425.1 | CEMS time |
| | | | | | Avg | 184.0 | 319.9 | 6.4 | 541.6 | 46.4 | 41.0 | 5.4 | 11.4 | 1.117 | 1.230 | 401.2 |] |

DESCRIPTION OF INSTALLATION

PROCESS DESCRIPTION (CONTINUED)

| | | | | | | | Unit 2 | Compl | Table | | ncess | Data | | | | | |
|-----------|--------|--------|-----------|-------|-------|---------|----------|-----------|-------|-------|---------|--------|--------|----------|-----------|--------|--------------------|
| PLANT NAM | NE: NO | RTH BR | ROWARD | | | | | ta From D | | | 00033 | | lated | Lin | ne Feed R | ate | |
| 2010 | | | | | | | | Fabric | SDA | Total | Diluton | | | | Slurry | | |
| | | | | | | Steam | FF inlet | Filter | Inlet | SDA | H2O | Slurry | Slurry | Slurry | CaO | CaO | |
| | Unit | Run | | Tì | me | Flow | Temp | Delta | Temp | Flow | flow | Flow | Conc. | Specific | Density | Flow | |
| Test | No. | No. | Date | Start | Stop | klbs/hr | deg F | In. H2O | deg F | gpm | gpm | gpm | % | Grav ity | lb/gai | lbs/hr | Test Run Comments |
| M-26A | 2 | 1 | 3/17/2010 | 06:54 | 07:54 | 184.7 | 323.0 | 6.1 | 518.1 | 38.0 | 31.0 | 7.0 | 14.9 | 1.109 | 1.136 | 474.4 | |
| HCI | | 2 | 3/17/2010 | 09:02 | 10:02 | 184.2 | 319.5 | 6.2 | 512.2 | 41.2 | 35.7 | 5.5 | 13.6 | 1.113 | 1.184 | 388.6 | All times based on |
| | | 3 | 3/17/2010 | 10:25 | 11:25 | 184.9 | 319.4 | 6.1 | 509.6 | 38.2 | 34.8 | 3.4 | 14.1 | 1.117 | 1.229 | 249.2 | CEMS time |
| | | | | | Avg | 184.6 | 320.6 | 6.1 | 513.3 | 39.1 | 33.9 | 5.3 | 14.2 | 1.1 13 | 1.183 | 370.7 | |
| | | | | | | | | | | | | | | | | | |
| M-29/5 | 2 | 1 | 3/18/2010 | 07:09 | 09:22 | 183.9 | 320.0 | 5.2 | 515.0 | 39.3 | 33.2 | 6.1 | 12.3 | 1.128 | 1.354 | 493.1 | |
| Metals | | 2 | 3/18/2010 | 09:49 | 12:02 | 182.9 | 320.2 | 5.4 | 515.2 | 38.6 | 32.8 | 5.9 | 12.4 | 1.129 | 1.361 | 481.0 | All times based on |
| PM | | 3 | 3/18/2010 | 12:27 | 14:39 | 183.9 | 320.6 | 6.3 | 520.2 | 41.4 | 34.3 | 7.1 | 11.7 | 1.128 | 1.354 | 579.2 | CEMS time |
| | | | | | Avg | 183.6 | 320.3 | 5.6 | 516.8 | 39.8 | 33.4 | 6.4 | 12.1 | 1.128 | 1.356 | 517.8 | |
| | | | | | | | | | | | | | | | | | |
| M-23 | 2 | 1 | 3/16/2010 | 08:44 | 13:36 | 184.1 | 314.2 | 6.1 | 505.6 | 37.6 | 30.0 | 7.6 | 15.8 | 1.101 | 1.063 | 487.3 | |
| dioxins | | 2 | 3/17/2010 | 06:54 | 12:19 | 184.3 | 321.2 | 6.1 | 513.8 | 39.3 | 34.0 | 5.4 | 14.3 | 1.113 | 1.184 | 380.1 | All times based on |
| | | 3 | 3/17/2010 | 12:53 | 17:26 | 183.9 | 320.3 | 6.1 | 523.4 | 43.1 | 39.3 | 3.9 | 12.3 | 1.117 | 1.231 | 285.1 | CEMS time |
| | | | | | Avg | 184.1 | 318.6 | 6.1 | 514.2 | 40.0 | 34.4 | 5.6 | 14.2 | 1.110 | 1.159 | 384.1 | 1 |
| | | | | | | | - | | | | | | | | | | |
| M-13B | 2 | 1 | 3/18/2010 | 07:09 | 08:24 | 183.9 | 320.6 | 5.9 | 514.0 | 39.3 | 32.8 | 6.5 | 12.3 | 1.1 29 | 1.357 | 530.0 | |
| HF | | 2 | 3/18/2010 | 08:56 | 10:10 | 184.2 | 319.6 | 3.4 | 512.5 | 37.4 | 31.9 | 5.5 | 12.8 | 1.129 | 1.359 | 448.5 | All times based on |
| | | 3 | 3/18/2010 | 10:45 | 12:05 | 183.0 | 319.9 | 6.0 | 514.7 | 38.4 | 32.1 | 6.3 | 12.5 | 1.129 | 1.360 | 512.4 | CEMS time |
| | | | | | Avg | 183.7 | 320.0 | 5.1 | 513.8 | 38.3 | 32.2 | 6.1 | 12.5 | 1.129 | 1.359 | 497.0 | 1 |

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CleanAir Project No: 10955-2

CleanAir

DESCRIPTION OF INSTALLATION

PROCESS DESCRIPTION (CONTINUED)

| <u> </u> | | | | | | | Unit 3 | Complia | ance T | est Pr | ocess | Data | | | | | |
|---------------------------|------|-----|-----------|-------|-------|-------------------------|----------|------------------|-------------------|--------------|----------------|--------|----------------|----------|---------------|--------|--------------------|
| PLANT NAME: NORTH BROWARD | | | | | | Data From DCS Printouts | | | | | Calcu | lated | Lime Feed Rate | | | | |
| 2010 | | | | | | Steam | FF Inlet | Fabric Filter | SDA Iniet | Total SDA | Diluton H2O | Siurry | Slurry | Slurry | Slurry CaO | CaO | |
| | Unit | Run | | Ti | me | Flow | Temp | Deita | Temp | Flow | flow | Flow | Conc. | Specific | Density | Flow | |
| Test | No. | No. | Date | Start | Stop | klbs/hr | deg F | In. H2O | deg F | gpm | gpm | gpm | % | Gravity | lb/gal | lbs/hr | Test Run Comments |
| M-26A | 3 | 1 | 3/16/2010 | 07:17 | 08:17 | 184.6 | 309.9 | 6.3 | 507.3 | 35.8 | 26.2 | 9.7 | 16.1 | 1.113 | 1.183 | 685.0 | |
| HCI | 1 | 2 | 3/16/2010 | 09:04 | 10:04 | 184.1 | 310.1 | 6.3 | 514.4 | 37.4 | 24.2 | 13.3 | 19.1 | 1.100 | 1.051 | 837.4 | All times based on |
| | | 3 | 3/16/2010 | 10:32 | 11:32 | 184.3 | 309.9 | 6.4 | 513.4 | 37.5 | 27.0 | 10.5 | 18.6 | 1.101 | 1.059 | 667.2 | CEMS time |
| | | | | | Avg | 184.3 | 310.0 | 6.3 | 511.7 | 36.9 | 25.8 | 11.1 | 17.9 | 1.105 | 1.098 | 729.9 | |
| | | | | | | | | | | | _ | | | | | | |
| M-29/5 | 3 | 1 | 3/17/2010 | 06:50 | 09:03 | 184.2 | 315.0 | 6.4 | 518. 9 | 37.8 | 33.4 | 4.5 | 14.8 | 1.109 | 1.142 | 304,9 | |
| Metals | | 2 | 3/17/2010 | 09:26 | 11:38 | 184.2 | 314.9 | 6.4 | 518.1 | 37.8 | 33.6 | 4.2 | 14.4 | 1.115 | 1.214 | 303.7 | All times based on |
| PM | | 3 | 3/17/2010 | 11:59 | 14:11 | 183.5 | 315.2 | 6.4 | 521.6 | 38.7 | 34.7 | 4.0 | 13.7 | 1.117 | 1.230 | 295.2 | CEMS time |
| | | | | | Avg | 184.0 | 315.0 | 6.4 | 519.5 | 38.1 | 33.9 | 4.2 | 14.3 | 1.114 | 1.195 | 301.3 | |
| | | | | | | | | | _ | | | | | _ | | | |
| M-13B | 3 | 1 | 3/16/2010 | 11:49 | 13:07 | 183.7 | 310.2 | 6.5 | 517.3 | 38.8 | 28.2 | 10.6 | 15.1 | 1.102 | 1.074 | 684.4 | |
| HF | | 2 | 3/16/2010 | 13:33 | 14:44 | 183.9 | 309.6 | 6.4 | 523.8 | 41.3 | 36.1 | 5.2 | 14.0 | 1.105 | 1.098 | 339.3 | All times based on |
| | | 3 | 3/16/2010 | 15:07 | 16:16 | 184.2 | 309.8 | 6.3 | 518.2 | 38.9 | 34.5 | 4.4 | 14.7 | 1.106 | 1.113 | 293.8 | CEMS time |
| | | | | | Avg | 184.0 | 309.9 | 6.4 | 519.7 | 39.7 | 32.9 | 6.7 | 14.6 | 1.104 | 1.095 | 439.2 |] |

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CleanAir Project No: 10955-2

Client Reference No: CleanAir Project No: 10955-2

3-6

DESCRIPTION OF INSTALLATION

DESCRIPTION OF SAMPLING LOCATIONS

Sampling point locations were determined according to EPA Method 1.

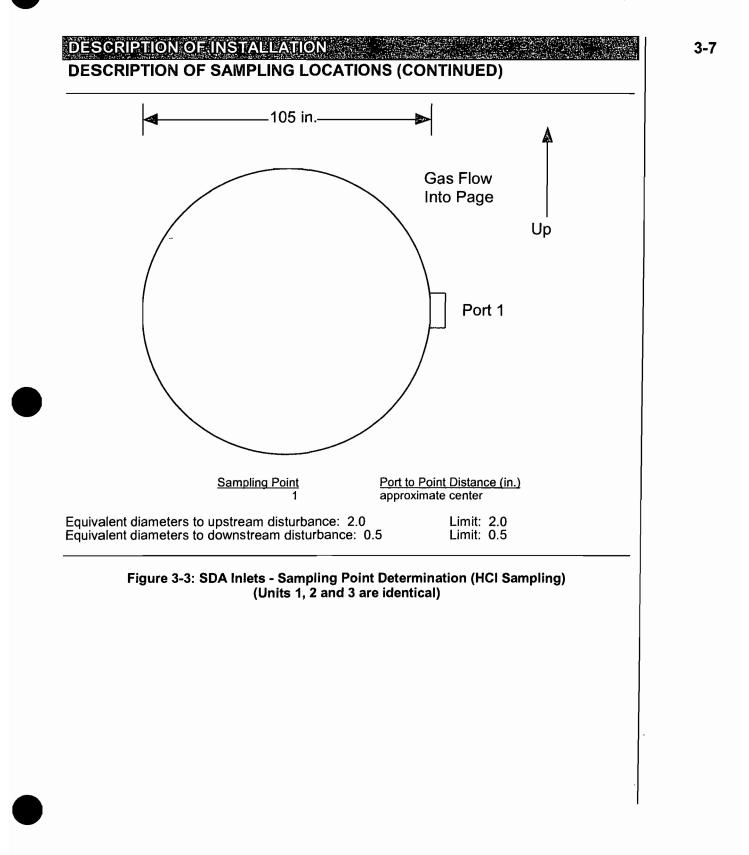
Table 3-4 outlines the sampling point configurations. Figures 3-3 and 3-4 (on pages 3-7 and 3-8) illustrate the sampling points and orientation of sampling ports for each of the sources that were tested in the program.

| | Table 3-4: Sampling Points | | | | | | | | | | | |
|--------------------------------|------------------------------------|------------|-------|----------------------|---------|------------------|--------|--|--|--|--|--|
| Location Constituent | Method | Run No. | Ports | .Points. per Port | Minutes | Total Minutes | Figure | | | | | |
| Units 1,2 and 3 SDA Inlets | | | | | | | - | | | | | |
| Hydrogen Chloride | 26A ¹ | 1-3 | 1 | 1 | 60 | 60 | 3-3 | | | | | |
| Units 1,2 and 3 FF Outlets | | | | | | | | | | | | |
| Particulate, Be, Cd, Pb and Hg | 5/29 ² | 1-3 | 5 | 5 | 5 | 125 | 3-4 | | | | | |
| Hydrogen Chloride | 26A ¹ | 1-3 | 1 | 1 | 60 | 60 | NA | | | | | |
| Fluorides | 13B | 1-3 | 5 | 5 | 2.5 | 62.5 | 3-4 | | | | | |
| PCDDs/PCDFs (Unit 2 only) | 23 | 1-3 | 5 | 5 | 10 | 250 | 3-4 | | | | | |

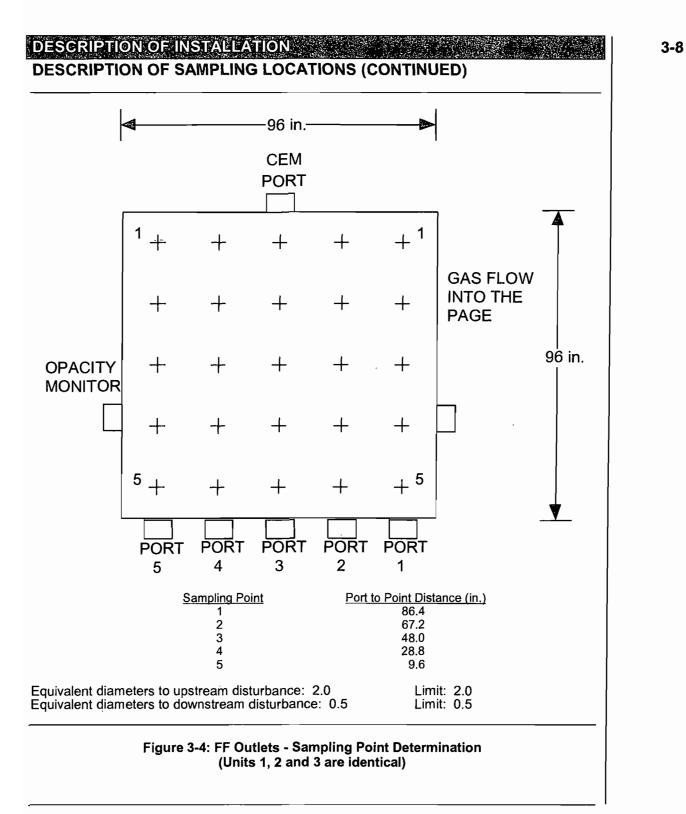
¹ Hydrogen chloride inlet testing utilized a modification of EPA Method 26A (single point constant sampling rate).

² Metals testing was done in conjunction with EPA Method 5 particulate sampling.

Client Reference No: CleanAir Project No: 10955-2



Client Reference No: CleanAir Project No: 10955-2



End of Section 3 - Description of Installation

4-1

| methods and the | |
|-----------------------------|--|
| monious una inc | ir respective sources. |
| | Table 4-1: |
| | Summary of Sampling Procedures |
| Title 40 CFR Part 6 | 0 Appendix A |
| Method 1 | "Sample and Velocity Traverses for Stationary Sources" |
| Method 2 | "Determination of Stack Gas Velocity and Volumetric Flow Rate (Type S Pitot Tube)" |
| Method 3 | "Gas Analysis for the Determination of Dry Molecular Weight" |
| Method 3A | "Determination of Oxygen and Carbon Dioxide Concentrations in Emissions from Stationary Sources (Instrumental Analyzer Procedure)" |
| Method 3B | "Gas Analysis for the Determination of Emission Rate Correction Factor or Excess Air" |
| Method 5 | "Determination of Particulate Matter Emissions from Stationary Sources" |
| Method 9 | "Visual Determination of the Opacity of Emissions from Stationary Sources" |
| Method 13B | "Determination of Total Fluoride Emissions from Stationary Sources (Specific Ion Electrode Method)" |
| Method 23 | "Determination of Polychlorinated Dibenzo-p-Dioxins and Polychlorinated Dibenzofurans from Municipal Waste Conductors" |
| Method 22 | "Visual Determination of Fugitive Emissions from Material Sources and Smoke Emissions from Flares" |
| Mod.Method 26A ¹ | "Determination of Hydrogen Halide and Halogen Emissions from Stationary Sources Isokinetic Method" |
| Method 29 | "Determination of Metals Emissions from Stationary Sources" |

¹ Hydrogen chloride testing utilized a modification of EPA Method 26A (single point constant sampling rate) at the inlet and outlet sampling locations.

These methods appear in detail in Title 40 of the Code of Federal Regulations (CFR) and on the World Wide Web at http://www.cleanair.com.

Diagrams of the sampling apparatus and major specifications of the sampling, recovery and analytical procedures are summarized for each method in Appendix A.

CleanAir followed specific quality assurance and quality control (QA/QC) procedures as outlined in the individual methods and in EPA "Quality Assurance Handbook for Air Pollution Measurement Systems: Volume III Stationary Source-Specific Methods", EPA/600/R-94/038C. Additional QA/QC methods, as prescribed in CleanAir's internal Quality Manual, were also followed. Results of all QA/QC activities performed by CleanAir are summarized in Appendix E.

End of Section 4 – Methodology

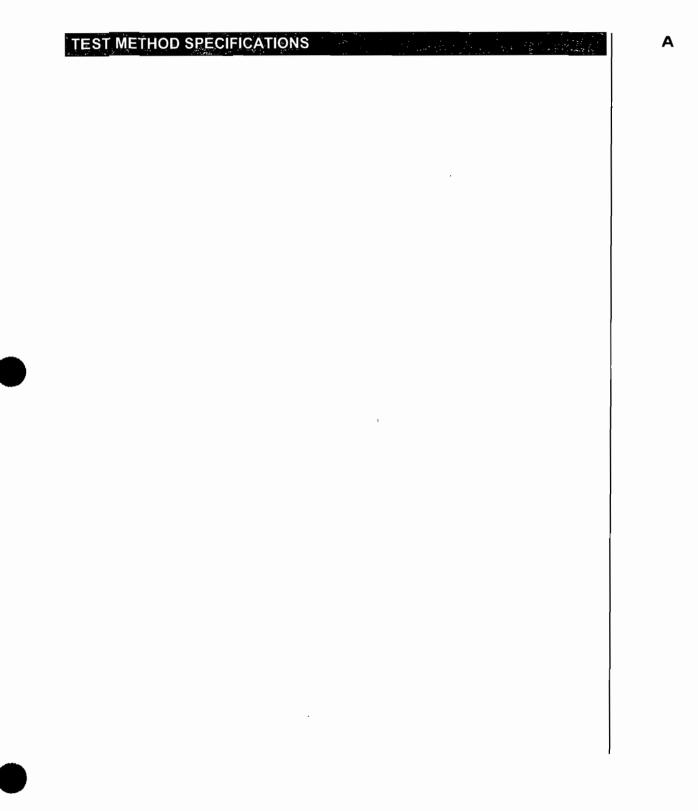


Client Reference No: CleanAir Project No: 10955-2

5-1

| APPENDIX | |
|--|---|
| TEST METHOD SPECIFICATIONS | A |
| SAMPLE CALCULATIONS | B |
| PLANT DATA | C |
| PARAMETERS | D |
| QA/QC DATA | E |
| ASTM D 6866-08 AND 7459-08 CO2 SAMPLING/ANALYSIS RESULTS | F |
| FIELD DATA | G |
| FIELD DATA PRINTOUTS | H |
| LABORATORY DATA | 1 |
| PERTINENT CERTIFICATIONS | J |
| CORRESPONDENCE AND CLARIFICATIONS | K |

CleanAir Project No: 10955-2



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EPA Method 5/29

Source Location Name(s) Pollutant(s) to be Determined Other Parameters to be Determined from Train Gas Density, Moisture, Flow Rate

Pollutant Sampling Information

Duration of Run No. of Sample Traverse Points Sample Time per Point Sampling Rate

Sampling Probe

Nozzie Material Nozzle Design Probe Liner Material Effective Probe Length Probe Temperature Set-Point

Velocity Measuring Equipment

Pitot Tube Design Pitot Tube Coefficient Pitot Tube Calibration by

Pitot Tube Attachment

Metering System Console

Meter Type Meter Accuracy Meter Resolution Meter Size Meter Calibrated Against Pump Type **Temperature Measurements Temperature Resolution** ∆P Differential Pressure Gauge ∆H Differential Pressure Gauge Barometer

Filter Description

Filter Location Filter Holder Material Filter Support Material Cyclone Material Filter Heater Set-Point Filter Material

Other Components

Description Location **Operating Temperature** Units 1, 2 and 3 FF Outlets Particulate Matter (PM) and Trace Metals (including Mercury)

Standard Method Specification

N/A N/A N/A Isokinetic (90-110%)

Borosilicate or Quartz Glass Button-Hook or Elbow Borosilicate or Quartz Glass N/A 248'F±25'F

Type S N/A Geometric or Wind Tunnel Attached to Probe

Dry Gas Meter ±2% N/A N/A Wet Test Meter or Standard DGM N/A N/A 5.4'F Inclined Manometer or Equivalent Inclined Manometer or Equivalent Mercury or Aneroid

After Probe **Borosilicate Glass** Teflon (or other non-metallic material) N/A 248°F±25°F Quartz or Fiberglass Fiber

N/A N/A N/A

125 minutes 25 5 minutes Isokinetic (90-110%)

Actual Specification Used

Borosilicate Glass Button-Hook Borosilicate Glass 8 feet 248'F±25'F

Type S 0.805 Wind-Tunnel Attached to Probe

Dry Gas Meter ±1% 0.01 cubic feet 0.1 dcf/revolution Wet Test Meter Rotary Vane Type K Thermocouple/Pyrometer 1.0°F Inclined Manometer Inclined Manometer Digital Barometer calibrated w/Mercury Aneroid

Exit of Probe **Borosilicate Glass** Teflon None 248'F±25'F Quartz Fiber

N/A N/A N/A

Impinger Train Description

Type of Glassware Connections Connection to Probe or Filter by Number of Impingers Impinger Stem Types Impinger 1 Impinger 2 Impinger 3 Impinger 3 Impinger 4 Impinger 5 Impinger 6 Impinger 7 Impinger 8

Gas Density Determination

Sample Collection Sample Collection Medium Sample Analysis

Sample Recovery Information

Probe Brush Matenal Probe Rinse Reagent Probe Rinse Wash Bottle Matenal Probe Rinse Storage Container Filter Recovered? Filter Storage Container Impinger Contents Recovered? Impinger Rinse Reagent Impinger Wash Bottle Impinger Storage Container

Analytical Information

Method 4 H₂O Determination by Filter Preparation Conditions Front-Half Rinse Preparation Back-Half Analysis Additional Analysis

EPA Method 5/29

Standard Method Specification

Ground Glass or Equivalent Direct Glass Connection 7

Modified Greenburg-Smith Modified Greenburg-Smith Greenburg-Smith Modified Greenburg-Smith Modified Greenburg-Smith Modified Greenburg-Smith

Multi-point integrated Flexible Gas Bag Orsat or Fyrite Analyzer

Non-metallic swab or bristle Acetone/0.1N Nitric Acid Glass or Teflon See Method 29 Recovery Flow Chart Yes Petri Dish - Glass or Polystyrene Yes See Method 29 Recovery Flow Chart Glass or Teflon See Recovery Flow Chart

Volumetric or Gravimetric See Method 29 Analytical Flow Chart See Method 29 Analytical Flow Chart See Method 29 Analytical Flow Chart Gravimetric (EPA Method 5)

Actual Specification Used

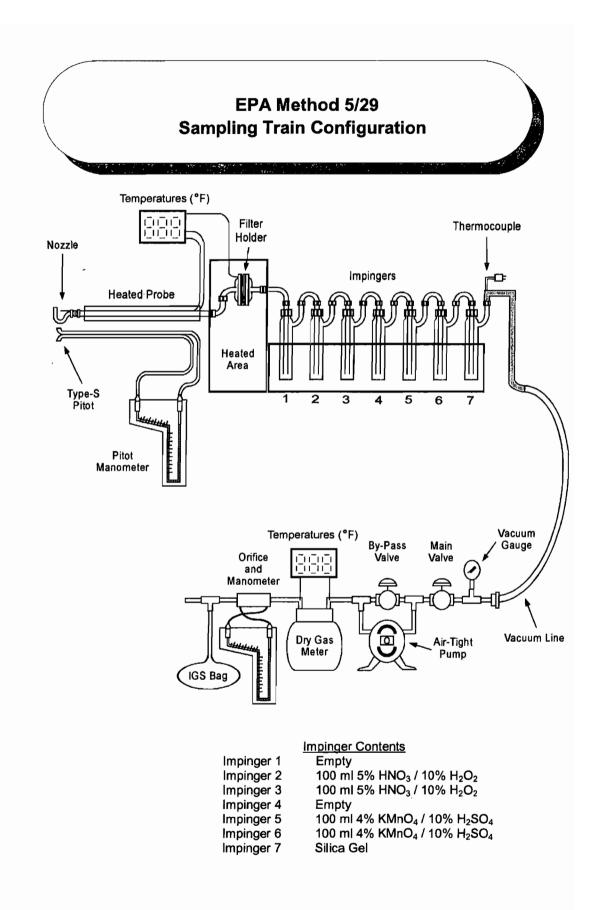
Screw Joint with Silicone Gasket Direct Glass Connection 7

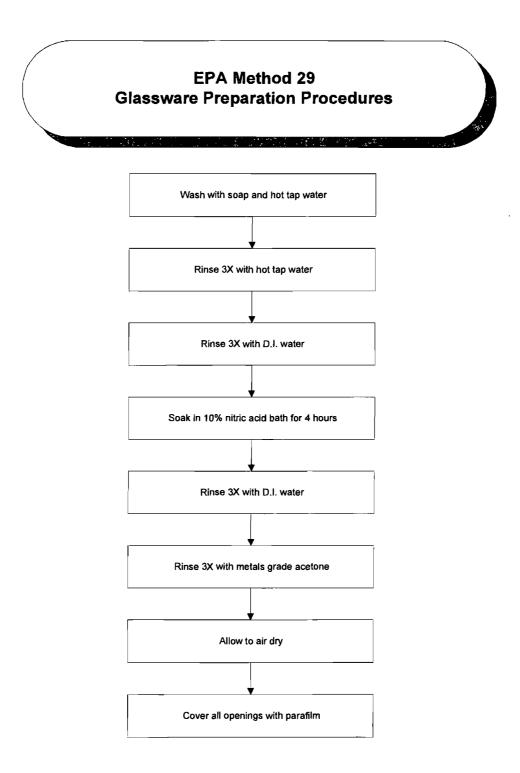
Modified Greenburg-Smith Modified Greenburg-Smith Greenburg-Smith Modified Greenburg-Smith Modified Greenburg-Smith Modified Greenburg-Smith Modified Greenburg-Smith

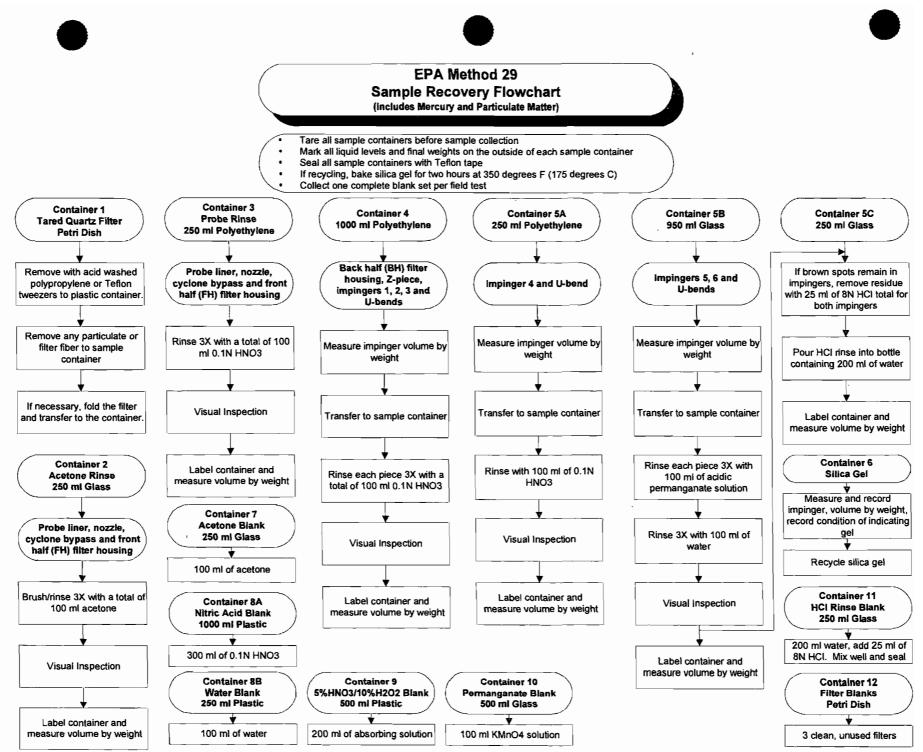
Multi-Point Integrated Vinyl Bag CEM

Teflon Mat Acetone/0.1N. Nitric Acid Teflon See Recovery Flow Chart Yes Glass Yes See Recovery Flow Chart Teflon See Recovery Flow Chart

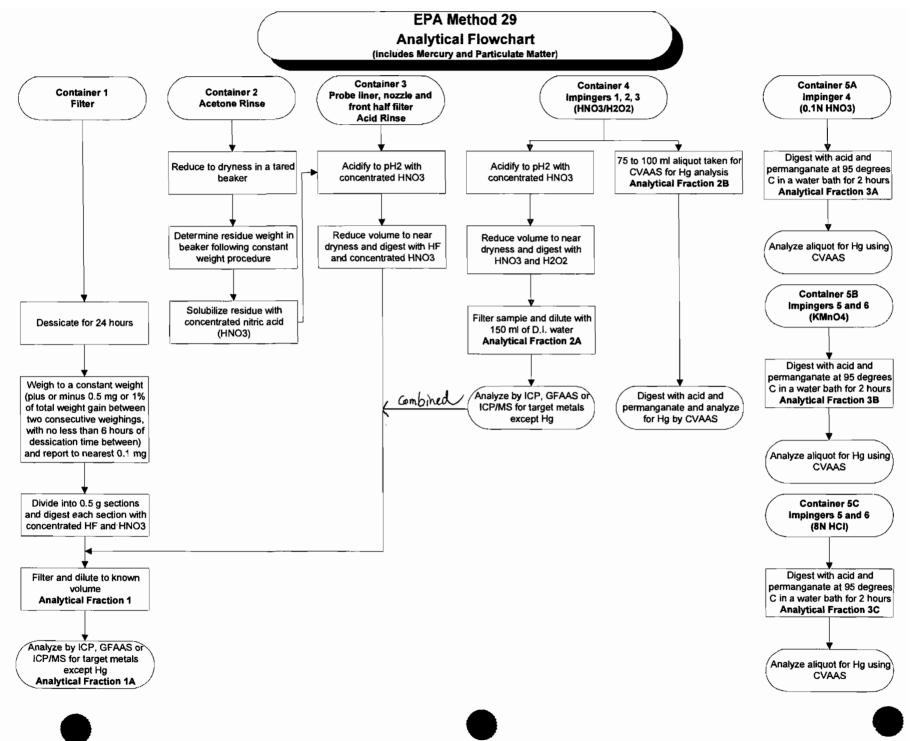
Gravimetric and Volumetric For Metals Analysis See Analytical Flow Chart See Analytical Flow Chart Gravimetric (EPA Method 5)







A - 7



EPA Method 13B

Standard Method Specification

Isokinetic (90-110%) 1 cfm maximum

Units 1,2 and 3 FF Outlets Source Location Name(s) Pollutant(s) to be Determined Total Fluoride (F) Other Parameters to be Determined from Trai Gas Density, Moisture, Flow Rate

N/A

N/A

N/A

Pollutant Sampling Information

Duration of Run No. of Sample Traverse Points Sample Time per Point Sampling Rate

Sampling Probe

Nozzle Material Nozzle Design Probe Liner Material Effective Probe Length Probe Temperature Set-Point

Velocity Measuring Equipment

Pitot Tube Design **Pitot Tube Coefficient** Pitot Tube Calibration by Pitot Tube Attachment

Metering System Console

Meter Type Meter Accuracy Meter Resolution Meter Size Meter Calibrated Against Pump Type **Temperature Measurements** Temperature Resolution ∆P Differential Pressure Gauge ∆H Differential Pressure Gauge Barometer

Filter Description

Filter Location Filter Holder Material

Filter Support Material Cyclone Material Filter Heater Set-Point

Filter Material

Other Components

Description Location **Operating Temperature**

Stainless Steel or Glass Button-Hook or Elbow Stainless Steel or Glass N/A 248'F±25'F (optional)

Type S N/A Geometric or Wind Tunnel Attached to Probe

Dry Gas Meter ±2% N/A N/A Wet Test Meter or Standard DGM N/A N/A 5.4'F Inclined Manometer or Equivalent Inclined Manometer or Equivalent Mercury or Aneroid

Exit of Probe or Between 3rd and 4th impingers Borosilicate Glass or Stainless Steel Stainless Steel if filter at probe exit; Glass Frit if filter after 3rd impinger

No. 1 if after 3rd impinger N/A N/A

N/A

N/A

N/A 248'F±25'F if after probe, unheated if after 3rd imp. Low F Quartz or Fiberglass if after probe, Whatman

Wet Test Meter Rotary Vane 1.0°F

25 2.5 minutes Isokinetic (90-110%) 1 cfm maximum

Actual Specification Used

Borosilicate Glass Button-Hook Borosilicate Glass 8 feet 248'F±25'F

62.5 minutes

Type S 0.812 Wind-Tunnel Attached to Probe

Dry Gas Meter ±1% 0.01 cubic feet 0.1 dcf/revolution Type K Thermocouple/Pyrometer Inclined Manometer Inclined Manometer Digital Barometer calibrated w/Mercury Aneroid

Exit of Probe **Borosilicate Glass**

Teflon None 248°F±25°F

N/A

N/A

Whatman No. 1 (Ashless)

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Impinger Train Description

Type of Glassware Connections Connection to Probe or Filter by Number of Impingers Impinger Stem Types Impinger 1

- Impinger 2
- Impinger 3
- Impinger 4 Impinger 5
- Impinger 6
- Impinger 7
- Impinger 8

Gas Density Determination

Sample Collection Sample Collection Medium Sample Analysis

Sample Recovery Information

Probe Brush Material Probe Rinse Reagent Probe Rinse Wash Bottle Material Probe Rinse Storage Container Filter Recovered? Filter Storage Container Impinger Contents Recovered? Impinger Rinse Reagent Impinger Wash Bottle Impinger Storage Container

Analytical Information

Method 4 H₂O Determination by Filter Preparation Conditions Front-Half Rinse Preparation Back-Half Analysis Additional Analysis

EPA Method 13B

Standard Method Specification

Ground Glass or Equivalent Direct Glass Connection 4

Modified Greenburg-Smith Greenburg-Smith Modified Greenburg-Smith Modified Greenburg-Smith

Multi-point integrated Flexible Gas Bag Orsat or Fyrite Analyzer

Nylon Bristle Deionized distilled water Glass or Polyethylene Polyethylene Yes Deionized Distilled Water Glass or Polyethylene Polyethylene

Volumetric or Gravimetric See analytical flow chart See analytical flow chart Ion Specific Electrode N/A

Actual Specification Used

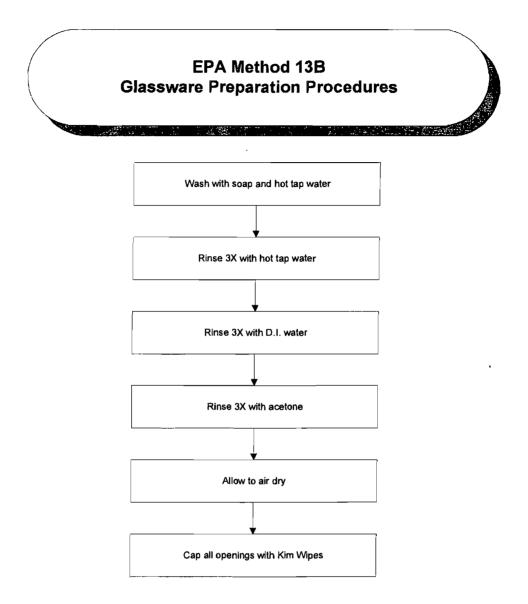
Screw Joint with Silicone Gasket Direct Glass Connection 4

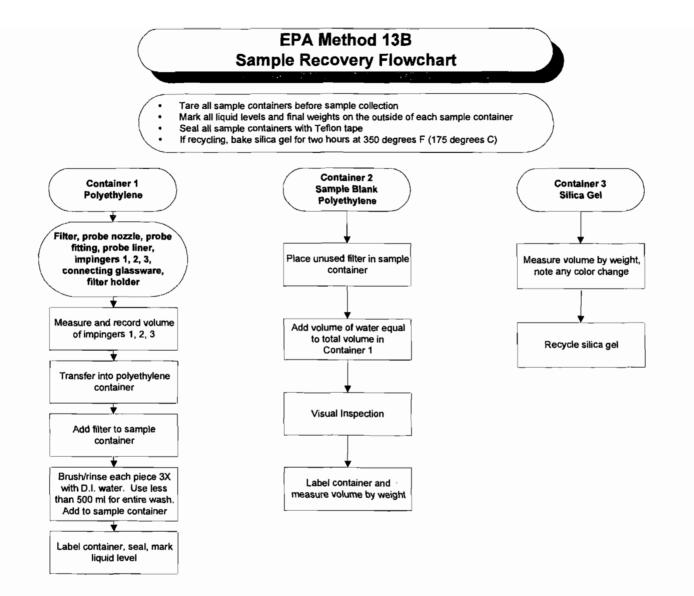
Modified Greenburg-Smith Greenburg-Smith Modified Greenburg-Smith Modified Greenburg-Smith

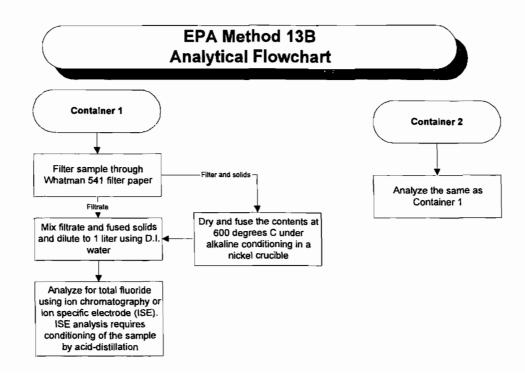
Multi-Point Integrated Vinyl Bag CEM

Nylon Bristle Deionized Distilled Water Teflon Polyethylene Yes Deionized Distilled Water Teflon Polyethylene

Gravimetric and Volumetric See Analytical Flow Chart See Analytical Flow Chart Ion Chromatography None







EPA Method 23

 Source Location Name(s)
 Unit 2 FF Outlet

 Pollutant(s) to be Determined
 Polychlorinated Dibenzo-p-Dioxins

 Other Parameters to be Determined from Train
 Gas Density, Moisture, Flow Rate

Unit 2 FF Outlet Polychlorinated Dibenzo-p-Dioxins and Polychlorinated Dibenzofurans (PCDD/PCDF) Gas Density, Moisture, Flow Rate

Pollutant Sampling Information

Duration of Run No. of Sample Traverse Points Sample Time per Point Sampling Rate

Sampling Probe

Nozzle Material Nozzle Design Probe Liner Material Effective Probe Length Probe Temperature Set-Point

Velocity Measuring Equipment

Pitot Tube Design Pitot Tube Coefficient Pitot Tube Calibration by Pitot Tube Attachment

Metering System Console

 Meter Type

 Meter Accuracy

 Meter Resolution

 Meter Size

 Meter Calibrated Against

 Pump Type

 Temperature Measurements

 Temperature Resolution

 ΔP Differential Pressure Gauge

 ΔH Differential Pressure Gauge

 Barometer

Filter Description

Filter Location Filter Holder Material Filter Support Material Cyclone Material Filter Heater Set-Point Filter Material

Other Components

Adsorbent Module Location Operating Temperature N/A N/A N/A Isokinetic (90-110%)

Standard Method Specification

Nickel, Quartz, Stainless Steel or Glass Button-Hook or Elbow Borosilicate or Quartz Glass N/A 248'F±25'F

Type S N/A Geometric or Wind Tunnel Attached to Probe

Dry Gas Meter ±2% N/A N/A Wet Test Meter or Standard DGM N/A N/A 5.4°F Inclined Manometer or Equivalent Inclined Manometer or Equivalent Mercury or Aneroid

After Probe Borosilicate Glass Glass Frit N/A 248'F±25'F Glass Fiber - Toluene Extracted

XAD-2 Trap After filter and condenser < 68°F 250 minutes 25 10 minutes Isokinetic (90-110%)

Actual Specification Used

Borosilicate Glass Button-Hook Borosilicate Glass 8 feet 248'F±25'F

Type S 0.834 Wind-Tunnel Attached to Probe

Dry Gas Meter ±1% 0.01 cubic feet 0.1 dcf/revolution Wet Test Meter Rotary Vane Type K Thermocouple/Pyrometer 1.0°F Inclined Manometer Inclined Manometer Digital Barometer calibrated w/Mercury Aneroid

Exit of Probe Borosilicate Glass Tefion None 248'F±25'F Glass Fiber - Toluene Extracted

XAD-II Adsorbent Trap After filter and condenser <68°F

Impinger Train Description Type of Glassware Connections

Connection to Probe or Filter by Number of Impingers Impinger Stem Types Impinger 1 Impinger 2 Impinger 3 Impinger 4 Impinger 5 Impinger 6 Impinger 7

Impinger 8

Gas Density Determination

Sample Collection Sample Collection Medium Sample Analysis

Sample Recovery Information

Probe Brush Material Probe Rinse Reagent Probe Rinse Wash Bottle Material Probe Rinse Storage Container Filter Recovered? Filter Storage Container Impinger Contents Recovered? Impinger Rinse Reagent Impinger Wash Bottle Impinger Storage Container

Analytical Information

Method 4 H₂O Determination by Filter Preparation Conditions Front-Half Rinse Preparation Back-Half Analysis Additional Analysis

EPA Method 23

Standard Method Specification

Ground Glass or Equivalent Direct Glass Connection 5

Modified Greenburg-Smith Modified Greenburg-Smith Greenburg-Smith Modified Greenburg-Smith Modified Greenburg-Smith

Multi-point integrated Flexible Gas Bag Orsat or Fyrite Analyzer

Inert Bristle Acetone/Methylene Chloride/Toluene Glass or Teflon Glass Yes Petri Dish - Glass or Polystyrene No N/A N/A N/A

Volumetric or Gravimetric See Method 23 Analytical Flow Chart See Method 23 Analytical Flow Chart N/A None

Actual Specification Used

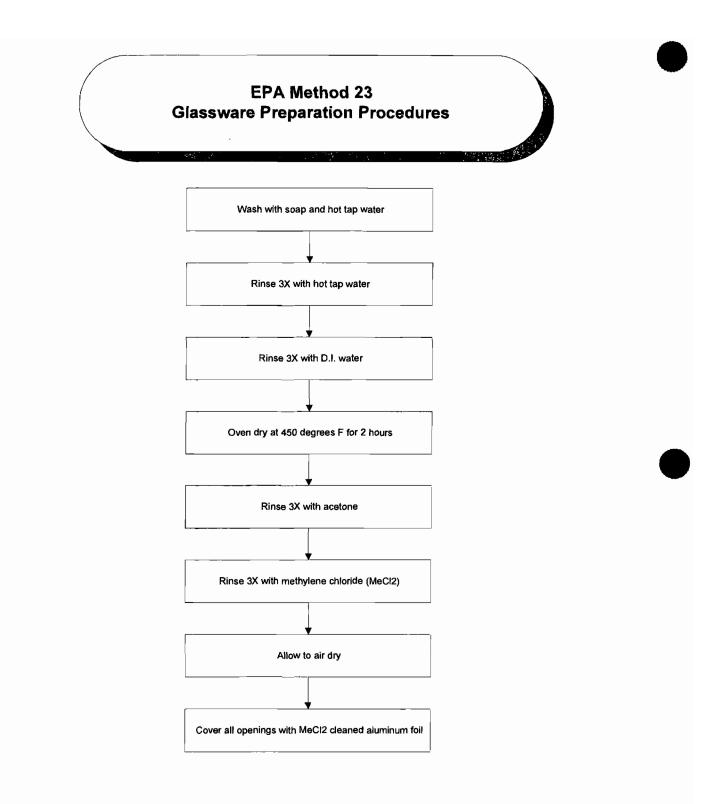
Screw Joint with Silicone Gasket Direct Glass Connection 5

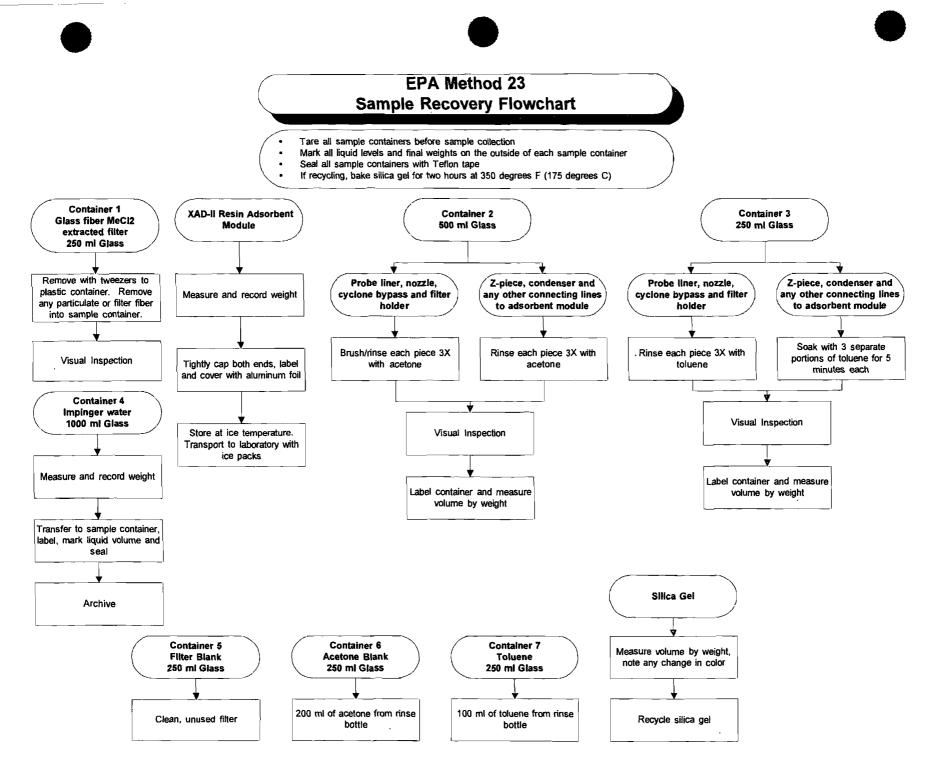
Shortened Stem (open tip) Modified Greenburg-Smith Greenburg-Smith Modified Greenburg-Smith Modified Greenburg-Smith

Multi-Point Integrated Vinyl Bag CEM

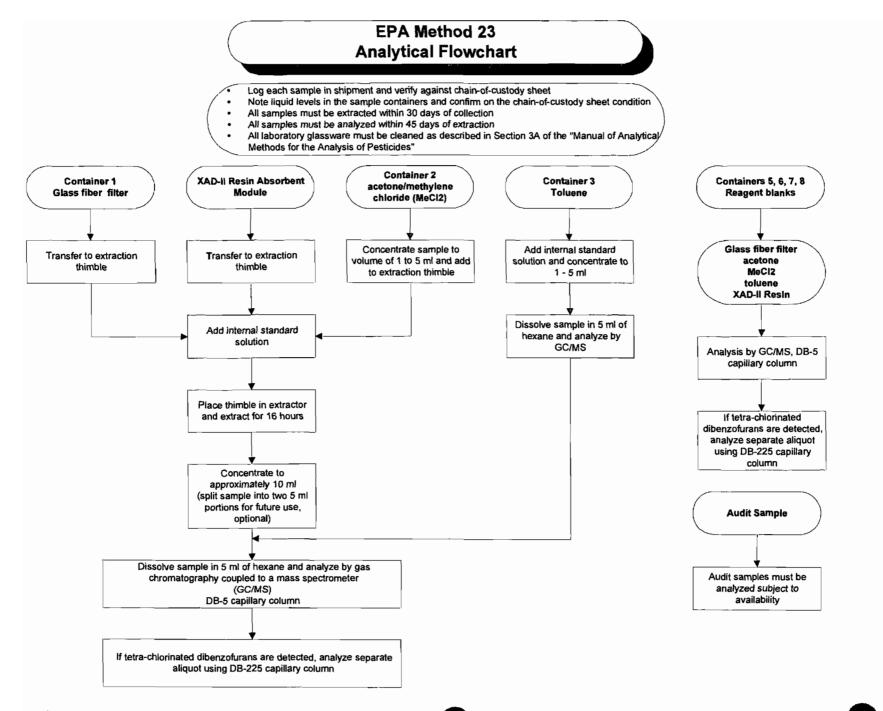
Teflon Mat Acetone/Toluene (see Appendix J) Teflon Glass Yes Glass Archived HPLC Water Teflon Polyethylene

Gravimetric For Organic Analysis Organic Analysis Archive None





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Source Location Name(s)

Pollutant(s) to be Determined

EPA Method 26A (modified)

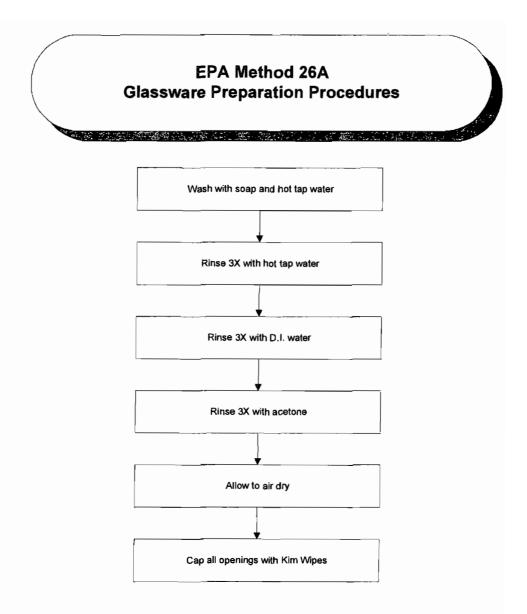
Units 1-3 SDA Inlets and Units 1-3 FF Outlets Hydrogen Chloride (HCI) Other Parameters to be Determined from Train Gas Density, Moisture

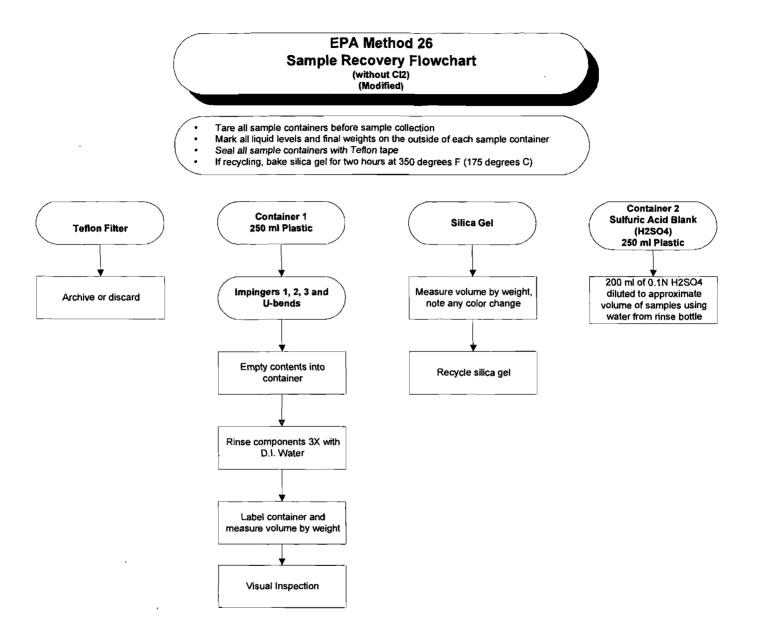
Note: Modification includes the use of full-size impingers instead of midget impingers.

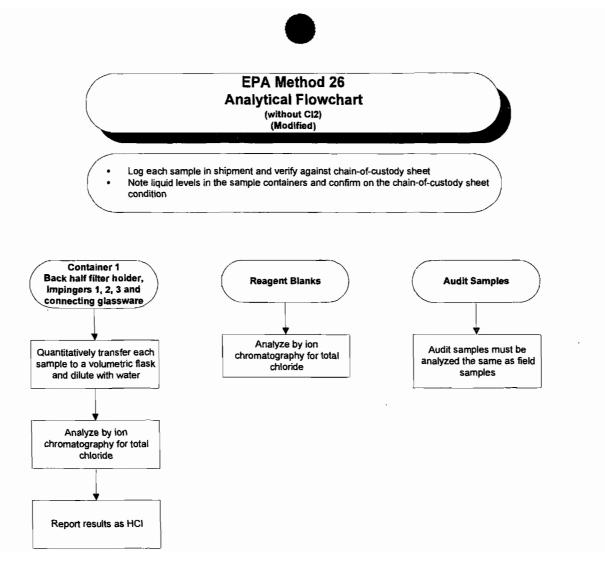
| | Standard Method Specification | Actual Specification Used |
|--------------------------------|--|--|
| Pollutant Sampling Information | | |
| Duration of Run | N/A | 60 minutes |
| No. of Sample Traverse Points | N/A | 1 |
| Sample Time per Point | N/A | 60 minutes |
| Sampling Rate | Constant Rate (±10%) | Constant Rate (±10%) |
| Sampling Probe | | |
| Nozzle Material | N/A | None |
| Nozzle Design | N/A | N/A |
| Probe Liner Material | Borosilicate Glass | Borosilicate Glass |
| Effective Probe Length | N/A | 4 feet |
| Probe Temperature Set-Point | >248°F | 350°F @ inlet, Stack Temp @ FF Outlet |
| Velocity Measuring Equipment | | |
| Pitot Tube Design | None | None |
| Pitot Tube Coefficient | N/A | N/A |
| Pitot Tube Calibration by | N/A | N/A |
| Pitot Tube Attachment | N/A | N/A |
| Metering System Console | | |
| Meter Type | Dry Gas Meter or Critical Orifice | Dry Gas Meter |
| Meter Accuracy | ±2% | ±1% |
| Meter Resolution | N/A | 0.01 cubic feet |
| Meter Size | 2 liters/minute | 0.1 dcf/revolution |
| Meter Calibrated Against | Wet Test Meter | Wet Test Meter |
| Pump Type | Diaphragm or equivalent | Rotary Vane |
| Temperature Measurements | Dial Thermometer or equivalent | Type K Thermocouple/Pyrometer |
| Temperature Resolution | 2°F-5.4°F | 1.0°F |
| ∆P Differential Pressure Gauge | N/A | N/A |
| ∆H Differential Pressure Gauge | N/A | Inclined Manometer |
| Barometer | Mercury, aneroid or other. | Digital Barometer calibrated w/Mercury Aneroid |
| Filter Description | | |
| Filter Location | After Probe | Exit of Probe |
| Filter Holder Material | Teflon or Quartz | Borosilicate Glass |
| Filter Support Material | Teflon Frit | Teflon |
| Cyclone Material | N/A | None |
| Filter Heater Set-Point | >248°F | 350'F @ Inlet, Stack Temp @ FF Outlet |
| Filter Material | Teflor/Glass Mat (Quartz, Optional High Temp>410F) | Quartz Fiber @ Inlet, Teflon on Glass @ Outlet |
| Other Components | | |
| Description | N/A | N/A |
| Location | N/A | N/A |
| Operating Temperature | N/A | N/A |

EPA Method 26A (modified)

| Sample Collection MediumN/AVinyl BagSample AnalysisN/ACEMSample Recovery InformationN/AN/AProbe Brush MaterialN/AN/AProbe Rinse ReagentN/AN/AProbe Rinse ReagentN/AN/AProbe Rinse Storage ContainerN/AN/AProbe Rinse Storage ContainerN/AN/AProbe Rinse Storage ContainerN/AN/AProbe Rinse ReagentN/AN/AProbe Rinse Storage ContainerN/AN/AProbe Rinse Storage ContainerN/AN/AIlter Recovered?NoNoFilter Storage ContainerN/AN/AImpinger Rinse ReagentDeionized Distilled WaterDeionized Distilled WaterImpinger Rinse ReagentDeionized Distilled WaterDeionized Distilled WaterImpinger Storage ContainerPolyethylene or glassPolyethyleneImpinger Storage ContainerPolyethylenePolyethyleneAnalytical InformationN/ASravimetricFilter Preparation ConditionsN/AN/AFront-Half Rinse PreparationN/AN/ABack-Half AnalysisIon ChromatographyIon Chromatography | • | • | |
|--|--|-------------------------------|----------------------------------|
| Type of Glassware ConnectionsGround Glass or EquivalentScrew Joint with Silicone GasketConnection to Probe or Filter byDirect Glass ConnectionDirect Glass ConnectionNumber of Impingers5 or 8 (Midget Impingers)5impinger 1Midget Shortened StemShortened Stem (open tip)Impinger 1Midget BubblerGreenburg-SmithImpinger 3Midget BubblerGreenburg-SmithImpinger 4Midget BubblerModified Greenburg-SmithImpinger 5Midget BubblerModified Greenburg-SmithImpinger 6Mae WestModified Greenburg-SmithImpinger 7Midget BubblerModified Greenburg-SmithImpinger 8N/ASingle Point IntegratedSample CollectionN/AVinyl BagSample Collection MediumN/AVinyl BagSample Collection MediumN/AVinyl BagSample Collection MediumN/AN/AProbe Rinse MaterialN/AN/AProbe Rinse ReagentN/AN/AProbe Rinse ReagentN/AN/AProbe Rinse ReagentN/AN/AProbe Rinse ReagentN/AN/AProbe Rinse ReagentN/AN/AImpinger ContainerYesYesImpinger Rinse ReagentDeionized Distilled WaterImpinger Rinse ReagentDeionized Distilled WaterImpinger Rinse ReagentDeionized Distilled WaterImpinger Rinse ReagentDeionized Distilled WaterImpinger Rinse ReagentDeionized Distilled Water <tr<< th=""><th></th><th>Standard Method Specification</th><th>Actual Specification Used</th></tr<<> | | Standard Method Specification | Actual Specification Used |
| Connection to Probe or Filter by Direct Glass Connection Direct Glass Connection Number of (mpingers) 5 or 6 (Midget Impingers) 5 impinger 1 Midget Shortened Stem Shortened Stem (open tip) Impinger 1 Midget Bubbler Greenburg-Smith Greenburg-Smith Midget Bubbler Greenburg-Smith Midget Bubbler Modified Greenburg-Smith Impinger 3 Midget Bubbler Modified Greenburg-Smith Impinger 5 Midget Bubbler Modified Greenburg-Smith Impinger 6 Mae West Impinger 7 Impinger 8 Sector 2000 Stratege Contents Nov 2000 Strate | Impinger Train Description | | |
| Number of Impingers5 or 8 (Midget Impingers)5Impinger Stem Typesimpinger 1Midget Shortened StemShortened Stem (open tip)Impinger 1Midget BubblerGreenburg-SmithImpinger 2Midget BubblerGreenburg-SmithImpinger 3Midget BubblerModified Greenburg-SmithImpinger 4Midget BubblerModified Greenburg-SmithImpinger 5Midget BubblerModified Greenburg-SmithImpinger 6Mae WestMidget BubblerImpinger 7impinger 8Sample Collection MediumN/ASample Collection MediumN/ASample Collection MediumN/ASample Collection MediumN/ASample Collection MediumN/ASample Collection MediumN/A <t< td=""><td>Type of Glassware Connections</td><td>Ground Glass or Equivalent</td><td>Screw Joint with Silicone Gasket</td></t<> | Type of Glassware Connections | Ground Glass or Equivalent | Screw Joint with Silicone Gasket |
| Impinger Stem TypesImpinger 1Midget Shortened StemImpinger 2Midget BubblerImpinger 3Midget BubblerImpinger 3Midget BubblerImpinger 4Midget BubblerImpinger 5Midget BubblerImpinger 6Mae WestImpinger 7Midget BubblerImpinger 8Madified Greenburg-SmithGas Density DeterminationSample Collection MediumN/ASample Collection MediumN/ASample Collection MediumN/ASample Collection MediumN/ACEMSample Collection MediumN/AVinyl BagSample CollectionNo <td< td=""><td>Connection to Probe or Filter by</td><td>Direct Glass Connection</td><td>Direct Glass Connection</td></td<> | Connection to Probe or Filter by | Direct Glass Connection | Direct Glass Connection |
| Impinger 1Midget Shortened StemShortened Stem (open tip)Impinger 2Midget BubblerGreenburg-SmithImpinger 3Midget BubblerGreenburg-SmithImpinger 4Midget BubblerModified Greenburg-SmithImpinger 5Midget BubblerModified Greenburg-SmithImpinger 6Mae WestForenburg-SmithImpinger 7Forenburg-SmithImpinger 8Mae WestSample Collection MediumN/ASample Collection MediumN/ASample Collection MediumN/ASample Recovery InformationN/AProbe Brush MaterialN/AProbe Brush MaterialN/AProbe Rinse ReagentN/AN/AN/AProbe Rinse Storage ContainerN/AFilter Recovered?YesMinginger ContainerN/AImpinger ContainerN/AImpinger ContainerPolyethylene or glassImpinger Rinse ReagentDelonized Distilled WaterDelonized Distilled WaterDelonized Distilled WaterImpinger ContainerPolyethylene or glassPolyethylenePolyethylene or glassPolyethylenePolyethyleneImpinger Rinse ReagentN/AMethod 414_0 Determination byN/AMethod 414_0 Determination byN/AMethod 414_0 Determination byN/AMaterial Filter Preparation ConditionsN/AMaterial Filter Preparation ConditionsN/AMethod 414_0 Determination byN/AMethod 414_0 AlaysisIon | Number of Impingers | 5 or 6 (Midget Impingers) | 5 |
| Impinger 2Midget BubblerGreenburg-SmithImpinger 3Midget BubblerGreenburg-SmithImpinger 4Midget BubblerModified Greenburg-SmithImpinger 5Midget BubblerModified Greenburg-SmithImpinger 6Mae WestModified Greenburg-SmithImpinger 7Impinger 7Impinger 8NAColspan="2">Single Point IntegratedSample CollectionN/ASample Collection MidumN/ASample Collection MidumN/ASample Collection MediumN/ASample Collection MediumN/ASample Collection MediumN/ASample Collection MediumN/ASample Recover InformationProbe Brush MaterialN/A <td>Impinger Stem Types</td> <td></td> <td></td> | Impinger Stem Types | | |
| Impinger 3Midget BubblerGreenburg-SmithImpinger 4Midget BubblerModified Greenburg-SmithImpinger 5Midget BubblerModified Greenburg-SmithImpinger 6Mae WestImpinger 7Maes WestImpinger 8N/ASingle Point IntegratedSample Collection MediumN/ASample Collection MediumN/ASample Recovery InformationProbe Rinse ReagentN/AN/AProbe Rinse ReagentN/AN/AProbe Rinse ReagentN/A< | Impinger 1 | Midget Shortened Stem | Shortened Stem (open tip) |
| Impinger 4Midget BubblerModified Greenburg-SmithImpinger 5Midget BubblerModified Greenburg-SmithImpinger 6Mae WestMain of Greenburg-SmithImpinger 7Impinger 7Impinger 8Mae WestSample CollectionN/ASample Collection MediumN/ASample Collection MediumN/AProbe Brush MaterialN/AProbe Rinse ReagentN/AN/AN/AProbe Rinse ReagentN/AN/AN/AProbe Rinse Storage ContainerN/AIlter Storage ContainerN/AImpinger Contents Recovered?YesImpinger Rinse ReagentDelonized Distilled WaterImpinger Rinse ReagentDelonized Distilled WaterImpinger Storage ContainerPolyethylene or glassImpinger Storage ContainerPolyethylene or glassImpinger Storage ContainerN/AImpinger Storage ContainerN/AImpinger Storage ContainerN/AImpinger Storage ContainerN/A <td>Impinger 2</td> <td>Midget Bubbler</td> <td>Greenburg-Smith</td> | Impinger 2 | Midget Bubbler | Greenburg-Smith |
| Impinger 5Midget BubblerModified Greenburg-SmithImpinger 6Mae WestImpinger 7Impinger 7Impinger 8Impinger 7Sample CollectionN/ASample CollectionN/ASample Collection MediumN/ASample Collection MediumN/ASample Collection MediumN/ASample Recovery InformationProbe Brush MaterialN/AProbe Brush MaterialN/AProbe Rinse ReagentN/AProbe Rinse ReagentN/AProbe Rinse Storage ContainerN/AFilter Recovered?NoNoN/AFilter Storage ContainerN/AImpinger Ninse ReagentDeionized Distilled WaterImpinger Rinse ReagentPolyethylene or glassPolyethylenePolyethyleneImpinger Storage ContainerN/AMaterialPolyethylene or glassPolyethylenePolyethyleneImpinger Wash BottlePolyethylene or glassPolyethylenePolyethyleneImpinger Storage ContainerN/AMethod 4 H ₂ O Determination byN/AFilter Preparation ConditionsN/AFilter Preparation ConditionsN/AFilter Preparation ConditionsN/AFinter Preparation ConditionsN/AFinter Preparation ConditionsN/AFinter Preparation ConditionsN/AFinter Preparation ConditionsN/AFinter Preparation ConditionsN/AFinter Preparation ConditionsN/A | Impinger 3 | Midget Bubbler | Greenburg-Smith |
| Implinger 6 Implinger 7 Implinger 8Mae WestGas Density DeterminationKasSample CollectionN/ASingle Point IntegratedSample Collection MediumN/AVinyl BagSample AnalysisN/ACEMSample Recovery InformationN/AN/AProbe Brush MaterialN/AN/AProbe Rinse ReagentN/AN/AProbe Rinse Storage ContainerN/AN/AProbe Rinse Storage ContainerN/AN/AFilter Recovered?YesYesImpinger Rinse ReagentDeionized Distilled WaterDeionized Distilled WaterImpinger Storage ContainerPolyethylene or glassPolyethyleneMethod 4 H ₂ O Determination byN/AMAMaMethod 4 H ₂ O Determination byN/AMAMaFront-Half Rinse PreparationN/AMAMaBack-Half AnalysisIon ChromatographyIon ChromatographyIon Chromatography | Impinger 4 | Midget Bubbler | Modified Greenburg-Smith |
| Impinger 7 Impinger 8 Gas Density Determination Sample Collection N/A Single Point Integrated Sample Collection Medium N/A Vinyl Bag Sample Collection Medium N/A CEM Sample Collection Medium N/A CEM Sample Collection Medium N/A CEM Sample Collection Medium N/A Sample Recovery Information Probe Brush Material N/A N/A Probe Brush Material N/A N/A Probe Rinse Reagent N/A N/A Probe Rinse Storage Container N/A N/A Probe Rinse Storage Container N/A N/A Impinger Contents Recovered? No No Filter Storage Container N/A N/A Impinger Kinse Reagent Deionized Distilled Water Deionized Distilled Water Impinger Storage Container Polyethylene or glass Polyethylene Impinger Storage Container Polyethylene Deionized Distilled Water Impinger Storage Container N/A Material Iter Preparation Conditions <td< td=""><td>Impinger 5</td><td>Midget Bubbler</td><td>Modified Greenburg-Smith</td></td<> | Impinger 5 | Midget Bubbler | Modified Greenburg-Smith |
| Impiger 8 Gas Density Determination Sample Collection N/A Single Point Integrated Sample Collection Medium N/A Vinyl Bag Sample Collection Medium N/A CEM Sample Collection Medium N/A CEM Sample Analysis N/A CEM Sample Recovery Information N/A N/A Probe Brush Material N/A N/A Probe Rinse Reagent N/A N/A Probe Rinse Reagent N/A N/A Probe Rinse Storage Container N/A N/A Filter Scorage Container N/A N/A Filter Scorage Container N/A N/A Impinger Rinse Reagent N/A N/A Impinger Contents Recovered? Yes Yes Impinger Rinse Reagent Deionized Distilled Water Deionized Distilled Water Impinger Storage Container Polyethylene or glass Polyethylene Impinger Storage Container Polyethylene or glass Polyethylene Impinger Storage Container N/A MA Kathelf Anglysis N/A | Impinger 6 | Mae West | |
| Gas Density Determination N/A Single Point Integrated Sample Collection N/A Vinyl Bag Sample Collection Medium N/A Vinyl Bag Sample Analysis N/A CEM Sample Recovery Information V/A V/A Probe Brush Material N/A N/A Probe Rinse Reagent N/A N/A Probe Rinse Vash Bottle Material N/A N/A Probe Rinse Vash Bottle Material N/A N/A Probe Rinse Vash Bottle Material N/A N/A Probe Rinse Storage Container N/A N/A Filter Storage Container N/A N/A Impinger Contents Recovered? Yes Yes Impinger Rinse Reagent Deionized Distilled Water Deionized Distilled Water Impinger Storage Container Polyethylene or glass Polyethylene Impinger Storage Container N/A Matort | Impinger 7 | | |
| Sample CollectionN/ASingle Point IntegratedSample Collection MediumN/AVinyl BagSample AnalysisN/ACEMSample Recovery InformationN/AN/AProbe Brush MaterialN/AN/AProbe Brush MaterialN/AN/AProbe Rinse ReagentN/AN/AProbe Rinse Storage ContainerN/AN/AProbe Rinse Storage ContainerN/AN/AFilter Storage ContainerN/AN/AFilter Storage ContainerN/AN/AImpinger Contents Recovered?YesYesImpinger Rinse ReagentDeionized Distilled WaterDeionized Distilled WaterImpinger Storage ContainerPolyethylene or glassPolyethyleneImpinger Storage ContainerPolyethyleneSample Distilled WaterImpinger Storage ContainerN/AMAImpinger Storage ContainerN/AMAImpinger Storage ContainerPolyethylene or glassPolyethyleneImpinger Storage ContainerN/AMAImpinger Storage Container | Impinger 8 | | |
| Sample Collection MediumN/AVinyl BagSample AnalysisN/ACEMSample Recovery InformationN/AN/AProbe Brush MaterialN/AN/AProbe Rinse ReagentN/AN/AProbe Rinse ReagentN/AN/AProbe Rinse Storage ContainerN/AN/AProbe Rinse Storage ContainerN/AN/AProbe Rinse Storage ContainerN/AN/AProbe Rinse ReagentN/AN/AProbe Rinse Storage ContainerN/AN/AProbe Rinse Storage ContainerN/AN/AIlter Recovered?NoNoFilter Storage ContainerN/AN/AImpinger Rinse ReagentDeionized Distilled WaterDeionized Distilled WaterImpinger Rinse ReagentDeionized Distilled WaterDeionized Distilled WaterImpinger Storage ContainerPolyethylene or glassPolyethyleneImpinger Storage ContainerPolyethylenePolyethyleneAnalytical InformationN/ASravimetricFilter Preparation ConditionsN/AN/AFront-Half Rinse PreparationN/AN/ABack-Half AnalysisIon ChromatographyIon Chromatography | Gas Density Determination | | |
| Sample AnalysisN/ACEMSample Recovery InformationProbe Brush MaterialN/AProbe Brush MaterialN/AProbe Rinse ReagentN/AN/AN/AProbe Rinse Storage ContainerN/AN/AN/AProbe Rinse Storage ContainerN/AN/AN/AProbe Rinse Storage ContainerN/AN/AN/AProbe Rinse Storage ContainerN/AN/AN/AImpinger Contents Recovered?YesYesYesImpinger Rinse ReagentDeionized Distilled WaterImpinger Rinse ReagentPolyethylene or glassImpinger Storage ContainerPolyethylenePolyethylenePolyethyleneImpinger Storage ContainerN/AMethod 4 H ₂ O Determination byN/AFilter Preparation ConditionsN/AFilter Preparation ConditionsN/AFront-Half Rinse PreparationN/ABack-Half AnalysisIon Chromatography | Sample Collection | N/A | Single Point Integrated |
| Sample Recovery InformationVIAProbe Brush MaterialN/AProbe Rinse ReagentN/AProbe Rinse ReagentN/AProbe Rinse Wash Bottle MaterialN/AProbe Rinse Storage ContainerN/AProbe Rinse Storage ContainerN/AProbe Rinse Storage ContainerN/AProbe Rinse Storage ContainerN/AProbe Rinse Storage ContainerN/AFilter Recovered?NoNoN/AImpinger Contents Recovered?YesImpinger Contents Recovered?YesImpinger Rinse ReagentDeionized Distilled WaterImpinger Storage ContainerPolyethylene or glassImpinger Storage ContainerPolyethyleneImpinger Storage ContainerPolyethyleneMethod 4 H ₂ O Determination byN/AMichtod 4 H ₂ O Determination byN/AFilter Preparation ConditionsN/AFront-Half Rinse PreparationN/ABack-Half AnalysisIon Chromatography | Sample Collection Medium | N/A | Vinyl Bag |
| Probe Brush MaterialN/AN/AProbe Rinse ReagentN/AN/AProbe Rinse ReagentN/AN/AProbe Rinse Wash Bottle MaterialN/AN/AProbe Rinse Storage ContainerN/AN/AProbe Rinse Storage ContainerN/AN/AFilter Recovered?NoNoFilter Storage ContainerN/AN/AImpinger Contents Recovered?YesYesImpinger Contents Recovered?YesYesImpinger Rinse ReagentDeionized Distilled WaterDeionized Distilled WaterImpinger Storage ContainerPolyethylene or glassPolyethyleneImpinger Storage ContainerPolyethylenePolyethyleneMethod 4 H2O Determination byN/AGravimetricFilter Preparation ConditionsN/AN/AFront-Half Rinse PreparationN/AN/ABack-Half AnalysisIon ChromatographyIon Chromatography | Sample Analysis | N/A | CEM |
| Probe Rinse ReagentN/AN/AProbe Rinse Wash Bottle MaterialN/AN/AProbe Rinse Storage ContainerN/AN/AProbe Rinse Storage ContainerN/AN/AFilter Recovered?NoNoFilter Storage ContainerN/AN/AImpinger Contents Recovered?YesYesImpinger Rinse ReagentDeionized Distilled WaterDeionized Distilled WaterImpinger Rinse ReagentDeionized Distilled WaterDeionized Distilled WaterImpinger Storage ContainerPolyethylene or glassPolyethyleneImpinger Storage ContainerPolyethylenePolyethyleneImpinger Storage ContainerN/AGravimetricFilter Preparation ConditionsN/AN/AFinter Preparation ConditionsN/AN/ABack-Half AnalysisIon ChromatographyIon Chromatography | Sample Recovery Information | | |
| Probe Rinse Wash Bottle MaterialN/AN/AProbe Rinse Storage ContainerN/AN/AProbe Rinse Storage ContainerN/AN/AFilter Recovered?NoNoFilter Storage ContainerN/AN/AImpinger Contents Recovered?YesYesImpinger Rinse ReagentDeionized Distilled WaterDeionized Distilled WaterImpinger Rinse ReagentPolyethylene or glassPolyethyleneImpinger Storage ContainerPolyethylenePolyethyleneImpinger Storage ContainerPolyethyleneScavimetricAnalytical InformationN/AGravimetricFilter Preparation ConditionsN/AN/AFront-Half Rinse PreparationN/AN/ABack-Half AnalysisIon ChromatographyIon Chromatography | Probe Brush Material | N/A | N/A |
| Probe Rinse Storage ContainerN/AFilter Recovered?NoNoFilter Recovered?NoNoFilter Storage ContainerN/AN/AImpinger Contents Recovered?YesYesImpinger Rinse ReagentDeionized Distilled WaterDeionized Distilled WaterImpinger Wash BottlePolyethylene or glassPolyethyleneImpinger Storage ContainerPolyethylenePolyethyleneImpinger Storage ContainerPolyethyleneScavimetricAnalytical InformationN/AGravimetricFilter Preparation ConditionsN/AN/AFront-Half Rinse PreparationN/AN/ABack-Half AnalysisIon ChromatographyIon Chromatography | Probe Rinse Reagent | N/A | N/A |
| Filter Recovered?NoNoFilter Storage ContainerN/AN/AImpinger Contents Recovered?YesYesImpinger Rinse ReagentDeionized Distilled WaterDeionized Distilled WaterImpinger Wash BottlePolyethylene or glassPolyethyleneImpinger Storage ContainerPolyethylenePolyethyleneAnalytical InformationN/ASravimetricFilter Preparation ConditionsN/AN/AFront-Half Rinse PreparationN/AN/ABack-Half AnalysisIon ChromatographyIon Chromatography | Probe Rinse Wash Bottle Material | N/A | N/A |
| Filter Storage ContainerN/AN/AImpinger Contents Recovered?YesYesImpinger Rinse ReagentDeionized Distilled WaterDeionized Distilled WaterImpinger Wash BottlePolyethylene or glassPolyethyleneImpinger Storage ContainerPolyethylenePolyethyleneAnalytical InformationN/AGravimetricMethod 4 H2O Determination byN/AGravimetricFilter Preparation ConditionsN/AN/AFront-Half Rinse PreparationN/AN/ABack-Half AnalysisIon ChromatographyIon Chromatography | Probe Rinse Storage Container | N/A | N/A |
| Impinger Contents Recovered?YesYesImpinger Contents Recovered?YesDeionized Distilled WaterDeionized Distilled WaterImpinger Rinse ReagentDeionized Distilled WaterDeionized Distilled WaterImpinger Wash BottlePolyethylene or glassPolyethyleneImpinger Storage ContainerPolyethylenePolyethyleneAnalytical InformationN/AGravimetricMethod 4 H2O Determination byN/AN/AFilter Preparation ConditionsN/AN/AFront-Half Rinse PreparationN/AN/ABack-Half AnalysisIon ChromatographyIon Chromatography | Filter Recovered? | No | No |
| Impinger Rinse ReagentDeionized Distilled WaterDeionized Distilled WaterImpinger Wash BottlePolyethylene or glassPolyethyleneImpinger Storage ContainerPolyethylenePolyethyleneAnalytical InformationPolyethylenePolyethyleneMethod 4 H2O Determination byN/AGravimetricFilter Preparation ConditionsN/AN/AFront-Half Rinse PreparationN/AN/ABack-Half AnalysisIon ChromatographyIon Chromatography | Filter Storage Container | N/A | N/A |
| Impinger Wash Bottle Polyethylene or glass Polyethylene Impinger Storage Container Polyethylene Polyethylene Analytical Information Polyethylene Polyethylene Method 4 H ₂ O Determination by N/A Gravimetric Filter Preparation Conditions N/A N/A Front-Half Rinse Preparation N/A N/A Back-Half Analysis Ion Chromatography Ion Chromatography | Impinger Contents Recovered? | Yes | Yes |
| Impinger Storage Container Polyethylene Polyethylene Analytical Information Filter Preparation Conditions N/A Gravimetric Filter Preparation Conditions N/A N/A Front-Half Rinse Preparation N/A N/A Back-Half Analysis Ion Chromatography Ion Chromatography | Impinger Rinse Reagent | Deionized Distilled Water | Deionized Distilled Water |
| Analytical Information Method 4 H ₂ O Determination by N/A Filter Preparation Conditions N/A Front-Half Rinse Preparation N/A Back-Half Analysis Ion Chromatography | Impinger Wash Bottle | Polyethylene or glass | Polyethylene |
| Method 4 H2O Determination by N/A Gravimetric Filter Preparation Conditions N/A N/A Front-Half Rinse Preparation N/A N/A Back-Half Analysis Ion Chromatography Ion Chromatography | Impinger Storage Container | Polyethylene | Polyethylene |
| Filter Preparation Conditions N/A N/A Front-Half Rinse Preparation N/A N/A Back-Half Analysis Ion Chromatography Ion Chromatography | Analytical Information | | |
| Front-Half Rinse Preparation N/A N/A Back-Half Analysis Ion Chromatography Ion Chromatography | Method 4 H ₂ O Determination by | N/A | Gravimetric |
| Back-Half Analysis Ion Chromatography Ion Chromatography | Filter Preparation Conditions | N/A | N/A |
| | Front-Half Rinse Preparation | N/A | N/A |
| Additional Analysis None None | Back-Half Analysis | Ion Chromatography | Ion Chromatography |
| | Additional Analysis | None | None |







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CleanAir Project No: 10955-2

| SAMPLE CALCULATIONS | В |
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EPA Method 1-4 Calculations

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USEPA Method 5/29 (Particulate/Metals) Sampling, Velocity and Moisture Sample Calculations

Sample data taken from Run 1

Note: The tables presenting the results are generated electronically from raw data. It may not be possible to exactly duplicate these results using a calculator. The reference method data, results, and all calculations are carried to sixteen decimal places throughout. The final table is formatted to an appropriate number of significant figures.

1. Volume of water collected (wscf)

$$= (0.04706)(V_{lc})$$

V_{wstd} Where:

| vhere: V _{ic} 0.04706 | = total volume of liquid collected in impingers and silica gel (ml) | | 459.4 0.04706 | ml ft ³ /ml |
|--------------------------------------|---|---|------------------|---------------------------|
| V _{wstd} | = volume of water vapor collected at standard conditions (ft ³) | = | 21.62 | ft ³ |

2. Volume of gas metered, standard conditions (dscf)

$$=\frac{(17.64)(V_m)\left(P_{bar}+\frac{\Delta H}{13.6}\right)(Y_d)}{(460+T_m)}$$

Where:

V_{msid}

| P_{bar} | | = | 30.05 | in. Hg |
|-------------------|---|---|--------|----------------------------|
| Tm | = average dry gas meter temperature (°F) | = | 69.90 | °F |
| V _m | volume of gas sample through the dry gas meter at meter conditions (dcf) | = | 84.67 | dcf |
| Yd | = gas meter correction factor (dimensionless) | = | 0.9904 | |
| ΔH | = average pressure drop across meter box orifice (in. H ₂ O) | = | 1.46 | in. H₂O |
| 17.64 | = standard temperature to pressure ratio (°R/in. Hg) | = | 17.64 | °R/in. Hg |
| 13.6 | = conversion factor (in. H ₂ O/in. Hg) | = | 13.6 | in.H ₂ 0/in. Hg |
| 460 | = °F to °R conversion constant | = | 460 | |
| V _{mstd} | volume of gas sampled through the dry gas meter at standard conditions (dscf) | = | 84.183 | dscf |

3. Sample gas pressure (in. Hg)

$$= P_{bar} + \left(\frac{P_g}{13.6}\right)$$

Where:

 P_{s}

| P _{bar} | = barometric pressure (in. Hg) | = | 30.05 | in. Hg |
|------------------|--|---|--------|----------------|
| Pg | = sample gas static pressure (in. H₂O) | = | -10.60 | in. H₂O |
| 13.6 | = conversion factor (in. H₂O/in. Hg) | = | 13.6 | in. H₂O/in. Hg |
| Ps | | = | 29.27 | in. Hg |

4. Actual water vapor pressure at sample gas temperature less than 212°F (in. Hg)

 $\left(18.3036 - \frac{3816.44}{\frac{5}{9}(T_s - 32) + 273.15 - 46.13}\right)$

 P_{ν}

| - | e | |
|---|---|------|
| - | | 25.4 |

W

| Vhere: | | | | |
|----------------|---|---|---------|--------------|
| Τ _s | = average sample gas temperature (°F) | = | 307.48 | °F |
| 18.3036 | = Antoine coefficient | = | 18.3036 | °κ |
| 3816.44 | = Antoine coefficient | = | 3816.44 | °K |
| 273.15 | = temperature conversion factor | = | 273.15 | °К |
| 46.13 | = Antoine coefficient | = | 46.13 | °K |
| 25.4 | = conversion factor | = | 25.4 | mm Hg/in. Hg |
| 5/9 | = Fahrenheit to Celsius conversion factor | = | 5/9 | °C/°F |
| 32 | = temperature conversion (°F) | = | 32 | °F |
| Pv | = vapor pressure, actual (in. Hg) | = | 29.27 | in. Hg |

5. Water vapor pressure at gas temperature greater than 212°F (in. Hg)

| P, | $= P_s$ | | | |
|--------------------------|---|---|-------|--------|
| Where: P _s | = absolute sample gas pressure (in. Hg) | = | 29.27 | in. Hg |
| Pv | = water vapor pressure, actual (in. Hg) | = | 29.27 | in. Hg |

6. Moisture measured in sample (% by volume)

$$B_{wo} = \frac{V_{wsid}}{\left(V_{msid} + V_{wsid}\right)}$$

Wh

| Where: | | | | |
|-------------------|---|---|--------|------|
| V _{mstd} | volume of gas sampled through the dry gas meter at standard conditions (dscf) | = | 84.183 | dscf |
| V _{wstd} | = volume of water collected at standard conditions (scf) | = | 21.62 | scf |
| Bwo | = proportion of water measured in the gas stream by volume | = | 0.2043 | |
| | | = | 20.43 | % |

7. Saturated moisture content (% by volume)

 $B_{ws} = \frac{P_v}{P_s}$ Wh

| Where: | | | | |
|-----------------|--|---|------------------|--------|
| Ps | = absolute sample gas pressure (in. Hg) | = | 29.27 | in. Hg |
| P _v | = water vapor pressure, actual (in. Hg) | = | 29.27 | in. Hg |
| B _{ws} | = proportion of water vapor in the gas stream by volume at saturated conditions | = | 1.0000 100.00 | % |
| | | | | |

8. Actual water vapor in gas (% by volume)

$$B_{w} = MINIMUM \left[B_{wo}, B_{ws}\right]$$

Where:

| B _{ws} | proportion of water vapor in the gas stream by volume at saturated conditions | = | 1.0000 | |
|-----------------|---|---|--------|---|
| B _{wo} | = proportion of water measured in the gas stream by volume | = | 0.2043 | |
| B _w | = actual water vapor in gas | = | 0.2043 | |
| | | = | 20.43 | % |

9. Nitrogen (plus carbon monoxide) in gas stream (% by volume, dry)

$$N_2 + CO = 100 - CO_2 - O_2$$

Where:

| CO ₂ | = proportion of carbon dioxide in the gas stream by volume (%) | = | 9.3 | % |
|-----------------|--|---|------|---|
| O ₂ | = proportion of oxygen in the gas stream by volume (%) | = | 10.1 | % |
| 100 | = conversion factor (%) | = | 100 | % |
| | | | | |

| N ₂ +CO = proportion of nitrogen and CO in the gas stream by volume | (%) | = | 80.68 | % |
|--|-----|---|-------|---|
|--|-----|---|-------|---|

10. Molecular weight of dry gas stream (lb/lb·mole)

| M_d | $= \left(M_{CO_2}\right) \frac{(CO_2)}{(100)} + \left(M_{O_2}\right) \frac{(O_2)}{(100)} + \left(M_{N_2+CO}\right) \frac{(N_2+CO)}{(100)}$ | | | |
|--------------------|--|---|-------|------------|
| Where: | | | | |
| M _{CO2} | = molecular weight of carbon dioxide (lb/lb mole) | = | 44.00 | lb/lb·mole |
| M _{O2} | = molecular weight of oxygen (lb/lb·mole) | = | 32.00 | lb/lb·mole |
| M _{N2+CO} | = molecular weight of nitrogen and carbon monoxide (lb/lb·mole) | = | 28.00 | lb/lb mole |
| CO ₂ | = proportion of carbon dioxide in the gas stream by volume (%) | = | 9.3 | % |
| O ₂ | = proportion of oxygen in the gas stream by volume (%) | = | 10.1 | % |
| N ₂ +CO | = proportion of nitrogen and CO in the gas stream by volume (%) | = | 80.7 | % |
| 100 | = conversion factor (%) | = | 100 | % |
| Md | = dry molecular weight of sample gas (Ib/Ib·mole) | = | 29.88 | lb/lb·mole |

11. Molecular weight of sample gas (lb/lb·mole)

$$M_{s} = (M_{d})(1 - B_{w}) + (M_{H_{2}O})(B_{w})$$

Where:

.

| B _w M _d M _{H2O} | proportion of water vapor in the gas stream by volume dry molecular weight of sample gas (lb/lb·mole) molecular weight of water (lb/lb·mole) | = | 0.2043 29.88 18.00 | lb/lb∙mole lb/lb∙mole |
|--|--|---|--------------------------|--------------------------|
| Ms | = molecular weight of sample gas, wet basis (lb/lb·mole) | = | 27.45 | lb/lb·mole |

EPA Method 1-4 Calculations

| QA/QC | |
|-------|--|
| Date | |

12. Velocity of sample gas (ft/sec)

$$V_{s} = (K_{p})(C_{p})\left(\sqrt{\Delta P}\right)\left(\sqrt{\frac{(\overline{T_{s}} + 460)}{(M_{s})(P_{s})}}\right)$$

Where:

| ۷ | VIICIC. | | | | |
|---|----------------|---|---|--------|------------|
| | К _р | = velocity pressure constant | = | 85.49 | |
| | Cp | = pitot tube coefficient | = | 0.81 | |
| | Ms | = wet molecular weight of sample gas, wet basis (lb/lb·mole) | = | 27.45 | lb/lb·mole |
| | Ps | = absolute sample gas pressure (in. Hg) | = | 29.27 | in. Hg |
| | Τ _s | = average sample gas temperature (°F) | = | 307.48 | °F |
| | V∆P | \Rightarrow average square roots of velocity heads of sample gas (in. H ₂ O) | = | 0.782 | √in. H₂O |
| | 460 | = °F to °R conversion constant | = | 460 | |
| | | | | | |
| | Vs | ≈ sample gas velocity (ft/sec) | = | 52.59 | ft/sec |
| | | | | | |

13. Volumetric flow rate of sample gas at actual gas conditions (acfm)

$$Q_a = (60)(A_s)(V_s)$$

Wh

| where: | | | | |
|----------------|--|---|---------|-----------------|
| As | = cross sectional area of sampling location (ft ²) | = | 64.00 | ft ² |
| Vs | = sample gas velocity (ft/sec) | = | 52.59 | ft/sec |
| 60 | conversion factor (sec/min) | = | 60 | sec/min |
| Q _a | = volumetric flow rate at actual conditions (acfm) | = | 201,928 | acfm |

14. Total flow of sample gas (scfm)

 $= (Q_a) \left(\frac{P_s}{29.92} \right) \left(\frac{68 + 460}{T_s + 460} \right)$ Q_s

Where:

| Qa | = volumetric flow rate at actual conditions (acfm) | = | 201,928 | acfm |
|---------------------------|---|---|---------|--------|
| Ps | = absolute sample gas pressure (in. Hg) | = | 29.27 | in. Hg |
| 29.92 | = standard pressure (in. Hg) | = | 29.92 | in. Hg |
| Ts | = average sample gas temperature (°F) | = | 307.5 | °F |
| 68 | | = | 68 | °F |
| 460 | = °F to °R conversion constant | = | 460 | |
| $\mathbf{Q}_{\mathbf{s}}$ | ⇒ volumetric flow rate at standard conditions, wet basis (scfm) | = | 135,904 | scfm |

15. Dry flow of sample gas (dscfm)

 $= (\mathcal{Q}_s)(1 - B_w)$ Q_{std}

Where:

| B _w Q _s | proportion of water vapor in the gas stream by volume volumetric flow rate at standard conditions, wet basis (scfm) | = | 0.2043 135,904 | scfm |
|----------------------------------|--|---|-------------------|-------|
| Q _{std} | = volumetric flow rate at standard conditions, dry basis (dscfm) | = | 108,134 | dscfm |

16. Dry flow of sample gas corrected to 7%O₂ (dscfm)

$$Q_{std7} = (Q_{std}) \left(\frac{20.9 - O_2}{20.9 - 7} \right)$$
Where:
 $Q_{std} = volumetric flow rate at standard conditions, dry basis (dscfm) = 108,134$
 $O_2 = proportion of oxygen in the gas stream by volume (%) = 10.1$
 $^120.9 = oxygen content of ambient air (%) = 20.9$
 $7 = oxygen content of corrected gas (%) = 7.0$
 $Q_{std7} = volumetric flow rate at STP and 7%O_2, dry basis (dscfm) = 84,251$

17. Hourly time basis conversion of volumetric flow rate (Q_{std} example)

$$Q_{std-hr} = (Q_{std-min})(60)$$

Where

| Q _{std-min} 60 | volumetric flow rate, english units (ft³/min) conversion factor (min/hr) | = | 108,134 60 | dscfm min/hr |
|----------------------------|--|---|---------------|-----------------|
| Q _{std-hr} | = volumetric flow rate, hourly basis (dscf/hr) | = | 6,488,019 | dscf/hr |

18. Metric Conversion of Gas Volumes (Q_{std} example)

 $= \left(Q_{std-english} \right) \left(\frac{60}{35.31} \right)$ $Q_{std-metric}$ Where: Q_{std-english}

dscfm = volumetric flow rate, english units (ft³/min) 108,134 35.31 = conversion factor (ft³/m³) 35.31 ft³/m³ 60 = conversion factor (min/hr) 60 min/hr =

 $Q_{\text{std-metric}}$ = volumetric flow rate, metric units (m³/hr) 183,745 dry std m3/hr =

19. Standard to Normal Conversion of Gas Volumes (Qstd example)

$$Q_{Normal} = \left(Q_{sd-metric}\right) \left(\frac{32+460}{68+460}\right)$$

M(horo)

| Q _{Normal} | = volumetric flow rate, metric units (dry Nm³/hr) | = | 171,216 | dry Nm³/hr | |
|-------------------------|---|---|---------|---------------|--|
| 460 | = standard temperature in Rankine (68°F) | = | 460 | | |
| 68 | standard temperature (°F) | = | 68 | °F | |
| 32 | = normal temperature (°F) | = | 32 | °F | |
| Q _{std-metric} | = volumetric flow rate, metric units (dry std m ³ /hr) | = | 183,745 | dry std m³/hr | |

EPA Method 1-4 Calculations

dscfm % % %

dscfm

20. Percent isokinetic (%)

| _ (0 | (0.0945 | $(\overline{T_s} +$ | 460 | (V _{mstd}) |
|------|--------------|---------------------------------|---------------|----------------------|
| - | $(P_s)(V_s)$ | $\frac{(D_n)^2(\pi)}{(144)(4)}$ | <u>(</u> ()() | $\overline{1-B_w}$ |

Where:

I

| Dn | = diameter of nozzle (in) | = | 0.270 | in. |
|-------------------|--|---|--------|--------|
| Bw | = proportion of water vapor in the gas stream by volume | = | 0.2043 | |
| Ps | = absolute sample gas pressure (in. Hg) | = | 29.27 | in. Hg |
| Ts | = average sample gas temperature (°F) | = | 307.5 | °F |
| V _{mstd} | volume of gas sample through the dry gas meter at standard conditions (dscf) | Ξ | 84.183 | dscf |
| Vs | = sample gas velocity (ft/sec) | = | 52.59 | ft/sec |
| θ | = total sampling time (min) | = | 125 | min |
| 0.0945 | = conversion constant | = | 0.0945 | |
| 460 | = °F to °R conversion constant | = | 460 | |
| | | | | |
| 1 | = percent of isokinetic sampling (%) | = | 100.31 | % |

21. Alternative Method 5 Post-Test Meter Calibration Factor

| Y_{qa} Where: | $= \frac{\Theta}{V_m} \sqrt{\frac{(0.0319)(T_m + 460)(28.96)}{(\Delta H_{@})(P_{bar} + \frac{\Delta H}{13.6})(M_d)}} (\sqrt{\Delta H})_{avg}$ | | | |
|--------------------|---|---|--------|----------------------------|
| θ | = total sampling time (min) | = | 125 | min |
| Vm | = volume of gas sample through the dry gas meter at meter conditions (dcf) | × | 84.67 | dcf |
| Tm | = average dry gas meter temperature (°F) | = | 69.90 | ۴F |
| ∆H _@ | = dry gas meter orifice coefficient | = | 1.7516 | |
| Pbar | = barometric pressure (in. Hg) | = | 30.05 | in. Hg |
| ΔH | = average pressure drop across meter box orifice (in. H ₂ O) | = | 1.460 | in. H ₂ O |
| Md | = dry molecular weight of sample gas (lb/lb·mole) | = | 29.88 | lb/lb·mole |
| √∆H _{avg} | = average of square root of pressure drop across meter orifice | = | 1.204 | √in. H₂O |
| 0.0319 | = conversion constant | = | 0.0319 | - |
| 28.96 | = molecular weight of ambient air (lb/lb-mole) | = | 28.96 | lb/lb-mole |
| 13.6 | = conversion factor (in. H_2O/in . Hg) | = | 13.6 | in.H ₂ O/in. Hg |
| 460 | \approx °F to °R conversion constant | = | 460 | _ |
| Y _{qa} | = alternative Method 5 post-test meter calibration factor | = | 0.9897 | |

USEPA Method 5/29 Filterable Particulate Gravimetric Analysis Calculations

Sample data taken from Run 1

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Note: The tables presenting the results are generated electronically from raw data. It may not be possible to exactly duplicate these results using a calculator. The reference method data, results, and all calculations are carried to sixteen decimal places throughout. The final table is formatted to an appropriate number of significant figures.

1. Total residue from gravimetric analysis of filters (g)

 $=\sum_{i=1}^n m_{fi}$

Where:

r_{si}

| m _{ft} | = residual mass of filter "1" from gravimetric analysis (g) | = | 0.00180 | g |
|-----------------|---|---|---------|---|
| m _{f2} | = residual mass of filter "2" from gravimetric analysis (g) | = | 0.00000 | g |
| m _{r3} | = residual mass of filter "3" from gravimetric analysis (g) | = | 0.00000 | g |
| m _{f4} | = residual mass of filter "4" from gravimetric analysis (g) | = | 0.00000 | g |
| | | | | |
| m _{fr} | = total filter residue from gravimetric analysis (g) | = | 0.00180 | g |

2. Total particulate collected on filters (g)

| m_{filter} | $= m_{fr}$ if $m_{fr} \ge 0$ | | | |
|---------------------------|--|---|---------|---|
| m _{filter} | $= 0$ if $m_{fr} < 0$ | | | |
| Where: m _{fr} | = total filter residue from gravimetric analysis (g) | = | 0.00180 | g |
| m _{filter} | = total particulate collected on filters (g) | = | 0.00180 | g |

3. Solvent rinse - sample residue mass (g)

$$= \left(r_{ai}\right) \left(\frac{v_{si}}{v_{ai}}\right)$$

| Where: | | | Acetone | | |
|-----------------|--|---|---------|----|--|
| r _{ai} | = aliquot residue mass for solvent "i" (g) | = | 0.00280 | g | |
| Vsł | = sample liquid volume for solvent rinse "i" (ml) | = | 98.0 | ml | |
| Vai | = aliquot liquid volume for solvent rinse "i" (ml) | = | 98.0 | mi | |
| r _{si} | = solvent rinse "i" - sample residue mass (g) | = | 0.00280 | g | |

4. Solvent ririse - blank residue (g)

| m _{i-blank} | $= r_{ai-blank}$ if $r_{ai-blank} \ge 0$ | | | | |
|---------------------------------|---|---|--------------------|---|--|
| m _{i-blank} | $= 0$ if $r_{ai-blank} < 0$ | | | | |
| Where: r _{al-blank} | = blank residue for solvent "i" from gravimetric analysis (g) | = | Acetone 0.00080 | g | |
| m _{l-blank} | ≓ solvent rinse - blank residue (g) | = | 0.00080 | g | |

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5. Solvent rinse - maximum allowable blank correction (g)

m_{bi} Where

| Nhere: | | | Acetone | | |
|----------------------|--|---|---------|------|--|
| m _{i-blank} | = solvent rinse - blank residue (g) | = | 0.00080 | g | |
| Vsi | = sample liquid volume for solvent rinse "i" (ml) | = | 98.0 | ៣ | |
| Val-blank | = blank liquid volume for solvent rinse "i" (ml) | = | 139.0 | ml | |
| 0.00001 | = EPA M5 fraction of total rinse that can be subtracted (g) | = | 0.00001 | g | |
| ρ | = density of solvent rinse "i" (g/ml) | = | 0.7845 | g/mł | |
| Г _{SI} | = solvent rinse "i" - sample residue mass (g) | = | 0.00280 | g | |
| | | | 0 00050 | | |
| ты | = solvent rinse "i" - maximum allowable blank correction (g) | = | 0.00056 | g | |

6. Solvent rinse - net residue (g)

 $m_i = (r_{si} - m_{bi}) \text{ if } r_{si} \ge m_{bi}$ $m_i = 0 \quad \text{ if } r_{si} < m_{bi}$

Where:

| Where: r _{si} m _{bi} | = solvent rinse "i" - sample residue mass (g) = solvent rinse "i" - maximum allowable blank correction (g) | | Acetone 0.00280 0.00056 | 0 |
|--|---|---|-------------------------------|---|
| m, | = solvent rinse "i" - net residue (g) | = | 0.00224 | g |

7. Total solvent residue - (g)

 $=\sum_{i=1}^{n}m_{i}$

Where:

ms

| r | n ₁ n ₂ n ₃ | = solvent rinse "1" - net residue (g) = solvent rinse "2" - net residue (g) = solvent rinse "3" - net residue (g) | = = = | 0.00224 N/A N/A | g g g | |
|---|--|---|-------------|-----------------------|-------------|--|
| ٢ | ns | = total solvent residue (g) | = | 0.00224 | g | |

8. Total gravimetric result (g)

| m_T | $= m_{filter} + m_s$ | | | | |
|---------------------|--|---|---------|---|--|
| Where: | | | | | |
| m _{fliter} | = total particulate collected on filters (g) | 2 | 0.00180 | g | |
| m _s | = total solvent residue (g) | = | 0.00224 | g | |
| mτ | = total gravimetric result (g) | = | 0.00404 | g | |

9. Total gravimetric detection limit (g)

$$m_D = (MDL_{filter})(n_f) + (MDL_{rinse})(n_r)$$

Where:

| MDL _{filter} | minimum detection limit for single filter analysis (g) number of filters in analysis | = | 0.00050 | g |
|--|---|---|--------------|---|
| MDL _{rinse} n _r | number of meta in analysis minimum detection limit for single rinse analysis (g) number of rinses in analysis | = | 0.00050 1 | g |
| m _D | = total gravimetric detection limit (g) | = | 0.00020 | g |

10. Total particulate matter (g)

| m _n | $= MAXIMUM[m_{T} or < m_{D}]$ | | | |
|----------------|---|---|---------|---|
| Where: | | | | |
| mτ | = total gravimetric result (g) | = | 0.00404 | g |
| mp | = total gravimetric detection limit (g) | = | 0.00020 | g |
| | | | | - |
| m | = total particulate matter (g) | = | 0.00404 | g |

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USEPA Method 5/29 Filterable Particulate Sample Calculations

USEPA Method 5/29 Filterable Particulate Sample Calculations

Sample data taken from Run 1

Note: The tables presenting the results are generated electronically from raw data. It may not be possible to exactly duplicate these results using a calculator. The reference method data, results, and all calculations are carried to sixteen decimal places throughout. The final table is formatted to an appropriate number of significant figures.

1. Particulate concentration (lb/dscf)

$$C_{sd} = \left(\frac{m_n}{V_{mstd}}\right) \left(2.205 \times 10^{-3}\right)$$

Where:

| m _n V _{mstd} 2.205 x 10 ⁻³ | = total particulate matter (g) = volume metered, standard (dscf) = conversion factor (lb/g) | 11 11 | 84.1826 | g dscf Ib/g |
|---|---|-------|------------|-------------------|
| C _{sd} | = particulate concentration (lb/dscf) | = | 1.0571E-07 | lb/dscf |

2. Particulate concentration (gr/dscf)

$$C_{sd} = \left(\frac{m_n}{V_{mstd}}\right) (15.43)$$

Where

| m _n | = total particulate matter (g) | = | 0.00404 | g |
|-------------------|---------------------------------------|---|---------|---------|
| V _{mstd} | = volume metered, standard (dscf) | = | 84.1826 | dscf |
| 15.43 | = conversion factor (gr/g) | = | 15.43 | gr/g |
| C _{sd} | = particulate concentration (gr/dscf) | = | 0.00074 | gr/dscf |

3. Particulate concentration (mg/dscm)

$$C_{sd} = \left(\frac{m_n}{V_{msid}}\right) (1000) (35.31)$$

Where: 0.00404 = total particulate matter (g) = m g V_{mstd} = volume metered, standard (dscf) = 84.1826 dscf 1.000 1,000 = conversion factor (mg/g) = mg/g 35.31 = conversion factor (dscf/dscm) 35.31 dscf/dscm = C_{sd} = particulate concentration (mg/dscm) 1.69287 mg/dscm =

041210 135959 к_к

4. Particulate concentration (mg/Nm³ dry)

$$C_{sd} = \left(\frac{m_n}{V_{mstd}}\right) (1000) (35.31) \left(\frac{68+460}{32+460}\right)$$
(here:

W

| mn | = total particulate matter (g) | = | 0.00404 | g |
|-------------------|-----------------------------------|---|---------|-----------|
| V _{mstd} | = volume metered, standard (dscf) | = | 84.1826 | dscf |
| 1,000 | = conversion factor (mg/g) | = | 1,000 | mg/g |
| 35.31 | = conversion factor (dscf/dscm) | = | 35.31 | dscf/dscm |
| 68 | = standard temperature (°F) | = | 68 | °F |
| 32 | = normal temperature (°F) | = | 32 | °F |
| 460 | = °F to °R conversion constant | = | 460 | |
| | | | | |

 C_{sd} 1.81674 = particulate concentration (mg/Nm³ dry) = mg/Nm³ dry

5. Particulate concentration corrected to x% O2 (gr/dscf example)

$$C_{sdx} = C_{sd} \left(\frac{20.9 - x}{20.9 - O_2} \right)$$

| Where: | | | | | |
|----------------|--|---|---------|---------|--|
| Csd | = particulate concentration (gr/dscf) | = | 0.00074 | gr/dscf | |
| x | = oxygen content of corrected gas (%) | = | 7.0 | % | |
| O ₂ | = proportion of oxygen in the gas stream by volume (%) | = | 10.1 | % | |
| 20.9 | = oxygen content of ambient air (%) | = | 20.9 | % | |
| | | | | | |

= particulate concentration corrected to x%O2 (gr/dscf) gr/dscf @ x%O2 Csdx = 0.00095

6. Particulate concentration corrected to y% CO2 (gr/dscf example)

$$C_{sdy} = C_{sd} \left(\frac{y}{CO_2} \right)$$

w

| Where: | | | | |
|------------------|--|---|---------|-----------------------------|
| C _{sd} | = particulate concentration (gr/dscf) | = | 0.00074 | gr/dscf |
| у | = carbon dioxide content of corrected gas (%) | = | 12.0 | % |
| CO₂ | = proportion of carbon dioxide in the gas stream by volume (%) | = | 9.3 | % |
| C _{sdy} | = particulate concentration corrected to y%CO2 (gr/dscf) | = | 0.00096 | gr/dscf @ y%CO ₂ |

7. Particulate concentration at actual gas conditions (gr/acf example)

$$C_a = C_{sd} \left(\frac{\mathcal{Q}_{std}}{\mathcal{Q}_a} \right)$$

| C _{sd} Q _{std} Q _a | particulate concentration (gr/dscf) volumetric flow rate at standard conditions, dry basis (dscfm) volumetric flow rate at actual conditions (acfm) | = = = | 0.00074 108,134 201,928 | gr/dscf dscfm acfm | |
|---|---|-------------|-------------------------------|--------------------------|--|
| Ca | = particulate concentration at actual gas conditions (gr/acf) | = | 0.00040 | gr/acf | |

USEPA Method 5/29 Filterable Particulate Sample Calculations

0.6859

=

lb/hr

8. Particulate rate (lb/hr)

$$E_{lb/hr} = \left(\frac{m_n}{V_{mstd}}\right) (2.205 \times 10^{-3}) (Q_{std}) (60)$$

Where:

| mn | ≈ total particulate matter (g) | = | 0.00404 | g |
|--------------------------|--|---|-----------|--------|
| V _{mstd} | = volume metered, standard (dscf) | = | 84.1826 | dscf |
| 2.205 x 10 ⁻³ | = conversion factor (lb/g) | = | 2.205E-03 | lb/g |
| Q _{std} | = volumetric flow rate at standard conditions, dry basis (dscfm) | = | 108,134 | dscfm |
| 60 | = conversion factor (min/hr) | = | 60 | min/hr |
| | | | | |

E_{lb/hr}

9. Particulate rate (kg/hr) $= \left(\frac{m_n}{V_{mstd}}\right) \left(\frac{(Q_{std})(60)}{1000}\right)$

= particulate rate (lb/hr)

Where:

 $E_{kg/hr}$

| WINGIG. | | | | |
|--------------------|--|---|---------|--------|
| m _n | = total particulate matter (9) | = | 0.00404 | g |
| V _{mstd} | = volume metered, standard (dscf) | = | 84.1826 | dscf |
| Q _{std} | = volumetric flow rate at standard conditions, dry basis (dscfm) | = | 108,134 | dscfm |
| 60 | = conversion factor (min/hr) | = | 60 | min/hr |
| 1,000 | = conversion factor (g/kg) | = | 1,000 | g/kg |
| E _{kg/hr} | = particulate rate (kg/hr) | = | 0.3111 | kg/hr |

10. Particulate rate (Ton/yr)

$$E_{T/yr} = \left(\frac{m_n}{V_{mstd}}\right) (2.205 \times 10^{-3}) (\mathcal{Q}_{std}) (60) \left(\frac{Cap}{2000}\right)$$

Where:

| WINCIC. | | | | | |
|--------------------------|--|---|-----------|----------|--|
| mn | = total particulate matter (g) | = | 0.00404 | g | |
| V _{mstd} | = volume metered, standard (dscf) | = | 84.1826 | dscf | |
| 2.205 x 10 ⁻³ | = conversion factor (lb/g) | = | 2.205E-03 | lb/g | |
| Q _{std} | = volumetric flow rate at standard conditions, dry basis (dscfm) | = | 108,134 | dscfm | |
| 60 | = conversion factor (min/hr) | = | 60 | min/hr | |
| Сар | = capacity factor for process (hours operated/year) | = | 8,760 | hours/yr | |
| 2,000 | = conversion factor (lb/Ton) | = | 2,000 | lb/Ton | |
| | | | | | |
| E⊺/yr | = particulate rate (Ton/yr) | = | 3.0041 | Ton/yr | |
| - | | | | - | |

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11. Particulate rate - F_d-based (lb/MMBtu)

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$$E_{Fd} = \left(\frac{m_n}{V_{mstd}}\right) \left(2.205 \times 10^{-3}\right) \left(F_d\right) \left(\frac{20.9}{20.9 - O_2}\right)$$
Where:
m_n = total particulate matter (g) = 0.00404 g
V_{mstd} = volume metered, standard (dscf) = 84.1826 dscf
2.205 x 10^3 = conversion factor (lb/g) = 2.205E-03 lb/g
F_d = ratio of gas volume to heat content of fuel (dscf/MMBtu) = 9,570 dscf/MMBtu
O_2 = proportion of oxygen in the gas stream by volume (%) = 10.1 %
20.9 = oxygen content of ambient air (%) = 20.9 %
E_{Fd} = particulate rate - F_d - based (lb/MMBtu) = 0.00195 lb/MMBtu
mticulate rate - F_c-based (lb/MMBtu)

12. Pa

$$E_{Fc} = \left(\frac{m_n}{V_{mstd}}\right) (2.205 \times 10^{-3}) (F_c) \left(\frac{100}{CO_2}\right)$$

Where:

| m _n | = total particulate matter (g) | = | 0.00404 | g | |
|-------------------|--|---|-----------|------------|--|
| V _{mstd} | = volume metered, standard (dscf) | = | 84.1826 | dscf | |
| 2.205 x 10 | ³ = conversion factor (lb/g) | = | 2.205E-03 | lb/g | |
| Fc | = ratio of gas volume to heat content of fuel (dscf/MMBtu) | = | 1,820 | dscf/MMBtu | |
| CO ₂ | = proportion of oxygen in the gas stream by volume (%) | = | 9.3 | % | |
| 100 | = conversion factor | = | 100 | | |
| | | | | | |
| EFc | = particulate rate - F _c - based (lb/MMBtu) | = | 0.00208 | lb/MMBtu | |
| | | | | | |

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LOGIC FOR TREATING DETECTION LIMITS

(mercury only)

1. Logic for Determining Total Blank (mTotal-B) from 5 Fractions

| | CASE 1 All 5 fractions are D. | CASE 2 1 to 4 fractions are ND | CASE 3 All 5 fractions are ND |
|----------------|-----------------------------------|-----------------------------------|-------------------------------------|
| Rule ND ≈ 0 | m _{Total-B} = Sum D, 1-5 | m _{Tota⊩B} = Sum D | m _{Total-B} = < Sum ND |
| | m _{Total-B} = Sum D, 1-5 | m _{TotaFB} = Sum D | m _{Total-B} = < Sum ND |
| ND≓0.5x | m _{Total-B} = Sum D, 1-5 | m _{⊤otal-B} = Sum D | m _{Total-B} = < 0.5 Sum ND |

2. Logic for Determining Total Sample (m_{Total-S}) from 5 Fractions

| | CASE 1 | CASE 2 | CASE 3 |
|---------|-----------------------------------|--|--|
| | All 5 fractions are D. | 1 to 4 fractions are ND | All 5 fractions are ND |
| Rule | m - Sum D 1.5 | | m _{Total-S} = < Sum ND |
| ND ≠ 0 | m _{Total-S} = Sum D, 1-5 | m _{Total-S} = Sum D | |
| ND=1x | m _{Total-S} = Sum D, 1-5 | m _{Total-S} = < [Sum D + Sum ND | |
| ND=0.5x | m _{Total-S} = Sum D, 1-5 | m _{Total-S} = < [SumD+0.5 SumN | $D_{m_{Total-S}} = < 0.5 \text{ Sum ND}$ |

3. Logic for Determining Maximum Allowable Blank Correction (m_{T-B-allow})

| | CASE 1 All 5 fractions are D. m _{Total-B} = D | CASE 2 1 to 4 sample fractions are ND m _{Total-B} = D | | CASE 4 Any type of fractions m _{Total-B} = ND |
|--------|---|--|----------------------------|--|
| Rule | | | | |
| ND = 0 | m _{T-B-allow} = M29 Rule | m _{T-B-allow} = M29 Rule | $m_{T-B-allow} = 0$ | m _{T-B-allow} ≈ 0 |
| ND=1x | m _{T-B-allow} = M29 Rule | | m _{T-B-allow} = 0 | $m_{T-B-allow} = 0$ |
| | m _{T-B-allow} = M29 Rule | | $m_{T-B-allow} = 0$ | $m_{T-B-allow} = 0$ |

* M29 rule using only detected sample quantities for logical comparisons.

4. Logic for Determining Blank-Corrected Sample Amount (mn)

| | CASE 1 All 5 fractions are D. $m_{Total-S} \sim m_{T-B-allow} \ge MIN(MDL)$ | $\begin{array}{l} \textbf{CASE 2} \\ \textbf{1 to 4 sample fractions are ND} \\ \textbf{m}_{\text{Total-S}} \text{ - } \textbf{m}_{\text{T-B-ellow}} \geq MIN(MDL) \end{array}$ | | CASE 4 Any type of fractions m _{Total-S} - m _{T-B-allow} < MIN(MDL) |
|------------|---|---|---|---|
| Rule | | | | |
| ND = 0 | $m_n = m_{Total-S} - m_{T-B-allow}$ | $m_n = m_{Total-S} - m_{T-B-allow}$ | m _n = < m _{Total-S} | $m_n = \langle MIN[MDL]$ |
| ND=1x | $m_n = m_{Total-S} - m_{T-B-allow}$ | $m_n = \langle [m_{Total-S} - m_{T-B-allow}]$ | $m_n = < m_{Total-S}$ | m _n = < MIN[MDL] |
| ND=0.5x | $m_n = m_{Total-S} - m_{T-B-allow}$ | $m_n = < [m_{Total-S} - m_{T-B-allow}]$ | m _n = < m _{Total-S} | m _n = < MIN[MDL] |
| Laborator | y Data | | | |
| | m _n | Net matter collected (g) | | |
| Filterable | Particulate Results | | | |
| | C _{sd} | Particulate Concentration (mg/dscn | n) | |
| | C _{sd7} | Particulate Concentration @7% O2 | (mg/dscm) | |

Definitions and Notes

The term "Rule" refers to the rule being implemented for handling non-detectable quantities in summations. MDL = minimum detection limit.

D = Detectable quantity reported as D.

ND = Non-Detectable quantity reported at a value of ND.

MIN[MDL] = lowest quantity of all detection limits for 5 fractions.

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USEPA Method 5/29 Mercury Analyte Calculations

Sample data taken from Run 1

Note: The tables presenting the results are generated electronically from raw data. It may not be possible to exactly duplicate these results using a calculator. The reference method data, results, and all calculations are carried to sixteen decimal places throughout. The final table is formatted to an appropriate number of significant figures.

Note: Please see the preceding page concerning treatment of minimum detection limits and mathematical operations on values that are below minimum detection limits.

1. Total blank amount (µg)

 $m_{total-B}$

 $=\sum_{i=1}^n m_{i-B}$

| Where: | | | | | |
|----------------------|---|---|---------|----|--|
| m _{1b-B} | = mercury amount in blank for Fraction 1b | = | <0.1000 | μg | |
| m _{2b-B} | = mercury amount in blank for Fraction 2b | = | <0.2000 | μg | |
| m _{3a-B} | = mercury amount in blank for Fraction 3a | = | <0.2000 | μg | |
| m _{зь-В} | = mercury amount in blank for Fraction 3b | = | <0.5000 | μg | |
| т _{зс-В} | = mercury amount in blank for Fraction 3c | = | <0.4000 | þð | |
| m _{total-B} | = total amount of mercury in blank | = | <1.4000 | μg | |

2. Total sample amount (µg)

$$= \sum_{i=1}^{n} m_{i-s}$$

Where:

m_{total - S}

| Where: | | | | | |
|----------------------|--|---|---------|----|--|
| m _{1b-S} | = mercury amount in sample for Fraction 1b | = | <0.1000 | μg | |
| m _{2b-S} | = mercury amount in sample for Fraction 2b | = | 9.1977 | μg | |
| m _{3a-S} | = mercury amount in sample for Fraction 3a | = | <0.2000 | μg | |
| m _{3b-S} | = mercury amount in sample for Fraction 3b | = | <0.5000 | μg | |
| m _{3c-S} | = mercury amount in sample for Fraction 3c | = | <0.4000 | μg | |
| m _{total-S} | = total amount of mercury in sample | = | 9.1977 | μg | |

3. Allowable blank correction (µg)

 $m_{T-B-allow}$

 $= m_{iolal-B} \text{ if } m_{iolal-B} \le 0.6$

$$m_{T-B-allow} = MAX \left[0.6, MIN \left(m_{ioial-B}, 0.05 \times m_{ioial-S}\right)\right] \text{ if } m_{ioial-B} > 0.6$$

Laboratory Data

m Net matter collected (g)

Filterable Particulate Results

C Particulate Concentration (mg/dscm)

C Particulate Concentration @7% O2 (mg/dscm)

| Where: |
|--------|
|--------|

| m _{total-8} | = total amount of mercury in blank | Ξ | <1.4000 | μg | |
|-----------------------------|--|---|---------|----|--|
| m _{total-S} | = total amount of mercury in sample | = | 9.1977 | μġ | |
| 0.05 x m _{total-S} | = 5% of m _{total-S} | = | 0.4599 | μg | |
| MAX | = arithmetic operator that returns the maximum of two values | | | | |
| MIN | = arithmetic operator that retums the minimum of two values | | | | |
| | | | | | |
| m _{T-B-allow} | = total allowable blank correction | = | 0.0000 | μg | |
| | | | | | |

NOTE: In this case, the second criteria applies.

4. Sample corrected for allowable blank - Total (µg)

| m _n | $= m_{total-S} - m_{T-B-allow}$ | | |
|------------------------|---|---|--------|
| Where: | | | |
| m _{total-S} | = total amount of mercury in sample | = | 9.1977 |
| m _{T-B-allow} | = total allowable blank correction | = | 0.0000 |
| m _n | = total mercury in sample corrected for allowable blank | = | 9.1977 |

5. Sample corrected for allowable blank - Prorated for each fraction (µg)

 (m_n)

$$m_{n-i} = \left(\frac{m_{i-S}}{m_{total-S}}\right)$$

Where:

| Where: | | | | |
|----------------------|--|---|---------|----|
| mn | total mercury in sample corrected for allowable blank | = | 9.1977 | μg |
| m _{1b-S} | = mercury amount in sample for Fraction 1b | = | <0.1000 | μg |
| m _{2b-S} | = mercury amount in sample for Fraction 2b | = | 9.1977 | μg |
| m _{3a-S} | = mercury amount in sample for Fraction 3a | = | <0.2000 | μg |
| m _{3b-S} | = mercury amount in sample for Fraction 3b | = | <0.5000 | μg |
| m _{3c-S} | = mercury amount in sample for Fraction 3c | = | <0.4000 | μg |
| m _{total-S} | = total amount of mercury in sample | = | 9.1977 | μg |
| m _{n-1b} | = mercury corrected for blank - prorated for Fraction 1b | = | <0.1000 | μg |
| m _{n-2b} | = mercury corrected for blank - prorated for Fraction 2b | = | 9.1977 | μg |
| m _{n-3a} | = mercury corrected for blank - prorated for Fraction 3a | = | <0.2000 | μg |
| m _{n-3b} | = mercury corrected for blank - prorated for Fraction 3b | = | <0.5000 | μg |
| m _{n-3c} | = mercury corrected for blank - prorated for Fraction 3c | = | <0.4000 | μg |
| | | | | |

hð hð

μg

USEPA Method 5/29 Mercury Sample Calculations

USEPA Method 5/29 Mercury Sample Calculations

Sample data taken from Run 1

Note: The tables presenting the results are generated electronically from raw data. It may not be possible to exactly duplicate these results using a calculator. The reference method data, results, and all calculations are carried to sixteen decimal places throughout. The final table is formatted to an appropriate number of significant figures.

| 1. Mercury concentra | ation (lb/dscf) | | | | 041210 140248 K_K |
|--|--|---|------------|------------|----------------------|
| C_{sd} | $= \left(\frac{m_n}{V_{msid}}\right) \left(\frac{2.205 \times 10^{-3}}{10^6}\right)$ | | | | |
| Where: | | | | | |
| m _n | = mercury collected in sample (total µg) | = | 9.1977 | hð | |
| V _{mstd} | = volume metered, standard (dscf) | = | 84.1826 | dscf | |
| 2.205 x 10 ⁻³ | = conversion factor (lb/g) | = | 2.205E-03 | lb/g | |
| 10 ⁶ | = conversion factor (μg/g) | = | 1.0E+06 | µg/g | |
| Ċsd | = mercury concentration (lb/dscf) | = | 2.4092E-10 | lb/dscf | |
| 2. Mercury concentra | ation (µg/dscm) | | | | |
| | $\left(\frac{m_n}{V_{mstd}}\right)(35.31)$ | | | | |
| Where: m _n | = mercury collected in sample (total µg) | * | 9.1977 | | |
| V _{mstd} | = volume metered, standard (dscf) | - | | µg dscf | |
| 35.31 | | - | 84.1826 | | |
| 30.31 | = conversion factor (dscf/dscm) | = | 35.31 | dscf/dscm | |
| C _{sd} | = mercury concentration (µg/dscm) | = | 3.8579E+00 | µg/dscm | |
| 3. Mercury concentra | tion (mg/dscm) | | | | |
| $C_{sd} = ($ | $\left(\frac{m_n}{V_{myd}}\right)\left(\frac{35.31}{1000}\right)$ | | | | |
| Where: | | | | | |
| m _n | = mercury collected in sample (total µg) | = | 9.1977 | hð | |
| V _{mstd} | = volume metered, standard (dscf) | = | 84.1826 | dscf | |
| Laboratory Data m Net matter collecte | d (g) | | | | |
| Filterable Particulate Res | sults | | | | |
| C Particulate Concen | | | | | |
| | tration @7% O ₂ (mg/dscm) | | | | |
| 35.31 | = conversion factor (dscf/dscm) | = | 35.31 | dscf/dscm | |
| 1000 | = conversion factor (µg/mg) | = | | µg/mg | |
| C _{sd} | = mercury concentration (mg/dscm) | = | 3.8579E-03 | mg/dscm | |

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4. Mercury concentration (µg/Nm3 dry) $=\left(\frac{m_n}{V_{11}}\right)(35.31)\left(\frac{68+460}{32+460}\right)$ C_{sd} Where: = mercury collected in sample (total µg) 9.1977 = μq mn = volume metered, standard (dscf) 84.1826 dscf V_{mstd} = 35.31 dscf/dscm 35.31 = conversion factor (dscf/dscm) = = standard temperature (°F) 68 °F 68 32 ≈ normal temperature (°F) 32 °F 460 = °F to °R conversion constant 460 C_{sd} = mercury concentration (µg/Nm3 dry) 4.1402E+00 µg/Nm³ dry = 5. Mercury concentration corrected to x% oxygen (lb/dscf example) $= C_{sd} \left(\frac{20.9 - x}{20.9 - O_2} \right)$ C_{sdx} Where: = mercury concentration (lb/dscf) 2.4092E-10 lb/dscf C_{sd} = oxygen content of corrected gas (%) 7.0 % x 02 = proportion of oxygen in the gas stream by volume (%) 10.1 % % 20.9 = oxygen content of ambient air (%) 20.9 3.0921E-10 lb/dscf @ x%O2 Csdx = mercury concentration corrected to x% oxygen (lb/dscf) = 6. Mercury concentration corrected to y% carbon dioxide (lb/dscf example) $=C_{sd}\left(\frac{y}{CO_2}\right)$ C_{sdy} Where: = mercury concentration (lb/dscf) 2.4092E-10 lb/dscf C_{sd} = carbon dioxide content of corrected gas (%) 12.0 % = proportion of carbon dioxide in the gas stream by volume (%) 9.3 % CO_2 = Csdy 3.1254E-10 lb/dscf @ y%CO2 = mercury conc. corrected to y% carbon dioxide (lb/dscf) = 7. Mercury concentration at actual gas conditions (lb/acf example) $= C_{sd} \left(\frac{Q_{std}}{Q_a} \right)$ С, Where: = mercury concentration (lb/dscf) 2.4092E-10 lb/dscf C_{sd} = volumetric flow rate at standard conditions, dry basis (dscfm) 108,134 dscfm Q_{std} = volumetric flow rate at actual conditions (acfm) 201,928 acfm Q, =

C_a = mercury concentration at actual gas conditions (lb/acf) = 1.2901E-10 lb/acf

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8. Mercury emission rate (lb/hr)

$$E_{lb/hr} = \left(\frac{m_n}{V_{mstd}}\right) \left(\frac{2.205 \times 10^{-3}}{10^6}\right) (Q_{std}) (60)$$

Where:

| m _n | = mercury collected in sample (total µg) | = | 9.1977 | μg |
|--------------------------|--|---|-----------|--------|
| V _{mstd} | = volume metered, standard (dscf) | = | 84.1826 | dscf |
| 2.205 x 10 ⁻³ | = conversion factor (lb/g) | = | 2.205E-03 | lb/g |
| 10 ⁶ | = conversion factor (μg/g) | Ξ | 1.0E+06 | µg/g |
| Q _{std} | = volumetric flow rate at standard conditions, dry basis (dscfm) | = | 108,134 | dscfm |
| 60 | = conversion factor (min/hr) | = | 60 | min/hr |
| | | | | |

E_{lb/hr} = mercury

= mercury emission rate (lb/hr) = 1.5631E-03 lb/hr

9. Mercury emission rate (g/s)

$$= \left(\frac{m_n}{V_{mstd}}\right) \left(\frac{Q_{std}}{(10^6)(60)}\right)$$

Where

 $E_{g/s}$

| Where: | | | | |
|-------------------|--|---|------------|---------|
| mn | = mercury collected in sample (total µg) | = | 9.1977 | μg |
| V _{mstd} | = volume metered, standard (dscf) | = | 84.1826 | dscf |
| Q _{std} | = volumetric flow rate at standard conditions, dry basis (dscfm) | = | 108,134 | dscfm |
| 10 ⁶ | = conversion factor (µg/g) | = | 1.0E+06 | µg/g |
| 60 | = conversion factor (sec/min) | = | 60 | sec/min |
| E | | | | |
| E _{g/s} | = mercury emission rate (g/s) | = | 1.9691E-04 | g/s |

10. Mercury emission rate (Ton/yr)

$$E_{T/yr} = \left(\frac{m_n}{V_{mstd}}\right) \left(\frac{2.205 \times 10^{-3}}{10^6}\right) (Q_{std}) (60) \left(\frac{Cap}{2000}\right)$$

| m _n | = mercury collected in sample (total µg) | = | 9.1977 | þg |
|--------------------------|--|---|------------|----------|
| V _{mstd} | volume metered, standard (dscf) | = | 84.1826 | dscf |
| 2.205 x 10 ⁻³ | = conversion factor (lb/g) | = | 2.205E-03 | lb/g |
| 10 ⁶ | = conversion factor (µg/g) | = | 1.0E+06 | hð\ð |
| Q _{std} | = volumetric flow rate at standard conditions, dry basis (dscfm) | = | 108,134 | dscfm |
| 60 | = conversion factor (min/hr) | = | 60 | min/hr |
| Cap | = capacity factor for process (hours operated/year) | = | 8,760 | hours/yr |
| 2000 | = conversion factor (lb/Ton) | = | 2000 | lb/Ton |
| | | | | |
| E _{T/yr} | = mercury emission rate (Ton/yr) | = | 6.8462E-03 | Ton/yr |
| | | | | |

= 4.4493E-06 lb/MMBtu

11. Mercury emission rate - Fd-based (lb/MMBtu)

$$E_{Fd} = \left(\frac{m_n}{V_{mstd}}\right) \left(\frac{2.205 \times 10^{-3}}{10^6}\right) \left(F_d\right) \left(\frac{20.9}{20.9 - O_2}\right)$$

Where:

| where: | | | | |
|--------------------------|--|---|-----------|------------|
| mn | ≍ mercury collected in sample (total µg) | = | 9.1977 | hð |
| V _{mstd} | = volume metered, standard (dscf) | = | 84.1826 | dscf |
| 2.205 x 10 ⁻³ | = conversion factor (lb/g) | = | 2.205E-03 | ib/g |
| 10 ⁶ | = conversion factor (μg/g) | = | 1.0E+06 | µg/g |
| Fd | = ratio of gas volume to heat content of fuel (dscf/MMBtu) | = | 9,570 | dscf/MMBtu |
| Oz | = proportion of oxygen in the gas stream by volume (%) | = | 10.1 | % |
| 20.9 | = oxygen content of ambient air (%) | = | 20.9 | % |
| | | | | |

 E_{Fd}

12. Mercury emission rate - Fc-based (Ib/MMBtu)

$$E_{Fc} = \left(\frac{m_n}{V_{mstd}}\right) \left(\frac{2.205 \times 10^{-3}}{10^6}\right) \left(F_c\right) \left(\frac{100}{CO_2}\right)$$

= mercury emission rate - Fd-based (lb/MMBtu)

| where: | | | | |
|--------------------------|--|---|-------------|----------------|
| mn | = mercury collected in sample (total µg) | = | 9.1977 | μg |
| V _{mstd} | = volume metered, standard (dscf) | = | 84.1826 | dscf |
| 2.205 x 10 ⁻³ | = conversion factor (lb/g) | = | 2.205E-03 | lb/g |
| 10 ⁶ | = conversion factor (μg/g) | = | 1.0E+06 | µg/g |
| Fc | = ratio of gas volume to heat content of fuel (dscf/MMBtu) | = | 1,820 | dscf/MMBtu |
| CO2 | = proportion of oxygen in the gas stream by volume (%) | = | 9.3 | % |
| 100 | = conversion factor | = | 100 | |
| E _{Fc} | ≈ mercury emission rate - Fc-based (lb/MMBtu) | 2 | 4.7402E-06 | lb/MMBtu |
| -rc | | | 1.1 1022 00 | 10/14/11/10 CG |

LOGIC FOR TREATING DETECTION LIMITS

(all metals except mercury)

1. Logic for Determining Maximum Allowable Front-Half Blank Correction (mFB-allow)

| | CASE 1 | CASE 2 |
|---------|----------------------------------|---------------------------|
| | m _{FB} = D | m _{FB} = ND |
| Rule | | |
| ND = 0 | m _{FB-allow} = M29 Rule | m _{FB-allow} = 0 |
| ND=1x | m _{FB-allow} = M29 Rule | m _{FB-allow} = 0 |
| ND=0.5x | m _{FB-ellow} = M29 Rule | m _{FB-allow} = 0 |

2. Logic for Determining Blank-Corrected Front-Half Sample Amount (m_F)

| | CASE 1 | CASE 2 |
|---------|--|---|
| | m _{FS} - m _{FB-allow} ≥ MDL | m _{FS} - m _{FB-allow} < MDL |
| | | |
| Rule | | |
| ND = 0 | $m_F = m_{FS} - m_{FB-allow}$ | $m_F = < MDL$ |
| ND=1x | $m_F = m_{FS} - m_{FB-allow}$ | m _F = < MDL |
| ND=0.5x | m _F = m _{FS} - m _{FB-allow} | m _F = < MDL |

3. Logic for Determining Maximum Allowable Back-Half Blank Correction (m_{BB-allow})

| | CASE 1 | CASE 2 |
|------------------|----------------------------------|---------------------------|
| | m _{ee} = D | m _{ee} = ND |
| Rule | | |
| ND = 0 | m _{BB-allow} = M29 Rule | m _{BB-allow} = 0 |
| ND=1x | m _{BB-allow} = M29 Rule | m _{BB-allow} = 0 |
| N D= 0.5x | m _{BB-allow} = M29 Rule | $m_{BB-allow} = 0$ |

4. Logic for Determining Blank-Corrected Back-Half Sample Amount (m₈)

| | CASE 1 m _{BS} - m _{BB-allow} ≥ MDL | CASE 2 m _{BS} - m _{BB-allow} < MDL |
|---------|---|---|
| Rule | | |
| ND = 0 | $m_B = m_{BS} - m_{BB-allow}$ | m ₈ = < MDL |
| ND=1x | $m_B = m_{BS} - m_{BB-allow}$ | m _B = < MDL |
| ND=0.5x | $m_B = m_{BS} - m_{BB-allow}$ | m _B = < MDL |

5. Logic for Adding Front and Back-Half Corrected Samples (mn)

| Laborator | y Data | | | | |
|------------|--|--|-------------------------------|--|--|
| | mn | Net matter collected (g) | | | |
| Filterable | Particulate Results | ۰. ۲ | | | |
| | C _{sd} | Particulate Concentration (mg/dscr | n) | | |
| | C _{sd7} | Particulate Concentration @7% O2 (mg/dscm) | | | |
| | CASE 1 | CASE 2 | CASE 3 | | |
| | Both are D | One is D, other is ND | Both are ND | | |
| Rule | | | | | |
| ND = 0 | m _n = m _F + m _B | m _n = D | m _n = < Sum ND | | |
| ND=1x | m _n = m _F + m _B | m _n = < [D + ND] | m _n = < Sum ND | | |
| ND=0.5x | $m_n = m_F + m_B$ | m _n = <[D + 0.5ND] | m _n = < 0.5 Sum ND | | |

Definitions and Notes

The term "Rule" refers to the rule being implemented for hanMDLing non-detectable quantities in summation: MDL = minimum detection limit.

D = Detectable quantity reported as D.

ND = Non-Detectable quantity reported at a value of ND.

If Front and Back-Half fractions are combined, then only Items 1 and 2 are used.

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USEPA Method 5/29 Beryllium Analyte Calculations

Wheelabrator North Broward, Inc. Clean Air Project No: 10955 Unit 2 FF Outlet

USEPA Method 5/29 Beryllium Analyte Calculations

Sample data taken from Run 1

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Note: The tables presenting the results are generated electronically from raw data. It may not be possible to exactly duplicate these results using a calculator. The reference method data, results, and all calculations are carried to sixteen decimal places throughout. The final table is formatted to an appropriate number of significant figures.

Note: Please see the preceding page concerning treatment of minimum detection limits and mathematical operations on values that are below minimum detection limits.

1. Maximum front-half blank correction criteria (µg)

$$A = (1.4) \left(\frac{3.141593}{4}\right) \left(\frac{D}{2.54}\right)^2$$

Where:

1

| viiele. | | | | |
|----------|--|---|----------|--------|
| D | = diameter of filter used in sample apparatus | = | 8.2 | cm |
| 1.4 | = allowable blank per square inch of filter area | = | 1.4 | µg/in² |
| 2.54 | = conversion constant | = | 2.54 | cm/in |
| 4 | = conversion constant | = | 4 | |
| 3.141593 | = conversion constant (pi) | 2 | 3.141593 | |
| A | = maximum front-half blank correction criteria | = | 12.46 | μg |

2. Allowable blank correction - combined front and back-half sample fractions (µg)

| m _{FB} - allow | $= m_{FB}$ if $m_{FB} \leq A + 1$ | | | |
|-------------------------|---|--------------------|----------------------------------|---------------|
| m _{FB -allow} | $= MAX \left[A + 1, MIN \left(m_{FB}, 0.05\right)\right]$ | $5 \times m_{\mu}$ | _{rs})]ifm _r | $T_B > A + 1$ |
| Where: | | | | |
| m _{FB} | = beryllium amount in combined front- and back-half blank | = | <0.0500 | μg |
| m _{FS} | = beryllium amount in combined front- and back-half sample | = | <0.0500 | μg |
| A+1 | = max combined front- & back-half blank correction criteria | = | 12.46 | рд |
| 0.05 x m _{FS} | = 5% of combined front- and back-half sample amount | = | <0.0025 | нg |

| m _{FB-allow} | = allowable combined Beryllium blank correction | = | 0.0000 | μg |
|-----------------------|---|---|--------|----|
| NOTE: In this | case, the first criteria applies. | | | |

= arithmetic operator that returns the maximum of two values

= arithmetic operator that returns the minimum of two values

3. Combined front- and back-half sample corrected for allowable blank (µg)

Laboratory Data

MAX

MIN

m Net matter collected (g)

Filterable Particulate Results

C Particulate Concentration (mg/dscm)

C Particulate Concentration @7% O2 (mg/dscm)

$$m_n = m_{FS} - m_{FB-allow}$$

| M _{FS} M _{FB-allow} | = beryllium amount in combined front- and back-half sample = allowable combined beryllium blank correction | | <0.0500 0.0000 | hð hð |
|--|---|---|-------------------|----------|
| m _n | = blank-corrected beryllium in combined sample | = | <0.0500 | μg |

USEPA Method 5/29 Beryllium Sample Calculations

USEPA Method 5/29 Beryllium Sample Calculations

Sample data taken from Run 1

Note: The tables presenting the results are generated electronically from raw data. It may not be possible to exactly duplicate these results using a calculator. The reference method data, results, and all calculations are carried to sixteen decimal places throughout. The final table is formatted to an appropriate number of significant figures.

| throughout. The final t | able is formatted to an appropriate number of significant figures. | | | | |
|---------------------------------------|--|---|-------------|-----------|---------------|
| | | | | | 041210 140337 |
| Beryllium concent | tration (lb/dscf) | | | | K_N |
| C_{sd} | $= \left(\frac{m_n}{V_{mstd}}\right) \left(\frac{2.205 \times 10^{-3}}{10^6}\right)$ | | | | |
| Where: | | | | | |
| m | ≠ beryllium collected in sample (total µg) | = | <0.0500 | μg | |
| V _{mstd} | = volume metered, standard (dscf) | = | 84.1826 | dscf | |
| 2.205 x 10 ⁻³ | = conversion factor (Ib/g) | = | 2.205E-03 | lb/g | |
| 10 ⁶ | = conversion factor ($\mu g/g$) | = | 1.0E+06 | µg/g | |
| 10 | | - | 1.02.00 | P3/3 | |
| C _{sd} | = beryllium concentration (lb/dscf) | = | <1.3097E-12 | lb/dscf | |
| 2. Beryllium concenti | ration (ug/dscm) | | | | |
| | | | | | |
| C _{sd} | $= \left(\frac{m_n}{V_{msid}}\right) (35.31)$ | | | | |
| Where: | | | | | |
| m | = beryllium collected in sample (total µg) | = | <0.0500 | μg | |
| Vmstd | ≃ volume metered, standard (dscf) | = | 84.1826 | dscf | |
| 35.31 | = conversion factor (dscf/dscm) | = | 35.31 | dscf/dscm | |
| | | | | | |
| C _{sd} | = beryllium concentration (µg/dscm) | = | <2.0972E-02 | µg/dscm | |
| 3. Beryllium concentr | ation (ma/dscm) | | | | |
| C_{sd} | $= \left(\frac{m_n}{V_{mstd}}\right) \left(\frac{35.31}{1000}\right)$ | | | | |
| Where: | | | | | |
| mn | = beryllium collected in sample (total µg) | ~ | <0.0500 | μg | |
| V _{mstd} | = volume metered, standard (dscf) | = | 84.1826 | dscf | |
| | | | | | |
| 35.31 | = conversion factor (dscf/dscm) | = | 35.31 | dscf/dscm | |
| 1000 | = conversion factor (μg/mg) | = | 1000 | µg/mg | |
| | | | | -33 | |
| C _{sd} | = beryllium concentration (mg/dscm) | = | <2.0972E-05 | mg/dscm | |

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4. Bervilium concentration (un/Nm3 dou)

| 4. Beryllium concentration (µg/Nm3 dry) | | | | | |
|---|--|---|-------------|----------------------------|--|
| C _{sd} | $= \left(\frac{m_n}{V_{mstd}}\right) (35.31) \left(\frac{68+460}{32+460}\right)$ | | | | |
| Where: | | | | | |
| m _n | ⇒ beryllium collected in sample (total µg) | = | <0.0500 | μg | |
| V _{mstd} | = volume metered, standard (dscf) | = | 84.1826 | dscf | |
| 35.31 | = conversion factor (dscf/dscm) | = | 35.31 | dscf/dscm | |
| 68 | = standard temperature (°F) | = | 68 | ۴F | |
| 32 | = normal temperature (°F) | = | 32 | ۴F | |
| 460 | = °F to °R conversion constant | = | 460 | | |
| C _{sd} | = beryllium concentration (µg/Nm3 dry) | = | <2.2507E-02 | µg/Nm ³ dry | |
| 5. Beryllium concent | ration corrected to x% oxygen (lb/dscf example) | | | | |
| C _{sdx} | $= C_{sd} \left(\frac{20.9 - x}{20.9 - O_2} \right)$ | | | | |
| Where: | | | | | |
| C _{sd} | = beryllium concentration (lb/dscf) | ≈ | <1.3097E-12 | lb/dscf | |
| x | = oxygen content of corrected gas (%) | = | 7.0 | % | |
| 0 ₂ | = proportion of oxygen in the gas stream by volume (%) | = | 10.1 | % | |
| 20.9 | = oxygen content of ambient air (%) | = | 20.9 | % | |
| C _{sdx} | = beryllium concentration corrected to x% oxygen (lb/dscf) | = | <1.6809E-12 | lb/dscf @ x%O ₂ | |
| 6. Beryllium concent | ration corrected to y% carbon dioxide (lb/dscf example) | | | | |
| C_{sdy} | $= C_{sd} \left(\frac{y}{CO_2} \right)$ | | | | |
| Where: | | | | | |
| C _{sd} | = beryllium concentration (lb/dscf) | = | <1.3097E-12 | lb/dscf | |
| У | = carbon dioxide content of corrected gas (%) | = | 12.0 | % | |
| CO ₂ | = proportion of carbon dioxide in the gas stream by volume (%) | = | 9.3 | % | |
| C _{sdy} | = beryllium conc. corrected to y% carbon dioxide (lb/dscf) | = | <1.6990E-12 | lb/dscf @ y%CO₂ | |
| 7. Beryllium concentr | ration at actual gas conditions (lb/acf example) | | | | |
| C _a | $= C_{sd} \left(\frac{Q_{std}}{Q_a} \right)$ | | | | |
| Where: | | | | | |
| C _{sd} | = beryllium concentration (lb/dscf) | = | <1.3097E-12 | lb/dscf | |
| Q _{std} | = volumetric flow rate at standard conditions, dry basis (dscfm) | = | 108,134 | dscfm | |
| Qa | = volumetric flow rate at actual conditions (acfm) | = | 201,928 | acfm | |
| Ca | = beryllium concentration at actual gas conditions (lb/acf) | = | <7.0133E-13 | lb/acf | |

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USEPA Method 5/29 Beryllium Sample Calculations

= <8.4971E-06 lb/hr

.

8. Beryllium emission rate (lb/hr)

yllium emission rate (lb/hr)

$$E_{lb/hr} = \left(\frac{m_n}{V_{mstd}}\right) \left(\frac{2.205 \times 10^{-3}}{10^6}\right) (Q_{std}) (60)$$

Where:

| m _n | = beryllium collected in sample (total µg) | = | <0.0500 | μg |
|--------------------------|--|---|-----------|--------|
| V _{mstd} | = volume metered, standard (dscf) | = | 84.1826 | dscf |
| 2.205 x 10 ⁻³ | = conversion factor (lb/g) | = | 2.205E-03 | lb/g |
| 10 ⁶ | = conversion factor (μg/g) | = | 1.0E+06 | µg/g |
| Q _{std} | = volumetric flow rate at standard conditions, dry basis (dscfm) | = | 108,134 | dscfm |
| 60 | = conversion factor (min/hr) | = | 60 | min/hr |
| | | | | |

.

E_{lb/hr}

9. Beryllium emission rate (g/s)

$$E_{g/s} = \left(\frac{m_n}{V_{nustd}}\right) \left(\frac{Q_{std}}{(10^6)(60)}\right)$$

= beryllium emission rate (lb/hr)

Where:

 $E_{g/s}$

| WINCIC. | | | | |
|-------------------|--|---|-------------|---------|
| m" | | = | <0.0500 | μg |
| V _{mstd} | = volume metered, standard (dscf) | = | 84.1826 | dscf |
| Q _{std} | ≠ volumetric flow rate at standard conditions, dry basis (dscfm) | = | 108,134 | dscfm |
| 10 ⁶ | = conversion factor (μg/g) | = | 1.0E+06 | µg/g |
| 60 | = conversion factor (sec/min) | = | 60 | sec/min |
| E _{g/s} | = beryllium emission rate (g/s) | = | <1.0704E-06 | g/s |

= beryllium emission rate (g/s)

10. Beryllium emission rate (Ton/yr)

$$E_{T/yr} = \left(\frac{m_n}{V_{mstd}}\right) \left(\frac{2.205 \times 10^{-3}}{10^6}\right) \left(\mathcal{Q}_{std}\right) (60) \left(\frac{Cap}{2000}\right)$$

Where:

| mn | = beryllium collected in sample (total µg) | = | <0.0500 | μg |
|--------------------------|--|---|-------------|----------|
| V _{mstd} | volume metered, standard (dscf) | = | 84.1826 | dscf |
| 2.205 x 10 ⁻³ | = conversion factor (lb/g) | = | 2.205E-03 | lb/g |
| 10 ⁶ | = conversion factor (μg/g) | = | 1.0E+06 | µg/g |
| Q _{std} | = volumetric flow rate at standard conditions, dry basis (dscfm) | = | 108,134 | dscfm |
| 60 | = conversion factor (min/hr) | = | 60 | min/hr |
| Сар | = capacity factor for process (hours operated/year) | = | 8,760 | hours/yr |
| 2000 | = conversion factor (lb/Ton) | = | 2000 | lb/Ton |
| | | | | |
| E _{Ton/yr} | = beryllium emission rate (Ton/yr) | = | <3.7217E-05 | Ton/yr |

USEPA Method 5/29 Beryllium Sample Calculations

= <2.4187E-08 lb/MMBtu

11. Beryllium emission rate - Fd-based (Ib/MMBtu)

$$E_{Fd} = \left(\frac{m_n}{V_{mstd}}\right) \left(\frac{2.205 \times 10^{-3}}{10^6}\right) \left(F_d\right) \left(\frac{20.9}{20.9 - O_2}\right)$$
Where:

$$m_n = \text{berylllum collected in sample (total µg)} = <0.0500 \text{ µg}$$

$$V_{mstd} = \text{volume metered, standard (dscf)} = 84.1826 \text{ dscf}$$

$$2.205 \times 10^{-3} = \text{conversion factor (lb/g)} = 2.205E-03 \text{ ib/g}$$

$$10^6 = \text{conversion factor (µg/g)} = 1.0E+06 \text{ µg/g}$$

$$F_d = \text{ratio of gas volume to heat content of fuel (dscf/MMBtu)} = 9,570 \text{ dscf/MMBtu}$$

$$O_2 = \text{proportion of oxygen in the gas stream by volume (%)} = 10.1 \%$$

12. Beryllium emission rate - Fc-based (Ib/MMBtu)

$$E_{Fc} = \left(\frac{m_n}{V_{mstd}}\right) \left(\frac{2.205 \times 10^{-3}}{10^6}\right) (F_c) \left(\frac{100}{CO_2}\right)$$

= beryllium emission rate - Fd-based (lb/MMBtu)

Where:

E_{Fd}

| ٧ | vnere: | | | | |
|---|--------------------------|--|---|-------------|------------|
| | m, | = beryllium collected in sample (total µg) | = | <0.0500 | рq |
| | V _{mstd} | = volume metered, standard (dscf) | = | 84.1826 | dscf |
| | 2.205 x 10 ⁻³ | = conversion factor (lb/g) | Ħ | 2.205E-03 | lb/g |
| | 10 ⁶ | = conversion factor (µg/g) | = | 1.0E+06 | hð\ð |
| | Fc | = ratio of gas volume to heat content of fuel (dscf/MMBtu) | = | 1,820 | dscf/MMBtu |
| | CO2 | = proportion of oxygen in the gas stream by volume (%) | = | 9.3 | % |
| | 100 | = conversion factor | 2 | 100 | |
| | E _{Fc} | = beryllium emission rate - Fc-based (lb/MMBtu) | = | <2.5768E-08 | lb/MMBtu |
| | | | | | |

QA/QC _____ Date _____

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USEPA Method 5/29 Cadmium Analyte Calculations

Sample data taken from Run 1

Note: The tables presenting the results are generated electronically from raw data. It may not be possible to exactly duplicate these results using a calculator. The reference method data, results, and all calculations are carried to sixteen decimal places throughout. The final table is formatted to an appropriate number of significant figures.

Note: Please see the preceding page concerning treatment of minimum detection limits and mathematical operations on values that are below minimum detection limits.

1. Maximum front-half blank correction criteria (µg)

$$A = (1.4) \left(\frac{3.141593}{4}\right) \left(\frac{D}{2.54}\right)^2$$

Where:

| D | | = | 8.2 | cm |
|----------|--|---|----------|--------|
| 1.4 | = allowable blank per square inch of filter area | = | 1.4 | µg/in² |
| 2.54 | = conversion constant | = | 2.54 | cm/in |
| 4 | = conversion constant | = | 4 | |
| 3.141593 | = conversion constant (pi) | = | 3.141593 | |
| A | = maximum front-half blank correction criteria | = | 12.46 | μg |

2. Allowable blank correction - combined front and back-half sample fractions (µg)

| M _{FB} - allow | $= m_{FB}$ if $m_{FB} \leq A + 1$ | | | |
|-------------------------|--|------------------|----------------------|---------------|
| m _{FB - allow} | $= MAX [A + 1, MIN (m_{FB}, 0.05)]$ | $\times m_{\mu}$ | _{~s})]ifm, | $T_B > A + 1$ |
| Where: | | | | |
| m _{FB} | = cadmium amount in combined front- and back-half blank | = | <0.2000 | μg |
| m _{FS} | = cadmium amount in combined front- and back-half sample | = | 0.4679 | μg |
| A+1 | = max combined front- & back-half blank correction criteria | = | 12.46 | μg |
| 0.05 x m _{FS} | = 5% of combined front- and back-half sample amount | = | 0.0234 | hð |
| MAX | = arithmetic operator that returns the maximum of two values | | | |
| MIN | = arithmetic operator that returns the minimum of two values | | | |
| m _{FB-allow} | = allowable combined Cadmium blank correction | = | 0.0000 | 49 |

NOTE: In this case, the first criteria applies.

3. Combined front- and back-half sample corrected for allowable blank (µg)

Laboratory Data

m Net matter collected (g)

Filterable Particulate Results

C Particulate Concentration (mg/dscm)

C Particulate Concentration @7% O2 (mg/dscm)

$$m_n = m_{FS} - m_{FB-allow}$$

Where:

| m _{FS} m _{FB-allow} | = cadmium amount in combined front- and back-half sample = allowable combined cadmium blank correction | = | 0.4679 0.0000 | hð hð |
|--|---|---|------------------|----------|
| m _n | = blank-corrected cadmium in combined sample | = | 0.4679 | μg |

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USEPA Method 5/29 Cadmium Sample Calculations

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USEPA Method 5/29 Cadmium Sample Calculations

Sample data taken from Run 1

Note: The tables presenting the results are generated electronically from raw data. It may not be possible to exactly duplicate these results using a calculator. The reference method data, results, and all calculations are carried to sixteen decimal places throughout. The final table is formatted to an appropriate number of significant figures.

1. Cadmium concentration (lb/dscf)

$$C_{sd} = \left(\frac{m_n}{V_{mstd}}\right) \left(\frac{2.205 \times 10^{-3}}{10^6}\right)$$

Where:

| m _n | = cadmium collected in sample (total μg) | = | 0.4679 | μg |
|---|---|---|----------------------|--------------|
| V _{mstd} 2.205 x 10 ⁻³ | = volume metered, standard (dscf) = conversion factor (lb/g) | = | 84.1826 2.205E-03 | dscf lb/g |
| 10 ⁶ | = conversion factor (µg/g) | = | 1.0E+06 | hð\ð |
| C _{sd} | = cadmium concentration (lb/dscf) | = | 1.2255E-11 | lb/dscf |

2. Cadmium concentration (µg/dscm)

$$C_{sd} = \left(\frac{m_n}{V_{mstd}}\right) (35.31)$$

Where:

| m _n V _{mstd} 35.31 | = cadmium collected in sample (total µg) = volume metered, standard (dscf) = conversion factor (dscf/dscm) | = = | 0.4679 84.1826 35.31 | µg dscf dscf/dscm |
|--|--|--------|----------------------------|-------------------------|
| C _{sd} | | = | 1.9624E-01 | µg/dscm |

3. Cadmium concentration (mg/dscm)

 $= \left(\frac{m_n}{V_{mstd}}\right) \left(\frac{35.31}{1000}\right)$

Where:

 C_{sd}

| mn | = cadmium collected in sample (total µg) | = | 0.4679 | μg |
|-------------------|--|---|---------|------|
| V _{mstd} | = volume metered, standard (dscf) | = | 84.1826 | dscf |

| 35.31 | = conversion factor (dscf/dscm) | = | 35.31 | dscf/dscm |
|----------|-----------------------------------|---|------------|-----------|
| 1000 | = conversion factor (μg/mg) | = | 1000 | µg/mg |
| C_{sd} | = cadmium concentration (mg/dscm) | = | 1.9624E-04 | mg/dscm |

4. Cadmium concentration (uo/Nm3 drv)

$$C_{xd} = \left(\frac{m_{x}}{|V_{wad}}\right)(35.31)\left(\frac{68 + 460}{32 + 460}\right)$$
Where:

$$m_{n} = \text{cadmium collected in sample (total µg)} = 0.4679 µg$$

$$V_{mad} = \text{volume metered, standard (dscf)} = 35.31 \text{ dscfd scm}$$

$$88.1828 \text{ dscf}$$

$$35.31 = \text{conversion factor (dscfdscm)} = 38.1828 \text{ dscf}$$

$$35.31 = \text{conversion factor (dscfdscm)} = 68 \text{ F}$$

$$32 = \text{normal temperature (F)} = 32 \text{ F}$$

$$460 = \text{F to 'R conversion constant} = 460$$

$$C_{xd} = \text{cadmium concentration (µg/Nm3 dry)} = 2.1060E-01 µg/Nm^3 dry$$
5. Cadmium concentration corrected to x% oxygen (b/dscf example)

$$C_{xd} = \text{cadmium concentration (b/dscf)} = 1.2255E-11 \text{ b/dscf}$$

$$x = 0xygen content of corrected gas (%) = 7.0 \%$$

$$20.9 = \text{oxygen content of corrected gas (%) = 20.9 \%$$

$$C_{xdx} = \text{cadmium concentration corrected to x% oxygen (b/dscf) = 1.5729E-11 \text{ b/dscf} @ x%O_2$$
6. Cadmium concentration corrected to y% carbon dioxide (b/dscf) = 1.2255E-11 \text{ b/dscf} @ x%O_2
6. Cadmium concentration corrected to y% carbon dioxide (b/dscf) = 1.5729E-11 \text{ b/dscf} @ x%O_2
6. Cadmium concentration corrected to y% carbon dioxide (b/dscf) = 1.2255E-11 \text{ b/dscf} @ x%O_2
6. Cadmium concentration corrected to y% carbon dioxide (b/dscf) = 1.2255E-11 \text{ b/dscf} @ x%O_2
6. Cadmium concentration (b/dscf) = 1.2255E-11 \text{ b/dscf} @ x%O_2
7. Cadmium concentration (b/dscf) = 1.2255E-11 \text{ b/dscf} @ x%O_2
7. Cadmium concentration dioxide (b/dscf) = 1.529E-11 \text{ b/dscf} @ y%CO_2
7. Cadmium concentration dioxide (b/dscf) = 1.5898E-11 \text{ b/dscf} @ y%CO_2
7. Cadmium concentration at actual gas conditions (b/dscf) = 1.2255E-11 \text{ b/dscf} @ y%CO_2
7. Cadmium concentration at actual gas conditions (b/dscf) = 1.2255E-11 \text{ b/dscf} @ y%CO_2
7. Cadmium concentration (b/dscf) = 1.2255E-11 \text{ b/dscf} @ y%CO_2
7. Cadmium concentration at actual gas conditions (difform) = 10.8,134 dscfm = 0.4, ($\frac{Q_{xf}}{Q_{xf}} = \text{ cdmium concentration (b/dscf)} = 1.2255E-11 b/dscf @ y%CO_2$
7. Cadmium concentration (b/dscf) = 1.2255E-11 b/dscf @ y%CO_2 = 0.0, (($\frac{Q_{xf}}{Q_{xf}}$

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USEPA Method 5/29 Cadmium Sample Calculations



7.9509E-05 lb/hr

=

8. Cadmium emission rate (lb/hr)

$$E_{lb/hr} = \left(\frac{m_n}{V_{mstd}}\right) \left(\frac{2.205 \times 10^{-3}}{10^6}\right) (\mathcal{Q}_{std}) (60)$$

= cadmium emission rate (lb/hr)

Where:

| m _n | = cadmium collected in sample (total µg) | = | 0.4679 | μg |
|--------------------------|--|---|-----------|--------|
| V _{mstd} | = volume metered, standard (dscf) | = | 84.1826 | dscf |
| 2.205 x 10 ⁻³ | = conversion factor (lb/g) | = | 2.205E-03 | lb/g |
| 10 ⁶ | = conversion factor (μg/g) | = | 1.0E+06 | µg/g |
| Q _{std} | = volumetric flow rate at standard conditions, dry basis (dscfm) | = | 108,134 | dscfm |
| 60 | = conversion factor (min/hr) | = | 60 | min/hr |
| | | | | |

Élb/hr

9. Cadmium emission rate (g/s)

$$E_{g/s} = \left(\frac{m_n}{V_{nstd}}\right) \left(\frac{Q_{std}}{(10^6)(60)}\right)$$

W

 $E_{g/s}$

| Where: | | | | |
|-------------------|--|---|------------|---------|
| mn | = cadmium collected in sample (total µg) | = | 0.4679 | μg |
| V _{mstd} | = volume metered, standard (dscf) | = | 84.1826 | dscf |
| Q _{std} | = volumetric flow rate at standard conditions, dry basis (dscfm) | = | 108,134 | dscfm |
| 10 ⁸ | = conversion factor (µg/g) | = | 1.0E+06 | µg/g |
| 60 | = conversion factor (sec/min) | = | 60 | sec/min |
| E _{g/s} | = cadmium emission rate (g/s) | = | 1.0016E-05 | g/s |

10. Cadmium emission rate (Ton/yr)

$$E_{T/yr} = \left(\frac{m_n}{V_{mstd}}\right) \left(\frac{2.205 \times 10^{-3}}{10^6}\right) (\mathcal{Q}_{std}) (60) \left(\frac{Cap}{2000}\right)$$

| mn | = cadmium collected in sample (total µg) | × | 0.4679 | μg |
|--------------------------|--|---|------------|----------|
| V _{mstd} | = volume metered, standard (dscf) | = | 84.1826 | dscf |
| 2.205 x 10 ⁻³ | = conversion factor (lb/g) | = | 2.205E-03 | lb/g |
| 10 ⁶ | = conversion factor (μg/g) | = | 1.0E+06 | µg/g |
| Q _{std} | = volumetric flow rate at standard conditions, dry basis (dscfm) | ÷ | 108,134 | dscfm |
| 60 | = conversion factor (min/hr) | = | 60 | min/hr |
| Сар | = capacity factor for process (hours operated/year) | = | 8,760 | hours/yr |
| 2000 | = conversion factor (lb/Ton) | = | 2000 | lb/Ton |
| E _{Ton/yr} | = cadmium emission rate (Ton/yr) | = | 3.4825E-04 | Ton/yr |
| | | | | |

11. Cadmium emission rate - Fd-based (lb/MMBtu)

$$E_{Fd} = \left(\frac{m_n}{V_{mstd}}\right) \left(\frac{2.205 \times 10^{-3}}{10^6}\right) (F_d) \left(\frac{20.9}{20.9 - O_2}\right)$$

Where:

| where: | | | | |
|--------------------------|--|---|-----------|------------|
| m'n | = cadmium collected in sample (total µg) | = | 0.4679 | hð |
| Vmstd | = volume metered, standard (dscf) | = | 84.1826 | dscf |
| 2.205 x 10 ⁻³ | = conversion factor (lb/g) | = | 2.205E-03 | lb/g |
| 10 ⁶ | = conversion factor (μg/g) | = | 1.0E+06 | hð\ð |
| Fd | = ratio of gas volume to heat content of fuel (dscf/MMBtu) | = | 9,570 | dscf/MMBtu |
| O ₂ | = proportion of oxygen in the gas stream by volume (%) | = | 10.1 | % |
| 20.9 | = oxygen content of ambient air (%) | = | 20.9 | % |
| | | | | |

12. Cadmium emission rate - Fc-based (lb/MMBtu)

E_{Fd}

$$E_{Fc} = \left(\frac{m_n}{V_{mstd}}\right) \left(\frac{2.205 \times 10^{-3}}{10^6}\right) (F_c) \left(\frac{100}{CO_2}\right)$$

Where:
$$m_n = \text{cadmium collected in sample (total µg)}$$
$$V_{mstd} = \text{volume metered, standard (dscf)}$$
$$2.205 \times 10^3 = \text{conversion factor (lb/a)}$$

= cadmium emission rate - Fd-based (lb/MMBtu)

lb/g 2.205E-03 = 2.205 x 10 conversion factor (ID/g) 10⁶ = conversion factor (µg/g) 1.0E+06 = µg/g Fc = ratio of gas volume to heat content of fuel (dscf/MMBtu) dscf/MMBtu = 1,820 CO_2 = proportion of oxygen in the gas stream by volume (%) = 9.3 % 100 = conversion factor 100 . =

E_{Fc} = cadmium emission rate - Fc-based (lb/MMBtu) = 2.4112E-07 lb/MMBtu

USEPA Method 5/29 Cadmium Sample Calculations

=

=

0.4679

84.1826

= 2.2632E-07 lb/MMBtu

μg

dscf

041210 140659

USEPA Method 5/29 Lead Analyte Calculations

Sample data taken from Run 1

Note: The tables presenting the results are generated electronically from raw data. It may not be possible to exactly duplicate these results using a calculator. The reference method data, results, and all calculations are carried to sixteen decimal places throughout. The final table is formatted to an appropriate number of significant figures.

Note: Please see the preceding page concerning treatment of minimum detection limits and mathematical operations on values that are below minimum detection limits.

1. Maximum front-half blank correction criteria (µg)

$$A = (1.4) \left(\frac{3.141593}{4}\right) \left(\frac{D}{2.54}\right)^2$$

Where:

| vilere. | | | | | |
|----------|--|---|----------|--------|--|
| D | = diameter of filter used in sample apparatus | = | 8.2 | cm | |
| 1.4 | = allowable blank per square inch of filter area | = | 1.4 | µg/in² | |
| 2.54 | = conversion constant | = | 2.54 | cm/in | |
| 4 | = conversion constant | = | 4 | | |
| 3.141593 | = conversion constant (pi) | = | 3.141593 | | |
| | | | | | |
| Α | = maximum front-half blank correction criteria | = | 12.46 | μg | |

2. Allowable blank correction - combined front and back-half sample fractions (µg)

| m _{FB} - allow | $= m_{FB}$ if $m_{FB} \leq A + 1$ | | | |
|-------------------------|--|--------------|---------------------|-----------------|
| m _{FB} - allow | $= MAX \left[A + 1, MIN \left(m_{FB}, 0.05\right)\right]$ | $\times m_F$ | _s)]if m | $_{FB} > A + 1$ |
| Where: | | | | |
| m _{FB} | = lead amount in combined front- and back-half blank | = | 0.4541 | рg |
| m _{FS} | = lead amount in combined front- and back-half sample | = | 2.8948 | hð |
| A+1 | = max combined front- & back-half blank correction criteria | = | 12.46 | нg |
| 0.05 x m _{FS} | = 5% of combined front- and back-half sample amount | = | 0.1447 | hð |
| MAX | = arithmetic operator that returns the maximum of two values | | | |
| MIN | = arithmetic operator that returns the minimum of two values | | | |
| m _{FB-allow} | = allowable combined Lead blank correction | = | 0.4541 | hð |

3. Combined front- and back-half sample corrected for allowable blank (µg)

Laboratory Data

m Net matter collected (g)

Filterable Particulate Results

C Particulate Concentration (mg/dscm)

C Particulate Concentration @7% O2 (mg/dscm)

NOTE: In this case, the first criteria applies.

$$m_n = m_{FS} - m_{FB-allow}$$

| m _{FS} m _{FB-allow} | lead amount in combined front- and back-half sample allowable combined lead blank correction | = | 2.8948 0.4541 | hð hð |
|--|---|---|------------------|----------|
| m'n | = blank-corrected lead in combined sample | = | 2.4408 | μg |

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K_N

USEPA Method 5/29 Lead Sample Calculations

Sample data taken from Run 1

Note: The tables presenting the results are generated electronically from raw data. It may not be possible to exactly duplicate these results using a calculator. The reference method data, results, and all calculations are carried to sixteen decimal places throughout. The final table is formatted to an appropriate number of significant figures.

1. Lead concentration (lb/dscf)

$$C_{sd} = \left(\frac{m_n}{V_{msid}}\right) \left(\frac{2.205 \times 10^{-3}}{10^6}\right)$$

Where:

| mn | = lead collected in sample (total μg) | = | 2.4408 | hð | |
|--------------------------|---------------------------------------|---|------------|---------|--|
| V _{mstd} | = volume metered, standard (dscf) | = | 84.1826 | dscf | |
| 2.205 x 10 ⁻³ | = conversion factor (lb/g) | = | 2.205E-03 | lb/g | |
| 10 ⁶ | = conversion factor (μg/g) | = | 1.0E+06 | µg/g | |
| C _{sd} | ≈ lead concentration (lb/dscf) | = | 6.3931E-11 | lb/dscf | |

2. Lead concentration (µg/dscm)

$$C_{sd} = \left(\frac{m_n}{V_{mstd}}\right) (35.31)$$

Where:

| m _n | = lead collected in sample (total μg) | = | 2.4408 | hð |
|-------------------|---------------------------------------|---|------------|-----------|
| V _{mstd} | = volume metered, standard (dscf) | = | 84.1826 | dscf |
| 35.31 | = conversion factor (dscf/dscm) | = | 35.31 | dscf/dscm |
| C _{sd} | .= lead concentration (µg/dscm) | = | 1.0238E+00 | µg/dscm |

3. Lead concentration (mg/dscm)

$$= \left(\frac{m_n}{V_{mstd}}\right) \left(\frac{35.31}{1000}\right)$$

Where:

 C_{sd}

| 35.31 | ≈ conversion factor (dscf/dscm) = conversion factor (µg/mg) | = | 35.31 | dscf/dscm |
|-----------------|---|---|------------|-----------|
| 1000 | | = | 1000 | µg/mg |
| C _{sd} | = lead concentration (mg/dscm) | = | 1.0238E-03 | mg/dscm |

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4. Lead concentration (µg/Nm3 dry)

 $=\left(\frac{m_n}{V_{max}}\right)(35.31)\left(\frac{68+460}{32+460}\right)$ C ... Where: = lead collected in sample (total µg) 2.4408 m = μg = volume metered, standard (dscf) 84.1826 V_{mstd} dscf = = conversion factor (dscf/dscm) 35.31 35.31 dscf/dscm = = standard temperature (°F) ٩F 68 68 = ٩F = normal temperature (°F) 32 32 = = °F to °R conversion constant 460 460 = Csd ≈ lead concentration (µg/Nm3 dry) = 1.0987E+00 µg/Nm³ dry 5. Lead concentration corrected to x% oxygen (lb/dscf example) $= C_{sd} \left(\frac{20.9 - x}{20.9 - O_2} \right)$ C_{sdx} Where: = lead concentration (lb/dscf) 6.3931E-11 lb/dscf C_{sd} = = oxygen content of corrected gas (%) 7.0 % х = **O**₂ = proportion of oxygen in the gas stream by volume (%) 10.1 % _ = oxygen content of ambient air (%) 20.9 % 20.9 8.2054E-11 lb/dscf @ x%O2 Csdx = lead concentration corrected to x% oxygen (lb/dscf) = 6. Lead concentration corrected to y% carbon dioxide (lb/dscf example) $=C_{sd}\left(\frac{y}{CO_{2}}\right)$ Csdv Where: C_{sd} = lead concentration (lb/dscf) 6.3931E-11 lb/dscf = = carbon dioxide content of corrected gas (%) 12.0 % = v CO_2 = proportion of carbon dioxide in the gas stream by volume (%) 9.3 % C_{sdy} = lead conc. corrected to y% carbon dioxide (lb/dscf) 8.2937E-11 lb/dscf @ y%CO2 = 7. Lead concentration at actual gas conditions (lb/acf example) $= C_{sd} \left(\frac{Q_{std}}{Q_a} \right)$ C_a Where: = lead concentration (lb/dscf) 6.3931E-11 lb/dscf = volumetric flow rate at standard conditions, dry basis (dscfm) 108,134 Q_{std} = dscfm Q_a = volumetric flow rate at actual conditions (acfm) = 201.928 acfm C_a = lead concentration at actual gas conditions (lb/acf) 3.4235E-11 lb/acf =

= 4.1479E-04 lb/hr

8. Lead emission rate (lb/hr)

$$E_{lb/hr} = \left(\frac{m_n}{V_{mstd}}\right) \left(\frac{2.205 \times 10^{-3}}{10^6}\right) (Q_{std}) (60)$$

Where:

| mn | = lead collected in sample (total µg) | = | 2.4408 | μg |
|--------------------------|--|---|-----------|--------|
| V _{mstd} | = volume metered, standard (dscf) | = | 84.1826 | dscf |
| 2.205 x 10 ⁻³ | = conversion factor (lb/g) | = | 2.205E-03 | ib/g |
| 10 ⁶ | = conversion factor (μg/g) | = | 1.0E+06 | µg/g |
| Q _{std} | volumetric flow rate at standard conditions, dry basis (dscfm) | = | 108,134 | dscfm |
| 60 | = conversion factor (min/hr) | = | 60 | min/hr |
| | | | | |

E_{lb/hr}

$$= \left(\frac{m_n}{V_{nstd}}\right) \left(\frac{Q_{std}}{(10^6)(60)}\right)$$

= lead emission rate (lb/hr)

Where:

 $E_{g/s}$

| 84.1826 108.134 | dscf dscfm |
|--------------------|---------------|
| | |
| | |
| 1.0E+06 | µg/g |
| 60 | sec/min |
| | |
| 5.2253E-05 | g/s |
| ; | 1.0E+06 60 |

E_{g/s}

10. Lead emission rate (Ton/yr)

$$E_{T/yr} = \left(\frac{m_n}{V_{mstd}}\right) \left(\frac{2.205 \times 10^{-3}}{10^6}\right) (Q_{std}) (60) \left(\frac{Cap}{2000}\right)$$

| winere. | - | | | |
|--------------------------|--|---|------------|----------|
| mn | = lead collected in sample (total µg) | = | 2.4408 | μg |
| V _{mstd} | = volume metered, standard (dscf) | = | 84.1826 | dscf |
| 2.205 x 10 ⁻³ | = conversion factor (lb/g) | = | 2.205E-03 | lb/g |
| 10 ⁶ | = conversion factor (μg/g) | = | 1.0E+06 | µg/g |
| Q _{std} | = volumetric flow rate at standard conditions, dry basis (dscfm) | = | 108,134 | dscfm |
| 60 | = conversion factor (mln/hr) | = | 60 | min/hr |
| Сар | = capacity factor for process (hours operated/year) | = | 8,760 | hours/yr |
| 2000 | = conversion factor (lb/Ton) | = | 2000 | lb/Ton |
| | | | | |
| E _{Ton/yr} | = lead emission rate (Ton/yr) | = | 1.8168E-03 | Ton/yr |
| | | | | |

11. Lead emission rate - Fd-based (lb/MMBtu)

$$\begin{split} E_{Fd} &= \left(\frac{m_n}{V_{mstd}}\right) \left(\frac{2.205 \times 10^{-3}}{10^6}\right) \left(F_d\right) \left(\frac{20.9}{20.9 - O_2}\right) \\ \text{Where:} \\ &m_n &= \text{lead collected in sample (total µg)} &= 2.4408 \quad \mu\text{g} \\ &V_{mstd} &= \text{volume metered, standard (dscf)} &= 84.1826 \quad \text{dscf} \\ &2.205 \times 10^3 &= \text{conversion factor (lb/g)} &= 2.205E-03 \quad \text{lb/g} \\ &10^6 &= \text{conversion factor (µg/g)} &= 1.0E+06 \quad \mu\text{g/g} \\ &F_d &= \text{ratio of gas volume to heat content of fuel (dscf/MMBtu)} &= 9,570 \quad \text{dscf/MMBtu} \\ &O_2 &= \text{proportion of oxygen in the gas stream by volume (\%)} &= 10.1 \quad \% \\ &20.9 &= \text{oxygen content of ambient air (\%)} &= 20.9 \quad \% \end{split}$$

12. Lead emission rate - Fc-based (lb/MMBtu)

$$E_{Fc} = \left(\frac{m_n}{V_{mstd}}\right) \left(\frac{2.205 \times 10^{-3}}{10^6}\right) (F_c) \left(\frac{100}{CO_2}\right)$$

Where:

| vvnere: | | | | | |
|--------------------------|--|---|------------|------------|--|
| mn | = lead collected in sample (total µg) | = | 2.4408 | μg | |
| V _{mstd} | = volume metered, standard (dscf) | = | 84.1826 | dscf | |
| 2.205 x 10 ⁻³ | = conversion factor (lb/g) | = | 2.205E-03 | lb/g | |
| 10 ⁶ | = conversion factor (µg/g) | = | 1.0E+06 | µg/g | |
| Fc | = ratio of gas volume to heat content of fuel (dscf/MMBtu) | = | 1,820 | dscf/MMBtu | |
| CO ₂ | = proportion of oxygen in the gas stream by volume (%) | = | 9.3 | % | |
| 100 | = conversion factor | = | 100 | | |
| E _{Fc} | = lead emission rate - Fc-based (lb/MMBtu) | = | 1.2579E-06 | lb/MMBtu | |
| | | | | | |

USEPA Method 5/29 Lead Sample Calculations

= 1.1807E-06 lb/MMBtu

EPA Method 1-4 Calculations

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USEPA Method 13B (Total Fluorides) Sampling, Velocity and Moisture Sample Calculations

Sample data taken from Run 1

Note: The tables presenting the results are generated electronically from raw data. It may not be possible to exactly duplicate these results using a calculator. The reference method data, results, and all calculations are carried to sixteen decimal places throughout. The final table is formatted to an appropriate number of significant figures.

1. Volume of water collected (wscf)

$$V_{wstd} = (0.04706)(V_{lc})$$

Where:

| V _{lc} | = total volume of liquid collected in impingers and silica gel (ml) = ideal gas conversion factor (ft³ water vapor/ml or gm) | = | 212.4 | mi |
|-------------------|--|---|---------|---------------------|
| 0.04706 | | = | 0.04706 | ft ³ /ml |
| V _{wstd} | = volume of water vapor collected at standard conditions (ft ³) | = | 10.00 | ft ³ |

2. Volume of gas metered, standard conditions (dscf)

$$=\frac{(17.64)(V_m)\left(P_{bar}+\frac{\Delta H}{13.6}\right)(Y_d)}{(460+T_m)}$$

Where:

V_{mstd}

| wnere: | | | | |
|-------------------|---|---|--------|---------------|
| P _{bar} | = barometric pressure (in. Hg) | = | 30.05 | in. Hg |
| T _m | = average dry gas meter temperature (°F) | = | 64.54 | °F |
| V _m | volume of gas sample through the dry gas meter at meter conditions (dcf) | = | 38.08 | dcf |
| Y _d | gas meter correction factor (dimensionless) | = | 0.9898 | |
| ΔH | = average pressure drop across meter box orifice (in. H ₂ O) | = | 1.26 | in. H₂O |
| 17. 6 4 | = standard temperature to pressure ratio (°R/in. Hg) | = | 17.64 | °R/in. Hg |
| 13.6 | = conversion factor (in. H ₂ O/in. Hg) | = | 13.6 | in.H₂O/in. Hg |
| 460 | = °F to °R conversion constant | = | 460 | |
| V _{mstd} | volume of gas sampled through the dry gas meter at standard conditions (dscf) | = | 38.207 | dscf |

3. Sample gas pressure (in. Hg)

$$= P_{bar} + \left(\frac{P_g}{13.6}\right)$$

Where:

 P_s

| P _{bar} | = barometric pressure (in. Hg) | = | 30.05 | in. Hg |
|------------------|---|---|--------|-----------------------------|
| Pg | = sample gas static pressure (in. H ₂ O) | = | -10.60 | in. H₂O |
| 13.6 | = conversion factor (in, H_2O/in . Hg) | = | 13.6 | in. H ₂ O/in. Hg |
| Ps | = absolute sample gas pressure (in. Hg) | = | 29.27 | in. Hg |

EPA Method 1-4 Calculations

4. Actual water vapor pressure at sample gas temperature less than 212°F (in. Hg)

 P_{ν}

$$=\frac{e^{\left(18.3036-\frac{3816.44}{\frac{5}{9}(7_{s}-32)+273.15-46.13}\right)}}{25.4}$$

Where:

| vvnere. | | | | |
|----------------|---|---|---------|--------------|
| Τ _s | = average sample gas temperature (°F) | = | 306.24 | ۴ |
| 18.3036 | = Antoine coefficient | = | 18.3036 | °K |
| 3816.44 | = Antoine coefficient | 3 | 3816.44 | °K |
| 273.15 | = temperature conversion factor | = | 273.15 | ۴K |
| 46.13 | = Antoine coefficient | = | 46.13 | °K |
| 25.4 | = conversion factor | = | 25.4 | mm Hg/in. Hg |
| 5/9 | = Fahrenheit to Celsius conversion factor | = | 5/9 | °C/°F |
| 32 | = temperature conversion (°F) | = | 32 | ۴F |
| Pv | = vapor pressure, actual (in. Hg) | = | 29.27 | in. Hg |
| | | | | |

5. Water vapor pressure at gas temperature greater than 212°F (in. Hg)

| P_{ν} | $= P_s$ | | | |
|--------------------------|---|---|-------|--------|
| Where: P _s | ≂ absolute sample gas pressure (in. Hg) | = | 29.27 | in. Hg |
| Pv | ≈ water vapor pressure, actual (in. Hg) | = | 29.27 | in. Hg |

6. Moisture measured in sample (% by volume)

$$B_{wo} = \frac{V_{wstd}}{(V_{mstd} + V_{wstd})}$$

Wł

| Where: | | | | |
|-------------------|---|---|--------|------|
| V _{mstd} | = volume of gas sampled through the dry gas meter at standard conditions (dscf) | = | 38.207 | dscf |
| V _{wstd} | = volume of water collected at standard conditions (scf) | = | 10.00 | scf |
| Bwo | = proportion of water measured in the gas stream by volume | = | 0.2074 | |
| | | = | 20.74 | % |

7. Saturated moisture content (% by volume)

 $B_{ws} = \frac{P_v}{P_s}$

| = absolute sample gas pressure (in. Hg) | = | 29.27 | in. Hg | |
|--|--|---|---|---|
| = water vapor pressure, actual (in. Hg) | = | 29.27 | in. Hg | |
| = proportion of water vapor in the gas stream by volume at saturated conditions | = | 1.0000 100.00 | % | |
| | = water vapor pressure, actual (in. Hg)= proportion of water vapor in the gas stream by volume at | = water vapor pressure, actual (in. Hg) = proportion of water vapor in the gas stream by volume at | = water vapor pressure, actual (in. Hg)=29.27= proportion of water vapor in the gas stream by volume at1.0000 | = water vapor pressure, actual (in. Hg)=29.27in. Hg= proportion of water vapor in the gas stream by volume at1.0000 |

8. Actual water vapor in gas (% by volume)

$$B_{w} = MINIMUM \left[B_{wo}, B_{ws}\right]$$

Where:

| B _{ws} | proportion of water vapor in the gas stream by volume at saturated conditions | = | 1.0000 | |
|-----------------|---|---|-----------------|----|
| B _{wo} | = proportion of water measured in the gas stream by volume | = | 0.2074 | |
| B _w | = actual water vapor in gas | = | 0.2074 20.74 | % |
| | | - | 20.74 | 70 |

9. Nitrogen (plus carbon monoxide) in gas stream (% by volume, dry)

 $N_2 + CO = 100 - CO_2 - O_2$

Where:

| CO ₂ | proportion of carbon dioxide in the gas stream by volume (%) proportion of oxygen in the gas stream by volume (%) conversion factor (%) | = | 9.3 | % |
|--------------------|---|---|-------|---|
| O ₂ | | = | 10.0 | % |
| 100 | | = | 100 | % |
| N ₂ +CO | = proportion of nitrogen and CO in the gas stream by volume (%) | = | 80.69 | % |

10. Molecular weight of dry gas stream (lb/lb mole)

| M_d | $= \left(M_{CO_2}\right) \frac{(CO_2)}{(100)} + \left(M_{O_2}\right) \frac{(O_2)}{(100)} + \left(M_{N_2+CO}\right) \frac{(N_2+CO)}{(100)}$ | | | |
|--------------------|--|---|-------|------------|
| Where: | | | | |
| M _{CO2} | = molecular weight of carbon dioxide (lb/lb·mole) | = | 44.00 | lb/lb·mole |
| M _{O2} | = molecular weight of oxygen (lb/lb·mole) | = | 32.00 | lb/lb·mole |
| MN2+CD | = molecular weight of nitrogen and carbon monoxide (lb/lb·mole) | = | 28.00 | lb/lb·mole |
| CO2 | = proportion of carbon dioxide in the gas stream by volume (%) | = | 9.3 | % |
| O ₂ | = proportion of oxygen in the gas stream by volume (%) | = | 10.0 | % |
| N ₂ +CO | = proportion of nitrogen and CO in the gas stream by volume (%) | = | 80.7 | % |
| 100 | = conversion factor (%) | = | 100 | % |
| M _d | = dry molecular weight of sample gas (Ib/Ib·mole) | = | 29.89 | lb/lb·mole |

11. Molecular weight of sample gas (lb/lb·mole)

$$M_{s} = (M_{d})(1-B_{w}) + (M_{H_{2}O})(B_{w})$$

Where:

| B _w M _d M _{H2O} | proportion of water vapor in the gas stream by volume dry molecular weight of sample gas (lb/lb·mole) molecular weight of water (lb/lb·mole) | = = = | 0.2074 29.89 18.00 | lb/lb∙mole lb/lb∙mole |
|--|--|-------------|--------------------------|--------------------------|
| Ms | = molecular weight of sample gas, wet basis (lb/lb·mole) | ·= | 27.42 | ib/ìb·mole |

EPA Method 1-4 Calculations

12. Velocity of sample gas (ft/sec)

$$V_{s} = (K_{p})(C_{p})\left(\sqrt{\Delta P}\right)\left(\sqrt{\frac{(\overline{T}_{s} + 460)}{(M_{s})(P_{s})}}\right)$$

Where:

| where. | | | | |
|----------------|---|---|--------|------------|
| Κ _ρ | = velocity pressure constant | = | 85.49 | |
| Cp | = pitot tube coefficient | = | 0.81 | |
| Ms | = wet molecular weight of sample gas, wet basis (lb/lb·mole) | = | 27.42 | lb/lb·mole |
| Ps | = absolute sample gas pressure (in. Hg) | = | 29.27 | in. Hg |
| Τ _s | = average sample gas temperature (°F) | = | 306.24 | ۴F |
| √∆P | = average square roots of velocity heads of sample gas (in. H ₂ O) | = | 0.730 | √in. H₂O |
| 460 | = °F to °R conversion constant | = | 460 | |
| Vs | = sample gas velocity (ft/sec) | = | 49.54 | ft/sec |
| | | | | |

13. Volumetric flow rate of sample gas at actual gas conditions (acfm)

$$Q_a = (60)(A_s)(V_s)$$

۷

| Where: | | | | |
|--------|--|---|-------|-----------------|
| As | = cross sectional area of sampling location (ft ²) | = | 64.00 | ft ² |
| Vs | = sample gas velocity (ft/sec) | = | 49.54 | ft/sec |
| 60 | conversion factor (sec/min) | = | 60 | sec/min |
| | | | | |

| Qa | = volumetric flow rate at actual conditions (acfm) | = | 190,226 | acfm |
|----|--|---|---------|------|
| - | | | | |

14. Total flow of sample gas (scfm)

| 0 | $-(\alpha)\left(\begin{array}{c}P_{s}\end{array}\right)$ | (68+460) |
|-------|--|--|
| Q_s | $= (Q_a) \left(\frac{P_s}{29.92} \right)$ | $\left(\frac{T_s + 460}{T_s + 460}\right)$ |

Where:

| withere. | | | | |
|----------------|---|---|---------|--------|
| Qa | volumetric flow rate at actual conditions (acfm) | = | 190,226 | acfm |
| Ps | = absolute sample gas pressure (in. Hg) | = | 29:27 | in. Hg |
| 29.92 | = standard pressure (in. Hg) | = | 29.92 | in. Hg |
| Τ _s | = average sample gas temperature (°F) | = | 306.2 | °F |
| 68 | = standard temperature (°F) | = | 68 | °F |
| 460 | = °F to °R conversion constant | - | 460 | |
| Qs | = volumetric flow rate at standard conditions, wet basis (scfm) | = | 128,236 | scfm |
| | | | | |

15. Dry flow of sample gas (dscfm)

Where:

| B _w Q _s | proportion of water vapor in the gas stream by volume volumetric flow rate at standard conditions, wet basis (scfm) | = | 0.2074 128,236 | scfm |
|----------------------------------|--|---|-------------------|-------|
| Q _{std} | = volumetric flow rate at standard conditions, dry basis (dscfm) | = | 101,644 | dscfm |

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16. Dry flow of sample gas corrected to 7%O₂ (dscfm)

$$\begin{aligned} \mathcal{Q}_{std 7} &= \left(\mathcal{Q}_{std}\right) \left(\frac{20.9 - O_2}{20.9 - 7}\right) \\ \end{aligned}$$
Where:

$$\begin{aligned} & \mathsf{Q}_{std} &= \mathsf{volumetric flow rate at standard conditions, dry basis (dscfm) &= 101,644 & dscfm \\ & \mathsf{O}_2 &= \mathsf{proportion of oxygen in the gas stream by volume (\%) &= 10.0 & \% \\ & 20.9 &= \mathsf{oxygen content of ambient air (\%)} &= 20.9 & \% \\ & 7 &= \mathsf{oxygen content of corrected gas (\%)} &= 7.0 & \% \\ & \mathsf{Q}_{std7} &= \mathsf{volumetric flow rate at STP and 7\%O_2, dry basis (dscfm)} &= 79,560 & dscfm \end{aligned}$$

Q_{std7} = volumetric flow rate at STP and 7%O₂, dry basis (dscfm) 79,560 =

17. Hourly time basis conversion of volumetric flow rate (Q_{std} example)

$$Q_{std-hr} = (Q_{std-min})(60)$$

Where

| Q _{std-min} 60 | volumetric flow rate, english units (ft³/min) conversion factor (min/hr) | = | 101,644 60 | dscfm min/hr |
|----------------------------|--|---|---------------|-----------------|
| Q _{std-hr} | = volumetric flow rate, hourly basis (dscf/hr) | = | 6,098,652 | dscf/hr |

18. Metric Conversion of Gas Volumes (Q_{std} example)

 $Q_{std-metric} = \left(Q_{std-english}\right)\left(\frac{60}{35,31}\right)$

| | (35.51) | | | | |
|--------------------------|--|---|---------|---------------------------------|--|
| Where: | | | | | |
| Q _{std-english} | = volumetric flow rate, english units (ft ³ /min) | = | 101,644 | dscfm | |
| 35.31 | = conversion factor (ft ³ /m ³) | = | 35.31 | ft ³ /m ³ | |
| 60 | = conversion factor (min/hr) | = | 60 | min/hr | |

Q_{std-metric} = volumetric flow rate, metric units (m³/hr) = 172,717 dry std m³/hr

19. Standard to Normal Conversion of Gas Volumes (Qstd example)

$$Q_{Normal} = \left(Q_{std-metric}\right) \left(\frac{32+460}{68+460}\right)$$

Where[.]

| Q _{Normal} | = volumetric flow rate, metric units (dry Nm ³ /hr) | = | 160,941 | dry Nm³/hr | |
|-------------------------|--|---|---------|---------------|--|
| 460 | = standard temperature in Rankine (68°F) | = | 460 | | |
| 68 | standard temperature (°F) | = | 68 | °F | |
| 32 | = normal temperature (°F) | = | 32 | ۴F | |
| Q _{std-metric} | = volumetric flow rate, metric units (dry std m³/hr) | = | 172,717 | dry std m³/hr | |

20. Percent isokinetic (%)

| $(0.09450)(\overline{T_s} +$ | $460 (V_{msid})$ |
|--|-------------------|
| $= \frac{(0.09450)(\overline{T_s} + (P_s)(V_s)(\overline{(D_n)^2(\pi)}))}{(144)(4)}$ | $(\Theta)(1-B_w)$ |

I

| D _n | a diameter of nozzle (in) | = | 0.268 | in. |
|-------------------|--|---|--------|--------|
| Bw | = proportion of water vapor in the gas stream by volume | = | 0.2074 | |
| Ps | = absolute sample gas pressure (in. Hg) | = | 29.27 | in. Hg |
| Τ _s | = average sample gas temperature (°F) | = | 306.2 | ۴F |
| V _{mstd} | volume of gas sample through the dry gas meter at standard conditions (dscf) | = | 38.207 | dscf |
| Vs | = sample gas velocity (ft/sec) | = | 49.54 | ft/sec |
| θ | = total sampling time (min) | = | 63 | min |
| 0.0945 | = conversion constant | = | 0.0945 | |
| 460 | = °F to °R conversion constant | = | 460 | |
| | | | | |
| I | = percent of isokinetic sampling (%) | = | 98.31 | % |

21. Alternative Method 5 Post-Test Meter Calibration Factor

EPA Method 1-4 Calculations

USEPA Method 13B HF Analyte Calculations

Sample data taken from Run 1

Note: The tables presenting the results are generated electronically from raw data. It may not be possible to exactly duplicate these results using a calculator. The reference method data, results, and all calculations are carried to sixteen decimal places throughout. The final table is formatted to an appropriate number of significant figures.

| | | | | 041210 144446 |
|------------------|--|---|---------|----------------|
| . Fluoride to HF | conversion factor | | | L |
| K_{HF} | $= \frac{MW_{HF}}{n \times MW_{FF}}$ | | | |
| Where: | F | | | |
| MWHE | = molecular weight of HF (mg/mg-mole) | = | 20.006 | mg/mg-mole |
| MW _{F-} | = molecular weight of fluoride ion (mg/mg-mole) | = | 18.998 | mg/mg-mole |
| n | = molar ratio of fluoride to HF | = | 1.0 | mole F/mole HF |
| K _{HF} | = conversion factor to convert mass F to mass HF | = | 1.053 | |
| Total HF collec | sted (mg) | | | |
| m _{HF} | $=K_{HF} \times \frac{(S_{F-1}v_1 + S_{F-2}v_2)}{1000}$ | | | |
| Where: | | | | |
| K _{HF} | = conversion factor to convert mass F to mass HF | = | 1.053 | |
| S _{F-1} | = fluoride concentration of sample fraction 1 (mg/liter) | = | <0.0380 | mg/liter |
| V ₁ | = liquid volume of sample fraction 1 (ml) | = | 900.0 | mi |
| S _{F-2} | = fluonde concentration of sample fraction 2 (mg/liter) | = | 0.0000 | mg/liter |
| V ₂ | = liquid volume of sample fraction 2 (ml) | = | 0.0 | m |
| 1000 | = conversion factor (ml/liter) | = | 1000 | ml/liter |
| m _{HF} | = total HF collected in sample (mg) | = | <0.0360 | mg |
| | Note: Non-detects are treated as zero in summations. | | | |

DEFINITION

Fraction 1 = entire sample except last impinger containing applicable absorbing reagent.

.

Fraction 2 = last impinger containing applicable absorbing reagent, analyzed separately to evaluate collection efficiency. If entire sample is analyzed as a single fraction, then data is included as Fraction 1 (Fraction 2 = 0).

`

3. Allowable blank subtraction (mg)

| <i>m</i> _b | $= K_{HF} \times B_{F} \times \frac{(v_{1} + v_{2})}{1000}$ | | | |
|-----------------------|---|---|---------|----------|
| <i>m</i> _b | $= 0$ if $B_F < MDL$ | | | |
| Where: | | | | |
| KHF | = conversion factor to convert mass F to mass HF | = | 1.053 | |
| B _F | = fluoride concentration of blank (mg/liter) | = | <0.0380 | mg/liter |
| V1 | = liquid volume of sample fraction 1 (ml) | = | 900.0 | ml |
| V ₂ | = liquid volume of sample fraction 2 (ml) | = | 0.0 | mi |
| 1000 | = conversion factor (ml/liter) | = | 1000 | ml/liter |
| m _b | = allowable blank subtraction (mg) | = | 0.0000 | mg |

4. Total HF collected, corrected for blank (mg)

$$m_{nb} = m_{HF} - m_b$$

Where:

| m _{HF} m _b | = total HF collected in sample (mg) = allowable blank subtraction (mg) | = | <0.0360 0.0000 | mg mg | |
|-----------------------------------|---|---|-------------------|----------|--|
| m _{nb} | = total HF collected, corrected for blank (mg) | = | <0.0360 | mg | |

5. Minimum detectable HF (mg)

$$m_{MDL} = K_{HF} \times MDL \times \frac{(v_1 + v_2)}{1000}$$

Where:

| vynere. | | | | | |
|-----------------|--|---|--------|----------|--|
| K _{HF} | = conversion factor to convert mass F to mass HF | = | 1.053 | | |
| MDL | = minimum detectable fluoride concentration | = | 0.008 | mg/liter | |
| V1 | = liquid volume of sample fraction 1 (ml) | = | 900.0 | mi | |
| V ₂ | = liquid volume of sample fraction 2 (ml) | = | 0.0 | ml | |
| 1000 | = conversion factor (ml/liter) | 2 | 1000 | ml/liter | |
| - | - minimum datastable UE (ma) | _ | 0.0076 | | |
| MMDL | = minimum detectable HF (mg) | = | 0.0076 | mg | |
| | | | | | |

6. Total HF value used in emission calculations (mg)

USEPA Method 13B HF Analyte Calculations

USEPA Method 13B HF Sample Calculations

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N_L

Wheelabrator North Broward, Inc. Clean Air Project No: 10955 Unit 2 FF Outlet

USEPA Method 13B HF Sample Calculations

Sample data taken from Run 1

Note: The tables presenting the results are generated electronically from raw data. It may not be possible to exactly duplicate these results using a calculator. The reference method data, results, and all calculations are carried to sixteen decimal places throughout. The final table is formatted to an appropriate number of significant figures.

1. HF concentration (lb/dscf)

$$C_{sd} = \left(\frac{m_n}{V}\right) \left(\frac{2.205 \times 10^{-10}}{100}\right)$$

 $= \left(\frac{m_n}{V_{mstd}}\right) \left(\frac{2.205 \times 10^{-3}}{1000}\right)$

| m _n V _{mstd} | = total HF collected, corrected for applicable blank (mg) = volume metered, standard (dscf) | = | <0.0360 38.2069 | mg dscf |
|-------------------------------------|---|-----|--------------------|--------------|
| 2.205 x 10 ⁻³ 1000 | = conversion factor (lb/g) = conversion factor (mg/g) | = | 2.205E-03 1.000 | lb/g mg/g |
| | | | ., | 00 |
| C _{sd} | = HF concentration (lb/dscf) | = < | <2.0784E-09 | iD/dscf |

2. HF concentration (ppmdv)

Where:

 C_{sd}

 $= \left(\frac{m_n}{V_{mstd}}\right) \left(\frac{0.850}{1000}\right) \left(\frac{10^6}{MW}\right)$

| (| <0.0360 mg 38.2069 dscf |
|-----|----------------------------|
| (| |
| = 3 | 28 2060 deaf |
| | 30.2008 USCI |
| = | 20.006 g/g-mole |
| = | 0.850 dscf/g-mole |
| = | 1,000 mg/g |
| = | 10 ⁶ ppm |
| = < | <0.0400 ppmdv |
| | и п п и |

 $= C_{sd} \left(1 - \frac{B_w}{100} \right)$

C_w Where:

| Where: | | | | |
|-----------------|-------------------------------------|---|---------|-------|
| C _{sd} | = HF concentration (ppmdv) | = | <0.0400 | ppmdv |
| Bw | = actual water vapor in gas (% v/v) | = | 20.7366 | % v/v |
| 100 | = conversion factor (%) | = | 100 | % |
| C" | = HF concentration (ppmwv) | = | <0.0317 | ppmwv |

4. HF concentration (mg/dscm)

$$C_{sd} = \left(\frac{m_n}{V_{mstd}}\right) (35.31)$$

Where:

:

| m _n V _{mstd} 35.31 | total HF collected, corrected for applicable blank (mg) volume metered, standard (dscf) conversion factor (dscf/dscm) | = = | <0.0360 38.2069 35.31 | mg dscf dscf/dscm | |
|--|---|--------|-----------------------------|-------------------------|--|
| C _{sd} | = HF concentration (mg/dscm) | = | <0.0333 | mg/dscm | |

5. HF concentration (mg/Nm³ dry)

$$= \left(\frac{m_n}{V_{nstd}}\right) (35.31) \left(\frac{68+460}{32+460}\right)$$

Where:

 C_{sd}

| = total HF collected, corrected for applicable blank (mg) | = | <0.0360 | mg |
|---|--|---|---|
| = volume metered, standard (dscf) | = | 38.2069 | dscf |
| = conversion factor (dscf/dscm) | = | 35.31 | dscf/dscm |
| = standard temperature (°F) | = | 68 | °F |
| = normal temperature (°F) | = | 32 | °F |
| = °F to °R conversion constant | = | 460 | |
| = HF concentration (mg/Nm ³ dry) | = | <0.0357 | mg/Nm ³ dry |
| | volume metered, standard (dscf) conversion factor (dscf/dscm) standard temperature (°F) normal temperature (°F) °F to °R conversion constant | = volume metered, standard (dscf)== conversion factor (dscf/dscm)== standard temperature (°F)== normal temperature (°F)== °F to °R conversion constant= | = volume metered, standard (dscf)= 38.2069= conversion factor (dscf/dscm)= 35.31= standard temperature (°F)= 68= normal temperature (°F)= 32= °F to °R conversion constant= 460 |

6. HF concentration corrected to x% O₂ (ppmdv example)

$$C_{sdx} = C_{sd} \left(\frac{20.9 - x}{20.9 - O_2} \right)$$

Where:

| vvilere. | | | | |
|----------------|---|---|---------|--------------------------|
| C_{sd} | = HF concentration (ppmdv) | = | <0.0400 | ppmdv |
| x | = oxygen content of corrected gas (%) | = | 7.0 | % |
| O ₂ | = proportion of oxygen in the gas stream by volume (%) | z | 10.0 | % |
| 20.9 | = oxygen content of ambient air (%) | = | 20.9 | % |
| Csdx | = HF concentration corrected to x %O ₂ (ppmdv) | = | <0.0512 | ppmdv @ x%O ₂ |
| - 502 | | | 10.0012 | FF |

7. HF concentration corrected to y% CO₂ (ppmdv example)

 $\frac{y}{CO_2}$

$$C_{sdy} = C_{sd}$$

Where:

| Where: | | | | | |
|------------------|--|---|---------|---------------|--|
| C_{sd} | = HF concentration (ppmdv) | = | <0.0400 | ppmdv | |
| у | = carbon dioxide content of corrected gas (%) | = | 12.0 | % | |
| CO2 | = proportion of carbon dioxide in the gas stream by volume (%) | = | 9.3 | % | |
| C _{sdy} | = HF concentration corrected to y%CO ₂ (ppmdv) | = | <0.0517 | ppmdv @ y%CO2 | |

USEPA Method 13B HF Sample Calculations

8. HF concentration at actual gas conditions (lb/acf example)

 $=C_{sd}\left(\frac{Q_{std}}{Q_a}\right)$

 C_a Wh

| Where: | | | | |
|--------------------------|---|---|-------------|---------|
| C _{sd} | = HF concentration (lb/dscf) | = | <2.0784E-09 | lb/dscf |
| Q _{std} | = volumetric flow rate at standard conditions, dry basis (dscfm) | = | 101,644 | dscfm |
| Qa | = volumetric flow rate at actual conditions (acfm) | = | 190,226 | acfm |
| Ca | = HF concentration at actual gas conditions (ib/acf) | = | <1.1105E-09 | lb/acf |
| 9. HF rate (lb/hr) | | | | |
| $E_{lb/hr}$ | $= \left(\frac{m_n}{V_{mstd}}\right) \left(\frac{2.205 \times 10^{-3}}{1000}\right) (\mathcal{Q}_{std}) (60)$ | | | |
| Where: | | | | |
| mn | = total HF collected, corrected for applicable blank (mg) | = | <0.0360 | mg |
| V _{mstd} | = volume metered, standard (dscf) | = | 38.2069 | dscf |
| 2.205 x 10 ⁻³ | = conversion factor (lb/g) | = | 2.205E-03 | ib/g |
| 1000 | = conversion factor (mg/g) | = | 1,000 | mg/g |
| Q _{std} | volumetric flow rate at standard conditions, dry basis (dscfm) | = | 101,644 | dscfm |
| 60 | ≈ conversion factor (min/hr) | = | 60 | min/hr |
| E _{ib/hr} | ≈ HF rate (lb/hr) | = | <0.0127 | ib/hr |

10. HF rate (kg/hr)

Where: m'n

60

 $E_{kg/hr}$

 $= \left(\frac{m_n}{V_{mstd}}\right) \left(\frac{(Q_{std})(60)}{10^6}\right)$

= total HF collected, corrected for applicable blank (mg) = < 0.0360 mg V_{mstd} = volume metered, standard (dscf) = 38.2069 dscf $\mathbf{Q}_{\mathsf{std}}$ = volumetric flow rate at standard conditions, dry basis (dscfm) dscfm = 101,644 = conversion factor (min/hr) min/hr 60 = 10⁶ = conversion factor (mg/kg) g/kg = 10⁶ E_{kg/hr} = HF rate (kg/hr) = <0.0057 kg/hr

 (α)

11. HF rate (Ton/yr)

$$E_{T/yr}$$

$$= \left(\frac{m_n}{V_{mstd}}\right) \left(\frac{2.205 \times 10^{-3}}{1000}\right) (Q_{std}) (60) \left(\frac{Cap}{2000}\right)$$

Where:

| mn | = total HF collected, corrected for applicable blank (mg) | = | <0.0360 | mg |
|--------------------------|--|---|-----------|----------|
| V _{mstd} | = volume metered, standard (dscf) | = | 38.2069 | dscf |
| 2.205 x 10 ⁻³ | = conversion factor (lb/g) | = | 2.205E-03 | lb/g |
| 1000 | = conversion factor (mg/g) | = | 1,000 | mg/g |
| Q _{std} | = volumetric flow rate at standard conditions, dry basis (dscfm) | ≒ | 101,644 | dscfm |
| 60 | = conversion factor (min/hr) | = | 60 | min/hr |
| Cap | = capacity factor for process (hours operated/year) | = | 8,760 | hours/yr |
| 2000 | = conversion factor (lb/Ton) | = | 2,000 | ib/Ton |
| | | | | |
| E _{T/yr} | = HF rate (Ton/yr) | = | <0.0555 | Ton/yr |
| | | | | |

12. HF rate - F_d-based (lb/MMBtu)

$$E_{Fd} = \left(\frac{m_n}{V_{mstd}}\right) \left(\frac{2.205 \times 10^{-3}}{1000}\right) \left(F_d\right) \left(\frac{20.9}{20.9 - O_2}\right)$$
Where:

$$m_n = \text{total HF collected, corrected for applicable blank (mg)} = <0.0360 \text{ mg}$$

$$V_{mstd} = \text{volume metered, standard (dscf)} = 38.2069 \text{ dscf}$$

$$2.205 \times 10^{-3} = \text{conversion factor (lb/g)} = 2.205E-03 \text{ lb/g}$$

$$1000 = \text{conversion factor (mg/g)} = 1,000 \text{ mg/g}$$

$$F_d = \text{ratio of gas volume to heat content of fuel (dscf/MMBtu)} = 9,570 \text{ dscf/MMBtu}$$

$$O_2 = \text{proportion of oxygen in the gas stream by volume (%)} = 10.0 \%$$

$$E_{Fd} = \text{HF rate (lb/MMBtu)} = 4.2000 \text{ mg/g}$$

13. HF rate - Fc-based (lb/MMBtu)

$$E_{F_c} = \left(\frac{m_n}{V_{mstd}}\right) \left(\frac{2.205 \times 10^{-3}}{1000}\right) (F_c) \left(\frac{100}{CO_2}\right)$$

Where:

m'n = total HF collected, corrected for applicable blank (mg) = < 0.0360 mg V_{mstd} = volume metered, standard (dscf) 38.2069 dscf = 2.205 x 10⁻³ = conversion factor (lb/g) 2.205E-03 = lb/g 1000 = conversion factor (mg/g) = 1,000 mg/g Fc = ratio of gas volume to heat content of fuel (dscf/MMBtu) = 1,820 dscf/MMBtu CO₂ = proportion of oxygen in the gas stream by volume (%) = 9.3 % 100 = conversion factor Ξ 100 \mathbf{E}_{Fc} = HF rate (lb/MMBtu) = <4.0717E-05 lb/MMBtu

QA/QC Date

USEPA Method 13B HF Sample Calculations

EPA Method 1-4 Calculations

USEPA Method 23 (PCDD/F) Sampling, Velocity and Moisture Sample Calculations

Sample data taken from Run 1

Note: The tables presenting the results are generated electronically from raw data. It may not be possible to exactly duplicate these results using a calculator. The reference method data, results, and all calculations are carried to sixteen decimal places throughout. The final table is formatted to an appropriate number of significant figures.

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1. Volume of water collected (wscf)

$$V_{wstd} = (0.04706)(V_{k})$$

Where:

| V _{ic} 0.04706 | = total volume of liquid collected in impingers and silica gel (ml) □ ideal gas conversion factor (ft ³ water vapor/ml or gm) | = | 836.5 0.04706 | ml ft ³ /ml |
|----------------------------|--|---|------------------|---------------------------|
| V _{wstd} | = volume of water vapor collected at standard conditions (ft ³) | = | 39.37 | ft ³ |

2. Volume of gas metered, standard conditions (dscf)

$$=\frac{(17.64)(V_m)\left(P_{bar}+\frac{\Delta H}{13.6}\right)(Y_d)}{(460+T_m)}$$

W

V_{mstd}

| Where: | | | | |
|-------------------|---|---|---------|----------------------------|
| Pbar | = barometric pressure (in. Hg) | = | 30.00 | in. Hg |
| T _m | = average dry gas meter temperature (°F) | = | 80.05 | °F |
| V _m | volume of gas sample through the dry gas meter at meter conditions (dcf) | = | 160.35 | dcf |
| Yd | = gas meter correction factor (dimensionless) | = | 0.9901 | |
| ΔH | = average pressure drop across meter box orifice (in. H ₂ O) | = | 1.29 | in. H₂O |
| 17.64 | = standard temperature to pressure ratio (°R/in. Hg) | = | 17.64 | °R/in, Hg |
| 13.6 | = conversion factor (in. H_2O/in . Hg) | = | 13.6 | in.H ₂ O/in. Hg |
| 460 | = °F to °R conversion constant | = | 460 | |
| V _{mstd} | volume of gas sampled through the dry gas meter at standard conditions (dscf) | = | 156.061 | dscf |

3. Sample gas pressure (in. Hg)

$$= P_{bar} + \left(\frac{P_g}{13.6}\right)$$

M/horo

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| Willici C. | | | | | |
|------------------|---|---|--------|-----------------------------|--|
| P _{bar} | = barometric pressure (in. Hg) | = | 30.00 | in. Hg | |
| Pg | = sample gas static pressure (in. H ₂ O) | = | -12.00 | in. H ₂ O | |
| 13.6 | = conversion factor (in. $H_2O/in. Hg$) | = | 13.6 | in. H ₂ O/in. Hg | |
| Ps | = absolute sample gas pressure (in. Hg) | = | 29.12 | in. Hg | |

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4. Actual water vapor pressure at sample gas temperature less than 212°F (in. Hg)

 P_{v}

$$=\frac{e^{\left(18.3036-\frac{3816.44}{\frac{1}{9}(7,-32)+273.15-46.13}\right)}}{25.4}$$

Where:

| where: | | | | |
|---------|---|---|---------|--------------|
| Ts | = average sample gas temperature (°F) | = | 300.64 | °F |
| 18.3036 | = Antoine coefficient | = | 18.3036 | °K |
| 3816.44 | = Antoine coefficient | = | 3816.44 | °K |
| 273.15 | = temperature conversion factor | = | 273.15 | ۳κ |
| 46.13 | = Antoine coefficient | = | 46.13 | °K |
| 25.4 | = conversion factor | = | 25.4 | mm Hg/in. Hg |
| 5/9 | = Fahrenheit to Celsius conversion factor | = | 5/9 | °C/°F |
| 32 | = temperature conversion (°F) | = | 32 | °F |
| Pv | = vapor pressure, actual (in. Hg) | = | 29.12 | in. Hg |
| | | | | |

5. Water vapor pressure at gas temperature greater than 212°F (in. Hg)

| P_{v} | $= P_s$ | | | |
|--------------------------|---|---|-------|--------|
| Where: P _s | = absolute sample gas pressure (in. Hg) | = | 29.12 | in. Hg |
| Pv | = water vapor pressure, actual (in. Hg) | z | 29.12 | in. Hg |

6. Moisture measured in sample (% by volume)

$$B_{wo} = \frac{V_{wstd}}{\left(V_{mstd} + V_{wstd}\right)}$$

W

| Nhere: | | | | |
|-------------------|---|---|---------|------|
| V _{mstd} | volume of gas sampled through the dry gas meter at standard conditions (dscf) | = | 156.061 | dscf |
| V _{wstd} | = volume of water collected at standard conditions (scf) | = | 39.37 | scf |
| B _{wo} | = proportion of water measured in the gas stream by volume | = | 0.2014 | |
| | | = | 20.14 | % |

7. Saturated moisture content (% by volume)

 $B_{ws} = \frac{P_v}{P_s}$

Where:

| P _s | = absolute sample gas pressure (in. Hg) | = | 29.12 | in. Hg | |
|-----------------|--|---|------------------|--------|--|
| P _v | = water vapor pressure, actual (in. Hg) | = | 29.12 | in. Hg | |
| B _{ws} | = proportion of water vapor in the gas stream by volume at saturated conditions | = | 1.0000 100.00 | % | |

8. Actual water vapor in gas (% by volume)

$$B_{w} = MINIMUM [B_{wo}, B_{ws}]$$

Where:

| B _{ws} | proportion of water vapor in the gas stream by volume at saturated conditions | = | 1.0000 | |
|-----------------|---|---|--------|---|
| B _{wo} | = proportion of water measured in the gas stream by volume | = | 0.2014 | |
| B _w | = actual water vapor in gas | = | 0.2014 | |
| | | = | 20.14 | % |

9. Nitrogen (plus carbon monoxide) in gas stream (% by volume, dry)

$$N_2 + CO = 100 - CO_2 - O_2$$

Where:

| CO ₂ · | proportion of carbon dioxide in the gas stream by volume (%) proportion of oxygen in the gas stream by volume (%) conversion factor (%) | = | 9.7 | % |
|--------------------|---|---|-------|---|
| O ₂ | | = | 9.7 | % |
| 100 | | = | 100 | % |
| N ₂ +CO | = proportion of nitrogen and CO in the gas stream by volume (%) | = | 80.58 | % |

= proportion of nitrogen and CO in the gas stream by volume (%) = N₂+CO 80.58

10. Molecular weight of dry gas stream (Ib/Ib-mole)

| M_d | $= \left(M_{CO_2}\right) \frac{(CO_2)}{(100)} + \left(M_{O_2}\right) \frac{(O_2)}{(100)} + \left(M_{N_2+CO}\right) \frac{(N_2+CO)}{(100)}$ | | | |
|--------------------|--|---|-------|------------|
| Where: | | | | |
| M _{CO2} | = molecular weight of carbon dioxide (lb/lb·mole) | = | 44.00 | lb/lb mole |
| M _{O2} | = molecular weight of oxygen (lb/lb·mole) | = | 32.00 | lb/łb·mole |
| M _{N2+CO} | = molecular weight of nitrogen and carbon monoxide (lb/lb·mole) | = | 28.00 | lb/lb·mole |
| CO2 | = proportion of carbon dioxide in the gas stream by volume (%) | = | 9.7 | % |
| O ₂ | = proportion of oxygen in the gas stream by volume (%) | = | 9.7 | % |
| N ₂ +CO | = proportion of nitrogen and CO in the gas stream by volume (%) | = | 80.6 | % |
| 100 | = conversion factor (%) | = | 100 | % |
| Md | = dry molecular weight of sample gas (lb/lb·mole) | = | 29.95 | lb/lb·mole |

11. Molecular weight of sample gas (Ib/Ib·mole)

$$M_{s} = (M_{d})(1-B_{w}) + (M_{H_{2}O})(B_{w})$$

Where:

| B _w M _d M _{H2O} | proportion of water vapor in the gas stream by volume dry molecular weight of sample gas (lb/lb·mole) molecular weight of water (lb/lb·mole) | | 0.2014 29.95 18.00 | lb/lb∙mole lb/lb∙mole |
|--|--|---|--------------------------|--------------------------|
| Ms | = molecular weight of sample gas, wet basis (lb/lb·mole) | = | 27.54 | lb/lb·mole |

EPA Method 1-4 Calculations

12. Velocity of sample gas (ft/sec)

$$V_{s} = (K_{p})(C_{p})(\sqrt{\Delta P})\left(\sqrt{\frac{(\overline{T_{s}} + 460)}{(M_{s})(P_{s})}}\right)$$

Where:

| VVIICIC. | | | | |
|----------------|---|---|--------|------------|
| К _р | = velocity pressure constant | = | 85.49 | |
| Cp | = pitot tube coefficient | = | 0.83 | |
| Ms | = wet molecular weight of sample gas, wet basis (lb/lb·mole) | = | 27.54 | lb/lb·mole |
| Ps | = absolute sample gas pressure (in. Hg) | = | 29.12 | in. Hg |
| Τ _s | = average sample gas temperature (°F) | = | 300.64 | °F |
| √∆P | = average square roots of velocity heads of sample gas (in. H ₂ O) | = | 0.746 | √in. H₂O |
| 460 | = °F to °R conversion constant | = | 460 | |
| Vs | = sample gas velocity (ft/sec) | = | 51.81 | ft/sec |
| - 5 | | | 01.01 | 10300 |

13. Volumetric flow rate of sample gas at actual gas conditions (acfm)

$$Q_a = (60)(A_s)(V_s)$$

۱

| Where: | | | | |
|--------|--|---|---------|-----------------|
| As | = cross sectional area of sampling location (ft ²) | = | 64.00 | ft ² |
| Vs | = sample gas velocity (ft/sec) | = | 51.81 | ft/sec |
| 60 | conversion factor (sec/min) | = | 60 | sec/min |
| Qa | = volumetric flow rate at actual conditions (acfm) | = | 198,967 | acfm |

14. Total flow of sample gas (scfm)

 $= (Q_a) \left(\frac{P_s}{29.92} \right) \left(\frac{68 + 460}{T_s + 460} \right)$ Q_s

| Where: | |
|--------|------------------------------|
| Qa | = volumetric flow rate at ac |
| D | ≂ obsoluto somolo ass pro |

| Qa | = volumetric flow rate at actual conditions (acfm) | = | 198,967 | acfm |
|-------|---|---|---------|--------|
| Ps | ≈ absolute sample gas pressure (in. Hg) | = | 29.12 | in. Hg |
| 29.92 | = standard pressure (in. Hg) | = | 29.92 | in. Hg |
| Τs | = average sample gas temperature (°F) | = | 300.6 | °F |
| 68 | = standard temperature (°F) | = | 68 | °F |
| 460 | = °F to °R conversion constant | = | 460 | |
| Qs | = volumetric flow rate at standard conditions, wet basis (scfm) | ~ | 134,410 | scfm |

15. Dry flow of sample gas (dscfm)

 $= (Q_s)(1 - B_w)$ Q std

Where:

| B _w Q _s | proportion of water vapor in the gas stream by volume volumetric flow rate at standard conditions, wet basis (scfm) | = | 0.2014 134,410 | scfm |
|----------------------------------|--|---|-------------------|-------|
| Q _{std} | = volumetric flow rate at standard conditions, dry basis (dscfm) | = | 107,335 | dscfm |

16. Dry flow of sample gas corrected to 7%O₂ (dscfm)

$$Q_{std 7} = (Q_{std}) \left(\frac{20.9 - O_2}{20.9 - 7} \right)$$

Where:

| Q _{std} | = volumetric flow rate at standard conditions, dry basis (dscfm) | = | 107,335 | dscfm | |
|------------------|--|---|---------|-------|--|
| O ₂ | = proportion of oxygen in the gas stream by volume (%) | = | 9.7 | % | |
| 20.9 | = oxygen content of ambient air (%) | = | 20.9 | % | |
| 7 | = oxygen content of corrected gas (%) | = | 7.0 | % | |
| | | | | | |

| Q _{std7} | = volumetric flow rate at STP and 7%O ₂ , dry basis (dscfm) | = | 86,640 | dscfm |
|-------------------|--|---|--------|--------------|
| Std7 | | - | 00,040 | U 301 |

17. Hourly time basis conversion of volumetric flow rate (Q_{std} example)

$$Q_{std - hr} = (Q_{std - min})(60)$$

Where

| Q _{std-min} | volumetric flow rate, english units (ft³/min) conversion factor (min/hr) | н | 107,335 | dscfm |
|----------------------|--|---|-----------|---------|
| 60 | | П | 60 | min/hr |
| Q _{std-hr} | ≍ volumetric flow rate, hourly basis (dscf/hr) | = | 6,440,103 | dscf/hr |

18. Metric Conversion of Gas Volumes (Q_{std} example)

$$Q_{std-metric} = (Q_{std-english}) \left(\frac{60}{35.31}\right)$$

Where:

vnere:
$$Q_{std-english}$$
= volumetric flow rate, english units (ft³/min)= 107,335dscfm35.31= conversion factor (ft³/m³)= 35.31ft³/m³60= conversion factor (min/hr)= 60min/hr

$$Q_{std-metric}$$
 = 182,388 dry std m³/hr) = 182,388 dry std m³/hr

19. Standard to Normal Conversion of Gas Volumes (Q_{std} example)

$$Q_{Normal} = (Q_{std-metric}) \left(\frac{32+460}{68+460} \right)$$

Where:

| Q _{Normal} | = volumetric flow rate, metric units (dry Nm ³ /hr) | = | 169,952 | dry Nm³/hr | |
|-------------------------|---|---|---------|---------------|--|
| 460 | = standard temperature in Rankine (68°F) | = | 460 | | |
| 68 | standard temperature (°F) | 5 | 68 | °F | |
| 32 | = normal temperature (°F) | = | 32 | °F | |
| Q _{std-metric} | = volumetric flow rate, metric units (dry std m ^o /hr) | = | 182,388 | dry std m³/hr | |

20. Percent isokinetic (%)

I

Where:

$$=\frac{(0.09450)(\overline{T_s}+460)(V_{mstd})}{(P_s)(V_s)((\overline{D_s})^2(\pi))(\Theta)(1-B_w)}$$

| D _n | = diameter of nozzle (in) | = | 0.264 | in. |
|-------------------|--|---|---------|--------|
| Bw | = proportion of water vapor in the gas stream by volume | = | 0.2014 | |
| Ps | = absolute sample gas pressure (in. Hg) | = | 29.12 | in. Hg |
| Τs | = average sample gas temperature (°F) | = | 300.6 | °F |
| V _{mstd} | volume of gas sample through the dry gas meter at standard conditions (dscf) | = | 156.061 | dscf |
| Vs | = sample gas velocity (ft/sec) | = | 51.81 | ft/sec |
| θ | = total sampling time (min) | = | 250 | min |
| 0.0945 | = conversion constant | = | 0.0945 | |
| 460 | = °F to °R conversion constant | = | 460 | |
| | | | | |
| I | = percent of isokinetic sampling (%) | = | 97.97 | % |
| | | | | |

21. Alternative Method 5 Post-Test Meter Calibration Factor

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USEPA Method 23 PCDD/PCDF Emissions Calculations

USEPA Method 23 PCDD/PCDF Emissions Calculations

Sample data taken from Run 1

Note: The tables presenting the results are generated electronically from raw data. It may not be possible to exactly duplicate these results using a calculator. The reference method data, results and all calculations are carried to sixteen decimal places throughout. The final table is formatted to an appropriate number of significant figures.

Note: PCDD/F results may be presented in two formats - normally expected levels and the maximum possible levels. In the normal case, data classified as ND (non-detect) or EMPC (estimated maximum possible concentration) are not counted. In the maximum possible emissions case, NDs and EMPCs are fully counted.

| 1. TEQ concentra | ation (ng/dscm) | | Normal Case (ND & EMPC = 0 | | Maximum Cas (ND & EMPC fully co | • |
|--------------------|---|---|-------------------------------|---------------------------|------------------------------------|----------------------------|
| C_{sd} | $= \left(\frac{m_{n_{-}TEQ}}{V_{mstd}}\right) \times 35.31$ | | | | | |
| Where: | | | | | | |
| m _{n_TEQ} | = total TEQ mass for PCDDs and PCDFs (ng) | = | 1.6800E-02 | ng | 2.1100E-02 | ng |
| Vmstd | = volume metered, standard (dscf) | = | 156.0614 | dscf | 156.0614 | dscf |
| 35.31 | = conversion factor (dscf/dscm) | = | 35.31 | dscf/dscm | 35.31 | dscf/dscm |
| C _{sd} | = PCDD/F TEQ concentration (ng/dscm) | = | 3.8011E-03 | ng/dscm | 4.7740E-03 | ng/dscm |
| 2. TEQ concentra | tion (ng/Nm3 dry) | | | | | |
| C _{sd} | $= \left(\frac{m_{n_TEQ}}{V_{mstd}}\right) (35.31) \left(\frac{68+460}{32+460}\right)$ | | | | | |
| Where: | | | | | | |
| m _{n_TEQ} | = total TEQ mass for PCDDs and PCDFs (ng) | = | 1.6800E-02 | ng | 2.1100E-02 | ng |
| V _{mstd} | = volume metered, standard (dscf) | = | 156.0614 | dscf | 156.0614 | dscf |
| 35.31 | = conversion factor (dscf/dscm) | = | 35.31 | dscf/dscm | 35.31 | dscf/dscm |
| 68 . | = standard temperature (°F) | = | 68 | °F | 68 | ۴F |
| 32 | = normal temperature (°F) | = | 32 | °F | 32 | ۴F |
| 460 | = °F to °R conversion constant | = | 460 | | 460 | |
| C _{sd} | = PCDD/F TEQ concentration (ng/Nm3 dry) | = | 4.0792E-03 | ng/Nm ³ dry | 5.1233E-03 | ng/Nm ³ dry |
| 3. TEQ concentra | tion at actual gas conditions (ng/acm example) | | | | | |
| C _a | $= C_{sd} \left(\frac{Q_{std}}{Q_a} \right)$ | | | | | |
| Where: | | | | | | |
| C _{sd} | = PCDD/F TEQ concentration (ng/dscm) | = | 3.8011E-03 | ng/dscm | 4.7740E-03 | ng/dscm |
| Q _{std} | = volumetric flow rate at standard conditions, dry basis (dscm/h) | = | 182,388 | dry std m ³ /h | r 182,388 | dry std m ³ /hr |

| C _{sd} Q _{std} Q _a | PCDD/F TEQ concentration (ng/oscm) volumetric flow rate at standard conditions, dry basis (dscm/h) volumetric flow rate at actual conditions (acm/h) | - | 3.8011E-03 182,388 338,092 | ng/dscm dry std m ³ /hr actual m ³ /hr | 4.7740E-03 182,388 338,092 | ng/dscm dry std m ³ /hr actual m ³ /hr |
|---|--|---|----------------------------------|--|----------------------------------|--|
| Ca | = PCDD/F TEQ concentration at actual gas conditions (ng/acm) | = | 2.0506E-03 | ng/acm | 2.5754E-03 | ng/acm |

USEPA Method 23 PCDD/PCDF Emissions Calculations

4. TEQ concentration corrected to x% O2 (ng/dscm example)

$$C_{sdx} = C_{sd} \left(\frac{20.9 - x}{20.9 - O_2} \right)$$

Wh

| where. | | | | | | | |
|-----------------|--|---|------------|-----------|------------|-----------|--|
| C _{ad} | PCDD/F TEQ concentration (ng/dscm) | = | 3.8011E-03 | ng/dscm | 4.7740E-03 | ng/dscm | |
| x | = oxygen content of corrected gas (%) | = | 7.0 | % | 7.0 | % | |
| O ₂ | proportion of oxygen in the gas stream by volume (%) | = | 9.7 | % | 9.7 | % | |
| 20.9 | = oxygen content of ambient air (%) | = | 20.9 | % | 20.9 | % | |
| <u> </u> | - PCDD/E TEO concentration (inc/decm corrected to $v% O$) | _ | 4 7001E 02 | naldaam @ | E 0142E 02 | naldeen @ | |

Csda DD/F TEQ concentration (ng/dscm corrected to x% O₂) 4.7091E-03 ng/dscm @ 5.9143E-03 ng/dscm @ x% O₂ x% O₂

5. TEQ concentration corrected to y% CO2 (ng/dscm example)

$$= C_{sd} \left(\frac{y}{CO_2} \right)$$

Where:

 C_{sdy}

= PCDD/F TEQ concentration (ng/dscm) 3.8011E-03 ng/dscm 4.7740E-03 C_{sd} = ng/dscm v = carbon dioxide content of corrected gas (%) = 12.0 % 12.0 % CO2 = proportion of carbon dioxide in the gas stream by volume (%) = 9.7 % % 9.7 = PCDD/F TEQ concentration (ng/dscm corrected to y% CO₂) = 4.6831E-03 5.8818E-03 ng/dscm @ Csdy ng/dscm @ y% CO₂ y% CO₂

6. TEQ Emission rate (lb/hr)

$$E_{lb/hr} = \left(\frac{m_{n_TEQ}}{V_{mstd}}\right) (2.205 \times 10^{-3}) (Q_{std}) \frac{(60)}{(10^{9})}$$

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| ۱ | /vnere: | | | | | | |
|---|--------------------------|--|---|------------|--------|------------|--------|
| | mn_TEQ | = total TEQ mass for PCDDs and PCDFs (ng) | = | 1.6800E-02 | ng | 2.1100E-02 | ng |
| | V _{mstd} | = volume metered, standard (dscf) | = | 156.0614 | dscf | 156.0614 | dscf |
| | 2.205 x 10 ⁻³ | = conversion factor (lb/g) | × | 2.205E-03 | lb/g | 2.205E-03 | lb/g |
| | Q _{std} | = volumetric flow rate at standard conditions, dry basis (dscfm) | z | 107,335 | dscfm | 107,335 | dscfm |
| | 60 | = conversion factor (min/hr) | = | 60 | min/hr | 60 | min/hr |
| | 10 ⁹ | = conversion factor to convert from ng to grams | = | 1.0E+09 | ng/g | 1.0E+09 | ng/g |
| | Elbyhr | = PCDDF TEQ Emission rate (lb/hr) | Ξ | 1.5287E-09 | lb/hr | 1.9199E-09 | lb/hr |

7. TEQ Emission rate (g/sec)

 $E_{g/sec}$

$$= \left(\frac{m_{n_{-}TEQ}}{V_{mstd}}\right) \left(\frac{Q_{std}}{60 \times 10^{9}}\right)$$

Where: = total TEQ mass for PCDDs and PCDFs (ng) = 1.6800E-02 ng 2.1100E-02 ng m_{n_TEQ} V_{msid} = volume metered, standard (dscf) 156.0614 dscf 156.0614 dscf 107,335 Q_{std} = volumetric flow rate at standard conditions, dry basis (dscfm) = dscfm 107,335 dscfm 60 = conversion factor (sec/min) 60 sec/min = 60 sec/min 10⁹ = conversion factor to convert from ng to grams = 1.0E+09 1.0E+09 ng/g ng/g E_{g/sec} = PCDDF TEQ Emission rate (g/sec) = 1.9258E-10 2.4187E-10 g/sec a/sec

.__

8. TEQ emission rate (Ton/yr)

$$E_{T/yr} = \left(\frac{m_{n_TEQ}}{V_{mstd}}\right) \left(\frac{2.205 \times 10^{-3}}{10^9}\right) (Q_{std}) (60) \left(\frac{Cap}{2000}\right)$$

Where:

| incle. | | | | | | |
|--------------------------|--|---|------------|----------|------------|----------|
| m _{n_TEQ} | = total TEQ mass for PCDDs and PCDFs (ng) | = | 1.6800E-02 | ng | 2.1100E-02 | ng |
| V _{mstd} | = volume metered, standard (dscf) | = | 156.0614 | dscf | 156.0614 | dscf |
| 2.205 x 10 ⁻³ | = conversion factor (lb/g) | = | 2.205E-03 | lb/g | 2.205E-03 | lb/g |
| Q _{std} | = volumetric flow rate at standard conditions, dry basis (dscfm) | = | 107,335 | dscfm | 107,335 | dscfm |
| 60 | = conversion factor (min/hr) | = | 60 | min/hr | 60 | min/hr |
| Сар | = capacity factor for process (hours operated/year) | = | 8,760 | hours/yr | 8,760 | hours/yr |
| 2000 | = conversion factor (lb/Ton) | = | 2,000 | lb/Ton | 2,000 | lb/Ton |
| 10 ⁹ | = conversion factor to convert from ng to grams | = | 1.0E+09 | ng/g | 1.0E+09 | ng/g |
| E _{T/yr} | = PCDDF TEQ Emission rate (Ton/yr) | = | 6.6956E-09 | Ton/yr | 8.4094E-09 | Ton/yr |
| | | | | | | |

9. TEQ emission rate - Fd-based (lb/MMBtu)

$$E_{Fd} = \left(\frac{m_{n_{-}TEQ}}{V_{mxtd}}\right) \left(\frac{2.205 \times 10^{-3}}{10^9}\right) \left(F_d\right) \left(\frac{20.9}{20.9 - O_2}\right)$$

| Where: | | | | | | |
|--------------------------|--|---|------------|------------|------------|------------|
| m _{n_TEQ} | = total TEQ mass for PCDDs and PCDFs (ng) | = | 1.6800E-02 | ng | 2.1100E-02 | ng |
| V _{mstd} | = volume metered, standard (dscf) | = | 156.0614 | dscf | 156.0614 | dscf |
| 2.205 x 10 ⁻³ | = conversion factor (lb/g) | = | 2.205E-03 | lb/g | 2.205E-03 | lb/g |
| Fa | = ratio of gas volume to heat content of fuel (dscf/MMBtu) | = | 9,570 | dscf/MMBtu | 9,570 | dscf/MMBtu |
| O ₂ | = proportion of oxygen in the gas stream by volume (%) | = | 9.7 | % | 9.7 | % |
| 20.9 | = oxygen content of ambient air (%) | = | 20.9 | % | 20.9 | % |
| 10 ⁹ | = conversion factor to convert from ng to grams | = | 1.0E+09 | ng/g | 1.0E+09 | ng/g |
| E _{Fd} | = PCDDF TEQ Emission rate (lb/MMBtu) | = | 4.2314E-12 | lb/MMBtu | 5.3145E-12 | lb/MMBtu |

10. TEQ emission rate - Fc-based (lb/MMBtu)

$$E_{Fc} = \left(\frac{m_{n_TEQ}}{V_{mstd}}\right) \left(\frac{2.205 \times 10^{-3}}{10^9}\right) \left(F_c\right) \left(\frac{100}{CO_2}\right)$$

,

v

| Where: | | | | | | |
|--------------------------|--|---|------------|------------|------------|------------|
| m _{n_TEQ} | = total TEQ mass for PCDDs and PCDFs (ng) | = | 1.6800E-02 | ng | 2.1100E-02 | ng |
| V _{mstd} | = volume metered, standard (dscf) | = | 156.0614 | dscf | 156.0614 | dscf |
| 2.205 x 10 ⁻³ | = conversion factor (lb/g) | = | 2.205E-03 | lb/g | 2.205E-03 | lb/g |
| Fe | = ratio of gas volume to heat content of fuel (dscf/MMBtu) | = | 1,820 | dscf/MMBtu | 1,820 | dscf/MMBtu |
| CO2 | = proportion of carbon dioxide in the gas stream by volume (%) | = | 9.7 | % | 9.7 | % |
| 100 | = conversion factor | = | 100 | | 100 | |
| 10 ^e | = conversion factor to convert from ng to grams | = | 1.0E+09 | ng/g | 1.0E+09 | ng/g |
| EFc | = PCDDF TEQ Emission rate (lb/MMBtu) | = | 4.4354E-12 | lb/MMBtu | 5.5707E-12 | lb/MMBtu |

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EPA Method 1-4 Calculations

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USEPA Method 26A (HCI) Sampling, Velocity and Moisture Sample Calculations

Sample data taken from Run 1

Note: The tables presenting the results are generated electronically from raw data. It may not be possible to exactly duplicate these results using a calculator. The reference method data, results, and all calculations are carried to sixteen decimal places throughout. The final table is formatted to an appropriate number of significant figures.

1. Volume of water collected (wscf)

$$V_{wstd} = (0.04706)(V_{lc})$$

Where:

| V _{lc} | = total volume of liquid collected in impingers and silica gel (ml) = ideal gas conversion factor (fl³ water vapor/ml or gm) | = | 234.7 | ml |
|-------------------|--|---|---------|---------------------|
| 0.04706 | | ≈ | 0.04706 | ft ³ /ml |
| V _{wstd} | = volume of water vapor collected at standard conditions (ft ³) | = | 11.04 | ft ³ |

2. Volume of gas metered, standard conditions (dscf)

$$=\frac{(17.64)(V_m)\left(P_{bar}+\frac{\Delta H}{13.6}\right)(Y_d)}{(460+T_m)}$$

Where:

V_{mstd}

| vvnere. | | | | |
|-------------------|---|---|--------|----------------------------|
| Pbar | ≈ barometric pressure (in. Hg) | = | 30.00 | in. Hg |
| Tm | = average dry gas meter temperature (°F) | = | 75.13 | °F |
| Vm | volume of gas sample through the dry gas meter at meter conditions (dcf) | = | 41.95 | dcf |
| Yd | = gas meter correction factor (dimensionless) | = | 0.9904 | |
| ΔH | = average pressure drop across meter box orifice (in. H ₂ O) | = | 1.50 | in. H ₂ O |
| 17.64 | standard temperature to pressure ratio (°R/in. Hg) | = | 17.64 | °R/in. Hg |
| 13.6 | = conversion factor (in. H ₂ O/in. Hg) | = | 13.6 | in.H ₂ O/in. Hg |
| 460 | = °F to °R conversion constant | = | 460 | |
| V _{mstd} | volume of gas sampled through the dry gas meter at standard conditions (dscf) | = | 41.238 | dscf |
| | | | | |

3. Sample gas pressure (in. Hg)

$$= P_{bar} + \left(\frac{P_g}{13.6}\right)$$

Where:

 P_{s}

| P _{bar} | = barometric pressure (in. Hg) | = | 30.00 | in. Hg |
|------------------|---|---|--------|-----------------------------|
| Pg | = sample gas static pressure (in. H ₂ O) | = | -12.50 | in. H ₂ O |
| 13.6 | = conversion factor (in. H ₂ O/in. Hg) | = | 13.6 | in. H ₂ O/in. Hg |
| Ps | = absolute sample gas pressure (in. Hg) | = | 29.08 | in. Hg |

=

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4. Actual water vapor pressure at sample gas temperature less than 212°F (in. Hg)

P,

$$\frac{e^{\left(18.3036-\frac{3816.44}{\frac{4}{9}(T_{*}-32)+273.15-46.13}\right)}}{25.4}$$

Where:

| = average sample gas temperature (°F) | = | 309.42 | °F |
|---|---|--|--|
| = Antoine coefficient | = | 18.3036 | °К |
| = Antoine coefficient | = | 3816.44 | ۴К |
| = temperature conversion factor | = | 273.15 | °K |
| = Antoine coefficient | = | 46.13 | °K |
| = conversion factor | = | 25.4 | mm Hg/in. Hg |
| = Fahrenheit to Celsius conversion factor | = | 5/9 | °C/°F |
| = temperature conversion (°F) | = | 32 | ۴F |
| = vapor pressure, actual (in. Hg) | = | 29.08 | in. Hg |
| | Antoine coefficient Antoine coefficient temperature conversion factor Antoine coefficient conversion factor Fahrenheit to Celsius conversion factor temperature conversion (°F) | Antoine coefficient Antoine coefficient temperature conversion factor Antoine coefficient Antoine coefficient conversion factor Fahrenheit to Celsius conversion factor temperature conversion (°F) | = Antoine coefficient=18.3036= Antoine coefficient=3816.44= temperature conversion factor=273.15= Antoine coefficient=46.13= conversion factor=25.4= Fahrenheit to Celsius conversion factor=5/9= temperature conversion (°F)=32 |

5. Water vapor pressure at gas temperature greater than 212°F (in. Hg)

| Pv | $= P_s$ | | | |
|--------------------------|---|---|----------------|--------|
| Where: P _s | = absolute sample gas pressure (in. Hg) | = | 2 9 .08 | in. Hg |
| Pv | = water vapor pressure, actual (in. Hg) | = | 29.08 | in. Hg |

6. Moisture measured in sample (% by volume)

$$=\frac{V_{wstd}}{\left(V_{mstd}+V_{wstd}\right)}$$

Where:

Bwo

| Where: | | | | |
|-------------------|---|---|--------|------|
| V _{mstd} | volume of gas sampled through the dry gas meter at standard conditions (dscf) | = | 41.238 | dscf |
| V _{wstd} | = volume of water collected at standard conditions (scf) | = | 11.04 | scf |
| B _{wo} | = proportion of water measured in the gas stream by volume | = | 0.2113 | |
| | | = | 21.13 | % |

7. Saturated moisture content (% by volume)

 $B_{ws} = \frac{P_v}{P_s}$

| Where: | | | | | |
|-----------------|--|---|--------|--------|--|
| Ps | = absolute sample gas pressure (in. Hg) | = | 29.08 | in. Hg | |
| Pv | = water vapor pressure, actual (in. Hg) | = | 29.08 | in. Hg | |
| B _{ws} | = proportion of water vapor in the gas stream by volume at | | 1.0000 | | |
| | saturated conditions | = | 100.00 | % | |

,

8. Actual water vapor in gas (% by volume)

$$B_{w} = MINIMUM \left[B_{wo}, B_{ws}\right]$$

Where:

| B _{ws} | = proportion of water vapor in the gas stream by volume at saturated conditions | = | 1.0000 | |
|-----------------|--|---|--------|---|
| B _{wo} | = proportion of water measured in the gas stream by volume | = | 0.2113 | |
| B _w | = actual water vapor in gas | = | 0.2113 | |
| | | = | 21.13 | % |

9. Nitrogen (plus carbon monoxide) in gas stream (% by volume, dry)

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$$N_2 + CO = 100 - CO_2 - O_2$$

Where:

| CO ₂ | = proportion of carbon dioxide in the gas stream by volume (%) = proportion of oxygen in the gas stream by volume (%) = conversion factor (%) | = | 9.7 | % |
|--------------------|---|---|-------|---|
| O ₂ | | = | 9.7 | % |
| 100 | | = | 100 | % |
| N ₂ +CO | = proportion of nitrogen and CO in the gas stream by volume (%) | = | 80.70 | % |

10. Molecular weight of dry gas stream (lb/lb mole)

| M_{d} | $= \left(M_{CO_2}\right) \frac{(CO_2)}{(100)} + \left(M_{O_2}\right) \frac{(O_2)}{(100)} + \left(M_{N_2+CO}\right) \frac{(N_2+CO)}{(100)}$ | | | |
|--------------------|--|---|-------|------------|
| Where: | | | | |
| M _{CO2} | = molecular weight of carbon dioxide (lb/lb·mole) | = | 44.00 | lb/lb·mole |
| M _{O2} | = molecular weight of oxygen (lb/lb·mole) | = | 32.00 | lb/lb·mole |
| M _{N2+CO} | = molecular weight of nitrogen and carbon monoxide (lb/lb·mole) | = | 28.00 | lb/lb-mole |
| CO2 | = proportion of carbon dioxide in the gas stream by volume (%) | = | 9.7 | % |
| O ₂ | = proportion of oxygen in the gas stream by volume (%) | = | 9.7 | % |
| N ₂ +CO | = proportion of nitrogen and CO in the gas stream by volume (%) | = | 80.7 | % |
| 100 | = conversion factor (%) | = | 100 | % |
| Md | = dry molecular weight of sample gas (Ib/Ib·mole) | = | 29.93 | ib/lb·mole |

11. Molecular weight of sample gas (lb/lb·mole)

$$M_{s} = (M_{d})(1-B_{w}) + (M_{H_{2}O})(B_{w})$$

Where:

| B _w M _d M _{H2O} | proportion of water vapor in the gas stream by volume dry molecular weight of sample gas (lb/lb·mole) molecular weight of water (lb/lb·mole) | = = = | 0.2113 29.93 18.00 | lb/ib∙mole lb/ib∙mole |
|--|--|-------------|--------------------------|--------------------------|
| Ms | = molecular weight of sample gas, wet basis (lb/lb·mole) | = | 27.41 | lb/lb·mole |

EPA Method 1-4 Calculations

1. Chloride to HCl conversion factor

USEPA Method 26A HCI Analyte Calculations

USEPA Method 26A HCI Analyte Calculations

Sample data taken from Run 1

Note: The tables presenting the results are generated electronically from raw data. It may not be possible to exactly duplicate these results using a calculator. The reference method data, results, and all calculations are carried to sixteen decimal places throughout. The final table is formatted to an appropriate number of significant figures.

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 $= \frac{MW_{IICI}}{n \times MW_{CI}}$ K HCI Where: MWHCI = molecular weight of HCI (mg/mg-mole) 36.461 mg/mg-mole = MW_{CF} = molecular weight of chloride ion (mg/mg-mole) = 35.453 mg/mg-mole = molar ratio of chloride to HCI mole Cl/mole HCI n = 1.0 **K_{HCI}** = conversion factor to convert mass CI to mass HCI = 1.028 2. Total HCl collected (mg) $=K_{HCl} \times \frac{(S_{CL1}v_1 + S_{CL2}v_2)}{1000}$ m_{HCI} Where: K_{HCI} = conversion factor to convert mass CI to mass HCI = 1.028 = chloride concentration of sample fraction 1 (mg/liter) 32.2600 S_{CI-1} ma/liter = liquid volume of sample fraction 1 (ml) 897.0 ml \mathbf{v}_1 = S_{CI-2} = chloride concentration of sample fraction 2 (mg/liter) 0.0000 mg/liter = = liquid volume of sample fraction 2 (ml) = 0.0 V₂ ml 1000 = conversion factor (ml/liter) 1000 ml/liter = m_{HCI} = total HCl collected in sample (mg) 29.7475 mg Note: Non-detects are treated as zero in summations. DEFINITION

Fraction 1 = entire sample except last impinger containing applicable absorbing reagent.

Fraction 2 = last impinger containing applicable absorbing reagent, analyzed separately to evaluate collection efficiency. If entire sample is analyzed as a single fraction, then data is included as Fraction 1 (Fraction 2 = 0).

3. Allowable blank subtraction (mg)

$$m_b = K_{HCl} \times B_{Cl} \times \frac{(v_1 + v_2)}{1000}$$
$$m_b = 0 \quad \text{if } B_{Cl} < MDL$$

Where:

| K _{HCI} | = conversion factor to convert mass CF to mass HCI | = | 1.0280 | |
|-----------------------|--|---|-----------|----------|
| B _{CI} | = chloride concentration of blank (mg/liter) | = | <0.1 | mg/liter |
| v ₁ | = liquid volume of sample fraction 1 (ml) | = | 897.0 | ml |
| V ₂ | = liquid volume of sample fraction 2 (ml) | = | 0 | ml |
| 1000 | = conversion factor (ml/liter) | = | 1000.0000 | ml/liter |
| m _b | = allowable blank subtraction (mg) | = | 0.0000 | mg |

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4. Total HCl collected, corrected for blank (mg)

$$m_{nb} = m_{HCl} - m_b$$

Where:

| m _{∺Ci} m _b | total HCl collected in sample (mg) allowable blank subtraction (mg) | = | 29.7475 0.0000 | mg mg |
|------------------------------------|--|---|-------------------|----------|
| m _{nb} | = total HCl collected, corrected for blank (mg) | = | 29.74746216 | 3 mg |

5. Minimum detectable HCI (mg)

$$\begin{split} m_{MDL} &= K_{HCl} \times MDL \times \frac{(v_1 + v_2)}{1000} \\ \text{Where:} \\ K_{HCl} &= \text{conversion factor to convert mass Cl' to mass HCl} &= 1.028 \\ \text{MDL} &= \text{minimum detectable chloride concentration} &= 0.0 mg/liter \\ v_1 &= \text{liquid volume of sample fraction 1 (ml)} &= 897.0 ml \\ v_2 &= \text{liquid volume of sample fraction 2 (ml)} &= 0 ml \\ 1000 &= \text{conversion factor (ml/liter)} &= 1000 ml/liter \\ m_{MDL} &= \text{minimum detectable HCl (mg)} &= 0.01383174 mg \end{split}$$

6. Total HCl value used in emission calculations (mg)

 $(v_1 + v_2)$

-

| m_n | $= MAXIMUM \left[m_{nb} or < m_{MDL} \right]$ | | | |
|------------------|--|---|-------------|----|
| Where: | | | | |
| m _{nb} | = total HCl collected, corrected for blank (mg) | = | 29.7475 | mg |
| m _{MDL} | = minimum detectable HCI (mg) | = | 0.01383174 | mg |
| m | = total HCI value used in emission calculations (mg) | = | 29.74746216 | ma |

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QA/QC Date

USEPA Method 26A HCI Analyte Calculations

USEPA Method 26A HCI Sample Calculations

USEPA Method 26A HCI Sample Calculations

Sample data taken from Run 1

Note: The tables presenting the results are generated electronically from raw data. It may not be possible to exactly duplicate these results using a calculator. The reference method data, results, and all calculations are carried to sixteen decimal places throughout. The final table is formatted to an appropriate number of significant figures.

| | | | | 042210 101340 | |
|--------------------------|--|---|-----------------|---------------|--|
| 1. HCI concentration | (lb/dscf) | | | 0_@ | |
| C_{sd} | $= \left(\frac{m_n}{V_{mstd}}\right) \left(\frac{2.205 \times 10^{-3}}{1000}\right)$ | | | | |
| Where: | | | | | |
| m _n | = total HCl collected, corrected for applicable blank (mg) | = | 29.7475 | mg | |
| V _{mstd} | = volume metered, standard (dscf) | = | 41.2383 | dscf | |
| 2.205 x 10 ⁻³ | = conversion factor (lb/g) | = | 2.205E-03 | lb/g | |
| 1000 | = conversion factor (mg/g) | = | 1,000 | mg/g | |
| C _{sd} | = HCl concentration (lb/dscf) | = | 1.5906E-06 | lb/dscf | |
| 2. HCl concentration | (ppmdv) | | | | |
| C_{sd} | $= \left(\frac{m_n}{V_{mstd}}\right) \left(\frac{0.850}{1000}\right) \left(\frac{10^6}{MW}\right)$ | | | | |
| Where: | | | | | |
| m _n | total HCl collected, corrected for applicable blank (mg) | = | 29.7475 | mg | |
| V _{mstd} | = volume metered, standard (dscf) | = | 41.2383 | dscf | |
| MW | = molecular weight of HCI (g/g-mole) | = | 36.461 | g/g-mole | |
| 0.850 | = conversion factor (dscf/g-mole) | = | 0.850 | dscf/g-mole | |
| 1000 | = conversion factor (mg/g) | = | 1,000 | mg/g | |
| 10 ⁶ | = conversion factor (ppm) | = | 10 ⁶ | ppm | |
| C _{sd} | = HCl concentration (ppmdv) | = | 16.8166 | ppmdv | |
| 3. HCI concentration | (ppmwv) | | | | |
| C, | $= C_{sd} \left(1 - \frac{B_w}{100} \right)$ | | | | |
| Where: | | | | | |
| C _{sd} | = HCI concentration (ppmdv) | = | 16.8166 | ppmdv | |
| Bw | = actual water vapor in gas (% v/v) | = | 21.1253 | % v/v | |
| 100 | = conversion factor (%) | = | 100 | % | |
| C _w | = HCl concentration (ppmwv) | = | 13.2641 | ppmwv | |

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4. HCI concentration (mg/dscm)

$$C_{sd} = \left(\frac{m_n}{V_{mstd}}\right) (35.31)$$

Where:

| m _n V _{mstd} 35.31 | = total HCl collected, corrected for applicable blank (mg) = volume metered, standard (dscf) = conversion factor (dscf/dscm) | = a = | 29.7475 41.2383 35.31 | mg dscf dscf/dscm | |
|--|--|-------------|-----------------------------|-------------------------|--|
| C _{sd} | = HCl concentration (mg/dscm) | z | 25.4710 | mg/dscm | |

5. HCl concentration (mg/Nm³ dry)

$$C_{sd} = \left(\frac{m_n}{V_{mstd}}\right) (35.31) \left(\frac{68+460}{32+460}\right)$$

Where:

| | | ~~ | |
|--|---|---|--|
| = total HCI collected, corrected for applicable blank (mg) | 3 | 29.7475 | mg |
| = volume metered, standard (dscf) | = | 41.2383 | dscf |
| = conversion factor (dscf/dscm) | = | 35.31 | dscf/dscm |
| = standard temperature (°F) | = | 68 | °F |
| = normal temperature (°F) | = | 32 | °F |
| = °F to °R conversion constant | = | 460 | |
| = HCl concentration (mg/Nm ³ dry) | = | 27.3348 | mg/Nm ³ dry |
| | = conversion factor (dscf/dscm) = standard temperature (°F) = normal temperature (°F) = °F to °R conversion constant | = volume metered, standard (dscf)== conversion factor (dscf/dscm)== standard temperature (°F)== normal temperature (°F)== °F to °R conversion constant= | = volume metered, standard (dscf)=41.2383= conversion factor (dscf/dscm)=35.31= standard temperature (°F)=68= normal temperature (°F)=32= °F to °R conversion constant=460 |

6. HCl concentration corrected to x% O2 (ppmdv example)

$$= C_{sd} \left(\frac{20.9 - x}{20.9 - O_2} \right) \quad .$$

Where:

 C_{sdx}

| TTTCIC. | | | | |
|------------------|---|---|---------|--------------------------|
| C _{sd} | = HCI concentration (ppmdv) | = | 16.8166 | ppmdv |
| x | = oxygen content of corrected gas (%) | = | 7.0 | % |
| O ₂ | = proportion of oxygen in the gas stream by volume (%) | = | 9.7 | % |
| 20.9 | = oxygen content of ambient air (%) | = | 20.9 | % |
| C _{sdx} | = HCl concentration corrected to x%O ₂ (ppmdv) | = | 20.7779 | ppmdv @ x%O ₂ |

7. HCl concentration corrected to y% CO2 (ppmdv example)

$$=C_{sd}\left(\frac{y}{CO_2}\right)$$

Wł

 C_{sdy}

| where: | | | | | |
|------------------|--|---|---------|---------------|--|
| C _{sd} | = HCI concentration (ppmdv) | = | 16.8166 | ppmdv | |
| у | = carbon dioxide content of corrected gas (%) | = | 12.0 | % | |
| CO ₂ | = proportion of carbon dioxide in the gas stream by volume (%) | = | 9.7 | % | |
| C _{sdy} | = HCl concentration corrected to y%CO2 (ppmdv) | = | 20.9119 | ppmdv @ y%CO₂ | |

= 2.8279E-02 lb/MMBtu

8. HCl rate - Fd-based (lb/MMBtu)

$$E_{Fd} = \left(\frac{m_n}{V_{msid}}\right) \left(\frac{2.205 \times 10^{-3}}{1000}\right) \left(F_d\right) \left(\frac{20.9}{20.9 - O_2}\right)$$

Where:

| mn | = total HCl collected, corrected for applicable blank (mg) | = | 29.7475 | mg |
|--------------------------|--|---|-----------|------------|
| V _{mstd} | = volume metered, standard (dscf) | = | 41.2383 | dscf |
| 2.205 x 10 ⁻³ | = conversion factor (lb/g) | = | 2.205E-03 | lb/g |
| 1000 | = conversion factor (mg/g) | = | 1,000 | mg/g |
| Fa | = ratio of gas volume to heat content of fuel (dscf/MMBtu) | = | 9,570 | dscf/MMBtu |
| O ₂ | = proportion of oxygen in the gas stream by volume (%) | = | 9.7 | % |
| 20.9 | = oxygen content of ambient air (%) | = | 20.9 | % |
| | | | | |

E_{Fd} = HCl rate (lb/MMBtu)

9. HCI rate - Fc-based (Ib/MMBtu)

$$E_{F_{c}} = \left(\frac{m_{n}}{V_{mstd}}\right) \left(\frac{2.205 \times 10^{-3}}{1000}\right) (F_{c}) \left(\frac{100}{CO_{2}}\right)$$

· Where:

| mn | = total HCI collected, corrected for applicable blank (mg) | = | 29.7475 | mg |
|--------------------------|--|---|------------|------------|
| Vmstd | = volume metered, standard (dscf) | = | 41.2383 | dscf |
| 2.205 x 10 ⁻³ | = conversion factor (lb/g) | = | 2.205E-03 | lb/g |
| 1000 | = conversion factor (mg/g) | = | 1,000 | mg/g |
| Fc | = ratio of gas volume to heat content of fuel (dscf/MMBtu) | = | 1,820 | dscf/MMBtu |
| CO2 | = proportion of oxygen in the gas stream by volume (%) | = | 9.7 | % |
| 100 | = conversion factor | = | 100 | |
| E _{Fc} | = HCl rate (lb/MMBtu) | = | 2.9999E-02 | lb/MMBtu |
| | | | | |

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WHEELABRATOR NORTH BROWARD, INC. POMPANO BEACH, FL

CleanAir Project No: 10955-2

| PLANT DATA | | No. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. | С |
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WHEELABRATOR NORTH BROWARD TONS OF REFUSE PROCESSED PER STACK TEST RUN LOG (2010)

| UNIT #1 | | | | | | |
|------------------------|------------------------|-------------|--------------|-----------------------|------------------------------|--|
| Date | The second second | Weltine # | 8. Nor (* 18 | Steering (15, 10) | Rectaur congristr (http://di | a finerandPrenegation ((Ciris)) |
| 3/18/2010 | HCI | 26A | 1 | 183.5 | 1.00 | 34.0 |
| 3/18/2010 | HCI | 26A | 2 | 184.1 | 1.02 | 34.8 |
| 3/18/2010 | HCI | 26A | 3 | 182.8 | 1.00 | 33.9 |
| 3/16/2010 | Particulate/Metals | 5/29 | 1 | 183.9 | 2.18 | 74.2 |
| 3/16/2010 | Particulate/Metals | 5/29 | 2 | 184.4 | 2.18 | 74.4 |
| 3/16/2010 | Particulate/Metals | 5/29 | 3 | 183.4 | 2.18 | 74.0 |
| 3/17/2010 | Fluorides | 13B | 1 | 184.0 | 1.17 | 39.9 |
| 3/17/2010 | Fluorides | 13B | 2 | 184.0 | 1.20 | 40.9 |
| 3/17/2010 | Fluorides | 13B | 3 | 184.1 | 1.13 | 38.5 |
| n/a | Dioxins/Furans | 23 | 1 | n/a | n/a | n/a |
| n/a | Dioxins/Furans | 23 | 2 | n/a | n/a | n/a |
| n/a | Dioxins/Furans | 23 | 3 | n/a | n/a | n/a |
| UNIT #2 | | | | | | |
| | | | | | Sentar Programa | Diefs Promessing Altonia |
| 3/17/2010 | HCI | 26A | 1 | 184.7 | 1.00 | 34.2 |
| 3/17/2010 | HCI | 26A | 2 | 184.2 | 1.00 | 34.1 |
| 3/17/2010 | HCI | 26A | 3 | 184.9 | 1.00 | 34.2 |
| 3/18/2010 | Particulate/Metals | 5/29 | 1 | 183.9 | 2.22 | 75.6 |
| 3/18/2010 | Particulate/Metals | 5/29 | 2 | 182.9 | 2.22 | 75.2 |
| 3/18/2010 | Particulate/Metals | 5/29 | 3 | 183.9 | 2.20 | 74.9 |
| | | 13B | | | | and the second sec |
| 3/18/2010 | Fluorides Fluorides | 13B | 1 | <u>183.9</u> 184.2 | 1.25 | 42.6 |
| 3/18/2010 3/18/2010 | Fluorides | 13B | 3 | 183.0 | 1.23 | 42.0 |
| λ | | | | | | All and the second second second second second second second second second second second second second second s |
| 3/16/2010 | Dioxins/Furans | 23 | 1 | 184.1 | 4.87 | 166.0 |
| 3/17/2010 | Dioxins/Furans | 23 23 | 2 | 184.3 | 5.42 | 184.9 |
| 3/17/2010 | Dioxins/Furans | 23 | 3 | 183.9 | 4.55 | 154.9 |
| UNIT #3 | | | | | | |
| | | Mistisler 4 | S CIAN | SGERIE MAN | BOIL SHOOL TO AND | ELEMPROPHOLOGIA |
| 3/16/2010 | HCI | 26A | 1 | 184.6 | 1.00 | 34.2 |
| 3/16/2010 | HCI | 26A | 2 | 184.1 | 1.00 | 34.1 |
| 3/16/2010 | HCI | 26A | 3 | 184.2 | 1.00 | 34.1 |
| 3/17/2010 | Particulate/Metals | 5/29 | 1 | 184.2 | 2.22 | 75.7 |
| 3/17/2010 | Particulate/Metals | 5/29 | 2 | 184.2 | 2.20 | 75.1 |
| 3/17/2010 | Particulate/Metals | 5/29 | 3 | 183.5 | 2.20 | 74.8 |
| 3/16/2010 | Fluorides | 13B | 1 | 183.7 | 1.30 | 44.2 |
| 3/16/2010 | Fluorides | 13B | 2 | 183.9 | 1.18 | 40.2 |
| 3/16/2010 | Fluorides | 13B | 3 | 184.2 | 1.15 | 39.2 |
| n/a | Dioxins/Furans | 23 | 1 | n/a | n/a | n/a |
| n/a n/a | Dioxins/Furans | 23 | 2 | n/a | n/a | n/a |
| n/a | Dioxins/Furans | 23 | 3 | n/a | n/a | |
| 1.74 | Dioxino/Futurio | | · | 1.0 | 104 | |

Metals: Cd (cadmium) Hg (mercury) Be (beryllium) Pb (lead)

Stack Test Process Data

| PLANT NA | ME: NO | RTH BI | ROWARD | | | | Dat | ta from DC | S Printou | ts | | Calcu | ulated | Lit | me Feed R | ate | |
|----------|--------|--------|-----------|-------|-------|---------|----------|------------|-----------|-------|---------|--------|--------|----------|-----------|--------|--------------------|
| 2010 | | | | | | | | Fabric | SDA | Total | Diluton | | | | Slurry | | |
| | | | | | | Steam | FF inlet | Filter | Inlet | SDA | H2O | Slurry | Slurry | Slurry | CaO | CaO | |
| | Unit | Run | | Ti | me | Flow | Temp | Deita | Temp | Flow | flow | Flow | Conc. | Specific | Density | Flow | |
| Test | No. | No. | Date | Start | Stop | klbs/hr | deg F | In. H2O | deg F | gpm | gpm | gpm | % | Gravity | lb/gal | lbs/hr | Test Run Comments |
| M-26A | 1 | 1 | 3/18/2010 | 07:02 | 08:02 | 183.5 | 320.2 | 6.6 | 510.8 | 38.0 | 30.1 | 7.9 | 13.5 | 1.129 | 1.357 | 641.6 | |
| нсі | | 2 | 3/18/2010 | 09:26 | 10:37 | 184.1 | 320.4 | 5.3 | 510.8 | 37.8 | 28.5 | 9.4 | 15.2 | 1.129 | 1.363 | 765.5 | All times based on |
| | | 3 | 3/18/2010 | 11:49 | 12:49 | 182.8 | 320.1 | 6.4 | 520.1 | 40.7 | 29.9 | 10.8 | 14.2 | 1.129 | 1.357 | 880.2 | CEMS time |
| | | | | | Avg | 183.4 | 320.2 | 6.1 | 513.9 | 38.8 | 29.5 | 9.4 | 14.3 | 1.129 | 1.359 | 762.4 | |
| | | | | | | | | | | | | | | | | | |
| M-29/5 | 1 | 1 | 3/16/2010 | 07:21 | 09:32 | 183.9 | 310.4 | 6.3 | 521.3 | 39.2 | 29.5 | 9.8 | 14.9 | 1.104 | 1.095 | 640.6 | |
| Metals | | 2 | 3/16/2010 | 10:00 | 12:11 | 184.4 | 312.5 | 6.1 | 524.0 | 39.3 | 28.8 | 10.5 | 15.1 | 1.101 | 1.061 | 671.0 | All times based on |
| PM | | 3 | 3/16/2010 | 12:36 | 14:47 | 183.4 | 320.2 | 6.3 | 529.0 | 40.0 | 32.9 | 7.2 | 14.5 | 1.104 | 1.091 | 468.0 | CEMS time |
| | | | | | Avg | 183.9 | 314.4 | 6.2 | 524.8 | 39.5 | 30.4 | 9.1 | 14.8 | 1.103 | 1.082 | 593.2 | |
| | | | | | | | | | | | | | | | | | |
| M-13B | 1 | 1 | 3/17/2010 | 11:46 | 12:56 | 184.0 | 320.1 | 6.4 | 543.7 | 47.4 | 42.5 | 4.9 | 11.2 | 1.117 | 1.232 | 362.2 | |
| HF | | 2 | 3/17/2010 | 13:15 | 14:27 | 184.0 | 319.9 | 6.4 | 541.6 | 46.7 | 41.0 | 5.7 | 11.3 | 1.116 | 1.228 | 416.3 | All times based on |
| | | 3 | 3/17/2010 | 14:45 | 15:53 | 184.1 | 319.8 | 6.3 | 539.4 | 45.2 | 39.4 | 5.8 | 11.7 | 1.117 | 1.230 | 425.1 | CEMS time |
| | | | | | Avg | 184.0 | 319.9 | 6.4 | 541.6 | 46.4 | 41.0 | 5.4 | 11.4 | 1.117 | 1.230 | 401.2 | |

C - 4

Stack Test Data Sheet Mar 10

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Stack Test Process Data

| PLANT NA | ME: NO | RTH BI | ROWARD | | | | Da | ta From D | CS Printo | uts | | Calcu | lated | Lir | ne Feed Ra | ate | |
|----------|--------|--------|-----------|-------|-------|---------|----------|-----------|-----------|--------|---------|--------|--------|----------|------------|--------|--------------------|
| 2010 | | | | | | | | Fabric | SDA | Total | Diluton | | | | Siurry | | 1 |
| | | - | | | | Steam | FF Inlet | Filter | Inlet | SDA | H2O | Slurry | Slurry | Slurry | CaO | CaO | |
| | Unit | Run | | Tir | me | Flow | Temp | Delta | Temp | Flow | flow | Flow | Conc. | Specific | Density | Flow | |
| Test | No. | No. | Date | Start | Stop | kibs/hr | deg F | In. H2O | deg F | gpm | gpm | gpm | % | Gravity | ib/gal | lbs/hr | Test Run Comments |
| M-26A | 2 | 1 | 3/17/2010 | 06:54 | 07:54 | 184.7 | 323.0 | 6.1 | 518.1 | 38.0 | 31.0 | 7.0 | 14.9 | 1.109 | 1.136 | 474.4 | |
| нсі | | 2 | 3/17/2010 | 09:02 | 10:02 | 184.2 | 319.5 | 6.2 | 512.2 | 41.2 | 35.7 | 5.5 | 13.6 | 1.113 | 1.184 | 388.6 | All times based on |
| | | 3 | 3/17/2010 | 10:25 | 11:25 | 184.9 | 319.4 | 6.1 | 509.6 | 38.2 | 34.8 | 3.4 | 14.1 | 1.117 | 1.229 | 249.2 | CEMS time |
| | | | | | Avg | 184.6 | 320.6 | 6.1 | 513.3 | 39.1 | 33.9 | 5.3 | 14.2 | 1.113 | 1.183 | 370.7 | |
| | | | - | - | _ | | | | | | | | | | | | |
| M-29/5 | 2 | 1 | 3/18/2010 | 07:09 | 09:22 | 183.9 | 320.0 | 5.2 | 515.0 | 39.3 | 33.2 | 6.1 | 12.3 | 1.128 | 1.354 | 493.1 | |
| Metals | | 2 | 3/18/2010 | 09:49 | 12:02 | 182.9 | 320.2 | 5.4 | 515.2 | 38.6 | 32.8 | 5.9 | 12.4 | 1.129 | 1.361 | 481.0 | All times based on |
| PM | | 3 | 3/18/2010 | 12:27 | 14:39 | 183.9 | 320.6 | 6.3 | 520.2 | 41.4 | 34.3 | 7.1 | 11.7 | 1.128 | 1.354 | 579.2 | CEMS time |
| | | | | | Avg | 183.6 | 320.3 | 5.6 | 516.8 | 39.8 | 33.4 | 6.4 | 12.1 | 1.128 | 1.356 | 517.8 | |
| | | | | | _ | | _ | | | | | | | | | | |
| M-23 | 2 | 1 | 3/16/2010 | 08:44 | 13:36 | 184.1 | 314.2 | 6.1 | 505.6 | 37.6 | 30.0 | 7.6 | 15.8 | 1.101 | 1.063 | 487.3 | |
| dioxins | | 2 | 3/17/2010 | 06:54 | 12:19 | 184.3 | 321.2 | 6.1 | 513.8 | 39.3 | 34.0 | 5.4 | 14.3 | 1.113 | 1.184 | 380.1 | All times based on |
| | | 3 | 3/17/2010 | 12:53 | 17:26 | 183.9 | 320.3 | 6.1 | 523.4 | _ 43.1 | 39.3 | 3.9 | 12.3 | 1.117 | 1.231 | 285.1 | CEMS time |
| | | | | - | Avg | 184.1 | 318.6 | . 6.1 | 514.2 | 40.0 | 34.4 | 5.6 | 14.2 | 1.110 | 1.159 | 384.1 | |
| | | | | | | | | | | | | | | | | | |
| M-13B | 2 | 1 | 3/18/2010 | 07:09 | 08:24 | 183.9 | 320.6 | 5.9 | 514.0 | 39.3 | 32.8 | 6.5 | 12.3 | 1.129 | 1.357 | 530.0 | |
| HF | | 2 | 3/18/2010 | 08:56 | 10:10 | 184.2 | 319.6 | 3.4 | 512.5 | 37.4 | 31.9 | 5.5 | 12.8 | 1.129 | 1.359 | 448.5 | All times based on |
| | | 3 | 3/18/2010 | 10:45 | 12:05 | 183.0 | 319.9 | 6.0 | 514.7 | 38.4 | 32.1 | 6.3 | 12.5 | 1.129 | 1.360 | 512.4 | CEMS time |
| | | | | | Avg | 183.7 | 320.0 | 5.1 | 513.8 | 38.3 | 32.2 | 6.1 | 12.5 | 1.129 | 1.359 | 497.0 | 1 |

Stack Test Data Sheet Mar 10

Stack Test Process Data

| PLANT NA | ME: NO | RTH BF | ROWARD | | | | Dat | a From DC | S Printou | ts | | Calcu | lated | Lir | ne Feed Ra | ate | |
|----------|----------|--------|-----------|-------|-------|---------|----------|------------------|--------------|--------------|----------------|----------------|--------|----------|---------------|--------|--------------------|
| 2010 | <u> </u> | _ | | | | Steam | FF inlet | Fabric Filter | SDA Inlet | Total SDA | Diluton H2O | Shumer | Slurry | Slurry | Slurry CaO | CaO | |
| | Unit | Run | | Tiı | me | Flow | Temp | Delta | Temp | Flow | flow | Slurry Flow | Conc. | Specific | Density | Flow | |
| Test | No. | No. | Date | Start | Stop | klbs/hr | deg F | In. H2O | deg F | gpm | gpm | gpm | % | Gravity | ib/gal | lbs/hr | Test Run Comments |
| M-26A | 3 | 1 | 3/16/2010 | 07:17 | 08:17 | 184.6 | 309.9 | 6.3 | 507.3 | 35.8 | 26.2 | 9.7 | 16.1 | 1.113 | 1.183 | 685.0 | |
| HCI | | 2 | 3/16/2010 | 09:04 | 10:04 | 184.1 | 310.1 | 6.3 | 514.4 | 37.4 | 24.2 | 13.3 | 19.1 | 1.100 | 1.051 | 837.4 | All times based on |
| | | 3 | 3/16/2010 | 10:32 | 11:32 | 184.3 | 309.9 | 6.4 | 513.4 | 37.5 | 27.0 | 10.5 | 18.6 | 1.101 | 1.059 | 667.2 | CEMS time |
| | | | | | Avg | 184.3 | 310.0 | 6.3 | <u>511.7</u> | 36.9 | 25.8 | 11.1 | 17.9 | 1.105 | 1.098 | 729.9 | |
| | | | | | | | | | | | | | | | | | |
| M-29/5 | 3 | 1 | 3/17/2010 | 06:50 | 09:03 | 184.2 | 315.0 | 6.4 | 518.9 | 37.8 | 33.4 | 4.5 | 14.8 | 1.109 | 1.142 | 304.9 | |
| Metals | | 2 | 3/17/2010 | 09:26 | 11:38 | 184.2 | 314.9 | 6.4 | 518.1 | 37.8 | 33.6 | 4.2 | 14.4 | 1.115 | 1.214 | 303.7 | All times based on |
| PM | | 3 | 3/17/2010 | 11:59 | 14:11 | 183.5 | 315.2 | 6.4 | 521.6 | 38.7 | 34.7 | 4.0 | 13.7 | 1.117 | 1.230 | 295.2 | CEMS time |
| | | | | | Avg | 184.0 | 315.0 | 6.4 | 519.5 | 38.1 | 33.9 | 4.2 | 14.3 | 1.114 | 1.195 | 301.3 | |
| | | | | | | | | | | | | | | | | | |
| M-13B | 3 | 1 | 3/16/2010 | 11:49 | 13:07 | 183.7 | 310.2 | 6.5 | 517.3 | 38.8 | 28.2 | 10.6 | 15.1 | 1.102 | 1.074 | 684.4 | |
| HF | | 2 | 3/16/2010 | 13:33 | 14:44 | 183.9 | 309.6 | 6.4 | 523.8 | 41.3 | 36.1 | 5.2 | 14.0 | 1.105 | 1.098 | 339.3 | All times based on |
| | | 3 | 3/16/2010 | 15:07 | 16:16 | 184.2 | 309.8 | 6.3 | 518.2 | 38.9 | 34.5 | 4.4 | 14.7 | 1.106 | 1.113 | 293.8 | CEMS time |
| | | | | | Avg | 184.0 | 309.9 | 6.4 | 519.7 | 39.7 | 32.9 | 6.7 | 14.6 | 1.104 | 1.095 | 439.2 | |

| Pompano | 48th Street Seach, FL 33073 971-8701 Fax: (954) 971-8703 | | In | 17/2010 10:55: 11 12:47: | 55AM 52PM |
|-----------|--|---------|--------|--------------------------------|--------------|
| Account | 623030 | Price/1 | on | 0.00 | |
| Customer | Chemical Lime | Fees | | 0.00 | |
| | Chemical Lime | Other | | 0.00 | |
| 1 | PO Box 7247-8945 Philadelphia. PA | Total | | 0.00 | |
| Decal # | LIME1 | | Pounds | Tons | |
| Vehicle # | LIME1 | Gross | 78220 | 39.11 | |
| Auto ID | 0 | Tare | | 13.75 | |
| Other | | Net | 50720 | 25.36 | |
| Product | 9020 Lime | | | | |
| Qty | 25.36 Ton | | | | |
| Origin | Wheelabrator No | | | | |
| Operator | Luisa Paredes | | | | |

| 2600 N. Pompar | Habrator - N. Broward W. 48th Street no Beach, FL 33073 4) 971-8701 Fax: (954) 971-8703 | | | | 362462 :55AM :52PM |
|-------------------|---|------------------------|--------|----------------------|---------------------------------|
| Account | 623030 | Price | Ton | 0.00 | |
| Customer | Chemical Lime Chemical Lime PO Box 7247-8945 Philadelphia. PA | Fees Other Total | | 0.00 0.00 0.00 | |
| Decal # | LIME1 | | Pounds | Tons | |
| Vehicle # | LIME1 | Gross | 78220 | 39.11 | |
| Auto ID | 0 | Tare | 27500 | 13.75 | |
| Other Product | 105949666 9020 25.36 Ton | Net | 50720 | 25.36 | |
| Qty Origin | Wheelabrator No | | | | |
| Operator | Luisa Paredes | | | | |

| Date: Start Time: End Time: | 03/18/10 7:02:00 8:02:00 | | SDAVOUNLENT TEMP | SEURRY/FIL | DIEWATER | TOTAL | LIME | TEMP | DP | IDINLET PRESS | SPECIFIC 22: GRAVITY |
|-----------------------------------|--------------------------------|-------------------|---------------------|-----------------|----------------|--------------------|-------------------|------------------|-------------------|-------------------|-------------------------|
| | | DEG F | DEG F | GPM | GPM | GPM | % | DEG F | " H2O | " H2O | " H2O |
| Unit 1 | 26A run 1 | 510.76 | 320.18 | 37.95 | 30.07 | 7.88 | 13.47 | 302.94 | 6.61 | -10.39 | 1.129 |
| Unit 2 | | 512.00 | 320.64 | 38.53 | 31.76 | 6.76 | 12.48 | 296.62 | 5.99 | -10.30 | 1.129 |
| Unit 3 | | 507.30 | 314.96 | 34.59 | 30.80 | 3.79 | 13.84 | 302,13 | 6.31 | -8.02 | 1.129 |
| C - 8 | | ELOW | SHOUT | FINALISTME | IOTAIR FLOW | EURNACE DRAFT | ECONO OUT-TEMP | SH ROLLS | SNCR CHEM FLOW | STEAM | |
| Unit 1 | | KLBs/hr 191.84 | DEG F 885.94 | DEG F 831.12 | KSCFM 82.00 | <u>" H2O</u> -0.10 | DEG F 274.45 | DEG F 1112.44 | GPH 4.79 | KLBs/hr 183.45 | 1.357 |
| | | | | | | | | | | | |
| Unit 2 | | 186.41 | 900.62 | 830.71 | 80.27 | -0.05 | 271.41 | 1209.02 | 3.58 | 184.03 | 1.357 |
| Unit 3 | | 189.87 | 903.30 | 823.06 | 79.10 | -0.16 | 280.70 | 1163.22 | 4.78 | 184.47 | 1.357 |

Page

| End Time: 10 | - | | | | | | | | | | |
|---|---------------------------------------|------------------|--------------------|-----------|-----------------------------------|----------------------------------|--|---------|---------------------------------|---|----------|
| | _ | DEG F | DEG F | GPM | GPM | GPM | % | DEG F | " H2O | " H2O | " H2O |
| | A run 2 | 510.81 | 320.37 | 37.84 | 28.48 | 9.36 | 15.24 | 304.06 | 5.33 | -8.96 | 1.1 |
| in the second second second second second second second second second second second second second second second | · · · · · · · · · · · · · · · · · · · | | | | | Aller herging management & aller | | | | | |
| Jnit 2 | | 513.74 | 320.26 | 38.04 | 32.58 | 5.46 | 12.59 | 296.16 | 4.11 | -8.28 | 1.1 |
| الله المركزية المركزية المركزية المركزية المركزية المركزية المركزية المركزية المركزية المركزية المركزية المركز مركزة المركزية المركز | the state and | en manage | | | | | مربعة بين المربعة المربعة المربعة المربعة المربعة المربعة المربعة المربعة المربعة المربعة المربعة المربعة المر مستحكمتهم المربعة المربعة المربعة المربعة المربعة المربعة المربعة المربعة المربعة المربعة المربعة المربعة المربع | | | مسیومی او او مرتب از این از این از این از این از این از این از این از این از این از این از این از این از این ا این این این این این این این این این این | |
| | | | 245 201 | 26 1 5 1 | 21 791 | 4.37 | 13.20 | 302.72 | 6.43 | -8,19 | 1.1 |
| Jnit 3 | l | 510.56 | 315.30 | 36.15 | 31.78 | | | | | | |
| Jnit 3 | | FEED H20 | | FINAL STM | | EURNACE | ECONO | SHROLL | SNCR | | |
| Jnit 3 | | FEED H20 | SH OUT | FINAL STM | TOT AIR | -EURNACE | ECONO OUT TEMP | SH-ROLL | SNCR HEM ÉLOW | STEAM | |
| | [| FEED H2O FLOW | SHOUT STM PRESS | FINAL STM | FLOW KSCFM | EURNACE | DEG F | SH ROLL | SNCR HEM ÊLOW GPH | STEAM ELOW KLBs/hr | AVAILABI |
| Jnit 1 | | FEED H2O FLOW | SH OUT | FINAL STM | FOT AIR FLOW KSCFM 81.31 | -EURNACE | DEG F 274.60 | SH-ROLL | SNCR HEM ÊLOW GPH 7.36 | STEAM | AVAILAB |

Page 1

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| Date: Start Time | | SDA INLET TEMP | SDA OUTLET TEMP | TOTAL SLURRY FL | DIL WATER FLOW | TOTAL LIME | LIME | FF OUT | FF DP | ID INLET PRESS | SPECIFIC GRAVITY |
|---------------------|-----------|---------------------------|--|----------------------------|------------------------|------------------|----------------------------|------------------|---------------------------------|-------------------|----------------------|
| End Time: | 12:49:00 | | | | | | | | | | |
| | | DEG F | DEG F | GPM | GPM | GPM | % | DEG F | " H2O | " H2O | " H2O |
| Unit 1 | 26A run 3 | 520.05 | 320.07 | 40.70 | 29.89 | 10.81 | 14.19 | 304.70 | 6.42 | -10.26 | 1.129 |
| | | | | | | | | | · · · · · | | |
| Unit 2 | | 514.98 | 320.02 | 38.86 | 30.53 | 8.33 | 12.32 | 295.38 | 6.22 | -10.35 | 1.129 |
| | | | | | | | | · • • | | | |
| Unit 3 | | 514.47 | 314.97 | 37.48 | 31.17 | 6.30 | 12.85 | 302.37 | 6.39 | -8.11 | <u>1.</u> 129 |
| | | | | | | | | | | | |
| C - 10 | | FEED H20 | SH OUT STM PRESS | FINAL STM | | | ECONO OUT TEMP | SH ROLL | SNCR CHEM FLOW | STEAM | |
| 1 | | | SH OUT STM PRESS DEG F | FINAL STM TEMP DEG F | | FURNAGE DRAFT | ECONO OUT TEMP DEG F | | | STEAM | |
| 1 | | FLOW | STM PRESS | TEMP | FLOW | DRAFT | OUT TEMP | Âvg | CHEM FLOW | FLOW | |
| - 10 | | FLOW KLBs/hr 190.84 | STM PRESS | DEG F | FLOW | " H2O -0.09 | DEG F | DEG F | CHEM FLOW | KLBs/hr 182.82 | CaO |
| Unit 1 Unit 2 | | FLOW KLBs/hr 190.84 | STM PRESS DEG F 883.32 899.91 | DEG F 824.80 | KSCFM 85.05 | " H2O -0.09 | DEG F 274.03 | | <u>CHEM FLOW</u> GPH 4.01 | KLBs/hr 182.82 | CaO |
| Unit 1 | | FLOW KLBs/hr 190.84 | DEG F 883.32 899.91 | DEG F 824.80 | FLOW KSCFM 85.05 | " H2O -0.09 | DEG F 274.03 | DEG F 1116.84 | GPH 4.01 | KLBs/hr 182.82 | ∴CaO 1.357 |

| Date: Start Time: End Time: | 03/16/10 7:21:00 9:32:00 | SDAINUET S TEMP | | LOTAL | DILWATER HELOW | | | HEFOULD IN DEMIP | DP. | IDINGET | SPECIFIC GRAVIN |
|-----------------------------------|--------------------------------|--------------------|-----------------|-----------------|-------------------|------------------|-----------------|---------------------|-------------|-------------------|--------------------|
| | | DEG F | DEG F | GPM | GPM | GPM | % | DEG F | " H2O | " H2O | " H2O |
| Unit 1 | 5/29 run 1 | 521.31 | 310.41 | 39.22 | 29.47 | 9.75 | 14.89 | 293.56 | 6.29 | -9.58 | 1.104 |
| Unit 2 | | 503.87 | 309.92 | 39.36 | 25.13 | 14.23 | 15.18 | 287.89 | 6.17 | 0.00 | 1.104 |
| Unit 3 | | 509.95 | 310.16 | 36.61 | 25.48 | 11.13 | 17.69 | 297.89 | 6.37 | -8.36 | 1.104 |
| C - 11 | | FEED H20 | SHOUT A | FINAL STM | TOLAIR FLOW | FURNACE DRAFT | | SHIROLL | | STEAM S | AVAILABILE: CaO |
| Unit 1 | | KLBs/hr 192.49 | DEG F 885.25 | DEG F 828.88 | KSCFM 80.00 | " H2O -0.10 | DEG F 274.46 | DEG F 1164.32 | GPH 8.17 | KLBs/hr 183.87 | 1.095 |
| Unit 2 | | 187.42 | 901.26 | 834.65 | 80.36 | -0.10 | 271.35 | 1124.31 | 6.52 | 184.65 | 1.095 |
| Unit 3 | | 191.24 | 903.31 | 835.06 | 80.89 | -0.25 | 280.72 | 1146.30 | 6.40 | 184.32 | 1.095 |

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| Date: Start Time: End Time: | 03/16/10 10:00:00 12:11:00 | SDAVINLET S | SDA OUTLEIT | TOTAL | DIEWATER FLOW | LIME | LIME | | F F DP | ID INLET | SPECIFIC |
|-----------------------------------|---|-------------|-------------|--------------------|------------------|-------|--------|---------|-------------------|----------|------------------|
| | | DEG F | DEG F | GPM | GPM | GPM | % | DEG F | " H2O | " H2O | " H2O |
| Unit 1 | 5/29 run 2 | 524.01 | 312.53 | 39.30 | 28.76 | 10.54 | 15.09 | 294.96 | 6.24 | -9.55 | 1.101 |
| Unit 2 | | 504.44 | 313.21 | 37.48 | 27.01 | 10.47 | 15.75 | 289.83 | 6.09 | -0.35 | 1.101 |
| Unit 3 | and All and All and All and All and All and All and All and All and All and All and All and All and All and Al All and All and All and All and All and All and | 514.03 | 309.93 | 37.81 | 27.42 | 10.39 | 17.56 | 298.21 | 6.40 | -8.34 | 1.101 |
| | | | | | | | | | | | |
| :- 12 | | FEED H201 | SH'OUT | FINALISTME TEMP | FLOW | DRAFT | | SH ROLL | SNCR CHEMIFLOW | ELOW | AVAILABLE Cao |
| | | | | | _ | | | | | | |
| | | KLBs/hr | DEG F | DEG F | KSCFM | " H2O | DEG F | DEG F | GPH | KLBs/hr | - |
| Unit 1 | | 193.41 | 885.00 | 832.09 | 79.86 | -0.10 | 274.60 | 1158.93 | 10.33 | 184.37 | 1.061 |
| Unit 2 | | 186.98 | 900.95 | 834.63 | 80.57 | -0.10 | 271.51 | 1129.20 | 8.65 | 183.97 | 1.061 |
| Unit 3 | | 191.07 | 902.88 | 833.00 | 81.15 | -0.25 | 280.85 | 1159.86 | 6.39 | 184.17 | 1.061 |

| Date: Start Time: | 03/16/10 12:36:00 | SDAINEET IS | SDAVOUITEEL -TIEMP | IOIAL SLURRY EL | DIE WATER ELOW | | | | | EIDINIET. PRESS | SPECIFIC CRAVIII |
|----------------------|----------------------|-------------|-----------------------|--------------------|-------------------|------------------|-------------------|---------|-------------------|--------------------|--------------------------|
| End Time: | 14:47:00 | DEG F | DEG F | GPM | GPM | GPM | % | DEG F | " H2O | " H2O | " H2O |
| Unit 1 | 5/29 run 3 | 528.96 | 320.15 | 40.01 | 32.86 | 7.15 | 14.47 | 299.89 | 6.30 | -9.68 | 1.104 |
| Unit 2 | | 510.02 | 319.33 | 37.13 | 32.36 | 4.77 | 15.60 | 295.73 | 6.02 | -6.02 | 1.104 |
| Unit 3 | | 522.97 | 310.00 | 40.90 | 34.57 | 6.32 | 14.17 | 298.77 | 6.45 | -8.59 | 1.104 |
| | | | | | | | | | | | |
| 0 | | | | | | | | | | | |
| - 13 | | FEEDH20 | SHOUT | | TOT AIR FLOW | FURNACE DRAFT | ECONO OUT-TEMP | AVG | SNCR SHEMIELOW | FLOW | AVAILABLE <u>Ca</u> O |
| | | | | | | | | | | | |
| 1 100 16 1 | | KLBs/hr | DEG F | DEG F | KSCFM | " H2O | DEG F | DEG F | GPH | KLBs/hr | 1 001 |
| Unit 1 | | 192.65 | 883.77 | 830.04 | 82.02 | -0.10 | 274.21 | 1158.27 | 4.40 | 183.37 | 1.091 |
| Unit 2 | | 186.25 | 899.37 | 827.33 | 82.06 | -0.09 | 271,12 | 1137.52 | 5.47 | 183.77 | 1.091 |
| Unit 3 | | 189.65 | 901.33 | 826.98 | 86.21 | -0.25 | 280.52 | 1157.95 | 4.26 | 183.42 | 1.091 |

| Date: Start Time: End Time: | 03/17/10 11:46:00 12:56:00 | SDAVINIET - | | SLURRY FL | DILWATER FLOW | TOTAL- | CONC | | DP | DINLET PRESS | SPECIFIC GRAVITY |
|-----------------------------------|----------------------------------|-------------|----------|-----------|------------------|---------|--------|---------|------------------|-----------------|---------------------|
| | | DEG F | DEG F | GPM | GPM | GPM | % | DEG F | " H2O | " H2O | " <u>H2O</u> |
| Unit 1 | 13B run 1 | 543.69 | 320.13 | 47.41 | 42.51 | 4.90 | 11.18 | 301.67 | 6.44 | -10.51 | 1.117 |
| Unit 2 | | 508.83 | 320.28 | 37.75 | 34.56 | 3.19 | 13.98 | 296.67 | 6.16 | -10.42 | 1.117 |
| Unit 3 | | 517.47 | 315.64 | 37.34 | 33.35 | 4.00 | 14.15 | 303.49 | 6.37 | -8.13 | 1.117 |
| | | | | | | | | | | | |
| 0 | | | | | | | | | | | |
| - 14 | | FEED H20 | STMPRESS | | ELOUAR C | FURNACE | | SHIROLL | SNOR HEMIELOW | SUEAM ELOW | |
| | | | | | | | | | | | |
| | | KLBs/hr | DEG F | DEG F | KSCFM | " H2O | DEG F | DEG F | GPH | KLBs/hr | |
| Unit 1 | | 192.13 | 885.22 | 827.80 | 90.17 | -0.11 | 274.07 | 1180.68 | 3.97 | 183.97 | 1.232 |
| Unit 2 | | 187.20 | 899.07 | 830.60 | 83.77 | -0.04 | 271.06 | 1189.49 | <u>.</u> 6.41 | 184.11 | 1.232 |
| Unit 3 | | 188.46 | 901.48 | 824.60 | 81.19 | -0.15 | 280.40 | 1201.87 | 3.92 | 182.84 | 1.232 |

| Date: Start Time: End Time: | 03/17/10 13:15:00 14:27:00 | SDAINLET S TEMP | | TOTAL SEURRYAP | DILWATER Z | | | | EF DP | IDINIET PRESS | SPECIEIC GRAVITY |
|-----------------------------------|------------------------------------|--------------------|--|-------------------|--------------|--------------|--------|-----------------|---------------|------------------|---------------------|
| Unit 1 | 13B run 2 | DEG F | DEG F 319.91 | GPM 46.69 | GPM 41.04 | GPM 5.65 | % | DEG F 300.84 | " H2O 6.39 | " H2O -10,35 | " H2O 1,116 |
| | | 541.00 | | 40.09 | 41.04 | 5.05 2.05 | 11.34 | | | | |
| Unit 2 | | 520.32 | 320.04 | 41.74 | 38.53 | 3.21 | 12.67 | 296.91 | 6.18 | -10.80 | 1.116 |
| Unit 3 | and the second state of the second | 523.92 | 314.91 | 39.46 | 35.44 | 4.02 | 13.43 | 303.75 | 6.40 | -8.32 | 1.116 |
| О | | | Service and the service of the servi | | | | | CUIDAR | | Money Names (189 | |
| - 15 | | FLOW | STM PRESS | TEMP | FLOW | DRAFI | | AVG | CHEMIFLOW | FLOW | <u>C:0</u> |
| | | KLBs/hr | DEG F | DEG F | KSCFM | " H2O | DEG F | DEG F | GPH | KLBs/hr | |
| Unit 1 | MC XX MITTIN ADDR | 192.62 | 885.70 | 831.95 | 89.16 | -0.08 | 273.84 | 1186.69 | 4.26 | 184.02 | 1.228 |
| Unit 2 | | 185.93 | 899.02 | 826.15 | 87.56 | -0.05 | 270.76 | 1208.10 | 3.47 | 183.68 | 1.228 |
| Unit 3 | | 189.66 | 902.08 | 825.01 | 83.42 | -0.14 | 280.14 | 1188.10 | 3.06 | 183.92 | 1.228 |

| Date: Start Time: End Time: | 03/17/10 14:45:00 15:53:00 | SDAVINUET S | IDAVOUITEETE TEMP | SEURRY FL | DIL WATER | TOTAL E | CONC | EFOUT TIEMP | EF DR | PRESS | SPECIFIC GRAVITY |
|-----------------------------------|----------------------------------|------------------|----------------------|-----------|-----------------|---------|-------------------|-----------------|------------------|---------------|---------------------|
| | | DEG F | DEG F | GPM | GPM | GPM | % | DEG F | " H2O | " H2O | <u>" H2O</u> |
| Unit 1 | 13B run 3 | 539.44 | 319.77 | 45.18 | 39.42 | 5.75 | 11.73 | 301.90 | 6.30 | -10.15 | 1.117 |
| Unit 2 | | 524.93 | 320.26 | 43.88 | 39.65 | 4.23 | 12.08 | 296.82 | 6.09 | -10.78 | 1.117 |
| Unit 3 | ini tahun karangan | 524.99 | <u>315</u> .19 | 39.61 | 35.62 | 3.99 | 13.36 | 304.00 | 6.45 | -8.34 | 1.117 |
| | | | | | | | | | | | |
| 0 | | | | | | | <u></u> | | | | |
| - - - - | | EEED H20 FLOW | SHOUT | FINAL STM | TOT AIR FLOW | DRAFT | ECONO OUT-TEMP | SH:ROLL | SNCR HEM FLOW | STEAM FLOW | AVAILABLE CaO |
| | | | | | | | | | | | |
| | | KLBs/hr | DEG F | DEG F | KSCFM | " H2O | DEG F | DEG F | GPH | KLBs/hr | |
| Unit 1 | | 193.20 | 885.11 | 834.55 | 87.28 | -0.09 | 274.08 | 1185.17 | 3.91 | 184.10 | 1.230 |
| Unit 2 | | 186.47 | 899.02 | 827.51 | 88.63 | -0.04 | 271.00 | 1223.99 | 3.28 | 183.70 | 1.230 |
| | | | | | | | | | | | |
| Unit 3 | | 189.03 | 901.99 | 822.61 | 83.28 | -0.14 | 280.34 | <u>1</u> 182.88 | 4.43 | 183.81 | 1.230 |

| Date: Start Time: End Time: | 03/17/10 6:54:00 7:54:00 | SDAINLET: S | DATOUNEER THEMP | SLURRYHT | DILWATER | | CONC | FEOUR TIEMP | EE DP | DINIET - | SRECIEIC EGRAVINY |
|-----------------------------------|--------------------------------|-------------------|--------------------|------------------|-----------------|----------------|-----------------|------------------|-------------|-------------------|----------------------|
| | | DEG F | DEG F | GPM | GPM | GPM | % | DEG F | " H2O | " H2O | " H2O |
| Unit 1 | | 535.88 | 317.13 | 45.14 | 37.65 | 7.49 | 12.44 | 298.63 | 6.37 | -10.19 | 1.109 |
| | 26A run 1 | 518.13 | 322.96 | 37.99 | 31.03 | 6.97 | 14.90 | 297.57 | 6.10 | -10.30] | 1.109 |
| Unit 3 | | 521.02 | 315.21 | 38.56 | 34.38 | 4.18 | 14.55 | 303.91 | 6.35 | -8.29 | 1.109 |
| C - 17 | | FEEDTH20 | SH OUT | FINALSTM TEMP | TOT AIR FLOW | TFURNACE | | SHROUES | SNCR- | STEAM FLOW | |
| Unit 1 | | KLBs/hr 191.66 | DEG F 884.81 | DEG F 822.80 | KSCFM 80.70 | " H2O -0.10 | DEG F 274.50 | DEG F 1202.73 | GPH 5.44 | KLBs/hr 184.13 | 1.136 |
| Unit 2 | | 186.49 | 899.80 | 826.57 | 80.89 | -0.09 | 271.45 | 1183.47 | 6.05 | 184.66 | 1.136 |
| Unit 3 | | 191.00 | 902.02 | 826.23 | 79.81 | -0.20 | 280.81 | 1186.47 | 4.01 | 184.63 | 1.136 |

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| Date: Start Time: | L. L. | SDA INLET S TEMP | DA OUTLET TEMP | TOTAL | DIL WATER FLOW | -total .^lime | CONC | FF OUT | FF DP | ID INLET PRESS | SPECIFIC GRAVITY |
|--|-----------|-------------------------------------|-----------------------------------|--|-------------------|-------------------------|---|------------------|------------------------|----------------------------------|------------------------------|
| End Time: | 10:02:00 | DEG F | DEG F | GPM | GPM | GPM | % | DEG F | " H2O | " H2O | " H2O |
| Unit 1 |] | 534.03 | 320.11 | 42.63 | 36.54 | 6.09 | 13.01 | 301.14 | 6.30 | -9.94 | 1.113 |
| | | | wert . | · · · · · · · · · · · · · · · · · · · | | - Th- | | A. Sures | | | - 11 |
| Unit 2 | 26A run 2 | 512.17 | 319.50 | 41.18 | 35.71 | 5.47 | 13.58 | 297.17 | 6.16 | -10.63 | 1.113 |
| 1 | | | and the state of the state of the | And a second secon | | | and a second and a second and a second and a second and a second and a second and a second and a second and a s | 1 | يوني . يەربىي دىرىي | | 1 |
| | ĺ | 518.41 | 315.12 | 37.93 | 33.70 | 4.23 | 14.59 | 303.64 | 6.40 | -8.17 | 1.113 |
| Unit 3 | L | | · | | | | | | | | |
| ບກແ 3 | | FEED H20 | SH QUT | The second second second second second second second | | FURNACE | EÇONO OUTL-TEMP | SH ROEL | SNCR SHEM FLOW | STEAM FLOW | AVAILABLE CaO |
| ר ' | | for any second second second second | SHOUT DEG F | FINAL STM TEMP | | | ECONO OUIL-TEMP DEG F | | | | AVAILABEE |
| C ∞ Unit 1 | | FLOW | DEG F 884.80 | DEG F 831.67 | KSCFM 84.47 | DRAFT | DEG F 273.89 | DEG F 1188.83 | GPH 3.00 | FLOW KLBs/hr 183.98 | CaO |
| 0 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 | | KLBs/hr 192.53 | DEG F 884.80 | DEG F | KSCFM 84.47 | DRAFT | DEG F | DEG F | <u>GPH 3.00</u> | KLBs/hr | <u>CaO</u> |
| Unit 1 | · | KLBs/hr 192.53 | DEG F 884.80 | DEG F 831.67 830.47 | KSCFM 84.47 | DRAFT " H2O -0.10 | DEG F 273.89 270.73 | DEG F 1188.83 | <u>GPH 3.00</u> | KLBs/hr 183.98 | CaO 1.184 1.184 |
| Unit 1 | | KLBs/hr 192.53 | DEG F 884.80 | DEG F 831.67 830.47 | KSCFM 84.47 | DRAFI " H2O -0.10 | DEG F 273.89 | DEG F 1188.83 | GPH 3.00 | KLBs/hr 183.98 | CaO 1.184 1.184 |

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| Date: Start Time: End Time: | 03/17/10 10:25:00 11:25:00 | | DAYOUTLET | SEURRY E | DIEWAHER | TOTAL | | | EE DP | DINUET | SPECIFIC GRAVITY |
|-----------------------------------|----------------------------------|----------|---------------|----------|----------|------------------|-------------------|---------|-------------------|---------------|---------------------|
| | | DEG F | DEG F | GPM | GPM | GPM | % | DEG F | " H2O | " H2O | " H2O |
| Unit 1 | | 542.08 | 320.74 | 46.84 | 42.97 | 3.87 | 11.51 | 301.82 | 6.43 | -10.43 | 1,117 |
| Unit 2 | 26A run 3 | 509.60 | <u>319.41</u> | 38.21 | 34.83 | 3.38 | 14.13 | 296.25 | 6.06 | -10.26 | 1.117 |
| Unit 3 | | 517.88 | 314.59 | 37.63 | 33.56 | 4.07 | 14.32 | 303.35 | 6.36 | -8.01 | 1.117 |
| 0 | | | | | | | | | | | |
| - 19 | | FEEDIH2O | STM PRESS | | | EURNAGE DRAFT | ECONO OUT TEMP | | SNGR CHEMIELOW | STEAM FLOW | AVAILABLE Cao |
| | | | | | | | | | | | _ |
| | | KLBs/hr | DEG F | DEG F | KSCFM | " H2O | DEG F | DEG F | GPH | KLBs/hr | |
| Unit 1 | | 191.05 | 884.66 | 827.58 | 89.75 | | 274.33 | 1179.78 | 3.84 | 183.08 | 1.229 |
| Unit 2 | | 188.03 | 899.89 | 833.74 | 82.10 | -0.05 | 271.22 | 1191.69 | 5.26 | 184.88 | 1.229 |
| Unit 3 | | 191.54 | 902.09 | 829.31 | 80.09 | -0.15 | 280.63 | 1186.79 | 4.16 | 184.83 | 1.229 |

| Date: Start Time: | 03/18/10 7:09:00 | SDA INLET TEMP | SDA OUTLET | TOTAL SLURRY FL | DIL WATER | TOTAL LIME | CONC | FF OUT | ∵EF -~DP | PRESS | SPECIFIC GRAVITY |
|----------------------|---------------------|---------------------|---------------------------|--------------------|--|-------------------------|--------------------|---------------------------------------|------------------|-------------------|---------------------|
| End Time: | 9:22:00 | | | | | | | | | | |
| | | DEG F | DEG F | GPM | GPM | GPM | % | DEG F | " H2O | " H2O | " H2O |
| Unit 1 | | 509.05 | 319.93 | 36.79 | 29.37 | 7.42 | 14.08 | 302.39 | 5.46 | | 1.128 |
| · _ · _ · | · · · | بيائلان. | | | 1 10 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 | 39 | an alla i | 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 | | <u>d</u> | ف، |
| Unit 2 | 5/29 run 1 | 515.00 | 320.03 | 39.29 | 33.22 | 6.07 | 12.25 | 296.06 | 5.18 | | 1.128 |
| | | 41 | | | | | | ing ing | | | |
| Unit 3 | | 507.70 | <u>314.</u> 95 | 34.65 | 30.39 | 4.26 | 13.84 | 301.49 | 5.87 | -7.55 | 1.128 |
| Offic 9 | | | | _ | | | | | | | |
| Olm 5 | | FEED.H20 FLOW | SH OUT STM PRESS | FINAL STM | | | EGONO OUT. TEMP | | SNCR HEM FLOW | | AVAILABLE CaO |
| | | FLOW | STM PRESS | TEMP | FLOW | DRAFT | <u>QUT, TEMP</u> | AVG | CHEM FLOW | FLOW | |
| Unit 1 | | | STM PRESS | | KSCFM | DRAFT | DEG F | AVG C | GPH | KLBs/hr | <u>CaO</u> - |
| Unit 1 | · · · · | ELOW KLBs/hr | DEG F 885.92 | DEG F | KSCFM 80.02 | DRAFT | <u>QUT, TEMP</u> | AVG | CHEM FLOW | KLBs/hr | <u>CaO</u> 1.354 |
| Unit 1 Unit 2 | ۰ | KLBs/hr | DEG F 885.92 | DEG F 832.20 | KSCFM 80.02 | DRAFT " H2O -0.11 | DEG F | DEG F 1106.97 | GPH 5.48 | KLBs/hr 184.14 | CaO 1.354 |
| Unit 1 | | KLBs/hr [193.02] | DEG F 885.92 900.86 | DEG F 832.20 | KSCFM 80.02 | " H2O -0.11 | DEG F 274.53 | DEG F 1106.97 | GPH 5.48 | KLBs/hr 184.14 | 1.354 |

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| Date: Start Time: End Time: | 03/18/10 9:49:00 12:02:00 | SDAINLET S | | SLURRY FL | DIL WATER | IOTAL EME | LIME CONC | TEMP | DP | IDIN ET | SPECIFIC GRAVITY |
|-----------------------------------|-------------------------------------|-------------------|-----------------|-----------------|----------------|-----------------|-----------------|---------|-------------------|-------------------|---------------------|
| | | DEG F | DEG F | GPM | GPM | GPM | % | DEG F | " H2O | " H2O | " H2O |
| Unit 1 | and the second second second second | 514.15 | 320.16 | 38.65 | 29.82 | 8.84 | 14.94 | 304.42 | 6.13 | -9.82 | 1.129 |
| Unit 2 | 5/29 run 2 | 515.23 | 320.23 | 38.64 | 32.75 | 5.89 | 12.40 | 295.98 | 5.37 | -9.57 | 1.129 |
| Unit 3 | N | 513.45 | 315.11 | 37.19 | 32.55 | 4.64 | 12.91 | 302.74 | 6.44 | -8.24 | 1.129 |
| с - 21 | | FEEDIH2OM | STMIPRESS | FINAL STM | TOT AIR | EURNACE | OUTTEMP | SH ROLL | SNCR CHEMIELOW | STEAM // | AVAILABLE CaO |
| Unit 1 | | KLBs/hr 192.07 | DEG F 883.96 | DEG F 826.50 | KSCFM 82.05 | " H2O -0.09] | DEG F 274.39 | DEG F | GPH 6.24 | KLBs/hr 183.42 | 1.361 |
| | | | | | | | | | | 103.42 | |
| Unit 2 | | 185.14 | 900.29 | 827.81 | 84.87 | -0.09 | 271.37 | 1227.88 | 5.09 | 182.93 | 1.361 |
| Unit 3 | | 189.39 | 902.46 | 825.87 | 81.36 | -0.14 | 280.61 | 1168.99 | 6.50 | 183.68 | 1.361 |

| Date: Start Time: End Time: | 03/18/10 12:27:00 14:39:00 | SDAINLET | SDAXOUIILEIN TEMP | SLURRY FL | DIL WATER | TOTAL | CONC | FFOUT | DP | ID NUET | SPECIFIC GRAVITY |
|-----------------------------------|---|-----------------|----------------------|-----------|-----------|-------|------------------|----------|----------|---------|---------------------|
| | | DEG F | DEG F | GPM | GPM | GPM | % | DEG F | " H2O | " H2O | " H2O |
| Unit 1 | | 508.26 | 319.44 | 35.25 | 27.72 | 7.53 | 14.86 | 303.24 | 6.29 | -9.69 | 1.128 |
| Unit 2 | 5/29 run 3 | 520.15 | 320.60 | 41.44 | 34.31 | 7.13 | 11.67 | 296.01 | 6.26 | -10.60 | 1.128 |
| Unit 3 | | 512.88 | 317.77 | 36.36 | 29.39 | 6.97 | 13.26 | 304.35 | 6.42 | -8.11 | 1.128 |
| | | | | | | | | | | | |
| ר י | | FEEDH2Q FLOW | SHIOUT | FINAL STM | TOTAIR | | ECONO | SHROL | SNCR | STEAM | AVAILABLE. |
| 3 | | PLOW | SIMPRESS | TEMP | ELOW | DRAI | OUNATEMPA | AVG care | CHEMELOW | FLOW | CaO |
| | | KLBs/hr | DEG F | DEG F | KSCFM | " H2O | DEG F | DEG F | GPH | KLBs/hr | |
| Unit 1 | | 170.05 | 877.67 | 827.72 | 79.85 | -0.09 | 272.46 | 1071.96 | 4.29 | 160.11 | 1.354 |
| | and the second se | | | | | | | | | | |
| Unit 2 | | 186.31 | 898.06 | 827.61 | 86.45 | -0.09 | 269.33 | 1213.56 | 6.30 | 183.88 | 1.354 |
| Unit 3 | | 190.78 | 900.35 | 829.24 | 80.90 | -0.15 | 278.64 | 1172.09 | 4.00 | 184.17 | 1.354 |

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| Date: Start Time: End Time: | 03/18/10 7:09:00 8:24:00 | TEMP | DA OUTLER TEMP | SLURRY FL | DIEWATER FLOW | | CONC | HEROUICA MEMP | EF DP | | SPECIFIC GRAVITY |
|-----------------------------------|--------------------------------|----------|-------------------|-----------|------------------|------------------|------------------|------------------|-------------------|---------------|---------------------|
| | | DEG F | DEG F | GPM | GPM | GPM | % | DEG F | " H2O | " H2O | " H2O |
| Unit 1 | and street its state | 510.38 | 319.89 | 37.54 | 29.91 | 7.63 | 13.58 | 302.69 | 6.30 | -10.04 | 1.129 |
| Unit 2 | 13B run 1 | 514.02 | 320.58 | 39.26 | 32.75 | 6.51 | 12.25 | 296.75 | 5.91 | -10.27 | 1.129 |
| Unit 3 | | 507.08 | 314.85 | 34.31 | 30.54 | 3.76 | 13.95 | 301.90 | 6.21 | -7.90 | 1.129 |
| | | | | | | | | | | | |
| 0 | | | | | | | | | | | |
| - 23 | | FEEDIH2O | SHOUT | FINAL STM | FLOW | FURNACE DRAFT | ECONO OUTTEMP | | SNCR CHEM FLOW | STEAM FLOW | |
| | | | | | | | | | | | |
| | | KLBs/hr | DEG F | DEG F | KSCFM | " H2O | DEG F | DEG F | GPH | KLBs/hr | |
| Unit 1 | | 192.79 | 886.09 | 833.76 | 80.97 | -0.11 | 274.46 | 1111.03 | 3.56 | 184.03 | 1.357 |
| Unit 2 | | 185.73 | 900.53 | 827.22 | 80.47 | -0.04 | 271.46 | 1210.14 | 2.53 | 183.90 | 1.357 |
| | | | | | | | | | | | |
| Unit 3 | | 189.92 | 903.17 | 822.15 | 78.90 | -0.16 | 280.74 | 1165.19 | 3.32 | 184.43 | 1.357 |

| Date: Start Time: End Time: | 03/18/10 8:56:00 10:10:00 | SDA IN DET | | ELOTAL SLURRY-EL | DIEWATER FLOW | Total Lime | CONG | TEMP | FE DP | DINEET | SRECIFIC GRAVITY |
|-----------------------------------|--|------------|-----------------------|---------------------|------------------|--------------------|-------------------|------------------|-------------------|-------------------|---------------------|
| | | DEG F | DEG F | GPM | GPM | GPM | % | DEG F | " H2O | " H2O | " H2O |
| Unit 1 | | 509.22 | 320.29 | 36.89 | 28.24 | 8.66 | 15.32 | 303.42 | 4.70 | -8.29 | 1.129 |
| | | | | | 24.04 | | | | | | 4.400 |
| Unit 2 | 13B run 2 | 512.53 | 319.63 | <u> </u> | 31.91 | 5.50 | 12.84 | 295.23 | 3.36 | -7.47 | 1.129 |
| Unit 3 | | 509.21 | 315.01 | 35.52 | 30.69 | 4.82 | 13.50 | 302.07 | 6.15 | -7.83 | 1.129 |
| C - 24 | | FEED H201 | SHIQUIT STIMIPRESS | FINALISTM TEMP | | EURNAGE | ECONO OUIMIEMP | SHROUL- | SNCR CHEMIELOW | ASTEAM FLOW | AVAILABLE: CaO |
| Unit 1 | | KLBs/hr | DEG F 885.22 | DEG F 829.71 | KSCFM 79.99 | <u>" H2O</u> -0.10 | DEG F 274.69 | DEG F 1096.14 | <u></u> | KLBs/hr 184.35 | 1.359 |
| | an an an an an an an an an an an an an a | | | | | | | | | | |
| Unit 2 | | 186.57 | 901.15 | 827.25 | 81.84 | -0.06 | 271.72 | 1238.36 | 6.29 | 184.23 | 1.359 |
| Unit 3 | | 190.29 | 903.19 | 828.86 | 79.76 | -0.13 | 280.90 | 1164.70 | 7.14 | 183.96 | 1.359 |

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| Date: Start Time: | 03/18/10 10:45:00 | SDA INLET | SDA OUTLET | TOTAL | DIL WATER | LIME | LIME | TEMP | DP | ID INLET | SPECIFIC GRAVITY |
|--|----------------------|---|--|--|--|-------------------------|---|--|---------------------|--|---------------------|
| End Time: | 12:05:00 | | | | | | | | | | |
| | | DEG F | DEG_F | <u>GPM</u> | GPM | GPM | % | _DEG F | " H2O | " H2O | <u>" H2O</u> |
| Unit 1 | | 515.91 | 320.26 | 39.20 | 30.38 | 8.82 | 14.75 | 304.56 | 6.41 | -10.15 | 1.12 |
| n - en tatman Sinta ang sinta ang s | | | | States and the second sec | And the second sec | | -يروند. موجوع | | | به هذها الملحة في مقوله المانية . | <u> </u> |
| Unit 2 | 13B run 3 | 514.74 | 319.91 | 38.36 | 32.08 | 6.27 | 12.51 | 295.62 | 5.95 | -10.10 | 1.129 |
| | | | ang war an an an an an an an an an an an an an | م معدد من مطلب جانب، ۲۰ م موالب جانب، ۲۰ م | | | and I and I and I and I and I and I and I and I and I and I and I and I and I and I and I and I and I and I and | ಸೆಯನ್ನು ಇದು ನಿರ್ವಾ ಕರ್ಷನ್ರಮ ಸಂಗಾಣ ಸಂಗಾಣ ಸಂಗಾಣ ಸಂಗಾಣ ಸಂಗಾಣ ಸಂಗಾಣ ಸಂಗಾಣ ಸಂಗಾಣ ಸಂಗಾಣ ಸಂಗಾಣ ಸಂಗಾಣ ಸಂಗಾಣ ಸಂಗಾಣ ಸಂಗಾಣ ಸಂಗಾಣ ಸಂಗಾಣ ಸಂ | | with the second se | |
| | | 515.33 | 315.17 | 37.92 | 32.88 | 5.04 | 12.69 | 302.68 | 6.42 | -8.24 | 1.129 |
| Unit 3 | | 313.33 | | | | | | | | | |
| Unit 3 | | FEED H203 | SHOUT | FINAL STM | FOT AIR FLOW | | | SH ROLL | | | VAILABLE |
| Unit 3 | | FEED H20 | SHOUT | FINAL STM | FLOW | FURNACE | ECONO OUT TEMP | SHROLL ; XVG ; C | SNCR HEM FLOW | STEAM 2 | VAILABLE CaQ2 |
| Unit 3 | | FEED H203 | SHOUT | FINAL STM | | FURNACE DRAFE | | SH ROLL C | SNCR HEM FLOW | STEAM FLOW KLBs/hr | VAILABLE CaO |
| Unit 1 | | KLBs/hr | SH QUT | FINAL STM | KSCFM 82.66 | DRAFT | OUT TEMP | | GPH 5.85 | KLBs/hr 183.13 | 1.36 |
| Unit 1 | | KLBs/hr | SH OUT STM PRESS | FINAL STM | FLOW KSCFM | | DEG F 274.29 | DEG F | GPH 5.85 | KLBs/hr 183.13 | |
| Unit 1 | | FEED H20 ELOW KLBs/hr 191.73 185.35 | SH OUT STN PRESS DEG F 883.74 | FINAL STM | KSCFM 82.66 | " H2O -0.09 -0.10 | DEG F 274.29 271.23 | DEG F 1118.22 | GPH 5.85 | KLBs/hr 183.13] 183.04 | 1.36 |
| Unit 1 | | FEED H20 ELOW KLBs/hr 191.73 185.35 | SH OUT STM PRESS DEG F 883.74 | FINAL STM TEMP. DEG F 826.78 829.43 | KSCFM 82.66 84.72 | " H2O -0.09 | DEG F 274.29 271.23 | DEG F 1118.22 | GPH 5.85 5.10 | KLBs/hr 183.13] | 1.360 |

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| Date: Start Time: | 03/16/10 8:44:00 | SDA INLET | SDA OUTLET | TOTAL SLURBY FL | DIL WATER FLOW | TOTAL Lime | LIME CONC | FF OUT TEMP | FF DP | ID INLET | SPECIFIC GRAVITY |
|----------------------|---|-----------------------------|---------------------------|---|-----------------------------------|---------------------------|---------------------------|-----------------------------|----------------------------|---|--|
| End Time: | 13:36:00 | | | | | | | | | | |
| - | | DEG F | DEG F | GPM | GPM | GPM | % | DEG F | " H2O | " H2O | " H2O |
| Unit 1 | | 525.17 | 314.21 | 39.66 | 29.53 | 10.14 | 14.93 | 296.10 | 6.26 | -9.60 | 1.101 |
| | | | 1977, 994, | یکه ۲۰۰۱ برور در برور افغ مصاحف میتیکنیمیس از ۲۰ | internet and the second second | 2466.5 | ند . منازع: | ∴¥996 _4 | 1927 a cara | 1.200 - 1.200 | |
| Unit 2 | 23 run 1 | 505.56 | 314.21 | 37.60 | 26.96 | 10.64 | 15.84 | 291.01 | 6.06 | -0.38 | 1.101 |
| · | 100 100 100 100 100 100 100 100 100 100 | 200 B | · | COLUMN ACTA SHE SHE | a. 94 20, 9920042) | الد چستالي التركيسية - | | عني⊤ ميور ليدم ويتيشت | | | and the second sec |
| Unit 3 | | 515.85 | 310.20 | 38.53 | 28.18 | 10.35 | 17.08 | 298.31 | 6.40 | -8.42 | 1.101 |
| | | | | | | | | | | | |
| C - 26 | | FEED H20 | SH OUT | FINAL STM | TOT AIR FLOW | FURNACE DRAFT | ECONO OUT.TEMP | | SNCR CHEM FLOW | STEAM FLOW | AVAILABLE CaO |
| - 26 | | KLBs/hr | DEG F | DEG F | KSCFM | " H20 | DEG F | DEG F | GPH | FLOW KLBs/hr | CaO |
| i | ^ | KLBs/hr | STM PRESS | DEG F 831.87 | KSCFM 80.69 | <u> </u> | DEG F 274.50 | DEG F 1161.83 | GPH 8.54 | FLQW KLBs/hr 183.93 | CaO |
| Unit 1 | | KLBs/hr 192.95 | DEG F 884.72 | DEG F 831.87 | KSCFM 80.69 | " H2O -0.10 | DEG F 274.50 | DEG F 1161.83 | GPH 8.54 | FLQW/ KLBs/hr 183.93 | CaO |
| Unit 1 Unit 2 | | KLBs/hr 192.95 186.84 | DEG F 884.72 900.56 | DEG F 831.87 | KSCFM 80.69 81.06 | " H2O -0.10 -0.09 | DEG F 274.50 271.41 | DEG F 1161.83 1130.51 | GPH 8.54 7.09 | FLQW/ KLBs/hr 183.93 184.07 | CaO |
| Unit 1 Unit 2 | | KLBs/hr 192.95 | DEG F 884.72 900.56 | DEG F 831.87 830.83 | KSCFM 80.69 | " H2O -0.10 -0.09 | DEG F 274.50 | DEG F 1161.83 | <u>GPH</u> 8.54 7.09 | FLOW KLBs/hr 183.93 184.07 | CaO |

| Date: Start Time: | | SDA INLET | DA OUTLET | TOTAL | DIL WATER FLOW | | LIME | EF OUT | FF DP | ID INLET | SPECIFIC GRAVITY |
|----------------------|----------|--|---|---------------------------|---|--|-----------------|------------------|---------------------------------|-----------------------------|---------------------|
| End Time: | 12:19:00 | | | | | | | | | | |
| | | DEG F | DEG F | GPM | GPM | GPM | % | DEG F | " H2O | " H2O | " H2O |
| Unit 1 | | 537.55 | 319.46 | 44.75 | 39.24 | 5.51 | 12.31 | 300.57 | 6.38 | -10.20 | 1.11 |
| | | دور روز مرد مستعمله الشيعيد مدينة و | 1. 2. Frank 17 | | | | n the second | 4 | ينين الإشار وي | 2 | |
| Unit 2 | 23 run 2 | 513.76 | 321.23 | 39.31 | 33.96 | 5.34 | 14.34 | 297.57 | 6.14 | -10.46 | 1.1 |
| • • • | | in de la contraction br>La contraction de la c | میں سے جنوب ہے۔ میں اور میں ان اور ان اور اور ان اور اور اور اور اور اور اور اور اور اور | | ^{ار} بیروه . ۲۰ - میدن میداند | And the second s | | ,249, | 64 | | . Y |
| Unit 3 | | 517.78 | 314.97 | 37.53 | 33.27 | 4.26 | 14.63 | 303.48 | 6.36 | -8.10 | 1.1 |
| Shito | | | | | | _ | | | | | |
| | | FEED H20 | SH OUT | | TOLAIR | EURNACE | ECONO | | SNCR | STEAM | |
| Sinco | | FLOW | STM PRESS | TEMP | | | ECONO | | <u> CHEM FLOW</u> | FLOW | |
| | | FLOW | STM PRESS | DEG F | KSCFM | " H2O | DEG F | DEG F | <u>CHEM FLOW</u> | FLOW | <u>Ca</u> Õ |
| Unit 1 | | FLOW KLBs/hr 192.02 | DEG F 884.65 | | KSCFM 86.08 | " H2O -0.10 | DEG F 274.09 | | <u>CĤEM FLOW</u> GPH 3.74 | FLOW | <u>CaŎ</u> |
| Unit 1 | | FLOW KLBs/hr 192.02 | DEG F 884.65 | DEG F 828.14 | KSCFM 86.08 | " H2O -0.10 | DEG F 274.09 | DEG F 1186.61 | GPH 3.74 | KLBs/hr 183.69 | CaO |
| Unit 1 Unit 2 | | KLBs/hr 192.02 | DEG F 884.65 899.37 | DEG F 828.14 831.64 | KSCFM 86.08 83.35 | " H2O -0.10 | DEG F 274.09 | DEG F 1186.61 | GPH 3.74 4.90 | KLBs/hr 183.69 184.25 | |
| Unit 1 Unit 2 | | KLBs/hr 192.02 | DEG F 884.65 | DEG F 828.14 831.64 | KSCFM 86.08 | " H2O -0.10 | DEG F 274.09 | DEG F 1186.61 | GPH 3.74 | KLBs/hr 183.69 184.25 | CaO |

| Date: Start Time | 03/17/10 : 12:53:00 | | SDA QUTEET TEMP | | DIL WATER | TOTAL LIME | | FF OUT TEMP | FF. DP | A 19 | SPECIFIC GRAVITY |
|---------------------------------------|--|----------|--|--|--|---|--|------------------------|-----------|---|-----------------------|
| End Time: | 17:26:00 | | | | | | | | | | |
| | | DEG F | DEG F | GPM | GPM | GPM | % | DEG F | " H2O | " H2O | " H2O |
| Unit 1 | | 540.04 | 319.73 | 45.57 | 39.94 | 5.63 | 11.61 | 301.42 | 6.31 | -10.19 | 1.117 |
| · · · · · · · · · · · · · · · · · · · | | | م میں اور اور اور اور اور اور اور اور اور اور | | ، (۲۵) میلید د میلید و در از از از از از از از از از از از از از | الم المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع المراجع ال المراجع المراجع ا | | | | | 1777 ····· |
| Unit 2 | 23 run 3 | 523.35 | 320.26 | 43.11 | 39.25 | 3.85 | 12.27 | 296.85 | 6.10 | -10.77 | 1.117 |
| | 2 8.5 45 | | | the designation of the big | | | ΞĒ. | | | الله به مراجع بر هو. مراجع محمد به معهد المع | |
| Unit 3 | | 525.77 | 315.08 | | 35.98 | 4.01 | 13.23 | 304.01 | 6.41 | -8.35 | 1.117 |
| о | | FEED H20 | SHOUT | FINAL STM | TOTAIR | EURNACE | ECONO | SHROEL | SNCR | STEAM | AVAILABLE |
| 28 | | FLOW | STM PRESS | TEMP | FLOW | DRAFT | OUT TEMP | AVG | CHEM FLOW | FLOW | GaO 3 |
| | | KLBs/hr | DEG F | DEG F | KSCFM | " H2O | DEG F | DEG F | GPH | KLBs/hr | |
| Unit 1 | | 192.65 | 885.16 | 830.70 | 87.67 | -0.09 | | 1185.54 | 4.34 | 183.90 | 1.231 |
| | | | and the second s | | | - | من من من من من من من من من من من من من م | يون در محمد المراجع | Ţ Ŵ | Marche - 6 | · · · · · · · · · · · |
| Unit 2 | | 186.18 | 898.94 | 826.74 | 88.04 | -0.05 | | 1220.36 | 3.31 | 183.85 | 1.231 |
| 1945 | ار بار می از بر مربع می از بر مربع می از می این می می ورود می می این از می | | - | مر الأورية بيلوث أريبية. الإليان مستخلف | 12 9 22 - Li | | موجود می اور د مراجع می اور د | · /4 - 7.7 | | 577782 2 1 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 | |
| Unit 3 | | 189,26 | 901.76 | 822.33 | 84.26 | -0.15 | 280.25 | 1185.92 | 3.41 | 183.82 | 1.231 |

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| Date: Start Time: End Time: | 03/16/10 7:17:00 8:17:00 | ESDAINLEIE S TEMPS | SDAYOUTIGET | TOTAL SLURRY FL | DIEWAHER FLOW | TOTAL SE | | TEMP | FF DP | DINEET PRESS | SPECIFIC GRAVITY |
|-----------------------------------|--------------------------------|-----------------------|-------------|--------------------|------------------|------------------|--------|--|----------|-----------------|---------------------|
| | | DEG F | DEG F | GPM | GPM | GPM | % | DEG F | " H2O | " H2O | " H2O |
| Unit 1 | | 518.33 | 310.44 | 37.88 | 29.54 | 8.35 | 14.46 | 293.63 | 6.20 | -9.44 | 1.113 |
| Unit 2 | | 502.44 | 309.96 | 39.18 | 28.80 | 10.38 | 14.08 | 287.71 | 6.06 | 0.00 | 1.113 |
| Unit 3 | 26A run 1 | 507.32 | 309.94 | 35.80 | 26.15 | 9.64 | 16.07 | 297.73 | 6.29 | -8.21 | 1.113 |
| | | · | | | | | | L | | | |
| c | | | | | | | | ta - a faire and a faire and a faire and a faire and a faire and a faire and a faire and a faire and a faire a | | | |
| - 29 | | FEEDH2O FLOW | SH OUT | EINAL SIM | | EURNAGE DRAFT | | SH ROLL | CHEMILOW | | |
| | | | | | | | | ····· | | | |
| | | KLBs/hr | DEG F | DEG F | KSCFM | " H2O | DEG F | DEG F | GPH | KLBs/hr | |
| Unit 1 | | 192.35 | 885.37 | 827.64 | 78.35 | -0.10 | 274.23 | 1163.29 | 7.06 | 184.15 | 1.183 |
| Unit 2 | | 187.30 | 901.20 | 836.77 | 80.06 | -0.08 | 271.11 | 1138.53 | 5.37 | 184.38 | 1.183 |
| Unit 3 | | 191.60 | 903.26 | 835.02 | 79.72 | -0.24 | 280.47 | 1143.29 | 4.76 | 184.60 | 1.183 |

| Date: Start Time: | 03/16/10 9:04:00 | SDA INLET | SDA OUTLET | | DIL WATER | | | FF OUT TEMP | FF DP | ID INLET | SPECIFIC GRAVITY |
|----------------------|---------------------|---------------------------------------|-----------------|--|---|---------------------|-------------------|-----------------------------|-----------------------|--|---|
| End Time: | 10:04:00 | | | | | | | | | | |
| | | DEG F | DEG F | GPM | GPM | GPM | % | DEG F | " H2O | " H2O | " H2O |
| Unit 1 | | 525.95 | 310.19 | 40.99 | 31.86 | 9.13 | 14.65 | 293.31 | 6.31 | -9.71 | 1.10 |
| | | ـــــــــــــــــــــــــــــــــــــ | | و و ¹¹¹ . ب_ ه در مسر بنمی | ا در کار در | (a) | | | रहाकर अस्त्र के कि | | |
| Unit 2 | | 501.87 | 309.30 | 37.44 | 24.16 | 13.28 | 16.28 | 287.41 | 6.01 | -0.23 | 1.10 |
| | | بر مسترد | | 545 - 5 - 5 | ا ^{بر} الشیبینی و و و | ميسند. م ديد 194 | | уч | د . رو ، تعیور | n - unita de la California. En la cal | and the second se |
| Unit 3 | 26A run 2 | 514.35 | 310.13 | 38.08 | 28.30 | 9.78 | 19.05 | 298.22 | 6.28 | -8.36 | 1.10 |
| Offic 9 | | | | | | | | | | | |
| | | FEED H20 | SH OUT | FINAL STM | TOT AIR FLOW | | ECONO OUT TEMP | SH ROLL | SNCR CHEM FLOW | STEAM FLOW | |
| | | | | | TOT AIR FLOW | FURNACE | OUT TEMR | | | 1.4.17 L | AVAILABLE CaO |
| , | | | DEG F | | KSCFM | FURNACE DRAFT | DEG F | | | 1.4.17 L | CaO |
| Unit 1 | | KLBs/hr 193.09 | DEG F 885.09 | TEMP | <u>FLOW</u> | <u>DRAFT</u> | DEG F 274.51 | DEG F 1163.90 | CHEMIFLOW | FLOW KLBs/hr 183.83 | CaO |
| Unit 1 | | KLBs/hr 193.09 | DEG F | DEG F 830.98 | KSCFM | <u>" H2O</u> | DEG F | DEG F 1163.90 | GPH | KLBs/hr 183.83 | CaO |
| Unit 1 | A Vices | KLBs/hr 193.09 | DEG F 885.09 | DEG F 830.98 828.35 | KSCFM 81.31 80.42 | " H2O -0.10 | DEG F 274.51 | DEG F 1163.90 1125.45 | GPH 8.81 5.76 | KLBs/hr 183.83 | ÇaO |
| Unit 1 | | KLBs/hr [193.09] | DEG F 885.09 | DEG F 830.98 | KSCFM 81.31 | " H2O -0.10 | DEG F 274.51 | DEG F 1163.90 1125.45 | GPH 8.81 | KLBs/hr 183.83 | 1.05 |

| Date: Start Time: End Time: | 03/16/10 10:32:00 11:32:00 | SDA INLET TEMP | SDA OUTLET | TOTAL SLÙRRY FL | DIL WATER F <u>LOW</u> | LINE | LIME | FF OUT. | DP - | ID INLET | SPECIFIC GRAVITY |
|-----------------------------------|---------------------------------------|-------------------|---|--|--|---------|-------------------|--------------|--|--|---------------------|
| | | DEG F | DEG F | GPM | GPM | GPM | % | DEG F | " H2O | " H2O | " H2O |
| Unit 1 | | 523.86 | 310.23 | 39.31 | 28.74 | 10.57 | 15.07 | 293.75 | 6.18 | -9.45 | 1.101 |
| | يوريون ورو | | 4.10- 13823 1 | Haland Cont on all states | State of the state | | 1.486 1.4 | 124 | (************************************* | معد به اور در همیدهدان. معرف به در میشوانید م | |
| Unit 2 | | 503.24 | 311.09 | 37.65 | 26.39 | 11.26 | 15.69 | 288.53 | 6.08 | -0.35 | 1.101 |
| · | · · · · · · · · · · · · · · · · · · · | | ار معلوظتی مید. مدر م او هشته است معاط از از ا | | | | | | | | [ها ا: مکر |
| Unit 3 | 26A run 3 | 513.38 | 309.94 | 37.45 | 26.95 | 10.49 | 18.57 | 298.15 | 6.43 | -8.35 | 1.101 |
|) - 2 | | FEED H20 FLOW | STM PRESS | FINAL STM | TOLAIR - | FURNAGE | ECONO OUT TEMP | SH ROPL | CHEM-FLOW | STEAM ELOW | |
| Unit 1 | | KLBs/hr | DEG F 885.14 | DEG F 834.99 | KSCFM 79.61 | H2O | DEG_F274.59 | DEG_F1163.54 | GPH 10.29 | KLBs/hr 184,51 | 1.059 |
| | | | | August 2 Street House (1997 19 76 77 - 7 | | | | | 10.20 | | |
| Unit 2 | | 186.43 | 900.78 | 829.96 | 80.32 | -0.08 | 271.53 | 1132.18 | 9.15 | 184.21 | 1.059 |
| | | | ALC: 1 | | | : A | | 10 See | · 14 · · · · · · · · · · · · · · · · · · | | |
| Unit 3 | · · · · · · · · · · · · · · · · · · · | 190.76 | 902.66 | 829.05 | 80.58 | -0.25 | 280.84 | 1163.19 | 5.38 | 184.30 | 1.059 |

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| Date: Start Time: | 03/17/10 6:50:00 | SDA INLET | SDA OUTLET | | DIL WATER FLOW | TOTAL LIME | | FF OUT | DP | ID INLET PRESS | SPECIFIC GRAVITY |
|----------------------|---------------------|-----------|------------------------|---------------------------|--|--|---------------------------|--|--|-----------------------------|---------------------|
| End Time: | 9:03:00 | | | | | | | | | | |
| | | DEG F | DEG F | GPM | GPM | GPM | % | DEG F | " H2O | " H2O | " H2O |
| Unit 1 | | 534.58 | 318.05 | 43.74 | 36.83 | 6.91 | 12.81 | 299.11 | 6.34 | -10.06 | 1.109 |
| | | | | | en de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de la comprese de | 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1 | د <u>م</u> لم م م | ilana data data data data data data data d | ارو ایرانده او ایرانده او ایراندا به مطلقه | RAN NAME | |
| Unit 2 | | 518.71 | 323.35 | 39.44 | 32.03 | 7.41 | 15.08 | 298.76 | 6.17 | -10.51 | 1.109 |
| | | <u> </u> | S. C. C. R. Barrer, B. | Lange and the second | | - T | | and the second second | | | _775.76 |
| Unit 3 | 5/29 run 1 | 518.91 | 315.03 | 37.81 | 33.36 | 4.45 | 14.79 | 303.64 | 6.36 | -8.17 | 1.109 |
| 3 | | FEED H20 | SH OUT | | TOTAR | FURNACE | ECONO | SHROLL | SNCR | STEAM | AVAILABLE |
| | | | | | FLOW | DRAFT | OUTTEMP | AVĞ | CHEM FLOW | FLOW | CaO |
| | | KLBs/hr | DEG F | DEG F | KSCFM | " H2O | DEG F | DEG F | GPH | KLBs/hr | CaO |
| Unit 1 | | 192.27 | 884.55 | DEG_F 827.85 | KSCFM 82.80 | " H2O 0.10 | <u> </u> | DEG F 1191.48 | GPH 4.22 | KLBs/hr 183.87 | 1.142 |
| | | 192.27 | 884.55 | DEG F 827.85 | KSCFM 82.80 | " H2O 10 | DEG F 274.04 | DEG F 1191.48 | GPH 4.22 | KLBs/hr 183.87 | 1.142 |
| Unit 2 | | 192.27 | 884.55 899.39 | DEG F 827.85 832.88 | KSCFM 82.80 83.43 | " H2O -0.10 -0.10 | DEG F 274.04 270.92 | DEG F 1191.48 | GPH 4.22 4.44 | KLBs/hr 183.87 183.94 | 1.142 1.142 |
| | ····· | 192.27 | 884.55 | DEG F 827.85 832.88 | KSCFM 82.80 83.43 | " H2O -0.10 -0.10 | DEG F 274.04 270.92 | DEG F 1191.48 | GPH 4.22 4.44 | KLBs/hr 183.87 | 1.142 1.142 |

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| Date: Start Time: End Time: | 03/17/10 9:26:00 11:38:00 | SDANNEET S | DA OUTLET | SLURRY PL | DIL WATER | | | | DP- | | SPECIFIC GRAVITY |
|-----------------------------------|---------------------------------|------------|-----------|-----------|-----------|---------|--------|---------|-------|---------|---------------------|
| | | DEG F | DEG F | GPM | GPM | GPM | % | DEG F | " H2O | " H2O | " H2O |
| Unit 1 | | 538.98 | 320.38 | 45.10 | 40.75 | 4.35 | 12.10 | 301.55 | 6.36 | -10.22 | 1.115 |
| Unit 2 | | 510.42 | 319.55 | 39.10 | 35.25 | 3.85 | 13.93 | 296.48 | 6.09 | -10.37 | 1.115 |
| Unit 3 | 5/29 run 2 | 518.06 | 314.86 | 37.78 | 33.61 | 4.17 | 14.42 | 303.42 | 6.42 | -8.13 | 1.115 |
| ۲ پ | | FEED'H2O' | SHOUTA | FINALSTMI | TOTAIR | FURNACE | | SHIROUL | SNCR | STEAM | |
| | | KLBs/hr | DEG F | DEG F | KSCFM | " H2O | DEG F | DEG F | GPH | KLBs/hr | |
| Unit 1 | | 192.25 | 884.64 | 829.15 | 87.64 | -0.10 | 274.34 | 1186.25 | 3.50 | 183.60 | 1.214 |
| Unit 2 | | 187.04 | 899.30 | 828.44 | 83.26 | -0.05 | 271.24 | 1194.99 | 4.18 | 184.42 | 1.214 |
| Unit 3 | | 190.81 | 901.62 | 827.89 | 80.87 | -0.15 | 280.64 | 1191.68 | 3.95 | 184.22 | 1.214 |

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| Date: Start Time: End Time: | 03/17/10 11:59:00 14:11:00 | SDA INLET TEMP | SDA OUTLET | SLURRY FL | DIL WATER FLOW | total Lime | LIME Conc | FF OUT- | FE DP | id inlet Press | SPECIFIC GRAVITY |
|-----------------------------------|---|---------------------------------------|-----------------|--------------|-------------------|---------------|-------------------|-----------------|---------------|-------------------|--|
| Unit 1 | | DEG F 542.45 | DEG F 319.87 | GPM 46.92 | GPM 41.66 | GPM 5.26 | <u>%</u> 11.28 | DEG F 301.15 | " H2O 6.37 | <u></u> | " H2O 1.117 |
| Unit 2 | میں میں میں میں میں اور اور اور اور اور اور اور اور اور اور | · · · · · · · · · · · · · · · · · · · | 319.87 | | 36.91 | 3.15 | 13.21 | 296.88 | States and | -10.39 | 1.117 |
| Unit 3 | 5/29 run 3 | 521.57 | 315.24 | | 34.73 | 4.00 | 13.66 | | 6.39 | -8.28 | 1.117 |
| | | | | | | | | | | | |
| C - 34 | | FEED H2O | SHOUT STM PRESS | | TOT AIR- | | | SFIROLL | SNGR | STEAM FLOW | |
| | | KLBs/hr | DEG F | DEG F | KSCFM | " H2O | DEG F | DEG F | GPH | KLBs/hr | |
| Unit 1 | - | 192.41 | 885.44 | 828.19 | 89.54 | -0.10 | 273.89 | 1187.27 | 3.95 | 184.20 | 1.230 |
| | • | | | 827.40 | | | | 1205.01 | | 103 50 | اند به کمد: میک معمود در میک 1 020 |
| | | 186.00 | 898.90 | 827.40 | 86.13 | -0.04 | 270.84 | 1205.01 | 4.28 | 183.58 | 1.230 |
| Unit 3 | en en l'ann | 189.20 | 901.75 | 824.28 | 82.65 | -0.15 | 280.21 | 1195.13 | 3.52 | 183.50 | 1.230 |

| Date: Start Time: | 03/16/10 11:49:00 | SDA INLET | SDA OUTLET TEMP | TOTAL SLURRY FL | DIL WATER | | LIME Cong | FF OUT | FF DP | ID INLET PRESS | SPECIFIC GRAVITY |
|----------------------|----------------------|---------------------------------------|--|-----------------------------------|-------------------------|----------------|---------------------------------|--------------------------------|--|---------------------------|---------------------|
| End Time: | 13:07:00 | | | | | | | | _ | | |
| | | DEG F | DEG F | GPM | GPM | GPM | % | DEG F | " H2O | " H2O | " H2O |
| Unit 1 | | 523.69 | 319.94 | 38.04 | 26.97 | 11.06 | 15.40 | 299.79 | 6.28 | -9.57 | 1.102 |
| Limit O | | 509.43 | 319.81 | 37.28 | 29.08 | 8.20 | 45.70 | | <u> </u> | 0.25 | 1.102 |
| Unit 2 | | 509.43 | | 31.20 | | | 15.72 | 295.29 | 5.95 | -0.35 | 1.102 3.46% |
| | 400 | 517.27 | 310.20 | 38.84 | 28.22 | 10.62 | 15.08 | 298.31 | 6.45 | -8.43 | 1.102 |
| Unit 3 | 13B run 1 | | | CIMAL CTR | TOT NR | -EUDNAGE I | FRONDA | <u>eurooi 1</u> | SHOP | CTEARA | |
| Unit 3 | 13B run 1 | | | | | | | | | | |
| Unit 3 | | FEED H20 | SH OUT STM PRESS | FINAL STM | TOT AIR ELOW | FURNACE DRAFT | ECONO ⁴¹ OUT TEMP | SH ROLL AVĞ | SNGR CHEM FLOW | STEAM | L 11/2 |
| Unit 3 | | FEED H20 | SHOUT | | | | | * 1 San * | | | L 0.0 |
| Unit 3 | | FEED H20 | SHOUT | | | | | * 1 San * | | | AVAILABLE; ČaO |
| Unit 3 | | FEED H2O FLOW | SH OUT SIM PRESS DEG F 884.15 | TEMP | <u>FLOW</u> | DRAFT | OUT TEMP | AVG DEG F 1160.56 | <u>СНЕМ FLOW</u> <u>GPH</u> 7.44 | FLOW KLBs/hr 183.80 | ČaO |
| Unit 1 | | FEED H2O FLOW KLBs/hr 192.55 | SH OUT STM PRESS DEG F 884.15 | TEMP, DEG F 829.65 | KSCFM 80.35 | " H2O -0.10 | DEG F 274.54 | AVG DEG F 1160.56 | <u>СНЕМ FLOW</u> GPH 7.44 | FLOW KLBs/hr 183.80 | CaO |
| Unit 1 | | FEED H2O FLOW KLBs/hr | SH OUT SIM PRESS DEG F 884.15 | TEMP DEG F 829.65 829.77 | KSCFM 80.35 81.31 | " H2O -0.10 | DEG F 274.54 | AVG DEG F 1160.56 | <u>СНЕМ FLOW</u> GPH | FLOW KLBs/hr 183.80 | ČaO |

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| Date: Start Time: | 03/16/10 13:33:00 | SDATINILET S | | | DIL WATERS | EIME | | | DP | DINLET PRESS | SPECIFIC GRAVITY |
|----------------------------|----------------------|--------------|------------|------------|------------|---------|-------------------|------------------|---------|--------------|---------------------|
| End Time: | 14:44:00 | | | | | | | | | | |
| | | DEG F | DEG F | GPM | GPM | GPM | % | DEG F | " H2O | " H2O | " H2O |
| Unit 1 | ······ | 530.14 | 319.82 | 40.37 | 34.51 | 5.86 | 14.28 | 299.53 | 6.31 | -9.70 | 1.105 |
| COLORIS IN THE PROPERTY IN | | | | | | | | | | | |
| Unit 2 | | 510.14 | 319.00 | 37.06 | 33.48 | 3.58 | 15.57 | 295.41 | 5.98 | -10.38 | 1.105 |
| Unit 3 | 13B run 2 | 523.75 | 309.60 | 41.25 | 36.10 | 5.14 | 12.00 | 298.87 | | -8.54 | 1.105 |
| Unit S | 130 101 2 | 523.75 | | 41.25 | 30.10 | 5.14 | 13.99 | 290.07 | 6.40 | ~0.54 | 1.105 |
| | | | | | | | | | | | |
| _ | | | | | | | | | | | |
| Ç ' | | BREEDH201 | SHOUT | FINAL STME | TOTAIR | FURNACE | ECONO | SHROLLE | SNCR | STEAM | VALABLE |
| 36 | | FEEDH201 | STIMPRESS: | TEMP | FLOW | DRAFT | ECONO OUT-TEMP | SHIROLLSE AVG | HEMELOW | STEAM | CaO |
| • | | | | | | | | | | | |
| | | | | | | | | | | | |
| | | KLBs/hr | DEG F | DEG F | KSCFM | " H2O | DEG F | DEG F | GPH | KLBs/hr | |
| Unit 1 | | 192.75 | 883.72 | 827.98 | 82.23 | -0.09 | 274.23 | 1155.16 | 3.55 | 183.42 | 1.098 |
| | | | | | | | | | | | |
| Unit 2 | | 186.36 | 899.41 | 829.43 | 81.67 | -0.10 | 271.14 | 1135.01 | 5.53 | 183.91 | 1.098 |
| Unit 3 | | 190.74 | | 828.59 | ec 201 | | 200 52 | 4400.00 | 4.70 | | |
| Unit 3 | | 190.74 | 901.41 | 020.59 | 86.28 | -0.25 | 280.52 | 1160.26 | 4.76 | 183.92 | 1.098 |

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| Date: Start Time: | 03/16/10 15:07:00 | SDA IN ET | SDA OUTLET | SLURRY FL | DILWATER | | CONC | HEMP | DP | PRESS | SPECIFIC GRAVITY |
|----------------------|---------------------------------------|-----------|------------|------------|----------------|-------|--------|---------|-------------|---------|---------------------|
| End Time: | 16:16:00 | DEG F | DEG F | GPM | GPM | GPM | % | DEG F | " H2O | " H2O | " H2O |
| Unit 1 | | 527.22 | 320.05 | 39.23 | 31.94 31.94 | 7.29 | 14.69_ | 298.23 | <u>6.26</u> | -9.48 | 1.106 |
| Unit 2 | | 511.31 | 314.91 | 38.17 | 33.82 | 4.35 | 14.94 | 292.16 | 5.97 | -10.03 | 1.106 |
| Unit 3 | 13B run 3 | 518.15 | 309.80 | 38.87 | 34.47 | 4.40 | 14.68 | 298.86 | 6.34 | -8.26 | 1.106 |
| | | | | | | | | | | | |
| 0 | | REEDH20 | SHOUT | CINATECTAR | ATATA D | | | | SNOD | STEAM | |
| - 37 | | FLOW | STM PRESS | | TOT AIR A | DRAET | | | HEMIFLOW | ELOW-F | |
| | | | | | | | | | | | |
| • | | KLBs/hr | DEG F | DEG F | KSCFM | " H2O | DEG F | DEG F | GPH | KLBs/hr | |
| Unit 1 | · · · · · · · · · · · · · · · · · · · | 193.35 | 883.40 | 826.50 | 80.32 | -0.10 | 274.66 | 1156.16 | 5.75 | 184.19 | 1.113 |
| Unit 2 | | 186.33 | 898.06 | 824.13 | 81.28 | -0.09 | 271.54 | 1172.85 | 4.37 | 184.17 | 1.113 |
| Unit 3 | | 190.60 | 900.56 | 827.40 | 82.97 | -0.25 | 280.97 | 1167.53 | 6.07 | 184.24 | 1.113 |

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Plant Name: NBWD General Average Report Reporting Period: 03/16/2010 to 03/16/2010

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Page: 1

Site Name: UNIT1 Data Averaging Type: 6m Time of Report: 03/18/10 13:21 Rolling Average Interval: 1

| | | OPACITY1 | |
|------------|---------|------------|--|
| Date | Time | (PERCENT) | |
| 03/16/10 | 07:18 | 2 | |
| | 07:24 | 2 | |
| | 07:30 | 2 | |
| | 07:36 | 2 | |
| | 07:42 | 2 | |
| | 07:48 | 2 | |
| | 07:54 | 2 | |
| | 08:00 | 2 | |
| | 08:06 | 2 | |
| | 08:12 | 2 | |
| | 08:19 | 2 | |
| | 08:24 | 2 | |
| | 08:30 | 2 | |
| | 08:36 | 2 | |
| | 08:42 | 2 | |
| | 08:48 | 2 | |
| | 08:54 | 2 | |
| | 09:00 | 2 | |
| | 09:06 | 2 | |
| | 09:12 | 2 | |
| | 09:18 | 2 | |
| | 09:24 | 2 | |
| | 09:30 | 2 | |
| | | | |
| Av | erage = | 2 | |
| Geometric | Avg. = | 2 | |
| Ma | ximum = | 2 | |
| Mi | nimum - | 2 | |
| Possible V | alues = | 23 | |
| Included V | | 23 | |
| | Total 🛥 | 43 | |

- excluded values (missing, OOC, invalid, suspect) ٠

- missing <
- out-of-control т
- invalid Ι
- 8 - suspect
- Ħ exceedance
- F stack not operating
- invalid (PADER) в
- missing data substituted σ

-999 - missing value

Plant Name: NBWD General Average Report Reporting Period: 03/16/2010 to 03/16/2010

Site Name: UNIT1 Data Averaging Typ

Data Averaging Type: 6m

Time of Report: 03/18/10 13:21 Rolling Average Interval: 1

| | | OPACITY: | 1 |
|----------|-------|----------|---|
| Date | Time | (PERCENT |) |
| 03/16/10 | 10:00 | | 2 |
| | 10:06 | | 2 |
| | 10:12 | | 2 |
| | 10:18 | | 2 |
| | 10:24 | | 2 |
| | 10:30 | | 2 |
| | 10:36 | | 2 |
| | 10:42 | | 2 |
| | 10:48 | | 2 |
| | 10:54 | | 2 |
| | 11:00 | | 2 |
| | 11:06 | | 2 |
| | 11:12 | | 2 |
| | 11:18 | | 2 |
| | 11:24 | | 2 |
| | 11:30 | | 2 |
| | 11:36 | | 2 |
| | 11:42 | | 2 |
| | 11:48 | | 2 |
| | 11:54 | | 2 |
| | 12:00 | | 2 |
| | 12:06 | | 2 |
| | | | |

| Average | = | 2 |
|-----------------|---|----|
| Geometric Avg. | = | 2 |
| Maximum | = | 2 |
| Minimum | = | 2 |
| Possible Values | = | 22 |
| Included Values | • | 22 |
| Total | = | 40 |
| | | |

excluded values (missing, OOC, invalid, suspect)

- < missing
- T Out-of-control
- I invalid
- S Suspect
- H exceedance
- F stack not operating
- B invalid (PADER)

U - missing data substituted

-999 - missing value

Plant Name: NBWD General Average Report Reporting Period: 03/16/2010 to 03/16/2010

Site Name: UNIT1 Data Averaging Type: 6m Time of Report: 03/18/10 13:22 Rolling Average Interval: 1

| | | OPACITY1 | |
|-------------|---------|----------|---|
| Date | Time | (PERCENT |) |
| 03/16/10 | 12:36 | | 2 |
| | 12:42 | | 2 |
| | 12:48 | | 2 |
| | 12:54 | | 2 |
| | 13:00 | | 2 |
| | 13:06 | | 2 |
| | 13:12 | | 2 |
| | 13:18 | | 2 |
| | 13:24 | | 2 |
| | 13:30 | | 2 |
| | 13:36 | | 2 |
| | 13:42 | | 2 |
| | 13:48 | | 2 |
| | 13:54 | | 2 |
| | 14:00 | | 2 |
| | 14:06 | | 2 |
| | 14:12 | | 2 |
| | 14:18 | | 2 |
| | 14:24 | | 2 |
| | 14:30 | | 2 |
| | 14:36 | | 2 |
| | 14:42 | | 2 |
| | | | |
| | arage = | | 2 |
| Geometric | - | | 2 |
| | cimum = | | 2 |
| | nimum = | | 2 |
| Possible Va | | 2 | |
| Included Va | | 2 | |
| 1 | Cotal = | 4 | 2 |

excluded values (missing, OOC, invalid, suspect)

< - missing

T - out-of-control

I - invalid

s - suspect

H - exceedance

F - stack not operating

B - invalid (PADER)

U - missing data substituted

-999 - missing value

Page: 1

Plant Name: NBWD General Average Report Reporting Period: 03/18/2010 to 03/18/2010

Site Name: UNIT2 Data Averaging Type: 6m Time of Report: 03/18/10 13:23 Rolling Average Interval: 1

| | | OPACITY2 |
|----------|-------|------------|
| Date | Time | (PERCENT) |
| 03/18/10 | 07:06 | 0 |
| | 07:12 | 0 |
| | 07:18 | 0 |
| | 07:24 | 0 |
| | 07:30 | 0 |
| | 07:36 | 0 |
| | 07:42 | 0 |
| | 07:48 | 0 |
| | 07:54 | 0 |
| | 08:00 | 0 |
| | 08:06 | 0 |
| | 08:12 | 0 |
| | 08:18 | 0 |
| | 08:24 | 0 |
| | 08:30 | 0 |
| | 08:36 | 0 |
| | 08:42 | 0 |
| | 08:48 | 0 |
| | 08:54 | 0 |
| | 09:00 | 0 |
| | 09:06 | 0 |
| | 09:12 | 0 |
| | 09:18 | 0 |
| _ | | |
| | | |

| Average | - | 0 |
|-----------------|---|----|
| Geometric Avg. | • | |
| Maximum | - | 0 |
| Minimum | - | 0 |
| Possible Values | - | 23 |
| Included Values | = | 23 |
| Total | = | 0 |

- excluded values (missing, OOC, invalid, suspect)
- < missing
- T out-of-control
- I invalid
- S suspect
- H exceedance
- F stack not operating
- B invalid (PADER)
- U missing data substituted
- -999 missing value
- -888 value could not be calculated

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Plant Name: NBWD General Average Report Reporting Period: 03/18/2010 to 03/18/2010

Site Name: UNIT2 Data Averaging Type: 6m Time of Report: 03/18/10 13:24 Rolling Average Interval: 1

| | | | OPACITY2 | |
|-----|------------|----------------|------------|---|
| ··• | Date | Time | (PERCENT) | |
| | 03/18/10 | 09:48 | 0 | |
| | | 09:54 | 0 | |
| | | 10:00 | 0 | |
| | | 10:06 | 0 | |
| | | 10:12 | 0 | |
| | | 10:19 | 0 | |
| | | 10:24 | 0 | |
| | | 10:30 | 0 | |
| | | 10:36 | 0 | |
| | | 10:42 | 0 | |
| | | 10:48 | O | |
| | | 10:54 | 0 | |
| | | 11:00 | 0 | |
| | | 11:06 | O | |
| | | 11:12 | o | |
| | | 11:19 | 0 | |
| | | 11:24 | 0 | · |
| | | 11:30 | 0 | |
| | | 11:36 | D | |
| | | 11:42 | 0 | |
| | | 11:48 | 0 | |
| | | 11:54 | O | |
| | | 12:00 | 0 | |
| - | | | | |
| | Ave | erage = | 0 | |
| | Geometric | λ vg. = | | |
| | Max | cimum = | 0 | |
| | Mir | 1mum = | D | |
| P | ossible Va | alues = | 23 | |
| 1 | ncluded Va | lues - | 23 | |
| | | | | |

excluded values (missing, OOC, invalid, suspect)

0

< - missing

T - out-of-control

I - invalid

8 - suspect

H - exceedance

F - stack not operating

Total =

B - invalid (PADER)

U - missing data substituted

-999 - missing value

Plant Name: NBWD General Average Report Reporting Period: 03/18/2010 to 03/18/2010

Site Name: UNIT2 Data Averaging Type: 6m

Time of Report: 03/18/10 14:42 Rolling Average Interval: 1

| | | UTACITI | |
|-----------|--------|----------|---|
| Date | Time | (PERCENT |) |
| 03/18/10 | 12:24 | | 0 |
| | 12:30 | | 0 |
| | 12:36 | | 0 |
| | 12:42 | | 0 |
| | 12:48 | | 0 |
| | 12:54 | | 0 |
| | 13:00 | | 0 |
| | 13:06 | | 0 |
| | 13:12 | | 0 |
| | 13:18 | | 0 |
| | 13:24 | | 0 |
| | 13:30 | | 0 |
| | 13:36 | | 0 |
| | 13:42 | | 0 |
| | 13:48 | | 0 |
| | 13:54 | | 0 |
| | 14:00 | | 0 |
| | 14:06 | | 0 |
| | 14:12 | | 0 |
| | 14:18 | | 0 |
| | 14:24 | | 0 |
| | 14:30 | | 0 |
| | 14:36 | | 0 |
| | | | |
| Ave | rage = | | 0 |
| Geometric | Avg. = | | |
| Max | imum = | | 0 |
| Min | imum = | | 0 |
| | | | |

OPACITY2

| Maximum | - | 0 |
|-----------------|---|----|
| Minimum | = | 0 |
| Possible Values | = | 23 |
| Included Values | = | 23 |
| Total | = | 0 |
| | | |

excluded values (missing, OOC, invalid, suspect)

- < missing
- T out-of-control
- I invalid
- S suspect
- H exceedance
- F stack not operating
- B invalid (PADER)
- U missing data substituted
- -999 missing value
- -988 value could not be calculated



C - 43

Plant Name: NBWD General Average Report Reporting Period: 03/17/2010 to 03/17/2010

Site Name: UNIT3 Data Averaging Type: 6m Time of Report: 03/18/10 13:22 Rolling Average Interval: 1

| | | OPACITY: | 3 |
|----------|-----------|------------|---|
| Date | Time | e (PERCENT |) |
| 03/17/10 | 06:48 | 1 | 0 |
| | 06:54 | ł | 0 |
| | 07:00 |) | 1 |
| | 07:06 | 5 | 1 |
| | 07:12 | 8 | 2 |
| | 07:18 | 1 | 2 |
| | 07:24 | | 1 |
| | 07:30 |) | 1 |
| | 07:36 | ; | 1 |
| | 07:42 | 2 | 1 |
| | 07:46 | 3 | 1 |
| | 07:54 | 6 | 1 |
| | 08:00 |) | 1 |
| | 08:06 | 5 | 1 |
| | 08:12 | 2 | 2 |
| | 08:18 | 1 | 2 |
| | 08:24 | 1 | 2 |
| | 08:30 |) | 2 |
| | 08:36 | 5 | 2 |
| | 08:42 | 2 | 2 |
| | 08:48 | 1 | 1 |
| | 08:54 | ł | 1 |
| | 09:00 |) | 2 |
| | | | |
| L L | Average = | • | 1 |
| Gøometri | ic Avg. = | • | 1 |
| 3 | faximum = | | 2 |
| 3 | (inimum = | | 0 |
| Possible | | - | 3 |
| Included | Values = | . 1 | 3 |
| | Total = | . 2 | 9 |

excluded values (missing, OOC, invalid, suspect)

< - missing

T - out-of-control

I - invalid

S - suspect

H - exceedance

F - stack not operating

B - invalid (PADER)

U - missing data substituted

-999 - missing value

Page: 1

Plant Name: NBWD General Average Report Reporting Period: 03/17/2010 to 03/17/2010

| Site | Name : | UNIT | :3 |
|------|--------|------|-------|
| Data | Averaç | ging | Type: |

6m

OPACITY3

Time of Report: 03/18/10 13:23 Rolling Average Interval: 1

| | | OFACILLD | |
|-----------|--------|----------|---|
| Date | Time | (PERCENT | |
| 03/17/10 | 09:24 | : | 2 |
| | 09:30 | : | 2 |
| | 09:36 | : | 2 |
| | 09:42 | : | 2 |
| | 09:48 | : | 1 |
| | 09:54 | : | 1 |
| | 10:00 | 1 | 0 |
| | 10:06 | | |
| | 10:12 | | D |
| | 10:18 | 1 | D |
| | 10:24 | | |
| | 10:30 | : | L |
| | 10:36 | : | 1 |
| | 10:42 | : | 1 |
| | 10:48 | : | L |
| | 10:54 | : | L |
| | 11:00 | | D |
| | 11:06 | | D |
| | 11:12 | | 0 |
| | 11:18 | | D |
| | 11:24 | : | 1 |
| | 11:30 | : | 1 |
| | 11:36 | | 1 |
| | | | |
| Ave | rage = | : | 1 |
| Geometric | | : | 1 |
| | imum = | : | 2 |
| | imum = | | |
| | | | |

| Minimum | = | 0 |
|-----------------|---|----|
| Possible Values | - | 23 |
| Included Values | = | 23 |
| Total | - | 18 |
| | | |

excluded values (missing, OOC, invalid, suspect)

- < missing
- T out-of-control
- I invalid
- s suspect
- H exceedance
- F stack not operating
- B invalid (PADER)
- U missing data substituted
- -999 missing value
- -888 value could not be calculated



Plant Name: NBWD General Average Report Reporting Period: 03/17/2010 to 03/17/2010

Site Name: UNIT3 Data Averaging Type: 6m Time of Report: 03/18/10 13:23 Rolling Average Interval: 1

1

| | | OPACITY3 | |
|-------------|---------|------------|--|
| Date | Tine | (PERCENT) | |
| 03/17/10 | 11:54 | 3 | |
| | 12:00 | 3 | |
| | 12:06 | 3 | |
| | 12:12 | 3 | |
| | 12:18 | 3 | |
| | 12:24 | 3 | |
| | 12:30 | 3 | |
| | 12:36 | 4 | |
| | 12:42 | 4 | |
| | 12:48 | 4 | |
| | 12:54 | 4 | |
| | 13:00 | 4 | |
| | 13:06 | 4 | |
| | 13:12 | 4 | |
| | 13:18 | 4 | |
| | 13:24 | 4 | |
| | 13:30 | 4 | |
| | 13:36 | 4 | |
| | 13:42 | 3 | |
| | 13:48 | 4 | |
| | 13:54 | 4 | |
| | 14:00 | 3 | |
| | 14:06 | 3 | |
| | | | |
| | erage = | 3 | |
| Geometric | Avg. = | 3 | |
| Mas | cimum = | 4 | |
| , Mir | 1mum = | 3 | |
| Possible Va | lues = | 23 | |
| Included Va | lues = | 23 | |
| | | | |

excluded values (missing, OOC, invalid, suspect)

80

< - missing

T - out-of-control

- I invalid
- S suspect
- H exceedance
- F stack not operating

Total =

- B invalid (PADER)
- U missing data substituted
- -999 missing value
- -888 value could not be calculated

WHEELABRATOR NORTH BROWARD, INC. POMPANO BEACH, FL

CleanAir Project No: 10955-2

| PARAMETERS | | | |
|------------|--|--|---|
| | | | |
| | | | |
| | | | |
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USEPA Method 5/29 (Particulate/Metals) Sampling, Velocity and Moisture Parameters

| Run No | | 1 | 2 | 3 | Average |
|--------------------|--|------------|------------|------------|------------|
| Date (20 | 010) | Mar 16 | Mar 16 | Mar 16 | |
| Start Tin | ne (approx.) | 07:21 | 10:00 | 12:36 | |
| Stop Tin | ne (approx.) | 09:32 | 12:14 | 14:47 | |
| Samplin | g Conditions | | | | |
| Yd | Dry gas meter correction factor | 0.9900 | 0.9900 | 0.9900 | |
| C, | Pitot tube coefficient | 0.8050 | 0.8050 | 0.8050 | |
| P, | Static pressure (in. H ₂ O) | -10.0000 | -10.0000 | -10.1000 | |
| Å | Sample location area (ft ²) | 64.0000 | 64.0000 | 64.0000 | |
| Pbar | Barometric pressure (in. Hg) | 30.05 | 30.05 | 30.05 | 30.0500 |
| Dn | Nozzle diameter (in.) | 0.2700 | 0.2700 | 0.2700 | |
| O ₂ | Oxygen (dry volume %) | 9.5300 | 9.4600 | 9.7400 | 9.5767 |
| CO ₂ | Carbon dioxide (dry volume %) | 9.8800 | 9.9300 | 9.8300 | 9.8800 |
| N ₂ +CC | Nitrogen plus carbon monoxide (dry volume %) | 80.5900 | 80.6100 | 80.4300 | 80.5433 |
| VIc | Total Liquid collected (ml) | 431.50 | 432.20 | 425.00 | |
| Vm | Volume metered, meter conditions (ft ³) | 80.2420 | 81.5000 | 82.9000 | |
| Tm | Dry gas meter temperature (°F) | 64.3800 | 68.7000 | 75.1800 | |
| T, | Sample temperature (°F) | 293.2800 | 295.0400 | 300.8000 | 296.3733 |
| ΔH | Meter box orifice pressure drop (in. H ₂ O) | 1.2680 | 1.3032 | 1.3268 | |
| θ | Total sampling time (min) | 125.0 | 125.0 | 125.0 | |
| Flow Re | sults | | | | |
| V _{wstd} | Volume of water collected (fl ³) | 20.3064 | 20.3393 | 20.0005 | 20.2154 |
| V _{mstd} | Volume metered, standard (dscf) | 80.5525 | 81.1539 | 81.5531 | 81.0865 |
| P. | Sample gas pressure, absolute (in. Hg) | 29.3147 | 29.3147 | 29.3074 | 29.3123 |
| Pv | Vapor pressure, actual (in. Hg) | 29.3147 | 29.3147 | 29.3074 | 29.3123 |
| Bwo | Moisture measured in sample (% by volume) | 20.1335 | 20.0401 | 19.6945 | 19.9560 |
| B _{wa} | Saturated moisture content (% by volume) | 100.0000 | 100.0000 | 100.0000 | 100.0000 |
| Bw | Actual water vapor in gas (% by volume) | 20.1335 | 20.0401 | 19.6945 | 19.9560 |
| V∆P | Velocity head (√in. H₂O) | 0.7507 | 0.7494 | 0.7563 | 0.7521 |
| Mď | MW of sample gas, dry (lb/lb-mole) | 29.9620 | 29.9672 | 29.9624 | 29.9639 |
| Ms | MW of sample gas, wet (lb/lb-mole) | 27.5536 | 27.5690 | 27.6065 | 27.5764 |
| Vs | Velocity of sample (ft/sec) | 49.8922 | 49.8492 | 50.4724 | 50.0712 |
| %1 | Isokinetic sampling (%) | 98.7688 | 99.7081 | 99.3122 | 99.2630 |
| Qa | Volumetric flow rate, actual (acfm) | 191,586 | 191,421 | 193,814 | 192,274 |
| Q, | Volumetric flow rate, standard (scfm) | 131,572 | 131,153 | 131,754 | 131,493 |
| Q _{std} | Volumetric flow rate, dry standard (dscfm) | 105,082 | 104,870 | 105,806 | 105,252 |
| Q _{std7} | Volumetric flow rate, dry std@7%O ₂ (dscfm) | 85,956 | 86,310 | 84,949 | 85,738 |
| Q, | Volumetric flow rate, actual (acf/hr) | 11,495,154 | 11,485,251 | 11,628,832 | 11,536,412 |
| Q, | Volumetric flow rate, standard (scf/hr) | 7,894,347 | 7,869,160 | 7,905,230 | 7,889,579 |
| Q _{atd} | Volumetric flow rate, dry standard (dscf/hr) | 6,304,942 | 6,292,173 | 6,348,333 | 6,315,149 |
| Q | Volumetric flow rate, actual (m ³ /hr) | 325,550 | 325,269 | 329,335 | 326,718 |
| Q, | Volumetric flow rate, standard (m ³ /hr) | 223,573 | 222,859 | 223,881 | 223,438 |
| Q _{std} | Volumetric flow rate, dry standard (dry m ³ /hr) | 178,560 | 178,198 | 179,789 | 178,849 |
| Q _{std7} | Volumetric flow rate, dry std@7%O ₂ (dry m ³ /hr) | 146,059 | 146,661 | 144,348 | 145,689 |
| Q, | Volumetric flow rate, normal (Nm ³ /hr) | 208,329 | 207,664 | 208,616 | 208,203 |
| Q _{std} | Volumetric flow rate, dry normal (Nm ³ /hr) | 166,385 | 166,048 | 167,530 | 166,655 |
| Q _{std7} | Volumetric flow rate, dry normal @7%O ₂ (Nm ³ /hr) | 136,101 | 136,661 | 134,506 | 135,756 |

Comments:

Average includes 3 runs.

Prepared by Clean Air Engineering Proprietary Software SS ISOKINETIC Version 2008-13d

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QA/QC

041310 090118 JMC @

Date _____

USEPA Method 5/29 **Filterable Particulate Parameters**

| Run No | | 1 | 2 | 3 | Average |
|---------------------------------------|--|--------------------|----------------------|--------------------|---------------------------|
| Date (20 |)10) | Mar 16 | Mar 16 | Mar 16 | |
| • | ne (approx.) | 07:21 | 10:00 | 12:36 | |
| | ne (approx.) | 09:32 | 12:14 | 14:47 | |
| - | s Conditions | | | | |
| Rp | Steam Production Rate (Klbs/hour) | 183.9 | 184.4 | 183.4 | 183.9 |
| Pí | Fabric Filter Inlet Temperature (°F) | 310 | 313 | 320 | 314 |
| Fa | Oxygen-based F-factor (dscf/MMBtu) | 9,570 | 9,570 | 9,570 | 9,570 |
| F, | Carbon dioxide-based F-factor (dscf/MMBtu) | 1,820 | 1,820 | 1,820 | 1,820 |
| Сар | Capacity factor (hours/year) | 8,760 | 8,760 | 8,760 | 8,760 |
| | | , . | | | |
| | nditions Oxygen (dry volume %) | 9.5300 | 9.4600 | 9.7400 | 9.5767 |
| O2 CO2 | Carbon dioxide (dry volume %) | 9.8800 | 9.9300 | 9.8300 | 9.8800 |
| T _s | Sample temperature (°F) | 293.2800 | 295.0400 | 300.8000 | 296.3733 |
| B _w | Actual water vapor in gas (% by volume) | 20.1335 | 20.0401 | 19.6945 | 19.9560 |
| | | 20.1303 | 20.0401 | 19.0040 | 13.5500 |
| Gas Flo | | 404 500 | 104 104 | 400.044 | 402.074 |
| Q, ′ | Volumetric flow rate, actual (acfm) | 191,586 | 191,421 | 193,814 | 192,274 |
| Q₅ | Volumetric flow rate, standard (scfm) | 131,572 | 131,153 | 131,754 | 131,493 |
| Q _{std} | Volumetric flow rate, dry standard (dscfm) | 105,082 | 104,870 | 105,806 | 105,252 |
| Q _{std7} | Volumetric flow rate, dry std@ $7\%O_2$ (dscfm) | 85,956 | 86,310 | 84,949 | 85,738 |
| Q, | Volumetric flow rate, actual (acf/hr) | 11,495,154 | 11,485,251 | 11,628,832 | 11,536,412 |
| Q, | Volumetric flow rate, standard (scf/hr) | 7,894,347 | 7,869,160 | 7,905,230 | 7,889,579 |
| Q _{std} | Volumetric flow rate, dry standard (dscf/hr) | 6,304,942 | 6,292,173 325,269 | 6,348,333 | 6,315,149 |
| Q, | Volumetric flow rate, actual (m ³ /hr) | 325,550 | | 329,335 | 326,718 |
| Q, | Volumetric flow rate, standard (m ³ /hr) | 223,573 | 222,859 | 223,881 | 223,438 |
| Q _{std} | Volumetric flow rate, dry standard (dry m ³ /hr) | 178,560 | 178,198 146,661 | 179,789 | 178,849 145,689 |
| Q _{std7} | Volumetric flow rate, dry std@7%O ₂ (dry m ³ /hr) | 146,059 208,329 | 207,664 | 144,348 208,616 | 208,203 |
| Q, Q. | Volumetric flow rate, normal (Nm ³ /hr) | 166,385 | 166,048 | 167,530 | 166,655 |
| Q _{std} Q _{std7} | Volumetric flow rate, dry normal (Nm ³ /hr) Volumetric flow rate, dry normal @7%O ₂ (Nm ³ /hr) | 136,101 | 136,661 | 134,506 | 135,756 |
| | | 100,101 | 100,001 | 134,000 | 100,700 |
| Samplin | - | 00 5505 | 04 4520 | 04 5504 | 04 0065 |
| V _{mstd} | Volume metered, standard (dscf) | 80.5525 | 81.1539 | 81.5531 | 81.0865 |
| %I | Isokinetic sampling (%) | 98.7688 | 99.7081 | 99.3122 | 99.2630 |
| Laborate | ory Data | | | | |
| m _{filter} | Matter collected on filter(s) (g) | 0.00010 | 0.00010 | 0.00010 | |
| m, | Matter collected in solvent rinse(s) (g) | 0.00049 | 0.00218 | 0.00001 | |
| mn | Total particulate matter collected (g) | 0.00049 | 0.00218 | <0.00020 | |
| Filterabl | e Particulate Results | | | | |
| C_{sd} | Particulate Concentration (lb/dscf) | 1.3509E-08 | 5.9287E-08 | <5.4075E-09 | <2.6068E-08 |
| C _{sd7} | Particulate Concentration @7% O ₂ (lb/dscf) | 1.6516E-08 | 7.2035E-08 | <6.7352E-09 | <3.1762E-08 |
| C _{sd12} | Particulate Concentration @12% CO ₂ (lb/dscf) | 1.6408E-08 | 7.1646E-08 | <6.6012E-09 | <3.1552E-08 |
| Ca | Particulate Concentration (lb/acf) | 7.4098E-09 | 3.2480E-08 | <2.9520E-09 | <1.4281E-08 |
| C _{sd} | Particulate Concentration (gr/dscf) | 0.00009 | 0.00041 | <0.00004 | <0.00018 |
| C _{sd7} | Particulate Concentration @7% O ₂ (gr/dscf) | 0.00012 | 0.00050 | <0.00005 | <0.00022 |
| C _{sd12} | Particulate Concentration @12% CO ₂ (gr/dscf) | 0.00011 | 0.00050 | < 0.00005 | < 0.00022 |
| Ca | Particulate Concentration (gr/acf) | 0.00005 | 0.00023 | <0.00002 | < 0.00010 |
| Csd | Particulate Concentration (mg/dscm) | 0.2163 | 0.9494 | <0.0866 | <0.4174 |
| C _{sd7} | Particulate Concentration @7% O ₂ (mg/dscm) | 0.2645 | 1.1535 | <0.1079 | <0.5086 |
| C _{ad12} | Particulate Concentration @12% CO ₂ (mg/dscm) | 0.2628 | 1.1473 | < 0.1057 | < 0.5053 |
| C, | Particulate Concentration (mg/m ³ (actual,wet)) | 0.1187 | 0.5201 | < 0.0473 | <0.2287 |
| C _{sd} | Particulate Concentration (mg/Nm ³ dry) | 0.2322 | 1.0189 | <0.0929 | <0.4480 |
| C _{ad7} | Particulate Concentration @7% O_2 (mg/Nm ³ dry) | 0.2838 | 1.2380 | <0.1157 | <0.5458 |
| C _{ad12} | Particulate Concentration @12% CO ₂ (mg/Nm ³ dry) | 0.2820 | 1.2313 | <0.1134 | <0.5422 |
| E _{lb/hr} | Particulate Rate (lb/hr) | 0.0852 | 0.3730 | < 0.0343 | <0.1642 |
| E _{kg/hr} | Particulate Rate (kg/hr) | 0.0386 | 0.1692 | < 0.0156 | <0.0745 |
| EThyr | Particulate Rate (Ton/yr) | 0.3731 | 1.6339 | <0.1504 | <0.7191 |
| E _{Fd} | Particulate Rate - F _d -based (lb/MMBtu) | 0.00024 | 0.0010 | <0.00010 | < 0.00046 |
| EFc | Particulate Rate - F _c -based (lb/MMBtu) | 0.00025 | 0.0011 | <0.00010 | <0.00048 |
| Commer | | | | | 041410 124302 JM/C@C_P |
| Averag | je includes 3 runs. | | | | 1 H C W_F |

Prepared by Clean Air Engineering Proprietary Software SS EPA 5-1 Version 2008-08b

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USEPA Method 5/29 Mercury (Hg) Emission Parameters

| Run No | D. | 1 | 2 | 3 | Average |
|-------------------------------------|--|------------|------------|------------------|------------------|
| Date (2 | 010) | Mar 16 | Mar 16 | Mar 16 | |
| | ime (approx.) | 07:21 | 10:00 | 12:36 | |
| Stop Ti | me (approx.) | 09:32 | 12:14 | 14:47 | |
| Proces | s Conditions | | | | |
| RP | Steam Production Rate (Klbs/hour) | 183.9 | 184.4 | 183.4 | 183.9 |
| P1 | Fabric Filter Inlet Temperature (°F) | 310 | 313 | 320 | 314 |
| Fd | Oxygen-based F-factor (dscf/MMBtu) | 9,570 | 9,570 | 9,570 | 9,570 |
| F, | Carbon dioxide-based F-factor (dscf/MMBtu) | 1,820 | 1,820 | 1,820 | 1,820 |
| Cap | Capacity factor (hours/year) | 8,760 | 8,760 | 8,760 | 8,760 |
| Gas Co | anditions | | | | |
| O ₂ | Oxygen (dry volume %) | 9.5300 | 9.4600 | 9,7400 | 9.5767 |
| CO2 | Carbon dioxide (dry volume %) | 9.8800 | 9.9300 | 9.8300 | 9.8800 |
| Тs | Sample temperature (°F) | 293.2800 | 295.0400 | 300.8000 | 296.3733 |
| B _w | Actual water vapor in gas (% by volume) | 20.1335 | 20.0401 | 19.6945 | 19.9560 |
| Gas Flo | ow Rate | | | | |
| Qa | Volumetric flow rate, actual (acfm) | 191,586 | 191,421 | 193,814 | 1 92 ,274 |
| Q, | Volumetric flow rate, standard (scfm) | 131,572 | 131,153 | 131,754 | 131,493 |
| Q _{std} | Volumetric flow rate, dry standard (dscfm) | 105,082 | 104,870 | 105,806 | 105,252 |
| Q _{std7} | Volumetric flow rate, dry std@7%O2 (dscfm) | 85,956 | 86,310 | 84,949 | 85,738 |
| Q, | Volumetric flow rate, actual (acf/hr) | 11,495,154 | 11,485,251 | 11,628,832 | 11,536,412 |
| Q, | Volumetric flow rate, standard (scf/hr) | 7,894,347 | 7,869,160 | 7,905,230 | 7,889,579 |
| Q _{std} | Volumetric flow rate, dry standard (dscf/hr) | 6,304,942 | 6,292,173 | 6,348,333 | 6,315,149 |
| Qa | Volumetric flow rate, actual (m ³ /hr) | 325,550 | 325,269 | 329,335 | 326,718 |
| Q, | Volumetric flow rate, standard (m ³ /hr) | 223,573 | 222,859 | 223,881 | 223,438 |
| Q _{std} | Volumetric flow rate, dry standard (dry m ³ /hr) | 178,560 | 178,198 | 179, 78 9 | 178,849 |
| Q _{std7} | Volumetric flow rate, dry std@7%O2 (dry m3/hr) | 146,059 | 146,661 | 144,348 | 145,689 |
| Q, | Volumetric flow rate, normal (Nm ³ /hr) | 208,329 | 207,664 | 208,616 | 208,203 |
| Q _{std} | Volumetric flow rate, dry normal (Nm ³ /hr) | 166,385 | 166,048 | 167,530 | 166,655 |
| Q _{std7} | Volumetric flow rate, dry normal @7%O ₂ (Nm ³ /hr) | 136,101 | 136,661 | 134,506 | 135,7 56 |
| Samplir | - | | | | |
| V _{mstd} | Volume metered, standard (dscf) | 80.5525 | 81.1539 | 81.5531 | 81.0865 |
| %! | Isokinetic sampling (%) | 98.7688 | 99.7081 | 99.3122 | 99.2630 |
| Laborat | ory Data | | | | |
| m _{n-1b} | Fraction 1B (µg) | <0.1000 | <0.1000 | <0.1000 | |
| m _{n-2b} | Fraction 2B (µg) | 7.7629 | 8.8151 | 9.7549 | |
| m _{n-3a} | Fraction 3A (µg) | <0.2000 | <0.2000 | <0.2000 | |
| m _{n-3b} | Fraction 3B (µg) | < 0.5000 | <0.5000 | <0.5000 | |
| m _{n-3c} | Fraction 3C (µg) | <0.4000 | <0.4000 | <0.4000 | |
| m'n | Total matter corrected for allowable blanks (µg) | 7.7629 | 8.8151 | 9.7549 | |
| | Results - Total | | | | |
| C _{sd} | Concentration (Ib/dscf) | 2.1250E-10 | 2.3951E-10 | 2.6375E-10 | 2.3859E-10 |
| C _{sd7} | Concentration @7% O ₂ (lb/dscf) | 2.5978E-10 | 2.9101E-10 | 3.2850E-10 | 2.9310E-10 |
| C _{sd12} | Concentration @12% CO ₂ (lb/dscf) | 2.5810E-10 | 2.8944E-10 | 3.2197E-10 | 2.8984E-10 |
| Ca | Concentration (Ib/acf) | 1.1655E-10 | 1.3122E-10 | 1.4398E-10 | 1.3058E-10 |
| C _{sd} | Concentration (µg/dscm) | 3.4029E+00 | 3.8354E+00 | 4.2236E+00 | 3.8206E+00 |
| C _{sd7} | Concentration @7% O ₂ (µg/dscm) | 4.1601E+00 | 4.6602E+00 | 5.2605E+00 | 4.6936E+00 |
| C _{sd12} | Concentration @12% CO ₂ (µg/dscm) | 4.1330E+00 | 4.6350E+00 | 5.1559E+00 | 4.6413E+00 |
| C _{sd} | Concentration (mg/dscm) | 3.4029E-03 | 3.8354E-03 | 4.2236E-03 | 3.8206E-03 |
| C _{sd7} | Concentration @7% O2 (mg/dscm) | 4.1601E-03 | 4.6602E-03 | 5.2605E-03 | 4.6936E-03 |
| C _{sd12} | Concentration @12% CO ₂ (mg/dscm) | 4.1330E-03 | 4.6350E-03 | 5.1559E-03 | 4.6413E-03 |
| Ca | Concentration (µg/m ³ (actual,wet)) | 1.8664E+00 | 2.1012E+00 | 2.3057E+00 | 2.0911E+00 |
| Csd | Concentration (µg/Nm ³ dry) | 3.6519E+00 | 4.1161E+00 | 4.5326E+00 | 4.1002E+00 |
| C _{sd7} | Concentration @7% O ₂ (µg/Nm ³ dry) | 4.4644E+00 | 5.0012E+00 | 5.6454E+00 | 5.0370E+00 |
| C _{sd12} | Concentration @12% CO ₂ (µg/Nm ³ dry) | 4.4354E+00 | 4.9741E+00 | 5.5332E+00 | 4.9809E+00 |
| Elp/hr | Rate (lb/hr) | 1.3398E-03 | 1.5070E-03 | 1.6744E-03 | 1.5071E-03 |
| E _{g/s} | Rate (g/s) | 1.6878E-04 | 1.8985E-04 | 2.1093E-04 | 1.8985E-04 |
| E _{T/yr} | Rate (Ton/yr) | 5.8683E-03 | 6.6009E-03 | 7.3337E-03 | 6.6009E-03 |
| EFd | Rate - Fd-based (lb/MMBtu) | 3.7381E-06 | 4.1875E-06 | 4.7270E-06 | 4.2175E-06 |
| E _{F c} Prepared by Cle | Rate - Fc-based (Ib/MMBtu) an Ar Engineering Proprietary Software | 3.9144E-06 | 4.3898E-06 | 4.8832E-06 | 4.3958E-06 |
| 55 Metals-1 Ver | | | | | |
| | | | | | |

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USEPA Method 5/29 Beryllium (Be) Emission Parameters

| Run No. | | 1 | 2 | 3 | Average |
|-------------------|--|-------------|-------------|----------------------------|-------------|
| Date (20 | 10) | Mar 16 | Mar 16 | Mar 16 | |
| - | ne (approx.) | 07:21 | 10:00 | 12:36 | |
| | e (approx.) | 09:32 | 12:14 | 14:47 | |
| | • • • • | | | | |
| | Conditions | 192.0 | 104.4 | 192.4 | 402.0 |
| R _P | Steam Production Rate (Klbs/hour) | 183.9 | 184.4 | 183.4 | 183.9 |
| P ₁ | Fabric Filter Inlet Temperature (°F) | 310 | 313 | 320 | 314 |
| F₄ | Oxygen-based F-factor (dscf/MMBtu) | 9,570 | 9,570 | 9,570 | 9,570 |
| F. | Carbon dioxide-based F-factor (dscf/MMBtu) | 1,820 | 1,820 | 1,820 | 1,820 |
| Сар | Capacity factor (hours/year) | 8.760 | 8,760 | 8,760 | 8,760 |
| Gas Cor | nditions | | | | |
| Oz | Oxygen (dry volume %) | 9.5300 | 9.4600 | 9,7400 | 9.5767 |
| CO ₂ | Carbon dioxide (dry volume %) | 9.8800 | 9.9300 | 9.8300 | 9.8800 |
| Τs | Sample temperature (°F) | 293.2800 | 295.0400 | 300.8000 | 296.3733 |
| B, | Actual water vapor in gas (% by volume) | 20.1335 | 20.0401 | 19.6945 | 19.9560 |
| Gas Flov | w Pate | | | | |
| Q, | Volumetric flow rate, actual (acfm) | 191,586 | 191,421 | 193,814 | 192,274 |
| Q, | Volumetric flow rate, standard (scfm) | 131,572 | 131,153 | 131,754 | 131,493 |
| Q _{sto} | Volumetric flow rate, dry standard (dscfm) | 105,082 | 104.870 | 105,806 | 105,252 |
| Q _{std7} | Volumetric flow rate, dry std@7%O ₂ (dscfm) | 85,956 | 86,310 | 84,949 | 85,738 |
| Q _a | Volumetric flow rate, actual (acf/hr) | 11,495,154 | 11,485,251 | 11,628,832 | 11,536,412 |
| Q, | Volumetric flow rate, standard (scf/hr) | 7,894,347 | 7,869,160 | 7,905,230 | 7,889,579 |
| Q _{std} | Volumetric flow rate, dry standard (dscf/hr) | 6,304,942 | 6,292,173 | 6,348,333 | 6,315,149 |
| Qa | Volumetric flow rate, actual (m ³ /hr) | 325,550 | 325,269 | 329,335 | 326,718 |
| Q, | Volumetric flow rate, standard (m ³ /hr) | 223,573 | 222,859 | 223,881 | 223,438 |
| - | , , , | 178,560 | 178,198 | 179,789 | 178,849 |
| Q _{std} | Volumetric flow rate, dry standard (dry m³/hr) Volumetric flow rate, dry std@7%O₂ (dry m³/hr) | 146,059 | 146,661 | 144,348 | 145,689 |
| Q _{std7} | | 208,329 | 207,664 | 208,616 | 208,203 |
| Q, | Volumetric flow rate, normal (Nm ³ /hr) | 166,385 | 166,048 | 167,530 | 166,655 |
| Q _{std} | Volumetric flow rate, dry normal (Nm ³ /hr) | 136,101 | 136,661 | 134,506 | 135,756 |
| Q _{std7} | Volumetric flow rate, dry normal @7%O ₂ (Nm ³ /hr) | 100,107 | 150,007 | 734,000 | 100,700 |
| Samplin | g Data | | | | |
| V _{mstd} | Volume metered, standard (dscf) | 80.5525 | 81.1539 | 81.5531 | 81.0865 |
| %! | IsokInetic sampling (%) | 98.7688 | 99.7081 | 99.3122 | 99.2630 |
| Laborato | ory Data | | | | |
| m | Total matter corrected for allowable blanks (µg) | <0.0500 | < 0.0500 | < 0.0500 | |
| | - Results Total | | | | |
| | m Results - Total | <1.3687E-12 | <1.3585E-12 | <1.3519E-12 | <1.3597E-12 |
| C _{sd} | Concentration (lb/dscf) Concentration @7% O_2 (lb/dscf) | <1.6732E-12 | <1.6507E-12 | <1.6838E-12 | |
| C _{sd7} | | <1.6624E-12 | | <1.6503E-12 | <1.6515E-12 |
| C _{ad12} | Concentration @12% CO ₂ (lb/dscf) Concentration (lb/acf) | <7.5070E-13 | | <7.3801E-13 | |
| C, | Concentration (µg/dscm) | <2.1917E-02 | <2.1755E-02 | <2.1648E-02 | |
| C _{sd} | Concentration @7% O ₂ (µg/dscm) | <2.6794E-02 | <2.6433E-02 | <2.6964E-02 | <2.6730E-02 |
| C _{sd7} | Concentration @12% CO ₂ (µg/dscm) | <2.6620E-02 | <2.6455E-02 | <2.6427E-02 | <2.6446E-02 |
| C _{sd12} | | <2.1917E-05 | <2.0250E-02 | <2.1648E-05 | <2.1774E-05 |
| C _{sd} | Concentration (mg/dscm) | <2.6794E-05 | <2.6433E-05 | <2.6964E-05 | <2.6730E-05 |
| C _{sd7} | Concentration @7% O ₂ (mg/dscm) Concentration @12% CO ₂ (mg/dscm) | <2.6620E-05 | | <2.6427E-05 | <2.6446E-05 |
| C _{sd12} | | | <2.6290E-05 | | |
| C _a | Concentration (µg/m ³ (actual,wet)) | <1.2021E-02 | <1.1918E-02 | <1.1818E-02 | <1.1919E-02 |
| C _{sd} | Concentration (μ g/Nm ³ dry) | <2.3521E-02 | <2.3347E-02 | <2.3233E-02 <2.8937E-02 | <2.3367E-02 |
| C _{sd7} | Concentration @7% O_2 (µg/Nm ³ dry) | <2.8755E-02 | <2.8367E-02 | | <2.8686E-02 |
| C _{sd12} | Concentration @12% CO ₂ (µg/Nm ³ dry) | <2.8568E-02 | <2.8214E-02 | <2.8361E-02 | <2.8381E-02 |
| Elb/hr | Rate (lb/hr) | <8.6294E-06 | <8.5481E-06 | <8.5822E-06 | <8.5866E-06 |
| E _{g/s} | Rate (g/s) | <1.0871E-06 | <1.0769E-06 | <1.0812E-06 | <1.0817E-06 |
| Ettyr | Rate (Ton/yr) | <3.7797E-05 | <3.7441E-05 | <3.7590E-05 | <3.7609E-05 |
| Efd | Rate - Fd-based (Ib/MMBtu) | <2.4077E-08 | <2.3752E-08 | <2.4229E-08 | <2.4019E-08 |
| E _{Fe} | Rate - Fc-based (lb/MMBtu) | <2.5212E-08 | <2.4900E-08 | <2.5030E-08 | <2.5047E-08 |

041410 124302 JMO@_M

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USEPA Method 5/29 Cadmium (Cd) Emission Parameters

e.

| Run N | 0. | 1 | 2 | 3 | Average |
|---|--|--|--|--|---|
| Date (2 | 2010) | Mar 16 | Mar 16 | Mar 16 | i |
| Start Ti | ime (approx.) | 07:21 | 10:00 | 12:36 | i |
| Stop TI | me (approx.) | 09:32 | 12:14 | 14:47 | |
| Proces | s Conditions | | | | |
| RP | Steam Production Rate (Klbs/hour) | 183.9 | 184.4 | 183.4 | 183.9 |
| P ₁ | Fabric Filter Inlet Temperature (°F) | 310 | 313 | 320 | 314 |
| Fa | Oxygen-based F-factor (dscf/MMBtu) | 9,570 | 9,570 | 9,570 | 9,570 |
| F. | Carbon dioxide-based F-factor (dscf/MMBtu) | 1,820 | 1,820 | 1,820 | 1,820 |
| Сар | Capacity factor (hours/year) | 8,760 | 8,760 | 8,760 | |
| Gas Co | onditions | | | | |
| O2 | Oxygen (dry volume %) | 9.5300 | 9.4600 | 9.7400 | 9.5767 |
| CO₂ | Carbon dioxide (dry volume %) | 9.8800 | 9.9300 | 9.8300 | 9.8800 |
| Т | Sample temperature (°F) | 293.2800 | 295.0400 | 300.8000 | 296.3733 |
| B _w | Actual water vapor in gas (% by volume) | 20.1335 | 20.0401 | 19.6945 | 19.9560 |
| Gas Flo | ow Rate | | | | |
| Q, | Volumetric flow rate, actual (acfm) | 191,586 | 191,421 | 193,814 | 192,274 |
| Q, | Volumetric flow rate, standard (scfm) | 131,572 | 131,153 | 131,754 | 131,493 |
| Q _{std} | Volumetric flow rate, dry standard (dscfm) | 105,082 | 104,870 | 105,806 | 105,252 |
| Q _{std7} | Volumetric flow rate, dry std@7%O ₂ (dscfm) | 85,956 | 86,310 | 84,949 | 85,738 |
| Q _a | Volumetric flow rate, actual (acf/hr) | 11,495,154 | 11,485,251 | 11,628,832 | 11,536,412 |
| Q, | Volumetric flow rate, standard (scf/hr) | 7,894,347 | 7,869,160 | 7,905,230 | 7,889,579 |
| Q _{std} | Volumetric flow rate, dry standard (dscf/hr) | 6,304,942 | 6,292,173 | 6,348,333 | 6,315,149 |
| Q _a | Volumetric flow rate, actual (m ³ /hr) | 325,550 | 325,269 | 329,335 | 326,718 |
| Q _s | Volumetric flow rate, actual (m /m) Volumetric flow rate, standard (m ³ /hr) | 223,573 | 222,859 | 223,881 | 223,438 |
| - | | 178,560 | 178,198 | 179,789 | 223,438 178,849 |
| Q _{std} | Volumetric flow rate, dry standard (dry m ³ /hr) | | | | |
| Q _{std7} Qa | Volumetric flow rate, dry std@7% O_2 (dry m ³ /hr) | 146,059 | 146,661 207,664 | 144,348 | 145,689 |
| | Volumetric flow rate, normal (Nm ³ /hr) | 208,329 | | 208,616 | 208,203 |
| Q _{std} Q _{std7} | Volumetric flow rate, dry normal (Nm ³ /hr) Volumetric flow rate, dry normal @7%O ₂ (Nm ³ /hr) | 166,385 136,101 | 166,048 136,661 | 167,530 134,506 | 166,655 135,756 |
| | , | 100,101 | 100,001 | 104,000 | 100,700 |
| - | ng Data | 00 5505 | 04 4520 | 04 6534 | 01 0005 |
| V _{mstd} | Volume metered, standard (dscf) | 80.5525 | 81.1539 | 81.5531 | 81.0865 |
| % | Isokinetic sampling (%) | 98.7688 | 99.7081 | 99.3122 | 99.2630 |
| | ory Data | | | | |
| m'n | Total matter corrected for allowable blanks (µg) | <0.2000 | 0.2093 | <0.2000 | |
| | m Results - Total | | | | |
| C _{sd} | Concentration (lb/dscf) | <5.4747E-12 | 5.6863E-12 | <5.4075E-12 | <5.5228E-12 |
| C _{ad7} | Concentration @7% O_2 (lb/dscf) | <6.6929E-12 | 6.9090E-12 | <6.7352E-12 | <6.7790E-12 |
| C _{sd12} | Concentration @12% CO ₂ (lb/dscf) | <6.6494E-12 | 6.8717E-12 | <6.6012E-12 | <6.7074E-12 |
| Ca | Concentration (lb/acf) | <3.0028E-12 | 3.1152E-12 | <2.9520E-12 | <3.0234E-12 |
| Csd | Concentration (µg/dscm) | <8.7669E-02 | 9.1058E-02 | <8.6594E-02 | <8.8440E-02 |
| C _{sd7} | Concentration @7% O ₂ (µg/dscm) | <1.0718E-01 | 1.1064E-01 | <1.0785E-01 | <1.0856E-01 |
| C _{sd12} | Concentration @12% CO ₂ (µg/dscm) | <1.0648E-01 | 1.1004E-01 | <1.0571E-01 | <1.0741E-01 |
| C _{sd} | Concentration (mg/dscm) | <8.7669E-05 | 9.1058E-05 | <8.6594E-05 | <8.8440E-05 |
| C _{sd7} | Concentration @7% O ₂ (mg/dscm) | <1.0718E-04 | 1.1064E-04 | <1.0785E-04 | <1.0856E-04 |
| | | <1.0648E-04 | 1.1004E-04 | <1.0571E-04 | <1.0741E-04 |
| Csd12 | Concentration @12% CO ₂ (mg/dscm) | <1.0040E-04 | 1.10046-04 | | |
| | Concentration @12% CO ₂ (mg/dscm) Concentration (µg/m ³ (actual,wet)) | <4.8086E-02 | 4.9886E-02 | <4.7273E-02 | <4.8415E-02 |
| C _{sd12} | | | | | <4.8415E-02 <9.4912E-02 |
| C _{sd12} C _a C _{sd} | Concentration (µg/m ³ (actual,wet)) | <4.8086E-02 | 4.9886E-02 9.7721E-02 | <4.7273E-02 | |
| C _{sd12} C _a C _{sd} C _{sd7} | Concentration (µg/m ³ (actual,wet)) Concentration (µg/Nm ³ dry) | <4.8086E-02 <9.4084E-02 | 4.9886E-02 | <4.7273E-02 <9.2930E-02 | <9.4912E-02 |
| C _{sd12} C _a C _{sd} C _{sd7} C _{sd12} | Concentration (μ g/m ³ (actual,wet)) Concentration (μ g/Nm ³ dry) Concentration @7% O ₂ (μ g/Nm ³ dry) Concentration @12% CO ₂ (μ g/Nm ³ dry) | <4.8086E-02 <9.4084E-02 <1.1502E-01 | 4.9886E-02 9.7721E-02 1.1873E-01 1.1809E-01 | <4.7273E-02 <9.2930E-02 <1.1575E-01 <1.1344E-01 | <9.4912E-02 <1.1650E-01 <1.1527E-01 |
| C _{sd12} C _a C _{sd} C _{sd7} C _{sd12} E _{lb/hr} | Concentration (μ g/m ³ (actual,wet)) Concentration (μ g/Nm ³ dry) Concentration @7% O ₂ (μ g/Nm ³ dry) Concentration @12% CO ₂ (μ g/Nm ³ dry) Rate (lb/hr) | <4.8086E-02 <9.4084E-02 <1.1502E-01 <1.1427E-01 <3.4518E-05 | 4.9886E-02 9.7721E-02 1.1873E-01 1.1809E-01 3.5779E-05 | <4.7273E-02 <9.2930E-02 <1.1575E-01 | <9.4912E-02 <1.1650E-01 <1.1527E-01 <3.4875E-05 |
| C _{sd12} C _a C _{sd} C _{sd7} C _{sd12} E _{lb/hr} E _{g/s} | Concentration (μ g/m ³ (actual,wet)) Concentration (μ g/Nm ³ dry) Concentration @7% O ₂ (μ g/Nm ³ dry) Concentration @12% CO ₂ (μ g/Nm ³ dry) Rate (lb/hr) Rate (g/s) | <4.8086E-02 <9.4084E-02 <1.1502E-01 <1.1427E-01 <3.4518E-05 <4.3484E-06 | 4.9886E-02 9.7721E-02 1.1873E-01 1.1809E-01 3.5779E-05 4.5073E-06 | <4.7273E-02 <9.2930E-02 <1.1575E-01 <1.1344E-01 <3.4329E-05 <4.3246E-06 | <9.4912E-02 <1.1650E-01 <1.1527E-01 <3.4875E-05 <4.3934E-06 |
| C _{sd12} C _a C _{sd} C _{sd7} C _{sd12} E _{lb/hr} | Concentration (μ g/m ³ (actual,wet)) Concentration (μ g/Nm ³ dry) Concentration @7% O ₂ (μ g/Nm ³ dry) Concentration @12% CO ₂ (μ g/Nm ³ dry) Rate (lb/hr) | <4.8086E-02 <9.4084E-02 <1.1502E-01 <1.1427E-01 <3.4518E-05 | 4.9886E-02 9.7721E-02 1.1873E-01 1.1809E-01 3.5779E-05 | <4.7273E-02 <9.2930E-02 <1.1575E-01 <1.1344E-01 <3.4329E-05 | <9.4912E-02 <1.1650E-01 <1.1527E-01 <3.4875E-05 |

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USEPA Method 5/29 Lead (Pb) Emission Parameters

| Run No. | | 1 | 2 | 3 | Average |
|----------------------|--|------------|-----------------|------------|------------|
| Date (20 | 10) | Mar 16 | Mar 16 | Mar 16 | |
| • | ne (approx.) | 07:21 | 10:00 | 12:36 | |
| | ne (approx.) | 09:32 | 12:14 | 14:47 | |
| - | | | | | |
| | Conditions Steam Production Rate (Klbs/hour) | 183.9 | 184.4 | 183.4 | 183.9 |
| R _P P1 | Fabric Filter Inlet Temperature (°F) | 310 | 313 | 320 | 314 |
| - | | 9,570 | 9,570 | 9,570 | 9,570 |
| Fa | Oxygan-based F-factor (dscf/MMBtu) Carbon dioxide-based F-factor (dscf/MMBtu) | 1,820 | 1,820 | 1,820 | 1,820 |
| F _e | Capacity factor (hours/year) | 8,760 | 8,760 | 8,760 | 8,760 |
| Сар | Capacity lactor (nours year) | 0,100 | 0,700 | 0,700 | 0,700 |
| Gas Cor | | 0 5300 | 0.4500 | 0 7/00 | 0.5707 |
| O₂ | Oxygen (dry volume %) | 9.5300 | 9.4600 | 9.7400 | 9.5767 |
| CO₂ | Carbon dioxide (dry volume %) | 9.8800 | 9.9300 | 9.8300 | 9.8800 |
| T, | Sample temperature (°F) | 293.2800 | 295.0400 | 300.8000 | 296.3733 |
| B, | Actual water vapor in gas (% by volume) | 20.1335 | 20.0401 | 19.6945 | 19.9560 |
| Gas Flo | w Rate | | | | |
| Q, | Volumetric flow rate, actual (acfm) | 191,586 | 191,421 | 193,814 | 192,274 |
| Q, | Volumetric flow rate, standard (scfm) | 131,572 | 131,153 | 131,754 | 131,493 |
| Q _{std} | Volumetric flow rate, dry standard (dscfm) | 105,082 | 104,870 | 105,806 | 105,252 |
| Q _{std7} | Volumetric flow rate, dry std@7%O ₂ (dscfm) | 85,956 | 86,310 | 84,949 | 85,738 |
| Q, | Volumetric flow rate, actual (acf/hr) | 11,495,154 | 11,485,251 | 11,628,832 | 11,536,412 |
| Q, | Volumetric flow rate, standard (scf/hr) | 7,894,347 | 7,869,160 | 7,905,230 | 7,889,579 |
| Q _{std} | Volumetric flow rate, dry standard (dscf/hr) | 6,304,942 | 6,292,173 | 6,348,333 | 6,315,149 |
| Q, | Volumetric flow rate, actual (m ³ /hr) | 325,550 | 325,269 | 329,335 | 326,718 |
| Q, | Volumetric flow rate, standard (m ³ /hr) | 223,573 | 222,859 | 223,881 | 223,438 |
| Q _{std} | Volumetric flow rate, dry standard (dry m ³ /hr) | 178,560 | 178,19 8 | 179,789 | 178,849 |
| Q _{sto7} | Volumetric flow rate, dry std@7%O2 (dry m3/hr) | 146,059 | 146,66 1 | 144,348 | 145,689 |
| Q, | Volumetric flow rate, normal (Nm ³ /hr) | 208,329 | 207,664 | 208,616 | 208,203 |
| Q _{std} | Volumetric flow rate, dry normal (Nm ³ /hr) | 166,385 | 166,048 | 167,530 | 166,655 |
| Q _{std7} | Volumetric flow rate, dry normal @7%O2 (Nm3/hr) | 136,101 | 136,661 | 134,506 | 135,756 |
| Samplin | n Data | | | | |
| V _{mstd} | Volume metered, standard (dscf) | 80.5525 | 81.1539 | 81.5531 | 81.0865 |
| %1 | Isokinetic sampling (%) | 98.7688 | 99.7081 | 99.3122 | 99.2630 |
| | | | | | |
| | ory Data Total matter corrected for allowable blanks (µg) | 1.0847 | 1.1424 | 1.2738 | |
| m _n | I Dial matter confected for allowable blanks (pg) | 1.0047 | 1.1727 | 1.2750 | |
| | sults - Total | | | | |
| C₅⊲ | Concentration (lb/dscf) | 2.9693E-11 | 3.1040E-11 | 3.4441E-11 | 3.1725E-11 |
| | Concentration @7% O ₂ (lb/dscf) | 3.6300E-11 | 3.7714E-11 | 4.2897E-11 | 3.8971E-11 |
| C _{sd12} | Concentration @12% CO ₂ (lb/dscf) | 3.6064E-11 | 3.7510E-11 | 4.2044E-11 | 3.8540E-11 |
| C, | Concentration (lb/acf) | 1.6286E-11 | 1.7005E-11 | 1.8802E-11 | 1.7364E-11 |
| C _{sd} | Concentration (µg/dscm) | 4.7549E-01 | 4.9706E-01 | 5.5153E-01 | 5.0803E-01 |
| C _{sd7} | Concentration @7% O ₂ (µg/dscm) | 5.8130E-01 | 6.0394E-01 | 6.8694E-01 | 6.2406E-01 |
| C _{sd12} | Concentration @12% CO ₂ (µg/dscm) | 5.7752E-01 | 6.0068E-01 | 6.7328E-01 | 6.1716E-01 |
| Csd | Concentration (mg/dscm) | 4.7549E-04 | 4.9706E-04 | 5.5153E-04 | 5.0803E-04 |
| C _{sd7} | Concentration @7% O ₂ (mg/dscm) | 5.8130E-04 | 6.0394E-04 | 6.8694E-04 | 6.2406E-04 |
| C _{ad12} | Concentration @12% CO ₂ (mg/dscm) | 5.7752E-04 | 6.0068E-04 | 6.7328E-04 | 6.1718E-04 |
| C, | Concentration (µg/m ³ (actual,wet)) | 2.6080E-01 | 2.7231E-01 | 3.0109E-01 | 2.7807E-01 |
| C ^{sd} | Concentration (µg/Nm ³ dry) | 5.1028E-01 | 5.3343E-01 | 5.9189E-01 | 5.4520E-01 |
| C _{sd7} | Concentration @7% O ₂ (µg/Nm ³ dry) | 6.2383E-01 | 6.4814E-01 | 7.3721E-01 | 6.6972E-01 |
| C _{sd12} | Concentration @12% CO ₂ (µg/Nm ³ dry) | 6.1978E-01 | 6.4463E-01 | 7.2255E-01 | 6.6232E-01 |
| Elotv | Rate (lb/hr) | 1.8721E-04 | 1.9531E-04 | 2.1865E-04 | 2.0039E-04 |
| E _{g/s} | Rate (g/s) | 2.3584E-05 | 2.4604E-05 | 2.7544E-05 | 2.5244E-05 |
| ET/yr | Rate (Ton/yr) | 8.1999E-04 | 8.5545E-04 | 9.5767E-04 | 8.7770E-04 |
| E _{Fd} | Rate - Fd-based (lb/MMBtu) | 5.2234E-07 | 5.4269E-07 | 6.1727E-07 | 5.6077E-07 |
| EFe | Rate - Fc-based (lb/MMBtu) | 5.4698E-07 | 5.6891E-07 | 6.3767E-07 | 5.8452E-07 |
| | | | | | |

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USEPA Method 13B (Total Fluorides) Sampling, Velocity and Moisture Parameters

| Run No | | 1 | 2 | 3 | Average |
|-------------------|--|------------|------------|------------|------------|
| Date (20 | 010) | Mar 17 | Mar 17 | Mar 17 | |
| Start Tin | ne (approx.) | 11:46 | 13:15 | 14:45 | |
| Stop Tin | ne (approx.) | 12:56 | 14:27 | 15:53 | |
| Samplin | ig Conditions | | | | |
| Y _d | Dry gas meter correction factor | 0.9900 | 0.9900 | 0.9900 | |
| C, | Pitot tube coefficient | 0.8120 | 0.8120 | 0.8120 | |
| Pg | Static pressure (in. H ₂ O) | -10.3000 | -10.4000 | -10.4000 | |
| A, | Sample location area (ft ²) | 64.0000 | 64.0000 | 64.0000 | |
| Phar | Barometric pressure (in. Hg) | 30.00 | 30.00 | 30.00 | 30.0000 |
| D _n | Nozzle diameter (in.) | 0.2680 | 0.2680 | 0.2680 | • |
| O2 | Oxygen (dry volume %) | 10.5500 | 10.1300 | 9,9600 | 10.2133 |
| CO ₂ | Carbon dioxide (dry volume %) | 9.1100 | 9.6200 | 9.8000 | 9.5100 |
| N₂+CO | Nitrogen plus carbon monoxide (dry volume %) | 80.3400 | 80.2500 | 80.2400 | 80.2767 |
| Vic | Total Liquid collected (ml) | 225.50 | 232.30 | 232.30 | |
| Vm | Volume metered, meter conditions (ft ³) | 42.9350 | 42.9200 | 41.4700 | |
| Tm | Dry gas meter temperature (°F) | 68.2800 | 71.6000 | 69.7000 | |
| T, | Sample temperature (°F) | 302.6000 | 302.0400 | 302.6000 | 302.4133 |
| ΔH | Meter box orifice pressure drop (in. H ₂ O) | 1.4560 | 1.4736 | 1.3528 | |
| θ | Total sampling time (min) | 62.5 | 62.5 | 62.5 | |
| Flow Res | sults | | | | |
| V _{wstd} | Volume of water collected (ft ³) | 10.6120 | 10.9320 | 10.9320 | 10.8254 |
| Vmstd | Volume metered, standard (dscf) | 42.7316 | 42.4517 | 41.1525 | 42.1120 |
| P. | Sample gas pressure, absolute (in. Hg) | 29.2426 | 29.2353 | 29.2353 | 29.2377 |
| Pv | Vapor pressure, actual (in. Hg) | 29.2426 | 29.2353 | 29.2353 | 29.2377 |
| Bwo | Moisture measured in sample (% by volume) | 19.8937 | 20.4782 | 20.9890 | 20.4536 |
| B _{wa} | Saturated moisture content (% by volume) | 100.0000 | 100.0000 | 100.0000 | 100.0000 |
| Bw | Actual water vapor in gas (% by volume) | 19.8937 | 20.4782 | 20.9890 | 20.4536 |
| √∆P | Velocity head (√in. H₂O) | 0.7935 | 0.7993 | 0.7657 | 0.7862 |
| Md | MW of sample gas, dry (lb/lb-mole) | 29.8796 | 29.9444 | 29.9664 | 29.9301 |
| Ma | MW of sample gas, wet (lb/lb-mole) | 27.5163 | 27.4984 | 27.4548 | 27.4898 |
| Vs | Velocity of sample (ft/sec) | 53.6266 | 54.0190 | 51.8104 | 53.1520 |
| %I | Isokinetic sampling (%) | 100.1239 | 99.4233 | 101.2130 | 100.2534 |
| Q, | Volumetric flow rate, actual (acfm) | 205,926 | 207,433 | 198,952 | 204,104 |
| Q, | Volumetric flow rate, standard (scfm) | 139,349 | 140,436 | 134,596 | 138,127 |
| Q _{std} | Volumetric flow rate, dry standard (dscfm) | 111,627 | 111,678 | 106,345 | 109,883 |
| Q _{std7} | Volumetric flow rate, dry std@7%O ₂ (dscfm) | 83,118 | 86,530 | 83,699 | 84,449 |
| Q _a | Volumetric flow rate, actual (acf/hr) | 12,355,565 | 12,445,974 | 11,937,120 | 12,246,220 |
| Qa | Volumetric flow rate, standard (scf/hr) | 8,360,935 | 8,426,184 | 8,075,745 | 8,287,621 |
| Q _{std} | Volumetric flow rate, dry standard (dscf/hr) | 6,697,635 | 6,700,653 | 6,380,726 | 6,593,005 |
| Qa | Volumetric flow rate, actual (m ³ /hr) | 349,917 | 352,477 | 338,066 | 346,820 |
| Q, | Volumetric flow rate, standard (m ³ /hr) | 236,787 | 238,634 | 228,710 | 234,710 |
| Q _{std} | Volumetric flow rate, dry standard (dry m ³ /hr) | 189,681 | 189,766 | 180,706 | 186,718 |
| Q _{std7} | Volumetric flow rate, dry std@7%O ₂ (dry m ³ /hr) | 141,237 | 147,035 | 142,225 | 143,499 |
| Q _s | Volumetric flow rate, normal (Nm ³ /hr) | 220,642 | 222,364 | 213,116 | 218,707 |
| Q _{std} | Volumetric flow rate, dry normal (Nm ³ /hr) | 176,748 | 176,828 | 168,385 | 173,987 |
| Q _{std7} | Volumetric flow rate, dry normal @7%O ₂ (Nm ³ /hr) | 131,607 | 137,010 | 132,528 | 133,715 |
| | | | | | |



Average includes 3 runs.

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QA/QC _____ Date _____

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USEPA Method 13B HF Parameters

| Run No. | | 1 | 2 | 3 | Average |
|-------------------------------------|--|-------------|-------------|-------------|-------------|
| Date (20 | 10) | Mar 17 | Mar 17 | Mar 17 | |
| | ie (approx.) | 11:46 | 13:15 | 14:45 | |
| | ie (approx.) | 12:56 | 14:27 | 15:53 | |
| | | | | | |
| | Conditions | 184.0 | 184.0 | 184.1 | 184.0 |
| R _P | Steam Production Rate (Klbs/hour) | 320 | 320 | 320 | 320 |
| P ₁ | Fabric Filter Inlet Temperature (°F) | 9,570 | 9,570 | 9,570 | 9,570 |
| Fa | Oxygen-based F-factor (dscf/MMBtu) | 1,820 | 1,820 | 1,820 | 1,820 |
| F _c | Carbon dioxide-based F-factor (dscf/MMBtu) Capacity factor (hours/year) | 8,760 | 8,760 | 8,760 | 8,760 |
| Сар | Capacity factor (nours/year) | 0,700 | 0,700 | 0,700 | 0,700 |
| Gas Cor | | | | | |
| Oz | Oxygen (dry volume %) | 10.5500 | 10.1300 | 9.9600 | 10.2133 |
| CO2 | Carbon dioxide (dry volume %) | 9.1100 | 9.6200 | 9.8000 | 9.5100 |
| T, | Sample temperature (°F) | 302.6000 | 302.0400 | 302.6000 | 302.4133 |
| Bw | Actual water vapor in gas (% by volume) | 19.8937 | 20.4782 | 20.9890 | 20.4536 |
| Gas Flor | w Rate | | | | |
| Qa | Volumetric flow rate, actual (acfm) | 205,926 | 207,433 | 198,952 | 204,104 |
| Q, | Volumetric flow rate, standard (scfm) | 139,349 | 140,436 | 134,596 | 138,127 |
| Q _{atd} | Volumetric flow rate, dry standard (dscfm) | 111,627 | 111,678 | 106,345 | 109,883 |
| Q _{std7} | Volumetric flow rate, dry std@7%O 2 (dscfm) | 83,118 | 86,530 | 83,699 | 84,449 |
| Q, | Volumetric flow rate, actual (acf/hr) | 12,355,565 | 12,445,974 | 11,937,120 | 12,246,220 |
| Q, | Volumetric flow rate, standard (scf/hr) | 8,360,935 | 8,426,184 | 8,075,745 | 8,287,621 |
| Q _{etd} | Volumetric flow rate, dry standard (dscf/hr) | 6,697,635 | 6,700,653 | 6,380,726 | 6,593,005 |
| Q, | Volumetric flow rate, actual (m ³ /hr) | 349,917 | 352,477 | 338,066 | 346,820 |
| Q, | Volumetric flow rate, standard (m ³ /hr) | 236,787 | 238,634 | 228,710 | 234,710 |
| Q _{std} | Volumetric flow rate, dry standard (dry m ³ /hr) | 189,681 | 189,766 | 180,706 | 186,718 |
| Q _{std7} | Volumetric flow rate, dry std@7%O 2 (dry m ³ /hr) | 141,237 | 147,035 | 142,225 | 143,499 |
| Q, | Volumetric flow rate, normal (Nm ³ /hr) | 220,642 | 222,364 | 213,116 | 218,707 |
| Q _{std} | Volumetric flow rate, dry normal (Nm 3/hr) | 176,748 | 176,828 | 168,385 | 173,987 |
| Q _{atd7} | Volumetric flow rate, dry normal @7%O 2 (Nm ³ /hr) | 131,607 | 137,010 | 132,528 | 133,715 |
| Samplin | g Data | | | | |
| Vmald | Volume metered, standard (dscf) | 42.7316 | 42.4517 | 41.1525 | 42.1120 |
| %1 | Isokinetic sampling (%) | 100.1239 | 99.4233 | 101.2130 | 100.2534 |
| Laborate | ory Data | | | | |
| mn | Total HF collected (mg) | <0.0368 | <0.0339 | <0.0389 | |
| | | | | | |
| Hydroge C _{sd} | n Fluoride (HF) Results HF Concentration (lb/dscf) | <1.8996E-09 | <1.7583E-09 | <2.0840E-09 | <1.9140E-09 |
| C _{ad} C _{ad7} | HF Concentration @7% O $_2$ (lb/dscf) | <2.5511E-09 | <2.2693E-09 | <2.6478E-09 | <2.4894E-09 |
| | HF Concentration @12% CO 2 (lb/dscf) | <2.5022E-09 | <2.1933E-09 | <2.5518E-09 | <2.4158E-09 |
| C _{ed12} C _a | HF Concentration (b/acf) | <1.0297E-09 | <9.4664E-10 | <1.1139E-09 | <1.0301E-09 |
| C _{ad} | HF Concentration (ppmdv) | <0.0366 | < 0.0339 | <0.0402 | < 0.0369 |
| | HF Concentration @7% O 2 (ppmdv) | <0.0492 | <0.0437 | < 0.0510 | <0.0480 |
| C _{sd12} | HF Concentration @12% CO 2 (ppmdv) | <0.0482 | <0.0423 | <0.0492 | <0.0465 |
| C _w | HF Concentration (ppmwv) | <0.0293 | <0.0269 | < 0.0317 | <0.0293 |
| C _{ad} | HF Concentration (mg/dscm) | < 0.0304 | <0.0282 | <0.0334 | <0.0306 |
| C _{ed7} | HF Concentration @7% O 2 (mg/dscm) | < 0.0409 | < 0.0363 | <0.0424 | < 0.0399 |
| C _{sd12} | HF Concentration @12% CO 2 (mg/dscm) | <0.0401 | < 0.0351 | < 0.0409 | <0.0387 |
| Ca | HF Concentration (mg/m ³ (actual,wet)) | < 0.0165 | <0.0152 | <0.0178 | <0.0165 |
| C _{sd} | HF Concentration (mg/Nm ³ dry) | <0.0326 | < 0.0302 | <0.0358 | <0.0329 |
| C _{sd7} | HF Concentration @7% O $_2$ (mg/Nm ³ dry) | <0.0438 | <0.0390 | <0.0455 | <0.0428 |
| C _{sd12} | HF Concentration @12% CO 2 (mg/Nm ³ dry) | <0.0430 | <0.0377 | <0.0439 | <0.0415 |
| Eliphr | HF Rate (lb/hr) | <0.0127 | <0.0118 | <0.0133 | <0.0126 |
| E _{kg/h} | HF Rate (kg/hr) | <0.0058 | <0.0053 | <0.0060 | <0.0057 |
| E _{T/yr} | HF Rate (Ton/yr) | <0.0557 | <0.0516 | <0.0582 | <0.0552 |
| EFd | HF Rate - Fd-based (lb/MMBtu) | <0.000037 | <0.000033 | <0.000038 | <0.000036 |
| Efc | HF Rate - Fc-based (lb/MMBtu) | <0.000038 | <0.000033 | <0.000039 | <0.000037 |
| | | | | | |

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USEPA Method 26A (HCI) Sampling, Velocity and Moisture Parameters

| Run No. | | 1 | 2 | 3 | Average |
|-----------------|--|-----------------|----------|------------------|----------------------|
| Date (20 | 10) | Mar 18 | Mar 18 | Mar 18 | |
| Start Tim | ne (approx.) | 07:02 | 09:26 | 11:49 | |
| Stop Tim | ne (approx.) | 08:02 | 10:37 | 12:49 | |
| Samplin | g Conditions | | | | |
| Yd | Dry gas meter correction factor | 1.0085 | 1.0085 | 1.0085 | |
| C _p | Pitot tube coefficient | 0.8400 | 0.8400 | 0.8400 | |
| Pg | Static pressure (in. H ₂ O) | -1.9000 | -1.7000 | -1.7000 | |
| As | Sample location area (ft ²) | 60.1320 | 60.1320 | 60.1320 | |
| P_{bar} | Barometric pressure (in. Hg) | 30.05 | 30.05 | 30.05 | 30.0500 |
| O ₂ | Oxygen (dry volume %) | 9.1100 | 9.0100 | 9.7000 | 9.2733 |
| CO2 | Carbon dioxide (dry volume %) | 10.2300 | 10.3500 | 9.8200 | 10.1333 |
| N₂+CO | Nitrogen plus carbon monoxide (dry volume %) | 80.6600 | 80.6400 | 80.4800 | 80.5933 |
| V _{lc} | Total Liquid collected (ml) | 1 7 2.30 | 157.10 | 150.30 | |
| Vm | Volume metered, meter conditions (ft ³) | 37.0500 | 35.7400 | 35.6000 | |
| Tm | Dry gas meter temperature (°F) | 60.1250 | 66.0833 | 75.3750 | |
| Τs | Sample temperature (°F) | 488.8333 | 489.0833 | 496.916 7 | 491.6111 |
| ΔH | Meter box orifice pressure drop (in. H ₂ O) | 1.1917 | 1.2000 | 1.2000 | |
| θ | Total sampling time (min) | 60.0 | 60.0 | 60.0 | |
| Flow Res | sults | | | | |
| V_{wstd} | Volume of water collected (ft ³) | 8.1084 | 7.3931 | 7.0731 | 7.5249 |
| V_{mstd} | Volume metered, standard (dscf) | 38.1913 | 36.4244 | 35.6520 | 36.7559 |
| Ps | Sample gas pressure, absolute (in. Hg) | 29.9103 | 29.9250 | 29.9250 | 29. 9 201 |
| Pv | Vapor pressure, actual (in. Hg) | 29.9103 | 29.9250 | 29.9250 | 29.9 201 |
| Bwo | Moisture measured in sample (% by volume) | 17.5129 | 16.8725 | 16.5549 | 16.9801 |
| B _{ws} | Saturated moisture content (% by volume) | 100.0000 | 100.0000 | 100.0000. | 100.0000 |
| Bw | Actual water vapor in gas (% by volume) | 17.5129 | 16.8725 | 16.5549 | 16.9801 |
| Md | MW of sample gas, dry (lb/lb-mole) | 30.0012 | 30.0164 | 29.9592 | 29.9923 |
| Ms | MW of sample gas, wet (lb/lb-mole) | 27.8994 | 27.9889 | 27.9794 | 27.9559 |

Comments:

Average includes 3 runs.

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Prepared by Clean Air Engineering Proprietary Software SS ISOKINETIC Version 2006-13d

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USEPA Method 26A HCI Parameters

| Run No. | | 1 | 2 | 3 | Average |
|-------------------|---|------------|------------|------------|------------|
| Date (20 | 10) | Mar 18 | Mar 18 | Mar 18 | |
| - | ne (approx.) | 07:02 | 09:26 | 11:49 | |
| Stop Tim | ne (approx.) | 08:02 | 10:37 | 12:49 | |
| Process | Conditions | | | | |
| R _P | Steam Production Rate (Klbs/hour) | 183.5 | 184.1 | 182.8 | 183.5 |
| P ₁ | Fabric Filter Inlet Temperature (°F) | 320 | 320 | 320 | 320 |
| Fd | Oxygen-based F-factor (dscf/MMBtu) | 9,570 | 9,570 | 9,570 | 9,570 |
| F。 | Carbon dioxide-based F-factor (dscf/MMBtu) | 1,820 | 1,820 | 1,820 | 1,820 |
| Cap | Capacity factor (hours/year) | 8,760 | 8,760 | 8,760 | 8,760 |
| Gas Co | | | | | |
| | Oxygen (dry volume %) | 9.1100 | 9.0100 | 9.7000 | 9.2733 |
| | Carbon dioxide (dry volume %) | 10.2300 | 10.3500 | 9.8200 | 10.1333 |
| T _s | Sample temperature (°F) | 488.8333 | 489.0833 | 496.9167 | 491.6111 |
| Bw | Actual water vapor in gas (% by volume) | 17.5129 | 16.8725 | 16.5549 | 16.9801 |
| | | • | | | |
| Samplin | - | 38.1913 | 36.4244 | 35.6520 | 36.7559 |
| V _{mstd} | Volume metered, standard (dscf) | 36.1913 | 30.4244 | 35.6520 | 30.7559 |
| Laborat | ory Data | | | | |
| m _n | Total HCI collected (mg) | 789.3812 | 879.5132 | 662.6796 | |
| Hydroge | en Chioride (HCI) Results | | | | |
| C_{sd} | HCI Concentration (lb/dscf) | 4.5575E-05 | 5.3243E-05 | 4.0985E-05 | 4.6601E-05 |
| C_{sd7} | HCI Concentration @7% O ₂ (lb/dscf) | 5.3732E-05 | 6.2243E-05 | 5.0866E-05 | 5.5614E-05 |
| C_{sd12} | HCI Concentration @12% CO ₂ (lb/dscf) | 5.3461E-05 | 6.1730E-05 | 5.0084E-05 | 5.5092E-05 |
| C_{sd} | HCI Concentration (ppmdv) | 481.8514 | 562.9118 | 433.3210 | 492.6948 |
| C_{sd7} | HCl Concentration @7% O_2 (ppmdv) | 568.0861 | 658.0719 | 537.7823 | 587.9801 |
| C _{sd12} | HCI Concentration @12% CO ₂ (ppmdv) | 565.2216 | 652.6514 | 529.5165 | 582.4632 |
| Cw | HCI Concentration (ppmwv) | 397.4651 | 467.9344 | 361.5850 | 408.9948 |
| C _{sd} | HCI Concentration (mg/dscm) | 729.8280 | 852.6048 | 656.3223 | 746.2517 |
| C_{sd7} | HCl Concentration @7% O ₂ (mg/dscm) | 860.4419 | 996.7373 | 814.5428 | 890.5740 |
| C_{sd12} | HCl Concentration @12% CO ₂ (mg/dscm) | 856.1033 | 988.5273 | 802.0231 | 882.2179 |
| C_{sd} | HCI Concentration (mg/Nm ³ dry) | 783.2301 | 914.9905 | 704.3458 | 800.8555 |
| C_{sd7} | HCI Concentration @7% O2 (mg/Nm ³ dry) | 923.4010 | 1069.6693 | 874.1435 | 955.7379 |
| C_{sd12} | HCl Concentration @12% CO ₂ (mg/Nm ³ dry) | 918.7450 | 1060.8585 | 860.7077 | 946.7704 |
| E _{Fd} | HCI Rate - Fd-based (lb/MMBtu) | 0.7732 | 0.8956 | 0.7319 | 0.8002 |
| Efc | HCI Rate - Fc-based (lb/MMBtu) | 0.8108 | 0.9362 | 0.7596 | 0.8356 |

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USEPA Method 26A (HCI) Sampling, Velocity and Moisture Parameters

| Run No. | | 1 | 2 | 3 | Average |
|-------------------|--|----------|----------|----------|-----------------|
| Date (20 | 10) | Mar 18 | Mar 18 | Mar 18 | |
| Start Tim | ne (approx.) | 07:02 | 09:26 | 11:49 | |
| Stop Tim | e (approx.) | 08:02 | 10:37 | 12:49 | |
| Samplin | g Conditions | | | | |
| Yd | Dry gas meter correction factor | 1.0066 | 1.0066 | 1.0066 | |
| C _p | Pitot tube coefficient | 0.8400 | 0.8400 | 0.8400 | |
| Pg | Static pressure (in. H ₂ O) | -11.1000 | -10.9000 | -11.0000 | |
| As | Sample location area (ft ²) | 64.0000 | 64.0000 | 64.0000 | |
| P _{bar} | Barometric pressure (in. Hg) | 30.05 | 30.05 | 30.05 | 30.0500 |
| O ₂ | Oxygen (dry volume %) | 9.8800 | 9.6900 | 10.0500 | 9.8733 |
| CO2 | Carbon dioxide (dry volume %) | 9.5000 | 9.6700 | 9.4200 | 9.5300 |
| N₂+CO | Nitrogen plus carbon monoxide (dry volume %) | 80.6200 | 80.6400 | 80.5300 | 80.5967 |
| Vic | Total Liquid collected (ml) | 217.40 | 236.20 | 211.10 | |
| Vm | Volume metered, meter conditions (ft ³) | 40.1050 | 39.9000 | 40.1550 | |
| Tm | Dry gas meter temperature (°F) | 62.6250 | 63.7917 | 69.0833 | |
| Τs | Sample temperature (°F) | 307.6667 | 309.0833 | 309.9167 | 308.8889 |
| ΔH | Meter box orifice pressure drop (in. H ₂ O) | 1.5000 | 1.5000 | 1.5000 | |
| θ | Total sampling time (min) | 60.0 | 60.0 | 60.0 | |
| Flow Res | Bults | | | | |
| V _{wstd} | Volume of water collected (ft ³) | 10.2308 | 11.1156 | 9.9344 | 10.4269 |
| V _{mstd} | Volume metered, standard (dscf) | 41.0960 | 40.7949 | 40.6450 | 40.8453 |
| Ps | Sample gas pressure, absolute (in. Hg) | 29.2338 | 29.2485 | 29.2412 | 29.2412 |
| Pv | Vapor pressure, actual (in. Hg) | 29.2338 | 29.2485 | 29.2412 | 29.2412 |
| Bwo | Moisture measured in sample (% by volume) | 19.9327 | 21.4130 | 19.6412 | 20.3290 |
| B _{ws} | Saturated moisture content (% by volume) | 100.0000 | 100.0000 | 100.0000 | 100.0000 |
| Bw | Actual water vapor in gas (% by volume) | 19.9327 | 21.4130 | 19.6412 | 20.3290 |
| M _d | MW of sample gas, dry (lb/lb-mole) | 29.9152 | 29.9348 | 29.9092 | 29.9 197 |
| Ms | MW of sample gas, wet (lb/lb-mole) | 27.5402 | 27.3792 | 27.5701 | 27.4965 |

Comments:

Average includes 3 runs.

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USEPA Method 26A HCI Parameters

| Run No | | 1 | 2 | 3 | Average |
|---------------------|---|------------|------------|------------|------------|
| Date (20 | 110) | Mar 18 | Mar 18 | Mar 18 | |
| - | ne (approx.) | 07:02 | 09:26 | 11:49 | |
| | ne (approx.) | 08:02 | 10:37 | 12:49 | |
| Process | s Conditions | | | | |
| R _P | Steam Production Rate (Klbs/hour) | 183.5 | 184.1 | 182.8 | 183.5 |
| P ₁ | Fabric Filter Inlet Temperature (°F) | 320 | 320 | 320 | 320 |
| Fd | Oxygen-based F-factor (dscf/MMBtu) | 9,570 | 9,570 | 9,570 | 9,570 |
| Fc | Carbon dioxide-based F-factor (dscf/MMBtu) | 1,820 | 1,820 | 1,820 | 1,820 |
| Сар | Capacity factor (hours/year) | 8,760 | 8,760 | 8,760 | 8,760 |
| | · · · · · · | | | | • |
| | nditions Oxygen (dry volume %) | 9.8800 | 9.6900 | 10.0500 | 9.8733 |
| | Carbon dioxide (dry volume %) | 9.5000 | 9.6700 | 9.4200 | 9.5300 |
| T _s | Sample temperature (°F) | 307.6667 | 309.0833 | 309.9167 | 308.8889 |
| ь В _w | Actual water vapor in gas (% by volume) | 19.9327 | 21.4130 | 19.6412 | 20.3290 |
| | | 10.0021 | 21.4100 | 10.0412 | 20.5250 |
| Samplin | - | | | | |
| V _{mstd} | Volume metered, standard (dscf) | 41.0960 | 40.7949 | 40.6450 | 40.8453 |
| Laborat | ory Data | | | | |
| mn | Total HCI collected (mg) | 30.4838 | 25.1430 | 26.4504 | |
| Hydrog | en Chloride (HCI) Results | | | | |
| C _{sd} | HCI Concentration (lb/dscf) | 1.6356E-06 | 1.3590E-06 | 1.4349E-06 | 1.4765E-06 |
| C _{sd7} | HCI Concentration @7% O ₂ (lb/dscf) | 2.0631E-06 | 1.6851E-06 | 1.8383E-06 | 1.8622E-06 |
| C _{sd12} | HCI Concentration @12% CO ₂ (lb/dscf) | 2.0660E-06 | 1.6865E-06 | 1.8279E-06 | 1.8601E-06 |
| C _{sd} | HCI Concentration (ppmdv) | 17.2926 | 14.3682 | 15.1710 | 15.6106 |
| C _{sd7} | HCI Concentration @7% O2 (ppmdv) | 21.8119 | 17.8160 | 19.4357 | 19.6879 |
| C _{sd12} | HCI Concentration @12% CO ₂ (ppmdv) | 21.8432 | 17.8302 | 19.3262 | 19.6665 |
| C _w | HCI Concentration (ppmwv) | 13.8457 | 11.2915 | 12.1913 | 12.4428 |
| C _{sd} | HCI Concentration (mg/dscm) | 26.1919 | 21.7625 | 22.9786 | 23.6443 |
| C _{sd7} | HCI Concentration @7% O ₂ (mg/dscm) | 33.0370 | 26.9848 | 29.4380 | 29.8199 |
| C _{sd12} | HCI Concentration @12% CO ₂ (mg/dscm) | 33.0845 | 27.0062 | 29.2721 | 29.7876 |
| C _{sd} | HCI Concentration (mg/Nm ³ dry) | 28.1084 | 23.3549 | 24.6599 | 25.3744 |
| C _{sd7} | HCI Concentration @7% O ₂ (mg/Nm ³ dry) | 35.4543 | 28.9592 | 31.5920 | 32.0018 |
| C _{sd12} | HCI Concentration @12% CO2 (mg/Nm3 dry) | 35.5053 | 28.9823 | 31.4139 | 31.9672 |
| E _{Fd} | HCI Rate - Fd-based (lb/MMBtu) | 0.0297 | 0.0242 | 0.0265 | 0.0268 |
| EFc | HCI Rate - Fc-based (lb/MMBtu) | 0.0313 | 0.0256 | 0.0277 | 0.0282 |
| | | | | | |

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USEPA Method 5/29 (Particulate/Metals) Sampling, Velocity and Moisture Parameters

| Run No | | 1 | 2 | 3 | Average |
|-------------------|--|------------|------------|------------|------------|
| Date (20 | 010) | Mar 18 | Mar 18 | Mar 18 | |
| Start Tir | ne (approx.) | 07:09 | 09:49 | 12:27 | |
| Stop Tin | ne (approx.) | 09:22 | 12:02 | 14:39 | |
| Samplin | ng Conditions | | | | |
| Yd | Dry gas meter correction factor | 0.9904 | 0.9904 | 0.9904 | |
| C, | Pitot tube coefficient | 0.8050 | 0.8050 | 0.8050 | |
| P, | Static pressure (in. H ₂ O) | -10.6000 | -10.6000 | -10.7000 | |
| Å, | Sample location area (ft ²) | 64.0000 | 64.0000 | 64.0000 | |
| P _{bar} | Barometric pressure (in. Hg) | 30.05 | 30.05 | 30.05 | 30.0500 |
| D | Nozzle diameter (in.) | 0.2700 | 0.2700 | 0.2700 | |
| O ₂ | Oxygen (dry volume %) | 10.0700 | 9.7500 | 9.8900 | 9.9033 |
| CO2 | Carbon dioxide (dry volume %) | 9.2500 | 9.6000 | 9.5800 | 9.4767 |
| N₂+CC | Nitrogen plus carbon monoxide (dry volume %) | 80.6800 | 80.6500 | 80.5300 | 80.6200 |
| Vic | Total Liquid collected (ml) | 459.40 | 434.20 | 463.60 | |
| Vm | Volume metered, meter conditions (ft ³) | 84.6670 | 81.6300 | 85.1700 | |
| Tm | Dry gas meter temperature (°F) | 69.9000 | 81.9000 | 86.4800 | |
| Тв | Sample temperature (°F) | 307.4800 | 307.6000 | 307.7600 | 307.6133 |
| ΔH | Meter box orifice pressure drop (in. H ₂ O) | 1.4596 | 1.3336 | 1.4432 | |
| θ | Total sampling time (min) | 125.0 | 125.0 | 125.0 | |
| Flow Re | sults | | | | |
| V _{wstd} | Volume of water collected (ft ³) | 21.6194 | 20.4335 | 21.8170 | 21.2899 |
| Vmstd | Volume metered, standard (dscf) | 84.1826 | 79.3413 | 82.1102 | 81.8780 |
| P۵ | Sample gas pressure, absolute (in. Hg) | 29.2706 | 29.2706 | 29.2632 | 29.2681 |
| P, | Vapor pressure, actual (in. Hg) | 29.2706 | 29.2706 | 29.2632 | 29.2681 |
| Bwo | Moisture measured in sample (% by volume) | 20.4338 | 20.4796 | 20.9926 | 20.6353 |
| B _{ws} | Saturated moisture content (% by volume) | 100.0000 | 100.0000 | 100.0000 | 100.0000 |
| Bw | Actual water vapor in gas (% by volume) | 20.4338 | 20.4796 | 20.9926 | 20.6353 |
| √∆P | Velocity head (√in. H₂O) | 0.7819 | 0.7481 | 0.7707 | 0.7669 |
| Md | MW of sample gas, dry (lb/lb-mole) | 29.8828 | 29.9260 | 29.9284 | 29.9124 |
| M _s | MW of sample gas, wet (lb/lb-mole) | 27.4547 | 27.4836 | 27.4243 | 27.4542 |
| Vs | Velocity of sample (ft/sec) | 52.5853 | 50.2877 | 51.8795 | 51.5842 |
| % | Isokinetic sampling (%) | 100.3071 | 98.9302 | 99.9317 | 99.7230 |
| Qa | Volumetric flow rate, actual (acfm) | 201,928 | 193,105 | 199,217 | 198,083 |
| Q, | Volumetric flow rate, standard (scfm) | 135,904 | 129,946 | 133,997 | 133,282 |
| Q _{std} | Volumetric flow rate, dry standard (dscfm) | 108,134 | 103,333 | 105,868 | 105,778 |
| Q _{std7} | Volumetric flow rate, dry std@7%O ₂ (dscfm) | 84,251 | 82,890 | 83,856 | 83,666 |
| Q, | Volumetric flow rate, actual (acf/hr) | 12,115,652 | 11,586,291 | 11,953,037 | 11,884,993 |
| Q, | Volumetric flow rate, standard (scf/hr) | 8,154,240 | 7,796,743 | 8,039,841 | 7,996,941 |
| Q _{std} | Volumetric flow rate, dry standard (dscf/hr) | 6,468,019 | 6,200,003 | 6,352,070 | 6,346,697 |
| Q, | Volumetric flow rate, actual (m ³ /hr) | 343,122 | 328,131 | 338,517 | 336,590 |
| Q, | Volumetric flow rate, standard (m ³ /hr) | 230,933 | 220,808 | 227,693 | 226,478 |
| Q _{std} | Volumetric flow rate, dry standard (dry m ³ /hr) | 183,745 | 175,588 | 179,894 | 179,742 |
| Q _{std7} | Volumetric flow rate, dry std@7%O ₂ (dry m ³ /hr) | 143,162 | 140,849 | 142,492 | 142,168 |
| Q, | Volumetric flow rate, normal (Nm ³ /hr) | 215,187 | 205,753 | 212,169 | 211,036 |
| Q _{std} | Volumetric flow rate, dry normal (Nm ³ /hr) | 171,216 | 163,616 | 167,629 | 167,487 |
| Q _{std7} | Volumetric flow rate, dry normal @7%O ₂ (Nm ³ /hr) | 133,401 | 131,246 | 132,777 | 132,474 |

Comments:

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Average includes 3 runs.

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QA/QC _____ Date _____

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USEPA Method 5/29 Filterable Particulate Parameters

| Run No. | | 1 | 2 | 3 | Average |
|-------------------------------------|---|------------|------------|-----------------|----------------------------|
| Date (20 | 10) | Mar 18 | Mar 18 | Mar 18 | |
| | ne (approx.) | 07:09 | 09:49 | 12:27 | |
| | ne (approx.) | 09:22 | 12:02 | 14:39 | |
| | Conditions | | | | |
| R _P | Steam Production Rate (Klbs/hour) | 183.9 | 182.9 | 183.9 | 183.6 |
| P ₁ | Fabric Filter Inlet Temperature (°F) | 320 | 320 | 321 | 320 |
| Fd | Oxygen-based F-factor (dscf/MMBtu) | 9,570 | 9,570 | 9,570 | 9,570 |
| F _c | Carbon dioxide-based F-factor (dscf/MMBtu) | 1,820 | 1,820 | 1,820 | 1,820 |
| Cap | Capacity factor (hours/year) | 8,760 | 8,760 | 8,760 | 8,760 |
| Gas Cor | differe | | | | |
| | Oxygen (dry volume %) | 10.0700 | 9.7500 | 9.8900 | 9.9033 |
| | Carbon dioxide (dry volume %) | 9.2500 | 9.6000 | 9.5800 | 9.4767 |
| т <u>,</u> | Sample temperature (°F) | 307.4800 | 307.6000 | 307.7600 | 307.6133 |
| B _w | Actual water vapor in gas (% by volume) | 20.4338 | 20.4796 | 20.9926 | 20.6353 |
| | | | | | |
| Gas Flo | W Rate Volumetric flow rate, actual (acfm) | 201,928 | 193,105 | 199,217 | 198,083 |
| Q, | Volumetric flow rate, standard (scfm) | 135,904 | 129,946 | 133,997 | 133,282 |
| Q, | Volumetric flow rate, dry standard (dscfm) | 108,134 | 103,333 | 105,868 | 105,778 |
| Q _{std} | Volumetric flow rate, dry std@7%O ₂ (dscfm) | 84,251 | 82,890 | 83,856 | 83,666 |
| Q _{std7} Q _a | Volumetric flow rate, actual (acf/hr) | 12,115,652 | 11,586,291 | 11,953,037 | 11,884,993 |
| Q, | Volumetric flow rate, standard (scf/hr) | 8,154,240 | 7,796,743 | 8,039,841 | 7,996,941 |
| Q _{std} | Volumetric flow rate, dry standard (dscf/hr) | 6,488,019 | 6,200,003 | 6,352,070 | 6,346,697 |
| Q, | Volumetric flow rate, actual (m^3/hr) | 343,122 | 328,131 | 338,517 | 336,590 |
| Q, | Volumetric flow rate, standard (m ³ /hr) | 230,933 | ~ 220,808 | 227,693 | 226,478 |
| Q _{std} | Volumetric flow rate, dry standard (dry m ³ /hr) | 183,745 | 175,588 | 179,894 | 179,742 |
| Q _{std7} | Volumetric flow rate, dry std@7% O_2 (dry m ³ /hr) | 143,162 | 140,849 | 142,492 | 142,168 |
| Q, | Volumetric flow rate, normal (Nm ³ /hr) | 215,187 | 205,753 | 212,169 | 211,036 |
| Q _{std} | Volumetric flow rate, dry normal (Nm ³ /hr) | 171,216 | 163,616 | 167,629 | 167,487 |
| Q _{std7} | Volumetric flow rate, dry normal @7%O2 (Nm3/hr) | 133,401 | 131,246 | 132, 777 | 132,474 |
| Samplin | | | | | |
| Vmstd | Volume metered, standard (dscf) | 84.1826 | 79.3413 | 82.1102 | 81.8780 |
| %1 | Isokinetic sampling (%) | 100.3071 | 98.9302 | 99.9317 | 99.7230 |
| Laborat | ory Data | | | | |
| m _{filter} | Matter collected on filter(s) (g) | 0.00180 | 0.00100 | 0.00090 | |
| ms | Matter collected in solvent rinse(s) (g) | 0.00224 | 0.00131 | 0.00162 | |
| m | Total particulate matter collected (g) | 0.00404 | 0.00231 | 0.00252 | |
| | e Particulate Results | | | | |
| C _{sd} | Particulate Concentration (lb/dscf) | 1.0571E-07 | 6.4320E-08 | 6.7580E-08 | 7.9205E-08 |
| C _{sd7} | Particulate Concentration @7% O ₂ (lb/dscf) | 1.3568E-07 | 8.0184E-08 | 8.5319E-08 | 1.0039E-07 |
| C _{sd12} | Particulate Concentration @12% CO2 (lb/dscf) | 1.3714E-07 | 8.0400E-08 | 8.4651E-08 | 1.0073E-07 |
| C _a | Particulate Concentration (Ib/acf) | 5.6611E-08 | 3.4419E-08 | 3.5913E-08 | 4.2314E-08 |
| C _{sd} | Particulate Concentration (gr/dscf) | 0.0007 | 0.0005 | 0.0005 | 0.0006 |
| C _{ad7} | Particulate Concentration @7% O2 (gr/dscf) | 0.0009 | 0.0006 | 0.0006 | 0.0007 |
| C _{sd12} | Particulate Concentration @12% CO ₂ (gr/dscf) | 0.0010 | 0.0006 | 0.0006 | 0.0007 |
| Ca | Particulate Concentration (gr/acf) | 0.0004 | 0.0002 | 0.0003 | 0.0003 |
| Csd | Particulate Concentration (mg/dscm) | 1.6929 | 1.0300 | 1.0822 | 1.2684 |
| Cad7 | Particulate Concentration @7% O ₂ (mg/dscm) | 2.1728 | 1.2840 | 1.3663 | 1.6077 |
| C _{ad12} | Particulate Concentration @12% CO ₂ (mg/dscm) | 2.1962 | 1.2875 | 1.3556 | 1. 6131 |
| Ca | Particulate Concentration (mg/m ³ (actual,wet)) | 0.9065 | 0.5512 | 0.5751 | 0.6776 |
| Cad | Particulate Concentration (mg/Nm ³ dry) | 1.8167 | 1.1054 | 1.1614 | 1.3612 |
| C _{ad7} | Particulate Concentration @7% O ₂ (mg/Nm ³ dry) | 2.3317 | 1.3780 | 1.4662 | 1.7253 |
| C _{sd12} | Particulate Concentration @12% CO ₂ (mg/Nm ³ dry) | 2.3568 | 1.3817 | 1.4548 | 1.7311 |
| E _{ib/hr} | Particulate Rate (lb/hr) | 0.6859 | 0.3988 | 0.4293 | 0.5046 |
| Ekg/hr | Particulate Rate (kg/hr) | 0.3111 | 0.1809 | 0.1947 | 0.2289 |
| E _{T/yr} | Particulate Rate (Ton/yr) | 3.0041 | 1.7467 | 1.8802 | 2.2103 |
| EFd | Particulate Rate - Fd-based (lb/MMBtu) | 0.0020 | 0.0012 | 0.0012 | 0.0014 |
| E _{Fc} | Particulate Rate - F _c -based (Ib/MMBtu) | 0.0021 | 0.0012 | 0.0013 | 0.0015 |
| Commer | | | | | 041310 093438 K i N Ø_K |
| Averag | ge includes 3 runs. | | | | |

Average includes 3 runs. Prepared by Clain Air Engineering Proprietary Software SS EPA 5-1 Version 2008-08b

QA/QC Date

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USEPA Method 5/29 Mercury (Hg) Emission Parameters

| Run No | . | 1 | 2 | 3 | Average |
|---|---|--|--|--|--|
| Date (20 | 010) | Mar 18 | Mar 18 | Mar 18 | |
| Start Tir | me (approx.) | 07:09 | 09:49 | 12:27 | |
| Stop Tin | ne (approx.) | 09:22 | 12:02 | 14:39 | |
| Process | s Conditions | | | | |
| R _P | Steam Production Rate (Klbs/hour) | 183.9 | 182.9 | 183.9 | 183.6 |
| P1 | Fabric Filter Inlet Temperature (*F) | 320 | 320 | 321 | 320.3 |
| Fd | Oxygen-based F-factor (dscf/MMBtu) | 9,570 | 9,570 | 9,570 | 9,570 |
| F。 | Carbon dioxide-based F-factor (dscf/MMBtu) | 1,820 | 1,820 | 1,820 | 1,820 |
| Сар | Capacity factor (hours/year) | 8,760 | 8,760 | 8,760 | 8,760 |
| Gas Co | nditions | | | | |
| O ₂ | Oxygen (dry volume %) | 10.0700 | 9.7500 | 9.8900 | 9.9033 |
| CO2 | Carbon dloxide (dry volume %) | 9.2500 | 9.6000 | 9.5800 | 9.4767 |
| Тs | Sample temperature (°F) | 307.4800 | 307.6000 | 307.7600 | 307.6133 |
| B, | Actual water vapor in gas (% by volume) | 20.4338 | 20.4796 | 20.9926 | 20.6353 |
| Gas Flo | w Rate | | | | |
| Q | Volumetric flow rate, actual (acfm) | 201,928 | 193,105 | 199,217 | 198,083 |
| Q, | Volumetric flow rate, standard (scfm) | 135,904 | 129,946 | 133,997 | 133,282 |
| Q _{std} | Volumetric flow rate, dry standard (dscfm) | 108,134 | 103,333 | 105,868 | 105,778 |
| Q _{std7} | Volumetric flow rate, dry std@7%O ₂ (dscfm) | 84,251 | 82,890 | 83,856 | 83,666 |
| Q, | Volumetric flow rate, actual (acf/hr) | 12,115,652 | 11,586,291 | 11,953,037 | 11,884,993 |
| Q, | Volumetric flow rate, standard (scf/hr) | 8,154,240 | 7,796,743 | 8,039,841 | 7,996,941 |
| Q _{std} | Volumetric flow rate, dry standard (dscf/hr) | 6,488,019 | 6,200,003 | 6,352,070 | 6,346,697 |
| Q | Volumetric flow rate, actual (m ³ /hr) | 343,122 | 328,131 | 338,517 | 336,590 |
| Q, | Volumetric flow rate, standard (m ³ /hr) | 230,933 | 220,808 | 227,693 | 226,478 |
| Q _{std} | Volumetric flow rate, dry standard (dry m ³ /hr) | 183,745 | 175,588 | 179,894 | 179,742 |
| Q _{std7} | Volumetric flow rate, dry std@7% O_2 (dry m ³ /hr) | 143,162 | 140,849 | 142,492 | 142,168 |
| Q _s | Volumetric flow rate, normal (Nm ³ /hr) | 215,187 | 205,753 | 212,169 | 211,036 |
| Q _{std} | Volumetric flow rate, dry normal (Nm ³ /hr) | 171,216 | 163,616 | 167,629 | 167,487 |
| Q _{std7} | Volumetric flow rate, dry normal $(0.7\%)^{3/hr}$ | 133,401 | 131,246 | 132,777 | 132,474 |
| | | | , | , | |
| Samplin | g Data Volume metered, standard (dscf) | 84.1826 | 79.3413 | 82.1102 | 81.8780 |
| V _{mstd} %l | Isokinetic sampling (%) | 100.3071 | 98.9302 | 99.9317 | 99.7230 |
| | | 100.3071 | 30.3302 | 33.3317 | 55.7250 |
| | bry Data | | | | |
| m _{n-1b} | Fraction 1B (µg) | <0.1000 | <0.1000 | <0.1000 | |
| m _{n-2b} | Fraction 2B (µg) | 9.1977 | 9.2740 | 10.1318 | |
| m _{n-3a} | Fraction 3A (µg) | <0.2000 | <0.2000 | <0.2000 | |
| m _{n-3b} | Fraction 3B (µg) | <0.5000 | <0.5000 | <0.5000 | |
| m _{n-3c} | Fraction 3C (µg) | <0.4000 | <0.4000 | <0.4000 | |
| m'n | Total matter corrected for allowable blanks (µg) | 9.1977 | 9.2740 | 10.1318 | |
| Aercury | Results - Total | | | | |
| C _{sd} | Concentration (lb/dscf) | 2.4092E-10 | 2.5774E-10 | 2.7208E-10 | 2.5691E-10 |
| C _{sd7} | Concentration @7% O ₂ (lb/dscf) | 3.0921E-10 | 3.2131E-10 | 3.4350E-10 | 3.2467E-10 |
| C_{sd12} | Concentration @12% CO ₂ (lb/dscf) | 3.1254E-10 | 3.2217E-10 | 3.4081E-10 | 3.2517E-10 |
| Ca | Concentration (lb/acf) | 1.2901E-10 | 1.3792E-10 | 1.4459E-10 | 1.3717E-10 |
| <u>^</u> | Concentration (µg/dscm) | 3.8579E+00 | 4.1273E+00 | 4.3570E+00 | 4.1141E+00 |
| C _{sd} | Concentration @7% O ₂ (µg/dscm) | 4.9515E+00 | 5.1453E+00 | 5.5007E+00 | 5.1992E+00 |
| C _{sd} C _{sd7} | Concentration (B) / CO2 (pg/dscin) | 4.93132100 | | | |
| | Concentration @12% CO_2 (µg/dscm) | 4.9313E+00 5.0049E+00 | 5.1591E+00 | 5.4576E+00 | 5.2072E+00 |
| C _{sd7} | | | | 5.4576E+00 4.3570E-03 | 5.2072E+00 4.1141E-03 |
| C _{sd7} C _{sd12} | Concentration @12% CO ₂ (µg/dscm) | 5.0049E+00 | 5.1591E+00 | | |
| C _{sd7} C _{sd12} C _{sd} | Concentration @12% CO_2 (μ g/dscm) Concentration (mg/dscm) | 5.0049E+00 3.8579E-03 | 5.1591E+00 4.1273E-03 | 4.3570E-03 | 4.1141E-03 |
| C _{sd7} C _{sd12} C _{sd} C _{sd7} | Concentration @12% CO_2 (µg/dscm) Concentration (mg/dscm) Concentration @7% O_2 (mg/dscm) | 5.0049E+00 3.8579E-03 4.9515E-03 | 5.1591E+00 4.1273E-03 5.1453E-03 | 4.3570E-03 5.5007E-03 | 4.1141E-03 5.1992E-03 |
| C _{sd7} C _{sd12} C _{sd} C _{sd7} C _{sd12} | Concentration @12% CO_2 (µg/dscm) Concentration (mg/dscm) Concentration @7% O_2 (mg/dscm) Concentration @12% CO_2 (mg/dscm) | 5.0049E+00 3.8579E-03 4.9515E-03 5.0049E-03 | 5.1591E+00 4.1273E-03 5.1453E-03 5.1591E-03 | 4.3570E-03 5.5007E-03 5.4576E-03 | 4.1141E-03 5.1992E-03 5.2072E-03 |
| C _{sd7} C _{sd12} C _{sd} C _{sd7} C _{sd12} C _a | Concentration @12% CO_2 (µg/dscm) Concentration (mg/dscm) Concentration @7% O_2 (mg/dscm) Concentration @12% CO_2 (mg/dscm) Concentration (µg/m ³ (actual,wet)) | 5.0049E+00 3.8579E-03 4.9515E-03 5.0049E-03 2.0659E+00 | 5.1591E+00 4.1273E-03 5.1453E-03 5.1591E-03 2.2086E+00 | 4.3570E-03 5.5007E-03 5.4576E-03 2.3154E+00 | 4.1141E-03 5.1992E-03 5.2072E-03 2.1966E+00 |
| C _{sd7} C _{sd12} C _{sd} C _{sd7} C _{sd12} C _a C _{sd} C _{sd} | Concentration @12% CO_2 (µg/dscm) Concentration (mg/dscm) Concentration @7% O_2 (mg/dscm) Concentration @12% CO_2 (mg/dscm) Concentration (µg/m ³ (actual,wet)) Concentration (µg/Nm ³ dry) | 5.0049E+00 3.8579E-03 4.9515E-03 5.0049E-03 2.0659E+00 4.1402E+00 | 5.1591E+00 4.1273E-03 5.1453E-03 5.1591E-03 2.2086E+00 4.4293E+00 | 4.3570E-03 5.5007E-03 5.4576E-03 2.3154E+00 4.6758E+00 | 4.1141E-03 5.1992E-03 5.2072E-03 2.1966E+00 4.4151E+00 |
| $\begin{array}{c} C_{sd7} \\ C_{sd12} \\ C_{sd} \\ C_{sd7} \\ C_{sd12} \\ C_a \\ C_a \\ C_{sd} \\ C_{sd7} \\ C_{sd12} \end{array}$ | Concentration @12% CO_2 (µg/dscm) Concentration (mg/dscm) Concentration @7% O_2 (mg/dscm) Concentration @12% CO_2 (mg/dscm) Concentration (µg/m ³ (actual,wet)) Concentration (µg/Nm ³ dry) Concentration @7% O_2 (µg/Nm ³ dry) | 5.0049E+00 3.8579E-03 4.9515E-03 5.0049E-03 2.0659E+00 4.1402E+00 5.3138E+00 | 5.1591E+00 4.1273E-03 5.1453E-03 5.1591E-03 2.2086E+00 4.4293E+00 5.5217E+00 | 4.3570E-03 5.5007E-03 5.4576E-03 2.3154E+00 4.6758E+00 5.9032E+00 | 4.1141E-03 5.1992E-03 5.2072E-03 2.1966E+00 4.4151E+00 5.5796E+00 |
| $\begin{array}{c} C_{sd7} \\ C_{sd12} \\ C_{sd} \\ C_{sd} \\ C_{sd7} \\ C_{sd12} \\ C_{a} \\ C_{sd} \\ C_{sd7} \\ C_{sd12} \\ E_{lb/hr} \\ \end{array}$ | Concentration @12% CO_2 (µg/dscm) Concentration (mg/dscm) Concentration @7% O_2 (mg/dscm) Concentration @12% CO_2 (mg/dscm) Concentration (µg/m ³ (actual,wet)) Concentration (µg/Nm ³ dry) Concentration @7% O_2 (µg/Nm ³ dry) Concentration @12% CO_2 (µg/Nm ³ dry) | 5.0049E+00 3.8579E-03 4.9515E-03 5.0049E-03 2.0659E+00 4.1402E+00 5.3138E+00 5.3711E+00 | 5.1591E+00 4.1273E-03 5.1453E-03 5.1591E-03 2.2086E+00 4.4293E+00 5.5217E+00 5.5366E+00 | 4.3570E-03 5.5007E-03 5.4576E-03 2.3154E+00 4.6758E+00 5.9032E+00 5.8570E+00 | 4.1141E-03 5.1992E-03 5.2072E-03 2.1966E+00 4.4151E+00 5.5796E+00 5.5882E+00 |
| $\begin{array}{c} C_{sd7} \\ C_{sd12} \\ C_{sd} \\ C_{sd} \\ C_{sd7} \\ C_{sd12} \\ C_{a} \\ C_{sd} \\ C_{sd7} \\ C_{sd12} \\ E_{lb/hr} \\ E_{g/s} \end{array}$ | Concentration @12% CO ₂ (μ g/dscm) Concentration (mg/dscm) Concentration @7% O ₂ (mg/dscm) Concentration @12% CO ₂ (mg/dscm) Concentration (μ g/m ³ (actual,wet)) Concentration (μ g/Nm ³ dry) Concentration @7% O ₂ (μ g/Nm ³ dry) Concentration @12% CO ₂ (μ g/Nm ³ dry) Rate (lb/hr) Rate (g/s) | 5.0049E+00 3.8579E-03 4.9515E-03 5.0049E-03 2.0659E+00 4.1402E+00 5.3138E+00 5.3711E+00 1.5631E-03 | 5.1591E+00 4.1273E-03 5.1453E-03 5.1591E-03 2.2086E+00 4.4293E+00 5.5217E+00 5.5366E+00 1.5980E-03 | 4.3570E-03 5.5007E-03 5.4576E-03 2.3154E+00 4.6758E+00 5.9032E+00 5.8570E+00 1.7283E-03 | 4.1141E-03 5.1992E-03 5.2072E-03 2.1966E+00 4.4151E+00 5.5796E+00 5.5882E+00 1.6298E-03 2.0531E-04 |
| $\begin{array}{c} C_{sd7} \\ C_{sd12} \\ C_{sd} \\ C_{sd} \\ C_{sd7} \\ C_{sd12} \\ C_{a} \\ C_{sd} \\ C_{sd7} \\ C_{sd12} \\ E_{lb/hr} \\ \end{array}$ | Concentration @12% CO_2 (µg/dscm) Concentration (mg/dscm) Concentration @7% O_2 (mg/dscm) Concentration @12% CO_2 (mg/dscm) Concentration (µg/m ³ (actual,wet)) Concentration (µg/Nm ³ dry) Concentration @7% O_2 (µg/Nm ³ dry) Concentration @12% CO_2 (µg/Nm ³ dry) Rate (lb/hr) | 5.0049E+00 3.8579E-03 4.9515E-03 5.0049E-03 2.0659E+00 4.1402E+00 5.3138E+00 5.3711E+00 1.5631E-03 1.9691E-04 | 5.1591E+00 4.1273E-03 5.1453E-03 5.1591E-03 2.2086E+00 4.4293E+00 5.5217E+00 5.5366E+00 1.5980E-03 2.0131E-04 | 4.3570E-03 5.5007E-03 5.4576E-03 2.3154E+00 4.6758E+00 5.9032E+00 5.8570E+00 1.7283E-03 2.1772E-04 | 4.1141E-03 5.1992E-03 5.2072E-03 2.1966E+00 4.4151E+00 5.5796E+00 5.5882E+00 1.6298E-03 |

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Date_

USEPA Method 5/29 Beryllium (Be) Emission Parameters

| Run No. | | 1 | 2 | 3 | Average |
|-------------------|--|------------------------|-------------------------|----------------------|--------------------|
| Date (20 | 10) | Mar 18 | Mar 18 | Mar 18 | |
| | ne (approx.) | 07:09 | 09:49 | 12:27 | |
| | ne (approx.) | 09:22 | 12:02 | 14:39 | |
| | Conditions | | | | |
| R _P | Steam Production Rate (Klbs/hour) | 183.9 | 182.9 | 183.9 | 183.6 |
| P ₁ | Fabric Filter Inlet Temperature (°F) | 320 | 320 | 321 | 320.3 |
| Fa | Oxygen-based F-factor (dscf/MMBtu) | 9,570 | 9,570 | 9,570 | 9,570 |
| F _e | Carbon dloxide-based F-factor (dscf/MMBtu) | 1,820 | 1,820 | 1,820 | 1,820 |
| Cap | Capacity factor (hours/year) | 8,760 | 8,760 | 8,760 | 8,760 |
| | | | | | |
| Gas Cor | Oxygen (dry volume %) | 10.0700 | 9.7500 | 9.8900 | 9.9033 |
| 02 CO2 | Carbon dioxide (dry volume %) | 9.2500 | 9.6000 | 9.5800 | 9.4767 |
| τ _s | Sample temperature (°F) | 307.4800 | 307.6000 | 307.7600 | 307.6133 |
| 's Bw | Actual water vapor in gas (% by volume) | 20.4338 | 20.4796 | 20.9926 | 20.6353 |
| | | 20.4000 | 20.4700 | LOUGED | 20/0000 |
| Gas Flo | | 004 008 | 102 105 | 100 017 | 409 093 |
| Q, | Volumetric flow rate, actual (acfm) | 201,928 | 193,105 | 199,217 | 198,083 |
| Q, | Volumetric flow rate, standard (scfm) | 135,904 | 129,946 | 133,997 105.868 | 133,282 |
| Q _{std} | Volumetric flow rate, dry standard (dscfm) | 108,134 | 103,333 | | 105,778 |
| Q _{std7} | Volumetric flow rate, dry std@7%O ₂ (dscfm) | 84,251 | 82,890 | 83,856 | 83,666 |
| Q, | Volumetric flow rate, actual (acf/hr) | 12,115,652 | 11,586,291 7,796,743 | 11,953,037 | 11,884,993 |
| Q, | Volumetric flow rate, standard (scf/hr) | 8,154,240 6,488,019 | | 8,039,841 | 7,996,941 |
| Q _{std} | Volumetric flow rate, dry standard (dscf/hr) | | 6,200,003 | 6,352,070 338,517 | 6,346,697 |
| Q, | Volumetric flow rate, actual (m ³ /hr) | 343,122 | 328,131 220,808 | 227,693 | 336,590 226,478 |
| Q, | Volumetric flow rate, standard (m ³ /hr) | 230,933 183,745 | 175,588 | 179,894 | 179,742 |
| Q _{std} | Volumetric flow rate, dry standard (dry m ³ /hr) | 143,162 | 140,849 | 179,894 | 142,168 |
| Q _{std7} | Volumetric flow rate, dry std@7%O ₂ (dry m ³ /hr) | 215,187 | 205,753 | 212,169 | 211,036 |
| Q, | Volumetric flow rate, normal (Nm ³ /hr) | 171,216 | 163,616 | 167,629 | 1 67,48 7 |
| Q _{std} | Volumetric flow rate, dry normal (Nm ³ /hr) Volumetric flow rate, dry normal @7%O ₂ (Nm ³ /hr) | 133,401 | 131,246 | 132,777 | 132,474 |
| Q _{std7} | Volumetric now rate, dry normal @7%02 (Nm /m) | 155,401 | 101,240 | 102,771 | 102,414 |
| Samplin | • | | | | |
| V _{metd} | Volume metered, standard (dscf) | 84.1826 | 79.3413 | 82.1102 | 81.8780 |
| %I | Isokinetic sampling (%) | 100.3071 | 98.9302 | 99.9317 | 99.7230 |
| Laborate | | | | | |
| mn | Total matter corrected for allowable blanks (µg) | <0.0500 | <0.0500 | <0.0500 | |
| Berviliu | m Results - Total | | | | |
| C _{sd} | Concentration (lb/dscf) | <1.3097E-12 | <1.3896E-12 | <1.3427E-12 | <1.3473E-12 |
| C _{sd7} | Concentration @7% O2 (lb/dscf) | <1.6809E-12 | <1.7323E-12 | <1.6952E-12 | <1.7028E-12 |
| C _{sd12} | Concentration @12% CO2 (lb/dscf) | <1.6990E-12 | <1.7370E-12 | <1.6819E-12 | <1.7060E-12 |
| C _a | Concentration (lb/acf) | <7.0133E-13 | <7.4358E-13 | <7.1354E-13 | <7.1948E-13 |
| C _{sd} | Concentration (µg/dscm) | <2.0972E-02 | <2.2252E-02 | <2.1502E-02 | <2.1575E-02 |
| C _{sd7} | Concentration @7% O ₂ (µg/dscm) | <2.6917E-02 | <2.7740E-02 | <2.7146E-02 | <2.7268E-02 |
| Csd12 | Concentration @12% CO ₂ (µg/dscm) | <2.7207E-02 | <2.7815E-02 | <2.6933E-02 | <2.7318E-02 |
| C _{sd} | Concentration (mg/dscm) | <2.0972E-05 | <2.2252E-05 | <2.1502E-05 | <2.1575E-05 |
| Csd7 | Concentration @7% O ₂ (mg/dscm) | <2.6917E-05 | <2.7740E-05 | <2.7146E-05 | <2.7268E-05 |
| Csd12 | Concentration @12% CO2 (mg/dscm) | <2.7207E-05 | <2.7815E-05 | <2.6933E-05 | <2.7318E-05 |
| C, | Concentration (µg/m ³ (actual,wet)) | <1.1231E-02 | <1.1907E-02 | <1.1426E-02 | <1.1522E-02 |
| C_{sd} | Concentration (µg/Nm ³ dry) | <2.2507E-02 | <2.3880E-02 | <2.3075E-02 | <2.3154E-02 |
| C _{sd7} | Concentration @7% O ₂ (µg/Nm ³ dry) | <2.8887E-02 | <2.9770E-02 | <2.9132E-02 | <2.9263E-02 |
| C _{sd12} | Concentration @12% CO2 (µg/Nm3 dry) | <2.9198E-02 | <2.9850E-02 | <2.8904E-02 | <2.9317E-02 |
| Elio/hr | Rate (lb/hr) | <8.4971E-06 | <8.6153E-06 | <8.5290E-06 | <8.5471E-06 |
| E _{g/s} | Rate (g/s) | <1.0704E-06 | <1.0853E-06 | <1.0744E-06 | <1.0767E-06 |
| E _{T/yr} | Rate (Ton/yr) | <3.7217E-05 | <3.7735E-05 | <3.7357E-05 | <3.7436E-05 |
| EFd | Rate - Fd-based (Ib/MMBtu) | <2.4187E-08 | <2.4927E-08 | <2.4392E-08 | <2.4502E-08 |
| Erc | Rate - Fc-based (ib/MMBtu) | <2.5768E-08 | <2.6344E-08 | <2.5509E-08 | <2.5874E-08 |
| | | | | | • |

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USEPA Method 5/29 Cadmium (Cd) Emission Parameters

| Run Na |). | 1 | 2 | 3 | Average |
|-------------------|--|------------|-------------|-------------------------------|-------------|
| Date (2 | 010) | Mar 18 | Mar 18 | Mar 18 | |
| | me (approx.) | 07:09 | | | |
| | me (approx.) | 09:22 | | | |
| • | s Conditions | | - | | |
| R _P | Steam Production Rate (Klbs/hour) | 183.9 | 182.9 | 183.9 | 183.6 |
| P ₁ | Fabric Filter Inlet Temperature (°F) | 320 | | 321 | 320.3 |
| Fa | Oxygen-based F-factor (dscf/MMBtu) | 9,570 | | 9,570 | 9,570 |
| Fc | Carbon dioxide-based F-factor (dsc//MMBtu) | 1,820 | | 9,570 1,820 | 1,820 |
| Сар | Capacity factor (hours/year) | 8,760 | 8,760 | 8,760 | 8,760 |
| • | nditions | 6,700 | 6,700 | 0,700 | 8,700 |
| 025 C0 O2 | Oxygen (dry volume %) | 10.0700 | 9.7500 | 9.8900 | 9.9033 |
| CO ₂ | Carbon dioxide (dry volume %) | 9.2500 | 9.6000 | 9.5800 | 9.4767 |
| τ, | Sample temperature (°F) | 307.4800 | 307.6000 | 307.7600 | 307.6133 |
| B _w | Actual water vapor in gas (% by volume) | 20.4338 | 20.4796 | 20.9926 | 20.6353 |
| | | 20.4000 | 20.4750 | 20.0020 | 20.0000 |
| Gas Flo | | 204 000 | 100 105 | 100 017 | 400 000 |
| Q, | Volumetric flow rate, actual (acfm) | 201,928 | 193,105 | 199,217 | 198,083 |
| Q, | Volumetric flow rate, standard (scfm) | 135,904 | 129,946 | 133,997 | 133,282 |
| Q _{std} | Volumetric flow rate, dry standard (dscfm) | 108,134 | 103,333 | 105,868 | 105,778 |
| Q _{std7} | Volumetric flow rate, dry std@7%O ₂ (dscfm) | 84,251 | 82,890 | 83,856 | 83,666 |
| Q, | Volumetric flow rate, actual (acf/hr) | 12,115,652 | 11,586,291 | 11,953,037 | 11,884,993 |
| Q, | Volumetric flow rate, standard (scf/hr) | 8,154,240 | 7,796,743 | 8,039,841 | 7,996,941 |
| Q _{std} | Volumetric flow rate, dry standard (dscf/hr) | 6,488,019 | 6,200,003 | 6,352,070 | 6,346,697 |
| Q, | Volumetric flow rate, actual (m ³ /hr) | 343,122 | 328,131 | 338,517 | 336,590 |
| Q, | Volumetric flow rate, standard (m ³ /hr) | 230,933 | 220,808 | 227,693 | 226,478 |
| Q _{std} | Volumetric flow rate, dry standard (dry m ³ /hr) | 183,745 | 175,588 | 179,894 | 179,742 |
| | Volumetric flow rate, dry std@7%O ₂ (dry m ³ /hr) | 143,162 | 140,849 | 142,492 | 142,168 |
| Q, | Volumetric flow rate, normal (Nm ³ /hr) | 215,187 | 205,753 | 212,169 | 211,036 |
| Q _{std} | Volumetric flow rate, dry normal (Nm ³ /hr) | 171,216 | 163,616 | 167,629 | 167,487 |
| Q _{std7} | Volumetric flow rate, dry normal @7%O ₂ (Nm ³ /hr) | 133,401 | 131,246 | 132,777 | 132,474 |
| Samplin | - | | | | |
| V _{mate} | Volume metered, standard (dscf) | 84.1826 | 79.3413 | 82.1102 | 81.8780 |
| %1 | Isokinetic sampling (%) | 100.3071 | 98.9302 | 99.9317 | 99.7230 |
| Laborate | ory Data | | | | |
| m" | Total matter corrected for allowable blanks (µg) | 0.4679 | <0.2000 | <0.2000 | |
| Cadmiu | m Results - Total | | | | |
| Csd | Concentration (Ib/dscf) | 1.2255E-11 | <5.5583E-12 | <5.3708E-12 | <7.7279E-12 |
| C _{sd7} | Concentration @7% O_2 (lb/dscf) | 1.5729E-11 | <6.9291E-12 | <6.7806E-12 | <9.8128E-12 |
| C _{sd12} | Concentration @12% CO ₂ (lb/dscf) | 1.5898E-11 | <6.9478E-12 | <6.7276E-12 | <9.8578E-12 |
| Ca | Concentration (lb/acf) | 6.5625E-12 | <2.9743E-12 | <2.8542E-12 | <4.1303E-12 |
| C _{sd} | Concentration (µg/dscm) | 1.9624E-01 | <8.9008E-02 | <8.6006E-02 | <1.2375E-01 |
| C _{sd7} | Concentration @7% O_2 (µg/dscm) | 2.5187E-01 | <1.1096E-01 | <1.0858E-01 | <1.5714E-01 |
| C _{sd12} | Concentration @12% CO ₂ (µg/dscm) | 2.5458E-01 | <1.1126E-01 | <1.0773E-01 | <1.5786E-01 |
| C_{sd} | Concentration (mg/dscm) | 1.9624E-04 | <8.9008E-05 | <8.6006E-05 | <1.2375E-04 |
| C _{sd7} | Concentration @7% O ₂ (mg/dscm) | 2.5187E-04 | <1.1096E-04 | <1.0858E-04 | <1.5714E-04 |
| C _{sd12} | Concentration @12% CO ₂ (mg/dscm) | 2.5458E-04 | <1.1126E-04 | <1.0 7 73 E -04 | <1.5786E-04 |
| Ca | Concentration (µg/m ³ (actual,wet)) | 1.0509E-01 | <4.7629E-02 | <4.5705E-02 | <6.6141E-02 |
| C _{sd} | Concentration (µg/Nm ³ dry) | 2.1060E-01 | <9.5521E-02 | <9.2300E-02 | <1.3281E-01 |
| C _{sd7} | Concentration @7% O_2 (µg/Nm ³ dry) | 2.7030E-01 | <1.1908E-01 | <1.1653E-01 | <1.6864E-01 |
| C _{sd12} | Concentration @12% CO ₂ (µg/Nm ³ dry) | 2.7321E-01 | <1.1940E-01 | <1.1562E-01 | <1.6941E-01 |
| Elb/hr | Rate (lb/hr) | 7.9509E-05 | <3.4461E-05 | <3.4116E-05 | <4.9362E-05 |
| E _{g/s} | Rate (g/s) | 1.0016E-05 | <4.3413E-06 | <4.2978E-06 | <6.2184E-06 |
| E _{T/yr} | Rate (Ton/yr) | 3.4825E-04 | <1.5094E-04 | <1.4943E-04 | <2.1621E-04 |
| EFd | Rate - Fd-based (lb/MMBtu) | 2.2632E-07 | <9.9706E-08 | <9.7569E-08 | <1.4120E-07 |
| E _{Fe} | Rate - Fc-based (lb/MMBtu) | 2.4112E-07 | <1.0538E-07 | <1.0203E-07 | <1.4951E-07 |
| | | | | | |

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USEPA Method 5/29 Lead (Pb) Emission Parameters

| Run No. | | 1 | 2 | 3 | Average |
|--------------------|---|--------------|-------------|--------------|-------------|
| Date (20 | 10) | Mar 18 | Mar 18 | Mar 18 | |
| - | ne (approx.) | 07:09 | 09:49 | 12:27 | |
| | ne (approx.) | 09:22 | 12:02 | 14:39 | |
| | | | | | |
| | Conditions | 102.0 | 197.0 | 192.0 | 192 C |
| RP | Steam Production Rate (Klbs/hour) | 183.9 320 | 182.9 | 183.9 321 | 183.6 |
| P1 | Fabric Filter Inlet Temperature (°F) | | 320 | | 320.3 |
| F₀ | Oxygen-based F-factor (dscf/MMBtu) | 9,570 | 9,570 | 9,570 | 9,570 |
| Fc | Carbon dioxide-based F-factor (dscf/MMBtu) | 1,820 | 1,820 | 1,820 | 1,820 |
| Cap | Capacity factor (hours/year) | 8,760 | 8,760 | 8,760 | 8,760 |
| Gas Co | nditions | | | | |
| O2 | Oxygen (dry volume %) | 10.0700 | 9.7500 | 9.8900 | 9.9033 |
| CO₂ | Carbon dioxide (dry volume %) | 9.2500 | 9.6000 | 9.5800 | 9.4767 |
| Τs | Sample temperature (°F) | 307.4800 | 307.6000 | 307.7600 | 307.6133 |
| Bw | Actual water vapor in gas (% by volume) | 20.4338 | 20.4796 | 20.9926 | 20.6353 |
| Gas Flo | w Rate | | | | |
| Q, | Volumetric flow rate, actual (acfm) | 201,928 | 193,105 | 199,217 | 198,083 |
| Qs | Volumetric flow rate, standard (scfm) | 135,904 | 129,946 | 133,997 | 133,282 |
| Q _{std} | Volumetric flow rate, dry standard (dscfm) | 108,134 | 103,333 | 105,868 | 105,778 |
| Q _{std7} | Volumetric flow rate, dry std@7%O2 (dscfm) | 84,251 | 82,890 | 83,856 | 83,666 |
| Q | Volumetric flow rate, actual (acf/hr) | 12,115,652 | 11,586,291 | 11,953,037 | 11,884,993 |
| Q, | Volumetric flow rate, standard (scf/hr) | 8,154,240 | 7,796,743 | 8,039,841 | 7,996,941 |
| Q _{std} | Volumetric flow rate, dry standard (dscf/hr) | 6,488,019 | 6,200,003 | 6,352,070 | 6,346,697 |
| Q, | Volumetric flow rate, actual (m ³ /hr) | 343,122 | 328,131 | 338,517 | 336, 590 |
| Q, | Volumetric flow rate, standard (m ³ /hr) | 230,933 | 220,808 | 227,693 | 226,478 |
| Q _{std} | Volumetric flow rate, dry standard (dry m ³ /hr) | 183,745 | 175,588 | 179,894 | 179,742 |
| Q _{std7} | Volumetric flow rate, dry std@7%O2 (dry m3/hr) | 143,162 | 140,849 | 142,492 | 142,168 |
| Qø | Volumetric flow rate, normal (Nm3/hr) | 215,187 | 205,753 | 212,169 | 211,036 |
| Q _{std} | Volumetric flow rate, dry normal (Nm ³ /hr) | 171,216 | 163,616 | 167,629 | 167,487 |
| Q _{std7} | Volumetric flow rate, dry normal @7%O2 (Nm3/hr) | 133,401 | 131,246 | 132,777 | 132,474 |
| Samplin | | | | | |
| V _{mstd} | Volume metered, standard (dscf) | 84,1826 | 79.3413 | 82,1102 | 81.8780 |
| * msta %l | Isokinetic sampling (%) | 100.3071 | 98.9302 | 99.9317 | 99.7230 |
| | | | | | |
| Laborate | | 0.4400 | -0.0000 | -0.0000 | |
| ma | Total matter corrected for allowable blanks (µg) | 2.4408 | <0.2000 | <0.2000 | |
| Lead Re | sults - Total | | | | |
| Csd | Concentration (lb/dscf) | 6.3931E-11 | <5.5583E-12 | <5.3708E-12 | <2.4953E-11 |
| C _{sd7} | Concentration @7% O ₂ (lb/dscf) | 8.2054E-11 | <6.9291E-12 | <6.7806E-12 | <3.1921E-11 |
| C _{sd12} | Concentration @12% CO ₂ (lb/dscf) | 8.2937E-11 | <6.9478E-12 | <6.7276E-12 | <3.2204E-11 |
| Ca | Concentration (Ib/acf) | 3.4235E-11 | <2.9743E-12 | <2.8542E-12 | <1.3355E-11 |
| C _{sd} | Concentration (µg/dscm) | 1.0238E+00 | <8.9008E-02 | <8.6006E-02 | <3.9959E-01 |
| C _{sd7} | Concentration @7% O ₂ (µg/dscm) | 1.3140E+00 | <1.1096E-01 | <1.0858E-01 | <5.1117E-01 |
| C _{sd12} | Concentration @12% CO ₂ (µg/dscm) | 1.3281E+00 | <1.1126E-01 | <1.0773E-01 | <5.1571E-01 |
| C _{sd} | Concentration (mg/dscm) | 1.0238E-03 | <8.9008E-05 | <8.6006E-05 | <3.9959E-04 |
| C _{sd7} | Concentration @7% O ₂ (mg/dscm) | 1.3140E-03 | <1.1096E-04 | <1.0858E-04 | <5.1117E-04 |
| C _{sd 12} | Concentration @12% CO ₂ (mg/dscm) | 1.3281E-03 | <1.1126E-04 | <1.0773E-04 | <5.1571E-04 |
| Ca | Concentration (µg/m ³ (actual,wet)) | 5.4823E-01 | <4.7629E-02 | <4.5705E-02 | <2.1386E-01 |
| C _{sd} | Concentration (µg/Nm ³ dry) | 1.0987E+00 | <9.5521E-02 | <9.2300E-02 | <4.2883E-01 |
| C _{sd7} | Concentration @7% O ₂ (µg/Nm ³ dry) | 1.4101E+00 | <1.1908E-01 | <1.1653E-01 | <5.4857E-01 |
| C _{sd12} | Concentration @12% CO2 (µg/Nm ³ dry) | 1.4253E+00 | <1.1940E-01 | <1.1562E-01 | <5.5344E-01 |
| Elp/hr | Rate (lb/hr) | 4.1479E-04 | <3.4461E-05 | <3.4116E-05 | <1.6112E-04 |
| E _{g/s} | Rate (g/s) | 5.2253E-05 | <4.3413E-06 | <4.2978E-06 | <2.0297E-05 |
| ET/yr | Rate (Tor/yr) | 1.8168E-03 | <1.5094E-04 | <1.4943E-04 | <7.0571E-04 |
| EFd | Rate - Fd-based (Ib/MMBtu) | 1.1807E-06 | <9.9706E-08 | <9.7569E-08 | <4.5933E-07 |
| EFc | Rate - Fc-based (lb/MMBtu) | 1.2579E-06 | <1.0538E-07 | <1.0203E-07 | <4.8843E-07 |

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USEPA Method 13B (Total Fluorides) Sampling, Velocity and Moisture Parameters

.

| Run No | | 1 | 2 | 3 | Average |
|--------------------|--|------------|------------|-----------------|------------|
| Date (20 | 010) | Mar 18 | Mar 18 | Mar 18 | |
| Start Tin | ne (approx.) | 07:09 | 08:56 | 10:45 | |
| Stop Tin | ne (approx.) | 08:24 | 10:10 | 12:05 | |
| Samolin | g Conditions | | | | |
| Y _d | Dry gas meter correction factor | 0.9898 | 0.9898 | 0.9898 | |
| C, | Pitot tube coefficient | 0.8120 | 0.8120 | 0.8120 | |
| P | Static pressure (in. H ₂ O) | -10.6000 | -10.6000 | -10.6000 | |
| Å | Sample location area (ft ²) | 64.0000 | 64.0000 | 64.0000 | |
| P _{bar} | Barometric pressure (in. Hg) | 30.05 | 30.05 | 30.05 | 30.0500 |
| D, | Nozzle diameter (in.) | 0.2680 | 0.2680 | 0.2680 | |
| O ₂ | Oxygen (dry volume %) | 10.0200 | 9.6400 | 10.1500 | 9.9367 |
| CO₂ | Carbon dioxide (dry volume %) | 9.2900 | 9.5800 | 9.1300 | 9.3333 |
| N ₂ +CC | | 80.6900 | 80.7800 | 80.7200 | 80.7300 |
| Vic | Total Liquid collected (ml) | 212.40 | 209.90 | 201.60 | |
| Vm | Volume metered, meter conditions (ft ³) | 38.0800 | 37.3850 | 38.3650 | |
| Tm | Dry gas meter temperature (°F) | 64.5400 | 73.1600 | 81.1000 | |
| T, | Sample temperature (°F) | 306.2400 | 305.4400 | 305.7200 | 305.8000 |
| ΔH | Meter box orifice pressure drop (in. H_2O) | 1.2560 | 1.1592 | 1.2068 | |
| θ | Total sampling time (min) | 62.5 | 62.5 | 62.5 | |
| Flow Re | sults | | | | |
| V _{wstd} | Volume of water collected (ft ³) | 9.9955 | 9.8779 | 9.4873 | 9.7869 |
| V _{mstd} | Volume metered, standard (dscf) | 38.2069 | 36.8944 | 37.3103 | 37.4705 |
| Ps | Sample gas pressure, absolute (in. Hg) | 29.2706 | 29.2706 | 29.2706 | 29.2706 |
| Pv | Vapor pressure, actual (in. Hg) | 29.2706 | 29.2706 | 29.2706 | 29.2706 |
| Bwo | Moisture measured in sample (% by volume) | 20.7366 | 21.1191 | 20.2730 | 20.7096 |
| Bws | Saturated moisture content (% by volume) | 100.0000 | 100.0000 | 100.0000 | 100.0000 |
| B, | Actual water vapor in gas (% by volume) | 20.7366 | 21.1191 | 20.2730 | 20.7096 |
| V∆P | Velocity head (√in. H₂O) | 0.7304 | 0.7020 | 0.7114 | 0.7146 |
| M _d | MW of sample gas, dry (lb/lb-mole) | 29.8872 | 29.9184 | 29.8668 | 29.8908 |
| Me | MW of sample gas, wet (lb/lb-mole) | 27.4222 | 27.4013 | 27.4610 | 27.4282 |
| V _s | Velocity of sample (ft/sec) | 49.5381 | 47.6055 | 48.2000 | 48.4479 |
| %I | Isokinetic sampling (%) | 98.3144 | 99.1667 | 98.0324 | 98.5045 |
| Qa | Volumetric flow rate, actual (acfm) | 190,226 | 182,805 | 185,088 | 186,040 |
| Q, | Volumetric flow rate, standard (scfm) | 128,236 | 123,362 | 124,857 | 125,485 |
| Q _{std} | Volumetric flow rate, dry standard (dscfm) | 101,644 | 97,309 | 99,545 | 99,499 |
| Q _{std7} | Volumetric flow rate, dry std@7%O ₂ (dscfm) | 79,560 | 78,827 | 76,986 | 78,458 |
| Qa | Volumetric flow rate, actual (acf/hr) | 11,413,588 | 10,968,309 | 11,105,290 | 11,162,396 |
| Q_s | Volumetric flow rate, standard (scf/hr) | 7,694,159 | 7,401,714 | 7,491,412 | 7,529,095 |
| \mathbf{Q}_{std} | Volumetric flow rate, dry standard (dscf/hr) | 6,098,652 | 5,838,538 | 5,972,675 | 5,969,955 |
| Qa | Volumetric flow rate, actual (m ³ /hr) | 323,240 | 310,629 | 314,508 | 316,126 |
| Q, | Volumetric flow rate, standard (m ³ /hr) | 217,903 | 209,621 | 212,161 | 213,228 |
| Q _{std} | Volumetric flow rate, dry standard (dry m ³ /hr) | 172,717 | 165,351 | 169,150 | 169,073 |
| Q _{std7} | Volumetric flow rate, dry std@7%O ₂ (dry m ³ /hr) | 135,192 | 133,946 | 130,817 | 133,318 |
| Q, | Volumetric flow rate, normal (Nm ³ /hr) | 203,046 | 195,329 | 197,696 | 198,690 |
| Q _{std} | Volumetric flow rate, dry normal (Nm ³ /hr) | 160,941 | 154,077 | 157, 617 | 157,545 |
| Q _{std7} | Volumetric flow rate, dry normal @7%O ₂ (Nm ³ /hr) | 125,974 | 124,813 | 121,898 | 124,228 |
| | | | | | |

Comments:

Average includes 3 runs.

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QA/QC _____ Date _____

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USEPA Method 13B HF Parameters

| Run No | | 1 | 2 | 3 | Average |
|-------------------------------------|--|----------------------------|----------------------------|----------------------------|----------------------------|
| Date (20 | 10) | Mar 18 | Mar 18 | Mar 18 | _ |
| | ne (approx.) | 07:09 | 08:56 | 10:45 | |
| | ne (approx.) | 08:24 | 10:10 | 12:05 | |
| - | | 00.24 | 10.10 | 12.00 | |
| | Conditions | 192.0 | 1010 | 400.0 | |
| R _P | Steam Production Rate (Klbs/hour) | 183.9 | 184.2 | 183.0 | 183.7 |
| P ₁ | Fabric Filter Inlet Temperature (°F) | 321 | 320 | 320 | 320 |
| Fd | Oxygen-based F-factor (dscf/MMBtu) | 9,570 | 9,570 | 9,570 | 9,570 |
| F。 | Carbon dioxide-based F-factor (dscf/MMBtu) Capacity factor (hours/year) | 1,820 8, 7 60 | 1,820 | 1,820 | 1,820 |
| Сар | | 5,760 | 8,760 | 8,760 | 8,760 |
| | nditions | | | | |
| 0 ₂ | Oxygen (dry volume %) | 10.0200 | 9.6400 | 10.1500 | 9.9367 |
| CO₂ | Carbon dioxide (dry volume %) | 9.2900 | 9.5800 | 9.1300 | 9.3333 |
| T, | Sample temperature ("F) | 306.2400 | 305.4400 | 305.7200 | 305.8000 |
| B _w | Actual water vapor in gas (% by volume) | 20.7366 | 21.1191 | 20.2730 | 20.7096 |
| Gas Flo | w Rate | | | | |
| Q, | Volumetric flow rate, actual (acfm) | 190,226 | 182,805 | 185,088 | 186,040 |
| Q, | Volumetric flow rate, standard (scfm) | 128,236 | 123,362 | 124,857 | 125,485 |
| Q _{std} | Volumetric flow rate, dry standard (dscfm) | 101,644 | 97,309 | 99,545 | 99,499 |
| Q _{std7} | Volumetric flow rate, dry std@7%O 2 (dscfm) | 79,560 | 78,827 | 76,986 | 78,458 |
| Qa | Volumetric flow rate, actual (acf/hr) | 11,413,588 | 10,968,309 | 11,105,290 | 11,162,396 |
| Q, | Volumetric flow rate, standard (scf/hr) | 7,694,159 | 7,401,714 | 7,491,412 | 7,529,095 |
| Q _{std} | Volumetric flow rate, dry standard (dscf/hr) | 6,098,652 | 5,838,538 | 5,972,675 | 5,969,955 |
| Qa | Volumetric flow rate, actual (m ³ /hr) | 323,240 | 310,629 | 314,508 | 316,126 |
| Q, | Volumetric flow rate, standard (m ³ /hr) | 217,903 | 209,621 | 212,161 | 213,228 |
| Q _{std} | Volumetric flow rate, dry standard (dry m ³ /hr) | 172,717 | 165,351 | 169,150 | 169,073 |
| Q _{std7} | Volumetric flow rate, dry std@7%O 2 (dry m ³ /hr) | 135,192 | 133,946 | 130,817 | 133,318 |
| Q, | Volumetric flow rate, normal (Nm ³ /hr) | 203,046 | 195,329 | 197,696 | 198,690 |
| Q _{std} | Volumetric flow rate, dry normal (Nm ³ /hr) | 160,941 | 154,077 | 157,617 | 157,545 |
| Q _{std7} | Volumetric flow rate, dry normal @7%O $_2$ (Nm ³ /hr) | 125,974 | 124,813 | 121,898 | 124,228 |
| Samplin | g Data | | | | |
| V _{mstd} | Volume metered, standard (dscf) | 38.2069 | 36.8944 | 37.3103 | 37.4705 |
| %! | Isokinetic sampling (%) | 98.3144 | 99.1667 | 98.0324 | 98.5045 |
| Laborate | prv Data | | | | |
| m _n | Total HF collected (mg) | < 0.0360 | <0.0345 | <0.0354 | |
| | | | •••• | | |
| | In Fluoride (HF) Results | <2 0784E.00 | <2 0614E 00 | <2 0005E 00 | <2 0769E 00 |
| C _{ed} C _{sd7} | HF Concentration (lb/dscf) HF Concentration @7% O $_{2}$ (lb/dscf) | <2.0784E-09 | <2.0614E-09 | <2.0905E-09 | <2.0768E-09 |
| - | HF Concentration @12% CO $_2$ (lb/dscf) | <2.6553E-09 <2.6846E-09 | <2.5447 E -09 | <2.7030E-09 | <2.6343E-09 |
| C _{sd12} C _a | HF Concentration (Ib/acf) | <1.1105E-09 | <2.5822E-09 <1.0973E-09 | <2.7476E-09 <1.1243E-09 | <2.6715E-09 <1.1107E-09 |
| C _{sd} | HF Concentration (ppmdv) | <0.0400 | < 0.0397 | <0.0403 | <0.0400 |
| C _{sd} C _{ad7} | HF Concentration (07% O ₂ (ppmdv) | <0.0512 | < 0.0391 | <0.0403 | <0.0508 |
| C _{sd12} | HF Concentration @12% CO ₂ (ppmdv) | < 0.0517 | <0.0498 | <0.0529 | <0.0515 |
| C _w | HF Concentration (ppmwv) | < 0.0317 | < 0.0313 | <0.0321 | <0.0317 |
| C _{sd} | HF Concentration (mg/dscm) | < 0.0333 | < 0.0330 | < 0.0335 | <0.0333 |
| C _{sd} 7 | HF Concentration @7% O ₂ (mg/dscm) | < 0.0425 | <0.0408 | <0.0433 | <0.0422 |
| C _{sd12} | HF Concentration @12% CO 2 (mg/dscm) | < 0.0430 | < 0.0413 | <0.0440 | <0.0428 |
| Ca | HF Concentration (mg/m ³ (actual,wet)) | < 0.0178 | < 0.0176 | < 0.0180 | <0.0178 |
| C _{ed} | HF Concentration (mg/Nm ³ dry) | < 0.0357 | < 0.0354 | < 0.0359 | <0.0357 |
| C _{sd7} | HF Concentration (mg/Nm ³ dry) | < 0.0456 | < 0.0437 | <0.0465 | <0.0453 |
| C _{ed12} | HF Concentration @12% CO 2 (mg/Nm ³ dry) | < 0.0461 | < 0.0444 | <0.0472 | <0.0459 |
| Elp/hr | HF Rate (lb/hr) | < 0.0127 | <0.0120 | <0.0125 | <0.0124 |
| E _{kg/hr} | HF Rate (kg/hr) | < 0.0057 | < 0.0055 | <0.0057 | <0.0056 |
| E _{T/yr} | HF Rate (Ton/yr) | < 0.0555 | <0.0527 | <0.0547 | <0.0543 |
| =,,,, E _{Fd} | HF Rate - Fd-based (lb/MMBtu) | <0.000038 | < 0.000037 | <0.000039 | <0.000038 |
| EFC | HF Rate - Fc-based (lb/MMBtu) | < 0.000041 | < 0.000039 | < 0.000042 | <0.000041 |
| | | | | | |

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USEPA Method 23 (PCDD/F) Sampling, Velocity and Moisture Parameters

| Run No | | 1 | 2 | 3 | Average |
|-------------------|--|------------------|------------|------------|------------|
| Date (20 | 010) | Mar 16 | Mar 17 | Mar 17 | |
| Start Tir | me (approx.) | 08:44 | 06:54 | 12:53 | |
| Stop Tir | ne (approx.) | 13:36 | 12:19 | 17:26 | |
| Samoli | ng Conditions | | | | |
| Yd | Dry gas meter correction factor | ` 0.9901 | 0.9901 | 0.9904 | |
| C, | Pitot tube coefficient | 0.8340 | 0.8340 | 0.8340 | |
| P _g | Static pressure (in. H ₂ O) | -12.0000 | -12.5000 | -10.4000 | |
| As | Sample location area (ft ²) | 64.0000 | 64.0000 | 64.0000 | |
| P _{bar} | Barometric pressure (in. Hg) | 30.00 | 30.00 | 30.00 | 30.0000 |
| Dn | Nozzle diameter (in.) | 0.2640 | 0.2640 | 0.2640 | |
| 0 ₂ | Oxygen (dry volume %) | 9.6800 | 9.7400 | 10.3100 | 9.9100 |
| CO₂ | Carbon dioxide (dry volume %) | 9.7400 | 9.8400 | 9.4700 | 9.6833 |
| N₂+CC | Nitrogen plus carbon monoxide (dry volume %) | 80.5800 | 80.4200 | 80.2200 | 80.4067 |
| V _{ic} | Total Liquid collected (ml) | 836.50 | 943.90 | 896.70 | |
| Vm | Volume metered, meter conditions (ft ³) | 160.3450 | 171.6150 | 166.1550 | |
| Tm | Dry gas meter temperature (°F) | 80.0500 | 74.6100 | 72.3700 | |
| Т | Sample temperature (°F) | 300.6400 | 307.4800 | 307.8400 | 305.3200 |
| ΔH | Meter box orifice pressure drop (in. H ₂ O) | 1.2940 | 1.5220 | 1.3680 | |
| θ | Total sampling time (min) | 250.0 | 250.0 | 250.0 | |
| Flow Re | sults | | | | |
| V _{wstd} | Volume of water collected (ft ³) | 39.3657 | 44.4199 | 42.1987 | 41.9948 |
| V _{mstd} | Volume metered, standard (dscf) | 156.0614 | 168.8240 | 164.1285 | 163.0046 |
| Ps | Sample gas pressure, absolute (in. Hg) | 29.1176 | 29.0809 | 29.2353 | 29.1446 |
| P, | Vapor pressure, actual (in. Hg) | 29.1176 | 29.0809 | 29.2353 | 29.1446 |
| Bwo | Moisture measured in sample (% by volume) | 20.1434 | 20.8306 | 20.4523 | 20.4754 |
| Bws | Saturated moisture content (% by volume) | 100.0000 | 100.0000 | 100.0000 | 100.0000 |
| Bw | Actual water vapor in gas (% by volume) | 20.1434 | 20.8306 | 20.4523 | 20.4754 |
| √∆P | Velocity head (√in. H₂O) | 0.7462 | 0.7983 | 0.7613 | 0.7686 |
| Md | MW of sample gas, dry (lb/lb-mole) | 29.9456 | 29.9640 | 29.9276 | 29.9457 |
| Мs | MW of sample gas, wet (lb/lb-mole) | 27.5393 | 27.4718 | 27.4881 | 27.4998 |
| Vs | Velocity of sample (fl/sec) | 51.8144 | 55.7840 | 53.0548 | 53.5511 |
| %I | Isokinetic sampling (%) | 97.9747 | 100.3189 | 101.5668 | 99.9535 |
| Qa | Volumetric flow rate, actual (acfm) | 198,967 | 214,211 | 203,730 | 205,636 |
| Q_s | Volumetric flow rate, standard (scfm) | 134,410 | 143,237 | 136,888 | 138,178 |
| Q_{std} | Volumetric flow rate, dry standard (dscfm) | 107,335 | 113,400 | 108,891 | 109,875 |
| Q _{std7} | Volumetric flow rate, dry std@7%O ₂ (dscfm) | 86,640 | 91,046 | 82,961 | 86,882 |
| Q _a | Volumetric flow rate, actual (acf/hr) | 11,938,029 | 12,852,643 | 12,223,823 | 12,338,165 |
| Qs | Volumetric flow rate, standard (scf/hr) | 8,064,586 | 8,594,197 | 8,213,270 | 8,290,684 |
| Q _{std} | Volumetric flow rate, dry standard (dscf/hr) | 6,440,103 | 6,803,976 | 6,533,466 | 6,592,515 |
| Qa | Volumetric flow rate, actual (m ³ /hr) | 338,092 | 363,994 | 346,186 | 349,424 |
| Q, | Volumetric flow rate, standard (m ³ /hr) | 228,394 | 243,393 | 232,605 | 234,797 |
| Q _{std} | Volumetric flow rate, dry standard (dry m ³ /hr) | 182,388 | 192,693 | 185,032 | 186,704 |
| Q _{std7} | Volumetric flow rate, dry std@7%O ₂ (dry m ³ /hr) | 147,222 | 154,709 | 140,970 | 147,634 |
| Q, | Volumetric flow rate, normal (Nm ³ /hr) | 212,822 | 226,798 | 216,745 | 218,788 |
| Q _{std} | Volumetric flow rate, dry normal (Nm ³ /hr) | 169,952 | 179,554 | 172,416 | 173,974 |
| Q _{std7} | Volumetric flow rate, dry normal @7%O ₂ (Nm ³ /hr) | 137,184 | 144,160 | 131,359 | 137,568 |
| | | | | | |

Comments:

Average includes 3 runs.

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USEPA Method 23 Parameters (NDs & EMPCs counted as Zero) Total Tetra- through Octa-PCDD/F Results (using USEPA/INTL 1989 TEFs)

| Run No. | | 1 | 2 | 3 | Average |
|---------------------|--|------------|------------|------------|------------|
| | | | | | Attenuge |
| Date (201 | • | Mar 16 | Mar 17 | Mar 17 | |
| | e (approx.) | 08:44 | 06:54 | 12:53 | |
| • | a (approx.) | 13:36 | 12:19 | 17:26 | |
| | Conditions | | | | |
| Rp | Steam Production Rate (Klbs/hour) | 184.1 | 184.3 | 183.9 | 184.1 |
| P, | Fabric Filter Inlet Temperature (°F) | 314 | 321 | 320 | 319 |
| Fd | Oxygen-based F-factor (dscf/MMBtu) | 9,570 | 9,570 | 9,570 | 9,570 |
| F. | Carbon dioxide-based F-factor (dscf/MMBtu) | 1,820 | 1,820 | 1,820 | 1,820 |
| Сар | Capacity factor (hours/year) | 8,760 | 8,760 | 8,760 | 8,760 |
| Gas Con | | | | | |
| O ₂ | Oxygen (dry volume %) | 9.6800 | 9.7400 | 10.3100 | 9.9100 |
| CO2 | Carbon dioxide (dry volume %) | 9.7400 | 9.8400 | 9.4700 | 9.6833 |
| т, | Sample temperature (°F) | 300.6 | 307.5 | 307.8 | 305.3 |
| B, | Actual water vapor in gas (% by volume) | 20.1434 | 20.8306 | 20.4523 | 20.4754 |
| Gas Flow | Rate | | | | |
| Q, | Volumetric flow rate, actual (acfm) | 198,967 | 214,211 | 203,730 | 205,636 |
| Q, | Volumetric flow rate, standard (scfm) | 134,410 | 143,237 | 136,888 | 138,178 |
| Q_{std} | Volumetric flow rate, dry standard (dscfm) | 107,335 | 113,400 | 108,891 | 109,875 |
| Q _{std7} | Volumetric flow rate, dry std@7%O ₂ (dscfm) | 86,640 | 91,046 | 82,961 | 86,882 |
| Q, | Volumetric flow rate, actual (acf/hr) | 11,938,029 | 12,852,643 | 12,223,823 | 12,338,165 |
| Q, | Volumetric flow rate, standard (scf/hr) | 8,064,586 | 8,594,197 | 8,213,270 | 8,290,684 |
| Q _{std} | Volumetric flow rate, dry standard (dscf/hr) | 6,440,103 | 6,803,976 | 6,533,466 | 6,592,515 |
| Q, | Volumetric flow rate, actual (m ³ /hr) | 338,092 | 363,994 | 346,186 | 349,424 |
| Q, | Volumetric flow rate, standard (m ³ /hr) | 228,394 | 243,393 | 232,605 | 234,797 |
| Q _{std} | Volumetric flow rate, dry standard (dry m ³ /hr) | 182,388 | 192,693 | 185,032 | 186,704 |
| | Volumetric flow rate, dry std@7%O2 (dry m³/hr) | 147,222 | 154,709 | 140,970 | 147,634 |
| Q, | Volumetric flow rate, normal (Nm ³ /hr) | 212,822 | 226,798 | 216,745 | 218,788 |
| Q _{atd} | Volumetric flow rate, dry normal (Nm ³ /hr) | 169,952 | 179,554 | 172,416 | 173,974 |
| Q _{std7} | Volumetric flow rate, dry normal @7%O ₂ (Nm ³ /hr) | 137,184 | 144,160 | 131,359 | 137,568 |
| Sampling | Data | • | | | |
| Vmaxd | Volume metered, standard (dscf) | 156.0614 | 168.8240 | 164.1285 | 163.0048 |
| %1 | Isokinetic sampling (%) | 97.9747 | 100.3189 | 101.5668 | 99.9535 |
| Laborato | ry Data from USEPA Method 23 | | | | |
| | Total PCDDs (ng) | 0.41220 | 0.56920 | 0.59770 | |
| | Total PCDFs (ng) | 0.85458 | 0.95310 | 1.07610 | |
| m | Total PCDDs & PCDFs (ng) | 1.26000 | 1.51000 | 1.67000 | |
| m _{n_TEQ} | Total TEQ PCDDs & PCDFs (ng) | 0.01660 | 0.02270 | 0.02700 | |
| Total PCI | DD/F Results (TEF=1) | | | | |
| Cad | PCDD/F Concentration (ng/dscm) | 2.8508E-01 | 3.1582E-01 | 3.5928E-01 | 3.2006E-01 |
| C _{ad7} | PCDD/F Concentration @7% O ₂ (ng/dscm) | 3.5318E-01 | 3.9336E-01 | 4.7157E-01 | 4.0604E-01 |
| C _{ed12} | PCDD/F Concentration @12% CO2 (ng/dscm) | 3.5123E-01 | 3.8515E-01 | 4.5526E-01 | 3.9721E-01 |
| C _{sd} | PCDD/F Concentration (ng/Nm ³ dry) | 3.0594E-01 | 3.3893E-01 | 3.8557E-01 | 3.4348E-01 |
| C _{ad7} | PCDD/F Concentration @7% O2 (ng/Nm ³ dry) | 3.7902E-01 | 4.2214E-01 | 5.0608E-01 | 4.3575E-01 |
| C _{sd12} | PCDD/F Concentration @12% CO2 (ng/Nm ³ dry) | 3.7693E-01 | 4.1333E-01 | 4.8857E-01 | 4.2628E-01 |
| Ether | PCDD/F Rate (lb/hr) | 1.1465E-07 | 1.3419E-07 | 1.4658E-07 | 1.3181E-07 |
| E _{p's} | PCDD/F Rate (g/s) | 1.4443E-08 | 1.6905E-08 | 1.8466E-08 | 1.6605E-08 |
| E _{T/yr} | PCDD/F Rate (Ton/yr) | 5.0217E-07 | 5.8774E-07 | 6.4204E-07 | 5.7732E-07 |
| EFd | PCDD/F Rate - F _d -based (lb/MMBtu) ⁻ | 3.1736E-10 | 3.5346E-10 | 4.2374E-10 | 3.6486E-10 |
| EFc | PCDD/F Rate - F _c -based (lb/MMBtu) | 3.3266E-10 | 3.6478E-10 | 4.3118E-10 | 3.7621E-10 |
| Total PCI | DD/F TEQ Results (using USEPA/INTL 1989 TEFs) | | | | |
| CsdTEQ | TEQ Concentration (ng/dscm) | 3.8011E-03 | 4.7478E-03 | 5.8087E-03 | 4.7859E-03 |
| Cad7TEQ | TEQ Concentration @7% O2 (ng/dscm) | 4.7091E-03 | 5.9134E-03 | 7.6242E-03 | 6.0822E-03 |
| Csd 12TEO | TEQ Concentration @12% CO ₂ (ng/dscm) | 4.6831E-03 | 5.7900E-03 | 7.3605E-03 | 5.9445E-03 |
| Cadifeo | TEQ Concentration (ng/Nm ³ dry) | 4.0792E-03 | 5.0952E-03 | 6.2337E-03 | 5.1360E-03 |
| Csd7TEQ | TEQ Concentration @7% O2 (ng/Nm3 dry) | 5.0536E-03 | 6.3461E-03 | 8.1821E-03 | 6.5273E-03 |
| Csd12TEQ | TEQ Concentration @12% CO2 (ng/Nm ³ dry) | 5.0258E-03 | 6.2136E-03 | 7.8991E-03 | 6.3795E-03 |
| EID/hrteo | TEQ Rate (lb/hr) | 1.5287E-09 | 2.0173E-09 | 2.3699E-09 | 1.9720E-09 |
| E _{g/steo} | TEQ Rate (g/sec) | 1.9258E-10 | 2.5413E-10 | 2.9855E-10 | 2.4842E-10 |
| ET/yr/TEQ | TEQ Rate (Ton/yr) | 6.6956E-09 | 8.8356E-09 | 1.0380E-08 | 8.6371E-09 |
| EFdTED | TEQ Rate - F _d -based (lb/MMBtu) | 4.2314E-12 | 5.3137E-12 | 6.8509E-12 | 5.4653E-12 |
| EFGTEQ | TEQ Rate - F _c -based (lb/MMBtu) | 4.4354E-12 | 5.4837E-12 | 6.9712E-12 | 5.6301E-12 |
| | | | | | |

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> QA/QC _____ Date _____

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USEPA Method 23 Maximum Emissions Parameters (NDs & EMPCs included) Total Tetra- through Octa-PCDD/F Results (TEQ based on USEPA/INTL 1989 TEFs)

| Run No. | | 1 | 2 | 3 | Average |
|---------------------|---|------------|------------|------------|------------|
| Date (20 |)10) | Mar 16 | Mar 17 | Mar 17 | |
| | ne (approx.) | 08:44 | | 12:53 | |
| | ne (approx.) | 13:36 | 12:19 | 17:26 | |
| Process | Conditions | | | | |
| Rp | Production rate - (units/hour) | 184.1 | 184.3 | 183.9 | 184.1 |
| P ₁ | Process data - (units) | 314 | 321 | 320 | 319 |
| Fd | Oxygen-based F-factor (dscf/MMBtu) | 9,570 | 9,570 | 9,570 | 9,570 |
| F. | Carbon dioxide-based F-factor (dscf/MMBtu) | 1,820 | 1,820 | 1,820 | 1,820 |
| Сар | Capacity factor (hours/year) | 8,760 | 8,760 | 8,760 | 8,760 |
| Gas Cor | nditions | | | | |
| O ₂ | Oxygen (dry volume %) | 9.6800 | 9.7400 | 10.3100 | 9.9100 |
| CO ₂ | Carbon dioxide (dry volume %) | 9.7400 | 9.8400 | 9.4700 | 9.6833 |
| T _s | Sample temperature (°F) | 300.6 | 307.5 | 307.8 | 305.3 |
| Bw | Actual water vapor in gas (% by volume) | 20.1434 | 20.8306 | 20.4523 | 20.4754 |
| Gas Flov | w Rate | | | | |
| Q, | Volumetric flow rate, actual (acfm) | 198,967 | 214,211 | 203,730 | 205,636 |
| Q, | Volumetric flow rate, standard (scfm) | 134,410 | 143,237 | 136,888 | 138,178 |
| Q _{std} | Volumetric flow rate, dry standard (dscfm) | 107,335 | 113,400 | 108,891 | 109,875 |
| Q _{std7} | Volumetric flow rate, dry std@7%O2 (dscfm) | 86,640 | 91,046 | 82,961 | 86,882 |
| Q, | Volumetric flow rate, actual (acf/hr) | 11,938,029 | 12,852,643 | 12,223,823 | 12,338,165 |
| Q, | Volumetric flow rate, standard (scf/hr) | 8,064,586 | 8,594,197 | 8,213,270 | 8,290,684 |
| Q _{std} | Volumetric flow rate, dry standard (dscf/hr) | 6,440,103 | 6,803,976 | 6,533,466 | 6,592,515 |
| Q, | Volumetric flow rate, actual (m ³ /hr) | 338,092 | 363,994 | 346,186 | 349,424 |
| Q, | Volumetric flow rate, standard (m ³ /hr) | 228,394 | 243,393 | 232,605 | 234,797 |
| Q _{std} | Volumetric flow rate, dry standard (dry m ³ /hr) | 182,388 | 192,693 | 185,032 | 186,704 |
| Q _{std7} | Volumetric flow rate, dry std@7%O2 (dry m3/hr) | 147,222 | 154,709 | 140,970 | 147,634 |
| Qs | Volumetric flow rate, normal (Nm ³ /hr) | 212,822 | 226,798 | 216,745 | 218,788 |
| Q _{std} | Volumetric flow rate, dry normal (Nm ³ /hr) | 169,952 | 179,554 | 172,416 | 173,974 |
| Q _{atd7} | Volumetric flow rate, dry normal @7%O2 (Nm3/hr) | 137,184 | 144,160 | 131,359 | 137,568 |
| Sampling | g Data | | | | |
| Vmstd | Volume metered, standard (dscf) | 156.0614 | 168.8240 | 164.1285 | 163.0046 |
| % | Isokinetic sampling (%) | 97.9747 | 100.3189 | 101.5668 | 99.9535 |
| Laborato | ry Data from USEPA Method 23, including NDs and EMPCs | | | | |
| m _n | Total PCDDs & PCDFs (ng) | 1.36000 | 1.77000 | 1.86000 | |
| m _{n_TEQ} | | 0.02110 | 0.02750 | 0.03050 | |
| | | | 0.02700 | 0.00000 | |
| C _{ad} | DD/F Results (TEF=1) PCDD/F Concentration (ng/dscm) | 3.0771E-01 | 3.7020E-01 | 4.0015E-01 | 3.5935E-01 |
| C _{ad7} | PCDD/F Concentration @7% O ₂ (ng/dscm) | 3.8121E-01 | 4.6109E-01 | 5.2523E-01 | 4.5584E-01 |
| C _{sd12} | PCDD/F Concentration @12% CO ₂ (ng/dscm) | 3.7911E-01 | 4.5146E-01 | 5.0706E-01 | 4.4588E-01 |
| C _{sd} | PCDD/F Concentration (ng/Nm ³ dry) | 3.3022E-01 | 3.9729E-01 | 4.2943E-01 | 3.8565E-01 |
| C _{ad7} | PCDD/F Concentration @7% O ₂ (ng/Nm ³ dry) | 4.0910E-01 | 4.9483E-01 | 5.6366E-01 | 4.8920E-01 |
| C _{sd12} | PCDD/F Concentration @12% CO ₂ (ng/Nm ³ dry) | 4.0685E-01 | 4.8450E-01 | 5.4416E-01 | 4.7850E-01 |
| Eib/hr | PCDD/F Rate (Ib/hr) | 1.2375E-07 | 1.5729E-07 | 1.6326E-07 | 1.4810E-07 |
| E _{g/s} | PCDD/F Rate (g/s) | 1.5590E-08 | 1.9815E-08 | 2.0567E-08 | 1.8657E-08 |
| E _{T/yr} | PCDD/F Rate (Ton/yr) | 5.4202E-07 | 6.8895E-07 | 7.1508E-07 | 6.4868E-07 |
| E _{Fd} | PCDD/F - F _d -based (lb/MMBtu) | 3.4254E-10 | 4.1433E-10 | 4.7195E-10 | 4.0961E-10 |
| EFG | PCDD/F Rate - Fe-based (lb/MMBtu) | 3.5906E-10 | 4.2759E-10 | 4.8024E-10 | 4.2229E-10 |
| | DD/F TEQ Results (using USEPA/INTL 1989 TEFs) | | | | |
| C _{sdTEQ} | TEQ Concentration (ng/dscm) | 4.7740E-03 | 5.7517E-03 | 6.5617E-03 | 5.6958E-03 |
| | TEQ Concentration @7% O ₂ (ng/dscm) | 5.9143E-03 | 7.1639E-03 | 8.6126E-03 | 7.2303E-03 |
| Caltore | TEQ Concentration @12% CO ₂ (ng/dscm) | 5.8818E-03 | 7.0143E-03 | 8.3147E-03 | 7.0702E-03 |
| | TEQ Concentration (ng/Nm ³ dry) | 5.1233E-03 | 6.1726E-03 | 7.0418E-03 | 6.1126E-03 |
| C _{sd7teq} | TEQ Concentration (ng/tim dry) TEQ Concentration @7% O₂ (ng/Nm ³ dry) | 6.3471E-03 | 7.6880E-03 | 9.2427E-03 | 7.7593E-03 |
| | TEQ Concentration @12% CO ₂ (ng/Nm ³ dry) | 6.3121E-03 | 7.5275E-03 | 8.9231E-03 | 7.5876E-03 |
| | TEQ Rate (lb/hr) | 1.9199E-09 | 2.4438E-09 | 2.6771E-09 | 2.3470E-09 |
| | TEQ Rate (g/sec) | 2.4187E-10 | 3.0786E-10 | 3.3725E-10 | 2.9566E-10 |
| Султео Ет/уптео | TEQ Rate (Ton/yr) | 8.4094E-09 | 1.0704E-08 | 1.1726E-08 | 1.0280E-08 |
| EFdTEQ | TEQ Rate - F _d -based (lb/MMBtu) | 5.3145E-12 | 6.4373E-12 | 7.7390E-12 | 6.4969E-12 |
| EFCTEQ | TEQ Rate - Fc-based (lb/MMBtu) | 5.5707E-12 | 6.6433E-12 | 7.8749E-12 | 6.6963E-12 |
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USEPA Method 26A (HCI) Sampling, Velocity and Moisture Parameters

| Run No. | | 1 | 2 | 3 | Average |
|--------------------|--|----------|----------|----------|----------|
| Date (201 | 10) | Mar 17 | Mar 17 | Mar 17 | |
| Start Tim | e (approx.) | 06:54 | 09:02 | 10:25 | |
| Stop Tim | e (approx.) | 07:54 | 10:02 | 11:25 | |
| Sampling | g Conditions | | | | |
| Yd | Dry gas meter correction factor | 0.9916 | 0.9916 | 0.9916 | |
| Cp | Pitot tube coefficient | 0.8400 | 0.8400 | 0.8400 | |
| Pg | Static pressure (in. H ₂ O) | -1.7000 | -1.9000 | -1.9000 | |
| As | Sample location area (ft ²) | 60.1320 | 60.1320 | 60.1320 | |
| Pbar | Barometric pressure (in. Hg) | 30.00 | 30.00 | 30.00 | 30.0000 |
| O ₂ | Oxygen (dry volume %) | 8.4100 | 9.2900 | 8.6800 | 8.7933 |
| CO₂ | Carbon dioxide (dry volume %) | 10.8600 | 10.1900 | 10.7400 | 10.5967 |
| N ₂ +CO | Nitrogen plus carbon monoxide (dry volume %) | 80.7300 | 80.5200 | 80.5800 | 80.6100 |
| VIc | Total Liquid collected (ml) | 161.80 | 151.20 | 164.00 | |
| Vm | Volume metered, meter conditions (ft ³) | 36.3250 | 36.4700 | 36.2450 | |
| Τm | Dry gas meter temperature (°F) | 72.7917 | 66.8333 | 67.0000 | |
| Τs | Sample temperature (°F) | 509.5000 | 503.5000 | 501.5833 | 504.8611 |
| ΔН | Meter box orifice pressure drop (in. H ₂ O) | 1.1917 | 1.2000 | 1.1917 | |
| θ | Total sampling time (min) | 60.0 | 60.0 | 60.0 | |
| Flow Res | sults | | | | |
| V _{wstd} | Volume of water collected (ft ³) | 7.6143 | 7.1155 | 7.7178 | 7.4825 |
| V _{mstd} | Volume metered, standard (dscf) | 35.8815 | 36.4329 | 36.1960 | 36.1702 |
| Ps | Sample gas pressure, absolute (in. Hg) | 29.8750 | 29.8603 | 29.8603 | 29.8652 |
| Pv | Vapor pressure, actual (in. Hg) | 29.8750 | 29.8603 | 29.8603 | 29.8652 |
| B _{wo} | Moisture measured in sample (% by volume) | 17.5058 | 16.3392 | 17.5750 | 17.1400 |
| B _{ws} | Saturated moisture content (% by volume) | 100.0000 | 100.0000 | 100.0000 | 100.0000 |
| Bw | Actual water vapor in gas (% by volume) | 17.5058 | 16.3392 | 17.5750 | 17.1400 |
| M _d | MW of sample gas, dry (lb/lb-mole) | 30.0740 | 30.0020 | 30.0656 | 30.0472 |
| Ms | MW of sample gas, wet (lb/lb-mole) | 27.9603 | 28.0410 | 27.9451 | 27.9821 |

Comments:

Average includes 3 runs.

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USEPA Method 26A HCI Parameters

| Run No | | 1 | 2 | 3 | Average |
|-------------------|---|-------------------|------------------|-------------------|------------|
| Date (20 | 010) | Mar 17 | Mar 17 | Mar 17 | |
| • | ne (approx.) | 06:54 | 09:02 | 10:25 | |
| | ne (approx.) | 07:54 | 10:02 | 11:25 | |
| Process | s Conditions | | | | |
| R _P | Steam Production Rate (Klbs/hour) | 184.7 | 184.2 | 184.9 | 184.6 |
| P ₁ | Fabric Filter Inlet Temperature (°F) | 323 | 320 | 319 | 321 |
| Fd | Oxygen-based F-factor (dscf/MMBtu) | 9,570 | 9,570 | 9,570 | 9,570 |
| F。 | Carbon dioxide-based F-factor (dscf/MMBtu) | 1,820 | 1,820 | 1,820 | 1,820 |
| Cap | Capacity factor (hours/year) | 8,760 | 8,760 | 8,760 | 8,760 |
| Gas Co | | | | | |
| Oas Co | Oxygen (dry volume %) | 8.4100 | 9.2900 | 8.6800 | 8.7933 |
| | Carbon dioxide (dry volume %) | 10.8600 | 10.1900 | 10.7400 | 10.5967 |
| T _s | Sample temperature (°F) | 509.5000 | 503.5000 | 501.5833 | 504.8611 |
| B _w | Actual water vapor in gas (% by volume) | 17.5058 | 16.3392 | 17.5750 | 17.1400 |
| | | | | | |
| Samplin | - | 35.8815 | 36.4329 | 36,1960 | 36.1702 |
| V_{mstd} | Volume metered, standard (dscf) | 33.0013 | 30.4323 | 30.1300 | 50.1702 |
| | ory Data | | 040 5050 | 0.40.0007 | |
| m'n | Total HCI collected (mg) | 680.9708 | 649.5973 | 646.9267 | |
| Hydroge | en Chloride (HCI) Results | | | | |
| C_{sd} | HCI Concentration (lb/dscf) | 4.1847E-05 | 3.9315E-05 | 3.9410E-05 | 4.0191E-05 |
| C_{sd7} | HCI Concentration @7% O ₂ (lb/dscf) | 4.6571E-05 | 4.7070E-05 | 4.4828E-05 | 4.6156E-05 |
| C _{sd12} | HCI Concentration @12% CO ₂ (lb/dscf) | 4.6240E-05 | 4.6298E-05 | 4.4033E-05 | 4.5524E-05 |
| \mathbf{C}_{sd} | HCI Concentration (ppmdv) | 442.4332 | 415.6619 | 416.6630 | 424.9194 |
| C_{sd7} | HCI Concentration @7% O_2 (ppmdv) | 492.3796 | 497.6486 | 473. 94 56 | 487.9913 |
| C_{sd12} | HCI Concentration @12% CO ₂ (ppmdv) | 488.8764 | 489.493 9 | 465.5453 | 481.3052 |
| C, | HCI Concentration (ppmwv) | 364.9816 | 347.7460 | 343.4346 | 352.0541 |
| C_{sd} | HCI Concentration (mg/dscm) | 670.1238 | 629.5752 | 631.0915 | 643.5968 |
| C_{sd7} | HCI Concentration @7% O ₂ (mg/dscm) | 745.7 7 43 | 753.7550 | 717.8536 | 739.1276 |
| C_{sd12} | HCI Concentration @12% CO ₂ (mg/dscm) | 740.4683 | 741.4036 | 705.1301 | 729.0007 |
| \mathbf{C}_{sd} | HCI Concentration (mg/Nm ³ dry) | 719.1573 | 675.6417 | 677.2689 | 690.6893 |
| C_{sd7} | HCI Concentration @7% O ₂ (mg/Nm ³ dry) | 800.3431 | 808.9078 | 770.3795 | 793.2101 |
| C_{sd12} | HCI Concentration @12% CO ₂ (mg/Nm ³ dry) | 794.6489 | 795.6526 | 756.7250 | 782.3422 |
| E _{Fd} | HCI Rate - Fd-based (lb/MMBtu) | 0.6701 | 0.6773 | 0.6450 | 0.6642 |
| E _{Fc} | HCI Rate - Fc-based (lb/MMBtu) | 0.7013 | 0.7022 | 0.6678 | 0.6904 |

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USEPA Method 26A (HCI) Sampling, Velocity and Moisture Parameters

| Run No. | | 1 | 2 | 3 | Average |
|-------------------|--|----------|----------|----------|----------|
| Date (20 | 10) | Mar 17 | Mar 17 | Mar 17 | |
| Start Tim | e (approx.) | 06:54 | 09:02 | 10:25 | |
| Stop Tim | e (approx.) | 07:54 | 10:02 | 11:25 | |
| Samplin | g Conditions | | | | |
| Yd | Dry gas meter correction factor | 0.9904 | 0.9904 | 0.9904 | |
| Cp | Pitot tube coefficient | 0.8400 | 0.8400 | 0.8400 | |
| Pg | Static pressure (in. H ₂ O) | -12.5000 | -12.5000 | -10.4000 | |
| As | Sample location area (ft ²) | 64.0000 | 64.0000 | 64.0000 | |
| P _{bar} | Barometric pressure (in. Hg) | 30.00 | 30.00 | 30.00 | 30.0000 |
| O ₂ | Oxygen (dry volume %) | 9.6500 | 10.3900 | 9.5300 | 9.8567 |
| CO ₂ | Carbon dioxide (dry volume %) | 9.6500 | 9.1400 | 9.9500 | 9.5800 |
| N₂+CO | Nitrogen plus carbon monoxide (dry volume %) | 80.7000 | 80.4700 | 80.5200 | 80.5633 |
| Vic | Total Liquid collected (ml) | 234.70 | 222.40 | 236.90 | |
| Vm | Volume metered, meter conditions (ft ³) | 41.9500 | 42.0650 | 42.2400 | |
| T _m | Dry gas meter temperature (°F) | 75.1250 | 79.6250 | 85.5417 | |
| Τs | Sample temperature (°F) | 309.4167 | 308.0833 | 307.3333 | 308.2778 |
| ΔH | Meter box orifice pressure drop (in. H ₂ O) | 1.5000 | 1.5000 | 1.5000 | |
| θ | Total sampling time (min) | 60.0 | 60.0 | 60.0 | |
| Flow Res | sults | | | | |
| V _{wstd} | Volume of water collected (ft ³) | 11.0450 | 10.4661 | 11.1485 | 10.8865 |
| V _{mstd} | Volume metered, standard (dscf) | 41.2383 | 41.0065 | 40.7305 | 40.9918 |
| Ps | Sample gas pressure, absolute (in. Hg) | 29.0809 | 29.0809 | 29.2353 | 29.1324 |
| Pv | Vapor pressure, actual (in. Hg) | 29.0809 | 29.0809 | 29.2353 | 29.1324 |
| Bwo | Moisture measured in sample (% by volume) | 21.1253 | 20.3334 | 21.4894 | 20.9827 |
| B _{ws} | Saturated moisture content (% by volume) | 100.0000 | 100.0000 | 100.0000 | 100.0000 |
| Bw | Actual water vapor in gas (% by volume) | 21.1253 | 20.3334 | 21.4894 | 20.9827 |
| M _d | MW of sample gas, dry (lb/lb-mole) | 29.9300 | 29.8780 | 29.9732 | 29.9271 |
| Ms | MW of sample gas, wet (lb/lb-mole) | 27.4098 | 27.4628 | 27.4002 | 27.4243 |

Comments:

Average includes 3 runs.

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USEPA Method 26A HCI Parameters

| Run No | | 1 | 2 | 3 | Average |
|-------------------|---|------------|------------|------------|------------|
| Date (2 | 010) | Mar 17 | Mar 17 | Mar 17 | |
| Start Ti | me (approx.) | 06:54 | 09:02 | 10:25 | |
| Stop Tir | ne (approx.) | 07:54 | 10:02 | 11:25 | |
| Proces | s Conditions | | | | |
| R _P | Steam Production Rate (Klbs/hour) | 184.7 | 184.2 | 184.9 | 184.6 |
| P ₁ | Fabric Filter Inlet Temperature (°F) | 323 | 320 | 319 | 321 |
| Fd | Oxygen-based F-factor (dscf/MMBtu) | 9,570 | 9,570 | 9,570 | 9,570 |
| Fc | Carbon dioxide-based F-factor (dscf/MMBtu) | 1,820 | 1,820 | 1,820 | 1,820 |
| Cap | Capacity factor (hours/year) | 8,760 | 8,760 | 8,760 | 8,760 |
| Gas Co | nditions | | | | |
| O ₂ | Oxygen (dry volume %) | 9.6500 | 10.3900 | 9.5300 | 9.8567 |
| CO₂ | Carbon dioxide (dry volume %) | 9.6500 | 9.1400 | 9.9500 | 9.5800 |
| Ts | Sample temperature (°F) | 309.4167 | 308.0833 | 307.3333 | 308.2778 |
| Bw | Actual water vapor in gas (% by volume) | 21.1253 | 20.3334 | 21.4894 | 20.9827 |
| Samplir | ng Data | | | | |
| V _{mstd} | Volume metered, standard (dscf) | 41.2383 | 41.0065 | 40.7305 | 40.9918 |
| Laborat | ory Data | | | | |
| mn | Total HCl collected (mg) | 29.7475 | 21.2780 | 23.2276 | |
| Hydroge | en Chloride (HCI) Results | | | | |
| C _{sd} | HCI Concentration (lb/dscf) | 1.5906E-06 | 1.1442E-06 | 1.2575E-06 | 1.3307E-06 |
| C_{sd7} | HCI Concentration @7% O ₂ (lb/dscf) | 1.9653E-06 | 1.5132E-06 | 1.5373E-06 | 1.6719E-06 |
| C_{sd12} | HCI Concentration @12% CO ₂ (lb/dscf) | 1.9779E-06 | 1.5022E-06 | 1.5165E-06 | 1.6655E-06 |
| \mathbf{C}_{sd} | HCI Concentration (ppmdv) | 16.8166 | 12.0967 | 13.2946 | 14.0693 |
| C_{sd7} | HCl Concentration @7% O_2 (ppmdv) | 20.7779 | 15.9985 | 16.2528 | 17.6764 |
| C_{sd12} | HCI Concentration @12% CO ₂ (ppmdv) | 20.9119 | 15.8819 | 16.0337 | 17.6092 |
| Cw | HCI Concentration (ppmwv) | 13.2641 | 9.6371 | 10.4377 | 11.1129 |
| C_{sd} | HCI Concentration (mg/dscm) | 25.4710 | 18.3221 | 20.1364 | 21.3099 |
| C_{sd7} | HCl Concentration @7% O_2 (mg/dscm) | 31.4709 | 24.2319 | 24.6171 | 26.7733 |
| C_{sd12} | HCI Concentration @12% CO ₂ (mg/dscm) | 31.6738 | 24.0553 | 24.2851 | 26.6714 |
| C_{sd} | HCI Concentration (mg/Nm ³ dry) | 27.3348 | 19.6627 | 21.6098 | 22.8691 |
| C_{sd7} | HCI Concentration @7% O ₂ (mg/Nm ³ dry) | 33.7736 | 26.0050 | 26.4183 | 28.7323 |
| C_{sd12} | HCI Concentration @12% CO ₂ (mg/Nm ³ dry) | 33.9914 | 25.8154 | 26.0621 | 28.6230 |
| \mathbf{E}_{Fd} | HCI Rate - Fd-based (lb/MMBtu) | 0.0283 | 0.0218 | 0.0221 | 0.0241 |
| E _{Fc} | HCl Rate - Fc-based (lb/MMBtu) | 0.0300 | 0.0228 | 0.0230 | 0.0253 |

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USEPA Method 5/29 (Particulate/Metals) Sampling, Velocity and Moisture Parameters

| Run No. | | 1 | 2 | 3 | Average |
|-----------------------------------|--|-----------------|----------------|------------|------------|
| Date (201 | 0) | Mar 17 | Mar 17 | Mar 17 | |
| Start Time | e (approx.) | 06:50 | 09:26 | 11:59 | |
| Stop Time | approx.) | 09:03 | 11:38 | 14:11 | |
| Sampling | Conditions | | | | |
| Y _d | Dry gas meter correction factor | 0.9898 | 0.9898 | 0.9898 | |
| C, | Pitot tube coefficient | 0.8050 | 0.8050 | 0.8050 | |
| С, P, | Static pressure (in. H ₂ O) | -11.0000 | -11.0000 | -10.3000 | |
| A _s | Sample location area (ft ²) | 64.0000 | 64.0000 | 64.0000 | |
| ∩s P _{bar} | Barometric pressure (in. Hg) | 30.00 | 30.00 | 30.00 | 30.0000 |
| D _n | Nozzle diameter (in.) | 0.2700 | 0.2700 | 0.2700 | |
| O ₂ | Oxygen (dry volume %) | 8.7100 | 8.3000 | 8.7200 | 8.5767 |
| CO ₂ | Carbon dioxide (dry volume %) | 10.4600 | 10.9400 | 10.8400 | 10.7467 |
| - | Nitrogen plus carbon monoxide (dry volume %) | 80.8300 | 80.7600 | 80.4400 | 80.6767 |
| Vic | Total Liquid collected (ml) | 442.10 | 478.40 | 464.40 | 00.07 07 |
| V _{ic} V _m | Volume metered, meter conditions (ft ³) | 72.2900 | 77.9350 | 76.6650 | |
| vm Tm | Dry gas meter temperature (°F) | 75.8000 | 80.2200 | 78.5800 | |
| | Sample temperature (°F) | 303,4400 | 304.0800 | 304.0000 | 303.8400 |
| T₅ ∆H | Meter box orifice pressure drop (in. H ₂ O) | 1.0824 | 1.2396 | 1.2104 | 505.0400 |
| <u>д</u> гі Ө | Total sampling time (min) | 125.0 | 125.0 | 125.0 | |
| 9 | Total sampling (inte (min)) | 125.0 | 125.0 | 120.0 | |
| Flow Res | | | | | |
| V _{watd} | Volume of water collected (ft ³) | 20.8052 | 22.5135 | 21.8547 | 21.7245 |
| V _{mstd} | Volume metered, standard (dscf) | 70.858 7 | 75.7961 | 74.7826 | 73.8125 |
| Ps | Sample gas pressure, absolute (in. Hg) | 29.1912 | 29.1912 | 29.2426 | 29.2083 |
| P, | Vapor pressure, actual (in. Hg) | 29.1912 | 29.1912 | 29.2426 | 29.2083 |
| Bwo | Moisture measured in sample (% by volume) | 22.6973 | 22.9006 | 22.6151 | 22.7377 |
| Bws | Saturated moisture content (% by volume) | 100.0000 | 100.0000 | 100.0000 | 100.0000 |
| Bw | Actual water vapor in gas (% by volume) | 22.6973 | 22.9006 | 22.6151 | 22.7377 |
| √∆P | Velocity head (√in. H₂O) | 0.6736 | 0.7224 | 0.7136 | 0.7032 |
| Md | MW of sample gas, dry (lb/lb-mole) | 30.0220 | 30.0824 | 30.0832 | 30.0625 |
| Ms | MW of sample gas, wet (lb/lb-mole) | 27.2933 | 27.3155 | 27.3506 | 27.3198 |
| Vs | Velocity of sample (fl/sec) | 45.3811 | 48.6680 | 48.0009 | 47.3500 |
| %I | Isokinetic sampling (%) | 100.4415 | 100.5326 | 100.0090 | 100.3277 |
| Qa | Volumetric flow rate, actual (acfm) | 174,264 | 186,885 | 184,323 | 181,824 |
| Q, | Volumetric flow rate, standard (scfm) | 117,586 | 125,997 | 124,502 | 122,695 |
| Q _{std} | Volumetric flow rate, dry standard (dscfm) | 90,897 | 97,143 | 96,346 | 94,795 |
| Q _{std7} | Volumetric flow rate, dry std@7%O ₂ (dscfm) | 79,715 | 88,05 7 | 84,424 | 84,065 |
| Qa | Volumetric flow rate, actual (acf/hr) | 10,455,817 | 11,213,097 | 11,059,399 | 10,909,438 |
| Q, | Volumetric flow rate, standard (scf/hr) | 7,055,162 | 7,559,806 | 7,470,113 | 7,361,694 |
| Q _{std} | Volumetric flow rate, dry standard (dscf/hr) | 5,453,832 | 5,828,564 | 5,780,736 | 5,687,711 |
| Qø | Volumetric flow rate, actual (m ³ /hr) | 296,115 | 317,562 | 313,209 | 308,962 |
| Q, | Volumetric flow rate, standard (m ³ /hr) | 199,806 | 214,098 | 211,558 | 208,488 |
| Q _{std} | Volumetric flow rate, dry standard (dry m3/hr) | 154,456 | 165,068 | 163,714 | 161,079 |
| Q _{std7} | Volumetric flow rate, dry std@7%O ₂ (dry m ³ /hr) | 135,454 | 149,630 | 143,456 | 142,847 |
| Q, | Volumetric flow rate, normal (Nm ³ /hr) | 186,183 | 199,501 | 197,134 | 194,272 |
| Q _{std} | Volumetric flow rate, dry normal (Nm ³ /hr) | 143,925 | 153,814 | 152,552 | 150,097 |
| Q _{std7} | Volumetric flow rate, dry normal @7%O ₂ (Nm ³ /hr) | 126,219 | 139,428 | 133,675 | 133,107 |
| | | | | | |

Comments:

Average includes 3 runs.

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USEPA Method 5/29 Filterable Particulate Parameters

| Run No | | 1 | 2 | 3 | Average |
|---------------------|---|------------------|------------------|------------------|--------------------------|
| Date (20 |)10) | Mar 17 | Mar 17 | Mar 17 | |
| | ne (approx.) | 06:50 | 09:26 | 11:59 | |
| | ne (approx.) | 09:03 | 11:38 | 14:11 | |
| | s Conditions | | | | |
| Rp | Steam Production Rate (Klbs/hour) | 184.2 | 184.2 | 183.5 | 184.0 |
| P ₁ | Fabric Filter Inlet Temperature (°F) | 315 | 315 | 315 | 315 |
| Fa | Oxygen-based F-factor (dscf/MMBtu) | 9,570 | 9,570 | 9,570 | 9,570 |
| F. | Carbon dioxide-based F-factor (dscf/MMBtu) | 1,820 | 1,820 | 1,820 | 1,820 |
| Cap | Capacity factor (hours/year) | 8,760 | 8,760 | 8,760 | 8,760 |
| Gas Co | nditions | | | | |
| 0 ₂ | Oxygen (dry volume %) | 8.7100 | 8.3000 | 8.7200 | 8.5767 |
| CO₂ | Carbon dioxide (dry volume %) | 10.4600 | 10.9400 | 10.8400 | 10.7467 |
| T _s | Sample temperature (°F) | 303.4400 | 304.0800 | 304.0000 | 303.8400 |
| Bw | Actual water vapor in gas (% by volume) | 22.6973 | 22.9006 | 22.6151 | 22.7377 |
| Gas Flo | Poto - | | | | |
| Q, | Volumetric flow rate, actual (acfm) | 174,264 | 186,885 | 184,323 | 181,824 |
| Q, | Volumetric flow rate, standard (scfm) | 117,586 | 125,997 | 124,502 | 122,695 |
| Q _{std} | Volumetric flow rate, dry standard (dscfm) | 90,897 | 97,143 | 96,346 | 94,795 |
| Q _{std7} | Volumetric flow rate, dry std@7%O ₂ (dscfm) | 79,715 | 88,057 | 84,424 | 84,065 |
| Q, | Volumetric flow rate, actual (acf/hr) | 10,455,817 | 11,213,097 | 11,059,399 | 10,909,438 |
| Q, | Volumetric flow rate, standard (scf/hr) | 7,055,162 | 7,559,806 | 7,470,113 | 7,361,694 |
| Q _{std} | Volumetric flow rate, dry standard (dscf/hr) | 5,453,832 | 5,828,564 | 5,780,736 | 5,687,711 |
| Q | Volumetric flow rate, actual (m ³ /hr) | 296,115 | 317,562 | 313,209 | 308,962 |
| Q, | Volumetric flow rate, standard (m ³ /hr) | 199,806 | 214,098 | 211,558 | 208,488 |
| Q _{std} | Volumetric flow rate, dry standard (dry m ³ /hr) | 154,456 | 165,068 | 163,714 | 161,079 |
| Qatd7 | Volumetric flow rate, dry std@7%O2 (dry m3/hr) | 135,454 | 149,630 | 143,456 | 142,847 |
| Qs | Volumetric flow rate, normal (Nm ³ /hr) | 186,183 | 199,501 | 197,134 | 194,272 |
| Q _{std} | Volumetric flow rate, dry normal (Nm ³ /hr) | 143,925 | 153,814 | 152,552 | 150,097 |
| Q _{std7} | Volumetric flow rate, dry normal @7%O2 (Nm3/hr) | 126,219 | 139,428 | 133,675 | 133,107 |
| Samplin | ig Data | | | | |
| V _{mstd} | Volume metered, standard (dscf) | 70.8587 | 75.7961 | 74.7826 | 73.8125 |
| %1 | Isokinetic sampling (%) | 100.4415 | 100.5326 | 100.0090 | 100.3277 |
| Laborate | ory Data | | | | |
| m _{filter} | Matter collected on filter(s) (g) | 0.00040 | <0.00010 | 0.00100 | |
| m, | Matter collected in solvent rinse(s) (g) | 0.00075 | 0.00130 | 0.00123 | |
| m'n | Total particulate matter collected (g) | 0.00115 | 0.00130 | 0.00223 | |
| Filterabl | e Particulate Results | | | | |
| C _{ad} | Particulate Concentration (Ib/dscf) | 3.5708E-08 | 3.7735E-08 | 6.5865E-08 | 4.6436E-08 |
| C _{sd7} | Particulate Concentration @7% O2 (lb/dscf) | 4.0717E-08 | 4.1628E-08 | 7.5166E-08 | 5.2504E-08 |
| C _{ad12} | Particulate Concentration @12% CO ₂ (lb/dscf) | 4.0965E-08 | 4.1391E-08 | 7.2913E-08 | 5.1756E-08 |
| Ca | Particulate Concentration (lb/acf) | 1.8625E-08 | 1.9615E-08 | 3.4428E-08 | 2.4223E-08 |
| Cad | Particulate Concentration (gr/dscf) | 0.0002 | 0.0003 | 0.0005 | 0.0003 |
| Cad7 | Particulate Concentration @7% O ₂ (gr/dscf) | 0.0003 | 0.0003 | 0.0005 | 0.0004 |
| C _{ad12} | Particulate Concentration @12% CO ₂ (gr/dscf) | 0.0003 | 0.0003 | 0.0005 | 0.0004 |
| Ca | Particulate Concentration (gr/acf) | 0.0001 | 0.0001 | 0.0002 | 0.0002 |
| C _{sd} | Particulate Concentration (mg/dscm) | 0.5718 | 0.6043 | 1.0547 | 0.7436 |
| C _{sd7} | Particulate Concentration @7% O ₂ (mg/dscm) | 0.6520 | 0.6666 | 1.2037 | 0.8408 |
| C _{sd12} | Particulate Concentration @12% CO ₂ (mg/dscm) | 0.6560 | 0.6628 | 1.1676 | 0.8288 |
| Ca | Particulate Concentration (mg/m ³ (actual,wet)) | 0.2983 | 0.3141 | 0.5513 | 0.3879 |
| C _{sd} | Particulate Concentration (mg/Nm ³ dry) | 0.6136 | 0.6485 | 1.1319 | 0.7980 |
| C _{sd7} | Particulate Concentration @7% O_2 (mg/Nm ³ dry) | 0.6997 | 0.7154 | 1,2918 | 0.9023 |
| C _{ad12} | Particulate Concentration @12% CO ₂ (mg/Nm ³ dry) | 0.7040 | 0.7113 | 1.2530 | 0.8895 |
| Elb/hr | Particulate Rate (lb/hr) | 0.1947 | 0.2199 | 0.3807 | 0.2651 0.1202 |
| E _{kg/hr} | Particulate Rate (kg/hr) | 0.0883 | 0.0997 | 0.1727 | 1.1613 |
| E _{T/yr} | Particulate Rate (Ton/yr) | 0.8530 | 0.9633 0.0006 | 1.6677 0.0011 | 0.0008 |
| E _{Fd} | Particulate Rate - F _d -based (lb/MMBtu) | 0.0006 0.0006 | 0.0006 | 0.0011 | 0.0008 |
| EFc | Particulate Rate - F _c -based (Ib/MMBtu) | 0.0000 | 0.0000 | 0.0011 | |
| Commen | | | | | 041310 084516 INM @_D |
| Averag | e includes 3 runs. | | | | |

Average includes 3 runs. Prepared by Clean Al: Engineering Proprietary Software 69 EPA 5-1 Version 2008-086

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USEPA Method 5/29 Mercury (Hg) Emission Parameters

| Run No. | | 1 | 2 | 3 | Average |
|--|---|--|--|--|--|
| Date (20 | - | Mar 17 | Mar 17 | Mar 17 | |
| | ne (approx.) | 06:50 | 09:26 | 11:59 | |
| | ne (approx.) | 09:03 | 11:38 | 14:11 | |
| | s Conditions Steam Production Rate (Klbs/hour) | 194.0 | 104.0 | 400 E | 484.0 |
| R _P | | 184.2 | 184.2 | 183.5 | 184.0 |
| P ₁ | Fabric Filter Inlet Temperature (°F) | 315 | 315 | 315 | 315 |
| F. | Oxygen-based F-factor (dscf/MMBtu) | 9,570 | 9,570 | 9,570 | 9,570 |
| F _c Cap | Carbon dloxIde-based F-factor (dscf/MMBtu) Capacity factor (hours/year) | 1,820 8,760 | 1,820 8,760 | 1,820 8,760 | 1,820 8,760 |
| • | nditions | -1 | 0,100 | -,, | 0,700 |
| 0 ₂ | Oxygen (dry volume %) | 8.7100 | 8.3000 | 8.7200 | 8.5767 |
| CO ₂ | Carbon dioxide (dry volume %) | 10.4600 | 10.9400 | 10.8400 | 10.7467 |
| Τ, | Sample temperature (°F) | 303.4400 | 304.0800 | 304.0000 | 303.8400 |
| в" | Actual water vapor in gas (% by volume) | 22.6973 | 22.9006 | 22.6151 | 22.7377 |
| Gas Flo | w Rate | | | | |
| Q, | Volumetric flow rate, actual (acfm) | 174,264 | 186,885 | 184,323 | 181,824 |
| Q, | Volumetric flow rate, standard (scfm) | 117,586 | 125,997 | 124,502 | 122,695 |
| Q _{std} | Volumetric flow rate, dry standard (dscfm) | 90,897 | 97,143 | 96,346 | 94,795 |
| Q _{std7} | Volumetric flow rate, dry std@7%O2 (dscfm) | 79,715 | 88,057 | 84,424 | 84,065 |
| Q, | Volumetric flow rate, actual (acf/hr) | 10,455,817 | 11,213,097 | 11,059,399 | 10,909,438 |
| Qs | Volumetric flow rate, standard (scf/hr) | 7,055,162 | 7,559,806 | 7,470,113 | 7,361,694 |
| Q _{std} | Volumetric flow rate, dry standard (dscf/hr) | 5,453,832 | 5,828,564 | 5,780,736 | 5,687,711 |
| Q, | Volumetric flow rate, actual (m ³ /hr) | 296,115 | 317,562 | 313,209 | 308,962 |
| Q, | Volumetric flow rate, standard (m ³ /hr) | 199,806 | 214,098 | 211,558 | 208,488 |
| Q _{std} | Volumetric flow rate, dry standard (dry m ³ /hr) | 154,456 | 165,068 | 163,714 | 161,079 |
| Q _{std7} | Volumetric flow rate, dry std@7%O2 (dry m3/hr) | 135,454 | 149,630 | 143,456 | 142,847 |
| Q, | Volumetric flow rate, normal (Nm ^{3/hr)} | 186,183 | 199,501 | 197,134 | 194,272 |
| Q _{std} | Volumetric flow rate, dry normal (Nm ³ /hr) | 143,925 | 153,814 | 152,552 | 150,097 |
| Q _{std7} | Volumetric flow rate, dry normal @7%O ₂ (Nm ³ /hr) | 126,219 | 139,428 | 133,675 | 133,107 |
| Samplin | - | | | | |
| V _{mstd} | Volume metered, standard (dscf) | 70.8587 | 75.7961 | 74.7826 | 73.8125 |
| %I | Isokinetic sampling (%) | 100.4415 | 100.5326 | 100.0090 | 100.3277 |
| | ory Data | | | | |
| т _{п-1b} | Fraction 1B (µg) | <0.1000 | <0.1000 | <0.1000 | |
| m _{n-2b} | Fraction 2B (µg) | 8.8257 | 8.9307 | 7.6261 | |
| m _{n-3a} | Fraction 3A (µg) | <0.2000 | <0.2000 | <0.2000 | |
| m _{n-3b} | Fraction 3B (µg) | <0.5000 | <0.5000 | <0.5000 | |
| m _{n-3c} | Fraction 3C (µg) | <0.4000 | <0.4000 | <0.4000 | |
| | | 0.0057 | | | |
| m, | Total matter corrected for allowable blanks (µg) | 8.8257 | 8.9307 | 7.6261 | |
| <i>l</i> ercury | Results - Total | | 8.9307 | 7.6261 | 2 52105 10 |
| Mercury C _{ed} | Results - Total Concentration (Ib/dscf) | 2.7464E-10 | 8.9307 2.5980E-10 | 7.6261 2.2486E-10 | 2.5310E-10 |
| Mercury C _{ad} C _{sd7} | Results - Total Concentration (Ib/dscf) Concentration @7% O ₂ (Ib/dscf) | 2.7464E-10 3.1317E-10 | 8.9307 2.5980E-10 2.8661E-10 | 7.6261 2.2486E-10 2.5661E-10 | 2.8546E-10 |
| Mercury C _{ad} C _{ad7} C _{ad12} | Results - Total Concentration (lb/dscf) Concentration @7% O ₂ (lb/dscf) Concentration @12% CO ₂ (lb/dscf) | 2.7464E-10 3.1317E-10 3.1507E-10 | 8.9307 2.5980E-10 2.8661E-10 2.8498E-10 | 7.6261 2.2486E-10 2.5661E-10 2.4892E-10 | 2.8546E-10 2.8299E-10 |
| fercury C _{ed} C _{sd7} C _{sd12} C _a | Results - Total Concentration (Ib/dscf) Concentration @7% O ₂ (Ib/dscf) Concentration @12% CO ₂ (Ib/dscf) Concentration (Ib/acf) | 2.7464E-10 3.1317E-10 3.1507E-10 1.4325E-10 | 8.9307 2.5980E-10 2.8661E-10 2.8498E-10 1.3505E-10 | 7.6261 2.2486E-10 2.5661E-10 2.4892E-10 1.1753E-10 | 2.8546E-10 2.8299E-10 1.3194E-10 |
| Mercury C _{ed} C _{sd7} C _{ed12} C _a C _{sd} | Results - Total Concentration (Ib/dscf) Concentration @7% O ₂ (Ib/dscf) Concentration @12% CO ₂ (Ib/dscf) Concentration (Ib/acf) Concentration (µg/dscm) | 2.7464E-10 3.1317E-10 3.1507E-10 1.4325E-10 4.3980E+00 | 8.9307 2.5980E-10 2.8661E-10 2.8498E-10 1.3505E-10 4.1604E+00 | 7.6261 2.2486E-10 2.5661E-10 2.4892E-10 1.1753E-10 3.6008E+00 | 2.8546E-10 2.8299E-10 1.3194E-10 4.0531E+00 |
| Mercury C _{ad} C _{ad7} C _{ad12} C _a C _a C _{sd} C _{sd7} | Results - Total Concentration (lb/dscf) Concentration @7% O2 (lb/dscf) Concentration @12% CO2 (lb/dscf) Concentration (lb/acf) Concentration (µg/dscm) Concentration @7% O2 (µg/dscm) | 2.7464E-10 3.1317E-10 3.1507E-10 1.4325E-10 4.3980E+00 5.0149E+00 | 8.9307 2.5980E-10 2.8661E-10 2.8498E-10 1.3505E-10 4.1604E+00 4.5897E+00 | 7.6261 2.2486E-10 2.5661E-10 2.4892E-10 1.1753E-10 3.6008E+00 4.1093E+00 | 2.8546E-10 2.8299E-10 1.3194E-10 4.0531E+00 4.5713E+00 |
| Mercury C _{ad} C _{ad7} C _{ad12} C _a C _{ad} C _{sd7} C _{sd12} | Results - Total Concentration (lb/dscf) Concentration @7% O2 (lb/dscf) Concentration @12% CO2 (lb/dscf) Concentration (lb/acf) Concentration (µg/dscm) Concentration @7% O2 (µg/dscm) Concentration @12% CO2 (µg/dscm) | 2.7464E-10 3.1317E-10 3.1507E-10 1.4325E-10 4.3980E+00 5.0149E+00 5.0455E+00 | 8.9307 2.5980E-10 2.8661E-10 2.8498E-10 1.3505E-10 4.1604E+00 4.5897E+00 4.5635E+00 | 7.6261 2.2486E-10 2.5661E-10 2.4892E-10 1.1753E-10 3.6008E+00 4.1093E+00 3.9861E+00 | 2.8546E-10 2.8299E-10 1.3194E-10 4.0531E+00 4.5713E+00 4.5317E+00 |
| fercury C _{sd} C _{sd7} C _{sd12} C _{sd} C _{sd} C _{sd7} C _{sd12} C _{sd12} C _{sd} | Results - Total Concentration (lb/dscf) Concentration @7% O2 (lb/dscf) Concentration @12% CO2 (lb/dscf) Concentration (lb/acf) Concentration (µg/dscm) Concentration @7% O2 (µg/dscm) Concentration @12% CO2 (µg/dscm) Concentration @12% CO2 (µg/dscm) Concentration @12% CO2 (µg/dscm) | 2.7464E-10 3.1317E-10 3.1507E-10 1.4325E-10 4.3980E+00 5.0149E+00 5.0455E+00 4.3980E-03 | 8.9307 2.5980E-10 2.8661E-10 2.8498E-10 1.3505E-10 4.1604E+00 4.5897E+00 4.5635E+00 4.1604E-03 | 7.6261 2.2486E-10 2.5661E-10 2.4892E-10 1.1753E-10 3.6008E+00 4.1093E+00 3.9861E+00 3.6008E-03 | 2.8546E-10 2.8299E-10 1.3194E-10 4.0531E+00 4.5713E+00 4.5317E+00 4.0531E-03 |
| Nercury C _{sd} C _{sd} 7 C _{sd} 12 C _s C _{sd} 7 C _{sd} 12 C _{sd} 7 C _{sd} 7 | Results - Total Concentration (lb/dscf) Concentration @7% O_2 (lb/dscf) Concentration @12% CO_2 (lb/dscf) Concentration (lb/acf) Concentration (µg/dscm) Concentration @7% O_2 (µg/dscm) Concentration @12% CO_2 (µg/dscm) Concentration @12% CO_2 (µg/dscm) Concentration @7% O_2 (µg/dscm) Concentration @7% O_2 (µg/dscm) | 2.7464E-10 3.1317E-10 3.1507E-10 1.4325E-10 4.3980E+00 5.0149E+00 5.0455E+00 4.3980E-03 5.0149E-03 | 8.9307 2.5980E-10 2.8661E-10 2.8498E-10 1.3505E-10 4.1604E+00 4.5635E+00 4.5635E+00 4.1604E-03 4.5897E-03 | 7.6261 2.2486E-10 2.5661E-10 2.4892E-10 1.1753E-10 3.6008E+00 4.1093E+00 3.9861E+00 3.6008E-03 4.1093E-03 | 2.8546E-10 2.8299E-10 1.3194E-10 4.0531E+00 4.5713E+00 4.5317E+00 4.0531E-03 4.5713E-03 |
| Mercuny C _{sd} C _{sd7} C _{sd12} C _s C _{sd} C _{sd7} C _{sd7} C _{sd7} C _{sd7} C _{sd7} | Results - Total Concentration (lb/dscf) Concentration @7% O_2 (lb/dscf) Concentration @12% CO_2 (lb/dscf) Concentration (lb/acf) Concentration (µg/dscm) Concentration @7% O_2 (µg/dscm) Concentration @12% CO_2 (µg/dscm) Concentration @12% CO_2 (µg/dscm) Concentration @7% O_2 (µg/dscm) Concentration @12% CO_2 (µg/dscm) Concentration @7% O_2 (mg/dscm) Concentration @12% CO_2 (mg/dscm) | 2.7464E-10 3.1317E-10 3.1507E-10 1.4325E-10 4.3980E+00 5.0149E+00 5.0455E+00 4.3980E-03 5.0149E-03 5.0149E-03 5.0455E-03 | 8.9307 2.5980E-10 2.8661E-10 2.8498E-10 1.3505E-10 4.1604E+00 4.5635E+00 4.1604E-03 4.5897E-03 4.5635E-03 | 7.6261 2.2486E-10 2.5661E-10 2.4892E-10 1.1753E-10 3.6008E+00 4.1093E+00 3.9861E+00 3.6008E-03 4.1093E-03 3.9861E-03 | 2.8546E-10 2.8299E-10 1.3194E-10 4.0531E+00 4.5713E+00 4.5317E+00 4.0531E-03 4.5713E-03 4.5317E-03 |
| Aercury C _{od} C _{sd7} C _{sd12} C _{sd} C _{sd7} C _{sd12} C _{sd7} C _{sd7} C _{sd7} C _{sd7} C _{sd7} C _{sd7} C _{sd7} | Results - Total Concentration (lb/dscf) Concentration @7% O_2 (lb/dscf) Concentration @12% CO_2 (lb/dscf) Concentration (lb/acf) Concentration (µg/dscm) Concentration @12% O_2 (µg/dscm) Concentration @12% CO_2 (µg/dscm) Concentration @12% CO_2 (µg/dscm) Concentration @7% O_2 (mg/dscm) Concentration @7% O_2 (mg/dscm) Concentration @12% CO_2 (mg/dscm) Concentration @12% CO_2 (mg/dscm) Concentration @12% CO_2 (mg/dscm) Concentration @12% CO_2 (mg/dscm) | 2.7464E-10 3.1317E-10 3.1507E-10 1.4325E-10 4.3980E+00 5.0149E+00 5.0455E+00 4.3980E-03 5.0149E-03 5.0455E-03 2.2940E+00 | 8.9307 2.5980E-10 2.8661E-10 2.8498E-10 1.3505E-10 4.1604E+00 4.5635E+00 4.1604E-03 4.5635E+00 4.5635E-03 2.1626E+00 | 7.6261 2.2486E-10 2.5661E-10 2.4892E-10 1.1753E-10 3.6008E+00 4.1093E+00 3.9861E+00 3.6008E-03 4.1093E-03 3.9861E-03 1.8821E+00 | 2.8546E-10 2.8299E-10 1.3194E-10 4.0531E+00 4.5713E+00 4.5317E+00 4.0531E-03 4.5713E-03 4.5317E-03 2.1129E+00 |
| Mercury C _{od} C _{sd7} C _{sd12} C _{sd} C _{sd7} C _{sd7} C _{sd7} C _{sd7} C _{sd7} C _{sd7} C _{sd7} C _{sd7} C _{sd7} C _{sd7} | Results - Total Concentration (lb/dscf) Concentration @7% O_2 (lb/dscf) Concentration @12% CO_2 (lb/dscf) Concentration (lb/acf) Concentration (ug/dscm) Concentration @7% O_2 (µg/dscm) Concentration @12% CO_2 (µg/dscm) Concentration @12% CO_2 (µg/dscm) Concentration @7% O_2 (mg/dscm) Concentration @7% O_2 (mg/dscm) Concentration @12% CO_2 (mg/dscm) Concentration @12% CO_2 (mg/dscm) Concentration (µg/m³ (actual,wet)) Concentration (µg/Nm³ dry) | 2.7464E-10 3.1317E-10 3.1507E-10 1.4325E-10 4.3980E+00 5.0149E+00 5.0455E+00 4.3980E-03 5.0149E-03 5.0455E-03 2.2940E+00 4.7198E+00 | 8.9307 2.5980E-10 2.8661E-10 2.8498E-10 1.3505E-10 4.1604E+00 4.5635E+00 4.1604E-03 4.5635E+00 4.5635E-03 2.1626E+00 4.4648E+00 | 7.6261 2.2486E-10 2.5661E-10 2.4892E-10 1.1753E-10 3.6008E+00 4.1093E+00 3.9861E+00 3.6008E-03 4.1093E-03 3.9861E-03 1.8821E+00 3.8643E+00 | 2.8546E-10 2.8299E-10 1.3194E-10 4.0531E+00 4.5713E+00 4.5317E+00 4.0531E-03 4.5713E-03 4.5317E-03 2.1129E+00 4.3496E+00 |
| Aercury C _{sd} C _{sd7} C _{sd12} C _a C _{sd} C _{sd7} C _{sd12} C _{sd7} C _{sd12} C _{sd7} C _{sd7} | Results - Total Concentration (lb/dscf) Concentration @7% O_2 (lb/dscf) Concentration (lb/acf) Concentration @7% O_2 (µg/dscm) Concentration @12% CO2 (µg/dscm) Concentration @12% CO2 (µg/dscm) Concentration @12% CO2 (mg/dscm) Concentration @12% CO2 (mg/dscm) Concentration (µg/m³ (actual,wet)) Concentration (µg/Nm³ dry) Concentration @7% O2 (µg/Nm³ dry) | 2.7464E-10 3.1317E-10 3.1507E-10 1.4325E-10 4.3980E+00 5.0149E+00 5.0455E+00 4.3980E-03 5.0149E-03 5.0455E-03 2.2940E+00 4.7198E+00 5.3819E+00 | 8.9307 2.5980E-10 2.8661E-10 2.8498E-10 1.3505E-10 4.1604E+00 4.5635E+00 4.1604E-03 4.5635E+00 4.5635E-03 2.1626E+00 4.4648E+00 4.9255E+00 | 7.6261 2.2486E-10 2.5661E-10 2.4892E-10 1.1753E-10 3.6008E+00 4.1093E+00 3.9861E+00 3.6008E-03 4.1093E-03 3.9861E-03 1.8821E+00 3.8643E+00 4.4100E+00 | 2.8546E-10 2.8299E-10 1.3194E-10 4.0531E+00 4.5713E+00 4.5317E+00 4.0531E-03 4.5713E-03 4.5317E-03 2.1129E+00 4.3496E+00 4.9058E+00 |
| Hercury C _{od} C _{sd7} C _{sd12} C _{sd7} C _{sd12} | Results - TotalConcentration (lb/dscf)Concentration @7% O_2 (lb/dscf)Concentration @12% CO_2 (lb/dscf)Concentration (lb/acf)Concentration (ug/dscm)Concentration @12% CO_2 (ug/dscm)Concentration @12% CO_2 (ug/dscm)Concentration @12% CO_2 (ug/dscm)Concentration @12% CO_2 (ug/dscm)Concentration @12% CO_2 (ug/dscm)Concentration @12% CO_2 (mg/dscm)Concentration @12% CO_2 (mg/dscm)Concentration (ug/m³ (actual,wet))Concentration (ug/Nm³ dry)Concentration @7% O_2 (ug/Nm³ dry)Concentration @12% CO_2 (ug/Nm³ dry) | 2.7464E-10 3.1317E-10 3.1507E-10 1.4325E-10 4.3980E+00 5.0149E+00 5.0455E+00 4.3980E-03 5.0149E-03 5.0455E-03 2.2940E+00 4.7198E+00 5.3819E+00 5.4147E+00 | 8.9307 2.5980E-10 2.8661E-10 2.8498E-10 1.3505E-10 4.1604E+00 4.5635E+00 4.1604E-03 4.5635E+00 4.5635E-03 2.1626E+00 4.4648E+00 4.9255E+00 4.8974E+00 | 7.6261 2.2486E-10 2.5661E-10 2.4892E-10 1.1753E-10 3.6008E+00 4.1093E+00 3.9861E+00 3.6008E-03 4.1093E-03 3.9861E-03 1.8821E+00 3.8643E+00 4.4100E+00 4.2778E+00 | 2.8546E-10 2.8299E-10 1.3194E-10 4.0531E+00 4.5713E+00 4.5317E+00 4.0531E-03 4.5713E-03 4.5317E-03 2.1129E+00 4.3496E+00 4.9058E+00 4.8633E+00 |
| Aercury C _{8d} C _{3d7} C _{9d12} C ₈ C _{5d7} C _{5d7} | Results - TotalConcentration (lb/dscf)Concentration @7% O_2 (lb/dscf)Concentration @12% CO_2 (lb/dscf)Concentration (lb/acf)Concentration @7% O_2 (µg/dscm)Concentration @12% CO_2 (mg/dscm)Concentration @12% CO_2 (mg/dscm)Concentration @12% CO_2 (µg/dscm)Concentration @12% CO_2 (µg/dscm)Concentration @12% CO_2 (µg/dscm)Concentration @12% CO_2 (µg/Nm³ dry)Concentration @12% CO_2 (µg/Nm³ dry)Concentration @12% CO_2 (µg/Nm³ dry)Rate (lb/hr) | 2.7464E-10 3.1317E-10 3.1507E-10 1.4325E-10 4.3980E+00 5.0149E+00 5.0455E+00 4.3980E-03 5.0149E-03 5.0455E-03 2.2940E+00 4.7198E+00 5.3819E+00 5.4147E+00 1.4978E-03 | 8.9307 2.5980E-10 2.8661E-10 2.8498E-10 1.3505E-10 4.1604E+00 4.5635E+00 4.1604E-03 4.5635E+00 4.1604E-03 4.5635E-03 2.1626E+00 4.4648E+00 4.9255E+00 4.8974E+00 1.5143E-03 | 7.6261 2.2486E-10 2.5661E-10 2.4892E-10 1.1753E-10 3.6008E+00 4.1093E+00 3.9861E+00 3.6008E-03 4.1093E-03 3.9861E-03 1.8821E+00 3.8643E+00 4.4100E+00 4.2778E+00 1.2999E-03 | 2.8546E-10 2.8299E-10 1.3194E-10 4.0531E+00 4.5713E+00 4.5317E+00 4.0531E-03 4.5317E-03 4.5317E-03 2.1129E+00 4.3496E+00 4.9058E+00 4.8633E+00 1.4373E-03 |
| Mercury C _{od} C _{sd7} C _{sd12} C _s C _{sd} C _{sd12} C _{sd2} | Results - TotalConcentration (lb/dscf)Concentration @7% O_2 (lb/dscf)Concentration @12% CO_2 (lb/dscf)Concentration (lb/acf)Concentration (ug/dscm)Concentration @7% O_2 (µg/dscm)Concentration @12% CO_2 (µg/dscm)Concentration @12% CO_2 (µg/dscm)Concentration @7% O_2 (mg/dscm)Concentration @12% CO_2 (µg/Nm3 dry)Concentration @7% O_2 (µg/Nm3 dry)Concentration @12% CO_2 (µg/Nm3 dry)Rate (lb/hr)Rate (g/s) | 2.7464E-10 3.1317E-10 3.1507E-10 1.4325E-10 4.3980E+00 5.0149E+00 5.0455E+00 4.3980E-03 5.0149E-03 5.0455E-03 2.2940E+00 4.7198E+00 5.3819E+00 5.4147E+00 1.4978E-03 1.8869E-04 | 8.9307 2.5980E-10 2.8661E-10 2.8498E-10 1.3505E-10 4.1604E+00 4.5635E+00 4.1604E-03 4.5635E+00 4.1604E-03 4.5635E-03 2.1626E+00 4.4648E+00 4.9255E+00 4.8974E+00 1.5143E-03 1.9076E-04 | 7.6261 2.2486E-10 2.5661E-10 2.4892E-10 1.1753E-10 3.6008E+00 4.1093E+00 3.9861E+00 3.6008E-03 4.1093E-03 3.9861E-03 1.8821E+00 3.8643E+00 4.4100E+00 4.2778E+00 1.2999E-03 1.6375E-04 | 2.8546E-10 2.8299E-10 1.3194E-10 4.0531E+00 4.5713E+00 4.5317E+00 4.0531E-03 4.5713E-03 4.5317E-03 2.1129E+00 4.3496E+00 4.9058E+00 4.8633E+00 1.4373E-03 1.8107E-04 |
| Mercury C _{sd} C _{sd} 7 C _{sd} 12 C _s C _{sd} C _{sd} 7 C _{sd} 12 C _{sd} C _{sd} 7 C _{sd} 12 C _{sd} C _{sd} 12 C _{sd} C _{sd} 12 C _{sd} C _{sd} 7 C _{sd} 12 C _{sd} C _{sd} 7 C br>C _{sd} 7 C C _{sd} 7 C C _{sd} 7 C C C _{sd} 7 C C C C C C C C C C C C C C C C C C C | Results - TotalConcentration (lb/dscf)Concentration @7% O_2 (lb/dscf)Concentration @12% CO_2 (lb/dscf)Concentration (lb/acf)Concentration (lb/acf)Concentration @7% O_2 (µg/dscm)Concentration @12% CO_2 (µg/dscm)Concentration @12% CO_2 (µg/dscm)Concentration @7% O_2 (µg/dscm)Concentration @12% CO_2 (µg/lscm)Concentration @12% CO_2 (µg/lscm)Concentration @12% CO_2 (µg/lscm)Concentration @12% CO_2 (µg/lscm)Rate (lb/hr)Rate (g/s)Rate (Ton/yr) | 2.7464E-10 3.1317E-10 3.1507E-10 1.4325E-10 4.3980E+00 5.0149E+00 5.0455E+00 4.3980E-03 5.0149E-03 5.0455E-03 2.2940E+00 4.7198E+00 5.3819E+00 5.4147E+00 1.4978E-03 1.8869E-04 6.5605E-03 | 8.9307 2.5980E-10 2.8661E-10 2.8498E-10 1.3505E-10 4.1604E+00 4.5635E+00 4.5635E+00 4.1604E-03 4.5635E-03 2.1626E+00 4.4648E+00 4.9255E+00 4.8974E+00 1.5143E-03 1.9076E-04 6.6326E-03 | 7.6261 2.2486E-10 2.5661E-10 2.4892E-10 1.1753E-10 3.6008E+00 3.9861E+00 3.9861E+00 3.6008E-03 4.1093E-03 3.9861E-03 1.8821E+00 3.8643E+00 4.4100E+00 4.2778E+00 1.2999E-03 1.6375E-04 5.6934E-03 | 2.8546E-10 2.8299E-10 1.3194E-10 4.0531E+00 4.5713E+00 4.5317E+00 4.0531E-03 4.5317E-03 2.1129E+00 4.3496E+00 4.9058E+00 4.8633E+00 1.4373E-03 1.8107E-04 6.2955E-03 |
| Mercury C _{sd} C _{sd7} C _{sd12} C _s C _{sd} C _{sd12} C _{sd} C _{sd12} C _{sd} C _{sd12} C _{sd} C _{sd12} C _{sd12} C _{sd12} C _{sd12} C _{sd} C _{sd12} C _{sd} C _{sd12} C _{sd} C _{sd7} C _{sd12} C _{sd} C _{sd7} C _{sd12} C _{sd} C _{sd7} C _{sd12} C _{sd} C _{sd12} C _{sd7} C _{sd12} C _{sd} C _{sd12} C _{sd12} C _{sd} C _{sd12} C _{sd} C _{sd12} C _{sd} C _{sd12} C _{sd12} | Results - TotalConcentration (lb/dscf)Concentration @7% O_2 (lb/dscf)Concentration @12% CO_2 (lb/dscf)Concentration (lb/acf)Concentration (ug/dscm)Concentration @7% O_2 (µg/dscm)Concentration @12% CO_2 (µg/dscm)Concentration @12% CO_2 (µg/dscm)Concentration @7% O_2 (mg/dscm)Concentration @12% CO_2 (µg/Nm3 dry)Concentration @7% O_2 (µg/Nm3 dry)Concentration @12% CO_2 (µg/Nm3 dry)Rate (lb/hr)Rate (g/s) | 2.7464E-10 3.1317E-10 3.1507E-10 1.4325E-10 4.3980E+00 5.0149E+00 5.0455E+00 4.3980E-03 5.0149E-03 5.0455E-03 2.2940E+00 4.7198E+00 5.3819E+00 5.4147E+00 1.4978E-03 1.8869E-04 | 8.9307 2.5980E-10 2.8661E-10 2.8498E-10 1.3505E-10 4.1604E+00 4.5635E+00 4.1604E-03 4.5635E+00 4.1604E-03 4.5635E-03 2.1626E+00 4.4648E+00 4.9255E+00 4.8974E+00 1.5143E-03 1.9076E-04 | 7.6261 2.2486E-10 2.5661E-10 2.4892E-10 1.1753E-10 3.6008E+00 4.1093E+00 3.9861E+00 3.6008E-03 4.1093E-03 3.9861E-03 1.8821E+00 3.8643E+00 4.4100E+00 4.2778E+00 1.2999E-03 1.6375E-04 | 2.8546E-10 2.8299E-10 1.3194E-10 4.0531E+00 4.5713E+00 4.5317E+00 4.0531E-03 4.5317E-03 2.1129E+00 4.3496E+00 4.9058E+00 4.8633E+00 1.4373E-03 1.8107E-04 |

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QA/QC_ Date _ .

USEPA Method 5/29 Beryllium (Be) Emission Parameters

| Run No | | 1 | 2 | 3 | Average |
|-------------------------------------|--|-------------|----------------------------|----------------------------|----------------------------|
| Date (20 | 010) | Mar 17 | Mar 17 | Mar 17 | |
| • | me (approx.) | 06:50 | 09:26 | | |
| | me (approx.) | 09:03 | 11:38 | | |
| | s Conditions | | | | |
| R _P | Steam Production Rate (Klbs/hour) | 184.2 | 184.2 | 183.5 | 184.0 |
| P ₁ | Fabric Filter Inlet Temperature (°F) | 315 | 315 | | 315 |
| Fd | Oxygen-based F-factor (dscf/MMBtu) | 9,570 | 9,570 | 9,570 | 9,570 |
| F | Carbon dioxide-based F-factor (dscf/MMBtu) | 1,820 | 1,820 | 1,820 | 1,820 |
| Сар | Capacity factor (hours/year) | 8,760 | 8,760 | 8,760 | 8,760 |
| | | 0,700 | 0,700 | 0,700 | 0,700 |
| | nditions | | | | |
| O₂ | Oxygen (dry volume %) | 8.7100 | 8.3000 | 8.7200 | 8.5767 |
| CO₂ | Carbon dioxide (dry volume %) | 10.4600 | 10.9400 | 10.8400 | 10.7467 |
| ĩ, | Sample temperature (°F) | 303.4400 | 304.0800 | 304.0000 | 303.8400 |
| B _w | Actual water vapor in gas (% by volume) | 22.6973 | 22.9006 | 22.6151 | 22.7377 |
| Gas Flo | w Rate | | | | |
| Q, | Volumetric flow rate, actual (acfm) | 174,264 | 186,885 | 184,323 | 181,824 |
| Q, | Volumetric flow rate, standard (scfm) | 117,586 | 125,997 | 124,502 | 122,695 |
| Q _{std} | Volumetric flow rate, dry standard (dscfm) | 90,897 | 97,143 | 96,346 | 94,795 |
| Q _{std7} | Volumetric flow rate, dry std@7%O ₂ (dscfm) | 79,715 | 88,057 | 84,424 | 84,065 |
| Q, | Volumetric flow rate, actual (acf/hr) | 10,455,817 | 11,213,097 | 11,059,399 | 10,909,438 |
| Q₅ | Volumetric flow rate, standard (scf/hr) | 7,055,162 | 7,559,806 | 7,470,113 | 7,361,694 |
| Q _{std} | Volumetric flow rate, dry standard (dscf/hr) | 5,453,832 | 5,828,564 | 5,780,736 | 5,687,711 |
| Q, | Volumetric flow rate, actual (m ³ /hr) | 296,115 | 317,562 | 313,209 | 308,962 |
| Q, | Volumetric flow rate, standard (m ³ /hr) | 199,806 | 214,098 | 211,558 | 208,488 |
| Q _{std} | Volumetric flow rate, dry standard (dry m ³ /hr) | 154,456 | 165,068 | 163,714 | 161,079 |
| Q _{std7} | Volumetric flow rate, dry std@7%O ₂ (dry m ³ /hr) | 135,454 | 149,630 | 143,456 | 142,847 |
| Qs | Volumetric flow rate, normal (Nm ³ /hr) | 186,183 | 199,501 | 197,134 | 194,272 |
| Q _{std} | Volumetric flow rate, dry normal (Nm ³ /hr) | 143,925 | 153,814 | 152,552 | 150,097 |
| Q _{std7} | Volumetric flow rate, dry normal @7%O ₂ (Nm ³ /hr) | 126,219 | 139,428 | 133,675 | 133,107 |
| Samplin | ng Data | | | | |
| V _{mstd} | Volume metered, standard (dscf) | 70.8587 | 75.7961 | 74.7826 | 73.8125 |
| %1 | Isokinetic sampling (%) | 100.4415 | 100.5326 | 100.0090 | 100.3277 |
| Laborat | any Doto | | | | |
| Laborate mn | Total matter corrected for allowable blanks (µg) | <0.0500 | <0.0500 | <0.0500 | |
| | | -0.0000 | ~0.0000 | -0.0000 | |
| | m Results - Total | <1.5559E-12 | <1 4548E 10 | <1 4742E 10 | 41 40 40E 40 |
| C _{sd} | Concentration (lb/dscf) | <1.7742E-12 | <1.4546E-12 | <1.4743E-12 | <1.4949E-12 <1.6871E-12 |
| C _{sd7} | Concentration @7% O_2 (lb/dscf) | <1.7850E-12 | <1.6046E-12 <1.5955E-12 | <1.6825E-12 <1.6320E-12 | |
| C _{sd12} C _a | Concentration @12% CO ₂ (lb/dscf) Concentration (lb/acf) | <8.1158E-13 | <7.5608E-12 | <7.7060E-12 | <1.6708E-12 <7.7942E-13 |
| | Concentration (ug/dscm) | <2.4916E-02 | <2.3293E-02 | | <2.3939E-02 |
| C _{sd} | | <2.8411E-02 | <2.5696E-02 | <2.3608E-02 <2.6942E-02 | <2.7016E-02 |
| C _{sd7} | Concentration @7% O ₂ (μ g/dscm) | <2.8584E-02 | <2.5550E-02 | <2.6135E-02 | <2.6756E-02 |
| C _{sd12} | Concentration @12% CO ₂ (µg/dscm) Concentration (mg/dscm) | <2.4916E-05 | <2.3293E-05 | <2.3608E-05 | <2.3939E-05 |
| C _{ed} | | | | _ | |
| Csd7 | Concentration @7% O_2 (mg/dscm) | <2.8411E-05 | <2.5696E-05 | <2.6942E-05 | <2.7016E-05 |
| C _{sd12} | Concentration @12% CO_2 (mg/dscm) | <2.8584E-05 | <2.5550E-05 | <2.6135E-05 | <2.6756E-05 |
| C, | Concentration (µg/m ³ (actual,wet)) | <1.2996E-02 | <1.2108E-02 | <1.2340E-02 | <1.2481E-02 |
| C _{ad} | Concentration ($\mu g/Nm^3 dry$) | <2.6739E-02 | <2.4997E-02 | <2.5336E-02 | <2.5691E-02 |
| C _{sd7} | Concentration @7% O ₂ (μ g/Nm ³ dry) | <3.0490E-02 | <2.7576E-02 | <2.8914E-02 | <2.8993E-02 |
| C _{sd12} | Concentration @12% CO ₂ (µg/Nm ³ dry) | <3.0676E-02 | <2.7419E-02 | <2.8047E-02 | <2.8714E-02 |
| Etevhr | Rate (lb/hr) | <8.4857E-06 | <8.4780E-06 | <8.5224E-06 | <8.4954E-06 |
| E _{g/s} | Rate (g/s) | <1.0690E-06 | <1.0680E-06 | <1.0736E-06 | <1.0702E-06 |
| E _{T/yr} | Rate (Ton/yr) | <3.7167E-05 | <3.7134E-05 | <3.7328E-05 | <3.7210E-05 |
| E _{Fd} | Rate - Fd-based (lb/MMBtu) | <2.5529E-08 | <2.3090E-08 | <2.4210E-08 | <2.4276E-08 <2.5341E-08 |
| EFc | Rate - Fc-based (lb/MMBtu) | <2.7072E-08 | <2.4198E-08 | <2.4753E-08 | -2.33412-00 |

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USEPA Method 5/29 Cadmium (Cd) Emission Parameters

| Run No | | 1 | 2 | 3 | Average |
|--------------------|--|-------------|-------------|-------------|-------------|
| Date (20 | 010) | Mar 17 | Mar 17 | Mar 17 | |
| | ne (approx.) | 06:50 | 09:26 | 11:59 | |
| | ne (approx.) | 09:03 | 11:38 | 14:11 | |
| | s Conditions | | | | |
| R _P | Steam Production Rate (Klbs/hour) | 184.2 | 184.2 | 183.5 | 184.0 |
| P₁ | Fabric Filter Inlet Temperature (°F) | 315 | 315 | 315 | 315 |
| Fa | Oxygen-based F-factor (dscf/MMBtu) | 9,570 | 9,570 | 9,570 | 9,570 |
| F _c | Carbon dioxide-based F-factor (dscf/MMBtu) | 1,820 | 1,820 | 1,820 | 1,820 |
| Сар | Capacity factor (hours/year) | 8,760 | 8,760 | 8,760 | 8,760 |
| | | 0,700 | 0,700 | 8,700 | 8,700 |
| | nditions | | | | |
| O ₂ | Oxygen (dry volume %) | 8.7100 | 8.3000 | 8.7200 | 8.5767 |
| CO ₂ | Carbon dioxide (dry volume %) | 10.4600 | 10.9400 | 10.8400 | 10.7467 |
| T _s | Sample temperature (°F) | 303.4400 | 304.0800 | 304.0000 | 303.8400 |
| B, | Actual water vapor in gas (% by volume) | 22.6973 | 22.9006 | 22.6151 | 22.7377 |
| Gas Flo | w Rate | | | | |
| Q, | Volumetric flow rate, actual (acfm) | 174,264 | 186,885 | 184,323 | 181,824 |
| Q, | Volumetric flow rate, standard (scfm) | 117,586 | 125,997 | 124,502 | 122,695 |
| Q _{std} | Volumetric flow rate, dry standard (dscfm) | 90,897 | 97,143 | 96,346 | 94,795 |
| Q _{std7} | Volumetric flow rate, dry std@7%O ₂ (dscfm) | 79,715 | 88,057 | 84,424 | 84,065 |
| Qa | Volumetric flow rate, actual (acf/hr) | 10,455,817 | 11,213,097 | 11,059,399 | 10,909,438 |
| Q, | Volumetric flow rate, standard (scf/hr) | 7,055,162 | 7,559,806 | 7,470,113 | 7,361,694 |
| Q _{std} | Volumetric flow rate, dry standard (dscf/hr) | 5,453,832 | 5,828,564 | 5,780,736 | 5,687,711 |
| Q, | Volumetric flow rate, actual (m ³ /hr) | 296,115 | 317,562 | 313,209 | 308,962 |
| Q, | Volumetric flow rate, standard (m ³ /hr) | 199,806 | 214,098 | 211,558 | 208,488 |
| Q _{std} | Volumetric flow rate, dry standard (dry m ³ /hr) | 154,456 | 165,068 | 163,714 | 161,079 |
| Q _{std7} | Volumetric flow rate, dry std@7%O ₂ (dry m ³ /hr) | 135,454 | 149,630 | 143,456 | 142,847 |
| Q, | Volumetric flow rate, normal (Nm ³ /hr) | 186,183 | 199,501 | 197,134 | 194,272 |
| Q _{std} | Volumetric flow rate, dry normal (Nm ³ /hr) | 143,925 | 153,814 | 152,552 | 150,097 |
| Q _{std7} | Volumetric flow rate, dry normal @7%O ₂ (Nm ³ /hr) | 126,219 | 139,428 | 133,675 | 133,107 |
| Samplin | g Data | | | | |
| V _{mstd} | Volume metered, standard (dscf) | 70.8587 | 75.7961 | 74.7826 | 73.8125 |
| % | Isokinetic sampling (%) | 100.4415 | 100.5326 | 100.0090 | 100.3277 |
| Laborate | ory Data | | | | |
| mn | Total matter corrected for allowable blanks (µg) | <0.2000 | <0.2000 | <0.2000 | |
| Cadmiu | m Results - Total | | | | |
| C _{sd} | Concentration (lb/dscf) | <6.2236E-12 | <5.8182E-12 | <5.8971E-12 | <5.9797E-12 |
| Csd7 | Concentration @7% O2 (lb/dscf) | <7.0967E-12 | <6.4185E-12 | <6.7299E-12 | <6.7484E-12 |
| C _{sd12} | Concentration @12% CO ₂ (lb/dscf) | <7.1399E-12 | <6.3820E-12 | <6.5281E-12 | <6.6834E-12 |
| C, | Concentration (lb/acf) | <3.2463E-12 | <3.0243E-12 | <3.0824E-12 | <3.1177E-12 |
| C _{sd} | Concentration (µg/dscm) | <9.9663E-02 | <9.3171E-02 | <9.4434E-02 | <9.5756E-02 |
| C _{sd7} | Concentration @7% O2 (µg/dscm) | <1.1364E-01 | <1.0278E-01 | <1.0777E-01 | <1.0807E-01 |
| Csd12 | Concentration @12% CO2 (µg/dscm) | <1.1434E-01 | <1.0220E-01 | <1.0454E-01 | <1.0702E-01 |
| C _{sd} | Concentration (mg/dscm) | <9.9663E-05 | <9.3171E-05 | <9.4434E-05 | <9.5756E-05 |
| Csd7 | Concentration @7% O2 (mg/dscm) | <1.1364E-04 | <1.0278E-04 | <1.0777E-04 | <1.0807E-04 |
| C _{sd12} | Concentration @12% CO ₂ (mg/dscm) | <1.1434E-04 | <1.0220E-04 | <1.0454E-04 | <1.0702E-04 |
| C, | Concentration (µg/m ³ (actual,wet)) | <5.1985E-02 | <4.8430E-02 | <4.9360E-02 | <4.9925E-02 |
| C _{sd} | Concentration (µg/Nm ³ dry) | <1.0696E-01 | <9.9988E-02 | <1.0134E-01 | <1.0276E-01 |
| C _{sd7} | Concentration @7% O_2 (µg/Nm ³ dry) | <1.2196E-01 | <1.1030E-01 | <1.1565E-01 | <1.1597E-01 |
| C _{sd12} | Concentration @12% CO_2 (µg/Nm ³ dry) | <1.2270E-01 | <1.0968E-01 | <1.1219E-01 | <1.1486E-01 |
| E _{lb/hr} | Rate (lb/hr) | <3.3943E-05 | <3.3912E-05 | <3.4090E-05 | <3.3981E-05 |
| E _{g/s} | Rate (g/s) | <4.2760E-06 | <4.2721E-06 | <4.2945E-06 | <4.2809E-06 |
| E _{T/yr} | Rate (Ton/yr) | <1.4867E-04 | <1.4853E-04 | <1.4931E-04 | <1.4884E-04 |
| E _{Fd} | Rate - Fd-based (lb/MMBtu) | <1.0212E-07 | <9.2359E-08 | <9.6839E-08 | <9.7105E-08 |
| EFc | Rate - Fc-based (lb/MMBtu) | <1.0829E-07 | <9.6793E-08 | <9.9010E-08 | <1.0136E-07 |
| | | | | | |

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USEPA Method 5/29 Lead (Pb) Emission Parameters

| Run No | . | 1 | 2 | 3 | Average |
|---------------------------------------|--|---------------------|--------------------------|--------------------------|------------|
| Date (2 | 010) | Mar 17 | Mar 17 | Mar 17 | |
| - | me (approx.) | 06:50 | 09:26 | 11:59 | |
| Stop Ti | me (approx.) | 09:03 | 11:38 | 14:11 | |
| Proces | s Conditions | | | | |
| Rp | Steam Production Rate (Klbs/hour) | 184.2 | 184.2 | 183.5 | 184.0 |
| P ₁ | Fabric Filter Inlet Temperature (°F) | 315 | 315 | 315 | 315 |
| Fd | Oxygen-based F-factor (dscf/MMBtu) | 9,570 | 9,570 | 9,570 | 9,570 |
| Fe | Carbon dioxide-based F-factor (dscf/MMBtu) | 1,820 | 1,820 | 1,820 | 1,820 |
| Сар | Capacity factor (hours/year) | 8,760 | 8,760 | 8,760 | 8,760 |
| • | Inditions | | | -, - | |
| O ₂ | Oxygen (dry volume %) | 8.7100 | 8.3000 | 8.7200 | 8.5767 |
| CO₂ | Carbon dioxide (dry volume %) | 10.4600 | 10.9400 | 10.8400 | 10.7467 |
| T, | Sample temperature (°F) | 303.4400 | 304.0800 | 304.0000 | 303.8400 |
| B, | Actual water vapor in gas (% by volume) | 22.6973 | 22.9006 | 22.6151 | 22.7377 |
| | | 12.00.0 | 22.0000 | 22.0101 | |
| Gas Flo | | 174 264 | 196 995 | 104 222 | 494 924 |
| Q, | Volumetric flow rate, actual (acfm) | 174,264 | 186,885 | 184,323 | 181,824 |
| Q, | Volumetric flow rate, standard (scfm) | 117,586 | 125,997 | 124,502 | 122,695 |
| Q _{std} | Volumetric flow rate, dry standard (dscfm) | 90,897 | 97,143 | 96,346 | 94,795 |
| Q _{std7} | Volumetric flow rate, dry std@7%O ₂ (dscfm) | 79,715 | 88,057 | 84,424 | 84,065 |
| Q, | Volumetric flow rate, actual (acf/hr) | 10,455,817 | 11,213,097 | 11,059,399 | 10,909,438 |
| . Q. | Volumetric flow rate, standard (scf/hr) | 7,055,162 | 7,559,806 | 7,470,113 | 7,361,694 |
| Q _{std} | Volumetric flow rate, dry standard (dscf/hr) | 5,453,832 | 5,828,564 | 5,780,736 | 5,687,711 |
| Q, | Volumetric flow rate, actual (m ³ /hr) | 296,115 | 317,562 | 313,209 | 308,962 |
| Qs | Volumetric flow rate, standard (m ³ /hr) | 199,806 | 214,098 | 211,558 | 208,488 |
| Q _{std} | Volumetric flow rate, dry standard (dry m ³ /hr) | 154,456 | 165,068 | 163,714 | 161,079 |
| Q _{std7} | Volumetric flow rate, dry std@7%O ₂ (dry m ³ /hr) | 135,454 | 149,630 | 143,456 | 142,847 |
| Q۵ | Volumetric flow rate, normal (Nm ³ /hr) | 186,183 | 199,501 | 197,134 | 194,272 |
| Q _{std} | Volumetric flow rate, dry normal (Nm ³ /hr) | 143,925 | 153,814 | 152,552 | 150,097 |
| Q _{std7} | Volumetric flow rate, dry normal @7%O ₂ (Nm ³ /hr) | 126,219 | 139,428 | 133,675 | 133,107 |
| Samplir | ng Data | | | | |
| V _{mstd} | Volume metered, standard (dscf) | 70.8587 | 75.7961 | 74.7826 | 73.8125 |
| %l | Isokinetic sampling (%) | 100.4415 | 100.5326 | 100.0090 | 100.3277 |
| Laborat | ory Data | | | | |
| m _n | Total matter corrected for allowable blanks (µg) | 0.2760 | 0.2230 | 0.3748 | |
| | sulta - Total | | | | |
| C _{sd} | Concentration (Ib/dscf) | 8.5888E-12 | 6.4883E-12 | 1.1052E-11 | 8.7098E-12 |
| C _{sd7} | Concentration @7% O ₂ (lb/dscf) | 9.7937E-12 | 7.1577E-12 | 1.2613E-11 | 9.8548E-12 |
| C _{sd12} | Concentration @12% CO ₂ (lb/dscf) | 9.8533E-12 | 7.1170E-12 | 1.2235E-11 | 9.7351E-12 |
| Ca | Concentration (Ib/acf) | 4.4800E-12 | 3.3726E-12 | 5,7769E-12 | 4.5432E-12 |
| C _{sd} | Concentration (µg/dscm) | 1.3754E-01 | 1.0390E-01 | 1.7698E-01 | 1.3947E-01 |
| C _{sd7} | Concentration @7% O ₂ (µg/dscm) | 1.5683E-01 | 1.1462E-01 | 2.0198E-01 | 1.5781E-01 |
| C _{sd12} | Concentration @12% CO ₂ (µg/dscm) | 1.5779E-01 | 1.1397E-01 | 1.9592E-01 | 1.5589E-01 |
| C _{sd} | Concentration (mg/dscm) | 1.3754E-04 | 1.0390E-04 | 1.7698E-04 | 1.3947E-04 |
| C _{sd} 7 | Concentration @7% O_2 (mg/dscm) | 1.5683E-04 | 1.1462E-04 | 2.0198E-04 | 1.5781E-04 |
| C _{sd7} C _{sd12} | Concentration @12% CO ₂ (mg/dscm) | 1.5779E-04 | 1.1397E-04 | 1.9592E-04 | 1.5589E-04 |
| C _{sd12} C _a | Concentration (µg/m ³ (actual,wet)) | 7.1741E-02 | 5.4008E-02 | 9.2510E-02 | 7.2753E-02 |
| | Concentration (µg/m ⁻ (actual,wet)) Concentration (µg/Nm ³ dry) | 1.4760E-01 | 1.1150E-02 | 9.2510E-02 1.8993E-01 | 1.4968E-01 |
| C _{sd} | | 1.6831E-01 | 1.2301E-01 | 2.1676E-01 | 1.6936E-01 |
| C _{sd7} | Concentration @7% O_2 (µg/Nm ³ dry) | 1.6933E-01 | 1.2301E-01 1.2231E-01 | | 1.6730E-01 |
| C _{sd12} | Concentration @12% CO ₂ (µg/Nm ³ dry) | | | 2.1026E-01 | |
| Elevhr | Rate (lb/hr) | 4.6842E-05 | 3.7817E-05 | 6.3890E-05 | 4.9516E-05 |
| E _{g/s} | Rate (g/s) | 5.9010E-06 | 4.7641E-06 | 8.0486E-06 | 6.2379E-06 |
| E _{T/yr} | Rate (Tor/yr) | 2.0517E-04 | 1.6564E-04 | 2.7984E-04 | 2.1688E-04 |
| EFa | Rate - Fd-based (lb/MMBtu) | 1.4093E-07 | 1.0300E-07 | 1.8149E-07 | 1.4180E-07 |
| Efc | Rate - Fc-based (lb/MMBtu) | 1. 4 944E-07 | 1.0794E-07 | 1.8556E-07 | 1.4765E-07 |

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USEPA Method 13B (Total Fluorides) Sampling, Velocity and Moisture Parameters

| Run No. | 1 | 2 | 3 | Average |
|--|---------------------------|------------|------------|------------------|
| Date (2010) | Mar 16 | Mar 16 | Mar 16 | |
| Start Time (approx.) | 11:49 | 13:33 | 15:07 | |
| Stop Time (approx.) | 13:07 | 14:44 | 16:16 | |
| Sampling Conditions | | | | |
| Y _d Dry gas meter correction factor | 0.9898 | 0.9898 | 0.9898 | |
| C _p Pitot tube coefficient | 0.8120 | 0.8120 | 0.8120 | |
| P _g Static pressure (in. H ₂ O) | -10.6000 | -10.6000 | -10.6000 | |
| A Sample location area (ft ²) | 64.0000 | 64.0000 | 64.0000 | |
| P _{bar} Barometric pressure (in. Hg) | 30.05 | 30.05 | 30.05 | 30.0500 |
| D _n Nozzle diameter (In.) | 0.2680 | 0.2680 | 0.2680 | |
| O ₂ Oxygen (dry volume %) | 9.9000 | 9.5300 | 9.7200 | 9.7167 |
| CO ₂ Carbon dioxide (dry volume %) | 9.7100 | 10.0400 | 9.9600 | 9.9033 |
| N ₂ +CO Nitrogen plus carbon monoxide (dry | volume %) 80.3900 | 80.4300 | 80.3200 | 80.3800 |
| Vic Total Liquid collected (ml) | 204.20 | 213.70 | 209.20 | |
| V _m Volume metered, meter conditions (| (t ³) 36.8000 | 37.7600 | 36.5800 | |
| T _m Dry gas meter temperature (°F) | 71.8000 | 77.1200 | 78.5000 | |
| T _s Sample temperature (°F) | 297.9600 | 299.4400 | 298.8800 | 298.7600 |
| ∆H Meter box orifice pressure drop (in. I | H ₂ O) 1.0948 | 1.1520 | 1.0672 | |
| θ Total sampling time (min) | 62.5 | 62.5 | 62.5 | |
| Flow Results | | | | |
| V _{wetd} Volume of water collected (ft ³) | 9.6097 | 10.0567 | 9.8450 | 9.8371 |
| V _{mstd} Volume metered, standard (dscf) | 36.4042 | 36.9891 | 35.7340 | 36.3758 |
| Ps Sample gas pressure, absolute (in. I | Hg) 29.2706 | 29.2706 | 29.2706 | 29.2706 |
| P, Vapor pressure, actual (in. Hg) | 29.2706 | 29.2706 | 29.2706 | 29.2706 |
| Bwo Moisture measured in sample (% by | volume) 20.8842 | 21.3764 | 21.5998 | 21.2868 |
| Bwe Saturated moisture content (% by vo | olume) 100.0000 | 100.0000 | 100.0000 | 100.0000 |
| B _w Actual water vapor in gas (% by volu | ime) 20.8842 | 21.3764 | 21.5998 | 21.2868 |
| √∆P Velocity head (√in. H₂O) | 0.6713 | 0.6926 | 0.6701 | 0.6780 |
| M _d MW of sample gas, dry (lb/lb-mole) | 29.9496 | 29.9876 | 29.9824 | 29.9732 |
| M _s MW of sample gas, wet (lb/lb-mole) | 27.4540 | 27.4251 | 27.3942 | 27.4244 |
| V _s Velocity of sample (ft/sec) | 45.2598 | 46.7645 | 45.2555 | 45.7599 |
| %I Isokinetic sampling (%) | 101.6122 | 100.7446 | 100.7835 | 101.0467 |
| Q _a Volumetric flow rate, actual (acfm) | 173,798 | 179,576 | 173,781 | 175,718 |
| Q _s Volumetric flow rate, standard (scfm) |) 118,441 | 122,140 | 118,286 | 119,622 |
| Q _{std} Volumetric flow rate, dry standard (d | scfm) 93,705 | 96,031 | 92,736 | 94,158 |
| Q _{std7} Volumetric flow rate, dry std@7%O ₂ | (dscfm) 74,155 | 78,552 | 74,589 | 7 5,766 |
| Q _a Volumetric flow rate, actual (acf/hr) | 10,427,863 | 10,774,535 | 10,426,862 | 10,543,087 |
| Q _s Volumetric flow rate, standard (scf/hi | , , , | 7,328,395 | 7,097,156 | 7,177,334 |
| Q _{std} Volumetric flow rate, dry standard (d | scf/hr) 5,622,323 | 5,761,845 | 5,564,184 | 5,649,451 |
| Q _a Volumetric flow rate, actual (m ³ /hr) | 295,323 | 305,141 | 295,295 | 298,586 |
| Q _s Volumetric flow rate, standard (m ³ /h | • | 207,544 | 200,996 | 203,266 |
| Q _{std} Volumetric flow rate, dry standard (d | • • • | 163,179 | 157,581 | 159,996 |
| Q _{atd7} Volumetric flow rate, dry std@7%O ₂ | , | 133,478 | 126,745 | 128,743 |
| Q _s Volumetric flow rate, normal (Nm ³ /hr | | 193,394 | 187,291 | 1 89,40 7 |
| Q _{std} Volumetric flow rate, dry normal (Nm | ³ /hr) 148,371 | 152,053 | 146,837 | 149,087 |
| Q _{std7} Volumetric flow rate, dry normal @79 | %O₂ (Nm³/hr) 117,416 | 124,377 | 118,103 | 119,965 |
| | | | | |

Comments:

Average includes 3 runs.

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USEPA Method 13B HF Parameters

| Run No | | 1 | 2 | 3 | Average |
|--------------------|--|----------------------|----------------------|----------------------|-------------------------|
| Date (20 | 010) | Mar 16 | Mar 16 | Mar 16 | |
| • • | ne (approx.) | 11:49 | 13:33 | 15:07 | |
| | ne (approx.) | 13:07 | 14:44 | 16:16 | |
| • | Conditions | | | | |
| Rp | Steam Production Rate (Klbs/hour) | 183.7 | 183.9 | 184.2 | 183.9 |
| P ₁ | Fabric Filter Inlet Temperature (°F) | 310 | 310 | 310 | 310 |
| Fd | Oxygen-based F-factor (dscf/MMBtu) | 9,570 | 9,570 | 9,570 | 9,570 |
| F | Carbon dioxide-based F-factor (dscf/MMBtu) | 1,820 | 1,820 | 1,820 | 1,820 |
| Сар | Capacity factor (hours/year) | 8,760 | 8,760 | 8,760 | 8,760 |
| • | | | -, | | -, |
| O2 | nditions Oxygen (dry volume %) | 9.9000 | 9.5300 | 9.7200 | 9.7167 |
| | Carbon dioxide (dry volume %) | 9.7100 | 10.0400 | 9.9600 | 9.9033 |
| T _a | Sample temperature ("F) | 297.9600 | 299.4400 | 298.8800 | 298.7600 |
| 'a Bw | Actual water vapor in gas (% by volume) | 20.8842 | 21.3764 | 21.5998 | 21.2868 |
| | | 20.0012 | 21.07.04 | 21.0000 | |
| Gas Flo | | 472 700 | 470 570 | 470 704 | 475 740 |
| Q, | Volumetric flow rate, actual (acfm) | 173,798 | 179,576 | 173,781 | 175,718 |
| Q, | Volumetric flow rate, standard (scfm) | 118,441 | 122,140 | 118,286 | 119,622 |
| Q _{std} | Volumetric flow rate, dry standard (dscfm) | 93,705 | 96,031 | 92,736 | 94,158 |
| Q _{std7} | Volumetric flow rate, dry std@7%O ₂ (dscfm) | 74,155 10,427,863 | 78,552 10,774,535 | 74,589 10,426,862 | 75,766 |
| Q, | Volumetric flow rate, actual (acf/hr) | 7,106,452 | 7,328,395 | 7,097,156 | 10,543,087 7,177,334 |
| Q, | Volumetric flow rate, standard (scf/hr) | 5,622,323 | 5,761.845 | 5,564,184 | 5,649,451 |
| Q _{std} | Volumetric flow rate, dry standard (dscf/hr) Volumetric flow rate, actual (m ³ /hr) | 295,323 | 305,141 | 295,295 | 298,586 |
| Q_ Q_ | Volumetric flow rate, actuar (m /hr) Volumetric flow rate, standard (m ³ /hr) | 201,259 | 207,544 | 200,996 | 203,266 |
| Q _{atd} | Volumetric flow rate, standard (m //m) Volumetric flow rate, dry standard (dry m ³ /hr) | 159,227 | 163,179 | 157,581 | 159,998 |
| Q _{std7} | Volumetric flow rate, dry standard (dry m 7m) Volumetric flow rate, dry std@7%O 2 (dry m ³ /hr) | 126,007 | 133,478 | 126,745 | 128,743 |
| Q _{std7} | Volumetric flow rate, normal (Nm ³ /hr) | 187,537 | 193,394 | 187,291 | 189,407 |
| Q _{atd} | Volumetric flow rate, dry normal (Nm ³ /hr) | 148,371 | 152,053 | 146,837 | 149,087 |
| Q _{std7} | Volumetric flow rate, dry normal (1411 / 147) Volumetric flow rate, dry normal @7%O 2 (Nm ³ /hr) | 117,416 | 124,377 | 118,103 | 119,965 |
| | · · | , | | | , |
| Samplin | - | 26 4042 | 26 0901 | 25 7240 | 26 2759 |
| Vmstd | Volume metered, standard (dscf) | 36.4042 101.6122 | 36.9891 100.7446 | 35.7340 100.7835 | 36.3758 101.0467 |
| %1 | Isokinetic sampling (%) | 101.0122 | 100.7446 | 100.7835 | 101.0407 |
| Laborato | - | | | | |
| mn | Total HF collected (mg) | <0.0359 | <0.0348 | <0.0326 | |
| Hydroge | n Fluoride (HF) Results | | | | |
| C _{ad} | HF Concentration (Ib/dscf) | <2.1740E-09 | <2.0752E-09 | <2.0123E-09 | <2.0872E-09 |
| C _{ed7} | HF Concentration @7% O ₂ (lb/dscf) | <2.7472E-09 | <2.5370E-09 | <2.5019E-09 | <2.5954E-09 |
| C _{sd12} | HF Concentration @12% CO 2 (lb/dscf) | <2.6867E-09 | <2.4804E-09 | <2.4245E-09 | <2.5305E-09 |
| Ca | HF Concentration (lb/acf) | <1.1721E-09 | <1.1098E-09 | <1.0739E-09 | <1.1186E-09 |
| C _{ad} | HF Concentration (ppmdv) | <0.0419 | <0.0400 | <0.0388 | <0.0402 |
| C _{sd7} | HF Concentration @7% O ₂ (ppmdv) | <0.0529 | <0.0489 | <0.0482 | <0.0500 |
| C _{ed12} | HF Concentration @12% CO 2 (ppmdv) | <0.0518 | <0.0478 | <0.0467 | <0.0488 |
| C, | HF Concentration (ppmwv) | <0.0331 | <0.0314 | < 0.0304 | <0.0317 |
| Cad | HF Concentration (mg/dscm) | <0.0348 | <0.0332 | <0.0322 | <0.0334 |
| C _{ad7} | HF Concentration @7% O_2 (mg/dscm) | <0.0440 | <0.0406 | <0.0401 | <0.0418 |
| C _{sd12} | HF Concentration @12% CO 2 (mg/dscm) | <0.0430 | <0.0397 | <0.0388 | <0.0405 |
| C _a | HF Concentration (mg/m ³ (actual,wet)) | <0.0188 | <0.0178 | < 0.0172 | <0.0179 |
| Ced | HF Concentration (mg/Nm ³ dry) | < 0.0374 | <0.0357 | <0.0346 | <0.0359 |
| C _{ed7} | HF Concentration @7% O ₂ (mg/Nm ³ dry) | <0.0472 | <0.0436 | <0.0430 | <0.0446 |
| C _{ed12} | HF Concentration @12% CO ₂ (mg/Nm ³ dry) | < 0.0462 | < 0.0426 | <0.0417 | < 0.0435 |
| E _{lb/hr} | HF Rate (lb/hr) | <0.0122 | <0.0120 | <0.0112 | <0.0118 |
| E _{kg/hr} | HF Rate (kg/hr) | <0.0055 | <0.0054 | <0.0051 | <0.0053 |
| E _{T/yr} | HF Rate (Ton/yr) | <0.0535 | <0.0524 | <0.0490 | <0.0517 |
| E _{Fd} | HF Rate - Fd-based (lb/MMBtu) | <0.000040 | <0.000037 | <0.000036 | <0.000037 <0.000038 |
| E _{Fc} | HF Rate - Fc-based (lb/MMBtu) | <0.000041 | <0.000038 | <0.000037 | ~0.000030 |

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USEPA Method 26A (HCI) Sampling, Velocity and Moisture Parameters

| Run No. | | 1 | 2 | 3 | Average |
|--------------------|--|----------|----------|----------|----------|
| Date (201 | 10) | Mar 16 | Mar 16 | Mar 16 | |
| Start Time | e (approx.) | 07:17 | 09:04 | 10:32 | |
| Stop Time | e (approx.) | 08:17 | 10:04 | 11:32 | |
| Sampling | g Conditions | | | | |
| Yd | Dry gas meter correction factor | 0.9916 | 0.9916 | 0.9916 | |
| C _p | Pitot tube coefficient | 0.8400 | 0.8400 | 0.8400 | |
| Pg | Static pressure (in. H ₂ O) | -2.1000 | -2.0000 | -2.2000 | |
| As | Sample location area (ft ²) | 60.1320 | 60.1320 | 60.1320 | |
| P _{bar} . | Barometric pressure (in. Hg) | 30.05 | 30.05 | 30.05 | 30.0500 |
| O ₂ | Oxygen (dry volume %) | 8.5900 | 8.2100 | 8.0700 | 8.2900 |
| CO2 | Carbon dioxide (dry volume %) | 10.7200 | 11.0700 | 11.1600 | 10.9833 |
| N₂+CO | Nitrogen plus carbon monoxide (dry volume %) | 80.6900 | 80.7200 | 80.7700 | 80.7267 |
| Vic | Total Liquid collected (ml) | 159.80 | 161.60 | 148.40 | |
| Vm | Volume metered, meter conditions (ft ³) | 35.6100 | 36.2500 | 35.4550 | |
| Tm | Dry gas meter temperature (°F) | 70.4167 | 73.3333 | 77.4167 | |
| Τs | Sample temperature (°F) | 503.1667 | 509.5833 | 508.1667 | 506.9722 |
| ΔH | Meter box orifice pressure drop (in. H ₂ O) | 1.1583 | 1.2000 | 1.1750 | |
| θ | Total sampling time (min) | 60.0 | 60.0 | 60.0 | |
| Flow Res | ults | | | | |
| V _{wstd} | Volume of water collected (ft ³) | 7.5202 | 7.6049 | 6.9837 | 7.3696 |
| V _{mstd} | Volume metered, standard (dscf) | 35.3886 | 35.8313 | 34.7771 | 35.3323 |
| P₅ | Sample gas pressure, absolute (in. Hg) | 29.8956 | 29.9029 | 29.8882 | 29.8956 |
| Pv | Vapor pressure, actual (in. Hg) | 29.8956 | 29.9029 | 29.8882 | 29.8956 |
| Bwo | Moisture measured in sample (% by volume) | 17.5260 | 17.5082 | 16.7231 | 17.2524 |
| B _{ws} | Saturated moisture content (% by volume) | 100.0000 | 100.0000 | 100.0000 | 100.0000 |
| Bw | Actual water vapor in gas (% by volume) | 17.5260 | 17.5082 | 16.7231 | 17.2524 |
| Md | MW of sample gas, dry (lb/lb-mole) | 30.0588 | 30.0996 | 30.1084 | 30.0889 |
| Ms | MW of sample gas, wet (lb/lb-mole) | 27.9454 | 27.9812 | 28.0835 | 28.0034 |

Comments:

Average includes 3 runs.

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Wheelabrator North Broward, Inc. Clean Air Project No: 10955 Unit 3 SDA Inlet

USEPA Method 26A HCI Parameters

| Run No | ». | 1 | 2 | 3 | Average |
|-------------------|---|------------|------------|-------------------|------------|
| Date (2 | 010) | Mar 16 | Mar 16 | Mar 16 | |
| Start Ti | me (approx.) | 07:17 | 09:04 | 10:32 | |
| Stop Tir | me (approx.) | 08:17 | 10:04 | 11:32 | |
| Proces | s Conditions | | | | |
| RP | Steam Production Rate (Klbs/hour) | 184.6 | 184.1 | 184.3 | 184.3 |
| P ₁ | Fabric Filter Inlet Temperature (°F) | 310 | 310 | 310 | 310 |
| Fd | Oxygen-based F-factor (dscf/MMBtu) | 9,570 | 9,570 | 9,570 | 9,570 |
| Fc | Carbon dioxide-based F-factor (dscf/MMBtu) | 1,820 | 1,820 | 1,820 | 1,820 |
| Cap | Capacity factor (hours/year) | 8,760 | 8,760 | 8,760 | 8,760 |
| Gas Co | nditions | | | | |
| O ₂ | Oxygen (dry volume %) | 8.5900 | 8.2100 | 8.0700 | 8.2900 |
| CO₂ | Carbon dioxide (dry volume %) | 10.7200 | 11.0700 | 11.1600 | 10.9833 |
| Ts | Sample temperature (°F) | 503.1667 | 509.5833 | 508.1667 | 506.9722 |
| Bw | Actual water vapor in gas (% by volume) | 17.5260 | 17.5082 | 16.7231 | 17.2524 |
| Samplir | ng Data | | | | |
| V _{mstd} | Volume metered, standard (dscf) | 35.3886 | 35.8313 | 34.7771 | 35.3323 |
| Laborat | ory Data | | | | |
| m _n | Total HCl collected (mg) | 860.2476 | 813.7980 | 9 1 0.7861 | |
| Hydroge | en Chloride (HCI) Results | | | | |
| C _{sd} | HCI Concentration (Ib/dscf) | 5.3600E-05 | 5.0080E-05 | 5.7747E-05 | 5.3809E-05 |
| C _{sd7} | HCI Concentration @7% O ₂ (lb/dscf) | 6.0524E-05 | 5.4855E-05 | 6.2563E-05 | 5.9314E-05 |
| C _{sd12} | HCI Concentration @12% CO ₂ (lb/dscf) | 6.0001E-05 | 5.4287E-05 | 6.2094E-05 | 5.8794E-05 |
| C _{sd} | HCI Concentration (ppmdv) | 566.6961 | 529.4742 | 610.5397 | 568.9033 |
| C _{sd7} | HCI Concentration @7% O ₂ (ppmdv) | 639.8925 | 579.9599 | 661.4577 | 627.1033 |
| C _{sd12} | HCI Concentration @12% CO ₂ (ppmdv) | 634.3613 | 573.9557 | 656.4943 | 621.6038 |
| Cw | HCI Concentration (ppmwv) | 467.3771 | 436.7727 | 508.4384 | 470.8627 |
| C_{sd} | HCI Concentration (mg/dscm) | 858.3366 | 801.9589 | 924.7435 | 861.6797 |
| C _{sd7} | HCI Concentration @7% O ₂ (mg/dscm) | 969.2021 | 878.4263 | 1001.8656 | 949.8313 |
| C _{sd12} | HCI Concentration @12% CO ₂ (mg/dscm) | 960.8245 | 869.3322 | 994.3479 | 941.5015 |
| C_{sd} | HCI Concentration (mg/Nm ³ dry) | 921.1417 | 860.6389 | 992.4077 | 924.7294 |
| C_{sd7} | HCI Concentration @7% O ₂ (mg/Nm ³ dry) | 1040.1194 | 942.7014 | 1075.1728 | 1019.3312 |
| C _{sd12} | HCI Concentration @12% CO ₂ (mg/Nm ³ dry) | 1031.1288 | 932.9419 | 1067.1051 | 1010.3919 |
| E _{Fd} | HCI Rate - Fd-based (lb/MMBtu) | 0.8709 | 0.7893 | 0.9003 | 0.8535 |
| E_{Fc} | HCI Rate - Fc-based (Ib/MMBtu) | 0.9100 | 0.8234 | 0.9418 | 0.8917 |

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USEPA Method 26A (HCI) Sampling, Velocity and Moisture Parameters

| Run No. | | 1 | 2 | 3 | Average |
|--------------------|---|----------|----------|----------|----------|
| Date (201 | 10) | Mar 16 | Mar 16 | Mar 16 | |
| Start Tim | e (approx.) | 07:17 | 09:04 | 10:32 | |
| Stop Tim | e (approx.) | 08:17 | 10:04 | 11:32 | |
| Sampling | g Conditions | | | | |
| Yd | Dry gas meter correction factor | 0.9892 | 0.9892 | 0.9892 | |
| Cp | Pitot tube coefficient | 0.8400 | 0.8400 | 0.8400 | |
| Pg | Static pressure (in. H ₂ O) | -10.4000 | -11.2000 | -10.7000 | |
| As | Sample location area (ft ²) | 64.0000 | 64.0000 | 64.0000 | |
| Pbar | Barometric pressure (in. Hg) | 30.05 | 30.05 | 30.05 | 30.0500 |
| O ₂ | Oxygen (dry volume %) | 9.0300 | 9.1000 | 8.9200 | 9.0167 |
| CO ₂ | Carbon dioxide (dry volume %) | 10.2700 | 10.2200 | 10.3800 | 10.2900 |
| N ₂ +CO | Nitrogen plus carbon monoxide (dry volume %) | 80.7000 | 80.6800 | 80.7000 | 80.6933 |
| Vic | Total Liquid collected (ml) | 235.50 | 240.70 | 247.10 | |
| Vm | Volume metered, meter conditions (ft ³) | 41.3400 | 41.3400 | 41.6050 | |
| Τm | Dry gas meter temperature (°F) | 56.3750 | 60.7083 | 65.4583 | |
| Τs | Sample temperature (°F) | 299.2500 | 300.3333 | 299.2500 | 299.6111 |
| ΔH | Meter box orifice pressure drop (in. H_2O) | 1.5000 | 1.5000 | 1.5000 | |
| θ | Total sampling time (min) | 60.0 | 60.0 | 60.0 | |
| Flow Res | sults | | | | |
| V _{wstd} | Volume of water collected (ft ³) | 11.0826 | 11.3273 | 11.6285 | 11.3462 |
| V _{mstd} | Volume metered, standard (dscf) | 42.1331 | 41.7825 | 41.6702 | 41.8619 |
| Ps | Sample gas pressure, absolute (in. Hg) | 29.2853 | 29.2265 | 29.2632 | 29.2583 |
| Pv | Vapor pressure, actual (in. Hg) | 29.2853 | 29.2265 | 29.2632 | 29.2583 |
| B _{wo} | Moisture measured in sample (% by volume) | 20.8258 | 21.3281 | 21.8176 | 21.3239 |
| B _{ws} | Saturated moisture content (% by volume) | 100.0000 | 100.0000 | 100.0000 | 100.0000 |
| Bw | Actual water vapor in gas (% by volume) | 20.8258 | 21.3281 | 21.8176 | 21.3239 |
| Md | MW of sample gas, dry (lb/lb-mole) | 30.0044 | 29.9992 | 30.0176 | 30.0071 |
| Ms | MW of sample gas, wet (lb/lb-mole) | 27.5044 | 27.4400 | 27.3956 | 27.4467 |

Comments:

Average includes 3 runs.

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QA/QC _____ Date _____

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Wheelabrator North Broward, Inc. Clean Air Project No: 10955 Unit 3 FF Outlet

USEPA Method 26A HCI Parameters

| $\begin{array}{c c c c c c c c c c c c c c c c c c c $ |
|---|
| Stop Time (approx.) 08:17 10:04 11:32 Process Conditions Image: Steam Production Rate (Klbs/hour) 184.6 184.1 184.3 184.3 P1 Fabric Filter Inlet Temperature (°F) 310 310 310 310 |
| Process Conditions R _P Steam Production Rate (Klbs/hour) 184.6 184.1 184.3 184.3 P ₁ Fabric Filter Inlet Temperature (°F) 310 310 310 310 |
| R _P Steam Production Rate (Klbs/hour) 184.6 184.1 184.3 184.3 P ₁ Fabric Filter Inlet Temperature (°F) 310 310 310 310 |
| R _P Steam Production Rate (Klbs/hour) 184.6 184.1 184.3 184.3 P ₁ Fabric Filter Inlet Temperature (°F) 310 310 310 310 |
| P1 Fabric Filter Inlet Temperature (°F) 310 310 310 310 |
| |
| |
| F _c Carbon dioxide-based F-factor (dscf/MMBtu) 1,820 1,820 1,820 1,820 1,820 |
| Cap Capacity factor (hours/year) 8,760 8,760 8,760 8,760 |
| Gas Conditions |
| O ₂ Oxygen (dry volume %) 9.0300 9.1000 8.9200 9.0167 |
| CO2 Carbon dioxide (dry volume %) 10.2700 10.2200 10.3800 10.2900 |
| Ts Sample temperature (°F) 299.2500 300.3333 299.2500 299.6111 |
| Bw Actual water vapor in gas (% by volume) 20.8258 21.3281 21.8176 21.3239 |
| Sampling Data |
| V _{mstd} Volume metered, standard (dscf) 42.1331 41.7825 41.6702 41.8619 |
| |
| |
| m _n Total HCl collected (mg) 26.0913 32.8638 23.8845 |
| Hydrogen Chloride (HCI) Results |
| C _{sd} HCI Concentration (lb/dscf) 1.3655E-06 1.7343E-06 1.2639E-06 1.4546E-06 |
| C _{sd7} HCI Concentration @7% O ₂ (lb/dscf) 1.5990E-06 2.0430E-06 1.4664E-06 1.7028E-06 |
| C _{sd12} HCl Concentration @12% CO ₂ (lb/dscf) 1.5955E-06 2.0364E-06 1.4611E-06 1.6977E-06 |
| C _{sd} HCl Concentration (ppmdv) 14.4365 18.3364 13.3623 15.3784 |
| C _{sd7} HCl Concentration @7% O ₂ (ppmdv) 16.9054 21.5996 15.5038 18.0030 |
| C _{sd12} HCl Concentration @12% CO ₂ (ppmdv) 16.8684 21.5300 15.4477 17.9487 |
| C _w HCl Concentration (ppmwv) 11.4300 14.4256 10.4470 12.1008 |
| C _{sd} HCI Concentration (mg/dscm) 21.8660 27.7729 20.2390 23.2926 |
| C _{sd7} HCl Concentration @7% O ₂ (mg/dscm) 25.6055 32.7155 23.4826 27.2679 |
| C _{sd12} HCl Concentration @12% CO ₂ (mg/dscm) 25.5494 32.6100 23.3976 27.1857 |
| C _{sd} HCI Concentration (mg/Nm ³ dry) 23.4660 29.8050 21.7199 24.9970 |
| C _{sd7} HCl Concentration @7% O ₂ (mg/Nm ³ dry) 27.4791 35.1093 25.2008 29.2631 |
| C _{sd12} HCl Concentration @12% CO ₂ (mg/Nm ³ dry) 27.4189 34.9961 25.1097 29.1749 |
| E _{Fd} HCl Rate - Fd-based (lb/MMBtu) 0.0230 0.0294 0.0211 0.0245 |
| E _{Fc} HCl Rate - Fc-based (lb/MMBtu) 0.0242 0.0309 0.0222 0.0257 |

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Wheelabrator North Broward, Inc. CleanAir Project No. 10955 Lime Silo

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Visible Emission Parameters

| Run | 1 | Time | | Time | (sec) | _ |] | Time | | Time | (sec) | |
|-------------|--------|----------|--------|--------|--------|--------|---|----------|----|--------|--------|--------|
| | | (min) | 15 | 30 | 45 | 60 | | (min) | 15 | 30 | 45 | 60 |
| Date (2010) | Mar 17 | 0 | 0 | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 |
| Start Time | 10:26 | 1 2 | 0 | 0 0 | 0 0 | 0 0 | 1 | 1 2 | 0 | 0 0 | 0 0 | 0 0 |
| | | 3 | ŏ | ŏ | ŏ | ŏ | | 3 | ŏ | ŏ | ŏ | õ |
| | | 4 | 0 | 0 | 0. | 0 | | 4 | 0 | 0 | 0 | 0 |
| | | 5 | 0 | 0 | 0 | 0 | | 5 | 0 | 0 | 0 | 0 |
| | | 6 | 0 | 0 | 0 | 0 0 | | 6 7 | 0 | 0 0 | 0 0 | 0 0 |
| | | 7 | 0 | 0 0 | 0 0 | 0 | | 8 | o | ŏ | Ő | Ö |
| | | 9 | ō | ŏ | ō | ō | | 9 | Ō | Ō | Ō | Ō |
| | | 10 | 0 | 0 | 0 | 0 | | 10 | 0 | 0 | 0 | 0 |
| | | 11 | 0 | 0 | 0 | 0 | | 11 | 0 | 0 | 0 0 | 0 |
| | | 12 13 | 0 | 0 0 | 0 0 | 0 0 | | 12 13 | 0 | 0 0 | 0 0 | 0 0 |
| | | 14 | ŏ | ŏ | õ | ŏ | | 14 | õ | õ | õ | ō |
| | | 15 | 0 | 0 | 0 | 0 | | 15 | 0 | 0 | 0 | 0 |
| | | 16 | 0 | 0 | 0 | 0 | | 16 | 0 | 0 | 0 | 0 |
| | | 17 | 0 | 0 0 | 0 0 | 0 0 | 1 | 17 18 | 0 | 0 0 | 0 0 | 0 0 |
| | | 18 19 | 0 | ō | 0 | õ | | 19 | ō | ŏ | ŏ | ŏ |
| | | 20 | ō | õ | Ō | Ō | | 20 | - | • | | |
| | | 21 | 0 | 0 | 0 | 0 | | 21 | | | | |
| | | 22 | 0 | 0 | 0 0 | 0 0 | | 22 23 | | | | |
| | | 23 24 | 0 | 0 0 | 0 | 0 | | 23 | | | | |
| | | 25 | ō | õ | Ō | õ | | 25 | | | | |
| | | 26 | 0 | 0 | 0 | 0 | | 26 | | | | |
| | | 27 | 0 | 0 | 0 | 0 | | 27 | | | | |
| | | 28 29 | 0 | 0 0 | 0 0 | 0 0 | | 28 29 | | | | |
| | | 30 | ō | ŏ | õ | ŏ | | 30 | | | | |
| | | 31 | 0 | 0 | 0 | 0 | | 31 | | | | |
| | | 32 | 0 | 0 | 0 | 0 | [| 32 | | | | |
| | | 33 34 | 0 | 0 0 | 0 0 | 0 0 | | 33 34 | | | | |
| | | 34 | 0 | Ö | 0 | ŏ | | 35 | | | | |
| | | 36 | 0 | Ō | 0 | 0 | | 36 | | | | |
| | | 37 | 0 | 0 | 0 | 0 | | 37 | | | | |
| | | 38 | 0 | 0 0 | 0 0 | 0 0 | | 38 39 | | | | |
| | | 39 40 | 0 | ŏ | Ő | 0 | | 40 | | | | |
| | | 41 | Ō | ō | Ō | Ō | | 41 | | | | |
| | | 42 | 0 | 0 | 0 | 0 | | 42 | | | | |
| | | 43 | 0 | 0 | 0 | 0 | | 43 44 | | | | |
| | | 44 45 | 0 0 | 0 0 | 0 0 | 0 0 | | 44 | | | | |
| | | 46 | õ | õ | ō | õ | | 46 | | | | |
| | | 47 | 0 | 0 | 0 | 0 | | 47 | | | | |
| | | 48 | 0 | 0 | 0 | 0 | | 48 | | | | |
| | | 49 50 | 0 | 0 0 | 0 0 | 0 0 | | 49 50 | | | | |
| | | 50 | 0 | ŏ | 0 | õ | | 51 | | | | |
| | | 52 | 0 | ō | 0 | 0 | | 52 | | | | |
| | | 53 | 0 | 0 | 0 | 0 | | 53 | | | | |
| | | 54 | 0 | 0 | 0 | 0 | | 54 55 | | | | |
| | | 55 56 | 0 0 | 0 0 | 0 0 | 0 0 | | 55 | | | | |
| | | 57 | Ő | ō | ŏ | ŏ | | 57 | | | | |
| | | 58 | 0 | 0 | 0 | 0 | | 58 | | | | |
| | | 59 | 0 | 0 | 0 | 0 | | 59 | | | acity | 0 |

Average Opacity 0 Minimum Reading 0

Maximum Reading 0 No. of Readings >5% 0

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WHEELABRATOR NORTH BROWARD, INC. POMPANO BEACH, FL

CleanAir Project No: 10955-2

| QA/QC DATA | i la Hallandi i di seconda di s | allanti in shifti i bilanin saya sa 1968ada | u – Miller Berland, Beller Brand Lee, Socher L | |
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Wheelabrator North Broward, Inc. Clean Air Project No: 10955 Unit 1 FF Outlet

USEPA Method 5/29 (Particulate/Metals) QA/QC Results

| Run No | | 1 | 2 | 3 | |
|--------------------|--|-------------|--------------|--------|---------|
| Date (20 | 010) | Mar 16 | Mar 16 | Mar 16 | |
| | ne (approx.) | 07:21 | 10:00 | 12:36 | |
| Stop Tin | ne (approx.) | 09:32 | 12:14 | 14:47 | |
| Total Du | iration of Test Run (min.) | 13 1 | 134 | 131 | |
| Net San | npling Time (min.) | 125 | 125 | 125 | |
| Samplin | ng System Calibration Summary | | | | |
| | Nozzle ID No: | 270-1 | 270-1 | 270-1 | |
| Dn | Nozzle Diameter (in): | 0.270 | 0.270 | 0.270 | |
| | Probe ID No: | 67-8-4 | 67-8-4 | 67-8-4 | |
| Cρ | Pitot Coefficient: | 0.8050 | 0.8050 | 0.8050 | |
| | Meter Box ID. No: | 61-6 | 61-6 | 61-6 | |
| Yd | Meter Box Yd - Field Sheet | 0.9900 | 0.9900 | 0.9900 | |
| | Meter Box Yd - Database | 0.9900 | 0.9900 | 0.9900 | |
| | Meter Box ∆H@ - Field Sheet | 1.6820 | 1.6820 | 1.6820 | |
| | Meter Box ∆H@ - Database | 1.6820 | 1.6820 | 1.6820 | |
| QA/QC | | | | | |
| | Final Leak Check | | | | |
| | (a) 4% of Sampling Rate (cfm) | 0.0257 | 0.0261 | 0.0265 | |
| | (b) Allowable Rate from Method (cfm) | 0.0200 | 0.0200 | 0.0200 | |
| | Allowable Limit - minimum of a and b (cfm) | 0.0200 | 0.0200 | 0.0200 | |
| | Actual Final Leak Rate (cfm) | 0.0020 | 0.0020 | 0.0030 | |
| | Sample Volume | | | | |
| | Minimum Volume Required (dscf) | 60.00 | 60.00 | 60.00 | |
| V _{mstd} | Actual Sample Volume (dscf) | 80.553 | 81.154 | 81.553 | |
| 1 | Alternative Method 5 Post-Test Calibration (EPA A | | | | |
| √∆H _{avg} | | 1.1230 | 1.1375 | 1.1463 | |
| Y_{qa} | Alternative Meter Calibration Factor | 0.9879 | 0.9891 | 0.9860 | Average |
| | Variation from full-test Y_d (average $\leq \pm 5\%$) | -0.2% | -0.1% | -0.4% | -0.2% |
| | Mean Isokinetic Sampling Rate Variation | | | | |
| | Minimum Allowable (%) | 90 | 90 | 90 | |
| | Maximum Allowable (%) | 110 | 1 1 0 | 110 | |
| %1 | Actual Variation (%) | 98.77 | 99.71 | 99.31 | |
| | Point-by-Point Isokinetic Variation | | | | |
| | Number of points <90% | 0 | 0 | 0 | |
| | Number of points >110% | 0 | 0 | 0 | |
| | Number of points <80% | 0 | 0 | 0 | |
| | Number of points >120% | 0 | 0 | 0 | |

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QA/QC Date _____

Wheelabrator North Broward, Inc. Clean Air Project No: 10955 Unit 2 FF Outlet

USEPA Method 5/29 (Particulate/Metals) QA/QC Results

| Run No. | | 1 | 2 | 3 |
|--------------------|--|---------------|--------|--------|
| Date (20 | 10) | Mar 18 | Mar 18 | Mar 18 |
| | e (approx.) | 07:09 | 09:49 | 12:27 |
| Stop Tim | e (approx.) | 09:22 | 12:02 | 14:39 |
| | ration of Test Run (min.) | 133 | 133 | 132 |
| Net Sam | pling Time (min.) | 125 | 125 | 125 |
| | | | | |
| <u>Şamplin</u> | g System Calibration Summary | | | |
| | Nozzie ID No: | 270-1 | 270-1 | 270-1 |
| Dn | Nozzle Diameter (in): | 0.270 | 0.270 | 0.270 |
| | Probe ID No: | 67-8-4 | 67-8-4 | 67-8-4 |
| Cp | Pitot Coefficient: | 0.8050 | 0.8050 | 0.8050 |
| | Meter Box ID. No: | 66-24 | 66-24 | 66-24 |
| Yd | Meter Box Yd - Field Sheet | 0.9904 | 0.9904 | 0.9904 |
| | Meter Box Yd - Database | 0.9904 | 0.9904 | 0.9904 |
| | Meter Box ∆H@ - Field Sheet | 1.7516 | 1.7516 | 1.7516 |
| | Meter Box ∆H@ - Database | 1.7516 | 1.7516 | 1.7516 |
| QA/QC | | | | |
| | Final Leak Check | | | |
| | (a) 4% of Sampling Rate (cfm) | 0.0271 | 0.0261 | 0.0273 |
| | (b) Allowable Rate from Method (cfm) | 0.0200 | 0.0200 | 0.0200 |
| | Allowable Limit - minimum of a and b (cfm) | 0.0200 | 0.0200 | 0.0200 |
| | Actual Final Leak Rate (cfm) | 0.0040 | 0.0020 | 0.0030 |
| | Sample Volume | | | |
| | Minimum Volume Required (dscf) | 60.00 | 60.00 | 60.00 |
| V _{mstd} | Actual Sample Volume (dscf) | 84.183 | 79.341 | 82.110 |
| • | Alternative Method 5 Post-Test Calibration (EPA AL | <u>T-009)</u> | | |
| √∆H _{avg} | Average of Square Root of ΔH (in. W.C.) | 1.2037 | 1.1523 | 1.1942 |
| Y _{qa} | Alternative Meter Calibration Factor | 0.9897 | 0.9931 | 0.9905 |
| | Variation from full-test Y_d (average $\leq \pm 5\%$) | -0.1% | 0.3% | 0.0% |
| | Mean Isokinetic Sampling Rate Variation | | | |
| | Minimum Allowable (%) | 90 | 90 | 90 |
| | Maximum Allowable (%) | 110 | 110 | 110 |
| % | Actual Variation (%) | 100.31 | 98.93 | 99.93 |
| | Point-by-Point Isokinetic Variation | | | |
| | Number of points <90% | 0 | 0 | 0 |
| | Number of points >110% | 0 | 0 | 0 |
| | Number of points <80% | 0 | 0 | 0 |
| | Number of points >120% | 0 | 0 | 0 |

Average 0.1%

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Wheelabrator North Broward, Inc. Clean Air Project No: 10955 Unit 3 FF Outlet

USEPA Method 5/29 (Particulate/Metals) QA/QC Results

| Run No | | 1 | 2 | 3 |
|--------------------|--|----------|--------|--------|
| Date (20 | 010) | Mar 17 | Mar 17 | Mar 17 |
| | ne (approx.) | 06:50 | 09:26 | 11:59 |
| | ne (approx.) | 09:03 | 11:38 | 14:11 |
| Total Du | iration of Test Run (min.) | 133 | 132 | 132 |
| Net San | npling Time (min.) | 125 | 125 | 125 |
| Samplir | ng System Calibration Summary | | | |
| | Nozzle ID No: | 270-1 | 270-1 | 270-1 |
| Dn | Nozzle Diameter (in): | 0.270 | 0.270 | 0.270 |
| Dn | Nozzie Diameter (m). | 0.270 | 0.270 | 0.270 |
| | Probe ID No: | 67-8-4 | 67-8-4 | 67-8-4 |
| C_p | Pitot Coefficient: | 0.8050 | 0.8050 | 0.8050 |
| | Meter Box ID. No: | 66-14 | 66-14 | 66-14 |
| Yd | Meter Box Yd - Field Sheet | 0.9898 | 0.9898 | 0.9898 |
| - | Meter Box Yd - Database | 0.9898 | 0.9898 | 0.9898 |
| | Meter Box ∆H@ - Field Sheet | 1.7643 | 1,7643 | 1,7643 |
| | Meter Box ∆H@ - Database | 1.7643 | 1.7643 | 1.7643 |
| | | | | |
| | Final Leak Check | | | |
| | (a) 4% of Sampling Rate (cfm) | 0.0231 | 0.0249 | 0.0245 |
| | (b) Allowable Rate from Method (cfm) | 0.0200 | 0.0200 | 0.0200 |
| | Allowable Limit - minimum of a and b (cfm) | 0.0200 | 0.0200 | 0.0200 |
| | Actual Final Leak Rate (cfm) | 0.0000 | 0.0030 | 0.0030 |
| | Sample Volume | 0.0000 | 0.0000 | 0.0000 |
| | Minimum Volume Required (dscf) | 60.00 | 60.00 | 60.00 |
| V _{mstd} | Actual Sample Volume (dscf) | 70.859 | 75.796 | 74.783 |
| 11500 | , , , | I T 000) | | |
| √∆H _{avg} | Alternative Method 5 Post-Test Calibration (EPA A Average of Square Root of Δ H (in. W.C.) | 1.0334 | 1.1107 | 1.0965 |
| | Alternative Meter Calibration Factor | 0.9959 | 0.9959 | 0.9979 |
| Y_{qa} | Variation from full-test Y_d (average $\leq \pm 5\%$) | 0.9959 | 0.9959 | 0.9979 |
| | | 0.078 | 0.078 | 0.078 |
| | Mean Isokinetic Sampling Rate Variation | | | |
| | Minimum Allowable (%) | 90 | 90 | 90 |
| | Maximum Allowable (%) | 110 | 110 | 110 |
| %I | Actual Variation (%) | 100.44 | 100.53 | 100.01 |
| | Point-by-Point Isokinetic Variation | | | |
| | Number of points <90% | 0 | 0 | 0 |
| | Number of points >110% | 0 | 0 | 0 |
| | Number of points <80% | 0 | 0 | 0 |
| | Number of points >120% | 0 | 0 | 0 |

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Average 0.7%

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Wheelabrator North Broward, Inc. Clean Air Project No: 10955 Unit 1 FF Outlet

USEPA Method 13B (Total Fluorides) QA/QC Results

| Run No. | , | 1 | 2 | 3 |
|--------------------|--|--------------|---------|---------|
| Date (20 | 10) | Mar 17 | Mar 17 | Mar 17 |
| Start Tin | ne (approx.) | 11:46 | 13:15 | 14:45 |
| Stop Tirr | ne (approx.) | 12:56 | 14:27 | 15:53 |
| | ration of Test Run (min.) | 70 | 72 | 68 |
| Net Sam | pling Time (min.) | 63 | 63 | 63 |
| <u>Samplin</u> | g System Calibration Summary | | | |
| | Nozzle ID No: | 268-1 | 268-1 | 268-1 |
| Dn | Nozzle Diameter (in): | 0.268 | 0.268 | 0.268 |
| | Probe ID No: | 67-8-14 | 67-8-14 | 67-8-14 |
| Cp | Pitot Coefficient: | 0.8120 | 0.8120 | 0.8120 |
| | Meter Box ID. No: | 61-6 | 61-6 | 61-6 |
| Yd | Meter Box Yd - Field Sheet | 0.9900 | 0.9900 | 0.9900 |
| | Meter Box Yd - Database | 0.9900 | 0.9900 | 0.9900 |
| | Meter Box △H@ - Field Sheet | 1.6820 | 1.6820 | 1.6820 |
| | Meter Box ∆H@ - Database | 1.6820 | 1.6820 | 1.6820 |
| QA/QC | | | | |
| | Final Leak Check | | | |
| | (a) 4% of Sampling Rate (cfm) | 0.0275 | 0.0275 | 0.0265 |
| | (b) Allowable Rate from Method (cfm) | 0.0200 | 0.0200 | 0.0200 |
| | Allowable Limit - minimum of a and b (cfm) | 0.0200 | 0.0200 | 0.0200 |
| | Actual Final Leak Rate (cfm) | 0.0010 | 0.0020 | 0.0020 |
| | Sample Volume | | | |
| | Minimum Volume Required (dscf) | 30.00 | 30.00 | 30.00 |
| V _{mstd} | Actual Sample Volume (dscf) | 42.732 | 42.452 | 41.153 |
| | Alternative Method 5 Post-Test Calibration (EPA A | | | |
| √∆H _{avg} | Average of Square Root of ∆H (in. W.C.) | 1.2034 | 1.2101 | 1.1602 |
| Y_{qa} | Alternative Meter Calibration Factor | 0.9949 | 1.0028 | 0.9931 |
| | Variation from full-test Y_d (average $\leq \pm 5\%$) | 0.5% | 1.3% | 0.3% |
| | Mean Isokinetic Sampling Rate Variation | | | |
| | Minimum Allowable (%) | 90 | 90 | 90 |
| | Maximum Allowable (%) | 1 1 0 | 110 | 110 |
| %I | Actual Variation (%) | 100.12 | 99.42 | 101.21 |
| | Point-by-Point Isokinetic Variation | | | |
| | Number of points <90% | 0 | 1 | 0 |
| | Number of points >110% | 0 | 1 | 0 |
| | Number of points <80% | 0 | 0 | 0 |
| | Number of points >120% | 0 | 0 | 0 |

Average 0.7%

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Wheelabrator North Broward, Inc. Clean Air Project No: 10955 Unit 2 FF Outlet

USEPA Method 13B (Total Fluorides) QA/QC Results

•

| Run No | | 1 | 2 | 3 | |
|--------------------|--|---------|---------|---------|--|
| Date (20 | 010) | Mar 18 | Mar 18 | Mar 18 | |
| | ne (approx.) | 07:09 | 08:56 | 10:45 | |
| Stop Tir | ne (approx.) | 08:24 | 10:10 | 12:05 | |
| Total Du | uration of Test Run (min.) | 75 | 74 | 80 | |
| Net San | npling Time (min.) | 63 | 63 | 63 | |
| Samplin | ng System Calibration Summary | | | | |
| | Nozzle ID No: | 268-1 | 268-1 | 268-1 | |
| Da | Nozzle Diameter (in): | 0.268 | 0.268 | 0.268 | |
| | Probe ID No: | 67.9.14 | 67.9.44 | 67.9.44 | |
| c | Pitot Coefficient: | 67-8-14 | 67-8-14 | 67-8-14 | |
| Cp | Phot Coemcient: | 0.8120 | 0.8120 | 0.8120 | |
| | Meter Box ID. No: | 66-14 | 66-14 | 66-14 | |
| Yd | Meter Box Yd - Field Sheet | 0.9898 | 0.9898 | 0.9898 | |
| | Meter Box Yd - Database | 0.9898 | 0.9898 | 0.9898 | |
| | Meter Box ∆H@ - Field Sheet | 1.7643 | 1.7643 | 1.7643 | |
| | Meter Box ∆H@ - Database | 1.7643 | 1.7643 | 1.7643 | |
| QA/QC | | | | | |
| | Final Leak Check | | | | |
| | (a) 4% of Sampling Rate (cfm) | 0.0244 | 0.0239 | 0.0246 | |
| | (b) Allowable Rate from Method (cfm) | 0.0200 | 0.0200 | 0.0200 | |
| | Allowable Limit - minimum of a and b (cfm) | 0.0200 | 0.0200 | 0.0200 | |
| | Actual Final Leak Rate (cfm) | 0.0040 | 0.0020 | 0.0030 | |
| | Sample Volume | | | | |
| | Minimum Volume Required (dscf) | 30.00 | 30.00 | 30.00 | |
| V _{mstd} | Actual Sample Volume (dscf) | 38.207 | 36.894 | 37.310 | |
| | Alternative Method 5 Post-Test Calibration (EPA A | LT-009) | | | |
| √∆H _{avg} | Average of Square Root of ∆H (in. W.C.) | 1.1156 | 1.0736 | 1.0938 | |
| Y _{qa} | Alternative Meter Calibration Factor | 1.0110 | 0.9988 | 0.9997 | |
| - | Variation from full-test Y_d (average $\leq \pm 5\%$) | 2.1% | 0.9% | 1.0% | |
| | Mean Isokinetic Sampling Rate Variation | | | | |
| | Minimum Allowable (%) | 90 | 90 | 90 | |
| | Maximum Allowable (%) | 110 | 110 | 110 | |
| %1 | Actual Variation (%) | 98.31 | 99.17 | 98.03 | |
| | Point-by-Point Isokinetic Vanation | | | | |
| | Number of points <90% | 2 | 0 | 0 | |
| | Number of points >110% | 1 | 0 | 0 | |
| | Number of points <80% | 2 | 0 | 0 | |
| | Number of points >120% | 0 | 0 | 0 | |

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Average 1.4%

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USEPA Method 13B (Total Fluorides) QA/QC Results

| Run No. | | 1 | 2 | 3 |
|--------------------|--|-----------------|---------|---------|
| Date (20 | 10) | Mar 16 | Mar 16 | Mar 16 |
| | ne (approx.) | 11:49 | 13:33 | 15:07 |
| | ne (approx.) | 13:07 | 14:44 | 16:16 |
| Total Du | ration of Test Run (min.) | 78 | 71 | 69 |
| Net Sam | pling Time (min.) | 63 | 63 | 63 |
| | | | | |
| <u>Samplin</u> | g System Calibration Summary | | | |
| | Nozzle ID No: | 268-1 | 268-1 | 268-1 |
| Dn | Nozzle Diameter (in): | 0.268 | 0.268 | 0.268 |
| | Probe ID No: | 67-8-14 | 67-8-14 | 67-8-14 |
| C _p | Pitot Coefficient: | 0.8120 | 0.8120 | |
| Υp | | 0.0120 | 0.0120 | 0.8120 |
| | Meter Box ID. No: | 66-14 | 66-14 | 66-14 |
| Yd | Meter Box Yd - Field Sheet | 0.9898 | 0.9898 | 0.9898 |
| | Meter Box Yd - Database | 0.9898 | 0.9898 | 0.9898 |
| | Meter Box ∆H@ - Field Sheet | 1.7643 | 1.7643 | 1.7643 |
| | Meter Box ∆H@ - Database | 1.7643 | 1.7643 | 1.7643 |
| QA/QC | | | | |
| | Final Leak Check | | | |
| | (a) 4% of Sampling Rate (cfm) | 0.0236 | 0.0242 | 0.0234 |
| | (b) Allowable Rate from Method (cfm) | 0.0200 | 0.0200 | 0.0200 |
| | Allowable Limit - minimum of a and b (cfm) | 0.0200 | 0.0200 | 0.0200 |
| | Actual Final Leak Rate (cfm) | 0.0020 | 0.0020 | 0.0020 |
| | Sample Volume | | | |
| | Minimum Volume Required (dscf) | 30.00 | 30.00 | 30.00 |
| V _{mstd} | Actual Sample Volume (dscf) | 36.404 | 36.989 | 35.734 |
| | Alternative Method 5 Post-Test Calibration (EPA A | <u>LT-009</u>) | | |
| √∆H _{avg} | Average of Square Root of ∆H (in. W.C.) | 1.0442 | 1.0697 | 1.0297 |
| Y_{qa} | Alternative Meter Calibration Factor | 0.9851 | 0.9877 | 0.9829 |
| | Variation from full-test Y_d (average $\leq \pm 5\%$) | -0.5% | -0.2% | -0.7% |
| | Mean Isokinetic Sampling Rate Variation | | | |
| | Minimum Allowable (%) | 90 | 90 | 90 |
| | Maximum Allowable (%) | 110 | 110 | 110 |
| %I | Actual Variation (%) | 101.61 | 100.74 | 100.78 |
| | Point-by-Point Isokinetic Variation | | | |
| | Number of points <90% | 3 | 2 | 1 |
| | Number of points >110% | 5 | 2 | 1 |
| | Number of points <80% | 0 | 1 | 0 |
| | Number of points >120% | 1 | . 1 | 0 |
| | | | | |

Average -0.5%

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Wheelabrator North Broward, Inc. Clean Air Project No: 10955 Unit 2 FF Outlet

USEPA Method 26A (HCI) QA/QC Results

| tun No | | 1 | 2 | 3 |
|--------------------|---|--------|--------|--------|
|)ate (20 | 010) | Mar 17 | Mar 17 | Mar 17 |
| tart Tin | ne (approx.) | 06:54 | 09:02 | 10:25 |
| top Tim | ne (approx.) | 07:54 | 10:02 | 11:25 |
| otal Du | ration of Test Run (min.) | 60 | 60 | 60 |
| let Sam | npling Time (min.) | 60 | 60 | 60 |
| amplin | g System Calibration Summary | | | |
| | Nozzle ID No: | NA | NA | NA |
| Dn | Nozzle Diameter (in): | NA | NA | NA |
| | Probe ID No: | 67-4-3 | 67-4-3 | 67-4-3 |
| | Meter Box ID. No: | 66-24 | 66-24 | 66-24 |
| Y₫ | Meter Box Yd - Field Sheet | 0.9904 | 0.9904 | 0.9904 |
| | Meter Box Yd - Database | 0.9904 | 0.9904 | 0.9904 |
| | Meter Box ∆H@ - Field Sheet | 1.7516 | 1.7516 | 1.7516 |
| | Meter Box ∆H@ - Database | 1.7516 | 1.7516 | 1.7516 |
| A/QC | | | | |
| | Final Leak Check | | | |
| | (a) 4% of Sampling Rate (cfm) | 0.0280 | 0.0280 | 0.0282 |
| | (b) Allowable Rate from Method (cfm) | 0.0200 | 0.0200 | 0.0200 |
| | Allowable Limit - minimum of a and b (cfm) | 0.0200 | 0.0200 | 0.0200 |
| | Actual Final Leak Rate (cfm) | 0.0020 | 0.0020 | 0.0030 |
| | Sample Volume | | | |
| | Minimum Volume Required (dscf) | 30.00 | 30.00 | 30.00 |
| V _{mstd} | Actual Sample Volume (dscf) | 41.238 | 41.007 | 40.731 |
| | Alternative Method 5 Post-Test Calibration (EPA A | | | |
| √∆H _{avg} | Average of Square Root of ΔH (in. W.C.) | 1.2247 | 1.2247 | 1.2247 |
| Y _{qa} | Alternative Meter Calibration Factor | 0.9803 | 0.9826 | 0.9823 |
| · qa | | | | |

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Average -0.9%

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QA/QC ____ Date ____

Wheelabrator North Broward, Inc. Clean Air Project No: 10955 Unit 2 FF Outlet

USEPA Method 23 (PCDD/F) QA/QC Results

| Run No. | | 1 | 2 | 3 |
|--------------------|--|------------------|---------|---------|
| Date (20 | 10) | Mar 16 | Mar 17 | Mar 17 |
| • | e (approx.) | 08:44 | 06:54 | 12:53 |
| | e (approx.) | 13:36 | 12:19 | 17:26 |
| Total Du | ration of Test Run (min.) | 292 | 325 | 273 |
| Net Sam | pling Time (min.) | 250 | 250 | 250 |
| | | | | |
| <u>Samplin</u> | g System Calibration Summary | | | |
| | Nozzle ID No: | 264-1 | 264-1 | 264-1 |
| Dn | Nozzle Diameter (in): | 0.264 | 0.264 | 0.264 |
| | Probe ID No: | 67-8-17 | 67-8-17 | 67-8-17 |
| C _p | Pitot Coefficient: | 0.8340 | 0.8340 | 0.8340 |
| | Meter Box ID. No: | 66-6 | 66-6 | 66-24 |
| Yd | Meter Box Yd - Field Sheet | 0.9901 | 0.9901 | 0.9904 |
| - 0 | Meter Box Yd - Database | 0.9901 | 0.9901 | 0.9904 |
| | Meter Box △H@ - Field Sheet | 1.7870 | 1.7870 | 1.7516 |
| | Meter Box ∆H@ - Database | 1.7870 | 1.7870 | 1.7516 |
| QA/QC | | | | |
| | Final Leak Check | | | |
| | (a) 4% of Sampling Rate (cfm) | 0.0257 | 0.0275 | 0.0266 |
| | (b) Allowable Rate from Method (cfm) | 0.0200 | 0.0200 | 0.0200 |
| | Allowable Limit - minimum of a and b (cfm) | 0.0200 | 0.0200 | 0.0200 |
| | Actual Final Leak Rate (cfm) | 0.0050 | 0.0050 | 0.0050 |
| | Sample Volume | | | |
| | Minimum Volume Required (dscf) | 120.00 | 120.00 | 120.00 |
| V _{mstd} | Actual Sample Volume (dscf) | 156.061 | 168.824 | 164.129 |
| | Alternative Method 5 Post-Test Calibration (EPA A | <u>(LT-009</u>) | | |
| √∆H _{avg} | Average of Square Root of ∆H (in. W.C.) | 1.1356 | 1.2325 | 1.1676 |
| Y _{qa} | Alternative Meter Calibration Factor | 0.9855 | 0.9937 | 0.9808 |
| | Variation from full-test Y_d (average $\leq \pm 5\%$) | -0.5% | 0.4% | -1.0% |
| | Mean Isokinetic Sampling Rate Variation | | | |
| | Minimum Allowable (%) | 90 | 90 | 90 |
| | Maximum Allowable (%) | 110 | 110 | 110 |
| %I | Actual Variation (%) | 97.97 | 100.32 | 101.57 |
| | Point-by-Point Isokinetic Variation | | | |
| | Number of points <90% | 0 | 0 | 0 |
| | Number of points >110% | 0 | 0 | 0 |
| | Number of points <80% | 0 | 0 | 0 |
| | Number of points >120% | 0 | 0 | 0 |

Average -0.4%

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QA/QC _____ Date _____

Wheelabrator North Broward, Inc. Clean Air Project No: 10955 Unit 1 SDA Inlet

USEPA Method 26A (HCI) QA/QC Results

| Run No | | 1 | 2 | 3 |
|--------------------|--|-----------------|--------|--------|
| Date (20 | 10) | Mar 18 | Mar 18 | Mar 18 |
| Start Tin | ne (approx.) | 07:02 | 09:26 | 11:49 |
| Stop Tin | ne (approx.) | 08:02 | 10:37 | 12:49 |
| Total Du | ration of Test Run (min.) | 60 | 71 | 60 |
| Net Sam | ppling Time (min.) | 60 | 60 | 60 |
| Samplin | g System Calibration Summary | | | |
| | Nozzle ID No: | NA | NA | NA |
| Dn | Nozzle Diameter (in): | NA | NA | NA |
| | Probe ID No: | 67-4-4 | 67-4-4 | 67-4-4 |
| Cp | Pitot Coefficient: | 0.8400 | 0.8400 | 0.8400 |
| | Meter Box ID. No: | 85-4 | 85-4 | 85-4 |
| Yd | Meter Box Yd - Field Sheet | 1.0085 | 1.0085 | 1.0085 |
| | Meter Box Yd - Database | 1.0085 | 1.0085 | 1.0085 |
| | Meter Box ∆H@ - Field Sheet | 1.7723 | 1.7723 | 1.7723 |
| | Meter Box ∆H@ - Database | 1.7723 | 1.7723 | 1.7723 |
| <u>QA/QC</u> | | | | |
| | Final Leak Check | | | |
| | (a) 4% of Sampling Rate (cfm) | 0.0247 | 0.0238 | 0.0237 |
| | (b) Allowable Rate from Method (cfm) | 0.0200 | 0.0200 | 0.0200 |
| | Allowable Limit - minimum of a and b (cfm) | 0.0200 | 0.0200 | 0.0200 |
| | Actual Final Leak Rate (cfm) | 0.0030 | 0.0030 | 0.0030 |
| | Sample Volume | | | |
| | Minimum Volume Required (dscf) | 30.00 | 30.00 | 30.00 |
| V _{mstd} | Actual Sample Volume (dscf) | 38.191 | 36.424 | 35.652 |
| | Alternative Method 5 Post-Test Calibration (EPA A | <u>LT-009</u>) | | |
| √∆H _{avg} | Average of Square Root of ΔH (in. W.C.) | 1.0916 | 1.0954 | 1.0954 |
| Y _{qa} | Alternative Meter Calibration Factor | 0.9680 | 1.0125 | 1.0264 |
| - | Variation from full-test Y_d (average $\leq \pm 5\%$) | -4.0% | 0.4% | 1.8% |

Average -0.6%

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QA/QC _____ Date _____

Wheelabrator North Broward, Inc. Clean Air Project No: 10955 Unit 1 FF Outlet

USEPA Method 26A (HCI) QA/QC Results

| Run No. | | 1 | 2 | 3 |
|--------------------|--|--------|--------|----------|
| Date (20 | 10) | Mar 18 | Mar 18 | Mar 18 |
| • | e (approx.) | 07:02 | 09:26 | 11:49 |
| Stop Tim | e (approx.) | 08:02 | 10:37 | 12:49 |
| Total Dur | ration of Test Run (min.) | 60 | 71 | 60 |
| Net Sam | pling Time (min.) | 60 | 60 | 60 |
| Samplin | g System Calibration Summary | | | |
| Samping | | | | |
| | Nozzle ID No: | NA | NA | NA |
| Dn | Nozzle Diameter (in): | NA | NA | NA |
| | Probe ID No: | 67-4-3 | 67-4-3 | 67-4-3 |
| Cp | Pitot Coefficient: | 0.8400 | 0.8400 | 0.8400 |
| | Meter Box ID. No: | 85-2 | 85-2 | 85-2 |
| Yd | Meter Box Yd - Field Sheet | 1.0066 | 1.0066 | 1.0066 |
| | Meter Box Yd - Database | 1.0066 | 1.0066 | 1.0066 |
| | Meter Box ∆H@ - Field Sheet | 1.7759 | 1.7759 | . 1.7759 |
| | Meter Box ∆H@ - Database | 1.7759 | 1.7759 | 1.7759 |
| QA/QC | | | | |
| | Final Leak Check | | | |
| | (a) 4% of Sampling Rate (cfm) | 0.0267 | 0.0266 | 0.0268 |
| | (b) Allowable Rate from Method (cfm) | 0.0200 | 0.0200 | 0.0200 |
| | Allowable Limit - minimum of a and b (cfm) | 0.0200 | 0.0200 | 0.0200 |
| | Actual Final Leak Rate (cfm) | 0.0030 | 0.0010 | 0.0020 |
| | Sample Volume | | | |
| | Minimum Volume Required (dscf) | 30.00 | 30.00 | 30.00 |
| V _{mstd} | Actual Sample Volume (dscf) | 41.096 | 40.795 | 40.645 |
| | Alternative Method 5 Post-Test Calibration (EPA ALT | | | |
| √∆H _{avg} | Average of Square Root of ∆H (in. W.C.) | 1.2247 | 1.2247 | 1.2247 |
| Y _{qa} | Alternative Meter Calibration Factor | 1.0058 | 1.0118 | 1.0108 |
| - | Variation from full-test Y_d (average $\leq \pm 5\%$) | -0.1% | 0.5% | 0.4% |

Average 0.3%

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USEPA Method 26A (HCI) QA/QC Results

| Run No. | | 1 | 2 | 3 |
|--------------------|--|--------|--------|--------|
| Date (20 | 10) | Mar 17 | Mar 17 | Mar 17 |
| | ne (approx.) | 06:54 | 09:02 | 10:25 |
| Stop Tim | ne (approx.) | 07:54 | 10:02 | 11:25 |
| Total Du | ration of Test Run (min.) | 60 | 60 | 60 |
| Net Sam | pling Time (min.) | 60 | 60 | 60 |
| <u>Samplin</u> | g System Calibration Summary | | | |
| | Nozzie ID No: | NA | NA | NA |
| D _n | Nozzle Diameter (in): | NA | NA | NA |
| | Probe ID No: | 67-4-5 | 67-4-5 | 67-4-5 |
| C_p | Pitot Coefficient: | 0.8400 | 0.8400 | 0.8400 |
| | Meter Box ID. No: | 61-8 | 61-8 | 61-8 |
| Yd | Meter Box Yd - Field Sheet | 0.9916 | 0.9916 | 0.9916 |
| | Meter Box Yd - Database | 0.9916 | 0.9916 | 0.9916 |
| | Meter Box ∆H@ - Field Sheet | 1.7580 | 1.7580 | 1.7580 |
| | Meter Box ∆H@ - Database | 1.7580 | 1.7580 | 1.7580 |
| QA/QC | | | | |
| | Final Leak Check | | | |
| | (a) 4% of Sampling Rate (cfm) | 0.0242 | 0.0243 | 0.0242 |
| | (b) Allowable Rate from Method (cfm) | 0.0200 | 0.0200 | 0.0200 |
| | Allowable Limit - minimum of a and b (cfm) | 0.0200 | 0.0200 | 0.0200 |
| | Actual Final Leak Rate (cfm) | 0.0040 | 0.0030 | 0.0040 |
| | Sample Volume | | | |
| | Minimum Volume Required (dscf) | 30.00 | 30.00 | 30.00 |
| V _{mstd} | Actual Sample Volume (dscf) | 35.882 | 36.433 | 36.196 |
| | Alternative Method 5 Post-Test Calibration (EPA A | | | |
| √∆H _{avg} | Average of Square Root of ΔH (in. W.C.) | 1.0916 | 1.0954 | 1.0916 |
| Y_{qa} | Alternative Meter Calibration Factor | 1.0029 | 0.9981 | 0.9998 |
| | Variation from full-test Y_d (average $\leq \pm 5\%$) | 1.1% | 0.7% | 0.8% |

Average 0.9%

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QA/QC ____ Date ____ Wheelabrator North Broward, Inc. Clean Air Project No: 10955 Unit 2 FF Outlet

USEPA Method 26A (HCI) QA/QC Results

| Run No. | | 1 | 2 | 3 |
|--------------------|--|---------|--------|--------|
| Date (20 | 10) | Mar 17 | Mar 17 | Mar 17 |
| Start Tim | ne (approx.) | 06:54 | 09:02 | 10:25 |
| Stop Tim | ne (approx.) | 07:54 | 10:02 | 11:25 |
| Total Du | ration of Test Run (min.) | 60 | 60 | 60 |
| Net Sam | pling Time (min.) | 60 | 60 | 60 |
| Samplin | g System Calibration Summary | | | |
| | Nozzle ID No: | NA | NA | NA |
| Dn | Nozzle Diameter (in): | NA | NA | NA |
| | Probe ID No: | 67-4-3 | 67-4-3 | 67-4-3 |
| | Meter Box ID. No: | 66-24 | 66-24 | 66-24 |
| Yd | Meter Box Yd - Field Sheet | 0.9904 | 0.9904 | 0.9904 |
| | Meter Box Yd - Database | 0.9904 | 0.9904 | 0.9904 |
| | Meter Box ∆H@ - Field Sheet | 1.7516 | 1.7516 | 1.7516 |
| | Meter Box ∆H@ - Database | 1.7516 | 1.7516 | 1.7516 |
| QA/QC | | | | |
| | Final Leak Check | | | |
| | (a) 4% of Sampling Rate (cfm) | 0.0280 | 0.0280 | 0.0282 |
| | (b) Allowable Rate from Method (cfm) | 0.0200 | 0.0200 | 0.0200 |
| | Allowable Limit - minimum of a and b (cfm) | 0.0200 | 0.0200 | 0.0200 |
| | Actual Final Leak Rate (cfm) | 0.0020 | 0.0020 | 0.0030 |
| | Sample Volume | | | |
| | Minimum Volume Required (dscf) | 30.00 | 30.00 | 30.00 |
| V _{mstd} | Actual Sample Volume (dscf) | 41.238 | 41.007 | 40.731 |
| | Alternative Method 5 Post-Test Calibration (EPA A | LT-009) | | |
| √∆H _{avg} | Average of Square Root of ∆H (in. W.C.) | 1.2247 | 1.2247 | 1.2247 |
| Y _{qa} | Alternative Meter Calibration Factor | 0.9803 | 0.9826 | 0.9823 |
| | Variation from full-test Y_d (average $\leq \pm 5\%$) | -1.0% | -0.8% | -0.8% |

Average -0.9%

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USEPA Method 26A (HCI) QA/QC Results

| Run No | | 1 | 2 | 3 | |
|--------------------|--|----------------|--------|--------------|--|
| Date (20 | 010) | Mar 16 | Mar 16 | Mar 16 | |
| Start Tir | ne (approx.) | 07:17 | 09:04 | 10:32 | |
| Stop Tin | ne (approx.) | 0 8 :17 | 10:04 | 11:32 | |
| Total Du | iration of Test Run (min.) | 60 | 60 | 60 | |
| Net San | npling Time (min.) | 60 | 60 | 60 | |
| <u>Samplir</u> | ng System Callbration Summary | | | | |
| | Nozzle ID No: | NA | NA | NA | |
| Dn | Nozzle Diameter (in): | NA | NA | NA | |
| | Probe ID No: | 67-4-5 | 67-4-5 | 67-4-5 | |
| Cp | Pitot Coefficient: | 0.8400 | 0.8400 | 0.8400 | |
| | Meter Box ID. No: | 61-8 | 61-8 | 61 -8 | |
| Yd | Meter Box Yd - Field Sheet | 0.9916 | 0.9916 | 0.9916 | |
| | Meter Box Yd - Database | 0.9916 | 0.9916 | 0.9916 | |
| | Meter Box ∆H@ - Field Sheet | 1.7580 | 1.7580 | 1.7580 | |
| | Meter Box ∆H@ - Database | 1.7580 | 1.7580 | 1.7580 | |
| QA/QC | | | | | |
| | Final Leak Check | | | | |
| | (a) 4% of Sampling Rate (cfm) | 0.0237 | 0.0242 | 0.0236 | |
| | (b) Allowable Rate from Method (cfm) | 0.0200 | 0.0200 | 0.0200 | |
| | Allowable Limit - minimum of a and b (cfm) | 0.0200 | 0.0200 | 0.0200 | |
| | Actual Final Leak Rate (cfm) | 0.0040 | 0.0030 | 0.0030 | |
| | Sample Volume | | | | |
| | Minimum Volume Required (dscf) | 30.00 | 30.00 | 30.00 | |
| V _{mstd} | Actual Sample Volume (dscf) | 35.389 | 35.831 | 34.777 | |
| | Alternative Method 5 Post-Test Calibration (EPA Al | LT-009) | | | |
| √∆H _{avg} | Average of Square Root of ΔH (in. W.C.) | 1.0757 | 1.0954 | 1.0836 | |
| Y_{qa} | Alternative Meter Calibration Factor | 1.0054 | 1.0078 | 1.0230 | |
| | Variation from full-test Y_d (average $\leq \pm 5\%$) | 1.4% | 1.6% | 3.2% | |

Average 2.1%

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Wheelabrator North Broward, Inc. Clean Air Project No: 10955 Unit 3 FF Outlet

USEPA Method 26A (HCI) QA/QC Results

| Run No. | | 1 | 2 | 3 |
|--------------------|--|-----------------|--------|--------|
| Date (20 | | Mar 16 | Mar 16 | Mar 16 |
| | ie (approx.) | 07:17 | 09:04 | 10:32 |
| • | e (approx.) | 08:17 | 10:04 | 11:32 |
| | ration of Test Run (min.) | 60 | 60 | 60 |
| Net Sam | pling Time (min.) | 60 | 60 | 60 |
| <u>Samplin</u> | g System Calibration Summary | | | |
| | Nozzle ID No: | NA | NA | NA |
| Dn | Nozzle Diameter (in): | NA | NA | NA |
| | Probe ID No: | 67-4-3 | 67-4-3 | 67-4-3 |
| Cp | Pitot Coefficient: | 0.8400 | 0.8400 | 0.8400 |
| | Meter Box ID. No: | 61-11 | 61-11 | 61-11 |
| Yd | Meter Box Yd - Field Sheet | 0.9892 | 0.9892 | 0.9892 |
| | Meter Box Yd - Database | 0.9892 | 0.9892 | 0.9892 |
| | Meter Box ∆H@ - Field Sheet | 1.7379 | 1.7379 | 1.7379 |
| | Meter Box ∆H@ - Database | 1.7379 | 1.7379 | 1.7379 |
| QA/QC | | | | |
| | Final Leak Check | | | |
| | (a) 4% of Sampling Rate (cfm) | 0.0276 | 0.0276 | 0.0277 |
| | (b) Allowable Rate from Method (cfm) | 0.0200 | 0.0200 | 0.0200 |
| | Allowable Limit - minimum of a and b (cfm) | 0.0200 | 0.0200 | 0.0200 |
| | Actual Final Leak Rate (cfm) | 0.0020 | 0.0010 | 0.0020 |
| | Sample Volume | | | |
| | Minimum Volume Required (dscf) | 30.00 | 30.00 | 30.00 |
| V _{mstd} | Actual Sample Volume (dscf) | 42.133 | 41.782 | 41.670 |
| | Alternative Method 5 Post-Test Calibration (EPA AL | <u>.T-009</u>) | | |
| √∆H _{avg} | Average of Square Root of ∆H (in. W.C.) | 1.2247 | 1.2247 | 1.2247 |
| Y_{qa} | Alternative Meter Calibration Factor | 0.9790 | 0.9832 | 0.9811 |
| | Variation from full-test Y_d (average $\leq \pm 5\%$) | -1.0% | -0.6% | -0.8% |

Average -0.8%

041210, 145856 LNK @

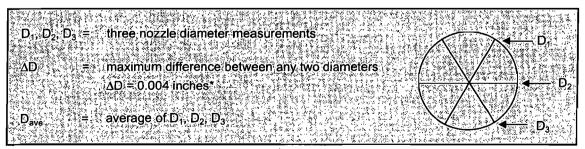
Prepared by Clean Air Engineering Proprietary Software SS ISOKINETIC Version 2006-13d

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Nozzle Calibration Sheet

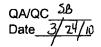
| | Client | Wheeld broton North Roward | Project Number | 0955 |
|-----------------------|---------------|----------------------------|----------------|------|
| Date 3(15/10 Runs - 3 | Calibrated by | 5. Brown | Unit | |
| | Date | 3(15/10 | | -3 |

| | Nozzle Identification | 1.4.4.X0.0.4/ BAY DENT MOL. C. | D ₂ (inches) | D ₃ (inches) | ∆D (inches) | D _{ave} (inches) |
|-------|--------------------------|--------------------------------|----------------------------|----------------------------|----------------|------------------------------|
| 5/29 | 0.270-1 | 0.270 | 0.270 | 0.271 | 0.00) | 0.270 |
| M23 | 0.264-1 | 0,265 | 0.264 | 0.263 | 0.002 | 0.264 |
| M13.B | 0.268-1 | 0.269 | 0.268 | 0.268 | 0.001 | 0.268 |
| inlot | 0.270-2 | 0.271 | 6-270 | 0-270 | 0.001 | 0.270 |
| | 0.270-3 | 0.270 | 0.270 | 0.270 | 0.000 | 0.270 |
| | | | | | | |



* (40 CFR 60, Appendix A, Method 5, Section 5.1)

CDS005A-Nozzie.xls, August 2004 Copyright © 2004 Clean Air Engineering, Inc.





Meter Box Full Test Calibration

Meter Box No: 61-6

Date of Calibration: 7/17/2009

Meter Box Y_d: 0.9900

Calibration conducted by: OLEG LAVROV

Meter Box ∆H@: 1.6820

Barometric Pressure: 29.04

| | | | | | indard Me s Volume (| • | | ter Box G olume (ft ³ | | | td. Met Deratur | - | | eter Box peratur | | Time (min.) | | ration ults |
|-------|------|-------|-----------------|---------|-------------------------|-----------------|---------|-------------------------------------|--------|------|--------------------|-----------------|------|---------------------|----------------|----------------|---------|----------------|
| | | | | | | V _{ds} | | | Vd | | | T _{ds} | | To | T _d | | | |
| Q | ΔH | ΔP | Y _{ds} | Initial | Final | Net | Initial | Final | Net | In | Out | Avg. | In | Out | Avg. | Θ | Yd | ∆н@ |
| 0.965 | 3.00 | -1.70 | 1.0000 | 0.000 | 10.000 | 10.000 | 209.181 | 219.284 | 10.103 | 77.0 | 77.0 | 77.00 | 85.0 | 77.0 | 81.00 | 9.89 | 0.9854 | 1.7309 |
| 0.971 | 3.00 | -1.70 | 1.0000 | 0.000 | 10.000 | 10.000 | 219.284 | 229.389 | 10.105 | 77.0 | 77.0 | 77.00 | 86.0 | 78.0 | 82.00 | 9.82 | 0.9870 | 1.7034 |
| 0.401 | 0.50 | -1.00 | 1.0000 | 0.000 | 5.000 | 5.000 | 234.378 | 239.419 | 5.041 | 77.0 | 77.0 | 77.00 | 81.0 | 78.0 | 79.50 | 11.88 | 0.9927 | 1.6620 |
| 0.401 | 0.50 | -1.00 | 1.0000 | 0.000 | 5.000 | 5.000 | 239.419 | 244.459 | 5.040 | 77.0 | 77.0 | 77.00 | 81.0 | 78.0 | 79.50 | 11.90 | 0.9929 | 1.6676 |
| 0.695 | 1.50 | -1.50 | 1.0000 | 0.000 | 10.000 | 10.000 | 253.277 | 263.387 | 10.110 | 76.0 | 76.0 | 76.00 | 84.0 | 79.0 | 81.50 | 13.76 | 0.9917 | 1.6629 |
| 0.694 | 1.50 | -1.50 | 1.0000 | 0.000 | 10.000 | 10.000 | 263.387 | 273.514 | 10.127 | 76.0 | 76.0 | 76.00 | 84.0 | 79.0 | 81.50 | 13.77 | 0.9900 | 1.6653 |
| | | | | | | | | | | | | | | | Ā | verages | 0.98996 | 1.68200 |

| Nomenclature | Equations |
|--|--|
| $\begin{array}{lll} P_b & \text{Barometric Pressure (in. Hg)} \\ Q & \text{Flow Rate (cfm)} \\ \Delta H & \text{Orifice Pressure differential (in. H_2O)} \\ \Delta P & \text{Inlet Pressure Differential (in. H_2O)} \\ V_d & \text{Gas Meter Volume - Dry (ft^3)} \\ V_{ds} & \text{Standard Meter Volume - Dry (ft^3)} \\ T_d & \text{Average Meter Box Temperature ("F)} \\ T_o & \text{Outlet Meter Box Temperature ("F)} \\ T_{ds} & \text{Average Standard Meter Temperature ("F)} \\ T_d & \text{Meter Correction Factor (unitless)}, Y_i \leq Y_{avg} \pm 0.02 \\ Y_{ds} & \text{Standard Meter Correction Factor (unitless)} \\ \Delta H@ & \text{Orifice Pressure Differential giving 0.75 cfm} \\ \text{of air at 68"F and 29.92 in. Hg (in. H_2O)} \\ \Delta H@_{avg} \pm 0.2 \\ \Theta & \text{Duration of Run (minutes)} \end{array}$ | $Y_{d} = (Y_{ds}) \left[\frac{V_{ds}}{V_{d}} \right] \left[\frac{T_{d} + 460}{T_{ds} + 460} \right] \left[\frac{P_{b} + \Delta P / 13.6}{P_{b} + \Delta H / 13.6} \right]$ $\Delta H @= \frac{(0.0319)(\Delta H)}{P_{b}(T_{o} + 460)} \left[\frac{(T_{ds} + 460)\Theta}{(V_{ds})(Y_{ds})} \right]^{2}$ $Q = \frac{17.64(V_{ds})(P_{b})}{(T_{ds} + 460)(\Theta)}$ |

| Standard | Gauge |
|----------|---------|
| (in.Hg) | (in.Hg) |
| 5.6 | 5.0 |
| 10.7 | 10.0 |
| 15.4 | 15.0 |
| 20.4 | 20.0 |
| 24.8 | 24.7 |
| | |
| | |
| | |



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Meter Box - Pyrometer Calibration Sheet

Meter Box No: 61-6

Calibrated by: OLEG LAVROV

Date:

1/18/08

Client: _____

Type of Calibration: Full-Test

Office:

Temperature Scale Used: Fahrenheit

Pyrometer Reading Calibration for each Channel Reference Settings (°F) (°F) Stack Probe Filter Imp Out DGM In DGM Out Aux

Tolerance = ±2°F difference from reference setting.

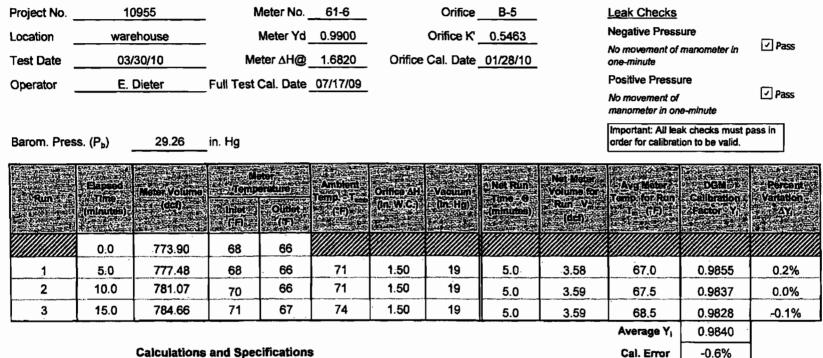
Calibration Reference Information

| Reference Used: | Omega CL23A | Serial No: | T-225950 |
|------------------------|--------------|------------|-----------|
| Calibrated By: | JH Metrology | Exp date : | 6/22/2010 |
| Calibration Report No: | R044791 | | |
| | | | |





Meter Box Critical Orifice Post-Test Calibration Data



Calculations and Specifications

$$Y_{i} = \frac{K \times P_{b} \times (T_{m} + 460) \times \theta}{17.64 \times V_{m} \times (P_{b} + \Delta H_{13.6}) \times \sqrt{T_{amb} + 460}}$$
$$\Delta Y_{i} = \frac{Y_{i} - \overline{Y}_{i}}{\overline{Y}_{i}} \times 100 \qquad \text{Spec.} : \Delta Y_{i} \le \pm 2\%$$
$$Cal.Error = \frac{\overline{Y}_{i} - Y_{d}}{Y_{d}} \times 100 \qquad \text{Spec.} : Cal.Error \le \pm 5\%$$

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Meter Box Full Test Calibration

Meter Box No: 61-8

Date of Calibration: 5/11/2009

•

Meter Box Y_d: 0.9916

Calibration Conducted by: OLEG LAVROV

Meter Box △H@: 1.7580

Barometric Pressure: 29.39

| | | | | | andard Me s Volume | | | ter Box G olume (ft ³ | | Std. Meter Temperature (*F) | | | Meter Box Temperature ('F) | | | Time (min.) | Calibr Res | ration ults |
|-------|------|-------|--------|---------|-----------------------|-----------------|---------|-------------------------------------|--------|--------------------------------|------|-----------------|-------------------------------|------|----------------|----------------|---------------|----------------|
| | | | | | | V _{ds} | | | Vd | Tis | Tos | T _{ds} | Τi | T。 | T _d | | | |
| Q | ΔH | ΔΡ | Yds | Initial | Final | Net | Initial | Final | Net | In | Out | Avg. | In | Out | Avg. | Θ | Ya | ∆н@ |
| 0.984 | 3.00 | -1.70 | 1.0000 | 0.000 | 10.000 | 10.000 | 62.712 | 72.772 | 10.060 | 68.0 | 68.0 | 68.00 | 73.0 | 69.0 | 71.00 | 9.98 | 0.9880 | 1.7092 |
| 0.972 | 3.00 | -1.70 | 1.0000 | 0.000 | 10.000 | 10.000 | 72.772 | 82.872 | 10.100 | 68.0 | 68.0 | 68.00 | 76.0 | 70.0 | 73.00 | 10.10 | 0.9878 | 1.7472 |
| 0.387 | 0.50 | -1.10 | 1.0000 | 0.000 | 5.000 | 5.000 | 86.333 | 91.393 | 5.060 | 68.0 | 68.0 | 68.00 | 75.0 | 72.0 | 73.50 | 12.68 | 0.9944 | 1.8290 |
| 0.385 | 0.50 | -1.10 | 1.0000 | 0.000 | 5.000 | 5.000 | 91.393 | 96.466 | 5.073 | 68.0 | 68.0 | 68.00 | 75.0 | 73.0 | 74.00 | 12.76 | 0.9928 | 1.8487 |
| 0.692 | 1.50 | -1.30 | 1.0000 | 0.000 | 10.000 | 10.000 | 98.815 | 108.963 | 10.148 | 68.0 | 68.0 | 68.00 | 78.0 | 73.0 | 75.50 | 14.19 | 0.9924 | 1.7147 |
| 0.694 | 1.50 | -1.30 | 1.0000 | 0.000 | 10.000 | 10.000 | 108.963 | 119.111 | 10.148 | 68.0 | 68.0 | 68.00 | 79.0 | 74.0 | 76.50 | 14.14 | 0.9943 | 1.6994 |
| | | | | | | | | | | | | | | | A | verages | 0.99164 | 1.75804 |

| | Nomenclature | Equations |
|--|--|--|
| ₽ _δ Q ΔH ΔP Vd Td To Tds Yd Yds ΔH@ | Barometric Pressure (in. Hg) Flow Rate (cfm) Orifice Pressure differential (in. H ₂ O) Inlet Pressure Differential (in. H ₂ O) Gas Meter Volume - Dry (ft ³) Standard Meter Volume - Dry (ft ³) Average Meter Box Temperature ("F) Outlet Meter Box Temperature ("F) Average Standard Meter Temperature ("F) Meter Correction Factor (unitless), Y ₁ \leq Y _{avg} ±0.02 Standard Meter Correction Factor (unitless) Orifice Pressure Differential giving 0.75 cfm of air at 68"F and 29.92 in. Hg (in. H ₂ O) Δ H@ ₁ \leq Δ H@ _{evg} ±0.2 Duration of Run (minutes) | $Y_{d} = (Y_{ds}) \left[\frac{V_{ds}}{V_{d}} \right] \left[\frac{T_{d} + 460}{T_{ds} + 460} \right] \left[\frac{P_{b} + \Delta P / 13.6}{P_{b} + \Delta H / 13.6} \right]$ $\Delta H @= \frac{(0.0319)(\Delta H)}{P_{b}(T_{o} + 460)} \left[\frac{(T_{ds} + 460)\Theta}{(V_{ds})(Y_{ds})} \right]^{2}$ $Q = \frac{17.64(V_{ds})(P_{b})}{(T_{ds} + 460)(\Theta)}$ |

| | Vacuum | Gauge |
|---|----------|---------|
| | Standard | Gauge |
| ł | (in.Hg) | (in.Hg) |
| | 4.7 | 5.0 |
| | 9.6 | 10.0 |
| | 14.6 | 15.0 |
| | 19.5 | 20.0 |
| | 23.3 | 24.0 |
| | | |
| | | |
| | | |



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Meter Box - Pyrometer Calibration Sheet

Meter Box No: 61-8

Calibrated by: OLEG LAVROV

Date:

Office:

Client:

Job No:

Temperature Scale Used: Fahrenheit

5/11/09

Type of Calibration: Full-Test

| Calibration Reference Settings | | Pyrometer Reading for each Channel (°F) | | | | | | | | | | | | |
|--------------------------------------|-------|---|--------|---------|-----|--------|---------|--|--|--|--|--|--|--|
| (°F) | 1 | 2 | 3 | 4 | 5 | 6 | 7 | | | | | | | |
| | Stack | Probe | Filter | Imp Out | Aux | DGM In | DGM Out | | | | | | | |
| 50 | 49 | 49 | 48 | | | | | | | | | | | |
| 100 | 99 | 99 | 98 | | | | | | | | | | | |
| 150 | 149 | 149 | 149 | | _ | | | | | | | | | |
| 200 | 199 | 199 | 199 | | | | | | | | | | | |
| 250 | 250 | 249 | 249 | | | | | | | | | | | |
| 300 | 300 | 299 | 299 | | | | | | | | | | | |
| 350 | 350 | 349 | 350 | | | | | | | | | | | |
| 400 | 400 | 399 | 399 | | | | | | | | | | | |
| 450 | 450 | 449 | 449 | | | | | | | | | | | |
| 500 | 500 | 499 | 499 | | | | | | | | | | | |
| 550 | 549 | 549 | 549 | | | | | | | | | | | |
| 600 | 599 | 599 | 599 | | | | | | | | | | | |

Tolerance = ±2°F difference from reference setting.

Calibration Reference Information

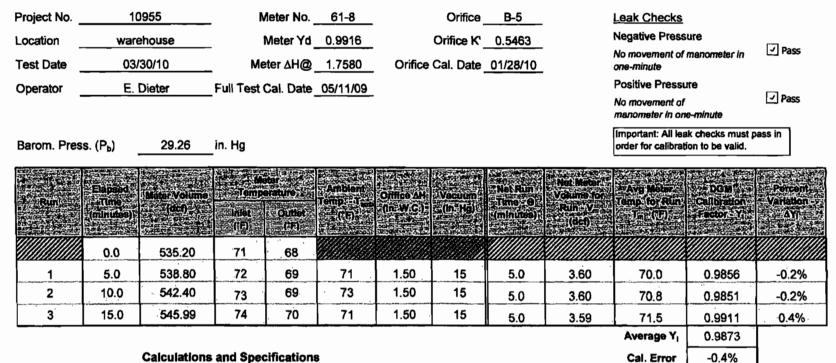
| Reference Used: | Omega CL23A | Serial No: | T-225950 |
|-----------------------|--------------|------------|------------|
| Calibrated By: | JH Metrology | Exp. Date: | 10/13/2009 |
| Calibration Report No | p: | | |
| | | | |



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Meter Box Critical Orifice Post-Test Calibration Data



Calculations and Specifications

$$Y_{l} = \frac{K \times P_{b} \times (T_{m} + 460) \times \theta}{17.64 \times V_{m} \times (P_{b} + \Delta H_{13.6}) \times \sqrt{T_{amb} + 460}}$$
$$\Delta Y_{l} = \frac{Y_{l} - \overline{Y}_{l}}{\overline{Y}_{l}} \times 100 \qquad \text{Spec.: } \Delta Y_{l} \le \pm 2\%$$
$$Cal.Error = \frac{\overline{Y}_{l} - Y_{d}}{Y_{l}} \times 100 \qquad \text{Spec.: } Cal.Error \le \pm 5\%$$

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Meter Box Full Test Calibration

Meter Box No: 61-11

Date of Calibration: 7/20/2009

Meter Box Y_d: 0.9892

Calibration Conducted by: ____OLEG LAVROV

Meter Box ∆H@: 1.7379

Barometric Pressure: 29.33

| | | | | | ndard Me Volume | | | Meter Box GasStd. MeterVolume (ft3)Temperature ("F) | | | Meter Box Temperature (°F) | | | Time (min.) | | libration esults | | |
|-------|------|-------|-----------------|---------|--------------------|-----------------|---------|---|--------|-----------------|-------------------------------|-----------------|----------------|----------------|----------------|---------------------|--------|--------|
| | | | | | | V _{ds} | | | Vd | T _{is} | Tos | T _{ds} | T _i | T _o | T _d | | | |
| Q | ΔH | ΔP | Y _{ds} | Initial | Final | Net | Initial | Final | Net | ١n | Out | Avg. | ิเก | Out | Avg. | Θ | Yd | ∆H@ |
| 0.967 | 3.00 | -1.80 | 1.0000 | 0.000 | 10.000 | 10.000 | 659.039 | 669.161 | 10.122 | 74.0 | 74.0 | 74.00 | 84.0 | 75.0 | 79.50 | 10.02 | 0.9862 | 1.7461 |
| 0.965 | 3.00 | -1.80 | 1.0000 | 0.000 | 10.000 | 10.000 | 669,161 | 679.296 | 10.135 | 74.0 | 74.0 | 74.00 | 86.0 | 77.0 | 81.50 | 10.04 | 0.9886 | 1.7465 |
| 0.393 | 0.50 | -1.10 | 1.0000 | 0.000 | 5.000 | 5.000 | 688.693 | 693.774 | 5.081 | 74.0 | 74.0 | 74.00 | 81.0 | 78.0 | 79.50 | 12.32 | 0.9902 | 1.7500 |
| 0.399 | 0.50 | -1.10 | 1.0000 | 0.000 | 5.500 | 5.500 | 693.774 | 699.354 | 5.580 | 74.0 | 74.0 | 74.00 | 81.0 | 78.0 | 79.50 | 13.36 | 0.9918 | 1.7007 |
| 0.682 | 1.50 | -1.40 | 1.0000 | 0.000 | 10.000 | 10.000 | 701.953 | 712.144 | 10.191 | 74.5 | 74.5 | 74.50 | 86.0 | 79.0 | 82.50 | 14.20 | 0.9887 | 1.7436 |
| 0.682 | 1.50 | -1.40 | 1.0000 | 0.000 | 10.000 | 10.000 | 712.144 | 722.346 | 10.202 | 74.5 | 74.5 | 74.50 | 87.0 | 80.0 | 83.50 | 14.20 | 0.9895 | 1.7404 |
| | - | | | | Averages 0.989 | | | | | | | | | | 0.98917 | 1.73789 | | |

| | Nomenclature | Equations |
|---|---|--|
| Q ΔH ΔP Vd Vd Td Td Td Yd Yd ΔH Q 4 4 4 4 4 4 4 4 4 4 4 4 4 | Barometric Pressure (in. Hg) Flow Rate (cfm) Orifice Pressure differential (in. H ₂ O) Inlet Pressure Differential (in. H ₂ O) Gas Meter Volume - Dry (ft ³) Standard Meter Volume - Dry (ft ³) Average Meter Box Temperature (*F) Outlet Meter Box Temperature (*F) Average Standard Meter Temperature (*F) Meter Correction Factor (unitless), Y ₁ ≤Y _{avg} ±0.02 Standard Meter Correction Factor (unitless) Orifice Pressure Differential giving 0.75 cfm of air at 68°F and 29.92 in. Hg (in. H ₂ O) $\Delta H@_i \leq \Delta H@_{avg} \pm 0.2$ Duration of Run (minutes) | $Y_{d} = (Y_{ds}) \left[\frac{V_{ds}}{V_{d}} \right] \left[\frac{T_{d} + 460}{T_{ds} + 460} \right] \left[\frac{P_{b} + \Delta P / 13.6}{P_{b} + \Delta H / 13.6} \right]$ $\Delta H @= \frac{(0.0319)(\Delta H)}{P_{b}(T_{o} + 460)} \left[\frac{(T_{ds} + 460)\Theta}{(V_{ds})(Y_{ds})} \right]^{2}$ $Q = \frac{17.64(V_{ds})(P_{b})}{(T_{ds} + 460)(\Theta)}$ |

| Standard | Gauge |
|----------|---------|
| (in.Hg) | (in.Hg) |
| 5.3 | 5.0 |
| 10.2 | 10.0 |
| 14.9 | 15.0 |
| 19.7 | 20.0 |
| 24.4 | 25.0 |
| | |
| | |
| | |



COSCIEC-Mater Full April 2004a Convicte to 2004 Clasm Air Engineerie

Meter Box - Pyrometer Calibration Sheet

Meter Box No: 61-11

Calibrated by: OLEG LAVROV

Date:

Office: Client:

Job No:

Type of Calibration: Full-Test

7/20/09

Temperature Scale Used: Fahrenheit

| Calibration Reference Settings | Pyrometer Reading for each Channel (°F) | | | | | | | | | | |
|--------------------------------------|---|-----------------|--------|---------|-----|---------------------|---------|--|--|--|--|
| (°F) | 1 | 2 | 3 | 4 | 5 | 6 | 7 | | | | |
| | Stack | Probe | Filter | Imp Out | Aux | DGM In | DGM Out | | | | |
| 50 | 48 | 49 | 48 | | | | | | | | |
| 100 | 98 | 99 | 98 | | | | | | | | |
| 150 | 148 | 149 | 148 | | | | | | | | |
| 200 | 198 | 199 | 198 | | | | | | | | |
| 250 | 248 | 249 | 248 | | | | 建設設 | | | | |
| 300 | 298 | 299 | 298 | | | 的認識 | | | | | |
| 350 | 348 | 349 | 348 | | | $\overline{\gamma}$ | | | | | |
| 400 | 398 | 39 9 | 398 | | 調整 | | | | | | |
| 450 | 448 | 449 | 448 | | | | | | | | |
| 500 | 498 | 499 | 498 | | | | | | | | |
| 550 | 548 | 549 | 548 | | | | | | | | |
| 600 | 59 8 | 599 | 598 | | 國語言 | | | | | | |

Tolerance = ±2°F difference from reference setting.

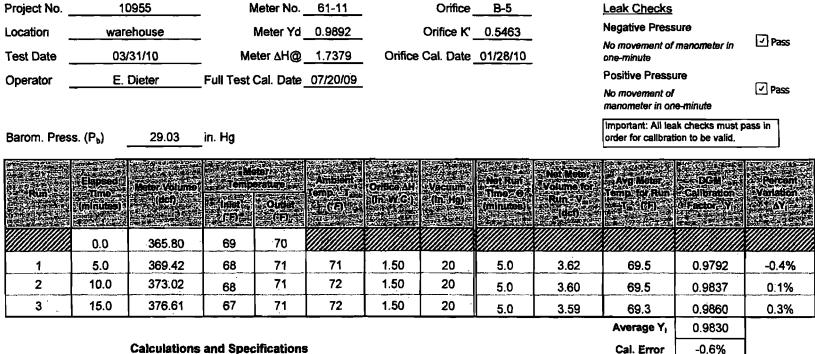
Calibration Reference Information

| Reference Used: | Omega CL23A | Serial No: | T-225950 |
|------------------------|--------------|------------|-----------|
| Calibrated By: | JH Metrology | Exp date : | 6/22/2010 |
| Calibration Report No: | R044701 | | |
| | | | |



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Meter Box Critical Orifice Post-Test Calibration Data



Calculations and Specifications

$$Y_{i} = \frac{K \times P_{b} \times (T_{m} + 460) \times \theta}{17.64 \times V_{m} \times (P_{b} + \Delta H_{13.6}) \times \sqrt{T_{amb} + 460}}$$
$$\Delta Y_{i} = \frac{Y_{i} - \overline{Y}_{i}}{\overline{Y}_{i}} \times 100 \qquad \text{Spec. : } \Delta Y_{i} \le \pm 2\%$$
$$Cal \ Error = \frac{\overline{Y}_{i} - Y_{d}}{Y_{i}} \times 100 \qquad \text{Spec. : } Cal \ Error \le \pm 5\%$$

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Meter Box Full Test Calibration

Meter Box No:

66-6

Date of Calibration: 1/12/2010

Meter Box Y_d: 0.9901

Calibration Conducted by: OLEG LAVROV

Barometric Pressure: 29.64

Meter Box ∆H@: 1.7870

| | Standard Meter Gas Volume (ft ³) | | | | ter Box G olume (ft ³ | | | | | | eter Box perature | | Time (min.) | _ | bration sults | | | |
|-------|---|-------|-----------------|------------------|-------------------------------------|-----------------|---------|---------|--------|-----------------|----------------------|-----------------|----------------|------|------------------|--------|--------|--------|
| T | | | | | | V _{ds} | | | Vd | T _{is} | Tos | T _{ds} | Ti | T, | Td | | | |
| Q | ΔН | ΔP | Y _{ds} | Initial | Final | Net | Initial | Final | Net | In | Out | Avg. | In | Out | Avg. | Θ | Yd | ∆H@ |
| 0.957 | 3.00 | -1.80 | 1.0000 | 0.000 | 10.000 | 10.000 | 595.744 | 605.900 | 10.156 | 67.0 | 67.0 | 67.00 | 77.0 | 74.0 | 75.50 | 10.37 | 0.9887 | 1.8058 |
| 0.956 | 3.00 | -1.80 | 1.0000 | 0.000 | 10.000 | 10.000 | 605.900 | 616.056 | 10.156 | 67.0 | 67.0 | 67.00 | 78.0 | 75.0 | 76.50 | 10.38 | 0.9905 | 1.8059 |
| 0.390 | 0.50 | -1.20 | 1.0000 | 0.000 | 5.000 | 5.000 | 624.508 | 629.613 | 5.105 | 67.0 | 67.0 | 67.00 | 77.0 | 75.0 | 76.00 | 12.71 | 0.9920 | 1.8051 |
| 0.390 | 0.50 | -1.20 | 1.0000 | 0.000 | 6.000 | 6.000 | 629.613 | 635.743 | 6.130 | 67.0 | 67.0 | 67.00 | 77.0 | 75.0 | 76.00 | 15.28 | 0.9913 | 1.8117 |
| 0.687 | 1.50 | -1.50 | 1.0000 | 0.000 | 10.000 | 10.000 | 644.660 | 654.890 | 10.230 | 67.0 | 67.0 | 67.00 | 79.0 | 76.0 | 77.50 | 14.45 | 0.9896 | 1.7466 |
| 0.687 | 1.50 | -1.50 | 1.0000 | 0.000 | 10.000 | 10.000 | 654.890 | 665.132 | 10.242 | 67.0 | 67.0 | 67.00 | 79.0 | 76.0 | 77.50 | 14.45 | 0.9884 | 1.7466 |
| | | | | Averages 0.99009 | | | | | | | | | | | | 1,7869 | | |

| Averages 0.9 | 9009 1.78696 |
|--------------|--------------|
|--------------|--------------|

| | Nomenclature | Equations |
|---|--|--|
| P _b Q ΔH ΔP V _{ds} T _d T _d Y _d Y _d ΔH@ | Barometric Pressure (in. Hg) Flow Rate (cfm) Orifice Pressure differential (in. H ₂ O) Inlet Pressure Differential (in. H ₂ O) Gas Meter Volume - Dry (ft ³) Standard Meter Volume - Dry (ft ⁴) Average Meter Box Temperature ("F) Outlet Meter Box Temperature ("F) Average Standard Meter Temperature ("F) Meter Correction Factor (unitless), Y ₁ \leq Y _{avg} ±0.02 Standard Meter Correction Factor (unitless) Orifice Pressure Differential giving 0.75 cfm of air at 68"F and 29.92 in. Hg (in. H ₂ O) Δ H@ ₄ \leq Δ H@ _{avg} ±0.2 Duration of Run (minutes) | $Y_{d} = (Y_{ds}) \left[\frac{V_{ds}}{V_{d}} \right] \left[\frac{T_{d} + 460}{T_{ds} + 460} \right] \left[\frac{P_{b} + \Delta P / 13.6}{P_{b} + \Delta H / 13.6} \right]$ $\Delta H @= \frac{(0.0319)(\Delta H)}{P_{b}(T_{o} + 460)} \left[\frac{(T_{ds} + 460)\Theta}{(V_{ds})(Y_{ds})} \right]^{2}$ $Q = \frac{17.64(V_{ds})(P_{b})}{(T_{ds} + 460)(\Theta)}$ |

| _ | Vacuum | Gauge_ |
|---|----------|----------|
| | Standard | Gauge |
| | (in.Hg) | (in.Hg) |
| | 5.2 | 5.0 |
| | 10.1 | 10.0 |
| | 15.3 | 15.0 |
| | 20.2 | 20.0 |
| | 24.9 | 25.0 |
| | | |
| | | |
| | | <u> </u> |



Meter Box - Pyrometer Calibration Sheet

| Meter Box No: | 66-6 | Office: |
|-------------------|--------------------|--------------------------------|
| Calibrated by: | OLEG LAVROV | Client: |
| Date: | 1/12/10 | Job No: |
| Temperature Scale | e Used: Fahrenheit | Type of Calibration: Full-Test |

| Calibration Reference Settings | | Pyrometer Reading for each Channel (°F) | | | | | | | | |
|--------------------------------------|-------|---|--------|---------|-----|--------|----------------|--|--|--|
| (°F) | 1 | 2 | 3 | 4 | 5 | 6 | 7 | | | |
| | Stack | Probe | Filter | Imp Out | Aux | DGM In | DGM Out | | | |
| 50 | 49 | 51 | 51 | | | | | | | |
| 100 | 99 | 101 | 101 | | | | | | | |
| 150 | 149 | 151 | 151 | | | | | | | |
| 200 | 199 | 201 | 201 | | | | | | | |
| 250 | 249 | 251 | 250 | | | | | | | |
| 300 | 299 | 301 | 300 | | | | | | | |
| 350 | 349 | 351 | 350 | | | | | | | |
| 400 | 399 | 401 | 400 | | | | REMOVED STATES | | | |
| 450 | 449 | 451 | 450 | | | | | | | |
| 500 | 499 | 501 | 500 | | | | | | | |
| 550 | 549 | 551 | 550 | | | | | | | |
| 600 | 599 | 601 | 600 | | | | | | | |

Tolerance = ±2°F difference from reference setting.

Calibration Reference Information

Reference Used: Omega CL23A Calibrated By: JH Metrology

Serial No:

Date Calibrated:

Calibration Report No: R044701



T-225950

10/7/2010

COSDOSC-Meter Fuß, April 2004a Copyright © 2004 Clean Air Engineering Inc.

Meter Box Critical Orifice Post-Test Calibration Data

| 1 | Project No. | 10 | 955 | N | leter No. | 66-6 | | Orifice | C-5 | | Leak Checks | | |
|--|-------------|-------------------|----------------------|---------------------------------|--------------|-----------------------|-----------|-----------|--|---|---|-------------|------------------------|
| ļ | Location | ware | ehouse | | Meter Yd | 0.9901 | | Orifice K | 0.5643 | | Negative Pressure | | [] |
| | Test Date | 03/ | 31/10 | Me | ter ∆H@ | 1.7870 | Orifice | Cal. Date | 02/03/10 | | No movement of manometer in one-minute | | ✓ Pass |
| , | Operator | E. | Dieter | Full Test | Cal. Date | 01/12/10 | | | | | Positive Pressu | Ire | _ |
| | | | | • | | | | | | | No movement of manometer in on | | ✓ Pass |
| Barom, Press. (P _b) 29.03 in. Hg | | | | | | | | | Important: All lea order for calibrat | , | ass in | | |
| | | | | Laboration of the second second | 101 | | | | Net Run v | Net Meter | Ave Meter | | |
| | Run | | Meter sVolume | Contraction of the local state | eruteri | Amblent- Temps-Tem | Office AH | -Vecuum | | all a second back of a second s | Temp (or Run | Calibration | Purcent. Vertetion6 |
| | | (esturior) | (dci) | | Outer (E) | - 10- | | | (minutes)) | Rún: V _a Sí (def)r | TE ED | Factor 11, | AY. |
| | | 0.0 | 47.30 | 72 | 71 | | | | | | | | |
| | 1 | 5.0 | 51.04 | 72 | 71 | 70 | 1.70 | 18 | 5.0 | 3.74 | 71.5 | 0.9831 | -0.3% |
| | 2 | 10.0 ⁻ | 54.77 | 73 | 71 | 70 | 1.70 | 18 | 5.0 | 3.73 | 71.8 | 0.9862 | 0.0% |
| | 3 | 15.0 | 58.49 | 73 | 72 | 71 | 1.70 | 18 | .5.0 | 3.72 | 72.3 | 0.9889 | 0.3% |

Calculations and Specifications

$$Y_{i} = \frac{K \times P_{b} \times (T_{m} + 460) \times \theta}{17.64 \times V_{m} \times (P_{b} + \Delta H_{13.6}) \times \sqrt{T_{amb} + 460}}$$
$$\Delta Y_{i} = \frac{Y_{i} - \overline{Y}_{i}}{\overline{Y}_{i}} \times 100 \qquad \text{Spec.: } \Delta Y_{i} \le \pm 2\%$$
$$Cal.Error = \frac{\overline{Y}_{i} - Y_{d}}{Y_{d}} \times 100 \qquad \text{Spec.: } Cal.Error \le \pm 5\%$$

<u>CleanAir</u>

Average Y

Cal. Error

0.9861

-0.4%

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Meter Box Full Test Calibration

Meter Box No:

66-14

Date of Calibration: 8/17/2009

Meter Box Y_d: 0.9898

Calibration Conducted by: 0. Lavrov

Meter Box ∆H@: 1.7643

Barometric Pressure: 29.21

| | | | | Standard Meter Gas Volume (ft ³) | | | | Meter Box Gas Volume (ft ³) | | - | Std. Meter Temperature ('F) | | | Meter Box Temperature ('F) | | Time (min.) | | ration ults |
|-------|------|-------|-----------------|---|--------|-----------------|---------|--|--------|-----------------|--------------------------------|-----------------|----------------|-------------------------------|----------------|----------------|---------|----------------|
| I | | | | | | V _{ds} | | | Vd | T _{is} | Tos | T _{ds} | T _i | To | Τ _d | | | |
| Q | ΔH | ΔP | Y _{ds} | Initial | Final | Net | Initial | Final | Net | In | Out | Avg. | In | Out | Avg. | Θ | Yd | ∆H@ |
| 0.943 | 3.00 | -1.80 | 1.0000 | 0.000 | 10.000 | 10.000 | 473.148 | 483.260 | 10,112 | 77.0 | 77.0 | 77.00 | 86.0 | 79.0 | 82.50 | 10.18 | 0.9871 | 1.8165 |
| 0.938 | 3.00 | -1.80 | 1.0000 | 0.000 | 10.000 | 10.000 | 483.260 | 493.403 | 10.143 | 77.0 | 77.0 | 77.00 | 88.0 | 81.0 | 84.50 | 10.23 | 0.9877 | 1.8276 |
| 0.392 | 0.50 | -1.20 | 1.0000 | 0.000 | 5.000 | 5.000 | 502.282 | 507.357 | 5.075 | 77.0 | 77.0 | 77.00 | 85.0 | 82.0 | 83.50 | 12.24 | 0.9929 | 1.7410 |
| 0.392 | 0.50 | -1.20 | 1.0000 | 0.000 | 5.000 | 5.000 | 507.357 | 512.444 | 5.087 | 77.0 | 77.0 | 77.00 | 85.0 | 82.0 | 83.50 | 12.25 | 0.9905 | 1.7439 |
| 0.680 | 1.50 | -1.40 | 1.0000 | 0.000 | 10.000 | 10.000 | 521.145 | 531.347 | 10.202 | 77.5 | 77.5 | 77.50 | 89.0 | 84.0 | 86.50 | 14.09 | 0.9894 | 1.7272 |
| 0.680 | 1.50 | -1.40 | 1.0000 | 0.000 | 10.000 | 10.000 | 531.347 | 541.532 | 10.185 | 77.5 | 77.5 | 77.50 | 89.0 | 84.0 | 86.50 | 14.10 | 0.9910 | 1.7296 |
| | | | | | | | | | i | | | | | | `A | verages | 0.98976 | 1.76429 |

| | Nomenclature | Equations |
|---|--|---|
| $\begin{array}{c} P_b \\ Q \\ \Delta H \\ \Delta P \\ V_d \\ T_d \\ T_o \\ T_{ds} \\ Y_d \\ Y_{ds} \\ \Delta H \\ \Theta \end{array}$ | Barometric Pressure (in. Hg) Flow Rate (cfm) Orifice Pressure differential (in. H ₂ O) Inlet Pressure Differential (in. H ₂ O) Gas Meter Volume - Dry (ft ⁴) Standard Meter Volume - Dry (ft ⁴) Average Meter Box Temperature (*F) Outlet Meter Box Temperature (*F) Average Standard Meter Temperature (*F) Meter Correction Factor (unitless), Y ₁ \leq Y _{avg} \pm 0.02 Standard Meter Correction Factor (unitless) Orifice Pressure Differential giving 0.75 cfm of air at 68*F and 29.92 in. Hg (in. H ₂ O) Δ H@ ₁ \leq Δ H@ _{avg} \pm 0.2 Duration of Run (minutes) | $Y_{d} = (Y_{ds}) \left[\frac{V_{ds}}{V_{d}} \right] \left[\frac{T_{d} + 460}{T_{ds} + 460} \right] \left[\frac{P_{b} + \Delta P / 13.6}{P_{b} + \Delta H / 13.6} \right]$ $\Delta H @ = \frac{(0.0319)(\Delta H)}{P_{b}(T_{o} + 460)} \left[\frac{(T_{ds} + 460)\Theta}{(V_{ds})(Y_{ds})} \right]^{2}$ $Q = \frac{17.64(V_{ds})(P_{b})}{(T_{ds} + 460)(\Theta)}$ |

| _Vacuum | Gauge |
|----------|---------|
| Standard | Gauge |
| (in.Hg) | (in.Hg) |
| 5.6 | 5.0 |
| 10.5 | 10.0 |
| 15.8 | 15.0 |
| 20.6 | 20.0 |
| 25.2 | 25.0 |
| | |
| | |
| | |



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Meter Box - Pyrometer Calibration Sheet

| Meter Box No: | 66-14 | Office: | |
|------------------|--------------------|----------------------|-----------|
| Calibrated by: | O. Lavrov | Client: | |
| Date: | 8/17/09 | Job No: | |
| Temperature Scal | e Used: Fahrenheit | Type of Calibration: | Full-Test |

| Calibration Reference Settings | | Pyrometer Reading for each Channel (°F) | | | | | | | | | |
|--------------------------------------|-------|---|--------|---------|-----------|----------|---------|--|--|--|--|
| (°F) | 1 | 2 | 3 | 4 | 5 | 6 | 7 | | | | |
| | Stack | Probe | Filter | Imp Out | Aux | DGM In | DGM Out | | | | |
| 50 | 49 | 51 | 52 | | | | | | | | |
| 100 | 99 | 101 | . 102 | | | | | | | | |
| 150 | 149 | 151 | 151 | | | | | | | | |
| 200 | 199 | 201 | 202 | | | li e e e | | | | | |
| 250 | 249 | 251 | 252 | | | | | | | | |
| 300 | 299 | 301 | 302 | | | · · · | · · · | | | | |
| 350 | 349 | 351 | 351 | | | | | | | | |
| 400 | 399 | 401 | 402 | | | | | | | | |
| 450 | 449 | 451 | 452 | | | | | | | | |
| 500 | 499 | 501 | 502 | | · · · · · | | | | | | |
| 550 | 549 | 551 | 551 | | | | | | | | |
| 600 | 599 | 601 | 602 | | | | | | | | |

Tolerance = ±2°F difference from reference setting.

Serial No:

Exp.date :

Calibration Reference Information

Reference Used: Omega CL23A

Calibrated By: JH Metrology

Calibration Report No: _____R044701

T-225950

6/22/2010

Meter Box Critical Orifice Post-Test Calibration Data

| Project No. | 1(| 0955 | | Aeter No. | 66-14 | | Orifice | C-5 | | Leak Checks | | |
|--|-----------------|--------------|---------------|-----------|----------------------|-------------------------|------------|-----------|------------------------------------|-----------------------------------|--------------|------------|
| Location | ware | ehouse | _ | Meter Yd | 0.9898 | | Orifice K' | 0.5643 | | Negative Press | ure | |
| Test Date | 03/ | /30/10 | Me | eter ∆H@ | 1.7643 | Orifice | Cal. Date | 02/03/10 | | No movement of one-minute | manometer in | 🗹 Pass |
| Operator | E. | Dieter | Full Test | Cal. Date | 08/17/09 | | | | | Positive Pressu | Jre | - |
| | | | | · | | | | | | No movement of manometer in on | | Pass |
| Barom, Press. (P _b) 29.26 in. Hg | | | | | | | | | | bass in | | |
| Rin | Elapsed Time | Meter Volume | | erature | Amblent Temp: Tem | Ornice AH -(In-W(C)) | Vection | Net Run | Net deter Volume to? Run: Va | | Calibration | |
| | (minutas) | | Jnlet (TF) | Outlet a | | | | (minutes) | (def) | र्सान (ग्रिस | Pactor 7 | $\sim N_0$ |
| | 0.0 | 753.30 | 73 | 71 | | | | | | | | |
| 1 | 5.0 | 756.99 | 72 | 70 | 74 | 1.70 | 19 | 5.0 | 3.69 | 71.5 | 0.9927 | 0.0% |
| 2 | 10.0 | 760.71 | 74 | 71 | 74 | . 1.70 | 19 | · 5.0 | 3.72 | 71.8 | 0.9852 | -0.8% |
| 3 | 15.0 | 764.38 | 75 | 71 | 73 | 1.70 | 19 | 5.0 | 3.67 | 72.8 | 1.0014 | 0.8% |
| | | | | | | | | | | Average Y _l | 0.9931 | |
| | | Calculations | ifications | 6 | | | | | Cal. Error | 0.3% | | |

Calculations and Specifications

$$Y_{i} = \frac{K \times P_{b} \times (T_{m} + 460) \times \theta}{17.64 \times V_{m} \times (P_{b} + \Delta H'_{13.6}) \times \sqrt{T_{amb} + 460}}$$
$$\Delta Y_{i} = \frac{Y_{i} - \overline{Y}_{i}}{\overline{Y}_{i}} \times 100 \qquad \text{Spec. : } \Delta Y_{i} \le \pm 2\%$$
$$Cal.Error = \frac{\overline{Y}_{i} - Y_{d}}{Y_{d}} \times 100 \qquad \text{Spec. : } Cal.Error \le \pm 5\%$$

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Meter Box Full Test Calibration

Meter Box No:

66-24

Date of Calibration: 8/19/2009

Meter Box Y_d: 0.9904

Calibration Conducted by:

_ _ _ -

OLEG LAVROV

Barometric Pressure: 29.15

Meter Box ∆H@: 1.7516

| | | | Standard Meter Gas Volume (ft ³) | | | Meter Box Gas Volume (ft ³) | | Std. Meter Temperature ('F) | | | Meter Box Temperature ('F) | | | Time (min.) | | ration ults | | |
|-------|------|-------|---|---------|--------|--|---------|--------------------------------|--------|----------|-------------------------------|-----------------|------|----------------|-------|----------------|---------|--------|
| | | | | | | V _{ds} | | | Vd | T_{is} | Tos | T _{ds} | T, | T, | Τd | | | , |
| Q | ΔH | ΔP | Y _{ds} | Initial | Final | Net | Initial | Final | Net | In | Out | Avg. | in | Out | Avg. | Θ | Yď | ∆H@ |
| 0.962 | 3.00 | -1.80 | 1.0000 | 0.000 | 10.000 | 10.000 | 580.884 | 591.020 | 10.136 | 76.5 | 76.5 | 76.50 | 86.0 | 79.0 | 82.50 | 9.96 | 0.9856 | 1.7392 |
| 0.967 | 3.00 | -1.80 | 1.0000 | 0.000 | 10.000 | 10.000 | 591.020 | 601.178 | 10.158 | 76.5 | 76.5 | 76.50 | 89.0 | 80.0 | 84.50 | 9.91 | 0.9871 | 1.7186 |
| 0.381 | 0.50 | -1.10 | 1.0000 | 0.000 | 5.000 | 5.000 | 615.932 | 621.024 | 5.092 | 77.0 | 77.0 | 77.00 | 86.0 | 84.0 | 85.00 | 12.58 | 0.9925 | 1.8361 |
| 0.381 | 0.50 | -1.10 | 1.0000 | 0.000 | 5.000 | 5.000 | 621.024 | 626.117 | 5.093 | 77.0 | 77.0 | 77.00 | 87.0 | 85.0 | 86.00 | 12.58 | 0.9942 | 1.8327 |
| 0.685 | 1.50 | -1.50 | 1.0000 | 0.000 | 10.000 | 10.000 | 629.337 | 639.566 | 10.229 | 77.0 | 77.0 | 77.00 | 92.0 | 86.0 | 89.00 | 13.98 | 0.9919 | 1.6944 |
| 0.685 | 1.50 | -1.50 | 1.0000 | 0.000 | 10.000 | 10.000 | 639.566 | 649.822 | 10.256 | 77.0 | 77.0 | 77.00 | 93.0 | 87.0 | 90.00 | 13.97 | 0.9911 | 1.6889 |
| | | | | | | | | | | | | | | - | A | 000000 | 0.00042 | 4 7640 |

Averages 0.99042 1.75163

| Nomenclature | Equations |
|---|--|
| PbBarometric Pressure (in. Hg)QFlow Rate (cfm)ΔHOrifice Pressure differential (in. H ₂ O)ΔPInlet Pressure Differential (in. H ₂ O)VdGas Meter Volume - Dry (ft ³)VdsStandard Meter Volume - Dry (ft ³)TdAverage Meter Box Temperature ("F)TdOutlet Meter Box Temperature ("F)TdsAverage Standard Meter Temperature ("F)TdsAverage Standard Meter Temperature ("F)TdsAverage Standard Meter Temperature ("F)TdsStandard Meter Correction Factor (united)ΔH@Orifice Pressure Differential giving 0.7of air at 68 "F and 29.92 in. Hg (in. H ₂ O)ΔH@ ₄ ≤ ΔH@ _{avg} ±0.2ΘDuration of Run (minutes) | $\begin{array}{c} \mathcal{Y}_{avg}\pm 0.02\\ \text{ttess})\\ \text{5 cfm} \end{array} \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad \qquad $ |

| Vacuum | Gauge |
|---------|---------|
| | • |
| (in.Hg) | (in.Hg) |
| 4.7 | 5.0 |
| 9.8 | 10.0 |
| 14.7 | 15.0 |
| 20.0 | 20.0 |
| 24.2 | 25.0 |
| | |
| | |
| | |



Meter Box - Pyrometer Calibration Sheet

| Meter Box No: | 66-24 | Office: |
|-------------------|--------------------|--------------------------------|
| Calibrated by: | OLEG LAVROV | Client: |
| Date: | 8/19/09 | Job No: |
| Temperature Scale | e Used: Fahrenheit | Type of Calibration: Full-Test |

| Calibration Reference Settings | | Pyrometer Reading for each Channel (°F) | | | | | | | | | | |
|--------------------------------------|-------|---|--------|---------|--|---|---------|--|--|--|--|--|
| (°F) | 1 | 2 | 3 | 4 | 5 | 6 | 7 | | | | | |
| | Stack | Probe | Filter | Imp Out | Aux | DGM In | DGM Out | | | | | |
| 50 | 49 | 48 | 48 | | | 1 | | | | | | |
| 100 | 99 | 98 | 98 | · · · | | | | | | | | |
| 150 | 149 | 148 | 148 | T - 1 | | | | | | | | |
| 200 | 199 | 198 | 198 | | | | | | | | | |
| 250 | 249 | 248 | 248 | | | | | | | | | |
| 300 | 299 | 298 | 299 | | | | | | | | | |
| 350 | 349 | 348 | 349 | | | | | | | | | |
| 400 | 399 | 398 | 398 | | | | | | | | | |
| 450 | 450 | 448 | 449 | | | : | | | | | | |
| 500 | 499 | 498 | 499 | | | | | | | | | |
| 550 | 549 | 548 | 549 | | | | | | | | | |
| 600 | 599 | 598 | 599 | ; | 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1 | an an an Andrewson br>An an Andrewson an An | | | | | | |

Tolerance = ±2°F difference from reference setting.

Calibration Reference Information

| Reference Used: | Omega CL23A | Serial No: | T-225950 |
|------------------------|--------------|-------------|-----------|
| Calibrated By: | JH Metrology | Exp. Date : | 6/22/2010 |
| Calibration Report No: | RO44791 | | |
| | | | |



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Meter Box Critical Orifice Post-Test Calibration Data

| Project No. | 1(|)955 | . • | leter No. | 66-24 | | Orifice | <u>B-5</u> | | Leak Checks | | |
|--------------------|-----------------------|--------------|-----------------------------|-----------|------------------|-------------------------|---------------------|------------|----------------|--|-------------|-------------|
| Location warehouse | | Meter Yd | | 0.9904 | | Orifice K' | | | Negative Press | ure | _ | |
| Test Date03/30/10 | | 30/10 | – – – Meter ∆H@ | | 1.7516 | Orifice | Cal. Date | 01/28/10 | | No movement of one-minute | ✓ Pass | |
| Operator | E. | Dieter | - Full Test Cal. Date | | 08/19/09 | | | | | Positive Pressu | Jre | _ |
| | | | • | | | | | | | No movement of manometer in on | | 🗹 Pass |
| Barom. Pres | ss. (P _b) | 29.26 | in. Hg | | | | | | | Important: All lea order for calibrat | | ass in |
| | Elapsed | | | | Amblent | | | Net Run | Not Water | Avg Motor | DGM | Percent |
| Run | | Meter Volume | Double for the state of the | eraturo | (emp Jac. (T) | Onffice AH (In W.C.) | Vacuum (In He)): | | Run Ym | Temp. for Run | Calibration | Variation - |
| | | | | | | | | | (4cf) | | | |
| | 0.0 | 253.50 | 69 | 67 | | | | | | | | |
| 1 | 5.0 | 257.08 | 70 | 67 | 71 | 1.50 | 20 | 5.0 | 3.58 | 68.3 | 0.9878 | 0.2% |
| 2 | 10.0 | 260.67 | 71 | 67 | 72 | 1.50 | 20 | 5.0 | 3.59 | 68.8 | 0.9851 | -0.1% |
| 3 | 15.0 | 264.26 | 73 | 69 | 74 | 1.50 | 20 | 5.0 | 3.59 | 70.0 | 0.9856 | -0.1% |
| | | | | | | | | | | Average Y _i | 0.9861 | |
| | | Calculations | and Spec | ification | 5 | | | | | Cal. Error | -0.4% | 1 |



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 $Y_{i} = \frac{K \times P_{b} \times (T_{m} + 460) \times \theta}{17.64 \times V_{m} \times (P_{b} + \Delta H_{13.6}) \times \sqrt{T_{omb} + 460}}$

 $\Delta Y_{i} = \frac{Y_{i} - \overline{Y}_{i}}{\overline{Y}_{i}} \times 100 \qquad \text{Spec. : } \Delta Y_{i} \le \pm 2\%$ $Cal.Error = \frac{\overline{Y}_{i} - Y_{d}}{Y_{d}} \times 100 \qquad \text{Spec. : } Cal.Error \le \pm 5\%$

Meter Box Full Test Calibration

Meter Box No:

0

85-2

Date of Calibration: 11/17/2009 **Meter Box Y**_d: 1.0066

Calibration Conducted by: OLEG LAVROV

Barometric Pressure: 29.35

١

Meter Box ∆H@: 1.7759

| | | | | | Indard Me Volume | · | | ter Box G olume (ft ³ | | Std. Meter Temperature ('F) | | | | | | | | Time (min.) | | ration ults |
|-------|------|-------|-----------------|---------|---------------------|-----------------|---------|-------------------------------------|--------|--------------------------------|------|-----------------|------|------|----------|---------|---------|----------------|--|----------------|
| | | | | | | V _{ds} | | | Vd | T _{is} | Tos | T _{ds} | T, | T. | Td | | | | | |
| Q | ΔH | ΔP | Y _{ds} | Initial | Final | Net | Initial | Final | Net | In | Out | Avg. | In | Out | Avg. | Θ | Yd | ∆H@ | | |
| 0.966 | 3.00 | -1.70 | 1.0000 | 0.000 | 10.000 | 10.000 | 200.383 | 210.311 | 9.928 | 67.5 | 67.5 | 67.50 | 77.0 | 74.0 | 75.50 | 10.16 | 1.0106 | 1.7539 | | |
| 0.959 | 3.00 | -1.70 | 1.0000 | 0.000 | 10.000 | 10.000 | 210.311 | 220.285 | 9.974 | 67.5 | 67.5 | 67.50 | 80.0 | 75.0 | 77.50 | 10.23 | 1.0097 | 1.7748 | | |
| 0.388 | 0.50 | -1.10 | 1.0000 | 0.000 | 5.000 | 5.000 | 222.808 | 227.844 | 5.036 | 68.0 | 68.0 | 68.00 | 75.0 | 75.0 | 75.00 | 12.65 | 1.0020 | 1.8126 | | |
| 0.388 | 0.50 | -1.10 | 1.0000 | 0.000 | 5.000 | 5.000 | 227.844 | 232.882 | 5.038 | 68.0 | 68.0 | 68.00 | 75.0 | 75.0 | 75.00 | 12.65 | 1.0016 | 1.8126 | | |
| 0.683 | 1.50 | -1.50 | 1.0000 | 0.000 | 10.000 | 10.000 | 237.848 | 247.883 | 10.035 | 68.0 | 68.0 | 68.00 | 81.0 | 75.0 | 78.00 | 14.36 | 1.0078 | 1.7518 | | |
| 0.683 | 1.50 | -1.50 | 1.0000 | 0.000 | 10.000 | 10.000 | 247.883 | 257.913 | 10.030 | 68.0 | 68.0 | 68.00 | 81.0 | 75.0 | 78.00 | 14.35 | 1.0083 | 1.7494 | | |
| | | | | | | | · | | | • | | - | | • | <u>م</u> | veranes | 1 00665 | 1 775 | | |

Averages 1.00665 1.77586

| Equations |
|--|
| $(Y_{ds}) \left[\frac{V_{ds}}{V_d} \right] \left[\frac{T_d + 460}{T_{ds} + 460} \right] \left[\frac{P_b + \Delta P / 13.6}{P_b + \Delta H / 13.6} \right]$ $P = \frac{(0.0319)(\Delta H)}{P_b(T_o + 460)} \left[\frac{(T_{ds} + 460)\Theta}{(V_{ds})(Y_{ds})} \right]^2$ $\frac{(7.64(V_{ds})(P_b)}{(T_{ds} + 460)(\Theta)}$ |
| |

| Vacuum | Gauge |
|----------|---------|
| Standard | Gauge |
| (in.Hg) | (in.Hg) |
| 4.9 | 5.0 |
| 10.1 | 10.0 |
| 15.3 | 15.0 |
| 20.5 | 20.0 |
| 25.3 | 25.0 |
| | |
| | |
| | |



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Meter Box - Pyrometer Calibration Sheet

Meter Box No: _____85-2 _____

Calibrated by: OLEG LAVROV

Office: _____

Client:

Job No:

Date: <u>11/17/09</u>

Temperature Scale Used: Fahrenheit

| Туре | of Calibration: | Full-Test |
|------|-----------------|-----------|
| | | |

| Calibration Reference Settings | | Pyrometer Reading for each Channel (°F) | | | | | | | | | |
|--------------------------------------|-------|---|--------|---|----------------|---|--|--|--|--|--|
| (°F) | 1 | 2 | 3 | 4 | 5 | 6 | 7 | | | | |
| | Stack | Probe | Filter | Imp Out | Aux | DGM In | DGM Out | | | | |
| 50 | 49 | 52 | 51 | | | | | | | | |
| 100 | 98 | 101 | 101 | | | | | | | | |
| 150 | 149 | 151 | 151 | | | | | | | | |
| 200 | 200 | 201 | 201 | Stand and | and the second | 1 6 83 Au in | e Antonio a se | | | | |
| 250 | 251 | 252 | 251 | | | | | | | | |
| 300 | 301 | 301 | 301 | and a state of the second second second second second second second second second second second second second s | | i . National and states of the | Stand in the state | | | | |
| 350 | 350 | 348 | 351 | | | ana an ing sa sa sa sa sa sa sa sa sa sa sa sa sa | | | | | |
| 400 | 400 | 401 | 400 | | | | | | | | |
| 450 | 450 | 451 | 450 | 1998 - 10 yes | | | | | | | |
| 500 | 500 | 502 | 500 | | | | ang sa sa sa sa sa sa sa sa sa sa sa sa sa | | | | |
| 550 | 550 | 551 | 550 | | Salar C.A. | с. 21 - 24 - 24 - 24 - 24 - 24 - 24 - 24 - | and a second second | | | | |
| 600 | 600 | 602 | 600 | | **** | an an an an an an an an an an an an an a | <u>.</u> | | | | |

Tolerance = ±2°F difference from reference setting.

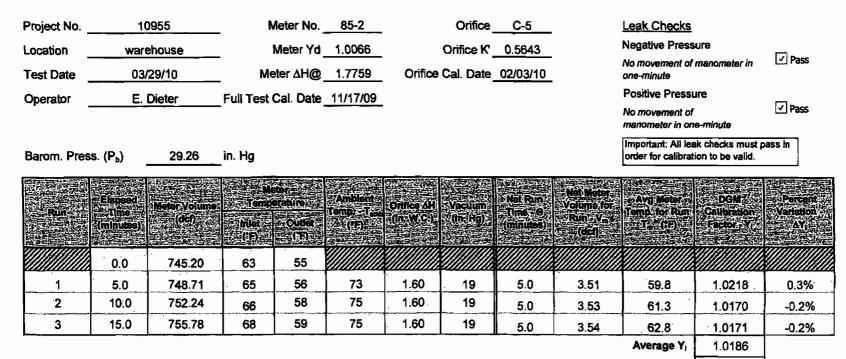
| Calibration | Reference | Information |
|-------------|-----------|-------------|
| | | |

| Reference Used: | Omega CL23A | Serial No: | T-225950 |
|------------------------|--------------|------------|-----------|
| Calibrated By: | JH Metrology | Exp. Date: | 10/7/2010 |
| Calibration Report No: | R044791 | | |
| | | | |



C03935C-Meter Full, April 2004a Copyright © 2004 Clean Air Engineering Inc.

Meter Box Critical Orifice Post-Test Calibration Data



Calculations and Specifications

$$Y_{i} = \frac{K \times P_{b} \times (T_{m} + 460) \times \theta}{17.64 \times V_{m} \times (P_{b} + \Delta H_{13.6}) \times \sqrt{T_{amb} + 460}}$$
$$\Delta Y_{i} = \frac{Y_{i} - \overline{Y}_{i}}{\overline{Y}_{i}} \times 100 \qquad \text{Spec.} : \Delta Y_{i} \le \pm 2\%$$
$$Cal.Error = \frac{\overline{Y}_{i} - Y_{d}}{Y_{d}} \times 100 \qquad \text{Spec.} : Cal.Error \le \pm 5\%$$

CD80058-Motor Post-CO, February 2004 Copyright © 2004 Clean Air Engineering, Inc.

Cal. Error

1.2%

1

Meter Box Full Test Calibration

Meter Box No: 85-4

Date of Calibration: 11/25/2009

Meter Box Y_d: 1.0085

1.7723

29.09

Calibration Conducted by: **OLEG LAVROV**

Barometric Pressure:

Meter Box ∆H@:

| _ | | | | | indard Me s Volume (| | Meter Box Gas Volume (ft ³) | | Std. Meter Temperature ('F) | | Meter Box Temperature ('F) | | | Time (min.) | Calibration Results | | | |
|-------|------|-------|-----------------|---------|-------------------------|-----------------|--|---------|--------------------------------|-----------------|-------------------------------|-----------------|------|----------------|------------------------|---------|---------|---------|
| | | | Т | | | V _{ds} | | | Vd | T _{is} | T _{os} | T _{ds} | Ti | Т。 | Td | | | |
| Q | ΔH | ΔΡ | Y _{ds} | Initial | Final | Net | Initial | Final | Net | In | Out | Avg. | In | Out | Avg. | Θ | Yd | ∆н@ |
| 0.965 | 3.00 | -1.70 | 1.0000 | 0.000 | 11.000 | 11.000 | 278.946 | 289.808 | 10.862 | 67.5 | 67.5 | 67.50 | 76.0 | 69.0 | 72.50 | 11.09 | 1.0103 | 1.7589 |
| 0.954 | 3.00 | -1.70 | 1.0000 | 0.000 | 10.000 | 10.000 | 289.808 | 299.707 | 9.899 | 67.5 | 67.5 | 67.50 | 79.0 | 71.0 | 75.00 | 10.20 | 1.0125 | 1.7936 |
| 0.385 | 0.50 | -1.10 | 1.0000 | 0.000 | 5.000 | 5.000 | 304.068 | 309.063 | 4.995 | 67.5 | 67.5 | 67.50 | 76.0 | 72.0 | 74.00 | 12.62 | 1.0092 | 1.8270 |
| 0.385 | 0.50 | -1.10 | 1.0000 | 0.000 | 5.000 | 5.000 | 309.063 | 314.066 | 5.003 | 67.5 | 67.5 | 67.50 | 76.0 | 73.0 | 74.50 | 12.65 | 1.0086 | 1.8322 |
| 0.687 | 1.50 | -1.30 | 1.0000 | 0.000 | 10.000 | 10.000 | 345.224 | 355.314 | 10.090 | 67.5 | 67.5 | 67.50 | 81.0 | 76.0 | 78.50 | 14.15 | 1.0046 | 1.7097 |
| 0.687 | 1.50 | -1.30 | 1.0000 | 0.000 | 10.000 | 10.000 | 355.314 | 365.392 | 10.078 | 67.5 | 67.5 | 67.50 | 81.0 | 76.0 | 78.50 | 14.16 | 1.0058 | 1.7122 |
| | | | | - | | | | | | | | | | | A | verages | 1.00850 | 1.77225 |

| | Nomenclature | Equations |
|--|--|--|
| P₅ Q ΔH V₀ T₀ T₀ T₀s Y₀ AH@ ∂ | Barometric Pressure (in. Hg) Flow Rate (cfm) Orifice Pressure differential (in. H ₂ O) Inlet Pressure Differential (in. H ₂ O) Gas Meter Volume - Dry (ft ³) Standard Meter Volume - Dry (ft ³) Average Meter Box Temperature ('F) Outlet Meter Box Temperature ('F) Average Standard Meter Temperature ('F) Meter Correction Factor (unitless), Y ₁ \leq Y _{avg} ±0.02 Standard Meter Correction Factor (unitless) Orifice Pressure Differential giving 0.75 cfm of air at 68'F and 29.92 in. Hg (in. H ₂ O) Δ H@ ₁ \leq Δ H@ _{avg} ±0.2 Duration of Run (minutes) | $Y_{d} = (Y_{ds}) \left[\frac{Y_{ds}}{V_{d}} \right] \left[\frac{T_{d} + 460}{T_{ds} + 460} \right] \left[\frac{P_{h} + \Delta P / 13.6}{P_{h} + \Delta H / 13.6} \right]$ $\Delta H @= \frac{(0.0319)(\Delta H)}{P_{h}(T_{o} + 460)} \left[\frac{(T_{ds} + 460)\Theta}{(V_{ds})(Y_{ds})} \right]^{2}$ $Q = \frac{17.64(V_{ds})(P_{h})}{(T_{ds} + 460)(\Theta)}$ |

| Vacuum | Vacuum Gauge | | | | | | | |
|----------|--------------|--|--|--|--|--|--|--|
| Standard | Gauge | | | | | | | |
| (in.Hg) | (in.Hg) | | | | | | | |
| 5.1 | 5.0 | | | | | | | |
| 9.9 | 10.0 | | | | | | | |
| 15.1 | 15.0 | | | | | | | |
| 19.5 | 20.0 | | | | | | | |
| 24.8 | 25.0 | | | | | | | |
| | | | | | | | | |
| | | | | | | | | |
| | | | | | | | | |



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Meter Box - Pyrometer Calibration Sheet

Meter Box No:

Calibrated by: OLEG LAVROV

Date: 11/25/09

Office:

Job No:

Client:

Temperature Scale Used: Fahrenheit

85-4

Type of Calibration: Full-Test

| Calibration Reference Settings | Pyrometer Reading for each Channel (°F) | | | | | | | | | |
|--------------------------------------|---|-------|--------|----------|-----|--------|--------------|--|--|--|
| (°F) | 1 | 2 | 3 | 4 | 5 | 6 | 7 | | | |
| | Stack | Probe | Filter | Imp Out | Aux | DGM In | DGM Out | | | |
| 50 | 49 | 52 | 52 | | | | | | | |
| 100 | 99 | 102 | 102 | | | | | | | |
| 150 | 150 | 152 | 152 | | | | | | | |
| 200 | 200 | 202 | 202 | | | 171% | | | | |
| 250 | 250 | 252 | 251 | | | 的机理 | 6 | | | |
| 300 | 300 | 302 | -301 | | | | | | | |
| 350 | 350 | 352 | 351 | | | | 如果。自 | | | |
| 400 | 400 | 401 | 401 | E Carlos | | | 111050 | | | |
| 450 | 450 | 452 | 452 | | | | | | | |
| 500 | 500 | 501 | 501 | C SCHOLE | | | 14.54 A. | | | |
| 550 | 550 | 551 | 551 | 1 | | | A CONTRACTOR | | | |
| 600 | 600 | 601 | 601 | | | | | | | |

Tolerance = ±2°F difference from reference setting.

Calibration Reference Information

| Reference Used: | Omega CL23A | Serial No: | T-225950 |
|------------------------|--------------|------------|-----------|
| Calibrated By: | JH Metrology | Exp date : | 10/7/2010 |
| Calibration Report No: | R044701 | | |
| | | | |



CDS005C-Meter Full, April 2004a Copyright (D 2004 Clean Air Engineering Inc

Meter Box Critical Orifice Post-Test Calibration Data

| Project No. | 1(|)955 | N | leter No. | 85-4 | | Orifice | C-5 | | Leak Checks | | |
|-------------|-----------|---------------|----------------|----------------|------------------|------------|-----------|------------------------|----------------------------------|--|-------------------------|-----------|
| Location | ware | ehouse | _ 1 | Meter Yd | 1.0085 | | Orifice K | 0.5643 | | Negative Press | ure | |
| Test Date | 03/ | 30/10 | Me | ter ∆H@ | 1.7723 | Orifice | Cal. Date | 02/03/10 | | No movement of one-minute | manometer in | Pass |
| Operator | E. | Dieter | Full Test | Cal. Date | 11/25/09 | | | | | Positive Pressu | ıre | |
| | | | - | | | | | | | No movement of manometer in on | | 🗸 Pass |
| Barom. Pres | s. (P₀) | 29.26 | in. Hg | | | | | | | Important: All les order for calibrat | | bass in |
| | Elapsed | Mirtar Volume | | nor Prature | Ambient | Orifice AH | | Net Rum | Net Menor v | Avy Meter x | DGM | Percent |
| Run | (minutes) | | inhet e (1) | Outlet | Temp Tun (FF) | (in W.a)) | | Time (O) (minutes): | Volume for Run Va 24 (def) | | Calibration Factor Y | Veriation |
| | 0.0 | 77.40 | 70 | 67 | | | | | | | | |
| 1 | 5.0 | 81.03 | 71 | 67 | 72 | 1.60 | 21 | 5.0 | 3.63 | 68.8 | 1.0061 | 0.0% |
| 2 | 10.0 | 84.67 | 72 | 68 | 72 | 1.60 | 21 | 5.0 | 3.64 | 69.5 | 1.0047 | -0.2% |
| 3 | 15.0 | 88.30 | 73 | 68 | 73 | 1.60 | .21 | 5.0 | 3.63 | 70.3 | 1.0080 | 0.2% |
| | | | | | | | | | | Average Y _i | 1.0063 | |
| | | Calculations | s and Spec | cification | 5 | | | | | Cal. Error | -0.2% | |



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 $Y_{i} = \frac{K \times P_{b} \times (T_{m} + 460) \times \theta}{17.64 \times V_{m} \times (P_{b} + \Delta H_{13.6}) \times \sqrt{T_{omb} + 460}}$

 $\Delta Y_i = \frac{Y_i - \overline{Y}_i}{\overline{Y}_i} \times 100 \qquad \text{Spec.}: \Delta Y_i \le \pm 2\%$

 $Cal.Error = \frac{\overline{Y}_{i} - Y_{d}}{Y_{d}} \times 100 \qquad \text{Spec.: } Cal.Error \leq \pm 5\%$

| Sample F | Probe | Calibration |
|----------|-------|-------------|
|----------|-------|-------------|

| Probe Type: | M5 with | S-Type Pitot | - | I.D. Number; | 67 | 7-4-4 | | | | |
|-------------------------------------|---|---|---------------------------|---|---------------------------------------|-----------------------|--|--|--|--|
| | | | | Project Number: | | | | | | |
| | | States and the | rmocouple/Callbr | alion | | | | | | |
| Reference Type | : Thermocouple | Reference I.D. No: | 15-078-39 | Pyrometer I.D. No: | 80512890 | Units: *F | | | | |
| Point No. | Target Temp. | Reference Temp. | Indicated Temp. | Temp. Difference | % Difference* | Specification | | | | |
| 1 | Ambient | 75 | 75 | 0 | 0.00% | | | | | |
| 2 | 200°F-250°F | 233 | 235 | -2 | 0.29% | %Difference ≤ 1.5 | | | | |
| | Based on Absolute Temperature (Rankine) Does thermocouple assembly meet specifications? YES | | | | | | | | | |
| | | Pitot Tube Calibrat | ion (Wind Tunnel) | Method @ 50 ft/sec | 建立498 5000 | | | | | |
| Referen | ce Pitot I.D. No: | Wind Tunnel | | Reference Pitot Cp: | 0.99 | | | | | |
| Pitot Side 'A' : | | | | Abs. Deviation | Speci | fication | | | | |
| Trial No. | Reference ∆P | Probe ∆P | Probe C _{p(S)} * | from Avg. C _{p(A)} ** | Avg. C, Dev | lations ≤ 0.01 | | | | |
| 1 | 0.539 | 0.771 | 0.828 | 0.000 | | | | | | |
| 2 | 0.542 | 0.774 | 0.828 | 0.001 | | | | | | |
| 3 | 0.540 | 0.775 | 0.826 | 0.001 | | | | | | |
| | Side 'A' A | verage Probe C _{p(A)} = | 0.8273 | 0.0008 | | | | | | |
| | | | | | | | | | | |
| Pitot Side 'B' : | | | | Abs. Deviation | Specif | fication | | | | |
| Trial No. | Reference ∆P | Probe ∆P | Probe C _{p(8)} * | from Avg. C _{p(B)} ** | Avg. C _p Dev | iations ≤ 0.01 | | | | |
| 1 | 0.545 | 0.778 | 0.829 | 0.001 | | | | | | |
| 2 | 0.540 | 0.782 | 0.822 | 0.005 | | | | | | |
| 3 | 0.546 | 0.773 | 0.832 | 0.004 | | | | | | |
| | Side 'B' A | verage Probe C _{p(B)} = | 0.8278 | 0.0035 | | | | | | |
| 'A' Average C _p 0.827 | [| 'B' Average C _p 0.828 | = [| Difference -0.001 | - | fication ce∣≤ 0.01 | | | | |
| Does assen specifica | | YES | • | lf "Yes", C _p = Ave values. If "No" | erage of Side 'A ', Pitot must be | • | | | | |
| • <i>C</i> _{P(S)} | $=C_{P(STD)}\sqrt{\frac{1}{2}}$ | $\frac{\Delta p_{(STD)}}{\Delta p_{(S)}}$ | " Dev | $iation = C_{P(S)} $ | $-\overline{C_P}_{(A \text{ or } B)}$ | | | | | |
| | | All/specifications an | from EPA-600/9 | 76-005 section 3 11 | | | | | | |
| Probe Cp= | 0.828 | Calibrated by: | B. ARNOLD | | Date: _ | 06/29/2009 | | | | |



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Sample Probe Calibration

| Probe Type | | S-Type Pitot | | I.D. Number: Project Number: | 67 | 7-4-5 |
|---|---|--|--|--|---|--|
| | | The | mocouple Calib | - | | |
| eference Type | e: Thermocouple | Reference I.D. No: | 15-078-39 | Pyrometer I.D. No: | 80512890 | Units: °F |
| Point No. | Target Temp. | Reference Temp. | Indicated Temp | Temp. Difference | % Difference* | Specificatio |
| <u> </u> | Ambient | 69 | 67 | 2 | 0.38% | |
| 2 | 200°F-250°F | 241 | 237 | 4 | 0.57% | %Difference : |
| oes thermoco | | meet specifications | | YES | | |
| STREET? | 计算机 | Pitot Tube Calibrat | on (Wind Tunnel | Method @ 49 ft/sec | 口 \$1629.36.51 | |
| Referen | nce Pitot I.D. No: | Wind Tunnel | | Reference Pitot Cp: | 0.99 | |
| Pitot Side 'A' : | | | | Abs. Deviation | Spec | ification |
| Trial No. | Reference ∆P | Probe ∆P | Probe C _{p(S)} * | from Avg. C _{p(A)} ** | Avg. C _p Dev | /iations ≤ 0.0 [.] |
| 1 | 0.551 | 0.773 | 0.836 | 0.001 | | |
| 2 | 0.549 | 0.778 | 0.832 | 0.003 | | |
| _ | | o 777 | 0.837 | 0.002 | | |
| 3 | 0.555 | 0.777 | 0.007 | 0.002 | | |
| | | 0.777 vørage Probe C _{p(A)} ≕ | 0.8348 | 0.002 | | |
| | | | | | | |
| 3 | Side 'A' A | | | | Speci | fication |
| | Side 'A' A | | | 0.0021 | • | |
| 3 itot Side 'B' : | Side 'A' A | vørage Probe C _{p(A)} ≕ | 0.8348 | 0.0021 Abs. Deviation | • | |
| 3 itot Side 'B' : Trial No. | Side 'A' A Reference ∆P | verage Probe C _{P(A)} ≕ Probe ∆P | 0.8348 Probe C _{p(s)} * | 0.0021 Abs. Deviation from Avg. C _{p(B)} ** | • | |
| 3 itot Side 'B' : Trial No. 1 | Sidə 'A' A Reference ∆P 0.566 0.557 0.568 | verage Probe C _{p(A)} = Probe ΔP 0.772 0.777 0.775 | 0.8348 Probe C _{p(S)} * 0.847 | 0.0021 Abs. Deviation from Avg. C _{p(B)} ** 0.003 | • | |
| 3 litot Side 'B' : Trial No. 1 2 | Sidə 'A' A Reference ∆P 0.566 0.557 0.568 | verage Probe C _{p(A)} = Probe ΔP 0.772 0.777 | 0.8348 Probe C _{p(5)} * 0.847 0.838 | 0.0021 Abs. Deviation from Avg. C _{p(B)} ** 0.003 0.006 | • | |
| 3 itot Side 'B' : Trial No. 1 2 3 | Sidə 'A' A Reference ∆P 0.566 0.557 0.568 | verage Probe C _{p(A)} = Probe Δ P 0.772 0.777 0.775 verage Probe C _{p(B)} = | 0.8348 Probe C _{P(S)} * 0.847 0.838 0.847 | 0.0021 Abs. Deviation from Avg. C _{p(B)} ** 0.003 0.006 0.003 0.0039 | Avg. C _p De∖ | viations ≤ 0.01 |
| 3 Itot Side 'B' : Trial No. 1 2 3 3 | Sidə 'A' A Reference ∆P 0.566 0.557 0.568 | verage Probe C _{p(A)} = <u>Probe ΔP</u> 0.772 0.777 0.775 verage Probe C _{p(B)} = 'B' Average C _p | 0.8348 Probe C _{P(S)} * 0.847 0.838 0.847 | 0.0021 Abs. Deviation from Avg. C _{p(B)} ** 0.003 0.006 0.003 0.003 0.0039 Difference | Avg. C _p De∖ Speci | riations ≤ 0.01 fication |
| 3 itot Side 'B' : Trial No. 1 2 3 | Sidə 'A' A Reference ∆P 0.566 0.557 0.568 | verage Probe C _{p(A)} = Probe Δ P 0.772 0.777 0.775 verage Probe C _{p(B)} = | 0.8348 Probe C _{P(S)} * 0.847 0.838 0.847 | 0.0021 Abs. Deviation from Avg. C _{p(B)} ** 0.003 0.006 0.003 0.0039 | Avg. C _p De∖ Speci | viations ≤ 0.01 |
| 3 Itot Side 'B' : Trial No. 1 2 3 3 | Side 'A' A Reference ∆P 0.566 0.557 0.568 Side 'B' Av | verage Probe C _{p(A)} = <u>Probe ΔP</u> 0.772 0.777 0.775 verage Probe C _{p(B)} = 'B' Average C _p | 0.8348 Probe C _{P(S)} * 0.847 0.838 0.847 | 0.0021 Abs. Deviation from Avg. C _{p(B)} ** 0.003 0.006 0.003 0.003 0.0039 Difference | Avg. C _p Dev Speci Differen | riations ≤ 0.01 fication ce ≤ 0.01 A' and 'B' Cp |
| 3 itot Side 'B' : Trial No. 1 2 3 X' Average C _p 0.835 Does asset specific: | Side 'A' A Reference △P 0.566 0.557 0.568 Side 'B' Av | verage Probe $C_{p(A)}$ = Probe ΔP 0.772 0.777 0.775 verage Probe $C_{p(B)}$ = 'B' Average C_p 0.844 | 0.8348 Probe C _{P(S)} * 0.847 0.838 0.847 0.8442 | 0.0021 Abs. Deviation from Avg. C _{p(B)} ** 0.003 0.006 0.003 0.0039 Difference -0.009 If "Yes", C _p = Ave | Avg. C _p Dev Speci (Differen erage of Side '. ', Pitot must bo | riations ≤ 0.01 fication ce ≤ 0.01 A' and 'B' Cp |
| 3 itot Side 'B' : Trial No. 1 2 3 X' Average C _p 0.835 Does asset specific: | Side 'A' A Reference ΔP 0.566 0.557 0.568 Side 'B' Au mbly meet ations? $C_{P(STD)} \sqrt{\frac{1}{2}}$ | verage Probe $C_{p(A)}$ = Probe ΔP 0.772 0.777 0.775 verage Probe $C_{p(B)}$ = 'B' Average C_p 0.844 YES $\Delta p_{(STD)}$ $\Delta p_{(S)}$ | 0.8348 | 0.0021 Abs. Deviation from Avg. C _{p(B)} ** 0.003 0.006 0.003 0.0039 Difference -0.009 If "Yes", C _p = Ave values. If "No" | Avg. C_p Dev Speci Different erage of Side ', ', Pitot must be $-\overline{C_P}(A \text{ or } B)$ | riations ≤ 0.01 fication ce¦ ≤ 0.01 A' and 'B' Cp |



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Sample Probe Calibration

| Probe Type: | M5 with | S-Type Pitot | - | I.D. Number: | | 7-8-4 | | | | |
|----------------------------|--|---|---------------------------|---|---|-------------------|--|--|--|--|
| | | | | Project Number: | | | | | | |
| | l Hazer | The | rmocouple Calibr | ation is also in the | | | | | | |
| Reference Type: | Thermocouple | Reference I.D. No: | 15-078-39 | _ Pyrometer I.D. No: | 80512890 | Units: °F | | | | |
| Point No. | Target Temp. | Reference Temp. | Indicated Temp. | Temp. Difference | % Difference* | Specification | | | | |
| 1 | Ambient | 75 | 70 | 5 | 0.93% | | | | | |
| 2 | 200°F-250°F | 246 | 240 | 6 | 0.85% | %Difference ≤ 1.5 | | | | |
| | * Based on Absolute Temperature (Rankine) Does thermocouple assembly meet specifications? YES | | | | | | | | | |
| | | Pitot Tube Calibrat | ion (Wind Tunnel | Method @ 49 ft/sec | | | | | | |
| Referen | ce Pitot I.D. No: | Wind Tunnel | | Reference Pitot Cp: | 0.99 | | | | | |
| Pitot Side 'A' : | | | | Abs. Deviation | • | fication | | | | |
| Trial No. | Reference ∆P | Probe ∆P | Probe C _{p(8)} * | from Avg. C _{p[A]} ** | Avg. C _p Dev | viations ≤ 0.01 | | | | |
| 1 | 0.538 | 0.814 | 0.805 | 0.000 | | | | | | |
| 2 | 0.540 | 0.815 | 0.806 | 0.001 | | | | | | |
| 3 | 0.539 | 0.816 | 0.805 | 0.001 | | | | | | |
| | Side 'A' A | verage Probe C _{p(A)} = | 0.8052 | 0.0008 | | | | | | |
| Pitot Side 'B' : | | | | Abs. Deviation | Speci | fication | | | | |
| Trial No. | Reference ∆P | Probe AP | Probe C _{p(S]} * | from Avg. C _{p(B)} ** | • | riations ≤ 0.01 | | | | |
| 1 | 0.542 | 0.818 | 0.806 | 0.002 | - • | | | | | |
| 2 | 0.536 | 0.814 | 0.803 | 0.001 | | | | | | |
| 3 | 0.538 | 0.818 | 0.803 | 0.001 | | | | | | |
| | Side 'B' A | verage Probe C _{p(B)} = | 0.8039 | 0.0012 | | | | | | |
| | | | | · · · · · · · · · · · · · · · · · · · | | | | | | |
| | | | | | | | | | | |
| 'A' Average C _p | _ | 'B' Average C _P | | Difference | Speci | fication | | | | |
| 0.805 | — | 0.804 | = | 0.001 |)Differen | ce¦ ≤ 0.01 | | | | |
| Does assen specifica | • | YES | | lf "Yes", C _p ≓ Ave values. if "No' | erage of Side '/ ', Pitot must be | | | | | |
| • <i>C</i> _{P(S)} | $= C_{P(STD)} \sqrt{\frac{1}{2}}$ | $\frac{\Delta p_{(STD)}}{\Delta p_{(S)}}$ | " Dev | viation = $ C_{P(S)} $ | $-\overline{C_{P}}_{(A \text{ or } B)}$ | | | | | |
| | | All specifications an | n from EPA 600/9 | 7.6-005; section 3.1%; | | | | | | |
| Probe Cp= | | Calibrated by: | | | Date: | 09/21/2009 | | | | |



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1.1

| | | Sample | Probe Ca | libration | 67 | . g.1 |
|----------------------------|---------------------------------------|----------------------------------|---------------------------|--|---------------------------|-----------------|
| Probe Type | : M5 with | S-Type Pitot | | I.D. Number: | | 96-1 |
| | | | - | Project Number: | | |
| | | | rmocouple/Gullbr | ation | | 19-1.X |
| <u>新行到</u> 建20世纪过度表示的 | and here and the second | | | | | |
| Reference Typ | e: Thermocouple | Reference I.D. No: | 15-078-39 | Pyrometer I.D. No: | 80512890 | Units |
| Point No. | Target Temp. | Reference Temp. | Indicated Temp. | Temp. Difference | % Difference* | Specific |
| 1 | Ambient | 75 | 72 | 3 | 0.56% | |
| 2 | 200°F-250°F | 247 | 254 | -7 | 0.99% | %Differen |
| | | | olute Temperature | | | |
| Does thermoc | ouple assembly | meet specifications | 7 | > YES | | |
| | | Disetti | | | | |
| | | Pitotalupe Calibrati | | Méthod @ 60 ft/sec | ことなどなるようもお言語 | 王王王 王子王王 |
| | | | | | | |
| Refere | nce Pitot I.D. No: | Wind Tunnel | | Reference Pitot Cp: | 0.99 | |
| | | | | | | . |
| Pitot Side 'A' | · · · · · · · · · · · · · · · · · · · | Deebe 4D | Dentro O. A | Abs. Deviation | | fication |
| Trial No. | Reference AP | Probe <u>AP</u> | Probe C _{p(S)} * | from Avg. C _{p(A)} ** | Avg. C _p Dev | |
| 1 | 0.547 | 0.808 | 0.815 | 0.001 | | |
| 2 | 0.548 | 0.813 | 0.813 | 0.001 | | |
| 3 | 0.548 | 0.811 | 0.814 | 0.000 | | |
| | Side 'A' A | verage Probe C _{p(A)} = | 0.8139 | 0.0008 | | |
| | | | r | Ale Declet | - | |
| Pitot Side 'B' : | | | Duch a | Abs. Deviation | • | fication |
| Trial No. | | Probe ∆P | Probe C _{p(S)} * | from Avg. C _{p(B)} ** | Avg. C _p Dev | lations 5 0 |
| 1 | 0.544 | 0.810 | 0.812 | 0.002 | | |
| 2 | 0.543 | 0.810 | 0.811 | 0.000 | | |
| 3 | 0.541 | 0.812 | 0.808 | 0.002 | | |
| | Side 'B' A | /erage Probe Ċ _{p(B)} ≓ | 0.8102 | 0.0014 | | |
| | | | | | | |
| | | | | D100 | 0 | |
| 'A' Average C _p | л — г | 'B' Average Cp | r | Difference | | ication |
| 0.814 | 3 L | 0.810 | — L | 0.004 | Dimeterio | ce) ≤ 0.01 |
| Deep appa | mbly most | | | | | and 'B' |
| Does asse specific | | YES - | | lf "Yes", C _p = Ave values if "No" | ', Pitot must be | |
| •••••• | | | | values. Il No | , Phot most so | Teplaceu. |
| • | | $\Delta p_{(STD)}$ | | 1 | | |
| CP(S | $= C_{P(STD)} \sqrt{\frac{1}{2}}$ | An | "Dev | $iation = C_{P(S)}$ | $-C_{P(A \text{ or } B)}$ | |
| | V | $\Delta P(s)$ | | 1 . (3) | (| |
| | CARL DEPENDENTS | | | 6-005 section 3.1 | | THE OWNER |
| a shirt was | COLUMN STATES AND THE CASE | | | | | |



Sample Probe Calibration

| Probe Type: | M5 with | S-Type Pitot | | I.D. Number: | 67 | -8-17 |
|-------------------------------------|--|---|---------------------------|--|---------------------------------------|---|
| | the second second second second second second second second second second second second second second second s | | | Project Number: | | |
| | | The | rmocouple Calibr | atton Laster as the | | |
| Reference Type | Thermocouple | Reference I.D. No: | 15-078-39 | Pyrometer I.D. No: | 80512890 | Units: °F |
| Point No. | Target Temp. | Reference Temp. | Indicated Temp. | Temp. Difference | % Difference* | Specification |
| 1 | Ambient | 69 | 71 | -2 | 0.38% | |
| 2 | 200°F-250°F | 240 | 235 | 5 | 0.71% | %Difference ≤ 1.5 |
| Does thermoco | | meet specifications | | YES | | ur Malifa Malanda Manakawa Ang Kanakawa Ang |
| | | Ritot Tube Calibrat | ion (Wind Tunnel | Method @:50 ft/sec | | |
| Referen | ce Pitot I.D. No: | Wind Tunnel | | Reference Pitot Cp: | 0.99 | |
| Pitot Side 'A' : | | | | Abs. Deviation | Speci | fication |
| Trial No. | Reference ∆P | Probe ∆P | Probe C _{p(S)} * | from Avg. C _{p(A)} ** | Avg. C _p Dev | iations ≤ 0.01 |
| 1 | 0.566 | 0.790 | 0.838 | 0.001 | | |
| 2 | 0.564 | 0.797 | 0.833 | 0.004 | | |
| 3 | 0.568 | 0.790 | 0.840 | 0.003 | | |
| | Side 'A' A | verage Probe C _{p(A)} = | 0.8368 | 0.0028 | | |
| | | | | | | |
| Pitot Side 'B' : | | | | Abs. Deviation | Specif | ilcation |
| Trial No. | Reference ∆P | Probe ∆P | Probe C _{p(S)} * | from Avg. C _{p(B)} ** | Avg. C _p Dev | iations ≤ 0.01 |
| 1 | 0.548 | 0.769 | 0.836 | 0.005 | | |
| 2 | 0.543 | 0.774 | 0.829 | 0.002 | | |
| 3 | 0.548 | 0.782 | 0.829 | 0.003 | | |
| | Side 'B' A | verage Probe C _{p(B)} = | 0.8315 | 0.0032 | | |
| 'A' Average C _p 0.837 | ! — [| 'B' Average C _p 0.831 | = | Difference 0.006 | - | ication ce∣ ≤ 0.01 |
| Does asser specifica | • | YES | → | lf "Yes", C _p ≃ Av values. If "No' | erage of Side 'A ', Pitot must be | |
| • <i>C</i> _{P(S)} | $=C_{P(STD)}\sqrt{1}$ | $\frac{\Delta p_{(STD)}}{\Delta p_{(S)}}$ | " Dev | viation = $ C_{P(S)} $ | $-\overline{C_P}_{(A \text{ or } B)}$ | |
| | | All specifications an | o from ERA-600/9 | 76-005 section 3.1 | | |
| Probe Cp= | | Calibrated by: | | | Date: _ | 03/04/2010 |



CDS002C-Pitol_TNL, Dec 2008 Copyright © 2008 Clean Air Engineering Inc.

| AIR LIQUID | E Air Liquide America | S) scott- | Zerc |
|------------------|---|--------------------------------|--|
| Shipped From: | 1290 COMBERME TROY Phone: 248-58 C E R T I F I | MI 4 | 8083 Fax: 248-589-2134 F ANALYSIS |
| SCOTT BROW | ENGINEERING IN IOOD STREET | | PROJECT #: 05-76361-001 PO#: 24559-66-65000 ITEM #: 0501813 AL |
| PALATINE | | IL 60067 | DATE: 29May2009 |
| | 8 #: AAL14589 SSURE: 02000 1 | PSIG | |
| PURE MATER | IAL: NITROGEN | | CA5# 7727-37-9 |
| GRADE : | ZERO GAS | 5 | |
| PURITY: 99 | .9988 | | |
| | IMPURITY THC | Maximum Concentrat 0.5 P | <u>tons</u> PM |
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| NALYST: | adrie | | |

| | | RATA | CLASS | | | | | |
|--|--|-------------------------------------|---|--|--|--|--|--|
| AIR LIQUIDE Air Liquide Ameri Specialty Gases L | CC Stratt | Dual-Anal | zed Calibration Standard | | | | | |
| 1290 COMBERMERE STREET, | TROY, MI 48083 | Phor | Phone: 248-589-2950 Fax: 248-589-213 | | | | | |
| CERTIFICATE OF ACCUR | ACY: FPA Protoco | Gas | | | | | | |
| Assay Laboratory | | Custo | mer | | | | | |
| - | P.O. No.: 57534-7 | | N AIR ENGINEERING | | | | | |
| AIR LIQUIDE AMERICA SPECIALTY GA 1290 COMBERMERE STREET | SES LLC Project No.: 05-78 | | Allen W. Wood Street | | | | | |
| TROY, MI 48083 | | | TINE IL 60067 | | | | | |
| ANALYTICAL INFORMATION | | | | | | | | |
| This certification was performed accord Procedure G-1; September, 1997. | ing to EPA Traceability Prot | ocol For Assay & Certific | ation of Gaseous Calibration Standards; | | | | | |
| | 1033730 Certification D | ate: 27Jul2009 | Exp. Date: 26Jul2012 | | | | | |
| Cylinder Pressure***: 200 | 0 PSIG | | | | | | | |
| COMPONENT | CERTIFIED CONCENTRA | | ALYTICAL COURACY** TRACEABILITY | | | | | |
| CARBON DIOXIDE | 5.91 % | | - 1% Direct NIST and NMi | | | | | |
| OXYGEN | 14.1 % | 6 +, | - 1% Direct NIST and NMi | | | | | |
| NITROGEN | B. | ALANCE | | | | | | |
| REFERENCE STANDARD TYPE/SRM NO. EXPIRATION DATE NTRM 2300 01Nov2010 NTRM 2350 01Dec2011 | CYLINDER NUMBER 1D002807 K016398 | CONCENTRATION 23.04 % 23.20 % | COMPONENT CARBON DIOXIDE OXYGEN | | | | | |
| INSTRUMENTATION | | | | | | | | |
| INSTRUMENT/MODEL/SERIAL# | <u>I</u> | DATE LAST CALIBRATED | ANALYTICAL PRINCIPLE | | | | | |
| 97/2000/609015 CAI/1109/V03018 | | 1 <i>6Ju</i> l2009 01Jul2009 | NDIR PARAMAGNETIC | | | | | |
| ANALYZER READINGS | | | | | | | | |
| (Z=Zer | o Gas R=Reference Ga | | Correlation Coefficient) | | | | | |
| First Triad Analysis | Second Triad | Analysis | Calibration Curve | | | | | |
| CARBON DIOXIDE | | | | | | | | |
| Date: 27Jul2009 Response Unit:MV Z1=0.00000 R1=102.5000 T1=43.00000 | | | Concentration = A + Bx + Cx2 + Dx3 + Ex4 $r = 0.999992$ | | | | | |
| R2=102,5000 Z2=0.00000 T2=43.00000 | | 1 | Constants: A = -0.00322681 | | | | | |
| Z3=0.00000 T3=43.00000 R3=102.5000 | | | B=0.13615338 C=-0.0005754 | | | | | |
| Avg. Concentration: 5.909 % | | | D=1.402196-05 E=0 | | | | | |
| OXYGEN | ı r | | | | | | | |
| Date: 28Jul2009 Response Unit:% | | | Concentration = $A + Bx + Cx^2 + Dx^3 + Ex^4$ | | | | | |
| Z1=0.00000 R1=23.20000 T1=14.06000 R2=23.20000 Z2=0.00000 T2=14.06000 | | | r=0.999992 Constants: A=-0.00675858 | | | | | |
| R2=23.20000 22=0.00000 72=14.06000 72=14.06000 23=0.00000 73≈14.06000 R3=23.20000 | | | B = 0.999864575 C = 0 | | | | | |
| Avg. Concentration: 14.05 % | | | D=0 E=0 | | | | | |
| APPROVED BY: | | | | | | | | |

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| | | | |] | RATA CLASS | |
|---------------------|---|----------------|-----------------------|-----------------------------|--------------------------------|--|
| | JIDE Air Liquide Ame | LLC | Scott | 1 | Dual-Analyzed Cali | bration Standard |
| 1290 | COMBERMERE STREET | r, troy | , MI 48083 | | Phone: 248-589 | -2950 Fax: 248-589-2 |
| CERTIFIC | ATE OF ACCU | RACY | : EPA Proto | ocol Gas | | |
| Assay Laborato | Ω. | | | | Customer | |
| | • | | P.O. No.: 574 | | CLEAN AIR ENG | NEERING |
| AIR LIQUIDE A | MERICA SPECIALTY G | ASES LL | C Project No.: O | 5-76738-005 | DON ALLEN 500 W. WOOD S | TOFFT |
| TROY, MI 4808 | | | | | PALATINE IL 6 | |
| | - | | | | | |
| | INFORMATION | | | | | |
| • | n was performed accor September, 1997. | ding to | EPA Traceability | Protocol For Ass | ay & Certification of Gas | eous Calibration Standards; |
| Cylinder Numb | • | M0462 | 55 Certificatio | n Date: 0 | 9Jun2009 Exp. | Date: 08Jun2012 |
| Cylinder Press | ure***: 20 | 00 PSI | 3 | | - | |
| | | | | | ANALYTICAL | |
| COMPONENT | 75 | CER | TIFIED CONCEN 13.9 | <u> 1 RATION (Mole</u> % | <u>s) ACCURACY</u> * +/- 1% | TRACEABILITY Direct NIST and NMi |
| CARBON DIOXI | | | 6.01 | % % | +/- 1% | Direct NIST and NMi |
| NITROGEN | | | | BALANCE | ., | |
| NTRM 1675 | 020ct2012 01Jan2010 | K0065 K0012 | | 13.93 10.03 | | OXIDE |
| NTRM 2658 | 01Jan2010 | K0012 | 90 | 10.03 | % OXYGEN | |
| INSTRUMENTAT | ION | | | | | |
| INSTRUMENT/MOL | | | | DATE LAST | CALIBRATED | ANALYTICAL PRINCIPLE |
| PIR/2000/609015 | | | | 11May | | NDIR |
| CAI/110P/V03018 | | | | 01Jun: | 2009 | PARAMAGNETIC |
| ANALYZER RI | ADINGS | | | | ····· | |
| • | | ro Gas | | | | - · · · • |
| First Tri | ad Analysis | | Second T | riad Analysis | C. | alibration Curve |
| CARBON DIOXID | E | _ | | | | |
| Date: 09Jun2009 | Response Unit:MV |] | | | Concentrat | ion = A + Bx + Cx2 + Dx3 + Ex4 |
| Z1=0.00000 R1= | 80.60000 T1 = 80.30000 | | | | r == 0.99991 | |
| | 0.00000 T2=80.30000 | 1 | 1 | | Constants: B=0.1118 | A = -0.00492643 14122 C = 0.00014738 |
| | 80.30000 R3=80.60000 13.86 % | ΄ | | | D=6.7609 | |
| Avg. Concentration: | 13.00 70 | J | L | • | | |
| OXYGEN | | , | | | | |
| Date: 09Jun2009 | lesponse Unit:% | | | | | cn = A + Bx + Cx2 + Dx3 + Ex4 |
| | 10.06000 T1 = 6.01000 | | | | r = 0.99999 | - |
| | D.00000 T2 = 6.01000 | | | | Constants: | A=-0.00970246 |
| | | | | | B ≈ 0.9998 | |
| Z3 = 0.00000 T3 = | 6.01000 R3 = 10.06000 | | | | D_0 | E=0 |
| | 6.01000 R3 = 10.06000 6.005 % | | | | D=0 | E=0 |
| Z3 = 0.00000 T3 = | |] / | | | D=0 | E=0 |
| Z3 = 0.00000 T3 = | | [| | | D-0 | E=0 |
| Z3 = 0.00000 T3 = | 6.005 % | / | | | D-0 | E=O |

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WHEELABRATOR NORTH BROWARD, INC. POMPANO BEACH, FL

CleanAir Project No: 10955-2

| ASTM D 6866-08 AND 7459-08 CO2 SAMPLING/ANALYSIS RESULTS | F |
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WHEELABRATOR NORTH BROWARD POMPANO BEACH, FL

Client Reference No: CleanAir Project No: 10955-2

| RESULTS | 5 | | | | | | | 11 | | | |
|-------------------|------------------|---------------------|----------------------------|---------------------------|----------|--------------------------------|--------------------------------|---|------------------------------|--------------------|------------------------------|
| | | | | Ta | ble 2-14 | k: | | | | | |
| | Air Flow Summary | | | | | | | | | | |
| Run Number | Run Date | Run Time | Steam Flow Klbs/hour | Flue Gas Temp Deg F | | O ₂ % | CO₂ % | CO₂ Sample Rate (ipm) ¹ | Stack Flow 2RSD (%) | Air Flow, DSCFM | Air Flow, DSC FM@ 7%O2 |
| 1-O-M5/29-1 | | 07:21-09:32 | 183.9 | 293 | 191,586 | 9.5 | 9.9 | 0.2 | 11.6% | 105,082 | 85,956 |
| 1-O-M5/29-2_ | | 10:00-12:14 | 184.4 | 295 | 191,421 | 9.5 | 9.9 | 0.2 | 12.2% | <u>104,870</u> | 86,310 |
| 1-O-M5/29-3 | | 12:36-14:47 | 183.4 | 301 | 193,814 | 9.7 | 9.8 | 0.2 | 15.3% | 105,806 | 84,949 |
| 1-O-M13B-1 | | 11:46-12:56 | 184.0 | 303 | 205,926 | 10.6 | <u>9.1</u> | 0.4 | 12.1% | 111,627 | 83,118 |
| 1-O-M13B-2 | | 13:15-14:27 | 184.0 | 302 | 207.433 | 10.1 | 9.6 | .0,4 | 12.9% | 111.678 | 86,530 |
| <u>1-O-M13B-3</u> | 3/17/2010 | 14:45-15:53 | 184.1 | 303 | 198,952 | 10.0 | 9,8 | 0.4 | 11.0% | 106.345 | 83.699 |
| | | AVATOR | | | | and a case of the state of the | the familie of the back for an | | | | |
| 2-O-M5/29-1 | | 07:09-09:22 | 1 <u>83.9</u> | 307 | 201,928 | 10,1 | 9.3 | 0.2 | _13.9% | 108,134 | 84,251 |
| 2-O-M5/29-2 | | 9;49-12:02 | 182.9 | 308 | 193,105 | 9.8 | 9.6 | 0,2 | 10.0% | <u>103,333</u> | 82.890 |
| 2-O-M5/29-3 | | 12:27-14:39 | 183.9 | 308 | 199.217 | <u>9</u> ,9 | 9,6 | 0,2 | <u>16,8%</u> | 105.806 | 83,856 |
| 2-O-M13B-1 | | 07:09-08:24 | 183,9 | 306 | 190,226 | 10.0 | 9.3 | 0.4 | 14,3% | 101.644 | 79,560 |
| 2-O-M13B-2 | | 08:56-10:10 | 184.2 | 305 | 182,805 | 9,6 | 9,6 | 0,4 | 10.0% | 97,309 | 78,827 |
| 2-O-M13B-3 | | 10:45-12:05 | 183.0 | 306 | 185,088 | 10.2 | 9.1 | 0,4_ | 13,4% | 99.545 | 76,986 |
| 2-O-M23-1 | | 08:44-13:36 | 184.1 | 301 | 198,967 | 9.7 | 9.7 | 0.1 | 8.7% | 107.335 | 86,640 |
| 2-O-M23-2 | | 06:54-12:19 | 184.3 | 307 | 214,211 | 9.7 | 9.8 | 0.1 | 7.0% | 113,400 | 91,046 |
| 2-O-M23-3 | 3/17/2010 | 12:53-17:26 | 183.9 | 308 | 203,730 | 10.3 | 9.5 | 0.1 | 8.8% | 108,891 | 82,961 |
| | | MAX MODERA | 的行政的政策 | | | 0023 | 100 | 512 | | 南10月10月 | 編集1002編 |
| 3-O-M5/29-1 | 3/17/2010 | 06;50-09:03 | 184,2 | 303 | 174,264 | 8.7 | 10,5 | 0,2 | 16,1% | 90,897 | 79,715 |
| 3-O-M5/29-2 | 3/17/2010 | 09:26-11:38 | 184.2 | 304 | 186,885 | 8.3 | 10.9 | 0.2 | 9.4% | 97,143 | 88,057 |
| 3-O-M5/29-3 | 3/17/2010 | 11:59-14:11 | 183.5 | 304 | 184,323 | 8.7 | 10.8 | 0.2 | 12.1% | 105,806 | 84,424 |
| 3-O-M13B-1 | 3/16/2010 | 11:4 <u>9-13:07</u> | 183.7 | 298 | 173,798 | 9.9 | 9.7 | 0.4 | 8.5% | 101,644 | 74,155 |
| 3-O-M13B-2 | 3/16/2010 | 13:33-14:44 | 183.9 | 299 | 179,576 | 9.5 | 10.0 | 0.4 | 11.4% | 96,031 | 78,552 |
| 3-O-M13B-3 | | 15:07-16:16 | 184,2 | 299 | 173.781 | 9.7 | 10.0 | 0.4 | 11.0% | 92,736 | 74,589 |
| | | AV/CETO2 | | | 新口的新闻 | | | | | 17767.6C | . <u>/</u> |
| - | EDINA | | | 3024 | 115 1924 | - C A-2 | | | | | 02,70 |

 1 CO2 gas sample flow rate was within 10% of initial flow rate throughout all test runs.

In accordance with the EPA Greenhouse Gas (GHG) Monitoring, Reporting and Recordkeeping Regulations (MRRR) an integrated gas sample (IGS) of all FF Outlet isokinetic sample trains was collected in accordance with ASTM Method 7459-08. All of the test run IGS bags that met the 2 times relative standard deviation (2RSD) stack flow rate criteria (<30%) were proportionally combined into a single Tedlar® bag for analysis by Beta Analytic, Inc for Biogenic CO₂ utilizing ASTM Method D6866-08. All of the IGS bags were collected within 10% of the initial sample rate. The IGS bag collection rate is recorded on the field data sheets presented in Appendix G. The stack flow rate 2RSD is calculated and presented in the field data printouts (Appendix H) of this report. All outlet isokinetic samples met the 2RSD requirements.



ISO-17025 Accredited Testing Laboratory

PJLA ISO/IEC 17025:2005 Testing Accreditation # 59423

Beta Analytic Inc. 4985 SW 74 Court Miami, Florida 33155 USA Tel: 305-667-5167 Fax: 305-663-0964 info@betalabservices.com www.betalabservices.com

Summary of Results : Biogenic CO2 Determination using ASTM-D6866

| Submitter: | Mr. Scott A. Brown | Date Received: | March 22, 2010 | | |
|-------------------|--|----------------|---------------------------|--|--|
| Company: | Company: Clean Air Engineering | Date Reported: | March 26, 2010 | | |
| Laboratory Number | Submitter Label | Material | Mean Biomass CO2 Content* | | |
| Beta-277290 | Wheelabrator North Broward - 3/16-18/2010 | Biogenic CO2 | 63% | | |

^{*} ASTM-D6866 cites precision on the Mean Biomass CO2 Content as +/- 3% (absolute). This is the most conservative estimate of error in the measurement of complex biomass containing solids and liquids based on empirical results. Real precision for readily combustible and homogenous materials (e.g. gasoline) and especially samples recieved as CO2 (e.g. flue gas or CEMS exhaust) can be as low as +/- 0.5-2%. The result only applies to the analyzed material. Fluctuations in carbon content within a batch of product, gasoline or flue gas must be determined separately (e.g. averaged measurements of multiple solids or liquids, and single measurement of the combination of gas aliquots collected over time). The accuracy of the result as it applies to the analyzed product, fuel, or flue gas relies upon all the carbon in the analyzed material originating from either recently respired atmospheric carbon dioxide (within the last decade) or fossil carbon (more than 50,000 years old). "Percent biomass" specifically relates % renewable (or fossil) carbon to total carbon, not to total mass or molecular weight. Mean Biomass CO2 estimates greater than 100% are assigned a value of 100% for simplification.

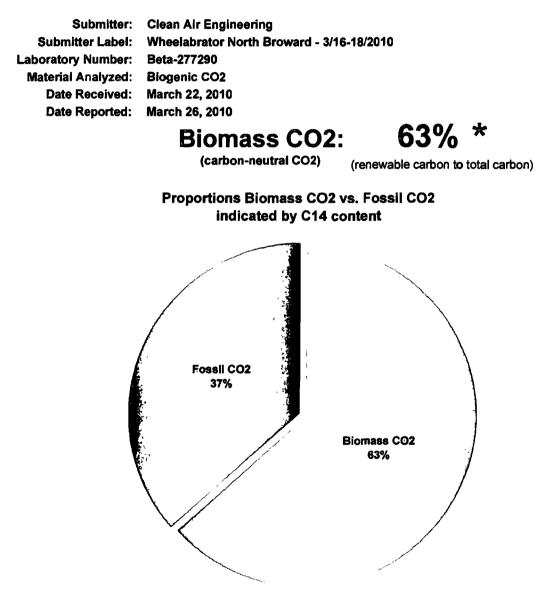


ISO-17025 Accredited Testing Laboratory

PJLA ISO/IEC 17025:2005 Testing Accreditation # 59423

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Report of Biomass CO2 Content Analysis using ASTM-D6866



* ASTM-D6866 cites precision on the mean Biomass CO2 Result as +/- 3% (absolute). This is the most conservative estimate of error in the measurement of complex biomass containing solids and liquids based on empirical results. Real precision for readily combustible and homogenous materials (e.g. gasoline) and especially samples recieved as CO2 (e.g. flue gas or CEMS exhaust) can be as low as +/- 0.5-2%. The result only applies to the analyzed material. Fluctuations in carbon content within a batch of product, gasoline or flue gas must be determined separately (e.g. averaged measurements of multiple solids or liquids, and single measurement of the combination of gas aliquots collected over time). The accuracy of the result as it applies to the analyzed product, fuel, or flue gas relies upon all the carbon in the analyzed material originating from either recently respired atmospheric carbon dioxide (within the last few decades) or fossil carbon (more than 50,000 years old). "Percent biomass" specifically relates % renewable (or fossil) carbon to total carbon, not to total mass or molecular weight. Mean Biomass CO2 estimates greater than 100% are assigned a value of 100% for simplification.



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Explanation of Results

Biomass Analysis using ASTM-D6866

The application of ASTM-D6866 to derive a "Biomass CO2 content" for carbon dioxide effluents is built upon the same concepts as those used by the US Department of Agriculture to derive the biobased content of manufactured products containing biomass carbon. It is done by comparing a relative amount of radiocarbon (C14) in an unknown sample to that of a modern reference standard. The ratio in contemporary biomass will be 100% and the ratio in fossil materials will be zero. Carbon dioxide derived from combustion of a mixture of present day biomass and fossil carbon will yield an ASTM-D6866 result that directly correlates to the amount of biomass carbon combusted and carbon-neutral CO2 generated.

The modern reference standard is a National Institute of Standards and Technology (NIST) standard with a defined radiocarbon content of 100% contemporary carbon for the year AD 1950. AD 1950 was chosen since it represented a time prior to thermo-nuclear weapons testing which introduced large amounts of excess radiocarbon into the atmosphere with each explosion (termed "bomb carbor"). This was a logical point in time to use as a reference since this excess bomb carbon would change with increased or decreased weapons testing. A fixed correction for this effect is applied per the ASTM-D6866 requirements, applying specifically to carbon removed from the atmospheric CO2 reservoir since about 1996. Carbon removed prior to about 1996 will contain elevated radiocarbon signatures, not directly applicable to the ASTM-D6866 correction. Typical areas to which the correction may not apply are landfills more than 5-10 years old and to trees which began to grow more than 20 years ago.

Carbon dioxide effluent derived from combustion of 100% present day biomass will yield results of 100% renewable content. Carbon dioxide effluent derived from the combustion of 100% fossil fuel will yield results of 0% renewable content. Carbon dioxide produced from mixed fuels (biomass plus fossil fuel) will yield a percentage result in direct proportion to the biomass carbon consumed vs. fossil carbon consumed in the combustion. The final result is referred to as the MEAN BIOMASS CO2 CONTENT and assumes all the carbon in the carbon dioxide was derived from either present day living or fossil sources.

The results provided in this report involved materials provided without any source information. This situation is highly probable in a real life situation. The MEAN VALUE quoted in this report encompasses an absolute range of 6% (plus and minus 3% on either side of the MEAN BIOMASS CO2 CONTENT to account for variations in end component radiocarbon signatures (a conservative approximation). It is presumed that all materials are present day or fossil in origin and that the desired result is the amount of biomass component "present" in the material, not the amount of biomass material "used" in the manufacturing process. The most conservative interpretation of the reported percentages is as maximum values.

ASTM-D6866 results relate directly to the percentage carbon-neutral CO2 in an incineration effluent. A value of 71% renewable content measured on CO2 effluent would indicate that 71% of the exhausted CO2 was from biomass (29% from fossil fuel). It does not represent the weight of biomass combusted or the weight of fossil fuel combusted. This is advantageous since the weight of the fuels only indirectly relate to the up-take of carbon dioxide from the atmosphere. The respiration uptake compound was carbon dioxide and the combustion effluent was carbon dioxide. The ASTM-D6866 result directly and specifically relates to the amount of carbon-neutral CO2 consumed and expelled.

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