

Continuation

of document

submitted on

March 7, 2003



**Georgia-Pacific**

Palatka Pulp and Paper Operations  
Consumer Products Division

P.O. Box 919  
Palatka, FL 32178-0919  
(386) 325-2001

December 13, 2002

Mr. Christopher L. Kirts  
District Air Program Administrator  
State of Florida  
Department of Environmental Protection  
7825 Baymeadows Way, Suite B200  
Jacksonville, Florida 32256-7590

Re: Bleach Plant Compliance Test – October 2002  
Georgia-Pacific Palatka Operations

Dear Mr. Kirts:

Continuous monitoring system (CMS) parameters, monitoring frequencies, averaging times and the rationale for selecting the CMS are required to be submitted for approval pursuant to 40 CFR 63.453 (n). This information has been updated from a previous submittal (letter dated October 25, 2002, Appendix A) reflecting recent compliance testing conducted in October 2002, which has been summarized and included in this correspondence for your review. (A copy of the test report is included as an attachment.)

The Bleach Plant scrubber collects and treats emissions from the No. 3 Bleach Plant as well as emissions from the R8/10 Chlorine Dioxide Generator. The pH of the gas scrubber effluent, the scrubber liquid influent flow rate, and the fan amps were continuously recorded during the testing. We have analyzed this information pursuant to 40 CFR 63.453 (n) as follows.

Although all runs demonstrated compliance with 40 CFR 63.445 (c) (2) by a considerable margin, four of the six runs were selected to develop operating parameter values providing the greatest operating flexibility while also demonstrating continuous compliance (see Table 1).

The average pH during these runs was 9.2 with a minimum during one run of 9.0 (see Figures 1 and 2 in Appendix B). We, therefore, propose for the Administrator's approval that we operate the scrubber effluent pH above a minimum of 9.0 as a rolling 3-hour average with a monitoring frequency of at least once every 15 minutes (see Table 2). We believe the monitoring frequency of once every 15 minutes to be appropriate because the standard deviation of the data was quite low. The average flow of the scrubber medium was 1257 gpm with a minimum of 1252 gpm. By the same rationale we propose for the Administrator's approval that we operate above a minimum flow of 1252 as a rolling 3-hour average with the same monitoring frequency described above.

Region 4 previously approved monitoring fan amperage of the bleaching system vent gas fan as an alternative monitoring parameter to 40 CFR 63.453 (c)(2) (letter dated December 22,

Mr. Christopher L. Kirts  
Page Two  
December 13, 2002

2000). The mill continuously monitors fan amperage and displays it as fan load on its Distributed Control System (DCS). Fan load during the time of the testing was calculated as follows (Equation 1).

$$\%Load = \frac{\text{measured amps}}{0.701 * \text{full load amps}} * 100 = \frac{\text{measured amps}}{0.701 * 25.7} * 100 = \frac{\text{measured amps}}{18.02} * 100$$

Please note 0.701 represents a conversion factor for ranging of the signal from the field instrumentation to the DCS.

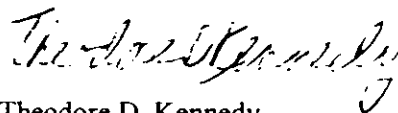
Figure 3 reflects the fan load/amperage when the Bleach Plant goes down. Because the mill continues to run the fan the amperage goes up although the process is down. We have also taken all the belts off the fan motor to determine its "no load" amperage, 9.8 amps. Because of data variability we propose to operate the fan such that the amperage is below 19.3 and above 10.8 amps as a rolling 3-hour average. This will be converted to fan load for convenience of the operators. Note that this calculation has been simplified according to the following (Equation 2) and became effective on December 5, 2002 at 13:05.

$$\%Load = \frac{\text{measured amps}}{\text{full load amps}} * 100 = \frac{\text{measured amps}}{25.7} * 100$$

Again, we propose to monitor fan amperage/load at least once every 15 minutes. In all cases, pH, flow, and % Load data will be transferred to a plant wide information (PI) system for record keeping purposes.

We respectfully request written approval as required by 40 CFR 63.453 (n). If you have any questions about our rationale please do not hesitate to call me at (386) 329-0918.

Sincerely,



Theodore D. Kennedy  
Vice President

tk

Enclosures

cc: Lee Page, EPA Region 4  
William Jernigan, Atlanta  
Scott Matchett, Atlanta  
Cindy Barlow  
Nickolai Selbach

# Appendix A

Letter Dated October 25, 2002



Palatka Pulp and Paper Operations  
Consumer Products Division

P.O. Box 919  
Palatka, FL 32178-0919  
(386) 325-2001

October 25, 2002

Mr. Mort Benjamin  
Air Compliance Supervisor  
Northeast District  
Florida Department of Environmental Protection  
7825 Baymeadows Way, Suite 200B  
Jacksonville, FL 32256-7577

**Re: Cluster Rule CMS Parameters (40 CFR 63.453(n))  
Georgia-Pacific Palatka Operations  
1070005**

Dear Mr. Benjamin:

During a recent review of recordkeeping and reporting procedures we discovered that continuous monitoring system (CMS) parameters, monitoring frequencies, averaging times and the rationale for choosing the CMS were not submitted in a readable, concise format and summary to the Department pursuant to 40 CFR 63.453 (n).

The CMS listed in the attached tables were chosen because they indicate when there is a breach of the Closed Vent Collection System, a bypass of the Condensate Collection System, or they otherwise indicate operation outside of tested operating ranges on the condensate, low-volume-high-concentration (LVHC) and bleach plant treatment systems specifically identified in 40 CFR Subpart S. The tables show the equipment, the parameters that are monitored, the CMS tag numbers, the limits that have been evaluated and the thresholds or minimum averaging times.

Limit switches, pressure measurements, stream flows, temperatures, pH, fan load, pH and indications of valve positions are forms of CMS that are generally accepted industry-wide for monitoring for compliance.

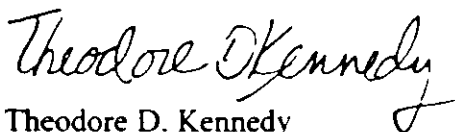
The parameters designated as "Valve Position" or "Vent Valve Position" in the attached Tables indicate that a system is either being collected (valve "Closed") or bypassed (valve "Open") to show compliance with the requirement to collect gases from the named LVHC systems.

The incinerator temperature values were selected because data collected during the IPT of the two incinerators indicated that compliance with the treatment requirements of 63.443(d) were met at all times when the temperatures were above the chosen values. The averaging time was selected based on run times of the reference test methods. Similarly, the parameter values shown for the stripper parameters mandated under 63.453(g) were based on data gathered during the stripper characterization study.

Finally, the scrubber parameters are either mandated by the rule (see 63.453(c)) or approved as acceptable alternative monitoring. Parameter values were chosen based on data gathered during the scrubber IPT and subsequent performance tests, and when the parameters are within the designated ranges, we meet the bleach plant treatment requirements found in 63.445(c). Averaging times were selected based on normal compliance test times.

If you have any more questions concerning this issue, please do not hesitate to contact either Joe Taylor at 386-329-0027 or via e-mail at [jetaylor@gapac.com](mailto:jetaylor@gapac.com) or me at 386-329-0918.

Sincerely,



Theodore D. Kennedy  
Vice-President  
Palatka Operations

Bc: S. D. Matchett (GA030-43)  
W. M. Jernigan (GA030-09)

## MACT I CONTINUOUS MONITORING SYSTEMS

Area	Parameter/Equipment	Parameter Monitored	PI Tag Number	Range/Limit	Threshold/Averaging Time
Bleach Plant (scrubber)	Scrubbant Recirculation Flow	Flow	40fi31.pv	≥ 1229 gpm	3-hr average
	Scrubber Fan Load	Load	40ii33.pv	≥ 85%	Continuous
	Scrubbant Recirculation pH	PH	40ai32.pv	≥ 9.1	3-hr average
Thermal Oxidizer	Primary Incinerator Temperature	Temperature	13ncgincin:13ttm22a.pnt	≥ 1300° F	3-hr rolling average
	Backup Incinerator Temperature	Temperature	13ncgincin:13ttm22b.pnt	≥ 1300° F	
Steam Stripper	Steam Flow to Stripper	Steam Flow	13constrip:13fcc01.meas		3-hr rolling average
	Condensate Flow to Stripper	Condensate Flow	13constrip:13fcc19.meas	N/A	3-hr rolling average
	Condensate Temperature entering Column	Temperature	13constrip:13ttc30.pnt	≥ 160° F	3-hr rolling average
Condensate Collection	Pre-evaporator 1 <sup>st</sup> and 2 <sup>nd</sup> effect foul, Pre-evaporator hotwell condensate	Flow, gpm	13concollect:13ftk20.pnt	N/A	Daily average rolled into 15-day rolling average
	1 <sup>st</sup> and 2 <sup>nd</sup> effect contaminated condensate, as makeup	Flow, gpm	13concollect:13ftk03.pnt	N/A	Daily average rolled into 15-day rolling average
	Turpentine Decanter Underflow and Secondary Condenser condensate	Flow, gpm	13concollect:13ftk21.pnt	N/A	Daily average rolled into 15-day rolling average

## MACT I CONTINUOUS MONITORING SYSTEMS

Area	Parameter/Equipment	Parameter Monitored	Loop Number	Range/Limit	Threshold/Averaging Time
Closed Vent System	#1 Blow Tank Safety Valve	Limit Switch	05VL1VNT	Open/Closed	minute
	#2 Blow Tank Safety Valve	Limit Switch	05VL2VNT	Open/Closed	minute
	#3 Blow Tank Safety Valve	Limit Switch	05VL3VNT	Open/Closed	minute
	Secondary Condenser Vent	Limit Switch	13D06	Open/Closed	minute
	Secondary Condenser Rupture Disc	Pressure Transmitter	13D07	14.5 psi	minute
	Secondary Condenser Rupture Disc	Pressure Transmitter	13D61	14.5 psi	minute
	Accumulator Safety Valve	Limit Switch	13A07	Open/Closed	minute
	Accumulator Safety Valve	Limit Switch	13A22	Open/Closed	minute
	Pre-evaporator Hotwell Loop Seal	Pressure Transmitter	13PTB23	14" water column	minute
	Pre-evaporator Hotwell Vent	Limit Switch	13D01	Open/Closed	minute
	Pre-evaporator Hotwell Rupture Disc	Pressure Switch	13D02	10 psi	minute
	Turpentine Condenser Vent	Limit Switch	13J01	Open/Closed	minute
	Turpentine Condenser Rupture Disc	Pressure Switch	13J02	10 psi	minute
	#1 Evaporator Hotwell Vent	Limit Switch	13J26	Open/Closed	minute



## MACT I CONTINUOUS MONITORING SYSTEMS

Area	Parameter/Equipment	Parameter Monitored	Loop Number	Range/Limit	Threshold/Averaging Time
Closed Vent System	#1 Evaporator Hotwell Rupture Disc	Pressure Switch	13J27	10 psi	minute
	#2 Evaporator Hotwell Vent	Limit Switch	13J21	Open/Closed	minute
	#2 Evaporator Hotwell Rupture Disc	Pressure Switch	13J22	10 psi	minute
	#3 Evaporator Hotwell Vent	Limit Switch	13J16	Open/Closed	minute
	#3 Evaporator Hotwell Rupture Disc	Pressure Switch	13J17	10 psi	minute
	#3 Evaporator Hotwell Loop Seal	Pressure Transmitter	11PTJ12	14" water column	minute
	#4 Evaporator Hotwell Vent	Limit Switch	13J11	Open/Closed	minute
	#4 Evaporator Hotwell Rupture Disc	Pressure Switch	13J12	10 psi	minute
	#4 Evaporator Hotwell Rupture Disc	Pressure Switch	13J15	10 psi	minute
	#4 Evaporator Hotwell Loop Seal	Pressure Transmitter	68PTO46	14" water column	minute
	Stripper Feed Tank Water Seal	Water Seal	13K09	8 psi	minute
	Stripper Feed Tank Rupture Disc	Pressure Transmitter	13K15	14.5 psi	minute
	Stripper-off-gas to Oxidizer	Limit Switch	13L04	Open/Closed	minute
	Stripper-off-gas to Oxidizer Rupture Disc	Temperature Transmitter	13L14	160° F	minute

## MACT I CONTINUOUS MONITORING SYSTEMS

Area	Parameter/Equipment	Parameter Monitored	Loop Number	Range/Limit	Threshold/Averaging Time
Closed Vent System	Stripper-off-gas to Boiler	Limit Switch	59D12	Open/Closed	
	Stripper-off-gas to Boiler Rupture Disc	Pressure Transmitter	59D35	14.5 psi	
	NCG Vent to Oxidizer	Limit Switch	13D70	Open/Closed	
	NCG to Oxidizer Rupture Disc	Pressure Transmitter	13D65	14.5 psi	
	NCG to Oxidizer Rupture Disc	Temperature Transmitter	13D68	160° F	
	Batch NCG to Boiler Rupture Disc	Pressure Transmitter	13D63	14.5 psi	
	NCG Vent to Boiler	Limit Switch	59D08	Open/Closed	
	NCG to Boiler Rupture Disc	Temperature Transmitter	59D06	160° F	

# Appendix B

## Miscellaneous Information

Table 1

Run 1      Run 2      Run 3      Run 4  
 Start = 10/29/02 12:18   10/31/02 13:32   10/31/02 15:50   10/31/02 17:10  
 End = 10/29/02 13:23   10/31/02 14:43   10/31/02 16:56   10/31/02 18:16

	Do Stage			Eop Stage		D1 Stage		BP Scrubber						R-10 Run Status		Test				
	BAST/h		STDEV	% Pine	% HW	% Pine	% HW	Flow (gpm)		pH		Fan Load (%)	Fan Load (amps)	Fan Delta P (in H2O)	ClO2 (STPD)	Cl2				
	43FYB04.PV	Maximum		43AYB04W.PV	Calculation	43AYD04W.PV	Calculation	43AYF04W.PV	Calculation	40FF31.PV	Minimum	STDEV	40AJF32.PV	Minimum	STDEV	40IF33.PV	40IF33.PV	40PIF03.PV	37FYF14.PV	ppm
Run 1	50	52	0.6	100.0	0.0	100.0	0.0	100.0	0.0	1262	1261	0.6	9.1	9.0	0.06	83.9	15.1	20.9	0.00	0.233
Run 2	50	52	0.8	100.0	0.0	100.0	0.0	100.0	0.0	1263	1252	1.0	9.3	9.3	0.01	85.5	15.4	21.4	31.6	0.073
Run 3	50	52	0.6	100.0	0.0	100.0	0.0	100.0	0.0	1268	1257	0.8	9.3	9.3	0.00	85.4	15.4	21.4	37.3	0.020
Run 4	50	52	0.6	100.0	0.0	100.0	0.0	100.0	0.0	1262	1260	0.9	9.3	9.2	0.02	85.6	15.4	21.4	30.3	0.032
Average =										1257			9.2			85.1		15.3		

Table 2

<b>No. 3 Bleach Plant</b>					
<b>Parameter</b>		<b>Test Condition</b>	<b>Proposed Operating Value</b>	<b>Monitoring Frequency</b>	<b>Averaging Time</b>
pH, Minimum		9.0	9.0	5 min	3-hr., rolling
Scrubber flow, Minimum	(gpm)	1252	1252	5 min	3-hr., rolling
Fan load Minimum	(amps)	15.11 <sup>a</sup>	10.8 <sup>c</sup>	5 min	3-hr., rolling
Fan load Maximum	(amps)	15.45 <sup>b</sup>	19.3 <sup>d</sup>	5 min	3-hr., rolling
Fan "No Load"	(amps)	9.8			

<sup>a</sup> Equivalent to 83.9% Load, using Equation 1

<sup>b</sup> Equivalent to 85.8% Load, using Equation 1

<sup>c</sup> Equivalent to 41.9% Load using Equation 2

<sup>d</sup> Equivalent to 75% Load using Equation 2

Figure 1

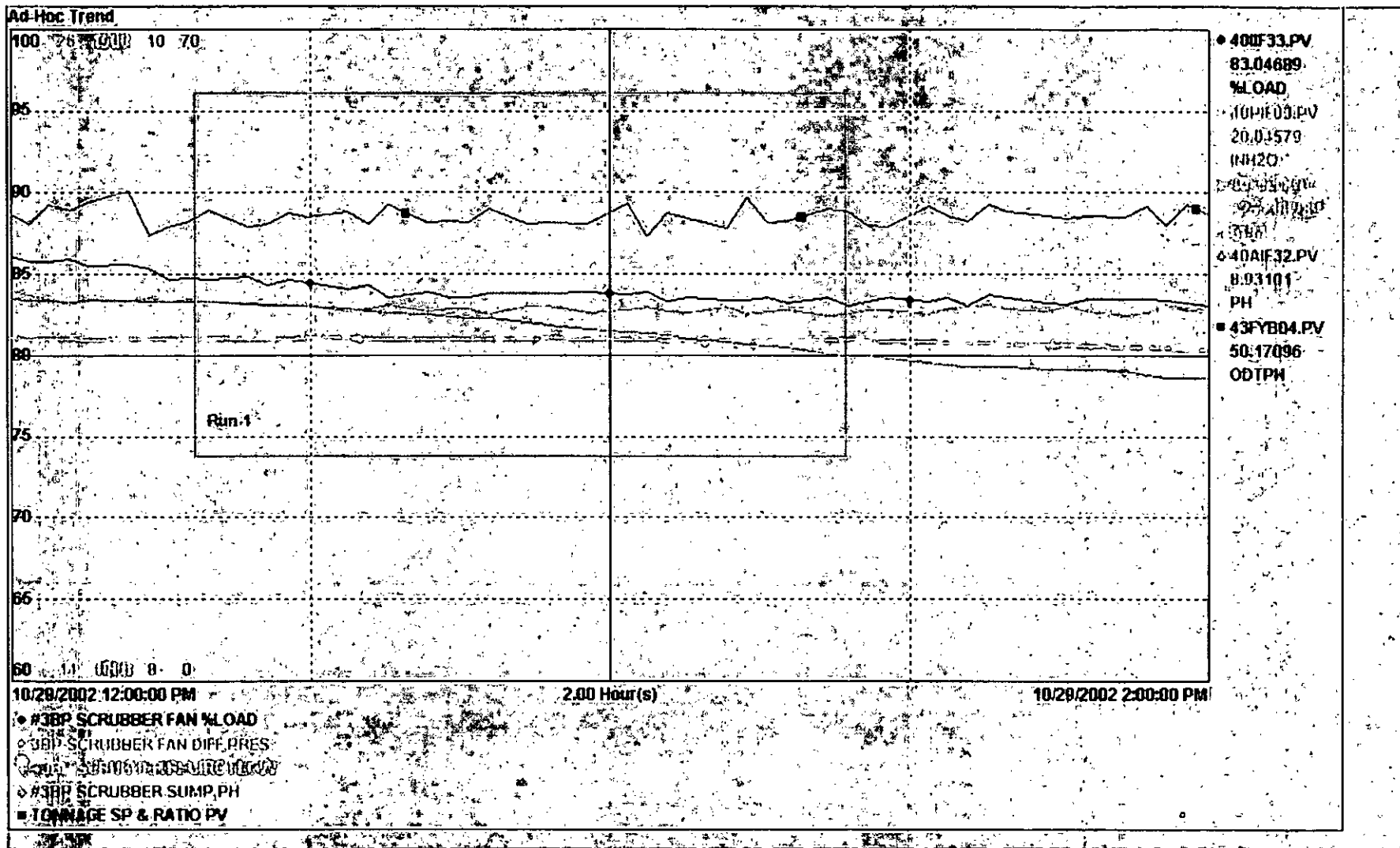


Figure 2

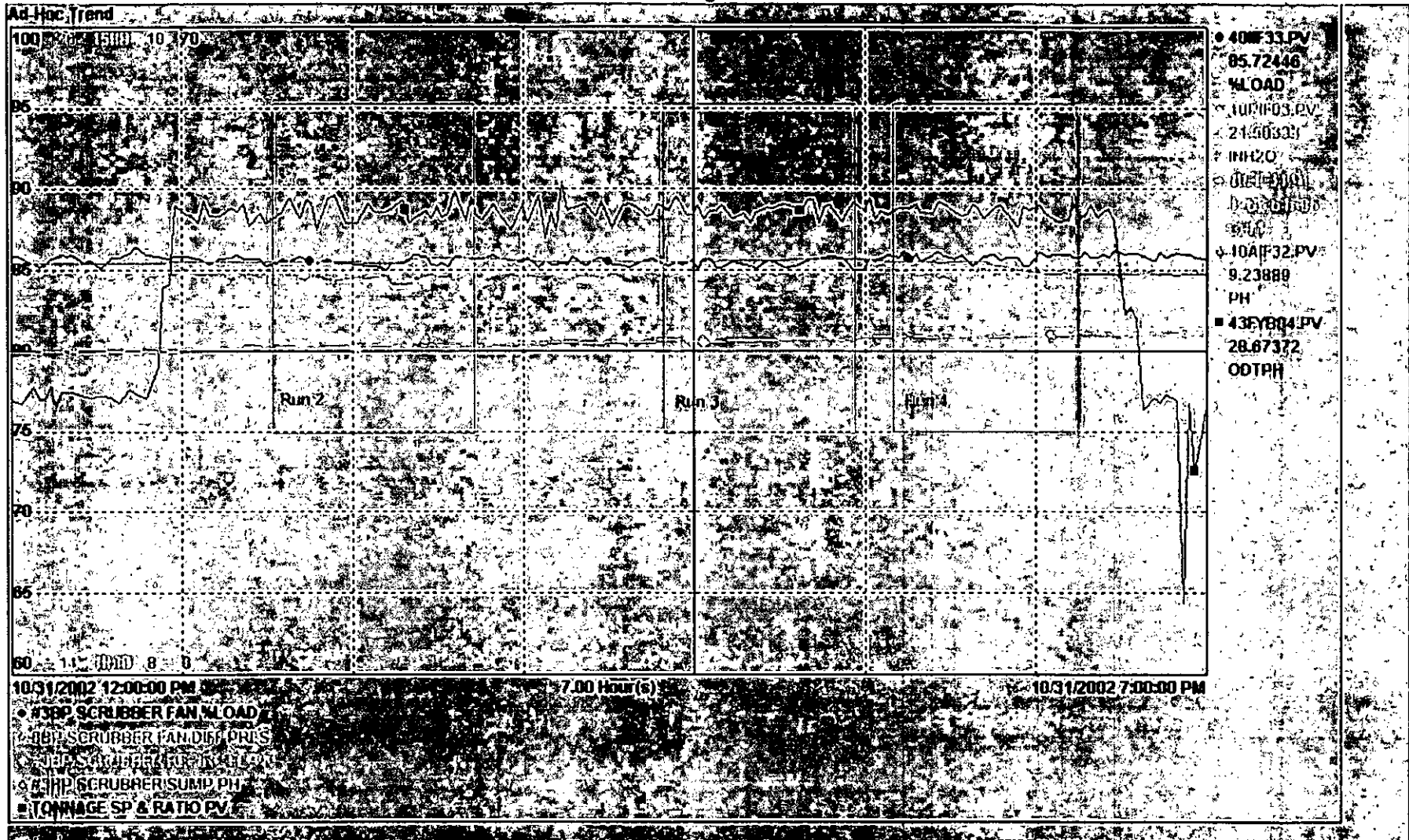
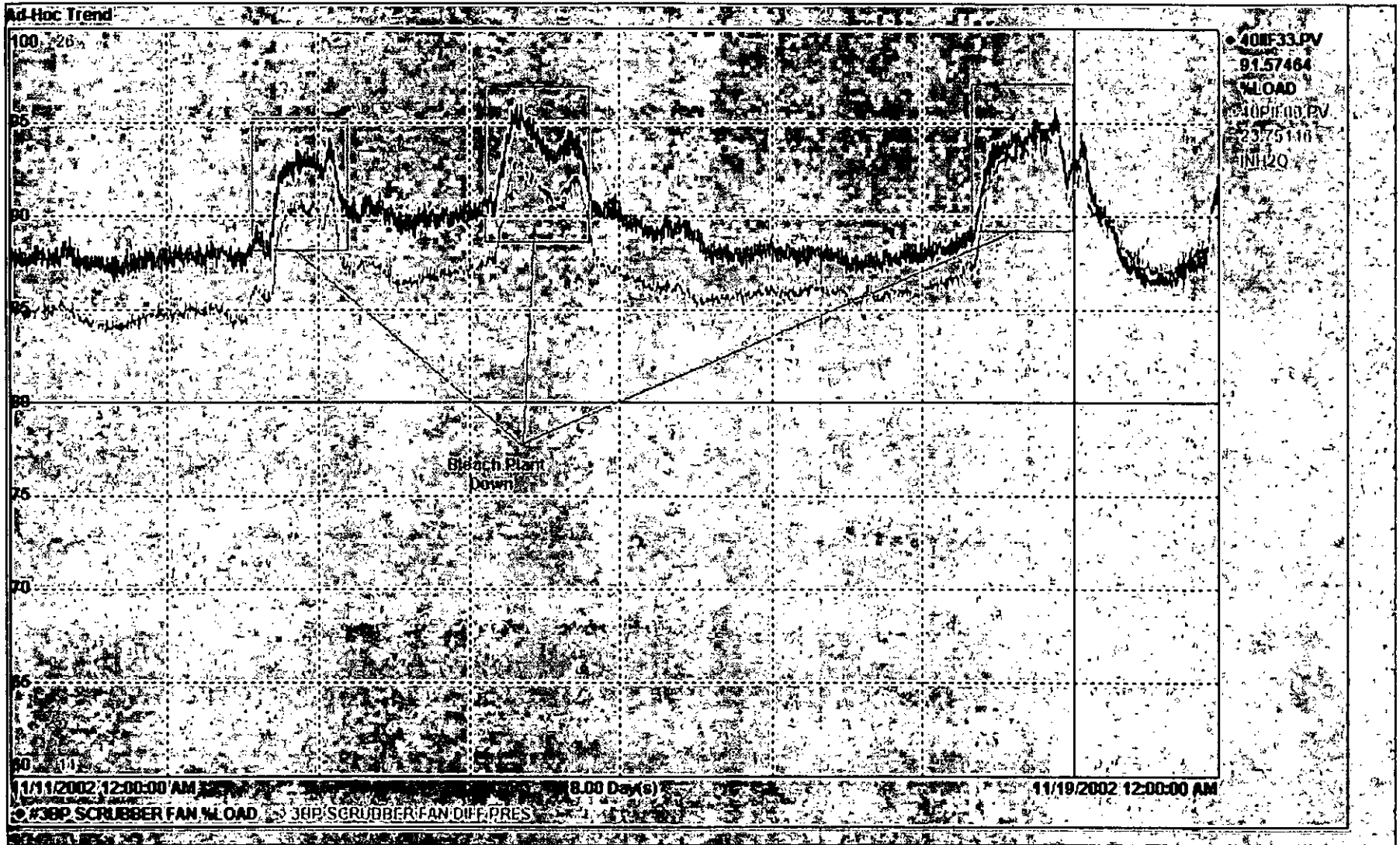


Figure 3





# Appendix C

Raw Data  
(5-minute averages)

pH Run 1		pH Run 2		pH Run 3		pH Run 4	
29-Oct-02 12:18:00	9.2	31-Oct-02 13:32:00	9.3	31-Oct-02 15:50:00	9.3	31-Oct-02 17:10:00	9.3
29-Oct-02 12:23:00	9.2	31-Oct-02 13:37:00	9.3	31-Oct-02 15:55:00	9.3	31-Oct-02 17:15:00	9.3
29-Oct-02 12:28:00	9.1	31-Oct-02 13:42:00	9.3	31-Oct-02 16:00:00	9.3	31-Oct-02 17:20:00	9.3
29-Oct-02 12:33:00	9.1	31-Oct-02 13:47:00	9.3	31-Oct-02 16:05:00	9.3	31-Oct-02 17:25:00	9.3
29-Oct-02 12:38:00	9.1	31-Oct-02 13:52:00	9.3	31-Oct-02 16:10:00	9.3	31-Oct-02 17:30:00	9.3
29-Oct-02 12:43:00	9.1	31-Oct-02 13:57:00	9.3	31-Oct-02 16:15:00	9.3	31-Oct-02 17:35:00	9.3
29-Oct-02 12:48:00	9.1	31-Oct-02 14:02:00	9.3	31-Oct-02 16:20:00	9.3	31-Oct-02 17:40:00	9.3
29-Oct-02 12:53:00	9.1	31-Oct-02 14:07:00	9.3	31-Oct-02 16:25:00	9.3	31-Oct-02 17:45:00	9.3
29-Oct-02 12:58:00	9.1	31-Oct-02 14:12:00	9.3	31-Oct-02 16:30:00	9.3	31-Oct-02 17:50:00	9.3
29-Oct-02 13:03:00	9.1	31-Oct-02 14:17:00	9.3	31-Oct-02 16:35:00	9.3	31-Oct-02 17:55:00	9.2
29-Oct-02 13:08:00	9.0	31-Oct-02 14:22:00	9.3	31-Oct-02 16:40:00	9.3	31-Oct-02 18:00:00	9.2
29-Oct-02 13:13:00	9.0	31-Oct-02 14:27:00	9.3	31-Oct-02 16:45:00	9.3	31-Oct-02 18:05:00	9.2
29-Oct-02 13:18:00	9.0	31-Oct-02 14:32:00	9.3	31-Oct-02 16:50:00	9.3	31-Oct-02 18:10:00	9.2
		31-Oct-02 14:37:00	9.3				

Flow Run 1		Flow Run 2		Flow Run 3		Flow Run 4	
29-Oct-02 12:18:00	1263	31-Oct-02 13:32:00	1253	31-Oct-02 15:50:00	1258	31-Oct-02 17:10:00	1261
29-Oct-02 12:23:00	1262	31-Oct-02 13:37:00	1253	31-Oct-02 15:55:00	1258	31-Oct-02 17:15:00	1261
29-Oct-02 12:28:00	1263	31-Oct-02 13:42:00	1252	31-Oct-02 16:00:00	1257	31-Oct-02 17:20:00	1261
29-Oct-02 12:33:00	1263	31-Oct-02 13:47:00	1252	31-Oct-02 16:05:00	1257	31-Oct-02 17:25:00	1261
29-Oct-02 12:38:00	1263	31-Oct-02 13:52:00	1253	31-Oct-02 16:10:00	1258	31-Oct-02 17:30:00	1261
29-Oct-02 12:43:00	1262	31-Oct-02 13:57:00	1252	31-Oct-02 16:15:00	1258	31-Oct-02 17:35:00	1261
29-Oct-02 12:48:00	1263	31-Oct-02 14:02:00	1252	31-Oct-02 16:20:00	1258	31-Oct-02 17:40:00	1261
29-Oct-02 12:53:00	1263	31-Oct-02 14:07:00	1252	31-Oct-02 16:25:00	1259	31-Oct-02 17:45:00	1262
29-Oct-02 12:58:00	1262	31-Oct-02 14:12:00	1252	31-Oct-02 16:30:00	1259	31-Oct-02 17:50:00	1262
29-Oct-02 13:03:00	1262	31-Oct-02 14:17:00	1253	31-Oct-02 16:35:00	1260	31-Oct-02 17:55:00	1262
29-Oct-02 13:08:00	1261	31-Oct-02 14:22:00	1254	31-Oct-02 16:40:00	1259	31-Oct-02 18:00:00	1263
29-Oct-02 13:13:00	1262	31-Oct-02 14:27:00	1254	31-Oct-02 16:45:00	1259	31-Oct-02 18:05:00	1263
29-Oct-02 13:18:00	1261	31-Oct-02 14:32:00	1254	31-Oct-02 16:50:00	1259	31-Oct-02 18:10:00	1263
		31-Oct-02 14:37:00	1255				

Fan Load (Amps) Run 1		Fan Load (Amps) Run 2		Fan Load (Amps) Run 3		Fan Load (Amps) Run 4	
29-Oct-02 12:18:00	15.26	31-Oct-02 13:32:00	15.40	31-Oct-02 15:50:00	15.37	31-Oct-02 17:10:00	15.47
29-Oct-02 12:23:00	15.23	31-Oct-02 13:37:00	15.44	31-Oct-02 15:55:00	15.39	31-Oct-02 17:15:00	15.44
29-Oct-02 12:28:00	15.20	31-Oct-02 13:42:00	15.43	31-Oct-02 16:00:00	15.39	31-Oct-02 17:20:00	15.45
29-Oct-02 12:33:00	15.14	31-Oct-02 13:47:00	15.41	31-Oct-02 16:05:00	15.38	31-Oct-02 17:25:00	15.48
29-Oct-02 12:38:00	15.09	31-Oct-02 13:52:00	15.40	31-Oct-02 16:10:00	15.38	31-Oct-02 17:30:00	15.45
29-Oct-02 12:43:00	15.07	31-Oct-02 13:57:00	15.38	31-Oct-02 16:15:00	15.38	31-Oct-02 17:35:00	15.39
29-Oct-02 12:48:00	15.10	31-Oct-02 14:02:00	15.36	31-Oct-02 16:20:00	15.36	31-Oct-02 17:40:00	15.46
29-Oct-02 12:53:00	15.11	31-Oct-02 14:07:00	15.34	31-Oct-02 16:25:00	15.40	31-Oct-02 17:45:00	15.45
29-Oct-02 12:58:00	15.10	31-Oct-02 14:12:00	15.38	31-Oct-02 16:30:00	15.35	31-Oct-02 17:50:00	15.44
29-Oct-02 13:03:00	15.05	31-Oct-02 14:17:00	15.43	31-Oct-02 16:35:00	15.39	31-Oct-02 17:55:00	15.38
29-Oct-02 13:08:00	15.03	31-Oct-02 14:22:00	15.47	31-Oct-02 16:40:00	15.43	31-Oct-02 18:00:00	15.47
29-Oct-02 13:13:00	15.03	31-Oct-02 14:27:00	15.38	31-Oct-02 16:45:00	15.45	31-Oct-02 18:05:00	15.48
29-Oct-02 13:18:00	15.03	31-Oct-02 14:32:00	15.40	31-Oct-02 16:50:00	15.42	31-Oct-02 18:10:00	15.47
		31-Oct-02 14:37:00	15.45				

Fan Load (%) Run 1		Fan Load (%) Run 2		Fan Load (%) Run 3		Fan Load (%) Run 4	
29-Oct-02 12:18:00	84.7	31-Oct-02 13:32:00	85.5	31-Oct-02 15:50:00	85.3	31-Oct-02 17:10:00	85.9
29-Oct-02 12:23:00	84.6	31-Oct-02 13:37:00	85.7	31-Oct-02 15:55:00	85.4	31-Oct-02 17:15:00	85.7
29-Oct-02 12:28:00	84.4	31-Oct-02 13:42:00	85.6	31-Oct-02 16:00:00	85.4	31-Oct-02 17:20:00	85.8
29-Oct-02 12:33:00	84.0	31-Oct-02 13:47:00	85.5	31-Oct-02 16:05:00	85.4	31-Oct-02 17:25:00	85.9
29-Oct-02 12:38:00	83.8	31-Oct-02 13:52:00	85.5	31-Oct-02 16:10:00	85.4	31-Oct-02 17:30:00	85.8
29-Oct-02 12:43:00	83.6	31-Oct-02 13:57:00	85.4	31-Oct-02 16:15:00	85.4	31-Oct-02 17:35:00	85.4
29-Oct-02 12:48:00	83.8	31-Oct-02 14:02:00	85.3	31-Oct-02 16:20:00	85.2	31-Oct-02 17:40:00	85.8
29-Oct-02 12:53:00	83.9	31-Oct-02 14:07:00	85.1	31-Oct-02 16:25:00	85.5	31-Oct-02 17:45:00	85.8
29-Oct-02 12:58:00	83.8	31-Oct-02 14:12:00	85.4	31-Oct-02 16:30:00	85.2	31-Oct-02 17:50:00	85.7
29-Oct-02 13:03:00	83.6	31-Oct-02 14:17:00	85.6	31-Oct-02 16:35:00	85.4	31-Oct-02 17:55:00	85.4
29-Oct-02 13:08:00	83.4	31-Oct-02 14:22:00	85.9	31-Oct-02 16:40:00	85.6	31-Oct-02 18:00:00	85.9
29-Oct-02 13:13:00	83.4	31-Oct-02 14:27:00	85.4	31-Oct-02 16:45:00	85.8	31-Oct-02 18:05:00	85.9
29-Oct-02 13:18:00	83.4	31-Oct-02 14:32:00	85.5	31-Oct-02 16:50:00	85.6	31-Oct-02 18:10:00	85.9
		31-Oct-02 14:37:00	85.7				

Attachment

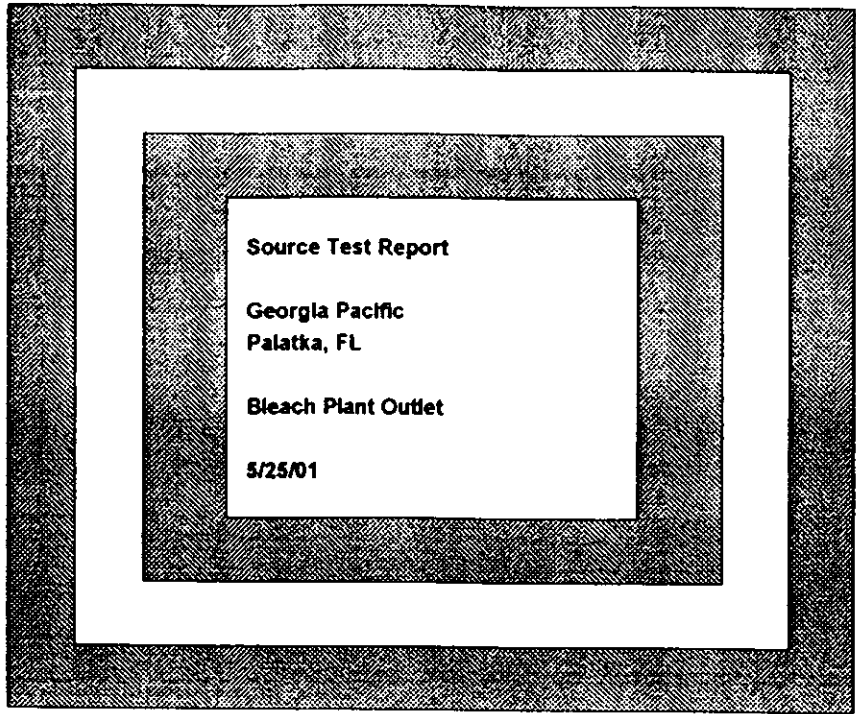


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\_\_\_\_\_  
**David Salter**

**USE OF THIS REPORT AND  
INFORMATION INCLUDED**

This Report and the information contained is the property of the individual or organization named on the face hereof and may be freely distributed in its present form.

**REPORT CERTIFICATION**

Technical Services, Inc. (TSI) has used its professional experience and best professional efforts in performing this compliance test. I have reviewed the results of these tests and to the best of my knowledge and belief they are true and correct.

**REPORT NO.**

0104A07

*Harvey C. Gray, Jr.*

HARVEY C. GRAY, JR.

DATE:

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## I. Introduction

Compliance testing for Chlorinated Haps emissions and Carbon Monoxide emissions from the Bleach Plant Scrubber, located at the Georgia Pacific Paper facility in Palatka, FL., was performed on May 25th, 2001. Three (3) test runs, each lasting one (1) hour, were completed on this source for both tests.

Testing and analytical procedures were in accordance with EPA's Methods ten (10), twenty-six (26A), and Florida DEP requirements.

We wish to express our appreciation to Mr. Joe Taylor and the operating staff at Georgia Pacific for their valuable assistance in the successful completion of this project.

## II. Summary and Discussion of Results

Results of the compliance tests are summarized in the following tables. Complete emissions data, along with supportive field and analytical data, are included in Appendices A, B, C, and G.

The Bleach Plant Scrubber was within compliance during the tests. The average emissions for Chlorinated Haps were 0.0089 lbs/hr, with an allowable emissions of 0.36 lbs/hr. The average emissions for Carbon Monoxide were 44.72 lbs/hr, with an allowable emissions of 46.0 lbs/hr.

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Volumetric Flow and Emission Output - Table I

FACILITY: Georgia Pacific  
 LOCATION: Palatka, FL  
 SOURCE: Bleach Plant Outlet

Date	Run Number	Chlorinated Haps Emissions			Vol. Flow Rate		Adjusted Volume SCFD	Percent H2O	Percent Isokinetic
		GR/SCF	LB/HR	ppm, vol.	ACFM	SCFMD			
5/25/01	1	0.00008	0.0098	0.13	15440.0	14275.0	35.391	4.6	96.4
5/25/01	2	0.00007	0.0083	0.11	15256.0	14178.0	36.388	5.1	99.8
5/25/01	3	0.00007	0.0084	0.11	15409.0	14413.0	36.716	5.4	99.0
<b>Mean</b>		0.00007	0.0089	0.12	15368.3	14288.7	36.165	5.0	98.4

Mean determined as arithmetic average of the results for each of the three runs.

REMARKS: MACT requires <10 ppm chlorinated HAPs

GEORGIA PACIFIC - PALATKA, FLORIDA BLEACH PLANT - SUMMARY OF CARBON MONOXIDE RESULTS - MAY 25 - 26, 2001

	START TIME	END TIME	STACK FLOW scfm d	CARBON MONOXIDE, ppm	CARBON MONOXIDE, lbs/hr
RUN 1	21:50	22:49	14183	670.4	41.5
RUN 2	23:02	0:01	14406	766.3	48.2
RUN 3A	0:12	2:13	14331	712.0	44.5
<b>TEST AVERAGE</b>			<b>14307</b>	<b>716.2</b>	<b>44.7</b>

*NOTE - DURING TEST RUN NUMBER THREE THE EOP MIXER TRIPPED. THE BLEACH PLANT PRODUCTION DECREASED AND THE TEST WAS SUSPENDED. ONCE NORMAL PRODUCTION RESUMED THE TEST RESTARTED.*

### III. Process Description And Operation

### III. Process Description and Operation

The bleaching process is an elemental chlorine-free (ECF) process. The  $\text{ClO}_2$  is produced on site.

The bleaching process consists of the staged introduction of  $\text{ClO}_2$  to the pulp slurry followed by washing of the bleached pulp. The off gases from all stages of the process are collected and passed through a wet scrubber utilizing an alkaline scrubbing solution.

**IV. Sampling Point Location**



**Air Report - Sampling Point Locations**

Facility Georgia Pacific  
 Location Palatka, FL  
 Source Name Bleach Plant Outlet

Stack Interior Diameter = 42.00 inches	
Sample Point Number	Inches Inside Stack Wall
1	1.85
2	6.13
3	12.43
4	29.57
5	35.87
6	40.15

Port Length 7 inches

**Distances From Nearest Disturbance**

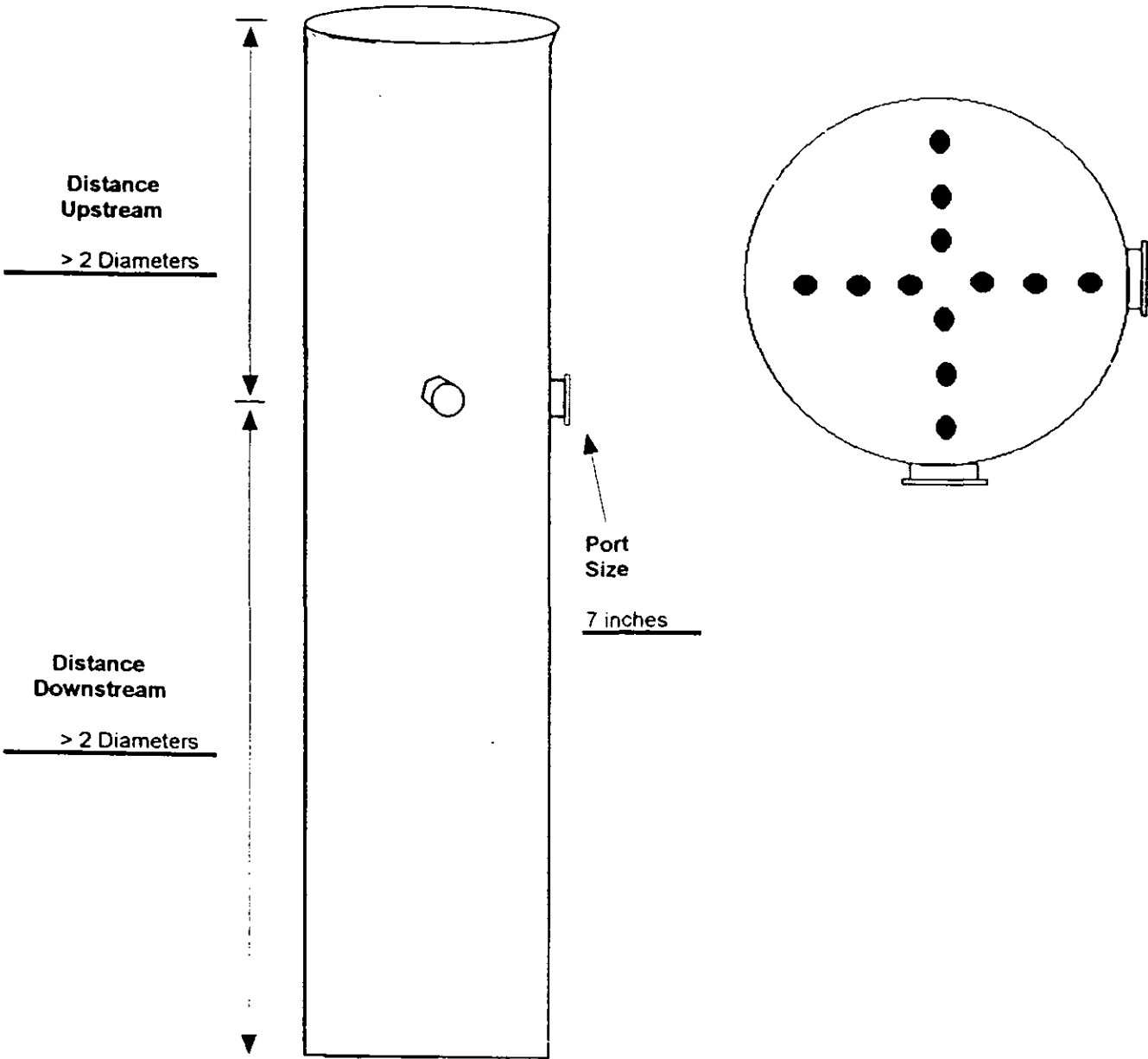
<u>Source</u>	<u>Stack Distance</u>
Downstream - - - - -	> 8 diameters
Upstream - - - - -	> 2 Diameters

The above mentioned Downstream and Upstream distances are approximate distances.

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# Air Report - Sampling Port Location Diagram

Facility	Georgia Pacific	Date	
Location	Palatka, FL		
Source	Bleach Plant Outlet		



**V. Field And Analytical Procedures**

## METHOD 10

### DETERMINATION OF CARBON MONOXIDE EMISSIONS FROM STATIONARY SOURCES

#### 1. Principle and Applicability

1.1 Principle. An integrated or continuous gas sample is extracted from a sampling point and analyzed for carbon monoxide (CO) content using a Luft-type nondispersive infrared analyzer (NDIR) or equivalent.

1.2 Applicability. This method is applicable for the determination of carbon monoxide emissions from stationary sources only when specified by the test procedures contained in this text or otherwise specified by the Director. The test procedure will indicate whether a continuous or an integrated sample is to be used.

#### 2. Range and Sensitivity

2.1 Range. 0 to 1,000 ppm.

2.2 Sensitivity. Minimum detectable concentration is 20 ppm for a 0 to 1,000 ppm span.

#### 3. Interferences

Any substance having a strong absorption of infrared energy will interfere to some extent. For example, discrimination ratios for water (H<sub>2</sub>O) and carbon dioxide (CO<sub>2</sub>) are 3.5 percent H<sub>2</sub>O per 7 ppm CO and 10 percent CO<sub>2</sub> per 10 ppm CO, respectively, for devices measuring in the 1,500 to 3,000 ppm range. For devices measuring in the 0 to 100 ppm range, interference ratios can be as high as 3.5 percent H<sub>2</sub>O per 25 ppm CO and 10 percent CO<sub>2</sub> per 50 ppm CO. The use of silica gel and ascarite traps will alleviate the major interference problems. The measured gas volume must be corrected if these traps are used.

#### 4. Precision and Accuracy

4.1 Precision. The precision of most NDIR analyzers is approximately  $\pm 2$  percent of span.

4.2 Accuracy. The accuracy of most NDIR analyzers is approximately  $\pm 5$  percent of span after calibration.

#### 5. Apparatus

5.1 Continuous sample (Figure 10-1).

5.1.1 Probe. Stainless steel or sheathed Pyrex glass, equipped with a filter to remove particulate matter.

5.1.2 Air-cooler condenser or equivalent. To remove any excess moisture.

5.2 Integrated sample (Figure 10.2).

5.2.1 Probe. Stainless steel or sheathed Pyrex glass, equipped with a filter to remove particulate matter.

5.2.2 Air-cooler condenser or equivalent. To remove any excess moisture.

5.2.3 Valve. Needle valve, or equivalent, to adjust flow rate.

5.2.4 Pump. Leak-free diaphragm type, or equivalent, to transport gas.

5.2.5 Rate meter. Rotameter, or equivalent, to measure a flow range from 0 to 1.0 liter per min. (0.035 cfm).

5.2.6 Flexible bag. Tedlar, or equivalent, with a capacity of 60 to 90 liters (2 to 3 ft<sup>3</sup>). Leak-test the bag in the laboratory before using by evacuating bag with a pump followed by a dry gas meter. When evacuation is complete, there should be no flow through the meter.

5.2.7 Pitot tube. Type S, or equivalent, attached to the probe so that the sampling rate can be regulated proportional to the stack gas velocity when velocity is varying with the time or a sample traverse is conducted.

5.3 Analysis (Figure 10-3).

5.3.1 Carbon monoxide analyzer. Nondispersive infrared spectrometer, or equivalent. This instrument should be demonstrated, preferably by the manufacturer, to meet or exceed manufacturer's specifications and those described in this method.

5.3.2 Drying tube. To contain approximately 200 g of silica gel.

5.3.3 Calibration gas. Refer to Section 6.1.

5.3.4 Filter. As recommended by NDIR manufacturer.

5.3.5 CO<sub>2</sub> removal tube. To contain approximately 500 g of ascarite.

5.3.6 Ice water bath. For ascarite and silica gel tubes.

5.3.7 Valve. Needle valve, or equivalent, to adjust flow rate.

5.3.8 Rate meter. Rotameter or equivalent to measure gas flow rate of 0 to 1.0 liter per minute (0.035 cfm) through NDIR.

5.3.9 Recorder (optional). To provide permanent record of NDIR readings.

## 6. Reagents

6.1 Calibration gases. Known concentration of CO in nitrogen (N<sub>2</sub>) for instrument span, prepurified grade of N<sub>2</sub> for zero, and two additional concentrations corresponding approximately to 60 percent and 30 percent span. The span concentration shall not exceed 1.5 times the applicable source performance standard. The calibration gases shall be certified by the manufacturer to be within  $\pm 2$  percent of the specified concentration.

6.2 Silica gel. Indicating type, 6 to 16 mesh, dried at 175°C (347°F) for 2 hours.

6.3 Ascarite. Commercially available.

## 7. Procedure

### 7.1 Sampling

7.1.1 Continuous sampling. Set up the equipment as shown in Figure 10-1 making sure all connections are leak free. Place the probe in the stack at a sampling point and purge the sampling line. Connect the analyzer and begin drawing sample into the analyzer. Allow 5 minutes for the system to stabilize, then record the analyzer reading as required by the test procedure. (See Sections 7.2 and 8). CO<sub>2</sub> content of the gas may be determined by using the Method 3 integrated sample procedure, or by weighing the ascarite CO<sub>2</sub> removal tube and computing CO<sub>2</sub> concentration from the gas volume sampled and the weight gain of the tube.

7.1.2 Integrated sampling. Evacuate the flexible bag. Set up the equipment as shown in Figure 10-2 with the bag

disconnected. Place the probe in the stack and purge the sampling line. Connect the bag, making sure that all connections are leak free. Sample at a rate proportional to the stack velocity. CO<sub>2</sub> content of the gas may be determined by using the Method 3 integrated sample procedures, or by weighing the ascarite CO<sub>2</sub> removal tube and computing CO<sub>2</sub> concentration from the gas volume sampled and the weight gain of the tube.

7.2 CO Analysis. Assemble the apparatus as shown in Figure 10-3, calibrate the instrument, and perform other required operations as described in Section 8. Purge analyzer with N<sub>2</sub> prior to introduction of each sample. Direct the sample stream through the instrument for the test period, recording the readings. Check the zero and span again after the test to assure that any drift or malfunction is detected. Record the sample data on Table 10-1.

### 8. Calibration

Assemble the apparatus according to Figure 10-3. Generally an instrument requires a warm-up period before stability is obtained. Follow the manufacturer's instructions for specific procedure. Allow a minimum time of 1 hour for warm-up. During this time check the sample conditioning apparatus, i.e., filter, condenser, drying tube, and CO<sub>2</sub> removal tube, to ensure that each component is in good operating condition. Zero and calibrate the instrument according to the manufacturer's procedures using, respectively, nitrogen and the calibration gases.

TABLE 10-1. FIELD DATA

Location.....	Comments:
Test.....	
Date.....	
Operator.....	
Clock Time	Rotameter setting, liters per minute (cubic feet per minute)

## 9. Calculation

Calculate the concentration of carbon monoxide in the stack using Equation 10-1.

$$C_{CO_{stack}} = C_{CO_{NDIR}} (1 - F_{CO_2})$$

where:

- $C_{CO_{stack}}$  = concentration of CO in stack, ppm by volume (dry basis).
- $C_{CO_{DNIR}}$  = concentration of CO measured by NDIR analyzer, ppm by volume (dry basis).
- $F_{CO_2}$  = volume fraction of CO<sub>2</sub> in sample, i.e., percent CO<sub>2</sub> from Orsat analysis divided by 100.

## 10. Alternative Procedure

10.1 Interference Trap. The sample condition system described in Method 10A, Sections 2.1.2 and 4.2 may be used as an alternate to the silica gel and ascarite traps.

## 11. Bibliography

1. McElroy, Frank, The Intertech NDIR-CO Analyzer, Presented at 11th Methods Conference on Air Pollution, University of California, Berkeley, Calif., April 1, 1970.
2. Jacobs, M.B., et al., Continuous Determination of Carbon Monoxide and Hydrocarbons in Air by a Modified Infrared Analyzer, J. Air Pollution Control Association, 9(2):110-114, August 1959.
3. MSA LIRA Infrared Gas and Liquid Analyzer Instruction Book, Mine Safety Appliances Co., Technical Products Division, Pittsburgh, Pa.
4. Models 215A, 315A, and 415A Infrared Analyzers, Beckman Instruments Inc., Beckman Instructions 1635-B, Fullerton, Calif., October 1967.
5. Continuous CO Monitoring System, Model A5611, Intertech Corp., Princeton, N.J.
6. UNOR Infrared Gas Analyzers, Bendix Corp., Ronceverte, West Virginia.



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ADDENDA

A. Performance Specifications for NDIR Carbon Monoxide Analyzers.

Range (minimum).....0-1000 ppm.  
Output (minimum).....0-10mV.  
Minimum detectable sensitivity.....20 ppm.  
Rise time, 90 percent (maximum).....30 seconds.  
Fall time, 90 percent (maximum).....30 seconds.  
Zero drift (maximum).....10% in 8 hours.  
Span drift (maximum).....10% in 8 hours.  
Precision (minimum).....+2% of full scale.  
Noise (maximum).....+1% of full scale.  
Linearity (maximum deviation).....2% of full scale.  
Interference rejection ration.....CO<sub>2</sub>--1000 to 1,H<sub>2</sub>O--500 to 1.

---

B. Definitions of Performance Specifications.

Range -- The minimum and maximum measurement limits.

Output -- Electrical signal which is proportional to the measurement; intended for connection to readout or data processing devices. Usually expressed as millivolts or milliamps full scale at a given impedance.

Full scale -- The maximum measuring limit for a given range.

Minimum detectable sensitivity -- The smallest amount of input concentration that can be detected as the concentration approaches zero.

Accuracy -- The degree of agreement between a measured value and the true value; usually expressed as  $\pm$  percent of full scale.

Time to 90 percent response -- The time interval from a step change in the input concentration at the instrument inlet to a reading of 90 percent of the ultimate recorded concentration.

Rise Time (90 percent) -- The interval between initial response time and time to 90 percent response after a step increase in the inlet concentration.

Fall Time (90 percent) -- The interval between initial response time and time to 90 percent response after a step decrease in the inlet concentration.

Zero Drift -- The change in instrument output over a stated time period, usually 24 hours, of unadjusted continuous operation when the input concentration is zero; usually expressed as percent full scale.

Span Drift -- The change in instrument output over a stated time period, usually 24 hours of unadjusted continuous operation when the input concentration is a stated upscale value; usually expressed as percent full scale.

Precision -- The degree of agreement between repeated measurements of the same concentration, expressed as the average deviation of the single results from the mean.

Noise -- Spontaneous deviations from a mean output not caused by input concentration changes.

Linearity -- The maximum deviation between an actual instrument reading and the reading predicted by a straight line drawn between upper and lower calibration points.

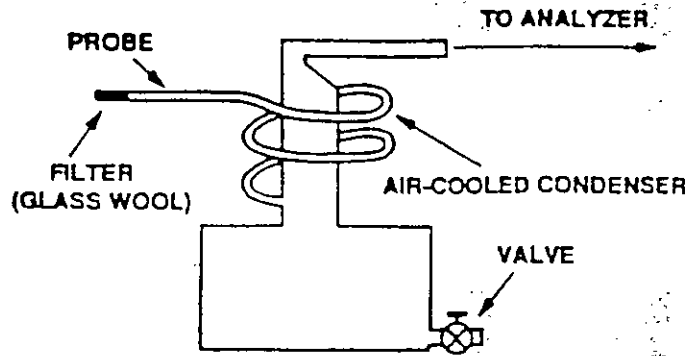


Figure 10-1. Continuous Sampling Train

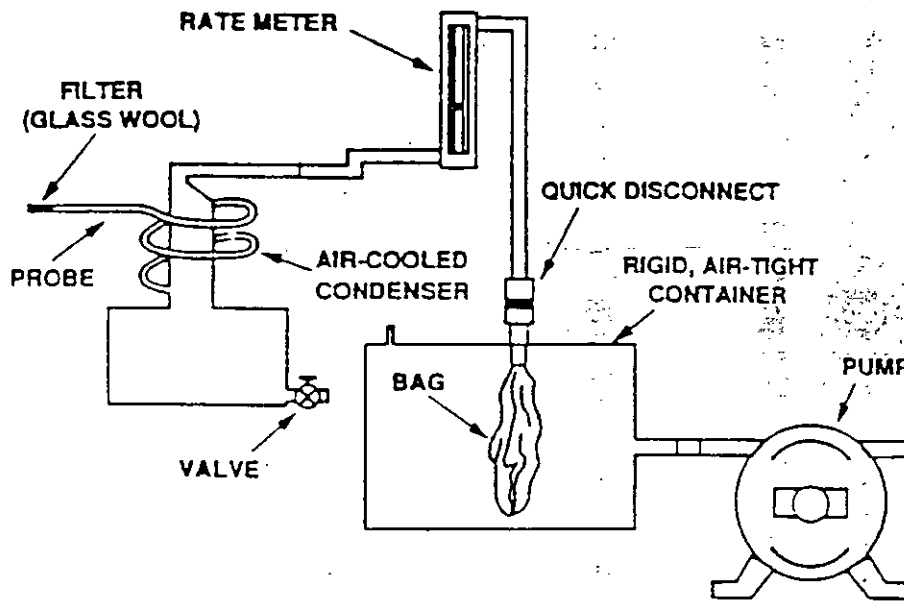


Figure 10-2. Integrated Gas-Sampling Train

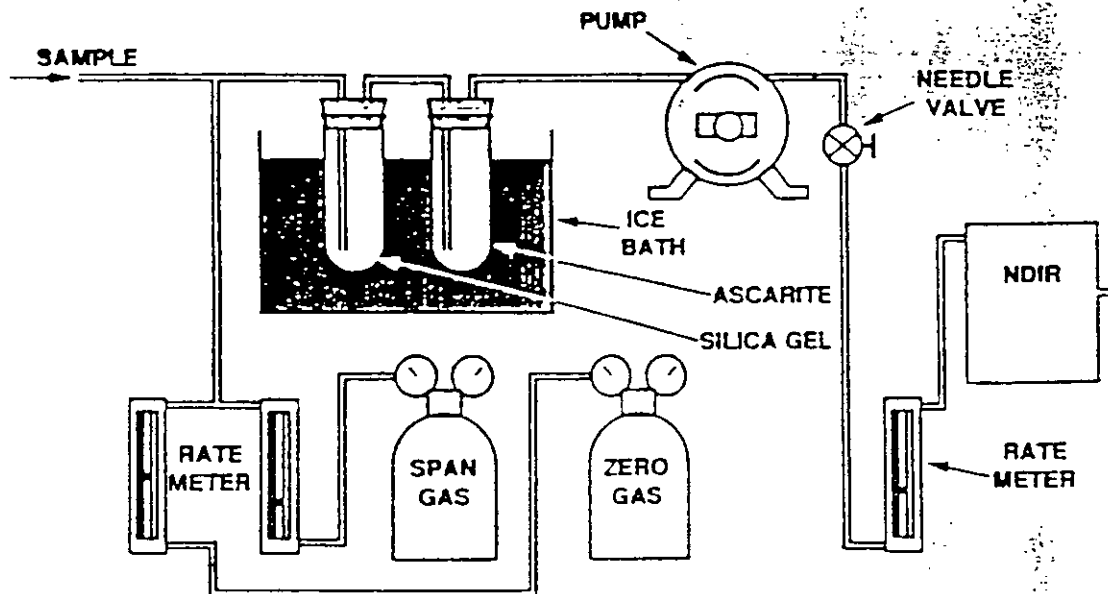


Figure 10-3. Analytical Equipment

METHOD 26A

DETERMINATION OF HYDROGEN HALIDE AND HALOGEN EMISSIONS  
FROM STATIONARY SOURCES - ISOKINETIC METHOD

1. Applicability, Principle, Interferences, Precision, Bias, and Stability

1.1 Applicability. This method is applicable for determining emissions of hydrogen halides (HX) [hydrogen chloride (HCL), hydrogen bromide (HBr), and hydrogen flouride (HF)] and halogens (X<sub>2</sub>) [chlorine (Cl<sub>2</sub>) and bromine (Br<sub>2</sub>)] from stationary sources. This method collects the emission sample isokinetically and is therefore particularly suited for sampling at sources, such as those controlled by wet scrubbers, emitting acid-particulate matter (e.g., hydrogen halides dissolved in water droplets). [NOTE: Mention of trade names or specific products does not constitute endorsement by the Environmental Protection Agency.]

1.2 Principle. Gaseous and particulate pollutants are withdrawn isokinetically from the source and collected in an optional cyclone, on a filter, and in absorbing solutions. The cyclone collects any liquid droplets and is not necessary if the source emissions do not contain them; however, it is preferable to include the cyclone in the sampling train to protect the filter from any moisture present. The filter collects other particulate matter including halide salts. Acidic and alkaline absorbing solutions collect the gaseous hydrogen halides and halogens, respectively. Following sampling of emissions containing liquid droplets, any halides/halogens dissolved in the liquid in the cyclone and on the filter are vaporized to gas and corrected in the impingers by pulling conditioned ambient air through the sampling train. The hydrogen halides are solubilized in the acidic solution and form chloride (Cl<sup>-</sup>), bromide (Br<sup>-</sup>), and fluoride (F<sup>-</sup>) ions. The halogens have a very low solubility in the acidic solution and pass through to the alkaline solution where they are hydrolyzed to form a proton (H<sup>+</sup>), the halide ion, and the hypohalous acid (HClO or HBrO). Sodium thiosulfate is added to the alkaline solution to assure reaction with the hypohalous acid to form a second halide ion, such that 2 halide ions are formed for each molecule of halogen gas. The halide ions in the separate solutions are measured by ion chromatography (IC). If desired, the particulate matter recovered from the filter and the probe is analyzed following the procedures in Method 5. [NOTE: If the tester intends to use this sampling arrangement to sample concurrently for particulate

matter, the alternative Teflon<sup>R</sup> probe liner, cyclone, and filter holder should not be used. The Teflon<sup>R</sup> filter support must be used. The tester must also meet the probe and filter temperature requirements of both sampling trains.]

1.3 Interferences. Volatile materials, such as chlorine dioxide ( $\text{ClO}_2$ ) and ammonium chloride ( $\text{NH}_4\text{Cl}$ ), which produce halide ions upon dissolution during sampling are potential interferents. Interferents for the halide measurements are the halogen gases which disproportionate to a hydrogen halide and an hypohalous acid upon dissolution in water. The use of acidic rather than neutral or basic solutions for collection of the hydrogen halides greatly reduces the dissolution of any halogens passing through this solution. The simultaneous presence of both HBr and  $\text{Cl}_2$  may cause a positive bias in the HCl result with a corresponding negative bias in the  $\text{Cl}_2$  result as well as affecting the HBr/ $\text{Br}_2$  split. High concentrations of nitrogen oxides ( $\text{NO}_x$ ) may produce sufficient nitrate ( $\text{NO}_3$ ) to interfere with measurements of very low Br levels.

1.4 Precision and Bias. The method has a possible measurable negative bias below 20 ppm HCl perhaps due to reaction with small amounts of moisture in the probe and filter. Similiar bias for the other hydrogen halides is possible.

1.5 Sample Stability. The collected  $\text{Cl}^-$  samples can be stored for up to 4 weeks for analysis for HCl and  $\text{Cl}_2$ .

1.6 Detection Limit. The in-stack detection limit for HCl is approximately 0.02 ug per liter of stack gas; the analytical detection limit for HCl is 0.1 ug/ml. Detection limits for the other analyses should be similiar.

## 2. Apparatus

2.1 Sampling. The sampling train is shown in Figure 26A-1; the apparatus is similiar to the Method 5 train where noted as follows:

2.1.1 Probe Nozzle. Borosilicate or quartz glass; constructed and calibrated according to Method 5, Sections 2.1.1 and 5.1, and coupled to the probe liner using a Teflon<sup>R</sup> union; a stainless steel nut is recommended for this union. When the stack temperature exceeds  $210^\circ\text{C}$  ( $410^\circ\text{F}$ ), a one-piece glass nozzle/liner assembly must be used.

2.1.2 Probe Liner. Same as Method 5, Section 2.1.2, except metal liners shall not used. Water-cooling of the stainless steel sheath is recommended at temperatures exceeding  $500^\circ\text{C}$ . Teflon<sup>R</sup> may be used in limited applications where the minimum

stack temperature exceeds 120°C (250°F) but never exceeds the temperature where Teflon<sup>R</sup> is estimated to become unstable (approximately 210°C).

2.1.3 Pitot Tube, Differential Pressure Gauge, Filter Heating System, Metering System, Barometer, Gas Density Determination Equipment. Same as Method 5, Sections 2.1.3, 2.1.4, 2.1.6, 2.1.8, 2.1.9, and 2.1.10.

2.1.4 Cyclone (Optional). Glass or Teflon<sup>R</sup>. Use of the cyclone is required only when the sample gas stream is saturated with moisture; however, the cyclone is recommended to protect the filter from any moisture droplets present.

2.1.5 Filter Holder. Borosilicate or quartz glass, or Teflon<sup>R</sup> filter holder, with a Teflon<sup>R</sup> filter support and a sealing gasket. The sealing gasket shall be constructed of Teflon<sup>R</sup> or equivalent materials. The holder design shall provide a positive seal against leakage at any point along the filter circumference. The holder shall be attached immediately to the outlet of the cyclone.

2.1.6 Impinger Train. The following system shall be used to determine the stack gas moisture content and to collect the hydrogen halides and halogens: five or six impingers connected in a series with leak-free ground glass fittings or any similar leak-free noncontaminating fittings. The first impinger shown in Figure 26A-1 (knockout or condensate impinger) is optional and is recommended as a water knockout trap for use under high moisture conditions. If used, this impinger should be constructed as described below for the alkaline impingers, but with a shortened stem, and should contain 50 ml of 0.1 N H<sub>2</sub>SO<sub>4</sub>. The following two impingers (acid impingers which each contain 100 ml of 0.1 H<sub>2</sub>SO<sub>4</sub>) shall be of the Greenburg-Smith design with the standard tip (Method 5, Section 2.1.7). The next two impingers (alkaline impingers which each contain 100 ml of 0.1 N NaOH) and the last impinger (containing silica gel) shall be of the modified Greenburg-Smith design (Method 5, Section 2.1.7). The condensate, acid, and alkaline impingers shall contain known quantities of the appropriate absorbing reagents. The last impinger shall contain a known weight of silica gel or equivalent desiccant. Teflon<sup>R</sup> impingers are an acceptable alternative.

2.1.7 Ambient Air Conditioning Tube (Optional). Tube tightly packed with approximately 150 g of fresh 8 to 20 mesh sodium hydroxide-coated silica, or equivalent, (AscariteII<sup>R</sup> has been found suitable) to dry and remove acid gases from the ambient air used to remove moisture from the filter and cyclone, when the cyclone is used. The inlet and outlet ends of the tube should be packed with at least 1-cm thickness of glass wool or

filter material suitable to prevent escape of fines. Fit one end with flexible tubing, etc. to allow connection to probe nozzle following the test run.

2.2 Sample Recovery. The following items are needed:

2.2.1 Probe-Liner and Probe-Nozzle Brushes, Wash Bottles, Glass Sample Storage Containers, Petri Dishes, Graduated Cylinder or Balance, and Rubber Policeman. Same as Method 5, Sections 2.2.1, 2.2.2, 2.2.3, 2.2.4, 2.2.5, and 2.2.7.

2.2.2 Plastic Storage Containers. Screw-cap polypropylene containers to store silica gel. High-density polyethylene bottles with Teflon screw cap liners to store impinger reagents, 1-liter.

2.2.3 Funnels. Glass or high-density polyethylene, to aid in sample recovery.

2.3 Analysis. For analysis, the following equipment is needed:

2.3.1 Volumetric Flasks. Class A, various sizes.

2.3.2 Volumetric Pipettes. Class A, assortment, to dilute samples to calibration range of the ion chromatograph (IC).

2.3.3 Ion Chromatograph. Suppressed or nonsuppressed, with a conductivity detector and electronic integrator operating in the peak area mode. Other detectors, a strip chart recorder, and peak heights may be used.

3. Reagents

Unless otherwise indicated, all reagents must conform to the specifications of the Committee on Analytical Reagents of the American Chemical Society (ACS reagent grade). When such specifications are not available, the best available grade shall be used.

3.1 Sampling.

3.1.1 Water. Deionized, distilled water that conforms to American Society of Testing and Materials (ASTM) Specification D 1193-77, Type 3.

3.1.2 Acidic Absorbing Solution, 0.1 N Sulfuric Acid ( $H_2SO_4$ ). To prepare 1 L, slowly add 2.80 ml of concentrated  $H_2SO_4$  to about 900 ml of water while stirring, and adjust the

final volume to 1 L using additional water. Shake well to mix the solution.

3.1.3 Alkaline Absorbing Solution, 0.1 N Sodium Hydroxide (NaOH). To prepare 1 L, dissolve 4.00 g of solid NaOH in about 900 ml of water and adjust the final volume to 1 L using additional water. Shake well to mix the solution.

3.1.4 Filter. Teflon mat (e.g., Pallflex<sup>R</sup> TX40H145) filter. When the stack gas temperature exceeds 210°C (410°F) a quartz fiber filter may be used.

3.1.5 Silica Gel, Crushed Ice, and Stopcock Grease. Same as Method 5, Sections 3.1.2, 3.1.4, and 3.1.5, respectively.

3.1.6 Sodium Thiosulfate, (Na<sub>2</sub>S<sub>2</sub>O<sub>3</sub> · 5 H<sub>2</sub>O).

3.2 Sample Recovery.

3.2.1 Water. Same as Section 3.1.1.

3.2.2 Acetone. Same as Method 5, Section 3.2.

3.3 Sample Analysis.

3.3.1 Water. Same as Section 3.1.1.

3.3.2 Reagent Blanks. A separate blank solution of each absorbing reagent should be prepared for analysis with the field samples. Dilute 200 ml of each absorbing solution (250 ml of the acidic absorbing solution, if a condensate impinger is used) to the same final volume as the field samples using the blank sample of rinse water. If a particulate determination is conducted, collect a blank sample of acetone.

3.3.3 Halide Salt Stock Standard Solutions. Prepare concentrated stock solutions from reagent grade sodium chloride (NaCl), sodium bromide (NaBr), and sodium fluoride (NaF). Each must be dried at 110°C for 2 or more hours and then cooled to room temperature in a desiccator immediately before weighing. Accurately weigh 1.6 to 1.7 g of the dried NaCl to within 0.1 mg, dissolve in water, and dilute to 1 liter. Calculate the exact Cl concentration using Equation 26A-1.

$$\text{uCl}^-/\text{ml} = \text{g of NaCl} \times 10^3 \times 35.453/58.44 \quad (\text{Equation 26A-1})$$

In a similar manner, accurately weigh and solubilize 1.2 to 1.3 g of dried NaBr and 2.2 to 2.3 g of NaF to make 1 liter solutions.



Use Equations 26A-2 and 26A-3 to calculate the  $\text{Br}^-$  and  $\text{F}^-$  concentrations.

$$\text{ugBr}^-/\text{ml} = \text{g of NaBr} \times 10^3 \times 79.904/102.90 \quad (\text{Equation 26A-2})$$

$$\text{ugF}^-/\text{ml} = \text{g of NaF} \times 10^3 \times 18.998/41.99 \quad (\text{Equation 26A-3})$$

Alternately, solutions containing a nominal certified concentration of 1000 mg/L NaCl are commercially available as convenient stock solutions from which standards can be made by appropriate volumetric dilution. Refrigerate the stock standard solutions and store no longer than 1 month.

3.3.4 Chromatographic Eluent. Same as Method 26, Section 3.2.4.

#### 4. Procedure

Because of the complexity of this method, testers and analysts should be trained and experienced with the procedures to ensure reliable results.

##### 4.1 Sampling.

4.1.1 Pretest Preparation. Follow the general procedure given in Method 5, Section 4.1.1, except the filter need only be desiccated and weighed if a particulate determination will be conducted.

4.1.2 Preliminary Determinations. Same as Method 5, Section 4.1.2.

4.1.3 Preparation of Sampling Train. Follow the general procedure given in Method 5, Section 4.1.3, except for the following variations:

And 50 ml of 0.1 N  $\text{H}_2\text{SO}_4$  to the condensate impinger, if used. Place 100 ml of 0.1 N  $\text{H}_2\text{SO}_4$  in each of the next two impingers. Finally, transfer approximately 200-300 g of preweighed silica gel from its container to the last impinger. Set up the train as in Figure 26A-1. When used, the optional cyclone is inserted between the probe liner and filter holder and located in the heated filter box.

4.1.4 Leak-Check Procedures. Follow the leak-check procedures given in Method 5, Sections 4.4.1 (Pretest Leak-Check), 4.1.4.2 (Leak-Checks During the Sample Run), and 4.1.4.3 (Post-Test Leak-Check).

4.1.5 Train Operation. Follow the general procedure given in Method 5, Section 4.1.5. Maintain a temperature around the filter and (cyclone, if used) of greater than 120°C (248°F). For each run, record the data required on a data sheet such as the one shown in Method 5, Figure 5-2. If the condensate impinger becomes too full, it may be emptied, recharged with 50 ml of 0.1 N H<sub>2</sub>SO<sub>4</sub>, and replaced during the sample run. The condensate emptied must be saved and included in the measurement of the volume of moisture collected and included in the sample for analysis. The additional 50 ml of absorbing reagent must also be considered in calculating the moisture. After the impinger is reinstalled in the train, conduct a leak-check as described in Method 5, Section 4.1.4.2.

4.1.6 Post-Test Moisture Removal (Optional). When the optional cyclone is included in the sampling train or when moisture is visible on the filter at the end of a sample run even in the absence of a cyclone, perform the following procedure. Upon completion of the test run, connect the ambient air conditioning tube at the probe inlet and operate the train with the filter heating system at least 120°C (248°F) at a low flow rate (e.g., ΔH = 1 in. H<sub>2</sub>O) to vaporize any liquid and hydrogen halides in the cyclone or on the filter and pull them through the train into the impingers. After 30 minutes, turn off the flow, remove the conditioning tube, and examine the cyclone and filter for any visible moisture. If moisture is visible, repeat this step for 15 minutes and observe again. Keep repeating until the cyclone is dry. [NOTE: It is critical that this is repeated until the cyclone is completely dry.]

4.2 Sample Recovery. Allow the probe to cool. When the probe can be handled safely, wipe off all the external surfaces of the tip of the probe nozzle and place a cap loosely over the tip. Do not cap the probe tip tightly while the sampling train is cooling down because this will create a vacuum in the filter holder, drawing water from the impingers into the holder. Before moving the sampling train to the cleanup site, remove the probe, wipe off any silicone grease, and cap the open outlet of the impinger train, being careful not to lose any condensate that might be present. Wipe off any silicone grease and cap the filter or cyclone inlet. Remove the umbilical cord from the last impinger and cap the impinger. If a flexible line is used between the first impinger and the filter holder, disconnect it at the filter holder and let any condensed water drain into the first impinger. Wipe off any silicone grease and cap the filter holder outlet and the impinger inlet. Ground glass stoppers, plastic caps, serum caps, Teflon tape, Parafilm, or aluminum foil may be used to close these openings. Transfer the probe and filter/impinger assembly to the cleanup area. This area should be clean and protected from the weather to minimize sample

contamination or loss. Inspect the train prior to and during disassembly and note any abnormal conditions. Treat samples as follows:

4.2.1 Container No. 1 (Optional; Filter Catch for Particulate Determination). Same as Method 5, Section 4.2, Container No. 1.

4.2.2 Container No. 2 (Optional; Front-Half Rinse for Particulate Determination). Same as Method 5, Section 4.2, Container No. 2.

4.2.3 Container No. 3 (Knockout and Acid Impinger Catch for Moisture and Hydrogen Halide Determination). Disconnect the impingers. Measure the liquid in the acid and knockout impingers to  $\pm 1$  ml by using a graduated cylinder or by weighing it to  $\pm 0.5$  g by using a balance. Record the volume or weight of liquid present. This information is required to calculate the moisture content of the effluent gas. Quantitatively transfer this liquid to a leak-free sample storage container. Rinse these impingers and connecting glassware including the back portion of the filter holder (and flexible tubing, if used) with water and add these rinses to the storage container. Seal the container, shake to mix, and label. The fluid level should be marked so that if any sample is lost during transport, a correction proportional to the lost volume can be applied. Retain rinse water and acidic absorbing solution blanks and analyze with the samples.

4.2.4 Container No. 4 (Alkaline Impinger Catch for Halogen and Moisture Determination). Measure and record the liquid in the alkaline impingers as described in Section 4.2.3. Quantitatively transfer this liquid to a leak-free sample storage container. Rinse these two impingers and connecting glassware with water and add these rinses to the container. Add 25 mg of sodium thiosulfate per ppm halogen-dscm of stack gas sample. [NOTE: This amount of sodium thiosulfate includes a safety factor of approximately 5 to assure complete reaction with the hypohalous acid to form a second  $\text{Cl}^-$  ion in the alkaline solution.] Seal the container, shake to mix, and label; mark the fluid level. Retain alkaline absorbing solution blank and analyze with the samples.

4.2.5 Container No. 5 (Silica Gel for Moisture Determination). Same as Method 5, Section 4.2, Container No. 3.

4.2.6 Container Nos. 6 through 9 (Reagent Blanks). Save portions of the absorbing reagents (0.1 N  $\text{H}_2\text{SO}_4$  and 0.1 N NaOH) equivalent to the amount used in the sampling train; dilute to the approximate volume of the corresponding samples using rinse water directly from the wash bottle being used. Add the same

ratio of sodium thiosulfate solution used in container No. 4 to the 0.1 N NaOH absorbing reagent blank. Also, save a portion of the rinse water alone and a portion of the acetone equivalent to the amount used to rinse the front half of the sampling train. Place each in a separate, prelabeled sample container.

4.2.7 Prior to shipment, recheck all sample containers to ensure that the caps are well-secured. Seal the lids of all containers around the circumference with Teflon tape. Ship all liquid samples upright and all particulate filters with the particulate catch facing upward.

4.3 Sample Preparation and Analysis. Note the liquid levels in the sample containers and confirm on the analysis sheet whether or not leakage occurred during transport. If a noticeable leakage has occurred, either void the sample or use methods, subject to the approval of the Administrator, to correct the final results.

4.3.1 Container Nos. 1 and 2 and Acetone Blank (Optional; Particulate Determination). Same as Method 5, Section 4.3.

4.3.2. Container No. 5. Same as Method 5, Section 4.3 for Silica gel.

4.3.3 Container Nos. 3 and 4 and Absorbing Solution and Water Blanks. Quantitatively transfer each sample to a volumetric flask or graduated cylinder and dilute with water to a final volume within 50 ml of the largest sample.

4.3.3.1 The IC conditions will depend upon analytical column type and whether suppressed or nonsuppressed IC is used. Prior to calibration and sample analysis, establish a stable baseline. Next, inject a sample of water, and determine if any  $\text{Cl}^-$ ,  $\text{Br}^-$ , or  $\text{F}^-$  appears in the chromatogram. If any of these ions are present, repeat the load/injection procedure until they are no longer present. Analysis of the acid and alkaline absorbing solution samples requires separate standard calibration curves; prepare each according to Section 5.2. Ensure adequate baseline separation of the analyses.

4.3.3.2 Between injections of the appropriate series of calibration standards, inject in duplicate the reagent blanks and the field samples. Measure the areas or heights of the  $\text{Cl}^-$ ,  $\text{Br}^-$ , and  $\text{F}^-$  peaks. Use the average response to determine the concentrations of the field samples and reagent blanks using the linear calibration curve. If the values from duplicate injections are not within 5 percent of their mean, the duplicate injection shall be repeated and all four values used to determine the average response. Dilute any sample and the blank

with equal volumes of water if the concentration exceeds that of the highest standard.

4.4 Audit Sample Analysis. Audit samples must be analyzed subject to availability.

## 5. Calibration

Maintain a laboratory log of all calibrations.

5.1 Probe Nozzle, Pitot Tube, Dry Gas Metering System, Probe Heater, Temperature Gauges, Leak-Check of Metering System, and Barometer. Same as Method 5, Sections 5.1, 5.2, 5.3, 5.4, 5.5, 5.6, and 5.7, respectively.

5.2 Ion Chromatograph. To prepare the calibration standards, dilute given amounts (1.0 ml or greater) of the stock standard solutions to convenient volumes, using 0.1 N  $H_2SO_4$  or 0.1 N NaOH, as appropriate. Prepare at least four calibration standards for each absorbing reagent containing the three stock solutions such that they are within the linear range of the field samples. Using one to the standards in each series, ensure adequate baseline separation for the peaks of interest. Inject the appropriate series of calibration standards, starting with the lowest concentration standard first both before and after injection of the quality control check sample, reagent blanks, and field samples. This allows compensation for any instrument drift occurring during sample analysis. Determine the peak areas, or height, of the standards and plot individual values versus halide ion concentrations in ug/ml. Draw a smooth curve through the points. Use linear regression to calculate a formula describing the resulting linear curve.

## 6. Quality Control

Same as Method 5, Section 4.4.

## 7. Quality Assurance

7.1 Applicability. When the method is used to demonstrate compliance with a regulation, a set of two audit samples shall be analyzed.

7.2 Audit Procedure. The currently available audit samples are chloride solutions. Concurrently analyze the two audit samples and a set of compliance samples in the same manner to evaluate the technique of the analyst and the standards preparation. The same analyst, analytical reagents, and analytical system shall be used both for compliance samples and the Environmental Protection Agency (EPA) audit samples.

7.3 Audit Sample Availability. Audit samples will be supplied only to enforcement agencies for compliance tests. Audit samples may be obtained by writing the Source Test Audit Coordinator (MD-77B), Quality Assurance Division, Atmospheric Research and Exposure Assessment Laboratory, U.S. Environmental Protection Laboratory, Research Triangle Park, NC 27711 or by calling the Source Test Audit Coordinator (STAC) at (919) 541-7834. The request for the audit samples should be made at least 30 days prior to the scheduled compliance sample analysis.

7.4 Audit Results. Calculate the concentrations in mg/dscm using the specified sample volume in the audit instructions. Include the results of both audit samples, their identification numbers, and the analyst's name with the results of the compliance determination samples in appropriate reports to the EPA regional office or the appropriate enforcement agency.

(NOTE: Acceptability of results may be obtained immediately by reporting the audit results in mg/dscm and compliance results in total ug HCl/sample to the responsible enforcement agency.) The concentrations of the audit samples obtained by the analyst shall be agree within 10 percent of the actual concentrations. If the 10 percent specification is not met, reanalyze the compliance samples and audit samples, and include intitial and reanalysis values in the test report. Failure to meet the 10 percent specification may require retests until the audit problems are resolved.

## 8. Calculations

Retain at least one extra decimal figure beyond those contained in the available data in intermediate calculations, and round off only the final answer appropriately.

8.1 Nomenclature. Same as Method 5, Section 6.1. In Addition:

$B_x$  = Mass concentration of applicable absorbing solution blank, ug halide ion ( $Cl^-$ ,  $Br^-$ ,  $F^-$ )/ml, not exceed 1 ug/ml which is 10 times the published analytical detection limit of 0.1 ug/ml. (It is also approximately 5 percent of the mass concentration anticipated to result from a one hour sample at 10 ppmv HCl.)

C = Concentration of hydrogen halide (HX) or halogen ( $X_2$ ), dry basis, mg/dscm.

$m_{HX}$  = Mass of HCl, HBr, or HF in sample, ug.

$m_{X_2}$  = Mass of  $Cl_2$  or  $Br_2$  in sample, ug.

$S_x^-$  = Analysis of sample, ug halide ion ( $Cl^-$ ,  $Br^-$ ,  $F^-$ )/ml.

$V_S$  = Volume of filtered and diluted sample, ml.

8.2 Average Dry Gas Meter Temperature and Average Orifice Pressure Drop. See data sheet (Figure 5-2 of Method 5).

8.3 Dry Gas Volume. Calculate  $V_m(\text{std})$  and adjust for leakage, if necessary, using the equation in Section 6.3 of Method 5.

8.4 Volume of Water Vapor and Moisture Content. Calculate the volume of water vapor  $V_w(\text{std})$  and moisture content  $B_{ws}$  from the data obtained in this method (Figure 5-2 of Method 5); use Equations 5-2 and 5-3 of Method 5.

8.5 Isokinetic Variation and Acceptable Results. Use Method 5, Sections 6.11 and 6.12.

8.6 Actone Blank Concentration, Acetone Wash Blank Residue Weight, Particulate Weight, and Particulate Concentration. For particulate determination.

8.7 Total ug HCl, HBr, or HF Per Sample.

$$m_{HX} = K V_S (S_{X-} - B_{X-}) \quad (\text{Equation 26A-4})$$

where:

$$K_{HCl} = 1.028 \text{ (ug HCl/ug-mole) / (ug Cl}^- \text{/ug-mole)}.$$

$$K_{HBr} = 1.013 \text{ (ug HBr/ug-mole) / (ug Br}^- \text{/ug-mole)}.$$

$$K_{HF} = 1.053 \text{ (ug HF/ug-mole) / (ug F}^- \text{/ug-mole)}.$$

8.8 Total ug  $Cl_2$  or  $Br_2$  Per Sample.

$$m_{X2} = V_S (S_{X-} - B_{X-}) \quad (\text{Equation 26A-5})$$

8.9 Concentration of Hydrogen Halide or Halogen in Flue Gas.

$$C = K m_{HX, X2} / V_m(\text{std}) \quad (\text{Equation 26A-6})$$

where:

$$K = 10^{-3} \text{ mg/ug}$$

8.10 Stack Gas Velocity and Volumetric Flow Rate. Calculate the average stack gas velocity and volumetric flow

rate, if needed, in using data obtained in this method and the equations in Sections 5.2 and 5.3 of Method 2.

## 9. Bibliography

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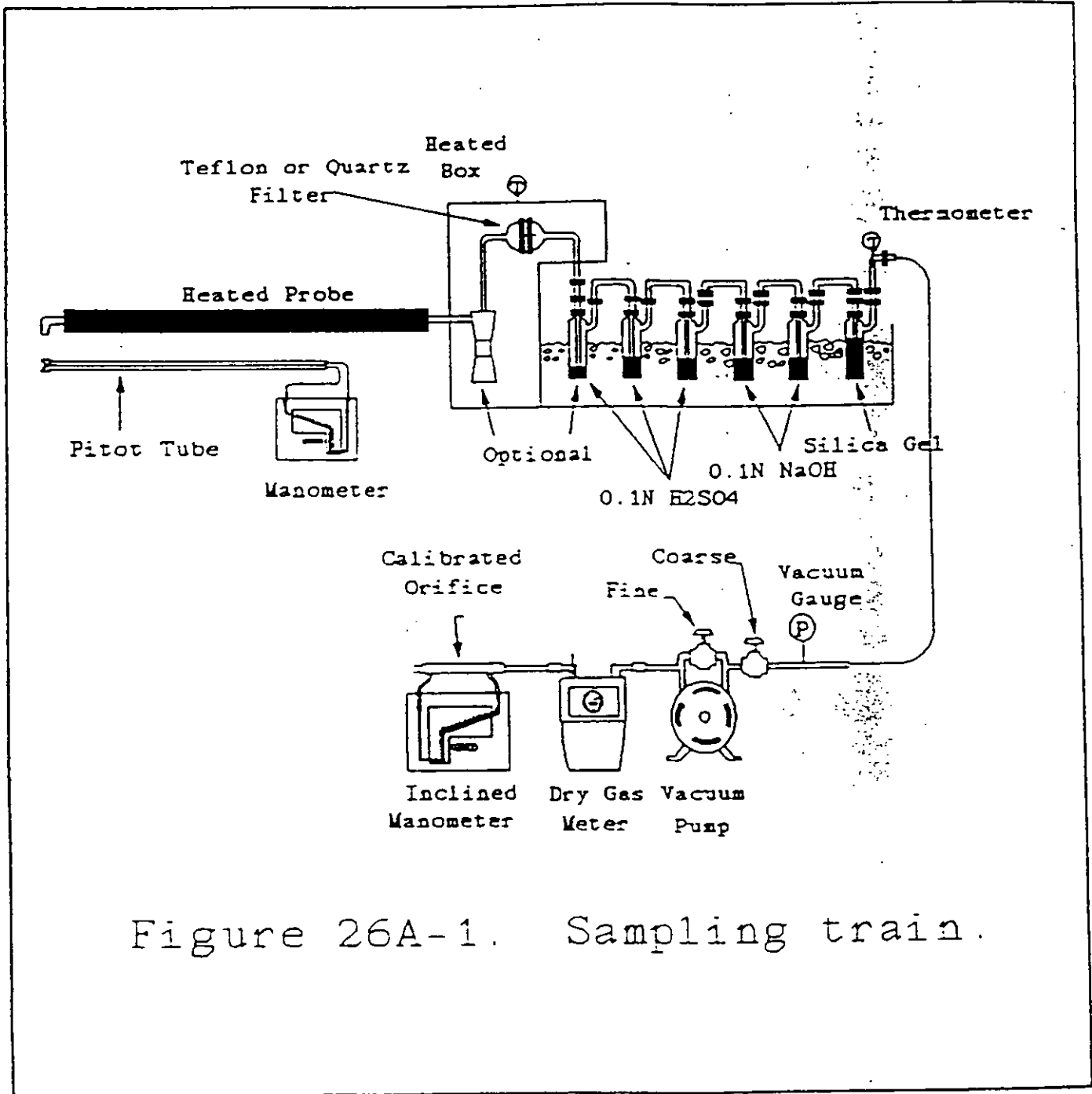


Figure 26A-1. Sampling train.

**APPENDIX A**  
**COMPLETE EMISSION DATA**

## Source Sampling Nomenclature Sheet

- PB - Barometric pressure, inches Hg.
- PS - Stack pressure, inches Hg.
- AS - Effective area of positive stack gas flow, sq. ft.
- As - stack area, sq. ft.
- NPTS - Number of traverse point where the pitot velocity head was greater than zero
- TS - Stack temperature, degrees fahrenheit
- TM - Meter temperature, degrees fahrenheit
- ASQH - Average square root of velocity head, inches H<sub>2</sub>O
- DH - Average meter orifice pressure differential, inches H<sub>2</sub>O
- AN - Sampling nozzle area, square feet
- CP - S-type pitot tube correction factor
- VM - Recorded meter volume sample, cubic feet (meter conditions)
- VC - Condensate and silica gel increase in impingers, milliliters
- PO - Pressure at the dry test meter orifice,  $PB + \frac{H}{13.6}$
- t - Test time in minutes
- VSTPD - Standard conditions, dry, 68 degrees fahrenheit (Tstd), 29.92 inches Hg (Pstd)
- Y - Average ratio of accuracy of wet test meter to dry gas meter, with a tolerance of plus or minus 0.02

- 
- VWV - Conversion of condensate in milliliters to water vapor in cubic feet (STP)
  - VSTPD - Volume sampled, cubic feet (STP)
  - VT - Total water vapor and dry gas volume sampled, cubic feet (STP)
  - W - Moisture fraction of stack gas
  - FDA - Dry gas fraction
  - MD - Molecular weight of stack gas, lbs/lb-mole (dry conditions)
  - MS - Molecular weight of stack gas, lbs/lb-mole (stack conditions)
  - GS - Specific gravity of stack gas, referred to air
  - EA - Excess air
  - U - Stack gas velocity, feet per minute
  - QS - Stack gas flow rate, cubic feet per minute (stack conditions)
  - QD - Stack gas flow rate, cubic feet per minute (dry conditions)
  - QSTPD - Stack gas flow rate, cubic feet per minute (STP)
  - PISO - Percent isokinetic volume sampled (method described in Federal Register)
  - ESTP - Particulate concentration at standard and dry conditions, grains/scf
  - E12 - ESTP corrected to 12 % CO<sub>2</sub>, grains/scf
  - E50 - ESTP corrected to 50 % excess air, grains/scf
  - EM - Mass emissions rate, lbs/hr
  - Eh - Mass emissions rate, lbs mmbTUs
  - E - ESTP corrected to % Excess Air.

## Equations For Calculating Particulate Emissions

$$VWV = (0.04707) \times (VC)$$

$$VSTPD = (17.65) \times (VM) \times \left( \frac{PB + DH}{13.6} \right) + (TM) \times (Y)$$

$$VT = (VWV) \times (VSTPD)$$

$$W = (VWV) + (VT)$$

$$FDA = (1.0) - (W)$$

$$MD = (0.44 \times \% CO_2) + (0.32 \times \% O_2) + (0.28 \times \% N_2) + (0.28 \times \% CO)$$

$$MS = (MD \times FDA) + (18 \times W)$$

$$CS = (MS) + (28.99)$$

$$EA = \left[ (100) \times \left( \% O_2 - \frac{\% CO}{2} \right) \right] / \left[ (0.266 \times \% N_2) - \left( O_2 - \frac{\% CO}{2} \right) \right]$$

$$U = (174) \times (CP) \times (ASQH) \times \sqrt{(TS \times 29.92) + (CS \times PS)}$$

$$QS = (U) \times (AS)$$

$$QD = (QS) \times (FDA)$$

$$QSTPD = (528) \times (QD) \times (PS) + (TS \times 29.9)$$

$$PISO = \frac{(100) \times T_s \times VSTPD \times P_{std}}{T_{std} \times U \times (t) \times A_n \times P_s \times (FDA)}$$

$$ESTP = \frac{(\text{SAMPLE WT. in mg.}) \times (0.01543)}{VSTPD}$$

$$E_{12} = \frac{(ESTP) \times (12)}{(\% CO_2)}$$

$$E_{50} = \frac{(ESTP) \times (100 + EA)}{150}$$

$$EM = \frac{(ESTP) \times (QSTPD) (60 \text{ min})}{7000}$$

$$E_h = \frac{(ESTP) \times \text{FUEL FACTOR} \times 20.9}{7000 (20.9 - \% O_2)}$$

$$E_{EA} = \frac{(ESTP) \times (100 + EA)}{\text{Desired EA}}$$

Facility: Georgia Pacific

Test Date: 5/25/01

Source: Bleach Plant Outlet

Run Number: 1

Example Calculations:

Page 1

1. Stack Pressure, (PS)

$$PS = PB + (PG / 13.6)$$

Example. PB =	30.09	Therefore PS =	<u>30.10</u>	in. Hg.
PG =	0.07			

2. Meter Pressure, (PM)

$$PM = (PB) + (*H / 13.6)$$

Example. *H =	1.508	Therefore PM =	<u>30.20</u>	in. Hg.
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3. Volume Water Vapor, (VWV).

$$VWV = (0.04707) \times (VC)$$

Example. VC =	37	Therefore VWV =	<u>1.718</u>	SCF
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4. Meter Volume, corrected to Standard Conditions, (VSTD)

$$VSTPD = \frac{(17.65) \times (VM) \times (PM) \times (Y)}{TM}$$

Example. VM =	35.618	Therefore VSTPD =	<u>35.391</u>	SCF
PM =	30.20			
TM =	553.1			
Y =	1.031			

5. Total Volume Of Sample, (VT).

$$VT = VWV + VSTPD$$

Example. VWV =	1.718	Therefore VT =	<u>37.109</u>	SCF
VSTPD =	35.391			

PB = Barometric Pressure, inches of Hg.

PG = Static Pressure of stack, inches of H2O.

\*H = Average meter orifice pressure differential inches of H2O.

VC = Volume condensate liquid volume + gain in silica gel wt., grams.

PM = See eq. 2.

TM = Temperature, meter, degrees Rankine.

Y = Meter Correction Factor

VWV = See eq. 3.

VSTPD = See eq. 4.

Facility: Georgia Pacific

Test Date: 5/25/01

Source: Bleach Plant Outlet

Run Number: 1

Example Calculations:  
Page 2

6. Fraction Water Vapor in Gas Stream, (W)

$$W = (VWV / VT)$$

Example. VWV = 1.718                      Therefore W = 0.046  
                  VT = 37.109

7. Fraction Dry Air, (FDA)

$$FDA = 1.0 - W$$

Example. W = 0.046                      Therefore FDA = 0.954

8. Molecular Weight of Stack Gas, Dry, (MD)

$$MD = (0.44 \times \%CO_2) + (0.32 \times \%O_2) + (0.28 \times \%N_2) + (0.28 \times \%CO)$$

Example. CO2 = 0                      Therefore MD = 28.84  
                  O2 = 20.9  
                  N2 = 79.1  
                  CO = 0

9. Molecular Weight of Stack Gas, Stack Conditions, (MS)

$$MS = (MD \times FDA) + (18 \times W)$$

Example. MD = 28.84                      Therefore MS = 28.34  
                  FDA = 0.954  
                  W = 0.046

10. Specific Gravity of Gas, Relative to Air, (GS)

$$GS = MS / 28.99$$

Example. MS = 28.34                      Therefore GS = 0.978

VWV = See eq. 3                      MS = See eq. 9  
VT = See eq. 5  
W = See eq. 6  
MD = See eq. 8

Facility: Georgia Pacific

Test Date: 5/25/01

Source: Bleach Plant Outlet

Run Number: 1

Example Calculations:

Page 3

11. Velocity of Stack Gas, as feet per minute, (U).

$$U = 174 \times CP \times H \times \sqrt{(TS \times 29.92) / (GS \times PS)}$$

Example. CP = 0.84                      Therefore U = 1604.8 FPM  
          H = 0.4652  
          TS = 548  
          PS = 30.10  
          GS = 0.978

12. Stack Gas Flow Rate, Stack Conditions, cubic feet per minute, (QS).

$$QS = U \times AS$$

Example. U = 1604.8                      Therefore QS = 15440 ACFM  
          AS = 9.621

13. Stack Gas Flow Rate, Dry (QD)

$$QD = QS \times FDA$$

Example. QS = 15440                      Therefore QD = 14730 CFMD  
          FDA = 0.954

14. Stack Gas Flow Rate, Standard Temperature and Pressure, Dry, (QSTPD)

$$QSTPD = (528 \times QD \times PS) / (TS \times 29.92)$$

Example QD = 14730                      Therefore QSTPD = 14275 SCFMD  
          PS = 30.09  
          TS = 548

CP = Pitot Coefficient

H = Average of square roots of velocity heads, in H<sub>2</sub>O.

TS = Temperature of stack, deg. R.

PS = See eq. 1

GS = See eq. 10

Facility: Georgia Pacific

Test Date: 5/25/01

Source: Bleach Plant Outlet

Run Number: 1

Example Calculations:

Page 4

15. Percent Isokinetic Volume Sampled, (PISO)

$$PISO = \frac{(100) \times T_s \times VSTPD \times P_{std}}{T_{std} \times U \times \bar{C} \times A_n \times P_s \times FDA}$$

Example. AN =	0.000413	Therefore PISO =	96.4
$\bar{C}$ =	60	Pstd =	29.92
VSTPD =	35.391	Tstd =	528
Ts =	548	Ps =	30.095147
U =	1604.8	FDA =	0.954

16. Particulate Concentration, grains per Standard Cubic Foot, (ESTP)

$$ESTP = (.01543 \times Mg.) / VSTPD$$

Example. Mg. =	0	Therefore ESTP =	0	Grs/ SCF.
VSTPD =	35.391			

17. Mass Emission Rate, Lbs / Hr, (EM)

$$EM = \frac{ESTP \times QSTPD \times 60 \text{ Min/ Hr}}{7000}$$

Example.		Therefore EM =	0	Lbs/ Hr
QSTPD =	14275			

VSTPD = See eq. 4

AN = Area Nozzle, Sq Ft

Mg. = Weight of particulate catch in milligrams.



**Technical Services, Inc.**  
**Environmental Consultants**  
**Analytical Chemists**

**2901 Danese Street**  
**Jacksonville, Fl. 32206**  
**(904) 353 - 5761**

**Facility** Georgia Pacific  
**Location** Palatka, FL  
**Stack** Bleach Plant Outlet  
**Run Date** 5/25/01  
**Run Number** 1  
**Start Time** 1850  
**Finish Time** 1952  
**Weather** Clear  
**Total Time (min.)** 60.00  
**Barometric Pressure** 30.09  
**Stack Diameter (in.)** 42.000  
**Stack Area sq. ft.** 9.621  
**Nozzle Area sq. ft.** 0.0004125  
**Number of Points** 12  
**Avg of SQRT of V.H.** 0.4652  
**Meter Correction (Y)** 1.031  
**Nozzle Diameter** 0.275  
**Pitot Correction Factor** 0.84

**Impinger Condensate , MI** 32  
**Silica Gel Condensate, Gm** 4.5  
**Volume Metered** 35.618  
**Meter Temp (Deg R)** 553.1  
**Orsat CO2 %** 0.0  
**Orsat O2 %** 20.9  
**Orsat CO %** 0.0  
**Orsat N %** 79.1  
**Condensate Volume, MI** 36.5  
**Delta H (Inches H2O)** 1.5080  
**Stack Pressure** 30.095  
**Stack Temp (Deg R)** 548.0

=====

**Volume Water Vapor, SCF** 1.718  
**Gas Volume Sampled, STPD** 35.391  
**Total Volume, STP** 37.109  
**Moisture in stack gas, volume fraction** 0.046  
**Dry Stack Gas, volume fraction** 0.954  
**Molecular Weight of Stack Gas (Dry Basis)** 28.84  
**Molecular Weight of Stack Gas (Stack conditions)** 28.34  
**Specific gravity of Stack Gas Relative to Air** 0.978  
**Excess Air (%)** 14864.9  
**Average Stack Velocity, FPM** 1604.8  
**Actual Stack Gas Flow Rate, ACFM** 15440  
**Actual Stack Gas Flow Rate, (Dry) ACFMD** 14730  
**Stack Gas Flow Rate, SCFMD** 14275  
**Percent Isokinetic** 96.4

Technical Services, Inc.  
Environmental Consultants  
Analytical Chemists

2901 Danese Street  
Jacksonville, FL 32206  
(904) 353-5761

Facility: Georgia Pacific  
Stack: Bleach Plant Outlet  
Run Date: 5/25/01  
Run No: 1

Field Data Points				
Trav. Pt.	Vel. Head	Meter Orif.	Stack °F	Meter °F
1	0.23	1.60	92	91
2	0.23	1.60	91	92
3	0.22	1.53	89	93
4	0.22	1.53	90	93
5	0.22	1.53	90	93
6	0.2	1.39	90	93
7	0.22	1.53	86	93
8	0.23	1.60	85	93
9	0.22	1.53	85	93
10	0.22	1.53	85	94
11	0.21	1.46	88	95
12	0.18	1.25	85	94
13	0		0	0
14	0		0	0
15	0		0	0
16	0		0	0
17	0		0	0
18	0		0	0
19	0		0	0
20	0		0	0
21	0		0	0
22	0		0	0
23	0		0	0
24	0		0	0
25	0		0	0
26	0		0	0
27	0		0	0
28	0		0	0
29	0		0	0
30	0		0	0

Facility			
Location	Palatka, FL		
Stack	Bleach Plant Outlet		
Run Date	5/25/01	Impinger Condensate, MI	36.0
Run Number	2	Silica Gel Condensate, Gm	5.2
Start Time	2130	Volume Metered	36.140
Finish Time	2234	Meter Temp (Deg R)	545.8
Weather	Scattered Clouds	Orsat CO2 %	0.0
Total Time (min.)	60.00	Orsat O2 %	20.9
Barometric Pressure	30.09	Orsat CO %	0.0
Stack Diameter (in.)	42.000	Orsat N %	79.1
Stack Area sq. ft.	9.621	Condensate Volume, MI	41.2
Nozzle Area sq. ft.	0.0004125	Delta H (inches H2O)	1.4850
Number of Points	12	Stack Pressure	30.094
Avg of SQRT of V.H.	0.4616	Stack Temp (Deg R)	542.3
Meter Correction (Y)	1.031		
Nozzle Diameter	0.275		
Pitot Correction Factor	0.84		

---

Volume Water Vapor, SCF	1.939
Gas Volume Sampled, STPD	36.388
Total Volume, STP	38.327
Moisture in stack gas, volume fraction	0.051
Dry Stack Gas, volume fraction	0.949
Molecular Weight of Stack Gas (Dry Basis)	28.84
Molecular Weight of Stack Gas (Stack conditions)	28.29
Specific gravity of Stack Gas Relative to Air	0.976
Excess Air (%)	14864.9
Average Stack Velocity, FPM	1585.7
Actual Stack Gas Flow Rate, ACFM	15256
Actual Stack Gas Flow Rate, (Dry) ACFMD	14478
Stack Gas Flow Rate, SCFMD	14178
Percent Isokinetic	99.8

Technical Services, Inc.  
Environmental Consultants  
Analytical Chemists

2901 Danese Street  
Jacksonville, Fl. 32206  
(904) 353 - 5761

Facility: Georgia Pacific  
Stack: Bleach Plant Outlet  
Run Date: 5/25/01  
Run No: 2

Field Data Points				
Trav. Pt.	Vel. Head	Meter Orif.	Stack ' F	Meter ' F
1	0.23	1.60	81	85
2	0.23	1.60	82	85
3	0.22	1.53	82	85
4	0.22	1.53	82	84
5	0.21	1.46	83	88
6	0.2	1.39	82	87
7	0.23	1.60	82	85
8	0.22	1.53	83	86
9	0.21	1.46	82	86
10	0.21	1.46	83	86
11	0.2	1.39	83	86
12	0.18	1.25	83	86
13	0		0	0
14	0		0	0
15	0		0	0
16	0		0	0
17	0		0	0
18	0		0	0
19	0		0	0
20	0		0	0
21	0		0	0
22	0		0	0
23	0		0	0
24	0		0	0
25	0		0	0
26	0		0	0
27	0		0	0
28	0		0	0
29	0		0	0
30	0		0	0

<b>Facility</b>	Georgia Pacific	<b>Impinger Condensate, MI</b>	40.0
<b>Location</b>	Palatka, FL	<b>Silica Gel Condensate, Gm</b>	4.9
<b>Stack</b>	Bleach Plant Outlet	<b>Volume Metered</b>	36.222
<b>Run Date</b>	5/25/01	<b>Meter Temp (Deg R)</b>	542.2
<b>Run Number</b>	3	<b>Orsat CO2 %</b>	0.0
<b>Start Time</b>	2300	<b>Orsat O2 %</b>	20.9
<b>Finish Time</b>	2402	<b>Orsat CO %</b>	0.0
<b>Weather</b>	Partly Cloudy	<b>Orsat N %</b>	79.1
<b>Total Time (min.)</b>	60	<b>Condensate Volume, MI</b>	44.9
<b>Barometric Pressure</b>	30.09	<b>Delta H (inches H2O)</b>	1.5250
<b>Stack Diameter (in.)</b>	42.000	<b>Stack Pressure</b>	30.094
<b>Stack Area sq. ft.</b>	9.621	<b>Stack Temp (Deg R)</b>	537.1
<b>Nozzle Area sq. ft.</b>	0.0004125		
<b>Number of Points</b>	12		
<b>Avg of SQRT of V.H.</b>	0.4680		
<b>Meter Correction (Y)</b>	1.031		
<b>Nozzle Diameter</b>	0.275		
<b>Pitot Correction Factor</b>	0.84		

---

<b>Volume Water Vapor, SCF</b>	2.113
<b>Gas Volume Sampled, STPD</b>	36.716
<b>Total Volume, STP</b>	38.829
<b>Moisture in stack gas, volume fraction</b>	0.054
<b>Dry Stack Gas, volume fraction</b>	0.946
<b>Molecular Weight of Stack Gas (Dry Basis)</b>	28.84
<b>Molecular Weight of Stack Gas (Stack conditions)</b>	28.25
<b>Specific gravity of Stack Gas Relative to Air</b>	0.974
<b>Excess Air (%)</b>	14864.9
<b>Average Stack Velocity, FPM</b>	1601.6
<b>Actual Stack Gas Flow Rate, ACFM</b>	15409
<b>Actual Stack Gas Flow Rate, (Dry) ACFMD</b>	14577
<b>Stack Gas Flow Rate, SCFMD</b>	14413
<b>Percent Isokinetic</b>	99.0

Technical Services, Inc.  
Environmental Consultants  
Analytical Chemists

2901 Danese Street  
Jacksonville, Fl. 32206  
(904) 353 - 5761

Facility: Georgia Pacific  
Stack: Bleach Plant Outlet  
Run Date: 5/25/01  
Run No: 3

Field Data Points				
Trav. Pt.	Vel. Head	Meter Orif.	Stack ' F	Meter ' F
1	0.23	1.60	80	82
2	0.22	1.53	81	83
3	0.22	1.53	80	83
4	0.22	1.53	78	82
5	0.2	1.39	78	82
6	0.2	1.39	78	82
7	0.23	1.60	76	82
8	0.23	1.60	76	82
9	0.24	1.67	75	82
10	0.22	1.53	75	82
11	0.22	1.53	74	82
12	0.2	1.39	74	82
13	0		0	0
14	0		0	0
15	0		0	0
16	0		0	0
17	0		0	0
18	0		0	0
19	0		0	0
20	0		0	0
21	0		0	0
22	0		0	0
23	0		0	0
24	0		0	0
25	0		0	0
26	0		0	0
27	0		0	0
28	0		0	0
29	0		0	0
30	0		0	0

**Ambient Air Services, Inc.**  
**Environmental Consultants**

106 Ambient Air Way  
 Starke, Florida 32091

(904) 964 - 8440  
 (904) 964 - 6675 fax

**Volumetric Air-Flow Rates**

<b>Plant</b>	GEORGIA PACIFIC		
<b>Location</b>	PALATKA, FL		
<b>Stack</b>	BLEACH PLANT		
<b>Run Date</b>	5/26/01		
<b>Run Number</b>	3	<b>Volume Metered</b>	0
<b>Start Time</b>	0	<b>Meter Temp (Deg R)</b>	ERR
<b>Finish Time</b>	0	<b>Orsat CO2 %</b>	0
<b>Barometric Pressure</b>	30.09	<b>Orsat O2 %</b>	21
<b>Stack Diameter (in.)</b>	42	<b>Orsat CO %</b>	0
<b>Stack Area sq. ft.</b>	9.621	<b>Orsat N %</b>	79
<b>Number of Points</b>	0	<b>Condensate Volume</b>	0
<b>Avg of SQRT of V.H.</b>	0.4641	<b>Delta H (inches H2O)</b>	ERR
<b>Meter Correction (Y)</b>	0	<b>Stack Pressure</b>	30.09
<b>Pitot Correction Factor</b>	0.84	<b>Stack Temp (Deg R)</b>	534.8

---

Moisture in stack gas, volume fraction	0.053
Dry Stack Gas, volume fraction	0.947
Molecular Weight of Stack Gas (Dry Basis)	28.84
Molecular Weight of Stack Gas (Stack conditions)	28.270
Specific gravity of Stack Gas Relative to Air	0.975
Excess Air (%)	
Average Stack Velocity, FPM	1584.2
Actual Stack Gas Flow Rate, ACFM	15242
Actual Stack Gas Flow Rate, (Dry) ACFMD	14434
Stack Gas Flow Rate (Standard conditions), SCFMD	14331
Stack Gas Flow Rate (Standard conditions), SCFMW	15133

**APPENDIX B**  
**FIELD DATA SHEETS**



TECHNICAL SERVICES, INC.

JACKSONVILLE, FL

(904)353-5761

BAROMETRIC PRESS 30.09

METER BOX ID 11

METER DELTA Ha 2.32

PROBE ID 5c5

PITOT CORR. FACTOR 0.84

NOZZLE DIA. 0.275 in.

PROBE TEMP. ~290

STACK ID (IN): 4642

PORT LENGTH 7"

SOURCE SAMPLING FIELD DATA SHEET

FACILITY: Georgia Pacific Palatka, GA RUN No. 1

SOURCE: Black Plant outlet DATE: 5-25-01

WEATHER: Clear PRE-TEST.

TYPE TEST: M26A Ts = 558

TESTERS: BA/BAN Tm = 555

17 PTS. @ 15 MIN/PT 60 MIN F.D.A. = 0.92

Y meter = 1.031 Filter No. =         

COMMENTS:

*Dave/GP Palatka*

TIME START	<u>1450</u>	START VOLUME	<u>212.658</u>
TIME END	<u>1952</u>	END VOLUME	<u>248.276</u>

*Ea = 0.36/hu*  
*Chlorinated hps*

Factors: 6.959

LEAK CHECK:

PRE-TEST 0.016 CFM@15". POST: 0.0062 2" Hg.

PITOT LEAK CHECK = OK AT 3"

VOL. WATER COLLECTED = 32 ML STAT. PRESS = +0.07  
WEIGHT MOIS. SILICA GEL = 45 GR

PORT & SAMPLE POINT	CLOCK TIME	GAS METER READING	STACK VELOCITY Dp	ORIFICE PRESS. DROP	STACK GAS TEMP.	METER TEMP (F)	FILTER TEMP (F)	LAST IMPINGER TEMP.	VACUUM INCHES Hg.	SCFMD = 17127
1-1	5	15.4	0.23	1.6	92	91	249	62	2	<del>LEAK</del>
2	10	18.2	0.23	1.6	91	92	252	60	2	
3	15	22.6	0.22	1.5	89	93	252	59	2	
4	20	25.2	0.22	1.5	90	93	253	60	2	
5	25	28.9	0.22	1.5	90	93	252	60	2	
6	30	31.1	0.20	1.4	90	93	251	61	2	
2-1	35	34.1	0.22	1.5	86	93	250	62	2	
2	40	36.8	0.23	1.6	85	93	259	62	2	
3	45	39.7	0.22	1.5	88	93	261	62	2	
4	50	42.2	0.22	1.5	88	94	260	63	2	
5	55	45.5	0.21	1.5	88	95	261	63	2	
6	60		0.18	1.3	88	94	262	63	2	

JACKSONVILLE, FL

(904)353-5761

BAROMETRIC PRESS 30.09

METER BOX ID 11

METER DELTA Ha 2.32

PROBE ID 509

PITOT CORR FACTOR 0.84

NOZZLE DIA 0.275 in

PROBE TEMP 28.6

STACK ID (IN) 4642

PORT LENGTH 7"

FACILITY: Georgia Pacific Palatka,

SOURCE: bleach plant outlet

WEATHER: Scattered Clouds PRE-TEST.

TYPE TEST: M26A Ts = \_\_\_\_\_

TESTERS: W/BM Tm = \_\_\_\_\_

12 PTS. @ 5 MIN/PT 60 MIN F.D.A. = \_\_\_\_\_

Y meter = 1.031 Filter No. = \_\_\_\_\_ Computer \_\_\_\_\_

Directory and file name \_\_\_\_\_

RUN No 2

DATE 5-27-00

ORSAT \_\_\_\_\_

CO2 0

O2 20.9

CO 0

TIME START 2130 START VOLUME ~~248~~ 351

TIME END 2234 END VOLUME 284.491

Factors: 6.959

LEAK CHECK: PRE-TEST: 0.016 CFM@15" POST: 0.001 Hg

PITOT LEAK CHECK: OK AT 3"

VOL. WATER COLLECTED = 36 ML STAT PRESS = +0.05  
WEIGHT MOIS. SILICA GEL = 5.2 GR

PORT & CLOCK GAS METER  
SAMPLE TIME READING

STACK VELOCITY Dp	ORIFICE PRESS DROP	STACK GAS TEMP	METER TEMP (F)	FILTER TEMP (F)	LAST IMPINGER TEMP	VACUUM INCHES Hg
0.23	1.6	81	85	249	64	3
0.23	1.6	82	85	249	60	3
0.22	1.5	82	85	254	60	3
0.22	1.5	82	88	251	61	3
0.21	1.5	83	87	247	61	3
0.21	1.4	82	87	247	61	3
0.23	1.6	82	85	242	61	3
0.22	1.5	85	86	245	60	3
0.21	1.5	82	86	251	61	3
0.21	1.5	83	86	249	61	3
0.20	1.4	83	86	242	61	3
0.18	1.3	83	86	230	62	3

COMMENTS: Sopped 25x

1-1 5 52.4  
 2 15 53.8  
 3 25 58.2  
 4 30 60.5  
 5 35 63.4  
 6 30 66.1

2-1 35 68.9  
 2 40 71.2  
 3 45 74.2  
 4 50 77.8  
 5 55 79.9  
 6 60

JACKSONVILLE, FL

(904)353-5761

BAROMETRIC PRESS 30.09

METER BOX ID 11

METER DELTA Ha 2.32

PROBE ID 549

PITOT CORR FACTOR 1.04

NOZZLE DIA 0.25 IN

PROBE TEMP ~ 270

STACK ID (IN) 46 42

PORT LENGTH 7"

LEAK CHECK:

PRE-TEST 0.00 CFM@15" POST 0.001 @ 3 Hg

PORT & SAMPLE POINT	CLOCK TIME	GAS METER READING
1-1	5	88.7
2	10	90.8
3	15	94.1
4	20	98.2
5	25	00.0
6	30	03.1

PITOT LEAK CHECK

= OK AT 3"

VOL. WATER COLLECTED = 40 ML

WEIGHT MOIS. SILICA GEL = 4.9 GR

STAT. PRESS =

70.06

TIME START	<u>2300</u>	START VOLUME	<u>285.953</u>
TIME END	<u>2402</u>	END VOLUME	<u>320.215</u>

Factors: 6.959

65

STACK VELOCITY (Dp)	ORIFICE PRESS DROP	STACK GAS TEMP	METER TEMP (F)	FILTER TEMP (F)	LAST IMPINGER TEMP	VACUUM INCHES Hg
0.23	1.6	80	82	249	62	3
0.22	1.5	81	83	255	60	3
0.22	1.5	80	85	256	59	3
0.22	1.4	78	82	252	60	3
0.20	1.4	78	82	247	59	3
0.20	1.4	78	82	248	59	3
0.23	1.6	76	82	242	60	3
0.23	1.6	76	82	240	60	3
0.24	1.7	75	82	240	60	3
0.22	1.4	75	82	242	60	3
0.22	1.4	74	82	245	60	3
0.20	1.4	74	82	236	61	3

COMMENTS

FACILITY: Georgia Pacific Plant No. 1, FL RUN No 3

SOURCE: Bleach Plant Outlet DATE: 5-25-01

WEATHER: Partly Cloudy PRE-TEST.

TYPE TEST: NDA Ts = \_\_\_\_\_

TESTERS: BA/BM Tm = \_\_\_\_\_

12 PTS. @ 5 MIN/PT 60 MIN F.D.A. = \_\_\_\_\_

Y meter = 1.031 Filter No. = \_\_\_\_\_ Computer \_\_\_\_\_

Directory and file name \_\_\_\_\_

ORSAT

CO2 0

O2 21.5

CO 0



**APPENDIX C**  
**LABORATORY ANALYSIS**

# TECHNICAL SERVICES, INC.

## ENVIRONMENTAL CONSULTANTS

For Georgia Pacific (Palatka)  
P O Box 919  
Palatka, FL 32178-0919  
Contact: Joe Taylor

Report Date 30-May-01  
Date Received 05/26/2001 @ 10:20  
Purchase Order #:

### CERTIFICATE OF ANALYSIS

LAB SAMPLE DESCRIPTION	MATRIX	SAMPLE DATE	SAMPLE TIME	SAMPLED BY
01050850 BLEACH PLANT INLET AND OUTLET, OUTLET RUN 1/ COMPOSITE	IMPINGER	05/25/2001	NA	TSI- D.S. , G.H.
01050851 BLEACH PLANT INLET AND OUTLET, OUTLET RUN 2/ COMPOSITE	IMPINGER	05/25/2001	NA	TSI- D.S. , G.H.
01050852 BLEACH PLANT INLET AND OUTLET, OUTLET RUN 3/ COMPOSITE	IMPINGER	05/25/2001	NA	TSI- D.S. , G.H.
01050853 BLEACH PLANT INLET AND OUTLET, OUTLET RUN 1/ COMPOSITE	IMPINGER	05/25/2001	NA	TSI- D.S. , G.H.
01050854 BLEACH PLANT INLET AND OUTLET, OUTLET RUN 2/ COMPOSITE	IMPINGER	05/25/2001	NA	TSI- D.S. , G.H.
01050855 BLEACH PLANT INLET AND OUTLET, OUTLET RUN 3/ COMPOSITE	IMPINGER	05/25/2001	NA	TSI- D.S. , G.H.

Respectfully submitted,  
Technical Services, Inc.



*Air and Water Pollution Sampling Surveys Testing and Analytical Services*

Georgia Pacific (Palatka)

Lab No	Parameter	Result	Code	Method	Detection Limit
01050850	Default	Not analyzed			
01050851	Default	Not analyzed			
01050852	Default	Not analyzed			
R-1 01050853	Chloride	0.971	ug/ml Cl-	Method 26A	0.02
01050853	Sample Volume	196 <i>190.3 µg</i>	mls		1
R-2 01050854	Chloride	0.808	ug/ml Cl-	Method 26A	0.02
01050854	Sample Volume	200 <i>161.6 µg</i>	mls		1
R-3 01050855	Chloride	0.838	ug/ml Cl-	Method 26A	0.02
01050855	Sample Volume	194 <i>162.6 µg</i>	mls		1

Georgia Pacific (Palatka)

Lab No	Parameter	Date of Analysis	Analysis Time	Analyst	Prep Date
01050850	Default			none	
01050851	Default			none	
01050852	Default			none	
01050853	Chloride	05/26/2001		WEM	
01050853	Sample Volume	05/26/2001		WEM	
01050854	Chloride	05/26/2001		WEM	
01050854	Sample Volume	05/26/2001		WEM	
01050855	Chloride	05/26/2001		WEM	
01050855	Sample Volume	05/26/2001		WEM	



**APPENDIX D**

**SCRUBBER DATA AND PROCESS CERTIFICATION**

# BLEACH PLANT PRODUCTION DATA

DATE	TIME	ADTUP	FAN LOAD, %
05/25/01	1850-1952	55	85.1
	2133-2300	50	85.6
	2300-2330	55	85.9
	2330-0042	50	85.8
	0145-0230	50	85.2

ADTUP is air-dried tons of unbleached pulp across the bleach plant.

Fan load is the % of full load (amperage) of the fan used as the surrogate flow measure.

The scrubber recirculation flow ranged from 1500 gpm to 1740 gpm during the testing.

The scrubber pH was 9.5 during the testing.

DATA CERTIFICATION BY OWNER OR HIS AUTHORIZED AGENT

1. Myra Carpenter,  
(print name)

certify that to my knowledge all data

submitted in this compliance test report

for the ECF Bleach Plant unit

on May 25, 2001  
(date)

are true and correct.

Myra Carpenter  
(signature and title)

**APPENDIX E**  
**CHAIN OF CUSTODY**

01050950 -  
01050875

Technical Services, Inc.  
2901 Danese St., Jacksonville, FL 32206  
(904) 353-5761 / fax (904) 358-2908

## CHAIN of CUSTODY RECORD

CLIENT NAME & ADDRESS (REPORT TO BE SENT TO): <i>Go Air Dept</i> <i>Georgia Pacific</i> <i>Palatka, FL</i>					REMARKS <i>Bleach Plant inlet + Outlet</i> <i>Method 264</i>				
PROJ. NO.		PROJECT NAME/ ADDRESS:			BOTTLE MAKEUP  TOTAL NO. of Containers <i>14 Poly's</i>				
SAMPLERS: (SIGNATURE) <i>[Signature]</i> <i>G Hawkins</i>									
Sample Location ID	DATE	TIME	COMP	GRAB				PARAMETERS	
<i>Outlet R-1</i>	<i>5-25-01</i>	<i>N/A</i>	<i>✓</i>	<i>✓</i>	<i>1</i>	<i>0.1N H<sub>2</sub>SO<sub>4</sub></i>			<i>M 264</i>
<i>2</i>	<i>↓</i>	<i>↓</i>	<i>↓</i>	<i>↓</i>	<i>1</i>	<i>↓</i>			
<i>3</i>	<i>↓</i>	<i>↓</i>	<i>↓</i>	<i>↓</i>	<i>1</i>	<i>↓</i>			
<i>R-1</i>	<i>↓</i>	<i>↓</i>	<i>↓</i>	<i>↓</i>	<i>1</i>	<i>0.1N NaOH</i>			
<i>2</i>	<i>↓</i>	<i>↓</i>	<i>↓</i>	<i>↓</i>	<i>1</i>	<i>↓</i>			
<i>3</i>	<i>↓</i>	<i>↓</i>	<i>↓</i>	<i>↓</i>	<i>1</i>	<i>↓</i>			
RELINQUISHED BY <i>[Signature]</i>			DATE/TIME RECEIVED BY <i>5/24/01 [Signature]</i>			DATE/TIME			
RELINQUISHED BY			DATE/TIME RECEIVED BY			DATE/TIME			
RELINQUISHED BY			DATE/TIME RECEIVED BY			DATE/TIME			
					RECEIVED FOR LABORATORY BY <i>[Signature]</i> DATE/TIME <i>5/24/01 11:20</i>				

APPENDIX F  
CALIBRATION DATA

**Annual Dry Gas Meter Calibration Data By TSI Reference Meter**

REFERENCE METER **R-275** TSI Reference Dry Meter Calibration Date: **8/09/00**

Yi of reference meter: **1.012**

Date **1/4/01**

Calibrated by **R Garza**

Barometric Pressure 30.12

Meter Box 11

Orifice Manometer Setting (DH) In. H2O	Reference Dry Gas Meter  Cu.ft.	Gas Volume		Temperature		Time (t), min	Delta H In. H2O	Yi	
		Reference Meter (Vw) Std.Cu. Ft.	Dry Gas Meter (VD) Cu. Ft.	Reference Meter (Tw) Deg ^F	Dry Gas Meter				
					Temperature (Td) Deg ^F				
0.5	10.015	10.099	9.715	73.2	X 66.40	29.34	2.39	1.025	
1	10.002	10.082	9.761	73.4	X 70.90	20.46	2.31	1.026	
1.5	10.005	10.044	9.642	75.6	X 73.30	17.00	2.42	1.033	
2	10.013	10.075	9.691	74.4	X 74.50	14.50	2.32	1.035	
3	10.012	10.057	9.645	75.3	X 75.40	11.39	2.16	1.035	
<b>Average Delta H and Y</b>							2.32	1.031	
Yi Allowance =						1.011	To	1.051	
DH Allowance =						2.12	To	2.52	

\* If there is only one thermometer on the dry gas meter, record the temperature under Td

Vw = Gas volume passing through the Reference test meter, (cu. ft.)

Vd = Gas volume passing through the dry gas meter, (cu. ft.)

Tw = Temperature of the gas in the Reference test meter, Deg F

Td = Temperature of the gas in the dry gas meter, Deg F

DH = Pressure differential across orifice, in H2O = pretest DH + or - 0.20

Yi = Ratio of accuracy of the Reference test meter to dry gas meter for each run

Y = Average ratio of the Reference test meter to dry gas meter for all three test runs;

tolerance = pretest Y + or - 0.02Y

Pb = Barometric pressure, in. Hg.

t = Time of calibration run, min.

T  
S  
I

Post-Test Dry Gas Meter Calibration Data Form (English Units)

*RA*

Test numbers All Date 5/31/01 Meter Box No. 11 Facility GP

Barometric Pressure, Pb 30.05 Reference Meter R-275 Pretest Y Value 1.024

Orifice Manometer Setting (DH) In. H2O	Gas Volume		Reference Meter (Tw) Deg ^F	Temperature			Time (t), min	Vacuum Setting In. Hg.	Yi
	Reference Meter (Vw) Cu. Ft.	Dry Gas Meter (VD) Cu. Ft.		Dry Gas Meter					
						Average (Td) Deg ^F			
1.5	10.003	9.831	75	X	X	75	16.87	< 2	1.014
1.5	10.001	9.823	75	X	X	76	16.56	<2	1.016
1.5	10.000	9.820	80	X	X	81	16.92	<2	1.016
Yi =									1.016

\* If there is only one thermometer on the dry gas meter, record the temperature under Td

- Vw = Gas volume passing through the reference test meter, (cu. ft.)
- Vd = Gas volume passing through the dry gas meter, (cu. ft.)
- Tw = Temperature of the gas in the reference test meter, Deg F
- (Td)i = Temperature of the inlet gas of the dry gas meter, Deg F
- (Td)o = Temperature of the outlet gas of the dry gas meter, Deg F
- Td = Average temperature of the gas in the dry gas meter, obtained by the average of (Td)i & (Td)o, Deg F
- DH = Pressure differential across orifice, in H2O
- Yi = Ratio of accuracy of the reference test meter to dry gas meter for each run
- Y = Average ratio of the reference test meter to dry gas meter for all three test runs; tolerance = pretest Y + or - 0.02Y
- Pb = Barometric pressure, in. Hg.
- t = Time of calibration run, min.

$$Y_i = \frac{V_w \cdot P_b \cdot (T_d + 460)}{V_d (P_b + (\Delta H/13.6)) \times (T_w + 460)}$$

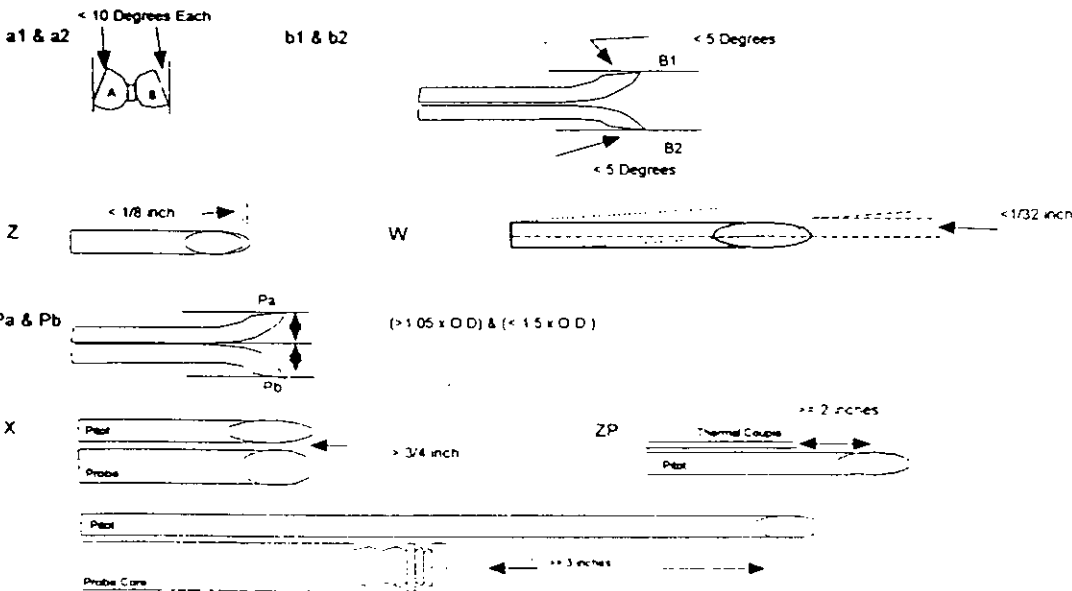


**ANNUAL PITOT TUBE CALIBRATION WORKSHEET**  
**MARCH 22, 2001**

Pitot Tube I.D. #	Coefficient	Pa Inches	Pb Inches	Dt Inches	Zs Inches	Ws Inches	a1 Degrees	a2 Degrees	b1 Degrees	b2 Degrees	X Inches	Zp Inches	Y Inches
WC1	0.84	0.555	0.533	0.373	0.07	< 0.313	0	2	2	3	0.74	2.0	4.0
3A	0.84	0.554	0.556	0.374	0.061	< 0.313	1	3	2	2	1.4	2.0	4.0
3AG	0.84	0.550	0.551	0.375	0.003	< 0.313	2	3	3	2	1.5	2.0	4.0
4A	0.84	0.540	0.538	0.375	0.049	< 0.313	1	3	2	2	1.4	2.0	4.0
4AG	0.84	0.557	0.554	0.373	0.03	< 0.313	1	1	3	0	1.5	2.0	4.0
6A	0.84	0.512	0.539	0.375	0.063	< 0.313	0	2	2	1	1.5	2.0	4.0
6B	0.84	0.405	0.415	0.375	0.06	< 0.313	0	3	2	1	1.2	2.0	4.0
5CG	0.84	0.540	0.551	0.375	0.066	< 0.313	2	3	2	2	1.12	2.0	4.0
7A	0.84	0.550	0.542	0.374	0.056	< 0.313	1	2	1	2	1.31	2.0	4.0
7B	0.84	0.549	0.542	0.375	0.06	< 0.313	3	1	1	1	1.38	2.0	4.0
7C	0.84	0.555	0.560	0.375	0.051	< 0.313	1	2	2	2	1.41	2.0	4.0
7AG	0.84	0.540	0.535	0.371	0.037	< 0.313	3	3	1	1	1.3	2.0	4.0
7BG	0.84	0.550	0.551	0.375	0.034	< 0.313	2	2	3	3	1.1	2.0	4.0
7CG	0.84	0.556	0.554	0.375	0.032	< 0.313	1	3	1	1	1.35	2.0	4.0
8A	0.84	0.531	0.545	0.375	0.031	< 0.313	2	2	0	2	1.2	2.0	4.0
9A	0.84	0.520	0.512	0.374	0.056	< 0.313	2	2	1	1	1.51	2.0	4.0
10A	0.84	0.554	0.544	0.374	0.078	< 0.313	2	2	0	1	1.28	2.0	4.0
10B	0.84	0.550	0.552	0.375	0.05	< 0.313	1	1	3	2	1.25	2.0	4.0
12A	0.84	0.407	0.411	0.374	0.059	< 0.313	3	3	2	2	1.35	2.0	4.0

Calibrations performed by George Hawkins

- Pa Distance between where pitots adjoin to tip of pitot (Must be between 1.05 & 1.50 times O.D. of tubing)
- Pb Distance between where pitots adjoin to tip of pitot (Must be between 1.05 & 1.50 times O.D. of tubing)
- Dt Diameter of pitot tube (0.375 inches on all pitots)
- Zs Distance between the tip of the impact and static line along the length of the pitot (Must be < 1/8 inch (0.1250))
- Ws Spacing between Pitot tubes when welded together (Must be < 1/32 inch (0.0313))
- a1 Angle across opening of Pitot tube from side to side or perpendicular to length of probe (Must be < 10 Deg)
- a2 Angle across opening of Pitot tube from side to side or perpendicular to length of probe (Must be < 10 Deg)
- b1 Angle across opening of Pitot tube from side to side or perpendicular to length of probe (Must be < 5 Deg)
- b2 Angle across opening of Pitot tube from side to side or perpendicular to length of probe (Must be < 5 Deg)
- X Distance between side of nozzle and side of pitot tube (Must be > 3/4 inch)
- Zp Distance from center of pitot opening back to tip of thermal couple (Must be >= 3/4 inch (0.75))
- Y Distance from center of pitot opening back to probe (Must be >= 3 inches)



**T S I** **Air Report - Method Five Equipment Calibrations**

**NOZZLE CALIBRATION**

Facility	Georgia Pacific	Date	5/25/01
Location	Palatka, FL		
Source Name	Bleach Plant Outlet	Analyst	NA

**Calibration Data**

All Technical Services, Inc. pitot tubes have been modified to comply with specifications as presented in the Thursday, August 18, 1977 Federal Register (Vol. 42, No. 160). A pitot tube correction factor of 0.84 has been assigned.

Our thermometers, pyrometers and thermocouples are calibrated against a standard mercury thermometer in a hot oven in our laboratory. (Data on following page.)

Our field barometer is checked before every test against that of our laboratory mercury barometer.

All probe nozzles are calibrated each test run to assure isokinetic sampling.

Nozzle Diameter in Inches: 0.275

				Mean
Run 1	0.275	0.275	0.275	0.275

**Air Report - Method Five Equipment Calibrations**

**THERMOCOUPLE CALIBRATIONS**

Facility: Georgia Pacific Date: 5/31/01  
 Location: Palatka, FL Analyst: NA  
 Source Name: Bleach Plant Outlet Inlet

**Calibration Data**

Ambient Temperature 75 Reference: Mercury in glass  X  
 Thermocouple Number 5cg Other   
 Barometric Pressure 29.97

Reference Point Number	Source(a) (specify)	Reference Thermometer Temperature	Thermocouple Temperature	Temperature Difference(b)
1	Ice Bath	<u>34</u>	<u>33</u>	0.20
2	Inter-mediate	<u>75</u>	<u>73</u>	0.37
3	Boiling Water	<u>212</u>	<u>212</u>	0.00
4	Hot Oil	<u>347</u>	<u>345</u>	0.25

≡ Type of calibration system used  
 =  $\frac{-(\text{REF. TEMP.} + 460) - (\text{THERMOCOUPLE TEMP.} + 460)}{\text{ref. temp} + 460} \times 100 \leq 1.5\%$

**GEORGIA PACIFIC**  
**PALATKA, FLORIDA**  
**SUMMARY OF CO CALIBRATIONS - BLEACH PLANT**  
**5/25/01 - 5/26/01**

<b>INSTRUMENT RANGE, PPM</b>		1200		
<b>CALIBRATION GAS PPM</b>	<b>INITIAL CALIBRATION</b>	<b>END RUN 1</b>	<b>END RUN 2</b>	<b>END RUN 3</b>
0.0	12.0	12.0	11.3	10.8
1015.0	1016.4	1020.0	1032.5	1031.6
594.7	575.1	N/A	N/A	N/A
301.9	293.5	N/A	N/A	N/A
<b>CALIBRATION ERROR</b>		<b>((INSTRUMENT RESPONSE-CALIBRATION GAS VALUE)/INSTRUMENT RANGE)X100</b>		
0.0	1.0	1.0	0.9	0.9
1015.0	0.1	0.4	1.5	1.4
594.7	-1.6	N/A	N/A	N/A
301.9	-0.7	N/A	N/A	N/A
<b>CALIBRATION DRIFT</b>		<b>((FINAL CALIBRATION - INITIAL CALIBRATION)/INSTRUMENT RANGE)X100</b>		
0.0	N/A	0.0	-0.1	-0.1
1015.0	N/A	0.3	1.3	1.3
594.7	N/A	N/A	N/A	N/A
<b>ZERO BIAS CHECKS</b>		<b>(SAMPLE SYSTEM-DIRECT)/RANGEX100</b>		
<b>SAMPLE ZERO</b>	<b>DIRECT ZERO</b>	<b>BIAS</b>		ALL CAL GASES INJECTED TO PROBE TIP ONLY
N/A	N/A	#VALUE!	INITIAL	
N/A	N/A	#VALUE!	FINAL	
<b>CALIBRATION BIAS CHECKS</b>				
<b>CALIBRATION GAS, PPM</b>	N/A			
<b>SAMPLE</b>	<b>DIRECT</b>	<b>BIAS</b>		
N/A	N/A	#VALUE!	INITIAL	
N/A	N/A	#VALUE!	FINAL	

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# CERTIFICATE OF ANALYSIS / EPA PROTOCOL GAS

CUSTOMER PRAXAIR SOUTHEAST

P.O NUMBER 333045-00

## REFERENCE STANDARD

COMPONENT	NIST SRM NO.	CYLINDER NO.	CONCENTRATION
CARBON MONOXIDE 503.2PPM GMIS VS	1680B	CLM-009396	490.4 PPM

## ANALYZER READINGS

R=REFERENCE STANDARD

Z=ZERO GAS

C=GAS CANDIDATE

COMPONENT	CARBON MONOXIDE 503.2PPM GMIS	ANALYZER MAKE-MODEL-S/N	Siemens Ultramat SE	S/N B8-900			
ANALYTICAL PRINCIPLE	NON-DISPERSIVE INFRARED		LAST CALIBRATION DATE	12/31/00			
FIRST ANALYSIS DATE	12/27/00		SECOND ANALYSIS DATE	11/13/01			
Z 0	R 503	C 301	CONC. 302.3	Z 0	R 504	C 302	CONC. 302.3
R 502	Z 0	C 302	CONC. 302.3	R 504	Z 0	C 302	CONC. 302.3
Z 0	C 302	R 503	CONC. 302.3	Z 0	C 303	R 504	CONC. 302.3
U/M ppm	MEAN TEST ASSAY	302.0	U/M ppm	MEAN TEST ASSAY	302.3		

VALUES NOT VALID BELOW 150 PSIG  
 UNCERTAINTY OF CARBON MONOXIDE 0.19PPM

THIS CYLINDER NO.	00114912	CERTIFIED CONCENTRATION	
HAS BEEN CERTIFIED ACCORDING TO SECTION	1.1	CARBON MONOXIDE	302.3PPM
OF TRACEABILITY PROTOCOL NO.	EPA 600/R577/101	AIR	BALANCE
PROCEDURE	31		
CERTIFIED ACCURACY	± 1 % NIST TRACEABLE		
CYLINDER PRESSURE	2000 PSIG		
CERTIFICATION DATE	01/03/01		
EXPIRATION DATE	01/03/04 TERM		

ANALYZED BY

JOHN PPIBISH

CERTIFIED BY

KEVIN BRADY

## CERTIFICATE OF ANALYSIS / EPA PROTOCOL GAS

**CUSTOMER** PRAXAIR SOUTHEAST

**P.O NUMBER** 333045-00

### REFERENCE STANDARD

<b>COMPONENT</b>	<b>NIST SRM NO.</b>	<b>CYLINDER NO.</b>	<b>CONCENTRATION</b>
CARBON MONOXIDE 503.2PPM GMIS VS	1680B	CLM-009396	490.4 PPM

### ANALYZER READINGS

**R=REFERENCE STANDARD**
**Z=ZERO GAS**
**C=GAS CANDIDATE**

<b>I. COMPONENT</b>	CARBON MONOXIDE 503.2PPM GMIS	ANALYZER MAKE-MODEL-S/N	Siemens Ultramat 5E S/N B8-900
<b>ANALYTICAL PRINCIPLE</b>	NON-DISPERSIVE INFRARED	<b>LAST CALIBRATION DATE</b>	12/31/00
<b>FIRST ANALYSIS DATE</b>	12/27/00	<b>SECOND ANALYSIS DATE</b>	01/03/01
Z 0	R 503	C 595	CONC. 595.6
R 502	Z 0	C 595	CONC. 595.6
Z 0	C 594	R 503	CONC. 595.6
U/M ppm	MEAN TEST ASSAY	595.3	U/M ppm

VALUES NOT VALID BELOW 150 PSIG  
 UNCERTAINTY OF CARBON MONOXIDE ±4.2PPM

<b>THIS CYLINDER NO.</b> SA12251	<b>CERTIFIED CONCENTRATION</b>
<b>HAS BEEN CERTIFIED ACCORDING TO SECTION</b> 2.3	CARBON MONOXIDE 594.7PPM
<b>OF TRACEABILITY PROTOCOL NO.</b> EPA-820/R97/121	AIR
<b>PROCEDURE</b> 01	BALANCE
<b>CERTIFIED ACCURACY</b> ± 1 % NIST TRACEABLE	
<b>CYLINDER PRESSURE</b> 2000 PSIG	
<b>CERTIFICATION DATE</b> 01/03/01	
<b>EXPIRATION DATE</b> 01/03/04	<b>TERM</b>

**ANALYZED BY**
**CERTIFIED BY**

JOHN P. DELOACH



# SPECTRA GASES

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## CERTIFICATE OF ANALYSIS

## EPA PROTOCOL MIXTURE

PROCEDURE #: G2

CUSTOMER: Ambient Air Service  
SGI ORDER #: 134478  
ITEM#: 1  
P.O.#: 07079802

CYLINDER #: CC88617  
CYLINDER PRES: 2000 PSIG  
CGA OUTLET: 350

CERTIFICATION DATE: 7/8/98  
EXPIRATION DATE: 7/8/2001

### CERTIFICATION HISTORY

COMPONENT	DATE OF ASSAY	MEAN CONCENTRATION	CERTIFIED CONCENTRATION	ANALYTICAL ACCURACY
Carbon Monoxide	2/24/98 7/8/98	1014 ppm 1017 ppm	1015 ppm	+/- 1%

BALANCE Nitrogen

### REFERENCE STANDARDS

COMPONENT	SRM/NTRM#	CYLINDER#	CONCENTRATION
Carbon Monoxide	NTRM-81681	CC55775	994 ppm

### INSTRUMENTATION

COMPONENT	MAKE/MODEL	SERIAL #	DETECTOR	CALIBRATION DATE(S)
Carbon Monoxide	Horiba VIA-510	570423011	NDIR	6/29/98

THIS STANDARD WAS CERTIFIED ACCORDING TO THE EPA PROTOCOL PROCEDURES.  
DO NOT USE THIS STANDARD IF THE CYLINDER PRESSURE IS LESS THAN 150 PSIG.

ANALYST: Fred Pikula  
FRED PIKULA

DATE: 7/8/98

**APPENDIX G**  
**CARBON MONOXIDE EMISSIONS**



## Georgia Pacific Bleach Plant - Carbon Monoxide Test

DATE / TIME	PPM	COMMENTS	ZERO CAL	1015 ppm cal	CORRECTED PPM	FLOW, scfm dry	POUNDS OF CO PER HOUR
5/25/01 18 46	1030.0	1015 ppm cal	10.98	1026.4			
5/25/01 18 46	1026.0	1015 ppm cal	10.98	1026.4			
5/25/01 18 46	1022.0	1015 ppm cal	10.98	1026.4			
5/25/01 18 46	1026.0	1015 ppm cal	10.98	1026.4			
5/25/01 18 47	1030.0	1015 ppm cal	10.98	1026.4			
5/25/01 18 47	1024.0	1015 ppm cal	10.98	1026.4			
5/25/01 18 47	1022.0	1015 ppm cal	10.98	1026.4			
5/25/01 18 47	1016.0	wart	10.98	1026.4			
5/25/01 18 48	923.8	wart	10.98	1026.4			
5/25/01 18 48	456.9	wart	10.98	1026.4			
5/25/01 18 48	144.2	wart	10.98	1026.4			
5/25/01 18 48	24.0	wart	10.98	1026.4			
5/25/01 18 49	14.0	wart	10.98	1026.4			
5/25/01 18 49	24.0	wart	10.98	1026.4			
5/25/01 18 49	56.1	wart	10.98	1026.4			
5/25/01 18 49	44.0	wart	10.98	1026.4			
5/25/01 18 50	18.0	wart	10.98	1026.4			
5/25/01 18 50	12.0	wart	10.98	1026.4			
5/25/01 18 50	12.0	wart	10.98	1026.4			
5/25/01 18 50	10.0	0 ppm cal	10.98	1026.4			
5/25/01 18 51	10.0	0 ppm cal	10.98	1026.4			
5/25/01 18 51	10.0	0 ppm cal	10.98	1026.4			
5/25/01 18 51	12.0	wart	10.98	1026.4			
5/25/01 18 51	16.0	wart	10.98	1026.4			
5/25/01 18 52	60.1	wart	10.98	1026.4			
5/25/01 18 52	154.3	wart	10.98	1026.4			
5/25/01 18 52	214.4	wart	10.98	1026.4			
5/25/01 18 52	270.5	wart	10.98	1026.4			
5/25/01 18 53	288.5	wart	10.98	1026.4			
5/25/01 18 53	292.5	301.9 ppm cal	10.98	1026.4			
5/25/01 18 53	294.5	301.9 ppm cal	10.98	1026.4			
5/25/01 18 53	294.5	301.9 ppm cal	10.98	1026.4			
5/25/01 18 54	292.5	301.9 ppm cal	10.98	1026.4			
5/25/01 18 54	292.5	301.9 ppm cal	10.98	1026.4			
5/25/01 18 54	294.5	301.9 ppm cal	10.98	1026.4			
5/25/01 18 54	294.5	301.9 ppm cal	10.98	1026.4			
5/25/01 18 55	292.5	301.9 ppm cal	10.98	1026.4			
5/25/01 18 55	286.5	wart	10.98	1026.4			
5/25/01 18 55	298.5	wart	10.98	1026.4			
5/25/01 18 55	440.8	wart	10.98	1026.4			
5/25/01 18 56	545.0	wart	10.98	1026.4			
5/25/01 18 56	575.1	wart	10.98	1026.4			
5/25/01 18 56	579.1	wart	10.98	1026.4			
5/25/01 18 56	581.1	594.7 ppm cal	10.98	1026.4			
5/25/01 18 57	583.1	594.7 ppm cal	10.98	1026.4			
5/25/01 18 57	583.1	594.7 ppm cal	10.98	1026.4			
5/25/01 18 57	581.1	594.7 ppm cal	10.98	1026.4			
5/25/01 18 57	581.1	594.7 ppm cal	10.98	1026.4			
5/25/01 18 58	581.1	594.7 ppm cal	10.98	1026.4			
5/25/01 18 58	581.1	594.7 ppm cal	10.98	1026.4			
5/25/01 18 58	643.2	wart	10.98	1026.4			
5/25/01 18 58	939.8	wart	10.98	1026.4			
5/25/01 18 59	1070.1	wart	10.98	1026.4			
5/25/01 18 59	1118.2	wart	10.98	1026.4			
5/25/01 21 37	12.0	0 ppm cal	11.982	1021.8			
5/25/01 21 37	12.0	0 ppm cal	11.982	1021.8			
5/25/01 21 38	12.0	0 ppm cal	11.982	1021.8			
5/25/01 21 38	12.0	0 ppm cal	11.982	1021.8			
5/25/01 21 38	12.0	0 ppm cal	11.982	1021.8			
5/25/01 21 38	12.0	0 ppm cal	11.982	1021.8			
5/25/01 21 39	12.0	0 ppm cal	11.982	1021.8			

## Georgia Pacific Bleach Plant - Carbon Monoxide Test

DATE / TIME	FEET	COMMENTS	ZERO CAL	1015 ppm cal	CORRECTED PPM	FLOW, act/m dry	POUNDS OF COPPER HOUR
5/25/01 21 39	12 0	0 ppm cal	11 982	1021 8			
5/25/01 21 39	14 0	wait	11 982	1021 8			
5/25/01 21 39	212 4	wait	11 982	1021 8			
5/25/01 21 40	649 2	wait	11 982	1021 8			
5/25/01 21 40	959 9	wait	11 982	1021 8			
5/25/01 21 40	1010 0	wait	11 982	1021 8			
5/25/01 21 40	1014 0		11 982	1021 8			
5/25/01 21 41	1018 0	1015 ppm cal	11 982	1021 8			
5/25/01 21 41	1018 0	1015 ppm cal	11 982	1021 8			
5/25/01 21 41	1012 0	1015 ppm cal	11 982	1021 8			
5/25/01 21 41	1018 0	1015 ppm cal	11 982	1021 8			
5/25/01 21 42	1020 0	1015 ppm cal	11 982	1021 8			
5/25/01 21 42	1014 0	1015 ppm cal	11 982	1021 8			
5/25/01 21 42	1018 0	1015 ppm cal	11 982	1021 8			
5/25/01 21 42	1018 0	1015 ppm cal	11 982	1021 8			
5/25/01 21 43	1014 0	1015 ppm cal	11 982	1021 8			
5/25/01 21 43	1020 0	1015 ppm cal	11 982	1021 8			
5/25/01 21 43	1016 0	1015 ppm cal	11 982	1021 8			
5/25/01 21 43	1014 0	1015 ppm cal	11 982	1021 8			
5/25/01 21 44	1018 0	1015 ppm cal	11 982	1021 8			
5/25/01 21 44	1008 0	wait	11 982	1021 8			
5/25/01 21 44	933 8	wait	11 982	1021 8			
5/25/01 21 44	729 4	wait	11 982	1021 8			
5/25/01 21 45	611 2	wait	11 982	1021 8			
5/25/01 21 45	581 1	wait	11 982	1021 8			
5/25/01 21 45	575 1	594 7 ppm cal	11 982	1018 2			
5/25/01 21 45	575 1	594 7 ppm cal	11 982	1018 2			
5/25/01 21 46	577 1	594 7 ppm cal	11 982	1018 2			
5/25/01 21 46	575 1	594 7 ppm cal	11 982	1018 2			
5/25/01 21 46	577 1	594 7 ppm cal	11 982	1018 2			
5/25/01 21 46	573 1	594 7 ppm cal	11 982	1018 2			
5/25/01 21 47	573 1	594 7 ppm cal	11 982	1018 2			
5/25/01 21 47	581 1	wait	11 982	1018 2			
5/25/01 21 47	601 1	wait	11 982	1018 2			
5/25/01 21 47	675 3	wait	11 982	1018 2			
5/25/01 21 48	701 3	wait	11 982	1018 2			
5/25/01 21 48	713 4	wait	11 982	1018 2			
5/25/01 21 48	721 4	wait	11 982	1018 2			
5/25/01 21 48	723 4	wait	11 982	1018 2			
5/25/01 21 49	717 4	wait	11 982	1018 2			
5/25/01 21 49	717 4	wait	11 982	1018 2			
5/25/01 21 49	719 4	wait	11 982	1018 2			
5/25/01 21 49	719 4	wait	11 982	1018 2			
5/25/01 21 50	715 4	run 1	11 982	1018 2	709 5	14183	43 9
5/25/01 21 50	713 4	run 1	11 982	1018 2	707 5	14183	43 8
5/25/01 21 50	711 4	run 1	11 982	1018 2	705 5	14183	43 7
5/25/01 21 50	709 4	run 1	11 982	1018 2	703 5	14183	43 5
5/25/01 21 51	705 4	run 1	11 982	1018 2	699 4	14183	43 3
5/25/01 21 51	695 3	run 1	11 982	1018 2	689 3	14183	42 7
5/25/01 21 51	695 3	run 1	11 982	1018 2	689 3	14183	42 7
5/25/01 21 51	697 3	run 1	11 982	1018 2	691 3	14183	42 8
5/25/01 21 52	687 3	run 1	11 982	1018 2	681 2	14183	42 2
5/25/01 21 52	679 3	run 1	11 982	1018 2	673 2	14183	41 7
5/25/01 21 52	683 3	run 1	11 982	1018 2	677 2	14183	41 9
5/25/01 21 52	687 3	run 1	11 982	1018 2	681 2	14183	42 2
5/25/01 21 53	687 3	run 1	11 982	1018 2	681 2	14183	42 2
5/25/01 21 53	691 3	run 1	11 982	1018 2	685 3	14183	42 4
5/25/01 21 53	691 3	run 1	11 982	1018 2	685 3	14183	42 4
5/25/01 21 53	685 3	run 1	11 982	1018 2	679 2	14183	42 0
5/25/01 21 54	587 3	run 1	11 982	1018 2	581 2	14183	42 2
5/25/01 21 54	583 3	run 1	11 982	1018 2	577 2	14183	41 9

### Georgia Pacific Bleach Plant - Carbon Monoxide Test

DATE / TIME	PPM	COMMENTS	ZERO CAL	1018 ppm Cal	CORRECTED PPM	FLOW scfm dry	POUNDS OF CO PER HOUR
5/25/01 21 54	675.3	N.S.	11.982	1018.2	669.1	14183	41.4
5/25/01 21 54	669.3	N.S.	11.982	1018.2	663.0	14183	41.0
5/25/01 21 55	669.3	N.S.	11.982	1018.2	663.0	14183	41.0
5/25/01 21 55	675.3	N.S.	11.982	1018.2	669.1	14183	41.4
5/25/01 21 55	673.3	N.S.	11.982	1018.2	667.1	14183	41.3
5/25/01 21 55	665.3	N.S.	11.982	1018.2	659.0	14183	40.8
5/25/01 21 56	669.3	N.S.	11.982	1018.2	663.0	14183	41.0
5/25/01 21 56	679.3	N.S.	11.982	1018.2	673.2	14183	41.7
5/25/01 21 56	675.3	N.S.	11.982	1018.2	669.1	14183	41.4
5/25/01 21 56	675.3	N.S.	11.982	1018.2	669.1	14183	41.4
5/25/01 21 57	679.3	N.S.	11.982	1018.2	673.2	14183	41.7
5/25/01 21 57	673.3	N.S.	11.982	1018.2	667.1	14183	41.3
5/25/01 21 57	667.3	N.S.	11.982	1018.2	661.0	14183	40.9
5/25/01 21 57	663.3	N.S.	11.982	1018.2	657.0	14183	40.5
5/25/01 21 58	667.3	N.S.	11.982	1018.2	661.0	14183	40.9
5/25/01 21 58	663.3	N.S.	11.982	1018.2	657.0	14183	40.6
5/25/01 21 58	655.3	N.S.	11.982	1018.2	648.9	14183	40.1
5/25/01 21 58	655.3	N.S.	11.982	1018.2	648.9	14183	40.1
5/25/01 21 59	661.3	N.S.	11.982	1018.2	655.0	14183	40.5
5/25/01 21 59	649.2	N.S.	11.982	1018.2	642.8	14183	39.8
5/25/01 21 59	633.2	N.S.	11.982	1018.2	626.7	14183	38.8
5/25/01 21 59	639.2	N.S.	11.982	1018.2	632.7	14183	39.1
5/25/01 22 00	647.2	N.S.	11.982	1018.2	640.8	14183	39.6
5/25/01 22 00	641.2	N.S.	11.982	1018.2	634.7	14183	39.3
5/25/01 22 00	639.2	N.S.	11.982	1018.2	632.7	14183	39.1
5/25/01 22 00	651.2	N.S.	11.982	1018.2	644.9	14183	39.9
5/25/01 22 01	655.3	N.S.	11.982	1018.2	648.9	14183	40.1
5/25/01 22 01	657.3	N.S.	11.982	1018.2	650.9	14183	40.3
5/25/01 22 01	665.3	N.S.	11.982	1018.2	659.0	14183	40.8
5/25/01 22 01	675.3	N.S.	11.982	1018.2	669.1	14183	41.4
5/25/01 22 02	685.3	N.S.	11.982	1018.2	679.2	14183	42.0
5/25/01 22 02	693.3	N.S.	11.982	1018.2	687.3	14183	42.5
5/25/01 22 02	693.3	N.S.	11.982	1018.2	687.3	14183	42.5
5/25/01 22 02	691.3	N.S.	11.982	1018.2	685.3	14183	42.4
5/25/01 22 03	693.3	N.S.	11.982	1018.2	687.3	14183	42.5
5/25/01 22 03	697.3	N.S.	11.982	1018.2	691.3	14183	42.8
5/25/01 22 03	697.3	N.S.	11.982	1018.2	691.3	14183	42.8
5/25/01 22 03	705.4	N.S.	11.982	1018.2	699.4	14183	43.3
5/25/01 22 04	705.4	N.S.	11.982	1018.2	699.4	14183	43.3
5/25/01 22 04	695.3	N.S.	11.982	1018.2	689.3	14183	42.7
5/25/01 22 04	685.3	N.S.	11.982	1018.2	679.2	14183	42.0
5/25/01 22 04	677.3	N.S.	11.982	1018.2	671.1	14183	41.5
5/25/01 22 05	669.3	N.S.	11.982	1018.2	663.0	14183	41.0
5/25/01 22 05	667.3	N.S.	11.982	1018.2	661.0	14183	40.9
5/25/01 22 05	667.3	N.S.	11.982	1018.2	661.0	14183	40.9
5/25/01 22 05	663.3	N.S.	11.982	1018.2	657.0	14183	40.6
5/25/01 22 06	659.3	N.S.	11.982	1018.2	652.9	14183	40.4
5/25/01 22 06	657.3	N.S.	11.982	1018.2	650.9	14183	40.3
5/25/01 22 06	651.2	N.S.	11.982	1018.2	644.9	14183	39.9
5/25/01 22 06	643.2	N.S.	11.982	1018.2	636.8	14183	39.4
5/25/01 22 07	647.2	N.S.	11.982	1018.2	640.8	14183	39.6
5/25/01 22 07	655.3	N.S.	11.982	1018.2	648.9	14183	40.1
5/25/01 22 07	653.2	N.S.	11.982	1018.2	646.9	14183	40.0
5/25/01 22 07	651.2	N.S.	11.982	1018.2	644.9	14183	39.9
5/25/01 22 08	655.3	N.S.	11.982	1018.2	648.9	14183	40.1
5/25/01 22 08	657.3	N.S.	11.982	1018.2	650.9	14183	40.3
5/25/01 22 08	653.2	N.S.	11.982	1018.2	646.9	14183	40.0
5/25/01 22 08	655.3	N.S.	11.982	1018.2	648.9	14183	40.1
5/25/01 22 09	663.3	N.S.	11.982	1018.2	657.0	14183	40.6
5/25/01 22 09	669.3	N.S.	11.982	1018.2	663.0	14183	41.0
5/25/01 22 09	665.3	N.S.	11.982	1018.2	659.0	14183	40.8

### Georgia Pacific Bleach Plant - Carbon Monoxide Test

DATE / TIME	PPM	COMMENTS	ZERO CAL	10 IS PPM CAL	CORRECTED PPM	FLOW, scfm, dry	POUNDS OF CO PER HOUR
5/25/01 22 09	663.3		11.982	1018.2	557.0	14183	40.6
5/25/01 22 10	671.3		11.982	1018.2	665.1	14183	41.2
5/25/01 22 10	679.3		11.982	1018.2	673.2	14183	41.7
5/25/01 22 10	679.3		11.982	1018.2	673.2	14183	41.7
5/25/01 22 10	681.3		11.982	1018.2	675.2	14183	41.8
5/25/01 22 11	683.3		11.982	1018.2	677.2	14183	41.9
5/25/01 22 11	677.3		11.982	1018.2	671.1	14183	41.5
5/25/01 22 11	675.3		11.982	1018.2	669.1	14183	41.4
5/25/01 22 11	677.3		11.982	1018.2	671.1	14183	41.5
5/25/01 22 12	667.3		11.982	1018.2	661.0	14183	40.9
5/25/01 22 12	681.3		11.982	1018.2	655.0	14183	40.5
5/25/01 22 12	665.3		11.982	1018.2	659.0	14183	40.8
5/25/01 22 12	665.3		11.982	1018.2	659.0	14183	40.8
5/25/01 22 13	667.3		11.982	1018.2	661.0	14183	40.9
5/25/01 22 13	671.3		11.982	1018.2	665.1	14183	41.2
5/25/01 22 13	671.3		11.982	1018.2	665.1	14183	41.2
5/25/01 22 13	675.3		11.982	1018.2	669.1	14183	41.4
5/25/01 22 14	681.3		11.982	1018.2	675.2	14183	41.8
5/25/01 22 14	681.3		11.982	1018.2	675.2	14183	41.8
5/25/01 22 14	673.3		11.982	1018.2	667.1	14183	41.3
5/25/01 22 14	671.3		11.982	1018.2	665.1	14183	41.2
5/25/01 22 15	677.3		11.982	1018.2	671.1	14183	41.5
5/25/01 22 15	683.3		11.982	1018.2	677.2	14183	41.9
5/25/01 22 15	683.3		11.982	1018.2	677.2	14183	41.9
5/25/01 22 15	677.3		11.982	1018.2	671.1	14183	41.5
5/25/01 22 16	671.3		11.982	1018.2	665.1	14183	41.2
5/25/01 22 16	669.3		11.982	1018.2	663.0	14183	41.0
5/25/01 22 16	667.3		11.982	1018.2	661.0	14183	40.9
5/25/01 22 16	667.3		11.982	1018.2	661.0	14183	40.9
5/25/01 22 17	669.3		11.982	1018.2	663.0	14183	41.0
5/25/01 22 17	669.3		11.982	1018.2	663.0	14183	41.0
5/25/01 22 17	675.3		11.982	1018.2	669.1	14183	41.4
5/25/01 22 17	679.3		11.982	1018.2	673.2	14183	41.7
5/25/01 22 18	679.3		11.982	1018.2	673.2	14183	41.7
5/25/01 22 18	675.3		11.982	1018.2	669.1	14183	41.4
5/25/01 22 18	673.3		11.982	1018.2	667.1	14183	41.3
5/25/01 22 18	675.3		11.982	1018.2	669.1	14183	41.4
5/25/01 22 19	679.3		11.982	1018.2	673.2	14183	41.7
5/25/01 22 19	679.3		11.982	1018.2	673.2	14183	41.7
5/25/01 22 19	681.3		11.982	1018.2	675.2	14183	41.8
5/25/01 22 19	685.3		11.982	1018.2	679.2	14183	42.0
5/25/01 22 20	685.3		11.982	1018.2	679.2	14183	42.0
5/25/01 22 20	681.3		11.982	1018.2	675.2	14183	41.8
5/25/01 22 20	675.3		11.982	1018.2	669.1	14183	41.4
5/25/01 22 20	673.3		11.982	1018.2	667.1	14183	41.3
5/25/01 22 21	671.3		11.982	1018.2	665.1	14183	41.2
5/25/01 22 21	669.3		11.982	1018.2	663.0	14183	41.0
5/25/01 22 21	669.3		11.982	1018.2	663.0	14183	41.0
5/25/01 22 21	669.3		11.982	1018.2	663.0	14183	41.0
5/25/01 22 22	671.3		11.982	1018.2	665.1	14183	41.2
5/25/01 22 22	675.3		11.982	1018.2	669.1	14183	41.4
5/25/01 22 22	677.3		11.982	1018.2	671.1	14183	41.5
5/25/01 22 22	679.3		11.982	1018.2	673.2	14183	41.7
5/25/01 22 23	679.3		11.982	1018.2	673.2	14183	41.7
5/25/01 22 23	681.3		11.982	1018.2	675.2	14183	41.8
5/25/01 22 23	679.3		11.982	1018.2	673.2	14183	41.7
5/25/01 22 23	683.3		11.982	1018.2	677.2	14183	41.9
5/25/01 22 24	689.3		11.982	1018.2	683.3	14183	42.3
5/25/01 22 24	693.3		11.982	1018.2	687.3	14183	42.5
5/25/01 22 24	687.3		11.982	1018.2	681.2	14183	42.2
5/25/01 22 24	689.3		11.982	1018.2	683.3	14183	42.3

## Georgia Pacific Bleach Plant - Carbon Monoxide Test

DATE / TIME	PPM	COMMENTS	ZERO CAL	1018 ppm cal	CORRECTED PPM	FLOW, acfm dry	POUNDS OF CO PER HOUR
5/25/01 22:25	687.3	run 1	11.982	1018.2	581.2	14183	42.2
5/25/01 22:25	681.3	run 1	11.982	1018.2	575.2	14183	41.8
5/25/01 22:25	685.3	run 1	11.982	1018.2	679.2	14183	42.0
5/25/01 22:25	683.3	run 1	11.982	1018.2	677.2	14183	41.9
5/25/01 22:26	679.3	run 1	11.982	1018.2	673.2	14183	41.7
5/25/01 22:26	679.3	run 1	11.982	1018.2	573.2	14183	41.7
5/25/01 22:26	679.3	run 1	11.982	1018.2	673.2	14183	41.7
5/25/01 22:26	687.3	run 1	11.982	1018.2	581.2	14183	42.2
5/25/01 22:27	693.3	run 1	11.982	1018.2	587.3	14183	42.5
5/25/01 22:27	695.3	run 1	11.982	1018.2	589.3	14183	42.7
5/25/01 22:27	695.3	run 1	11.982	1018.2	589.3	14183	42.7
5/25/01 22:27	697.3	run 1	11.982	1018.2	691.3	14183	42.8
5/25/01 22:28	699.3	run 1	11.982	1018.2	693.4	14183	42.9
5/25/01 22:28	697.3	run 1	11.982	1018.2	691.3	14183	42.8
5/25/01 22:28	695.3	run 1	11.982	1018.2	689.3	14183	42.7
5/25/01 22:28	695.3	run 1	11.982	1018.2	689.3	14183	42.7
5/25/01 22:29	697.3	run 1	11.982	1018.2	691.3	14183	42.8
5/25/01 22:29	697.3	run 1	11.982	1018.2	691.3	14183	42.8
5/25/01 22:29	699.3	run 1	11.982	1018.2	693.4	14183	42.9
5/25/01 22:29	709.4	run 1	11.982	1018.2	703.5	14183	43.5
5/25/01 22:30	717.4	run 1	11.982	1018.2	711.6	14183	44.0
5/25/01 22:30	711.4	run 1	11.982	1018.2	705.5	14183	43.7
5/25/01 22:30	703.3	run 1	11.982	1018.2	697.4	14183	43.2
5/25/01 22:30	701.3	run 1	11.982	1018.2	595.4	14183	43.0
5/25/01 22:31	695.3	run 1	11.982	1018.2	589.3	14183	42.7
5/25/01 22:31	693.3	run 1	11.982	1018.2	587.3	14183	42.5
5/25/01 22:31	695.3	run 1	11.982	1018.2	689.3	14183	42.7
5/25/01 22:31	697.3	run 1	11.982	1018.2	691.3	14183	42.8
5/25/01 22:32	695.3	run 1	11.982	1018.2	689.3	14183	42.7
5/25/01 22:32	693.3	run 1	11.982	1018.2	687.3	14183	42.5
5/25/01 22:32	687.3	run 1	11.982	1018.2	681.2	14183	42.2
5/25/01 22:32	681.3	run 1	11.982	1018.2	675.2	14183	41.8
5/25/01 22:33	673.3	run 1	11.982	1018.2	667.1	14183	41.3
5/25/01 22:33	671.3	run 1	11.982	1018.2	665.1	14183	41.2
5/25/01 22:33	669.3	run 1	11.982	1018.2	663.0	14183	41.0
5/25/01 22:33	655.3	run 1	11.982	1018.2	648.9	14183	40.1
5/25/01 22:34	647.2	run 1	11.982	1018.2	640.8	14183	39.6
5/25/01 22:34	647.2	run 1	11.982	1018.2	640.8	14183	39.6
5/25/01 22:34	641.2	run 1	11.982	1018.2	634.7	14183	39.3
5/25/01 22:34	639.2	run 1	11.982	1018.2	632.7	14183	39.1
5/25/01 22:35	639.2	run 1	11.982	1018.2	632.7	14183	39.1
5/25/01 22:35	641.2	run 1	11.982	1018.2	634.7	14183	39.3
5/25/01 22:35	641.2	run 1	11.982	1018.2	634.7	14183	39.3
5/25/01 22:36	647.2	run 1	11.982	1018.2	640.8	14183	39.6
5/25/01 22:36	655.3	run 1	11.982	1018.2	648.9	14183	40.1
5/25/01 22:36	661.3	run 1	11.982	1018.2	655.0	14183	40.5
5/25/01 22:36	665.3	run 1	11.982	1018.2	659.0	14183	40.8
5/25/01 22:37	657.3	run 1	11.982	1018.2	650.9	14183	40.3
5/25/01 22:37	657.3	run 1	11.982	1018.2	650.9	14183	40.3
5/25/01 22:37	663.3	run 1	11.982	1018.2	657.0	14183	40.6
5/25/01 22:37	659.3	run 1	11.982	1018.2	652.9	14183	40.4
5/25/01 22:38	655.3	run 1	11.982	1018.2	648.9	14183	40.1
5/25/01 22:38	663.3	run 1	11.982	1018.2	657.0	14183	40.6
5/25/01 22:38	667.3	run 1	11.982	1018.2	661.0	14183	40.9
5/25/01 22:38	667.3	run 1	11.982	1018.2	661.0	14183	40.9
5/25/01 22:39	661.3	run 1	11.982	1018.2	655.0	14183	40.5
5/25/01 22:39	655.3	run 1	11.982	1018.2	648.9	14183	40.1
5/25/01 22:39	657.3	run 1	11.982	1018.2	650.9	14183	40.3
5/25/01 22:39	661.3	run 1	11.982	1018.2	655.0	14183	40.5
5/25/01 22:40	657.3	run 1	11.982	1018.2	650.9	14183	40.3

### Georgia Pacific Bleach Plant - Carbon Monoxide Test

DATE / TIME	PPM	COMMENTS	ZERO CAL	1015 ppm cal	CORRECTED PPM	FLOW active-dry	POUNDS OF CO PER HOUR
5/25/01 22 40	657.3	run 1	11.982	1018.2	650.9	14183	40.3
5/25/01 22 40	657.3	run 1	11.982	1018.2	650.9	14183	40.3
5/25/01 22 40	661.3	run 1	11.982	1018.2	655.0	14183	40.5
5/25/01 22 41	669.3	run 1	11.982	1018.2	663.0	14183	41.0
5/25/01 22 41	673.3	run 1	11.982	1018.2	667.1	14183	41.3
5/25/01 22 41	673.3	run 1	11.982	1018.2	667.1	14183	41.3
5/25/01 22 41	675.3	run 1	11.982	1018.2	669.1	14183	41.4
5/25/01 22 42	679.3	run 1	11.982	1018.2	673.2	14183	41.7
5/25/01 22 42	677.3	run 1	11.982	1018.2	671.1	14183	41.5
5/25/01 22 42	669.3	run 1	11.982	1018.2	663.0	14183	41.0
5/25/01 22 42	663.3	run 1	11.982	1018.2	657.0	14183	40.6
5/25/01 22 43	659.3	run 1	11.982	1018.2	652.9	14183	40.4
5/25/01 22 43	659.3	run 1	11.982	1018.2	652.9	14183	40.4
5/25/01 22 43	663.3	run 1	11.982	1018.2	657.0	14183	40.6
5/25/01 22 43	667.3	run 1	11.982	1018.2	661.0	14183	40.9
5/25/01 22 44	677.3	run 1	11.982	1018.2	671.1	14183	41.5
5/25/01 22 44	683.3	run 1	11.982	1018.2	677.2	14183	41.9
5/25/01 22 44	683.3	run 1	11.982	1018.2	677.2	14183	41.9
5/25/01 22 44	681.3	run 1	11.982	1018.2	675.2	14183	41.8
5/25/01 22 45	685.3	run 1	11.982	1018.2	679.2	14183	42.0
5/25/01 22 45	697.3	run 1	11.982	1018.2	691.3	14183	42.8
5/25/01 22 45	699.3	run 1	11.982	1018.2	693.4	14183	42.9
5/25/01 22 45	691.3	run 1	11.982	1018.2	685.3	14183	42.4
5/25/01 22 46	687.3	run 1	11.982	1018.2	681.2	14183	42.2
5/25/01 22 46	697.3	run 1	11.982	1018.2	691.3	14183	42.8
5/25/01 22 46	703.3	run 1	11.982	1018.2	697.4	14183	43.2
5/25/01 22 46	701.3	run 1	11.982	1018.2	695.4	14183	43.0
5/25/01 22 47	699.3	run 1	11.982	1018.2	693.4	14183	42.9
5/25/01 22 47	701.3	run 1	11.982	1018.2	695.4	14183	43.0
5/25/01 22 47	703.3	run 1	11.982	1018.2	697.4	14183	43.2
5/25/01 22 47	705.4	run 1	11.982	1018.2	699.4	14183	43.3
5/25/01 22 48	705.4	run 1	11.982	1018.2	699.4	14183	43.3
5/25/01 22 48	701.3	run 1	11.982	1018.2	695.4	14183	43.0
5/25/01 22 48	695.3	run 1	11.982	1018.2	689.3	14183	42.7
5/25/01 22 48	697.3	run 1	11.982	1018.2	691.3	14183	42.8
5/25/01 22 49	705.4	run 1	11.982	1018.2	699.4	14183	43.3
5/25/01 22 49	703.3	run 1	11.982	1018.2	697.4	14183	43.2
5/25/01 22 49	699.3	run 1	11.982	1018.2	693.4	14183	42.9
5/25/01 22 49	705.4	run 1	11.982	1018.2	699.4	14183	43.3
5/25/01 22 50	711.4	wait	11.982	1018.2			
5/25/01 22 50	711.4	wait	11.982	1018.2			
5/25/01 22 50	711.4	wait	11.982	1018.2			
5/25/01 22 50	713.4	wait	11.982	1018.2			
5/25/01 22 51	701.3	wait	11.982	1018.2			
5/25/01 22 51	703.3	wait	11.982	1018.2			
5/25/01 22 51	701.3	wait	11.982	1018.2			
5/25/01 22 51	689.3	wait	11.982	1018.2			
5/25/01 22 52	757.5	wait	11.982	1018.2			
5/25/01 22 52	909.8	wait	11.982	1018.2			
5/25/01 22 52	993.9	wait	11.982	1018.2			
5/25/01 22 52	1014.0	wait	11.982	1018.2			
5/25/01 22 53	1016.0	1015 ppm cal	11.982	1018.2			
5/25/01 22 53	1016.0	1015 ppm cal	11.982	1018.2			
5/25/01 22 53	1016.0	1015 ppm cal	11.65	1026.2			
5/25/01 22 53	1016.0	1015 ppm cal	11.65	1026.2			
5/25/01 22 54	1016.0	1015 ppm cal	11.65	1026.2			
5/25/01 22 54	1014.0	wait	11.65	1026.2			
5/25/01 22 54	1010.0	wait	11.65	1026.2			
5/25/01 22 54	1012.0	wait	11.65	1026.2			
5/25/01 22 55	995.9	wait	11.65	1026.2			
5/25/01 22 55	963.7	wait	11.65	1026.2			

## Georgia Pacific Bleach Plant - Carbon Monoxide Test

DATE / TIME	PPM	COMMENTS	ZERO CAL	1018 ppm cal	CORRECTED PPM	FLOW, scfm, dry	POUNDS OF CO PER HOUR
5/25/01 22 55	679.3	wart	11.85	1026.2			
5/25/01 22 55	593.1	wart	11.85	1026.2			
5/25/01 22 56	581.1	594.7 ppm cal	11.85	1026.2			
5/25/01 22 56	581.1	594.7 ppm cal	11.85	1026.2			
5/25/01 22 56	579.1	594.7 ppm cal	11.85	1026.2			
5/25/01 22 56	577.1	594.7 ppm cal	11.85	1026.2			
5/25/01 22 57	577.1	594.7 ppm cal	11.85	1026.2			
5/25/01 22 57	577.1	594.7 ppm cal	11.85	1026.2			
5/25/01 22 57	490.9	wart	11.85	1026.2			
5/25/01 22 57	232.4	wart	11.85	1026.2			
5/25/01 22 58	60.1	wart	11.85	1026.2			
5/25/01 22 58	16.0	wart	11.85	1026.2			
5/25/01 22 58	12.0	0 ppm cal	11.85	1026.2			
5/25/01 22 58	12.0	0 ppm cal	11.85	1026.2			
5/25/01 22 59	12.0	0 ppm cal	11.85	1026.2			
5/25/01 22 59	12.0	0 ppm cal	11.85	1026.2			
5/25/01 22 59	12.0	0 ppm cal	11.85	1026.2			
5/25/01 22 59	12.0	0 ppm cal	11.85	1026.2			
5/25/01 23 00	12.0	0 ppm cal	11.85	1026.2			
5/25/01 23 00	12.0	0 ppm cal	11.85	1026.2			
5/25/01 23 00	12.0	0 ppm cal	11.85	1026.2			
5/25/01 23 00	82.1	wart	11.85	1026.2			
5/25/01 23 01	362.7	wart	11.85	1026.2			
5/25/01 23 01	613.2	wart	11.85	1026.2			
5/25/01 23 01	671.3	wart	11.85	1026.2			
5/25/01 23 01	671.3	wart	11.85	1026.2			
5/25/01 23 02	677.3	run 2	11.85	1026.2	665.9	14406	41.9
5/25/01 23 02	677.3	run 2	11.85	1026.2	665.9	14406	41.9
5/25/01 23 02	677.3	run 2	11.85	1026.2	665.9	14406	41.9
5/25/01 23 02	681.3	run 2	11.85	1026.2	669.9	14406	42.1
5/25/01 23 03	683.3	run 2	11.85	1026.2	671.9	14406	42.2
5/25/01 23 03	683.3	run 2	11.85	1026.2	671.9	14406	42.2
5/25/01 23 03	587.3	run 2	11.85	1026.2	675.9	14406	42.5
5/25/01 23 03	693.3	run 2	11.85	1026.2	682.0	14406	42.9
5/25/01 23 04	693.3	run 2	11.85	1026.2	682.0	14406	42.9
5/25/01 23 04	703.3	run 2	11.85	1026.2	692.0	14406	43.5
5/25/01 23 04	709.4	run 2	11.85	1026.2	698.0	14406	43.9
5/25/01 23 04	706.4	run 2	11.85	1026.2	694.0	14406	43.6
5/25/01 23 05	703.3	run 2	11.85	1026.2	692.0	14406	43.5
5/25/01 23 05	706.4	run 2	11.85	1026.2	694.0	14406	43.6
5/25/01 23 05	706.4	run 2	11.85	1026.2	694.0	14406	43.6
5/25/01 23 05	706.4	run 2	11.85	1026.2	694.0	14406	43.6
5/25/01 23 06	701.3	run 2	11.85	1026.2	690.0	14406	43.4
5/25/01 23 06	701.3	run 2	11.85	1026.2	690.0	14406	43.4
5/25/01 23 06	699.3	run 2	11.85	1026.2	688.0	14406	43.2
5/25/01 23 06	699.3	run 2	11.85	1026.2	688.0	14406	43.2
5/25/01 23 07	696.3	run 2	11.85	1026.2	684.0	14406	43.0
5/25/01 23 07	699.3	run 2	11.85	1026.2	688.0	14406	43.2
5/25/01 23 07	703.3	run 2	11.85	1026.2	692.0	14406	43.5
5/25/01 23 07	703.3	run 2	11.85	1026.2	692.0	14406	43.5
5/25/01 23 08	706.4	run 2	11.85	1026.2	694.0	14406	43.6
5/25/01 23 08	711.4	run 2	11.85	1026.2	700.0	14406	44.0
5/25/01 23 08	715.4	run 2	11.85	1026.2	704.0	14406	44.2
5/25/01 23 08	711.4	run 2	11.85	1026.2	700.0	14406	44.0
5/25/01 23 09	713.4	run 2	11.85	1026.2	702.0	14406	44.1
5/25/01 23 09	719.4	run 2	11.85	1026.2	708.0	14406	44.5
5/25/01 23 09	713.4	run 2	11.85	1026.2	702.0	14406	44.1
5/25/01 23 09	713.4	run 2	11.85	1026.2	702.0	14406	44.1
5/25/01 23 10	711.4	run 2	11.85	1026.2	700.0	14406	44.0
5/25/01 23 10	706.4	run 2	11.85	1026.2	694.0	14406	43.5
5/25/01 23 10	706.4	run 2	11.85	1026.2	698.0	14406	43.9

## Georgia Pacific Bleach Plant - Carbon Monoxide Test

DATE / TIME	PPM	COMMENTS	ZERO CAL	1018 ppm cal	CORRECTED PPM	FLOW actm- day	POUNDS OF CO PER HOUR
5/25/01 23 10	707.4	run 2	11.65	1026.2	696.0	14406	43.7
5/25/01 23 11	705.4	run 2	11.65	1026.2	694.0	14406	43.6
5/25/01 23 11	707.4	run 2	11.65	1026.2	696.0	14406	43.7
5/25/01 23 11	707.4	run 2	11.65	1026.2	696.0	14406	43.7
5/25/01 23 11	703.3	run 2	11.65	1026.2	692.0	14406	43.5
5/25/01 23 12	701.3	run 2	11.65	1026.2	690.0	14406	43.4
5/25/01 23 12	705.4	run 2	11.65	1026.2	694.0	14406	43.6
5/25/01 23 12	705.4	run 2	11.65	1026.2	694.0	14406	43.6
5/25/01 23 12	701.3	run 2	11.65	1026.2	690.0	14406	43.4
5/25/01 23 13	703.3	run 2	11.65	1026.2	692.0	14406	43.5
5/25/01 23 13	699.3	run 2	11.65	1026.2	688.0	14406	43.2
5/25/01 23 13	697.3	run 2	11.65	1026.2	686.0	14406	43.1
5/25/01 23 13	701.3	run 2	11.65	1026.2	690.0	14406	43.4
5/25/01 23 14	699.3	run 2	11.65	1026.2	688.0	14406	43.2
5/25/01 23 14	699.3	run 2	11.65	1026.2	688.0	14406	43.2
5/25/01 23 14	701.3	run 2	11.65	1026.2	690.0	14406	43.4
5/25/01 23 14	701.3	run 2	11.65	1026.2	690.0	14406	43.4
5/25/01 23 15	703.3	run 2	11.65	1026.2	692.0	14406	43.5
5/25/01 23 15	699.3	run 2	11.65	1026.2	688.0	14406	43.2
5/25/01 23 15	695.3	run 2	11.65	1026.2	684.0	14406	43.0
5/25/01 23 15	695.3	run 2	11.65	1026.2	684.0	14406	43.0
5/25/01 23 16	703.3	run 2	11.65	1026.2	692.0	14406	43.5
5/25/01 23 16	705.4	run 2	11.65	1026.2	694.0	14406	43.6
5/25/01 23 16	713.4	run 2	11.65	1026.2	702.0	14406	44.1
5/25/01 23 16	723.4	run 2	11.65	1026.2	712.0	14406	44.7
5/25/01 23 17	725.4	run 2	11.65	1026.2	714.0	14406	44.9
5/25/01 23 17	729.4	run 2	11.65	1026.2	718.0	14406	45.1
5/25/01 23 17	731.4	run 2	11.65	1026.2	720.1	14406	45.3
5/25/01 23 17	737.4	run 2	11.65	1026.2	726.1	14406	45.6
5/25/01 23 18	737.4	run 2	11.65	1026.2	726.1	14406	45.6
5/25/01 23 18	737.4	run 2	11.65	1026.2	726.1	14406	45.6
5/25/01 23 18	733.4	run 2	11.65	1026.2	722.1	14406	45.4
5/25/01 23 18	737.4	run 2	11.65	1026.2	726.1	14406	45.6
5/25/01 23 19	733.4	run 2	11.65	1026.2	722.1	14406	45.4
5/25/01 23 19	727.4	run 2	11.65	1026.2	716.0	14406	45.0
5/25/01 23 19	725.4	run 2	11.65	1026.2	714.0	14406	44.9
5/25/01 23 19	725.4	run 2	11.65	1026.2	714.0	14406	44.9
5/25/01 23 20	731.4	run 2	11.65	1026.2	720.1	14406	45.3
5/25/01 23 20	725.4	run 2	11.65	1026.2	714.0	14406	44.9
5/25/01 23 20	719.4	run 2	11.65	1026.2	708.0	14406	44.5
5/25/01 23 20	721.4	run 2	11.65	1026.2	710.0	14406	44.6
5/25/01 23 21	723.4	run 2	11.65	1026.2	712.0	14406	44.7
5/25/01 23 21	725.4	run 2	11.65	1026.2	714.0	14406	44.9
5/25/01 23 21	727.4	run 2	11.65	1026.2	716.0	14406	45.0
5/25/01 23 21	723.4	run 2	11.65	1026.2	712.0	14406	44.7
5/25/01 23 22	721.4	run 2	11.65	1026.2	710.0	14406	44.6
5/25/01 23 22	725.4	run 2	11.65	1026.2	714.0	14406	44.9
5/25/01 23 22	721.4	run 2	11.65	1026.2	710.0	14406	44.6
5/25/01 23 22	717.4	run 2	11.65	1026.2	706.0	14406	44.4
5/25/01 23 23	719.4	run 2	11.65	1026.2	708.0	14406	44.5
5/25/01 23 23	723.4	run 2	11.65	1026.2	712.0	14406	44.7
5/25/01 23 23	725.4	run 2	11.65	1026.2	714.0	14406	44.9
5/25/01 23 23	731.4	run 2	11.65	1026.2	720.1	14406	45.3
5/25/01 23 24	727.4	run 2	11.65	1026.2	716.0	14406	45.0
5/25/01 23 24	735.4	run 2	11.65	1026.2	724.1	14406	45.5
5/25/01 23 24	759.5	run 2	11.65	1026.2	748.1	14406	47.0
5/25/01 23 24	767.5	run 2	11.65	1026.2	756.1	14406	47.5
5/25/01 23 25	767.5	run 2	11.65	1026.2	756.1	14406	47.5
5/25/01 23 25	761.5	run 2	11.65	1026.2	750.1	14406	47.1
5/25/01 23 25	759.5	run 2	11.65	1026.2	748.1	14406	47.0
5/25/01 23 25	761.5	run 2	11.65	1026.2	750.1	14406	47.1



**Georgia Pacific Bleach Plant - Carbon Monoxide Test**

DATE / TIME	FEET	COMMENTS	ZERO CAL	TOTAL ppm cal	CORRECTED ppm	FLOW, acim dry	POUNDS OF CO PER HOUR
5/25/01 23 26	763.5	run 2	11.65	1026.2	752.1	14406	47.3
5/25/01 23 26	763.5	run 2	11.65	1026.2	752.1	14406	47.3
5/25/01 23 26	759.5	run 2	11.65	1026.2	748.1	14406	47.0
5/25/01 23 26	753.4	run 2	11.65	1026.2	742.1	14406	46.5
5/25/01 23 27	753.4	run 2	11.65	1026.2	742.1	14406	46.5
5/25/01 23 27	759.5	run 2	11.65	1026.2	748.1	14406	47.0
5/25/01 23 27	763.5	run 2	11.65	1026.2	752.1	14406	47.3
5/25/01 23 27	759.5	run 2	11.65	1026.2	748.1	14406	47.0
5/25/01 23 28	759.5	run 2	11.65	1026.2	748.1	14406	47.0
5/25/01 23 28	761.5	run 2	11.65	1026.2	750.1	14406	47.1
5/25/01 23 28	761.5	run 2	11.65	1026.2	750.1	14406	47.1
5/25/01 23 28	763.5	run 2	11.65	1026.2	752.1	14406	47.3
5/25/01 23 29	787.5	run 2	11.65	1026.2	756.1	14406	47.5
5/25/01 23 29	777.5	run 2	11.65	1026.2	766.2	14406	48.2
5/25/01 23 29	783.5	run 2	11.65	1026.2	772.2	14406	48.5
5/25/01 23 29	775.5	run 2	11.65	1026.2	764.2	14406	48.0
5/25/01 23 30	787.5	run 2	11.65	1026.2	756.1	14406	47.5
5/25/01 23 30	787.5	run 2	11.65	1026.2	756.1	14406	47.5
5/25/01 23 30	789.5	run 2	11.65	1026.2	758.1	14406	47.6
5/25/01 23 30	775.5	run 2	11.65	1026.2	764.2	14406	48.0
5/25/01 23 31	793.5	run 2	11.65	1026.2	782.2	14406	49.2
5/25/01 23 31	801.5	run 2	11.65	1026.2	790.2	14406	49.7
5/25/01 23 31	797.5	run 2	11.65	1026.2	786.2	14406	49.4
5/25/01 23 31	793.5	run 2	11.65	1026.2	782.2	14406	49.2
5/25/01 23 32	787.5	run 2	11.65	1026.2	776.2	14406	48.8
5/25/01 23 32	785.5	run 2	11.65	1026.2	774.2	14406	48.7
5/25/01 23 32	783.5	run 2	11.65	1026.2	772.2	14406	48.5
5/25/01 23 32	779.5	run 2	11.65	1026.2	768.2	14406	48.3
5/25/01 23 33	781.5	run 2	11.65	1026.2	770.2	14406	48.4
5/25/01 23 33	785.5	run 2	11.65	1026.2	774.2	14406	48.7
5/25/01 23 33	781.5	run 2	11.65	1026.2	770.2	14406	48.4
5/25/01 23 33	781.5	run 2	11.65	1026.2	770.2	14406	48.4
5/25/01 23 34	787.5	run 2	11.65	1026.2	776.2	14406	48.8
5/25/01 23 34	791.5	run 2	11.65	1026.2	780.2	14406	49.0
5/25/01 23 34	795.5	run 2	11.65	1026.2	784.2	14406	49.3
5/25/01 23 34	799.5	run 2	11.65	1026.2	788.2	14406	49.5
5/25/01 23 35	803.5	run 2	11.65	1026.2	792.2	14406	49.8
5/25/01 23 35	803.5	run 2	11.65	1026.2	792.2	14406	49.8
5/25/01 23 35	809.6	run 2	11.65	1026.2	798.2	14406	50.2
5/25/01 23 35	811.6	run 2	11.65	1026.2	800.2	14406	50.3
5/25/01 23 36	795.5	run 2	11.65	1026.2	784.2	14406	49.3
5/25/01 23 36	789.5	run 2	11.65	1026.2	778.2	14406	48.9
5/25/01 23 36	811.6	run 2	11.65	1026.2	800.2	14406	50.3
5/25/01 23 36	831.6	run 2	11.65	1026.2	820.3	14406	51.6
5/25/01 23 37	847.6	run 2	11.65	1026.2	836.3	14406	52.6
5/25/01 23 37	851.6	run 2	11.65	1026.2	840.3	14406	52.8
5/25/01 23 37	847.6	run 2	11.65	1026.2	836.3	14406	52.6
5/25/01 23 37	847.6	run 2	11.65	1026.2	836.3	14406	52.6
5/25/01 23 38	853.6	run 2	11.65	1026.2	842.3	14406	52.9
5/25/01 23 38	871.7	run 2	11.65	1026.2	860.4	14406	54.1
5/25/01 23 38	883.7	run 2	11.65	1026.2	872.4	14406	54.8
5/25/01 23 38	879.7	run 2	11.65	1026.2	868.4	14406	54.6
5/25/01 23 39	869.7	run 2	11.65	1026.2	858.4	14406	53.9
5/25/01 23 39	869.7	run 2	11.65	1026.2	858.4	14406	53.9
5/25/01 23 39	875.7	run 2	11.65	1026.2	864.4	14406	54.3
5/25/01 23 39	869.7	run 2	11.65	1026.2	858.4	14406	53.9
5/25/01 23 40	859.7	run 2	11.65	1026.2	848.4	14406	53.3
5/25/01 23 40	859.7	run 2	11.65	1026.2	848.4	14406	53.3
5/25/01 23 40	855.6	run 2	11.65	1026.2	844.3	14406	53.1
5/25/01 23 40	855.6	run 2	11.65	1026.2	844.3	14406	53.1
5/25/01 23 41	851.5	run 2	11.65	1026.2	840.3	14406	52.8

### Georgia Pacific Bleach Plant - Carbon Monoxide Test

DATE / TIME	PPM	COMMENTS	ZERO CAL	1018 ppm cal	CORRECTED PPM	FLOW scfm dry	POUNDS OF CO PER HOUR
5/25/01 23 41	847.6	run 2	11.65	1026.2	838.3	14406	52.6
5/25/01 23 41	851.6	run 2	11.65	1026.2	840.3	14406	52.8
5/25/01 23 41	851.6	run 2	11.65	1026.2	840.3	14406	52.8
5/25/01 23 42	849.6	run 2	11.65	1026.2	838.3	14406	52.7
5/25/01 23 42	853.6	run 2	11.65	1026.2	842.3	14406	52.9
5/25/01 23 42	859.7	run 2	11.65	1026.2	848.4	14406	53.3
5/25/01 23 42	857.7	run 2	11.65	1026.2	846.4	14406	53.2
5/25/01 23 43	851.6	run 2	11.65	1026.2	840.3	14406	52.8
5/25/01 23 43	853.6	run 2	11.65	1026.2	842.3	14406	52.9
5/25/01 23 43	853.6	run 2	11.65	1026.2	842.3	14406	52.9
5/25/01 23 43	849.6	run 2	11.65	1026.2	838.3	14406	52.7
5/25/01 23 44	851.6	run 2	11.65	1026.2	840.3	14406	52.8
5/25/01 23 44	857.7	run 2	11.65	1026.2	846.4	14406	53.2
5/25/01 23 44	869.7	run 2	11.65	1026.2	858.4	14406	53.9
5/25/01 23 44	865.7	run 2	11.65	1026.2	874.4	14406	55.3
5/25/01 23 45	895.7	run 2	11.65	1026.2	984.4	14406	56.6
5/25/01 23 45	889.7	run 2	11.65	1026.2	878.4	14406	55.2
5/25/01 23 45	885.7	run 2	11.65	1026.2	874.4	14406	55.0
5/25/01 23 45	889.7	run 2	11.65	1026.2	878.4	14406	55.2
5/25/01 23 46	879.7	run 2	11.65	1026.2	868.4	14406	54.6
5/25/01 23 46	857.7	run 2	11.65	1026.2	846.4	14406	53.2
5/25/01 23 46	839.6	run 2	11.65	1026.2	828.3	14406	52.1
5/25/01 23 46	837.6	run 2	11.65	1026.2	826.3	14406	51.9
5/25/01 23 47	835.6	run 2	11.65	1026.2	824.3	14406	51.8
5/25/01 23 47	835.6	run 2	11.65	1026.2	824.3	14406	51.8
5/25/01 23 47	831.6	run 2	11.65	1026.2	820.3	14406	51.6
5/25/01 23 47	825.6	run 2	11.65	1026.2	814.3	14406	51.2
5/25/01 23 48	825.6	run 2	11.65	1026.2	814.3	14406	51.2
5/25/01 23 48	829.6	run 2	11.65	1026.2	818.3	14406	51.4
5/25/01 23 48	829.6	run 2	11.65	1026.2	818.3	14406	51.4
5/25/01 23 48	829.6	run 2	11.65	1026.2	818.3	14406	51.4
5/25/01 23 49	829.6	run 2	11.65	1026.2	818.3	14406	51.4
5/25/01 23 49	829.6	run 2	11.65	1026.2	818.3	14406	51.4
5/25/01 23 49	829.6	run 2	11.65	1026.2	818.3	14406	51.4
5/25/01 23 49	833.6	run 2	11.65	1026.2	822.3	14406	51.7
5/25/01 23 49	839.6	run 2	11.65	1026.2	828.3	14406	52.1
5/25/01 23 50	833.6	run 2	11.65	1026.2	822.3	14406	51.7
5/25/01 23 50	823.6	run 2	11.65	1026.2	812.3	14406	51.0
5/25/01 23 50	823.6	run 2	11.65	1026.2	812.3	14406	51.0
5/25/01 23 50	827.6	run 2	11.65	1026.2	816.3	14406	51.3
5/25/01 23 51	825.6	run 2	11.65	1026.2	814.3	14406	51.2
5/25/01 23 51	829.6	run 2	11.65	1026.2	818.3	14406	51.4
5/25/01 23 51	829.6	run 2	11.65	1026.2	818.3	14406	51.4
5/25/01 23 51	827.6	run 2	11.65	1026.2	816.3	14406	51.3
5/25/01 23 52	829.6	run 2	11.65	1026.2	818.3	14406	51.4
5/25/01 23 52	831.6	run 2	11.65	1026.2	820.3	14406	51.6
5/25/01 23 52	829.6	run 2	11.65	1026.2	818.3	14406	51.4
5/25/01 23 52	823.6	run 2	11.65	1026.2	812.3	14406	51.0
5/25/01 23 53	815.6	run 2	11.65	1026.2	804.3	14406	50.5
5/25/01 23 53	813.6	run 2	11.65	1026.2	802.2	14406	50.4
5/25/01 23 53	813.6	run 2	11.65	1026.2	802.2	14406	50.4
5/25/01 23 53	811.5	run 2	11.65	1026.2	800.2	14406	50.3
5/25/01 23 54	809.5	run 2	11.55	1026.2	798.2	14406	50.2
5/25/01 23 54	811.5	run 2	11.65	1026.2	800.2	14406	50.3
5/25/01 23 54	815.6	run 2	11.65	1026.2	804.3	14406	50.5
5/25/01 23 54	817.6	run 2	11.65	1026.2	806.3	14406	50.7
5/25/01 23 55	813.6	run 2	11.55	1026.2	802.2	14406	50.4
5/25/01 23 55	809.6	run 2	11.55	1026.2	798.2	14406	50.2
5/25/01 23 55	805.6	run 2	11.55	1026.2	794.2	14406	49.9
5/25/01 23 55	803.5	run 2	11.55	1026.2	792.2	14406	49.8
5/25/01 23 56	809.6	run 2	11.65	1026.2	798.2	14406	50.2
5/25/01 23 56	815.6	run 2	11.65	1026.2	804.3	14406	50.5

## Georgia Pacific Bleach Plant - Carbon Monoxide Test

DATE / TIME	PPM	COMMENTS	ZERO CAL	1015 ppm cal	CORRECTED PPM	FLOW, scfm, dry	POUNDS OF COPPER HOUR
5/25/01 23 56	815.6	run 2	11.65	1026.2	804.3	14406	50.5
5/25/01 23 56	815.6	run 2	11.65	1026.2	804.3	14406	50.5
5/25/01 23 57	821.6	run 2	11.65	1026.2	810.3	14406	50.9
5/25/01 23 57	829.6	run 2	11.65	1026.2	818.3	14406	51.4
5/25/01 23 57	835.6	run 2	11.65	1026.2	824.3	14406	51.8
5/25/01 23 57	837.6	run 2	11.65	1026.2	826.3	14406	51.9
5/25/01 23 58	833.6	run 2	11.65	1026.2	822.3	14406	51.7
5/25/01 23 58	829.6	run 2	11.65	1026.2	818.3	14406	51.4
5/25/01 23 58	827.6	run 2	11.65	1026.2	816.3	14406	51.3
5/25/01 23 58	829.6	run 2	11.65	1026.2	818.3	14406	51.4
5/25/01 23 59	825.6	run 2	11.65	1026.2	814.3	14406	51.2
5/25/01 23 59	815.6	run 2	11.65	1026.2	804.3	14406	50.5
5/25/01 23 59	805.6	run 2	11.65	1026.2	794.2	14406	49.9
5/25/01 23 59	801.5	run 2	11.65	1026.2	790.2	14406	49.7
5/26/01 0 00	799.5	run 2	11.65	1026.2	788.2	14406	49.5
5/26/01 0 00	803.5	run 2	11.65	1026.2	792.2	14406	49.8
5/26/01 0 00	803.5	run 2	11.65	1026.2	792.2	14406	49.8
5/26/01 0 00	805.6	run 2	11.65	1026.2	794.2	14406	49.9
5/26/01 0 01	805.6	run 2	11.65	1026.2	794.2	14406	49.9
5/26/01 0 01	805.6	run 2	11.65	1026.2	794.2	14406	49.9
5/26/01 0 01	815.6	run 2	11.65	1026.2	804.3	14406	50.5
5/26/01 0 01	829.6	run 2	11.65	1026.2	818.3	14406	51.4
5/26/01 0 02	823.6	wait	11.65	1026.2			
5/26/01 0 02	815.6	wait	11.65	1026.2			
5/26/01 0 02	789.5	wait	11.65	1026.2			
5/26/01 0 02	739.4	wait	11.65	1026.2			
5/26/01 0 03	887.7	wait	11.65	1026.2			
5/26/01 0 03	1597.1	wait	11.65	1026.2			
5/26/01 0 03	1959.8	wait	11.65	1026.2			
5/26/01 0 03	1959.8	wait	11.65	1026.2			
5/26/01 0 04	1362.7	wait	11.65	1026.2			
5/26/01 0 04	478.9	wait	11.65	1026.2			
5/26/01 0 04	85.1	wait	11.65	1026.2			
5/26/01 0 04	18.0	wait	11.65	1026.2			
5/26/01 0 05	12.0	0 ppm cal	11.65	1026.2			
5/26/01 0 05	12.0	0 ppm cal	11.65	1026.2			
5/26/01 0 05	12.0	0 ppm cal	11.65	1026.2			
5/26/01 0 05	10.0	0 ppm cal	11.65	1026.2			
5/26/01 0 05	10.0	0 ppm cal	11.65	1026.2			
5/26/01 0 05	12.0	0 ppm cal	11.65	1026.2			
5/26/01 0 05	16.0	wait	11.65	1026.2			
5/26/01 0 05	126.2	wait	11.65	1026.2			
5/26/01 0 07	595.1	wait	11.65	1026.2			
5/26/01 0 07	909.8	wait	11.65	1026.2			
5/26/01 0 07	1030.0	1015 ppm cal	11.65	1026.2			
5/26/01 0 07	1038.0	1015 ppm cal	11.65	1026.2			
5/26/01 0 08	1036.0	1015 ppm cal	11.65	1026.2			
5/26/01 0 08	1026.0	1015 ppm cal	11.65	1026.2			
5/26/01 0 08	935.8	wait	11.047	1032.0			
5/26/01 0 08	765.5	wait	11.047	1032.0			
5/26/01 0 09	635.2	wait	11.047	1032.0			
5/26/01 0 09	607.2	wait	11.047	1032.0			
5/26/01 0 09	603.2	wait	11.047	1032.0			
5/26/01 0 09	601.1	wait	11.047	1032.0			
5/26/01 0 10	601.1	wait	11.047	1032.0			
5/26/01 0 10	595.1	wait	11.047	1032.0			
5/26/01 0 10	657.3	wait	11.047	1032.0			
5/26/01 0 10	725.4	wait	11.047	1032.0			
5/26/01 0 11	806.6	wait	11.047	1032.0			
5/26/01 0 11	835.6	wait	11.047	1032.0			
5/26/01 0 11	845.6	wait	11.047	1032.0			

### Georgia Pacific Bleach Plant - Carbon Monoxide Test

DATE / TIME	PPM	COMMENTS	ZERO CAL	1019 ppm cal	CORRECTED PPM	FLOW, scfm dry	POUNDS OF CO PER HOUR
5/26/01 0 11	847.8	wait	11 047	1032.0			
5/26/01 0 12	845.8	run 3a	11 047	1032.0	829.7	1433.1	51.9
5/26/01 0 12	841.8	run 3a	11 047	1032.0	825.7	1433.1	51.8
5/26/01 0 12	845.8	run 3a	11 047	1032.0	829.7	1433.1	51.9
5/26/01 0 12	851.8	run 3a	11 047	1032.0	835.7	1433.1	52.2
5/26/01 0 13	957.7	run 3a	11 047	1032.0	841.5	1433.1	52.6
5/26/01 0 13	853.8	run 3a	11 047	1032.0	837.5	1433.1	52.4
5/26/01 0 13	847.8	run 3a	11 047	1032.0	831.7	1433.1	52.0
5/26/01 0 13	845.8	run 3a	11 047	1032.0	829.7	1433.1	51.9
5/26/01 0 14	843.8	run 3a	11 047	1032.0	827.7	1433.1	51.7
5/26/01 0 14	843.8	run 3a	11 047	1032.0	827.7	1433.1	51.7
5/26/01 0 14	845.8	run 3a	11 047	1032.0	829.7	1433.1	51.9
5/26/01 0 14	849.8	run 3a	11 047	1032.0	833.7	1433.1	52.1
5/26/01 0 15	851.8	run 3a	11 047	1032.0	835.7	1433.1	52.2
5/26/01 0 15	849.8	run 3a	11 047	1032.0	833.7	1433.1	52.1
5/26/01 0 15	845.8	run 3a	11 047	1032.0	829.7	1433.1	51.9
5/26/01 0 15	847.8	run 3a	11 047	1032.0	831.7	1433.1	52.0
5/26/01 0 16	853.8	run 3a	11 047	1032.0	837.5	1433.1	52.4
5/26/01 0 16	855.8	run 3a	11 047	1032.0	839.5	1433.1	52.5
5/26/01 0 16	849.8	run 3a	11 047	1032.0	833.7	1433.1	52.1
5/26/01 0 16	853.8	run 3a	11 047	1032.0	837.5	1433.1	52.4
5/26/01 0 17	871.7	run 3a	11 047	1032.0	855.5	1433.1	53.5
5/26/01 0 17	871.7	run 3a	11 047	1032.0	855.5	1433.1	53.5
5/26/01 0 17	869.7	run 3a	11 047	1032.0	853.5	1433.1	53.4
5/26/01 0 17	869.7	run 3a	11 047	1032.0	853.5	1433.1	53.4
5/26/01 0 18	865.7	run 3a	11 047	1032.0	849.5	1433.1	53.1
5/26/01 0 18	867.7	run 3a	11 047	1032.0	851.5	1433.1	53.2
5/26/01 0 18	875.7	run 3a	11 047	1032.0	859.5	1433.1	53.7
5/26/01 0 18	873.7	run 3a	11 047	1032.0	857.5	1433.1	53.6
5/26/01 0 19	861.7	run 3a	11 047	1032.0	845.5	1433.1	52.9
5/26/01 0 19	857.7	run 3a	11 047	1032.0	841.5	1433.1	52.6
5/26/01 0 19	861.7	run 3a	11 047	1032.0	845.5	1433.1	52.9
5/26/01 0 19	861.7	run 3a	11 047	1032.0	845.5	1433.1	52.9
5/26/01 0 20	863.7	run 3a	11 047	1032.0	847.5	1433.1	53.0
5/26/01 0 20	869.7	run 3a	11 047	1032.0	853.5	1433.1	53.4
5/26/01 0 20	869.7	run 3a	11 047	1032.0	853.5	1433.1	53.4
5/26/01 0 20	869.7	run 3a	11 047	1032.0	853.5	1433.1	53.4
5/26/01 0 21	865.7	run 3a	11 047	1032.0	849.5	1433.1	53.1
5/26/01 0 21	863.7	run 3a	11 047	1032.0	847.5	1433.1	53.0
5/26/01 0 21	871.7	run 3a	11 047	1032.0	855.5	1433.1	53.5
5/26/01 0 21	877.7	run 3a	11 047	1032.0	861.5	1433.1	53.9
5/26/01 0 22	879.7	run 3a	11 047	1032.0	863.5	1433.1	54.0
5/26/01 0 22	877.7	run 3a	11 047	1032.0	861.5	1433.1	53.9
5/26/01 0 22	883.7	run 3a	11 047	1032.0	867.5	1433.1	54.2
5/26/01 0 22	887.7	run 3a	11 047	1032.0	871.5	1433.1	54.5
5/26/01 0 23	881.7	run 3a	11 047	1032.0	865.5	1433.1	54.1
5/26/01 0 23	877.7	run 3a	11 047	1032.0	861.5	1433.1	53.9
5/26/01 0 23	879.7	run 3a	11 047	1032.0	863.5	1433.1	54.0
5/26/01 0 23	881.7	run 3a	11 047	1032.0	865.5	1433.1	54.1
5/26/01 0 24	887.7	run 3a	11 047	1032.0	871.5	1433.1	54.5
5/26/01 0 24	891.7	run 3a	11 047	1032.0	875.5	1433.1	54.7
5/26/01 0 24	891.7	run 3a	11 047	1032.0	875.5	1433.1	54.7
5/26/01 0 24	895.7	run 3a	11 047	1032.0	879.5	1433.1	55.0
5/26/01 0 25	917.8	run 3a	11 047	1032.0	901.4	1433.1	56.4
5/26/01 0 25	913.8	run 3a	11 047	1032.0	897.4	1433.1	56.1
5/26/01 0 25	901.7	run 3a	11 047	1032.0	885.5	1433.1	55.4
5/26/01 0 25	893.7	run 3a	11 047	1032.0	877.5	1433.1	54.9
5/26/01 0 26	899.7	run 3a	11 047	1032.0	883.5	1433.1	55.2
5/26/01 0 26	905.7	run 3a	11 047	1032.0	889.5	1433.1	55.6
5/26/01 0 26	899.7	run 3a	11 047	1032.0	883.5	1433.1	55.2
5/26/01 0 26	899.7	run 3a	11 047	1032.0	883.5	1433.1	55.2

### Georgia Pacific Bleach Plant - Carbon Monoxide Test

DATE / TIME	PPM	COMMENTS	ZERO CAL	1018 ppm cel	CORRECTED PPM	FLOW acfm dry	POUNDS OF COPPER HOUR
5/26/01 0 27	893.7	run 3a	11 047	1032.0	877.5	14331	54.5
5/26/01 0 27	887.7	run 3a	11 047	1032.0	871.5	14331	54.5
5/26/01 0 27	891.7	run 3a	11 047	1032.0	875.5	14331	54.7
5/26/01 0 27	895.7	run 3a	11 047	1032.0	879.5	14331	55.0
5/26/01 0 28	893.7	run 3a	11 047	1032.0	877.5	14331	54.9
5/26/01 0 28	889.7	run 3a	11 047	1032.0	873.5	14331	54.6
5/26/01 0 28	887.7	run 3a	11 047	1032.0	871.5	14331	54.5
5/26/01 0 28	885.7	run 3a	11 047	1032.0	873.5	14331	54.6
5/26/01 0 29	895.7	run 3a	11 047	1032.0	873.5	14331	54.6
5/26/01 0 29	891.7	run 3a	11 047	1032.0	875.5	14331	54.7
5/26/01 0 29	887.7	run 3a	11 047	1032.0	871.5	14331	54.5
5/26/01 0 29	881.7	run 3a	11 047	1032.0	865.5	14331	54.1
5/26/01 0 30	877.7	run 3a	11 047	1032.0	861.6	14331	53.9
5/26/01 0 30	877.7	run 3a	11 047	1032.0	861.6	14331	53.9
5/26/01 0 30	885.7	run 3a	11 047	1032.0	869.5	14331	54.4
5/26/01 0 30	891.7	run 3a	11 047	1032.0	875.5	14331	54.7
5/26/01 0 31	885.7	run 3a	11 047	1032.0	869.5	14331	54.4
5/26/01 0 31	887.7	run 3a	11 047	1032.0	871.5	14331	54.5
5/26/01 0 31	887.7	run 3a	11 047	1032.0	871.5	14331	54.5
5/26/01 0 31	877.7	run 3a	11 047	1032.0	861.6	14331	53.9
5/26/01 0 32	883.7	run 3a	11 047	1032.0	867.5	14331	54.2
5/26/01 0 32	889.7	run 3a	11 047	1032.0	873.5	14331	54.6
5/26/01 0 32	883.7	run 3a	11 047	1032.0	867.5	14331	54.2
5/26/01 0 32	875.7	run 3a	11 047	1032.0	859.6	14331	53.7
5/26/01 0 33	871.7	run 3a	11 047	1032.0	855.6	14331	53.5
5/26/01 0 33	869.7	run 3a	11 047	1032.0	853.6	14331	53.4
5/26/01 0 33	867.7	run 3a	11 047	1032.0	851.6	14331	53.2
5/26/01 0 33	871.7	run 3a	11 047	1032.0	856.6	14331	53.5
5/26/01 0 34	873.7	run 3a	11 047	1032.0	857.6	14331	53.6
5/26/01 0 34	879.7	run 3a	11 047	1032.0	863.5	14331	54.0
5/26/01 0 34	883.7	run 3a	11 047	1032.0	867.5	14331	54.2
5/26/01 0 34	879.7	run 3a	11 047	1032.0	863.5	14331	54.0
5/26/01 0 35	877.7	run 3a	11 047	1032.0	861.6	14331	53.9
5/26/01 0 35	879.7	run 3a	11 047	1032.0	863.5	14331	54.0
5/26/01 0 35	879.7	run 3a	11 047	1032.0	863.5	14331	54.0
5/26/01 0 35	873.7	run 3a	11 047	1032.0	857.6	14331	53.6
5/26/01 0 36	867.7	run 3a	11 047	1032.0	851.6	14331	53.2
5/26/01 0 36	869.7	run 3a	11 047	1032.0	853.6	14331	53.4
5/26/01 0 36	869.7	run 3a	11 047	1032.0	853.6	14331	53.4
5/26/01 0 36	865.7	run 3a	11 047	1032.0	849.6	14331	53.1
5/26/01 0 37	871.7	run 3a	11 047	1032.0	855.6	14331	53.5
5/26/01 0 37	879.7	run 3a	11 047	1032.0	863.5	14331	54.0
5/26/01 0 37	885.7	run 3a	11 047	1032.0	869.5	14331	54.4
5/26/01 0 37	885.7	run 3a	11 047	1032.0	869.5	14331	54.4
5/26/01 0 38	881.7	run 3a	11 047	1032.0	865.5	14331	54.1
5/26/01 0 38	877.7	run 3a	11 047	1032.0	861.6	14331	53.9
5/26/01 0 38	879.7	run 3a	11 047	1032.0	863.5	14331	54.0
5/26/01 0 38	875.7	run 3a	11 047	1032.0	859.6	14331	53.7
5/26/01 0 39	867.7	run 3a	11 047	1032.0	851.6	14331	53.2
5/26/01 0 39	865.7	run 3a	11 047	1032.0	849.6	14331	53.1
5/26/01 0 39	867.7	run 3a	11 047	1032.0	851.6	14331	53.2
5/26/01 0 39	871.7	run 3a	11 047	1032.0	855.6	14331	53.5
5/26/01 0 40	869.7	run 3a	11 047	1032.0	853.6	14331	53.4
5/26/01 0 40	865.7	run 3a	11 047	1032.0	849.6	14331	53.1
5/26/01 0 40	871.7	run 3a	11 047	1032.0	855.6	14331	53.5
5/26/01 0 40	869.7	run 3a	11 047	1032.0	853.6	14331	53.4
5/26/01 0 41	861.7	run 3a	11 047	1032.0	845.6	14331	52.9
5/26/01 0 41	855.6	run 3a	11 047	1032.0	839.6	14331	52.5
5/26/01 0 41	855.6	run 3a	11 047	1032.0	839.6	14331	52.5
5/26/01 0 41	851.6	run 3a	11 047	1032.0	835.6	14331	52.2
5/26/01 0 42	857.7	run 3a	11 047	1032.0	841.6	14331	52.6

### Georgia Pacific Bleach Plant - Carbon Monoxide Test

DATE / TIME	PPM	COMMENTS	ZERO CAL	1016 ppm cal	CORRECTED PPM	FLOW, scfm, dry	POUNDS OF CO PER HOUR
5/26/01 0 42	865.7	run 3a	11 047	1032.0	849.5	1433	52.1
5/26/01 0 42	845.6	run 3a	11 047	1032.0	829.7	1433	51.9
5/26/01 0 42	823.6	run 3a	11 047	1032.0	807.8	1433	50.5
		run 3a Average			856.9		52.5
5/26/01 0 43	813.6	plant upset/delay	11 047	1032.0			
5/26/01 0 43	823.6	plant upset/delay	11 047	1032.0			
5/26/01 0 43	831.6	plant upset/delay	11 047	1032.0			
5/26/01 0 43	823.6	plant upset/delay	11 047	1032.0			
5/26/01 0 44	817.6	plant upset/delay	11 047	1032.0			
5/26/01 0 44	815.6	plant upset/delay	11 047	1032.0			
5/26/01 0 44	813.6	plant upset/delay	11 047	1032.0			
5/26/01 0 44	807.6	plant upset/delay	11 047	1032.0			
5/26/01 0 45	811.8	plant upset/delay	11 047	1032.0			
5/26/01 0 45	825.6	plant upset/delay	11 047	1032.0			
5/26/01 0 45	833.6	plant upset/delay	11 047	1032.0			
5/26/01 0 45	829.6	plant upset/delay	11 047	1032.0			
5/26/01 0 46	825.6	plant upset/delay	11 047	1032.0			
5/26/01 0 46	823.6	plant upset/delay	11 047	1032.0			
5/26/01 0 46	813.6	plant upset/delay	11 047	1032.0			
5/26/01 0 46	799.5	plant upset/delay	11 047	1032.0			
5/26/01 0 47	793.5	plant upset/delay	11 047	1032.0			
5/26/01 0 47	791.5	plant upset/delay	11 047	1032.0			
5/26/01 0 47	789.5	plant upset/delay	11 047	1032.0			
5/26/01 0 47	781.5	plant upset/delay	11 047	1032.0			
5/26/01 0 48	777.5	plant upset/delay	11 047	1032.0			
5/26/01 0 48	781.5	plant upset/delay	11 047	1032.0			
5/26/01 0 48	783.5	plant upset/delay	11 047	1032.0			
5/26/01 0 48	777.5	plant upset/delay	11 047	1032.0			
5/26/01 0 49	781.5	plant upset/delay	11 047	1032.0			
5/26/01 0 49	787.5	plant upset/delay	11 047	1032.0			
5/26/01 0 49	783.5	plant upset/delay	11 047	1032.0			
5/26/01 0 49	777.5	plant upset/delay	11 047	1032.0			
5/26/01 0 50	781.5	plant upset/delay	11 047	1032.0			
5/26/01 0 50	785.5	plant upset/delay	11 047	1032.0			
5/26/01 0 50	785.5	plant upset/delay	11 047	1032.0			
5/26/01 0 50	785.5	plant upset/delay	11 047	1032.0			
5/26/01 0 51	785.5	plant upset/delay	11 047	1032.0			
5/26/01 0 51	791.5	plant upset/delay	11 047	1032.0			
5/26/01 0 51	803.5	plant upset/delay	11 047	1032.0			
5/26/01 0 51	813.6	plant upset/delay	11 047	1032.0			
5/26/01 0 52	817.6	plant upset/delay	11 047	1032.0			
5/26/01 0 52	819.6	plant upset/delay	11 047	1032.0			
5/26/01 0 52	827.6	plant upset/delay	11 047	1032.0			
5/26/01 0 52	833.6	plant upset/delay	11 047	1032.0			
5/26/01 0 53	829.6	plant upset/delay	11 047	1032.0			
5/26/01 0 53	819.6	plant upset/delay	11 047	1032.0			
5/26/01 0 53	807.6	plant upset/delay	11 047	1032.0			
5/26/01 0 53	791.5	plant upset/delay	11 047	1032.0			
5/26/01 0 54	773.5	plant upset/delay	11 047	1032.0			
5/26/01 0 54	759.5	plant upset/delay	11 047	1032.0			
5/26/01 0 54	741.4	plant upset/delay	11 047	1032.0			
5/26/01 0 54	723.4	plant upset/delay	11 047	1032.0			
5/26/01 0 55	711.4	plant upset/delay	11 047	1032.0			
5/26/01 0 55	709.4	plant upset/delay	11 047	1032.0			
5/26/01 0 55	701.3	plant upset/delay	11 047	1032.0			
5/26/01 0 55	585.3	plant upset/delay	11 047	1032.0			
5/26/01 0 56	583.3	plant upset/delay	11 047	1032.0			
5/26/01 0 56	589.3	plant upset/delay	11 047	1032.0			
5/26/01 0 56	593.3	plant upset/delay	11 047	1032.0			
5/26/01 0 56	593.3	plant upset/delay	11 047	1032.0			
5/26/01 0 57	589.3	plant upset/delay	11 047	1032.0			

## Georgia Pacific Bleach Plant - Carbon Monoxide Test

DATE / TIME	PPM	COMMENTS	ZERO CAL	1016 ppm cal	CORRECTED PPM	FLOW scfm dry	MOUNUS UP (1) PPM HOUR
5/26/01 0 57	677.3	plant upset/delay	11.047	1032.0			
5/26/01 0 57	663.3	plant upset/delay	11.047	1032.0			
5/26/01 0 57	655.3	plant upset/delay	11.047	1032.0			
5/26/01 0 58	657.3	plant upset/delay	11.047	1032.0			
5/26/01 0 58	663.3	plant upset/delay	11.047	1032.0			
5/26/01 0 58	659.3	plant upset/delay	11.047	1032.0			
5/26/01 0 58	661.3	plant upset/delay	11.047	1032.0			
5/26/01 0 59	669.3	plant upset/delay	11.047	1032.0			
5/26/01 0 59	661.3	plant upset/delay	11.047	1032.0			
5/26/01 0 59	655.3	plant upset/delay	11.047	1032.0			
5/26/01 0 59	649.2	plant upset/delay	11.047	1032.0			
5/26/01 1 00	635.2	plant upset/delay	11.047	1032.0			
5/26/01 1 00	621.2	plant upset/delay	11.047	1032.0			
5/26/01 1 00	621.2	plant upset/delay	11.047	1032.0			
5/26/01 1 00	621.2	plant upset/delay	11.047	1032.0			
5/26/01 1 01	617.2	plant upset/delay	11.047	1032.0			
5/26/01 1 01	609.2	plant upset/delay	11.047	1032.0			
5/26/01 1 01	603.2	plant upset/delay	11.047	1032.0			
5/26/01 1 01	601.1	plant upset/delay	11.047	1032.0			
5/26/01 1 02	597.1	plant upset/delay	11.047	1032.0			
5/26/01 1 02	595.1	plant upset/delay	11.047	1032.0			
5/26/01 1 02	593.1	plant upset/delay	11.047	1032.0			
5/26/01 1 02	595.1	plant upset/delay	11.047	1032.0			
5/26/01 1 03	593.1	plant upset/delay	11.047	1032.0			
5/26/01 1 03	589.1	plant upset/delay	11.047	1032.0			
5/26/01 1 03	583.1	plant upset/delay	11.047	1032.0			
5/26/01 1 03	579.1	plant upset/delay	11.047	1032.0			
5/26/01 1 04	581.1	plant upset/delay	11.047	1032.0			
5/26/01 1 04	585.1	plant upset/delay	11.047	1032.0			
5/26/01 1 04	591.1	plant upset/delay	11.047	1032.0			
5/26/01 1 04	589.1	plant upset/delay	11.047	1032.0			
5/26/01 1 05	587.1	plant upset/delay	11.047	1032.0			
5/26/01 1 05	593.1	plant upset/delay	11.047	1032.0			
5/26/01 1 05	603.2	plant upset/delay	11.047	1032.0			
5/26/01 1 05	615.2	plant upset/delay	11.047	1032.0			
5/26/01 1 06	621.2	plant upset/delay	11.047	1032.0			
5/26/01 1 06	615.2	plant upset/delay	11.047	1032.0			
5/26/01 1 06	607.2	plant upset/delay	11.047	1032.0			
5/26/01 1 06	609.2	plant upset/delay	11.047	1032.0			
5/26/01 1 07	613.2	plant upset/delay	11.047	1032.0			
5/26/01 1 07	617.2	plant upset/delay	11.047	1032.0			
5/26/01 1 07	621.2	plant upset/delay	11.047	1032.0			
5/26/01 1 07	623.2	plant upset/delay	11.047	1032.0			
5/26/01 1 08	627.2	plant upset/delay	11.047	1032.0			
5/26/01 1 08	631.2	plant upset/delay	11.047	1032.0			
5/26/01 1 08	627.2	plant upset/delay	11.047	1032.0			
5/26/01 1 08	619.2	plant upset/delay	11.047	1032.0			
5/26/01 1 09	613.2	plant upset/delay	11.047	1032.0			
5/26/01 1 09	613.2	plant upset/delay	11.047	1032.0			
5/26/01 1 09	615.2	plant upset/delay	11.047	1032.0			
5/26/01 1 09	617.2	plant upset/delay	11.047	1032.0			
5/26/01 1 10	613.2	plant upset/delay	11.047	1032.0			
5/26/01 1 10	609.2	plant upset/delay	11.047	1032.0			
5/26/01 1 10	609.2	plant upset/delay	11.047	1032.0			
5/26/01 1 10	617.2	plant upset/delay	11.047	1032.0			
5/26/01 1 11	621.2	plant upset/delay	11.047	1032.0			
5/26/01 1 11	633.2	plant upset/delay	11.047	1032.0			
5/26/01 1 11	659.3	plant upset/delay	11.047	1032.0			
5/26/01 1 11	679.3	plant upset/delay	11.047	1032.0			
5/26/01 1 12	677.3	plant upset/delay	11.047	1032.0			
5/26/01 1 12	677.3	plant upset/delay	11.047	1032.0			

### Georgia Pacific Bleach Plant - Carbon Monoxide Test

DATE / TIME	PPM	COMMENTS	ZERO CAL	1010 ppm cal	CORRECTED PPM	FLOW, acfm, dry	POUNDS OF CO PER HOUR
5/26/01 1:12	685.3	plant upset/delay	11.047	1032.0			
5/26/01 1:12	697.3	plant upset/delay	11.047	1032.0			
5/26/01 1:13	697.3	plant upset/delay	11.047	1032.0			
5/26/01 1:13	693.3	plant upset/delay	11.047	1032.0			
5/26/01 1:13	687.3	plant upset/delay	11.047	1032.0			
5/26/01 1:13	683.3	plant upset/delay	11.047	1032.0			
5/26/01 1:14	679.3	plant upset/delay	11.047	1032.0			
5/26/01 1:14	681.3	plant upset/delay	11.047	1032.0			
5/26/01 1:14	679.3	plant upset/delay	11.047	1032.0			
5/26/01 1:14	675.3	plant upset/delay	11.047	1032.0			
5/26/01 1:15	683.3	plant upset/delay	11.047	1032.0			
5/26/01 1:15	685.3	plant upset/delay	11.047	1032.0			
5/26/01 1:15	685.3	plant upset/delay	11.047	1032.0			
5/26/01 1:15	685.3	plant upset/delay	11.047	1032.0			
5/26/01 1:16	681.3	plant upset/delay	11.047	1032.0			
5/26/01 1:16	677.3	plant upset/delay	11.047	1032.0			
5/26/01 1:16	673.3	plant upset/delay	11.047	1032.0			
5/26/01 1:16	675.3	plant upset/delay	11.047	1032.0			
5/26/01 1:17	679.3	plant upset/delay	11.047	1032.0			
5/26/01 1:17	679.3	plant upset/delay	11.047	1032.0			
5/26/01 1:17	679.3	plant upset/delay	11.047	1032.0			
5/26/01 1:17	671.3	plant upset/delay	11.047	1032.0			
5/26/01 1:18	669.3	plant upset/delay	11.047	1032.0			
5/26/01 1:18	665.3	plant upset/delay	11.047	1032.0			
5/26/01 1:18	669.3	plant upset/delay	11.047	1032.0			
5/26/01 1:18	671.3	plant upset/delay	11.047	1032.0			
5/26/01 1:19	667.3	plant upset/delay	11.047	1032.0			
5/26/01 1:19	665.3	plant upset/delay	11.047	1032.0			
5/26/01 1:19	665.3	plant upset/delay	11.047	1032.0			
5/26/01 1:19	671.3	plant upset/delay	11.047	1032.0			
5/26/01 1:20	673.3	plant upset/delay	11.047	1032.0			
5/26/01 1:20	671.3	plant upset/delay	11.047	1032.0			
5/26/01 1:20	673.3	plant upset/delay	11.047	1032.0			
5/26/01 1:20	679.3	plant upset/delay	11.047	1032.0			
5/26/01 1:21	679.3	plant upset/delay	11.047	1032.0			
5/26/01 1:21	675.3	plant upset/delay	11.047	1032.0			
5/26/01 1:21	671.3	plant upset/delay	11.047	1032.0			
5/26/01 1:21	673.3	plant upset/delay	11.047	1032.0			
5/26/01 1:22	677.3	plant upset/delay	11.047	1032.0			
5/26/01 1:22	681.3	plant upset/delay	11.047	1032.0			
5/26/01 1:22	683.3	plant upset/delay	11.047	1032.0			
5/26/01 1:22	697.3	plant upset/delay	11.047	1032.0			
5/26/01 1:23	707.4	plant upset/delay	11.047	1032.0			
5/26/01 1:23	711.4	plant upset/delay	11.047	1032.0			
5/26/01 1:23	705.4	plant upset/delay	11.047	1032.0			
5/26/01 1:23	705.4	plant upset/delay	11.047	1032.0			
5/26/01 1:24	709.4	plant upset/delay	11.047	1032.0			
5/26/01 1:24	711.4	plant upset/delay	11.047	1032.0			
5/26/01 1:24	709.4	plant upset/delay	11.047	1032.0			
5/26/01 1:24	707.4	plant upset/delay	11.047	1032.0			
5/26/01 1:25	705.4	plant upset/delay	11.047	1032.0			
5/26/01 1:25	701.3	plant upset/delay	11.047	1032.0			
5/26/01 1:25	697.3	plant upset/delay	11.047	1032.0			
5/26/01 1:25	583.3	plant upset/delay	11.047	1032.0			
5/26/01 1:26	571.3	plant upset/delay	11.047	1032.0			
5/26/01 1:26	575.3	plant upset/delay	11.047	1032.0			
5/26/01 1:26	679.3	plant upset/delay	11.047	1032.0			
5/26/01 1:26	569.3	plant upset/delay	11.047	1032.0			
5/26/01 1:27	565.3	plant upset/delay	11.047	1032.0			
5/26/01 1:27	563.3	plant upset/delay	11.047	1032.0			
5/26/01 1:27	561.3	plant upset/delay	11.047	1032.0			



### Georgia Pacific Bleach Plant - Carbon Monoxide Test

DATE / TIME	PIN	COMMENTS	ZERO CAL	1018 ppm Cal	CORRECTED PPM	FLOW, scfm dry	POUNDS OF CO PER HOUR
5/26/01 1:27	667 3	plant upset/delay	11.047	1032.0			
5/26/01 1:28	667 3	plant upset/delay	11.047	1032.0			
5/26/01 1:28	661 3	plant upset/delay	11.047	1032.0			
5/26/01 1:28	661 3	plant upset/delay	11.047	1032.0			
5/26/01 1:28	665 3	plant upset/delay	11.047	1032.0			
5/26/01 1:29	661 3	plant upset/delay	11.047	1032.0			
5/26/01 1:29	653 2	plant upset/delay	11.047	1032.0			
5/26/01 1:29	655 3	plant upset/delay	11.047	1032.0			
5/26/01 1:29	659 3	plant upset/delay	11.047	1032.0			
5/26/01 1:30	659 3	plant upset/delay	11.047	1032.0			
5/26/01 1:30	659 3	plant upset/delay	11.047	1032.0			
5/26/01 1:30	665 3	plant upset/delay	11.047	1032.0			
5/26/01 1:30	669 3	plant upset/delay	11.047	1032.0			
5/26/01 1:31	665 3	plant upset/delay	11.047	1032.0			
5/26/01 1:31	659 3	plant upset/delay	11.047	1032.0			
5/26/01 1:31	653 2	plant upset/delay	11.047	1032.0			
5/26/01 1:31	653 2	plant upset/delay	11.047	1032.0			
5/26/01 1:32	659 3	plant upset/delay	11.047	1032.0			
5/26/01 1:32	667 3	plant upset/delay	11.047	1032.0			
5/26/01 1:32	669 3	plant upset/delay	11.047	1032.0			
5/26/01 1:32	661 3	plant upset/delay	11.047	1032.0			
5/26/01 1:33	657 3	plant upset/delay	11.047	1032.0			
5/26/01 1:33	657 3	plant upset/delay	11.047	1032.0			
5/26/01 1:33	655 3	plant upset/delay	11.047	1032.0			
5/26/01 1:33	653 2	plant upset/delay	11.047	1032.0			
5/26/01 1:34	645 2	plant upset/delay	11.047	1032.0			
5/26/01 1:34	639 2	plant upset/delay	11.047	1032.0			
5/26/01 1:34	643 2	plant upset/delay	11.047	1032.0			
5/26/01 1:34	635 2	plant upset/delay	11.047	1032.0			
5/26/01 1:35	627 2	plant upset/delay	11.047	1032.0			
5/26/01 1:35	629 2	plant upset/delay	11.047	1032.0			
5/26/01 1:35	633 2	plant upset/delay	11.047	1032.0			
5/26/01 1:35	629 2	plant upset/delay	11.047	1032.0			
5/26/01 1:36	627 2	plant upset/delay	11.047	1032.0			
5/26/01 1:36	623 2	plant upset/delay	11.047	1032.0			
5/26/01 1:36	623 2	plant upset/delay	11.047	1032.0			
5/26/01 1:36	627 2	plant upset/delay	11.047	1032.0			
5/26/01 1:37	623 2	plant upset/delay	11.047	1032.0			
5/26/01 1:37	613 2	plant upset/delay	11.047	1032.0			
5/26/01 1:37	615 2	plant upset/delay	11.047	1032.0			
5/26/01 1:37	617 2	plant upset/delay	11.047	1032.0			
5/26/01 1:38	615 2	plant upset/delay	11.047	1032.0			
5/26/01 1:38	609 2	plant upset/delay	11.047	1032.0			
5/26/01 1:38	611 2	plant upset/delay	11.047	1032.0			
5/26/01 1:38	621 2	plant upset/delay	11.047	1032.0			
5/26/01 1:39	625 2	plant upset/delay	11.047	1032.0			
5/26/01 1:39	625 2	plant upset/delay	11.047	1032.0			
5/26/01 1:39	621 2	plant upset/delay	11.047	1032.0			
5/26/01 1:39	617 2	plant upset/delay	11.047	1032.0			
5/26/01 1:40	617 2	plant upset/delay	11.047	1032.0			
5/26/01 1:40	615 2	plant upset/delay	11.047	1032.0			
5/26/01 1:40	613 2	plant upset/delay	11.047	1032.0			
5/26/01 1:40	605 2	plant upset/delay	11.047	1032.0			
5/26/01 1:41	601 1	plant upset/delay	11.047	1032.0			
5/26/01 1:41	605 2	plant upset/delay	11.047	1032.0			
5/26/01 1:41	603 2	plant upset/delay	11.047	1032.0			
5/26/01 1:41	595 1	plant upset/delay	11.047	1032.0			
5/26/01 1:42	607 2	plant upset/delay	11.047	1032.0			
5/26/01 1:42	611 2	plant upset/delay	11.047	1032.0			
5/26/01 1:42	607 2	plant upset/delay	11.047	1032.0			
5/26/01 1:42	605 2	plant upset/delay	11.047	1032.0			

## Georgia Pacific Bleach Plant - Carbon Monoxide Test

DATE / TIME	PPM	COMMENTS	ZERO CAL	1018 ppm cal	CORRECTED PPM	FLOW: acfm - dry	POUNDS OF COPPER HOUR
5/26/01 1:43	609.2	plant upse/delay	11.047	1032.0			
5/26/01 1:43	605.2	plant upse/delay	11.047	1032.0			
5/26/01 1:43	601.1	plant upse/delay	11.047	1032.0			
5/26/01 1:43	601.1	plant upse/delay	11.047	1032.0			
5/26/01 1:44	597.1	plant upse/delay	11.047	1032.0			
5/26/01 1:44	595.1	plant upse/delay	11.047	1032.0			
5/26/01 1:44	595.1	plant upse/delay	11.047	1032.0			
5/26/01 1:44	595.1	plant upse/delay	11.047	1032.0			
5/26/01 1:45	595.1	run 3b	11.047	1032.0	580.7	1433.1	36.3
5/26/01 1:45	599.1	run 3b	11.047	1032.0	584.6	1433.1	36.6
5/26/01 1:45	603.2	run 3b	11.047	1032.0	588.6	1433.1	36.8
5/26/01 1:45	605.2	run 3b	11.047	1032.0	590.6	1433.1	36.9
5/26/01 1:46	611.2	run 3b	11.047	1032.0	596.6	1433.1	37.3
5/26/01 1:46	609.2	run 3b	11.047	1032.0	594.6	1433.1	37.2
5/26/01 1:46	595.1	run 3b	11.047	1032.0	580.7	1433.1	36.3
5/26/01 1:46	579.1	run 3b	11.047	1032.0	564.7	1433.1	35.3
5/26/01 1:47	569.1	run 3b	11.047	1032.0	554.8	1433.1	34.7
5/26/01 1:47	563.1	run 3b	11.047	1032.0	548.8	1433.1	34.3
5/26/01 1:47	565.1	run 3b	11.047	1032.0	550.8	1433.1	34.4
5/26/01 1:47	563.1	run 3b	11.047	1032.0	548.8	1433.1	34.3
5/26/01 1:48	557.1	run 3b	11.047	1032.0	542.8	1433.1	33.9
5/26/01 1:48	551.0	run 3b	11.047	1032.0	536.8	1433.1	33.6
5/26/01 1:48	557.1	run 3b	11.047	1032.0	542.8	1433.1	33.9
5/26/01 1:48	563.1	run 3b	11.047	1032.0	548.8	1433.1	34.3
5/26/01 1:49	561.1	run 3b	11.047	1032.0	546.8	1433.1	34.2
5/26/01 1:49	561.1	run 3b	11.047	1032.0	546.8	1433.1	34.2
5/26/01 1:49	565.1	run 3b	11.047	1032.0	550.8	1433.1	34.4
5/26/01 1:49	567.1	run 3b	11.047	1032.0	552.8	1433.1	34.6
5/26/01 1:50	565.1	run 3b	11.047	1032.0	550.8	1433.1	34.4
5/26/01 1:50	563.1	run 3b	11.047	1032.0	548.8	1433.1	34.3
5/26/01 1:50	561.1	run 3b	11.047	1032.0	546.8	1433.1	34.2
5/26/01 1:50	565.1	run 3b	11.047	1032.0	550.8	1433.1	34.4
5/26/01 1:51	565.1	run 3b	11.047	1032.0	550.8	1433.1	34.4
5/26/01 1:51	561.1	run 3b	11.047	1032.0	546.8	1433.1	34.2
5/26/01 1:51	565.1	run 3b	11.047	1032.0	550.8	1433.1	34.4
5/26/01 1:51	569.1	run 3b	11.047	1032.0	554.8	1433.1	34.7
5/26/01 1:52	569.1	run 3b	11.047	1032.0	554.8	1433.1	34.7
5/26/01 1:52	571.1	run 3b	11.047	1032.0	556.7	1433.1	34.8
5/26/01 1:52	575.1	run 3b	11.047	1032.0	560.7	1433.1	35.1
5/26/01 1:52	573.1	run 3b	11.047	1032.0	558.7	1433.1	34.9
5/26/01 1:53	571.1	run 3b	11.047	1032.0	556.7	1433.1	34.8
5/26/01 1:53	577.1	run 3b	11.047	1032.0	562.7	1433.1	35.2
5/26/01 1:53	581.1	run 3b	11.047	1032.0	566.7	1433.1	35.4
5/26/01 1:53	577.1	run 3b	11.047	1032.0	562.7	1433.1	35.2
5/26/01 1:54	569.1	run 3b	11.047	1032.0	554.8	1433.1	34.7
5/26/01 1:54	565.1	run 3b	11.047	1032.0	550.8	1433.1	34.4
5/26/01 1:54	563.1	run 3b	11.047	1032.0	548.8	1433.1	34.3
5/26/01 1:54	563.1	run 3b	11.047	1032.0	548.8	1433.1	34.3
5/26/01 1:55	563.1	run 3b	11.047	1032.0	548.8	1433.1	34.3
5/26/01 1:55	561.1	run 3b	11.047	1032.0	546.8	1433.1	34.2
5/26/01 1:55	559.1	run 3b	11.047	1032.0	544.8	1433.1	34.1
5/26/01 1:55	563.1	run 3b	11.047	1032.0	548.8	1433.1	34.3
5/26/01 1:56	565.1	run 3b	11.047	1032.0	550.8	1433.1	34.4
5/26/01 1:56	563.1	run 3b	11.047	1032.0	548.8	1433.1	34.3
5/26/01 1:56	563.1	run 3b	11.047	1032.0	548.8	1433.1	34.3
5/26/01 1:56	565.1	run 3b	11.047	1032.0	550.8	1433.1	34.4
5/26/01 1:57	565.1	run 3b	11.047	1032.0	550.8	1433.1	34.4
5/26/01 1:57	561.1	run 3b	11.047	1032.0	546.8	1433.1	34.2
5/26/01 1:57	559.1	run 3b	11.047	1032.0	544.8	1433.1	34.1
5/26/01 1:57	561.1	run 3b	11.047	1032.0	546.8	1433.1	34.2
5/26/01 1:58	569.1	run 3b	11.047	1032.0	554.8	1433.1	34.7

### Georgia Pacific Bleach Plant - Carbon Monoxide Test

DATE / TIME	PPM	COMMENTS	ZERO CAL	1015 ppm cal	CORRECTED PPM	FLOW, acfm dry	POUNDS OF CO PER HOUR
5/26/01 1:58	571.1	run 3b	11 047	1032.0	556.7	1433.1	34.8
5/26/01 1:58	567.1	run 3b	11 047	1032.0	552.8	1433.1	34.6
5/26/01 1:58	571.1	run 3b	11 047	1032.0	556.7	1433.1	34.8
5/26/01 1:59	577.1	run 3b	11 047	1032.0	562.7	1433.1	35.2
5/26/01 1:59	579.1	run 3b	11 047	1032.0	564.7	1433.1	35.3
5/26/01 1:59	577.1	run 3b	11 047	1032.0	562.7	1433.1	35.2
5/26/01 2:00	581.1	run 3b	11 047	1032.0	566.7	1433.1	35.4
5/26/01 2:00	587.1	run 3b	11 047	1032.0	572.7	1433.1	35.8
5/26/01 2:00	591.1	run 3b	11 047	1032.0	576.7	1433.1	36.1
5/26/01 2:00	593.1	run 3b	11 047	1032.0	578.7	1433.1	36.2
5/26/01 2:00	595.1	run 3b	11 047	1032.0	580.7	1433.1	36.3
5/26/01 2:01	591.1	run 3b	11 047	1032.0	576.7	1433.1	36.1
5/26/01 2:01	581.1	run 3b	11 047	1032.0	566.7	1433.1	35.4
5/26/01 2:01	577.1	run 3b	11 047	1032.0	562.7	1433.1	35.2
5/26/01 2:01	577.1	run 3b	11 047	1032.0	562.7	1433.1	35.2
5/26/01 2:02	575.1	run 3b	11 047	1032.0	560.7	1433.1	35.1
5/26/01 2:02	573.1	run 3b	11 047	1032.0	558.7	1433.1	34.9
5/26/01 2:02	577.1	run 3b	11 047	1032.0	562.7	1433.1	35.2
5/26/01 2:02	575.1	run 3b	11 047	1032.0	560.7	1433.1	35.1
5/26/01 2:03	573.1	run 3b	11 047	1032.0	558.7	1433.1	34.9
5/26/01 2:03	573.1	run 3b	11 047	1032.0	558.7	1433.1	34.9
5/26/01 2:03	575.1	run 3b	11 047	1032.0	560.7	1433.1	35.1
5/26/01 2:03	573.1	run 3b	11 047	1032.0	558.7	1433.1	34.9
5/26/01 2:04	567.1	run 3b	11 047	1032.0	552.8	1433.1	34.6
5/26/01 2:04	565.1	run 3b	11 047	1032.0	550.8	1433.1	34.4
5/26/01 2:04	565.1	run 3b	11 047	1032.0	550.8	1433.1	34.4
5/26/01 2:04	567.1	run 3b	11 047	1032.0	552.8	1433.1	34.6
5/26/01 2:05	569.1	run 3b	11 047	1032.0	554.8	1433.1	34.7
5/26/01 2:05	569.1	run 3b	11 047	1032.0	554.8	1433.1	34.7
5/26/01 2:05	567.1	run 3b	11 047	1032.0	552.8	1433.1	34.6
5/26/01 2:05	565.1	run 3b	11 047	1032.0	550.8	1433.1	34.4
5/26/01 2:05	567.1	run 3b	11 047	1032.0	552.8	1433.1	34.6
5/26/01 2:05	567.1	run 3b	11 047	1032.0	552.8	1433.1	34.6
5/26/01 2:06	571.1	run 3b	11 047	1032.0	556.7	1433.1	34.8
5/26/01 2:06	567.1	run 3b	11 047	1032.0	552.8	1433.1	34.6
5/26/01 2:07	561.1	run 3b	11 047	1032.0	546.8	1433.1	34.2
5/26/01 2:07	561.1	run 3b	11 047	1032.0	546.8	1433.1	34.2
5/26/01 2:07	559.1	run 3b	11 047	1032.0	544.8	1433.1	34.1
5/26/01 2:07	555.1	run 3b	11 047	1032.0	544.8	1433.1	34.1
5/26/01 2:08	563.1	run 3b	11 047	1032.0	548.8	1433.1	34.3
5/26/01 2:08	565.1	run 3b	11 047	1032.0	550.8	1433.1	34.4
5/26/01 2:08	565.1	run 3b	11 047	1032.0	550.8	1433.1	34.4
5/26/01 2:08	567.1	run 3b	11 047	1032.0	552.8	1433.1	34.6
5/26/01 2:08	571.1	run 3b	11 047	1032.0	556.7	1433.1	34.8
5/26/01 2:09	569.1	run 3b	11 047	1032.0	554.8	1433.1	34.7
5/26/01 2:09	569.1	run 3b	11 047	1032.0	554.8	1433.1	34.7
5/26/01 2:10	571.1	run 3b	11 047	1032.0	556.7	1433.1	34.8
5/26/01 2:10	571.1	run 3b	11 047	1032.0	556.7	1433.1	34.8
5/26/01 2:10	567.1	run 3b	11 047	1032.0	552.8	1433.1	34.6
5/26/01 2:10	563.1	run 3b	11 047	1032.0	548.8	1433.1	34.3
5/26/01 2:11	563.1	run 3b	11 047	1032.0	548.8	1433.1	34.3
5/26/01 2:11	561.1	run 3b	11 047	1032.0	546.8	1433.1	34.2
5/26/01 2:11	563.1	run 3b	11 047	1032.0	548.8	1433.1	34.3
5/26/01 2:11	565.1	run 3b	11 047	1032.0	550.8	1433.1	34.4
5/26/01 2:12	569.1	run 3b	11 047	1032.0	554.8	1433.1	34.7
5/26/01 2:12	575.1	run 3b	11 047	1032.0	560.7	1433.1	35.1
5/26/01 2:12	583.1	run 3b	11 047	1032.0	568.7	1433.1	35.6
5/26/01 2:12	583.1	run 3b	11 047	1032.0	570.7	1433.1	35.7
5/26/01 2:13	581.1	run 3b	11 047	1032.0	566.7	1433.1	35.4
5/26/01 2:13	583.1	run 3b	11 047	1032.0	568.7	1433.1	35.6

### Georgia Pacific Bleach Plant - Carbon Monoxide Test

DATE - TIME	PPM	COMMENTS	ZERO CAL	1016 ppm cal	CORRECTED PPM	FLOW, scfm, dry	POUNDS OF CO PER HOUR
5/26/01 2 13	583.1	run 3c	11.047	1032.0	568.7	14331	35.8
5/26/01 2 13	577.1	run 3c	11.047	1032.0	562.7	14331	35.2
		run 3c Average			557.1		34.8
5/26/01 2 14	573.1	wait	11.047	1032.0			
5/26/01 2 14	571.1	wait	11.047	1032.0			
5/26/01 2 14	577.1	wait	11.047	1032.0			
5/26/01 2 14	579.1	wait	11.047	1032.0			
5/26/01 2 15	579.1	wait	11.047	1032.0			
5/26/01 2 15	575.1	wait	11.047	1032.0			
5/26/01 2 15	577.1	wait	11.047	1032.0			
5/26/01 2 15	587.1	wait	11.047	1032.0			
5/26/01 2 16	589.1	wait	11.047	1032.0			
5/26/01 2 16	585.1	wait	11.047	1032.0			
5/26/01 2 16	593.1	wait	11.047	1032.0			
5/26/01 2 16	603.2	wait	11.047	1032.0			
5/26/01 2 17	607.2	wait	11.047	1032.0			
5/26/01 2 17	607.2	wait	11.047	1032.0			
5/26/01 2 17	613.2	wait	11.047	1032.0			
5/26/01 2 17	613.2	wait	11.047	1032.0			
5/26/01 2 18	509.2	wait	11.047	1032.0			
5/26/01 2 18	613.2	wait	11.047	1032.0			
5/26/01 2 18	615.2	wait	11.047	1032.0			
5/26/01 2 18	611.2	wait	11.047	1032.0			
5/26/01 2 19	611.2	wait	11.047	1032.0			
5/26/01 2 19	615.2	wait	11.047	1032.0			
5/26/01 2 19	611.2	wait	11.047	1032.0			
5/26/01 2 19	611.2	wait	11.047	1032.0			
5/26/01 2 20	615.2	wait	11.047	1032.0			
5/26/01 2 20	611.2	wait	11.047	1032.0			
5/26/01 2 20	605.2	wait	11.047	1032.0			
5/26/01 2 20	605.2	wait	11.047	1032.0			
5/26/01 2 21	605.2	wait	11.047	1032.0			
5/26/01 2 21	599.1	wait	11.047	1032.0			
5/26/01 2 21	589.1	wait	11.047	1032.0			
5/26/01 2 21	587.1	wait	11.047	1032.0			
5/26/01 2 22	585.1	wait	11.047	1032.0			
5/26/01 2 22	573.1	wait	11.047	1032.0			
5/26/01 2 22	567.1	wait	11.047	1032.0			
5/26/01 2 22	569.1	wait	11.047	1032.0			
5/26/01 2 23	561.1	wait	11.047	1032.0			
5/26/01 2 23	557.1	wait	11.047	1032.0			
5/26/01 2 23	561.1	wait	11.047	1032.0			
5/26/01 2 23	559.1	wait	11.047	1032.0			
5/26/01 2 24	549.0	wait	11.047	1032.0			
5/26/01 2 24	450.8	wait	11.047	1032.0			
5/26/01 2 24	204.4	wait	11.047	1032.0			
5/26/01 2 24	48.1	wait	11.047	1032.0			
5/26/01 2 25	16.0	wait	11.047	1032.0			
5/26/01 2 25	10.0	0 ppm cal	11.047	1032.0			
5/26/01 2 25	12.0	0 ppm cal	11.047	1032.0			
5/26/01 2 25	12.0	0 ppm cal	11.047	1032.0			
5/26/01 2 26	10.0	0 ppm cal	11.047	1032.0			
5/26/01 2 26	10.0	0 ppm cal	11.047	1032.0			
5/26/01 2 26	128.2	wait	11.047	1032.0			
5/26/01 2 26	567.1	wait	11.047	1032.0			
5/26/01 2 27	917.8	wait	11.047	1032.0			
5/26/01 2 27	1026.0	1015 ppm cal	11.047	1032.0			
5/26/01 2 27	1032.0	1015 ppm cal	11.047	1032.0			
5/26/01 2 27	1032.0	1015 ppm cal	11.047	1032.0			
5/26/01 2 28	1036.0	1015 ppm cal	11.047	1032.0			
5/26/01 2 28	1032.0	1015 ppm cal	11.047	1032.0			

### Georgia Pacific Bleach Plant - Carbon Monoxide Test

DATE / TIME	PPM	COMMENTS	ZERO CAL	1016 ppm cal	CORRECTED PPM	FLOW, acfm, dry	POUNDS OF CO PER HOUR
5/26/01 2 28	989.9	wait	11.047	1032.0			
5/26/01 2 28	813.6	wait	11.047	1032.0			
5/26/01 2 29	663.3	wait	11.047	1032.0			
5/26/01 2 29	607.2	wait	11.047	1032.0			
5/26/01 2 29	599.1	594.7 ppm cal	11.047	1032.0			
5/26/01 2 29	599.1	594.7 ppm cal	11.047	1032.0			
5/26/01 2 30	601.1	594.7 ppm cal	11.047	1032.0			
5/26/01 2 30	591.1	594.7 ppm cal	11.047	1032.0			
5/26/01 2 30	436.8	wait	11.047	1032.0			
5/26/01 2 30	176.3	wait	11.047	1032.0			
5/26/01 2 31	50.1	wait	11.047	1032.0			
5/26/01 2 31	18.0	wait	11.047	1032.0			
5/26/01 2 31	12.0	wait	11.047	1032.0			
5/26/01 2 31	12.0	wait	11.047	1032.0			
5/26/01 2 32	12.0	wait	11.047	1032.0			
5/26/01 2 32	12.0	wait	11.047	1032.0			
5/26/01 2 32	10.0	wait	11.047	1032.0			
5/26/01 2 32	12.0	wait	11.047	1032.0			
5/26/01 2 33	12.0	wait	11.047	1032.0			
5/26/01 2 33	10.0	0 ppm cal	11.047	1032.0			
5/26/01 2 33	10.0	0 ppm cal	11.047	1032.0			
5/26/01 2 33	10.0	0 ppm cal	11.047	1032.0			
5/26/01 2 34	10.0	0 ppm cal	11.047	1032.0			
5/26/01 2 34	10.0	0 ppm cal	11.047	1032.0			
5/26/01 2 34	10.0	0 ppm cal	11.047	1032.0			
5/26/01 2 34	10.0	0 ppm cal	11.047	1032.0			
5/26/01 2 35	10.0	0 ppm cal	11.047	1032.0			
5/26/01 2 35	10.0	0 ppm cal	11.047	1032.0			
5/26/01 2 35	10.0	0 ppm cal	11.047	1032.0			
5/26/01 2 35	10.0	0 ppm cal	11.047	1032.0			
5/26/01 2 36	10.0	0 ppm cal	11.047	1032.0			
5/26/01 2 36	10.0	0 ppm cal	11.047	1032.0			
5/26/01 2 36	10.0	0 ppm cal	11.047	1032.0			
5/26/01 2 36	10.0	0 ppm cal	11.047	1032.0			
5/26/01 2 37	4.1	end test	11.047	1032.0			
		<b>Grand Average</b>			716.2		44.71764667
<b>TEST AVERAGE</b>					716.24	14307	44.72

**APPENDIX H**  
**PROJECT PARTICIPANTS**

**Project Participants**

DAVID SALTER

FIELD TESTING  
CALIBRATIONS  
CALCULATIONS  
REPORT PREPARATION

WALTER MOCK

LAB ANALYSIS

BEN MOORE

FIELD TESTING

JOE COOKSEY

CO TESTING

CRAIG COHEN

CO TESTING

GEORGE HAWKINS

FIELD TESTING

HARVEY C. GRAY

REPORT REVIEW

# **SOURCE TEST REPORT**

Georgia-Pacific Corporation  
Palatka, Florida

## **Bleach Plant**

October 29-31, 2002

Prepared By:

**AAS Inc.**

**Ambient Air Services, Inc.**

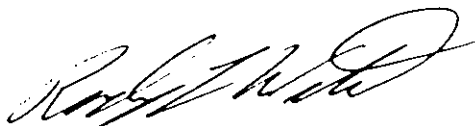
106 Ambient Airway • Starke, FL 32091 • (904) 964-8440 • Fax (904) 964-6675



Ambient Air Services, Inc. of Starke, Florida, has completed the testing as described in this report for Georgia-Pacific Corporation's Palatka, Florida Bleach Plant. To the best of our knowledge and abilities, we certify that all information, facts, and test data are true and correct. Information supplied to AASI for use in this report from Georgia-Pacific Corporation is perceived to be accurate and is used as such where necessary. This report was prepared and certified by:

**Report Number: 504-02-09**

Prepared By:



Randy L Weston  
19 November 2002

Reviewed By:



David Sholtes  
19 November 2002

**EXECUTIVE SUMMARY:**

On 29 and 31 October, 2002 Ambient Air Services, Inc. performed the FDEP required permit stack test at Georgia-Pacific Corporation's Palatka, Florida Bleach Plant. During this test all required stack testing parameters were met. Table I summarizes the results of the test.

**TABLE I**

Georgia-Pacific Corporation Palatka, Florida 29 & 31 October, 2002					
PARAMETER	TEST RESULTS				
<b>29 October</b>					
	Permit Limits	R 1	R 2	R 3	Avg
Carbon Monoxide (CO)	N/A	979.0 ppm	788.7 ppm	N/A	883.9 ppm
	46 lb/hr	58.0 lb/hr	44.5 lb/hr	N/A	51.2 lb/hr
Chlorinated HAP (Cl <sub>2</sub> )	10 ppm	0.233 ppm	0.160 ppm	0.164 ppm	0.186 ppm
	N/A	0.016 lb/hr	0.011 lb/hr	0.012 lb/hr	0.013 lb/hr
<b>31 October</b>					
	Permit Limits	R 1	R 2	R 3	Avg
Carbon Monoxide (CO)	N/A	1155.1 ppm	1212.2 ppm	533.1 ppm	983.5 ppm
	46 lb/hr	72.4 lb/hr	74.6 lb/hr	36.5 lb/hr	61.1 lb/hr
Chlorinated HAP (Cl <sub>2</sub> )	10 ppm	0.073 ppm	0.020 ppm	0.032 ppm	0.042 ppm
	N/A	0.005 lb/hr	0.001 lb/hr	0.002 lb/hr	0.003 lb/hr

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**Sample Chain of Custody**  
**Calibration Gas Certificates**  
**Process Weight Verification**  
**Project Participants**

## 1.0 Introduction

Georgia-Pacific Corporation contracted with Ambient Air Services Inc. of Starke, Florida to perform the Chlorine and Carbon Monoxide compliance testing on the Bleach Plant located in Palatka, Florida.

This testing was conducted in order to satisfy testing requirements of Permit Number 1070005-010-AC for emission sources associated with the Palatka, Florida Bleach Plant. For the testing perspective the requirements of the permit associated with this facility was tested under one mobilization effort.

A summary of the testing performed is summarized in Table 2.

The testing was conducted on October 29 & 31, 2002. Florida DEP was notified of the test dates.

Table 2

Georgia-Pacific Corporation Palatka, Florida 29 & 31 October, 2002 Summary of Permit Requirements Performance Emission Testing					
Source Description	Approx. Stack Flow	Tests	EPA Method	No. of Runs	Min. hrs
Bleach Plant	13,135 scfmd	Cl	40CFR60 AppA, Meth 26a	6	1 hour
		CO	40CFR60 AppA, Meth 10	5	1 hour

## 2.0 Summary and Discussion of Results

### 2.1 Summary of Results

The following is the summary table for the test conducted with all results in Parts per Million and lbs/hr:

Table 3

Georgia Pacific - Palatka, Florida Bleach Plant Carbon Monoxide Test  October 29, 2002  <i>Carbon Monoxide Emission Summary</i>						
RUN NUMBER	START TIME	END TIME	Total Minutes Tested	Flow, SCFM-D	Carbon Monoxide, parts per million	Carbon Monoxide, pounds per hour
1	12:25	13:24	60	12676	979.0	58.0
2	14:33	15:32	60	12068	788.7	44.5
Averages			120	12372	883.9	51.2

Table 4

Georgia Pacific - Palatka, Florida Bleach Plant Carbon Monoxide Test						
October 31, 2002						
<i>Carbon Monoxide Emission Summary</i>						
RUN NUMBER	START TIME	END TIME	Total Minutes Tested	Flow, SCFM-D	Carbon Monoxide, parts per million	Carbon Monoxide, pounds per hour
1	13:30	14:29	60	13401	1155.1	72.4
2	15:47	16:46	60	13171	1212.2	74.6
3	17:10	18:09	60	13375	583.1	36.5
Averages			180	13316	983.5	61.1

Table 5

**Chlorine Emissions Summary**  
 USEPA Method 26A (40 CFR Part 60 Appendix A)  
**Georgia Pacific**  
**Palatka, Fl.**  
  
**October 29, 2002**  
 AASI USEPA Method 26A 12 Point Template - Rev 0/11-7-2002

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Run			Chlorine Emissions			Volumetric Flow Rates		Stack		Sample Volume	Percent
Date	Number	Time (EDT)	GR/SCFD	PPM	LBS/HR	ACFM	SCFMD	Temp °F	Moisture %	SCFD	Isokinetic
10/29/02	1	12:18 13:23	1.50E-04	0.233	0.016	16316	12775	144.3	10.7	34.421	104.7
10/29/02	2	14:33 15:38	1.03E-04	0.160	0.011	15336	12139	145.0	9.6	32.247	103.3
10/29/02	3	17:00 18:02	1.06E-04	0.164	0.012	16770	13454	142.2	8.8	36.523	105.5
Average			1.20E-04	0.186	0.013	16141	12789	143.8	9.7	34.397	104.5



Table 6

**Chlorine Emissions Summary**  
 USEPA Method 26A (40 CFR Part 60 Appendix A)  
**Georgia Pacific**  
**Palatka, Fl.**  
  
**October 31, 2002**  
 AASI USEPA Method 26A 12 Point Template - Rev 0/11-14-2002

AASI

Date	Run		Chlorine Emissions			Volumetric Flow Rates		Stack		Sample Volume	Percent
	Number	Time (H:DT)	GR/SCFD	PPM	LBS/HR	ACFM	SCFMD	Temp °F	Moisture %	SCFD	Isokinetic
10/31/02	1	13:32 14:43	4.73E-05	0.073	0.005	16387	13401	142.0	7.4	35.830	103.9
10/31/02	2	15:50 16:56	1.29E-05	0.020	0.001	16475	13134	143.1	9.0	35.928	106.3
10/31/02	J	17:10 18:16	2.06E-05	0.032	0.002	16123	12870	140.3	9.3	35.118	105.1
Average			2.69E-05	0.042	0.003	16328	13135	141.8	8.6	35.625	105.4

### 3.0 Process Description

#### 3.1 Source Operating Parameters

The following conditions were met and the required information was collected during the compliance test.

1. The Bleach Plant had been stabilized for one hour prior to testing.
2. The production rate, species, Kappa, and ClO<sub>2</sub> application rates were recorded during the test.

#### 3.2 Process Description

The absorbance of visible light by wood pulp fibers is caused mainly by lignin, one of the main constituents of wood. Residual lignin remaining after chemical pulping processes is highly colored. It also darkens with age. Most of the lignin is removed during the pulping process. Bleaching is a process whereby chemicals are applied to the pulp to increase its brightness by continuing the delignification process.

Bleaching increases the usefulness of the paper by enhancing its capacity for accepting printed or written images. It is also a means of purifying pulp, increasing its stability, and enhancing some of its properties.

The chemicals used in the Georgia-Pacific Palatka Mill include oxidants (chlorine dioxide, oxygen and peroxide) and an alkali (sodium hydroxide). The bleaching sequence is first a chlorine dioxide stage (D<sub>0</sub>), followed by a caustic extraction stage enhanced with oxygen and peroxide (E<sub>op</sub>), and finally another chlorine dioxide stage (D<sub>1</sub>). These chemicals are mixed with pulp suspensions at prescribed pH, temperature, and concentration conditions for a specified time period. Bleaching chemicals are applied sequentially with intermediate washing between stages, because it is not possible to achieve sufficient delignification by the action of any one chemical in a single stage. Reaction times for bleaching chemicals range from a few minutes to several hours, requiring large towers to provide adequate retention time.

## 4.0 Sampling Point Location

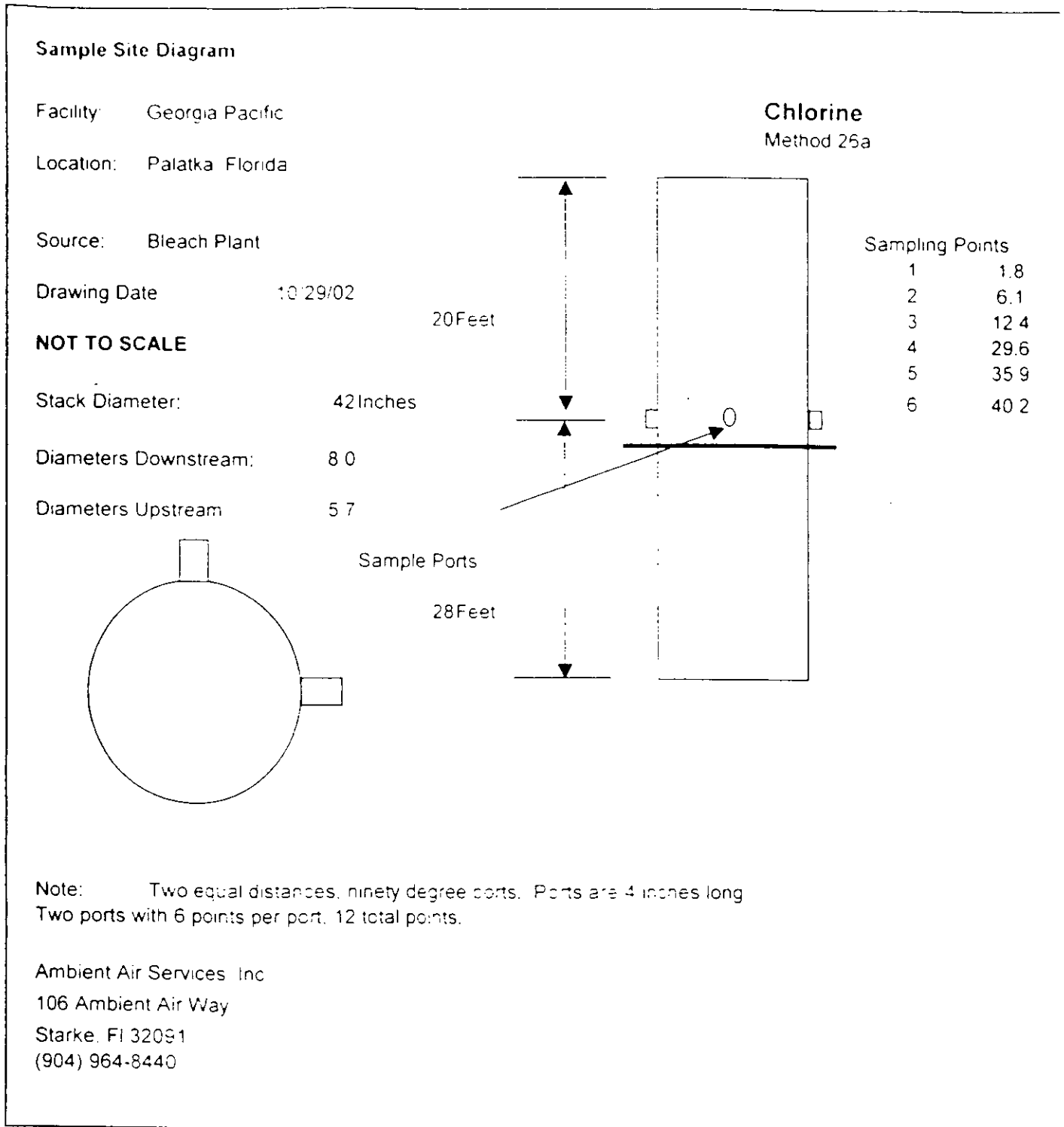


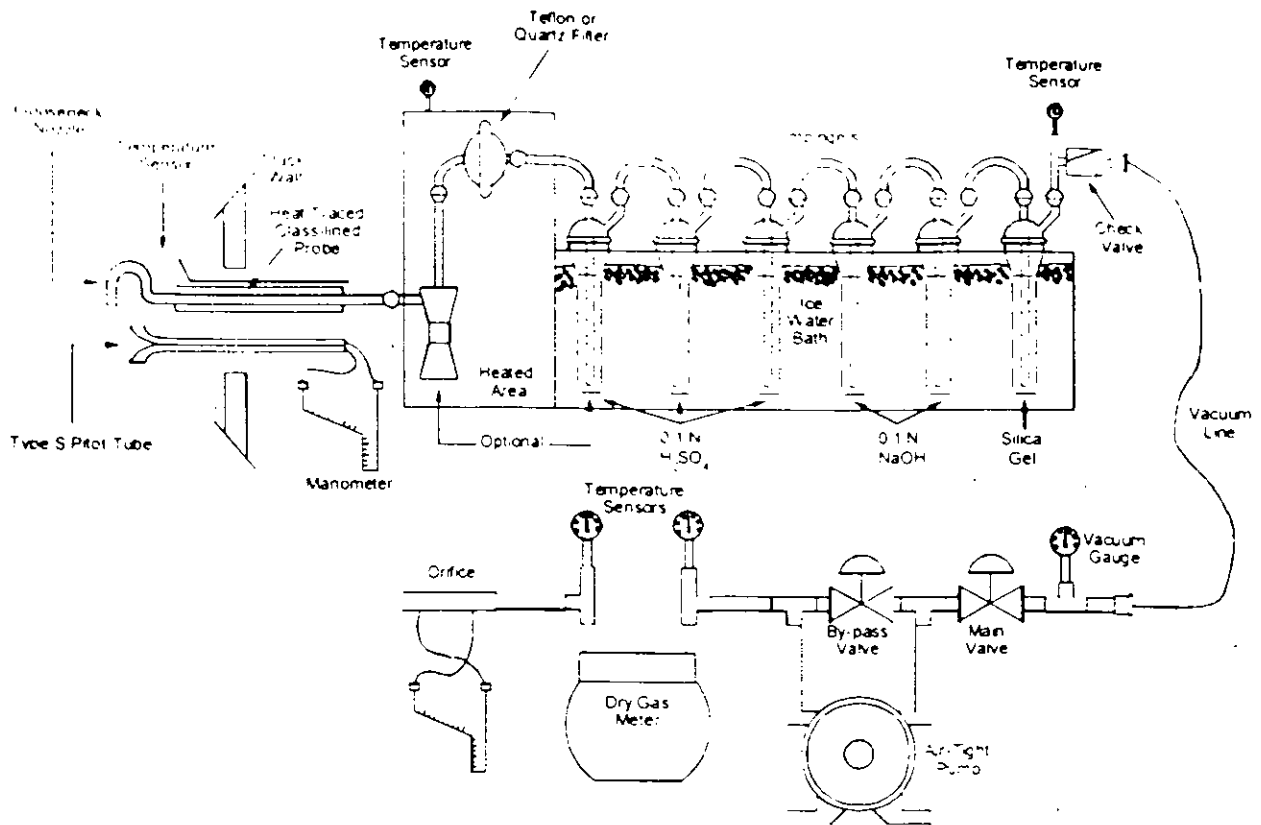
Figure 2-1

## 5.0 Testing Methodology and Procedures

### 5.1 Chlorine Testing (Method 26a)

USEPA method 26a was conducted on the Bleach Plant. The following is a synopsis of the method and a diagram illustrating the equipment in use.

Gaseous and particulate pollutants are withdrawn isokinetically from the source and collected in an optional cyclone, on a filter, and in absorbing solutions. The cyclone collects any liquid droplets and is not necessary if the source emissions do not contain them; however, it is preferable to include the cyclone in the sampling train to protect the filter from any liquid present. The filter collects particulate matter including halide salts but is not routinely recovered or analyzed. Acidic and alkaline absorbing solutions collect the gaseous hydrogen halides and halogens, respectively. Following sampling of emissions containing liquid droplets, any halides/halogens dissolved in the liquid in the cyclone and on the filter are vaporized to gas and collected in the impingers by pulling conditioned ambient air through the sampling train. The hydrogen halides are solubilized in the acidic solution and form chloride ( $\text{Cl}^-$ ), bromide ( $\text{Br}^-$ ), and fluoride ( $\text{F}^-$ ) ions. The halogens have a very low solubility in the acidic solution and pass through to the alkaline solution where they are hydrolyzed to form a proton ( $\text{H}^+$ ), the halide ion, and the hypohalous acid ( $\text{HClO}$  or  $\text{HBrO}$ ). Sodium thiosulfate is added to the alkaline solution to assure reaction with the hypohalous acid to form a second halide ion such that 2 halide ions are formed for each molecule of halogen gas. The halide ions in the separate solutions are measured by ion chromatography (IC). If desired, the particulate matter recovered from the filter and the probe is analyzed following the procedures in Method 5.



## 5.2 Carbon Monoxide Testing (Method 10)

An integrated or continuous gas sample is extracted from a sampling point and analyzed for carbon monoxide (CO) content using a Luft-type nondispersive infrared analyzer (NDIR) or equivalent.

## APPENDICES

Appendix A	Complete Emission Data - Emissions Run Summaries - Flow Calculation Data
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**APPENDIX – A**

**Complete Emission Data  
- Emissions Run Summaries  
- Flow Calculation Data**

**Ambient Air Services, Inc.**  
**Environmental Consultants**

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AASI USEPA Method 5 24 Point Template - Rev 011-1-2002

**CI Summary Run 1**

<b>Facility</b>	Georgia Pacific	<b>Impinger Condensate</b>	81.0
<b>Location</b>	Palatka, Fl.	<b>Silica Gel Condensate</b>	7.0
<b>Stack</b>	Bleach Plant	<b>Volume Metered</b>	37.030
<b>Run Date</b>	10/29/02	<b>Meter Temp (Deg R)</b>	572.0
<b>Run Number</b>	1	<b>Carbon Dioxide, %</b>	0.0
<b>Start Time</b>	12:18	<b>Oxygen, %</b>	20.9
<b>Finish Time</b>	13:23	<b>Carbon Monoxide, %</b>	0.0
<b>Weather</b>	Clear, Warm	<b>Nitrogen, %</b>	79.1
<b>Total Time (minutes)</b>	60	<b>Condensate Volume</b>	88.0
<b>Barometric Pressure</b>	30.03	<b>Delta H (inches H2O)</b>	1.2900
<b>Stack Diameter (inches)</b>	42.00	<b>Stack Pressure</b>	30.025
<b>Stack Area square feet</b>	9.621	<b>Stack Temp (Rainkin Degrees)</b>	604.3
<b>Nozzle Area square feet</b>	0.0004125	<b>Laboratory Results (ug)</b>	438.9
<b>Number of Points</b>	12	<b>Blank Correction</b>	104.3
<b>Avg of SQRT of V.H.</b>	0.4616	<b>Total</b>	334.6
<b>Meter Correction (Y)</b>	1.000		
<b>Nozzle Diameter</b>	0.275		
<b>Pitot Correction Factor</b>	0.84		
<b>Volume Water Vapor, SCF</b>			
			4.142
<b>Gas Volume Sampled, STPD</b>			
			34.421
<b>Total Volume, STP</b>			
			38.563
<b>Moisture in stack gas, volume fraction</b>			
			0.107
<b>Dry Stack Gas, volume fraction</b>			
			0.893
<b>Molecular Weight of Stack Gas (Dry Basis)</b>			
			28.84
<b>Molecular Weight of Stack Gas (Stack conditions)</b>			
			27.68
<b>Specific gravity of Stack Gas Relative to Air</b>			
			0.955
<b>Excess Air (%)</b>			
			14864.9
<b>Average Stack Velocity, FPM</b>			
			1695.9
<b>Actual Stack Gas Flow Rate, ACFM</b>			
			1631.6
<b>Actual Stack Gas Flow Rate, ACFMD</b>			
			1457.0
<b>Stack Gas Flow Rate, SCFMD</b>			
			1277.5
<b>Stack Gas Flow Rate Wet, SCFMW</b>			
			1431.8
<b>Percent Isokinetic</b>			
			105
<b>Stack Emissions:</b>	<b>Grains per DSCF</b>		0.00115
	<b>Pounds per Hour</b>		0.013



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CI Summary Run 2

Facility	Georgia Pacific	Impinger Condensate	66.0
Location	Palatka, FL	Silica Gel Condensate	6.9
Stack	Bleach Plant	Volume Metered	35.145
Run Date	10/29/02	Meter Temp (Deg R)	579.3
Run Number	2	Carbon Dioxide, %	0.0
Start Time	14:33	Oxygen, %	20.9
Finish Time	15:38	Carbon Monoxide, %	0.0
Weather	Partial Clouds	Nitrogen, %	79.1
Total Time (minutes)	60	Condensate Volume	72.9
Barometric Pressure	30.03	Delta H (inches H2O)	1.1530
Stack Diameter (inches)	42.00	Stack Pressure	30.018
Stack Area square feet	9.621	Stack Temp (Rainkin Degrees)	605.0
Nozzle Area square feet	0.0004125	Laboratory Results (ug)	320.0
Number of Points	12	Blank Correction	104.3
Avg of SQRT of V.H.	0.4345	Total	215.7
Meter Correction (Y)	1.000		
Nozzle Diameter	0.275		
Pitot Correction Factor	0.84		
Volume Water Vapor, SCF			3.431
Gas Volume Sampled, STPD			32.247
Total Volume, STP			35.678
Moisture in stack gas, volume fraction			0.096
Dry Stack Gas, volume fraction			0.904
Molecular Weight of Stack Gas (Dry Basis)			28.84
Molecular Weight of Stack Gas (Stack conditions)			27.8
Specific gravity of Stack Gas Relative to Air			0.959
Excess Air (%)			14864.9
Average Stack Velocity, FPM			1594.0
Actual Stack Gas Flow Rate, ACFM			15336
Actual Stack Gas Flow Rate, ACFMD			13864
Stack Gas Flow Rate, SCFMD			12139
Stack Gas Flow Rate Wet, SCFMW			13428
Percent Isokinetic			103
Stack Emissions:	Grains per DSCF		0.00010
	Pounds per Hour		0.011

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CI Summary Run 3

Facility	Georgia Pacific	Impinger Condensate	68.0
Location	Palatka, FL	Silica Gel Condensate	7.1
Stack	Bleach Plant	Volume Metered	38.870
Run Date	10/29/02	Meter Temp (Deg R)	566.0
Run Number	3	Carbon Dioxide, %	0.0
Start Time	17:00	Oxygen, %	20.9
Finish Time	18:02	Carbon Monoxide, %	0.0
Weather	Partial Clouds	Nitrogen, %	79.1
Total Time (minutes)	60	Condensate Volume	75.1
Barometric Pressure	30.03	Delta H (inches H2O)	1.3840
Stack Diameter (inches)	42.00	Stack Pressure	30.019
Stack Area square feet	9.621	Stack Temp (Rainkin Degrees)	602.2
Nozzle Area square feet	0.0004125	Laboratory Results (ug)	354.6
Number of Points	12	Blank Correction	104.3
Avg of SQRT of V.H.	0.4770	Total	250.3
Meter Correction (Y)	1.000		
Nozzle Diameter	0.275		
Pitot Correction Factor	0.84		
Volume Water Vapor, SCF			3.535
Gas Volume Sampled, STPD			36.523
Total Volume, STP			40.058
Moisture in stack gas, volume fraction			0.088
Dry Stack Gas, volume fraction			0.912
Molecular Weight of Stack Gas (Dry Basis)			28.84
Molecular Weight of Stack Gas (Stack conditions)			27.89
Specific gravity of Stack Gas Relative to Air			0.962
Excess Air (%)			14864.9
Average Stack Velocity, FPM			1743.1
Actual Stack Gas Flow Rate, ACFM			16770
Actual Stack Gas Flow Rate, ACFMD			15294
Stack Gas Flow Rate, SCFMD			13454
Stack Gas Flow Rate Wet, SCFMW			14752
Percent Isokinetic			105
Stack Emissions:	Grains per DSCF		0.00011
	Pounds per Hour		0.012

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AASI USEPA Method 26A 12 Point Template - Rev 011-14-2002

### CI Summary Run 1

Facility	Georgia Pacific	Impinger Condensate	54.0
Location	Palatka, FL	Silica Gel Condensate	7.0
Stack	Bleach Plant	Volume Metered	37.945
Run Date	10/31/02	Meter Temp (Deg R)	564.1
Run Number	1	Carbon Dioxide, %	0.0
Start Time	13.32	Oxygen, %	20.9
Finish Time	14.43	Carbon Monoxide, %	0.0
Weather	Cloudy	Nitrogen, %	79.1
Total Time (minutes)	60	Condensate Volume	61.0
Barometric Pressure	30.14	Delta H (inches H2O)	1.3530
Stack Diameter (inches)	42.00	Stack Pressure	30.128
Stack Area square feet	9.621	Stack Temp (Rankin Degrees)	602.0
Nozzle Area square-foot	0.0024125	Laboratory Results (ug)	214.2
Number of Points	12	Blank Correction	194.3
Avg of SQRT of V.H.	0.4683	Total	109.9
Meter Correction (Y)	0.998		
Nozzle Diameter	0.275		
Pitot Correction Factor	0.84		
Volume Water Vapor, SCF			2.871
Gas Volume Sampled, STPD			35.830
Total Volume, STP			38.701
Moisture in stack gas, volume fraction			0.074
Dry Stack Gas, volume fraction			0.926
Molecular Weight of Stack Gas (Dry Basis)			28.84
Molecular Weight of Stack Gas (Stack conditions)			28.04
Specific gravity of Stack Gas Relative to Air			0.967
Excess Air (%)			14864.9
Average Stack Velocity, FPM			1703.3
Actual Stack Gas Flow Rate, ACFM			16387
Actual Stack Gas Flow Rate, ACFMD			15174
Stack Gas Flow Rate, SCFMD			13401
Stack Gas Flow Rate Wet, SCFMW			14472
Percent Isokinetic			104
Stack Emissions:	Grains per DSCF		0.00005
	Pounds per Hour		0.005

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**CI Summary Run 2**

Facility	Georgia Pacific	Impinger Condensate	68.0
Location	Palatka, FL	Silica Gel Condensate	7.1
Stack	Bleach Plant	Volume Metered	38.025
Run Date	10/31/02	Meter Temp (Deg R)	560.2
Run Number	2	Carbon Dioxide, %	0.0
Start Time	15:50	Oxygen, %	20.9
Finish Time	16:56	Carbon Monoxide, %	0.0
Weather	Partial Clouds	Nitrogen, %	79.1
Total Time (minutes)	60	Condensate Volume	75.1
Barometric Pressure	29.95	Delta H (inches H2O)	1.3480
Stack Diameter (inches)	42.00	Stack Pressure	29.940
Stack Area square feet	9.621	Stack Temp (Rankin Degrees)	603.1
Nozzle Area square feet	0.0004125	Laboratory Results (ug)	154.3
Number of Points	12	Blank Correction	104.3
Avg of SQRT of V.H.	0.4674	Total	30.0
Meter Correction (Y)	0.998		
Nozzle Diameter	0.275		
Pitot Correction Factor	0.84		
Volume Water Vapor, SCF			3.535
Gas Volume Sampled, STPD			35.928
Total Volume, STP			39.463
Moisture in stack gas, volume fraction			0.090
Dry Stack Gas, volume fraction			0.91
Molecular Weight of Stack Gas (Dry Basis)			28.84
Molecular Weight of Stack Gas (Stack conditions)			27.86
Specific gravity of Stack Gas Relative to Air			0.951
Excess Air (%)			14854.9
Average Stack Velocity, FPM			1712.4
Actual Stack Gas Flow Rate, ACFM			16475
Actual Stack Gas Flow Rate, ACFMD			14992
Stack Gas Flow Rate, SCFMD			13134
Stack Gas Flow Rate Wet, SCFMW			14433
Percent Isokinetic			106
Stack Emissions:	Grains per DSCF		0.0001
	Pounds per Hour		0.001

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CI Summary Run 3

Facility	Georgia Pacific	Impinger Condensate	70.0
Location	Palatka, FL	Silica Gel Condensate	6.9
Stack	Bleach Plant	Volume Metered	37.000
Run Date	10/31/02	Meter Temp (Deg R)	557.6
Run Number	3	Carbon Dioxide, %	0.0
Start Time	17:10	Oxygen, %	20.9
Finish Time	18:16	Carbon Monoxide, %	0.0
Weather	Partial Clouds	Nitrogen, %	79.1
Total Time (minutes)	60	Condensate Volume	76.9
Barometric Pressure	29.95	Delta H (inches H2O)	1.2970
Stack Diameter (inches)	42.00	Stack Pressure	29.938
Stack Area square feet	9.621	Stack Temp (Rainkin Degrees)	600.3
Nozzle Area square feet	0.0004125	Laboratory Results (ug)	151.1
Number of Points	12	Blank Correction	104.3
Avg of SQRT of V.H.	0.4582	Total	46.8
Meter Correction (Y)	0.998		
Nozzle Diameter	0.275		
Pitot Correction Factor	0.84		
Volume Water Vapor, SCF			3.620
Gas Volume Sampled, STPD			35.118
Total Volume, STP			38.738
Moisture in stack gas, volume fraction			0.093
Dry Stack Gas, volume fraction			0.907
Molecular Weight of Stack Gas (Dry Basis)			28.84
Molecular Weight of Stack Gas (Stack conditions)			27.53
Specific gravity of Stack Gas Relative to Air			0.950
Excess Air (%)			14864.9
Average Stack Velocity, FPM			1675.8
Actual Stack Gas Flow Rate, ACFM			16123
Actual Stack Gas Flow Rate, ACFMD			14524
Stack Gas Flow Rate, SCFMD			12870
Stack Gas Flow Rate Wet, SCFMW			14190
Percent Isokinetic			100
Stack Emissions:	Grains per DSCF		0.00102
	Pounds per Hour		0.112

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AAST USEPA Method 5 24 Point Template - Rev C 11-7-2002

Volumetric Flow Calculations Worksheet

Data Request Entry Area	CI Run 1
Facility	Georgra Pacific
Location	Palatka, Fl.
Source	Bleach Plant
Date	10/29/02
Run Number	1
Start Time	12:18
Finish Time	13:23
Weather	Clear, Warm
Total Time (minutes)	60.00
Number of Points	12
Barometric Pressure	30.03
Static Pressure (inches of water)	-0.05
Stack Diameter (inches)	42.000
Nozzle Diameter (inches)	0.275
Meter Y Factor	1.000
Pitot Factor	0.84
Final Meter Reading (cubic feet)	193.480
Initial Meter Reading (cubic feet)	156.450
Condensate (ml)	81
Silica Gel Weight (grams)	7.0
Carbon Dioxide (percent)	0.0
Oxygen (percent)	20.9
Carbon Monoxide (percent)	0.0
Nitrogen (percent)	79.1
Laboratory Results (ug)	438.9
Blank Correction	104.3
Isokinetic Rate Factor	6.00

Ambient Air Services, Inc.  
Environmental Consultants

106 Ambient Air Way  
Starke, FL. 32091  
(904) 964-8440

AAS USEPA Method 5 24 Point Template - Rev 0111-2002

Field Data Points - CI Run 1				Georgia Pacific		Bleach Plant	
Port	Traverse Point	Velocity Head	Meter Orifice	Stack Temp. (°F)	Meter Inlet Temp. (°F)	Meter Outlet Temp. (°F)	Square Root of Velocity Head
1	1	0.26	1.56	142	106	106	0.51
	2	0.26	1.56	142	107	107	0.51
	3	0.23	1.38	145	107	107	0.48
	4	0.22	1.32	145	108	108	0.47
	5	0.16	1.08	143	110	110	0.42
	6	0.16	0.96	141	111	111	0.40
2	7	0.26	1.56	144	113	113	0.51
	8	0.27	1.62	145	114	114	0.52
	9	0.22	1.32	148	115	115	0.47
	10	0.15	1.08	148	117	117	0.42
	11	0.15	1.08	145	118	118	0.42
	12	0.15	0.96	143	118	118	0.40

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AASI USEPA Method 5 24 Point Template - Rev 0/11-7-2002

Volumetric Flow Calculations Worksheet

Data Request Entry Area	CI Run 2
Facility	Georgia Pacific
Location	Palatka, FL
Source	Bleach Plant
Date	10/29/02
Run Number	2
Start Time	14:33
Finish Time	15:38
Weather	Partial Clouds
Total Time (minutes)	60.0
Number of Points	12
Barometric Pressure	30.03
Static Pressure (inches of water)	-0.16
Stack Diameter (inches)	42.00
Nozzle Diameter (inches)	0.275
Meter Y Factor	1.005
Pitot Factor	0.84
Final Meter Reading (cubic feet)	230.200
Initial Meter Reading (cubic feet)	195.055
Condensate (ml)	66
Silica Gel Weight (grams)	6.9
Carbon Dioxide (percent)	0.0
Oxygen (percent)	20.9
Carbon Monoxide (percent)	
Nitrogen (percent)	79.1
Laboratory Results (ug)	320.0
Blank Correction	104.3
Isokinetic Rate Factor	6.04



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AASI USEPA Method 5 24 Point Template - Rev 0/11-7-2002

Field Data Points - CI Run 2				Georgia Pacific		Bleach Plant	
Port	Traverse Point	Velocity Head	Meter Orifice	Stack Temp. (°F)	Meter Inlet Temp. (°F)	Meter Outlet Temp. (°F)	Square Root of Velocity Head
1	1	0.21	1.27	145	115	115	0.46
	2	0.2	1.21	145	117	117	0.45
	3	0.16	0.97	146	118	118	0.40
	4	0.16	0.97	147	118	118	0.40
	5	0.16	0.97	145	119	119	0.40
	6	0.12	0.72	139	120	120	0.35
2	7	0.25	1.51	146	120	120	0.50
	8	0.25	1.51	146	120	120	0.50
	9	0.23	1.33	147	121	121	0.47
	10	0.22	1.33	147	121	121	0.47
	11	0.18	1.09	144	121	121	0.42
	12	0.16	0.97	143	121	121	0.40

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(904) 964-8440

AASI USEPA Method 5 24 Point Template - Rev 0 11-7-2002

**Volumetric Flow Calculations Worksheet**

Data Request Entry Area	CI Run 3
Facility	Georgia Pacific
Location	Palatka, Fl
Source	Bleach Plant
Date	10/29 02
Run Number	3
Start Time	17.00
Finish Time	18.02
Weather	Partial Clouds
Total Time (minutes)	60 0
Number of Points	12
Barometric Pressure	30.03
Static Pressure (inches of water)	-0 15
Stack Diameter (inches)	42.00
Nozzle Diameter (inches)	0.275
Meter Y Factor	1.000
Pitot Factor	0.84
Final Meter Reading (cubic feet)	269.620
Initial Meter Reading (cubic feet)	230.750
Condensate (ml)	68
Silica Gel Weight (grams)	7.1
Carbon Dioxide (percent)	0.0
Oxygen (percent)	20.9
Carbon Monoxide (percent)	
Nitrogen (percent)	79.1
Laboratory Results (ug)	354.6
Blank Correction	104.3
Isokinetic Rate Factor	6.04

**Ambient Air Services, Inc.**  
**Environmental Consultants**

**106 Ambient Air Way**  
**Starke, FL 32091**  
**(904) 964-8440**

AASI USEPA Method 924 Print Template - Rev 0/11-7-2002

Field Data Points - CI Run 3				Georgia Pacific		Bleach Plant	
Port	Traverse Point	Velocity Head	Meter Orifice	Stack Temp. (°F)	Meter Inlet Temp. (°F)	Meter Outlet Temp. (°F)	Square Root of Velocity Head
1	1	0.26	1.57	144	109	109	0.51
	2	0.28	1.69	142	102	102	0.53
	3	0.26	1.57	144	107	107	0.51
	4	0.25	1.51	143	107	107	0.50
	5	0.2	1.21	141	107	107	0.45
	6	0.18	1.09	140	107	107	0.42
2	7	0.26	1.57	141	106	106	0.51
	8	0.28	1.69	143	106	106	0.53
	9	0.22	1.33	144	106	106	0.47
	10	0.2	1.21	142	105	105	0.45
	11	0.18	1.09	142	105	105	0.42
	12	0.18	1.09	140	105	105	0.42

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AAST USEPA Method 26A 12 Point Template Rev 011-14-2002

Volumetric Flow Calculations Worksheet

Data Request Entry Area	CI Run 1
Facility	Georgia Pacific
Location	Palatka, Fl
Source	Bleach Plant
Date	10/31/02
Run Number	1
Start Time	13:32
Finish Time	14:43
Weather	Cloudy
Total Time (minutes)	60.00
Number of Points	12
Barometric Pressure	30.14
Static Pressure (inches of water)	-0.17
Stack Diameter (inches)	42.000
Nozzle Diameter (inches)	0.275
Meter Y Factor	0.998
Pitot Factor	0.84
Final Meter Reading (cubic feet)	313.155
Initial Meter Reading (cubic feet)	275.210
Condensate (ml)	54
Silica Gel Weight (grams)	7.0
Carbon Dioxide (percent)	0.0
Oxygen (percent)	20.9
Carbon Monoxide (percent)	0.0
Nitrogen (percent)	79.1
Laboratory Results (ug)	214.2
Blank Correction	104.3
Isokinetic Rate Factor	6.08

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AASI USEPA Method 9A-1 Point Template - Rev 0 11-14-2002

Field Data Points - CI Run 1				Georgia Pacific		Bleach Plant	
Port	Traverse Point	Velocity Head	Meter Orifice	Stack Temp. (°F)	Meter Inlet Temp. (°F)	Meter Outlet Temp. (°F)	Square Root of Velocity Head
1	1	0.28	1.70	142	100	101	0.53
	2	0.26	1.58	144	102	100	0.51
	3	0.24	1.46	141	103	99	0.49
	4	0.18	1.09	141	105	100	0.42
	5	0.16	0.97	141	108	101	0.40
	6	0.14	0.85	142	108	102	0.37
2	7	0.27	1.64	141	109	103	0.52
	8	0.29	1.76	141	109	103	0.54
	9	0.27	1.64	142	109	103	0.52
	10	0.24	1.46	142	109	102	0.49
	11	0.18	1.09	144	109	102	0.42
	12	0.16	0.97	143	109	102	0.40

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AASI USEPA Method 26A 12 Point Template - Rev 0/11-14 2002

**Volumetric Flow Calculations Worksheet**

Data Request Entry Area	CI Run 2
Facility	Georgia Pacific
Location	Palatka, Fl
Source	Bleach Plant
Date	10/31/02
Run Number	2
Start Time	15:50
Finish Time	16:56
Weather	Partial Clouds
Total Time (minutes)	60.0
Number of Points	12
Barometric Pressure	29.95
Static Pressure (inches of water)	-0.14
Stack Diameter (inches)	42.00
Nozzle Diameter (inches)	0.275
Meter Y Factor	0.998
Pitot Factor	0.84
Final Meter Reading (cubic feet)	359.105
Initial Meter Reading (cubic feet)	321.080
Condensate (ml)	68
Silica Gel Weight (grams)	7.1
Carbon Dioxide (percent)	0.0
Oxygen (percent)	20.9
Carbon Monoxide (percent)	
Nitrogen (percent)	79.1
Laboratory Results (ug)	134.3
Blank Correction	104.3
Isokinetic Rate Factor	6.08

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AASI USEPA Method 21A 12 Point Template - Rev 0/11-14-2002

Field Data Points - CI Run 2				Georgia Pacific		Bleach Plant	
Port	Traverse Point	Velocity Head	Meter Orifice	Stack Temp. (°F)	Meter Inlet Temp. (°F)	Meter Outlet Temp. (°F)	Square Root of Velocity Head
1	1	0.27	1.64	140	94	93	0.52
	2	0.28	1.70	141	95	92	0.53
	3	0.24	1.46	143	103	96	0.49
	4	0.22	1.34	145	103	96	0.47
	5	0.18	1.09	144	105	97	0.42
	6	0.16	0.97	144	105	97	0.40
2	7	0.29	1.76	141	105	97	0.54
	8	0.3	1.82	142	105	97	0.55
	9	0.22	1.34	144	108	99	0.47
	10	0.2	1.22	145	108	98	0.45
	11	0.16	0.97	144	108	98	0.40
	12	0.14	0.85	144	108	97	0.37

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AASHTO USEPA Method 26A 12 Point Template - Rev 01/14/2002

Volumetric Flow Calculations Worksheet

Data Request Entry Area	CI Run 3
Facility	Georgia Pacific
Location	Palatka, FL
Source	Bleach Plant
Date	10/31/02
Run Number	3
Start Time	17:10
Finish Time	18:16
Weather	Partial Clouds
Total Time (minutes)	60.0
Number of Points	12
Barometric Pressure	29.95
Static Pressure (inches of water)	-0.16
Stack Diameter (inches)	42.00
Nozzle Diameter (inches)	0.275
Meter Y Factor	0.998
Pitot Factor	0.84
Final Meter Reading (cubic feet)	396.405
Initial Meter Reading (cubic feet)	359.405
Condensate (ml)	70
Silica Gel Weight (grams)	6.9
Carbon Dioxide (percent)	0.0
Oxygen (percent)	20.9
Carbon Monoxide (percent)	
Nitrogen (percent)	79.1
Laboratory Results (ug)	151.1
Blank Correction	104.3
Isokinetic Rate Factor	6.08



Ambient Air Services, Inc.  
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AASI USEPA Method 26A 12 Point Template - Rev 0.11.14.2002

Field Data Points - CI Run 3				Georgia Pacific		Bleach Plant	
Port	Traverse Point	Velocity Head	Meter Orifice	Stack Temp. (°F)	Meter Inlet Temp. (°F)	Meter Outlet Temp. (°F)	Square Root of Velocity Head
1	1	0.28	1.70	138	97	95	0.53
	2	0.26	1.58	140	100	96	0.51
	3	0.22	1.34	142	98	95	0.47
	4	0.2	1.22	140	100	93	0.45
	5	0.16	0.97	139	101	93	0.40
	6	0.14	0.85	142	102	94	0.37
2	7	0.3	1.82	142	102	94	0.55
	8	0.26	1.58	141	102	94	0.51
	9	0.24	1.46	140	102	94	0.49
	10	0.2	1.22	140	102	94	0.45
	11	0.16	0.97	139	103	95	0.40
	12	0.14	0.85	140	102	95	0.37

**APPENDIX – B**

- Field Data Sheets**  
**- Chlorine and Flow Data Sheets**  
**- Carbon Monoxide Data**



AMBIENT AIR SERVICES  
106 AMBIENT AIR WAY  
STARKE FL. 32091 (904) 964-8440

SOURCE SAMPLING FIELD DATA SHEET

FACILITY: GP Palatka

SOURCE: Bleach Plant

WEATHER: Partial Clouds

TYPE TEST: CTM-027

TESTERS: RW, RD

12 PTS. @ 5 MIN/PT = 60 MIN F.D.A. = .94

Y meter = 0.998 Filter No. = \_\_\_\_\_

COMMENTS:

TIME START 11:33 START VOLUME 195.055 *static*  
TIME END 15:38 END VOLUME \_\_\_\_\_ *-.16*  
PORT LENGTH (IN) 7" Factors: 6.04

BAROMETRIC PRESS. 30.03  
METER BOX ID: RS+ 10  
METER DELTA H: 2.050  
PROBE ID: 6P  
PITOT CORR FACTOR 0.84  
NOZZLE DIA. 0.275 in.  
PROBE TEMP N/A  
STACK ID (IN.) = 42"  
UP/DOWN STREAM 28 22

CTM-027  
HCL

RUN No 2  
DATE 10/29/02

CO \_\_\_\_\_  
CO 20.9  
CO \_\_\_\_\_

9286.22  
1570 X 170.55 X .005  
1536.7

LEAK CHECK:

PRE-TEST 0 CFM@15" POST: .015 8" Hg.

PITOT LEAK CHECK = OK AT 3"

VOL. WATER COLLECTED = 66 ML  
WEIGHT MOIS. SILICA GEL = GR

STAT PRESS = -.16

PORT & SAMPLE POINT	CLOCK TIME	GAS METER READING	STACK VELOCITY Dp	ORRIFICE PRESS. DROP	STACK GAS TEMP	METER TEMP (F)	FILTER TEMP (F)	LAST IMPINGER TEMP	VACUUM INCHES Hg	PROBE GAS TEMP
1-1	0:25	195.055	.21	1.3	145	115	125	76	30.5	N/A
2	5:5	197.7	.2	1.2	145	117	274	60	6	
3	10:75	201.1	.16	.96	146	118	254	59	4.5	
4	15:10	205.8	.16	.96	147	118	220	60	4.5	
5	20:125	206.5	.16	.96	145	119	263	56	4.5	
6	25:16	209.2	.12	.72	139	120	245	54	4	
2-1	30:175	211.605	.25	1.5	146	120	274	54	5	
2	35:20	214.7	.25	1.5	146	120	238	50	5	
3	40:225	218.0	.22	1.3	147	121	284	52	5	
4	45:25	221.2	.22	1.3	147	121	272	52	5	
5	50:275	224.4	.18	1.1	147	121	221	54	5	
6	55:30	227.4	.16	.96	143	121	259	55	4.5	
	60	230.2	-	-	-	-	-	-	-	

a)  $(.28^2 \times .94)^2$   
b)  $(1.6 \times .94) 605$   
c)  $571 \times 2.05$



AMBIENT AIR SERVICES, INC.

STARKE, FL

(904)964-8440

BAROMETRIC PRESS \_\_\_\_\_

METER BOX ID 10

METER DELTA Ha 2.05

PROBE ID \_\_\_\_\_

PITOT CORR. FACTOR 0.84

NOZZLE DIA. 0.275 in.

PROBE TEMP. ~ 250

STACK ID (IN): 4.2"

PORT LENGTH 6"

LEAK CHECK:

PRE-TEST 0.012 CFM @ 15" POS 0.014/0 " Hg.

PORT & CLOCK GAS METER STACK ORIFICE  
SAMPLE TIME READING VELOCITY PRESS.  
POINT Dp DROP TEMP.

PORT & CLOCK POINT	GAS METER READING	STACK VELOCITY Dp	ORIFICE PRESS. DROP	STACK GAS TEMP.
1-1 0	275.210	0.28	1.70	142
2 5	78.64	0.26	1.58	144
3 10	82.01	0.24	1.45	141
4 15	85.32	0.18	1.09	141
5 20	88.35	0.16	0.97	141
6 25	91.11	0.14	0.85	142
2-1 30	94.105	0.27	1.64	141
2 35	97.45	0.29	1.76	141
3 40	300.74	0.27	1.64	142
4 45	04.18	0.24	1.95	142
5 50	07.71	0.18	1.09	144
6 55	10.44	0.16	0.97	143
60	313.153			

SOURCE SAMPLING FIELD DATA SHEET

FACILITY: Georgia-Pacific, Palatka

SOURCE: Bleach Plant

WEATHER: p. cloudy

TYPE TEST: HCl method 26A

TESTERS: \_\_\_\_\_

12 PTS. @ 5 MIN/PT = 60 MIN

Y meter = 0.998 Filter No. = \_\_\_\_\_

COMMENTS:

TIME START 1332

TIME END 1443

START VOLUME 275.210

END VOLUME \_\_\_\_\_

Factors: \_\_\_\_\_

RUN No. 1

DATE 10/31/02

ORSAT \_\_\_\_\_

CO2 \_\_\_\_\_

O2 \_\_\_\_\_

CO \_\_\_\_\_

F=1570(aXc)/b

a = (Dp \* 2 \* X \* FDA) \* 2

b = (1.6 + FDA) \* Ts

c = Tm \* DHa

PITOT LEAK CHECK

= OK AT 3"

VOL. WATER COLLECTED = 68 ML STAT. PRESS = \_\_\_\_\_

WT. MOIS. SILICA GEL = \_\_\_\_\_ GR

METER TEMP (F)	METER TEMP (F)	FILTER TEMP (F)	LAST IMPINGE TEMP	VACUUM INCHES Hg
100	101	246	64	<5
102	100	256	56	<6
103	99	258	56	<5
105	100	259	55	<5
108	101	260	56	<5
108	102	258	56	<5
109	103	261	57	<6
109	103	260	55	<5
109	103	262	55	<6
109	102	259	56	<6
109	102	241	56	<5
109	102	258	56	<5

1085 = 1.1







**Georgia Pacific - Palatka, Florida**  
**Bleach Plant Carbon Monoxide Test**

October 29, 2002

**DATA RECORDER PRINTOUT and TEST SUMMARY**

Time	CO, ppm	Run Number	COMMENTS	CO C <sub>1</sub>	CO C <sub>2</sub>	CO C <sub>3</sub>	CO, ppm Drift Corrected	Flow, SCFM-Dry	CO, pounds per Hour
10/29/02 12:01	1982.2		1994 CO Cal						
10/29/02 12:02	1929.0								
10/29/02 12:03	982.2								
10/29/02 12:04	995.6		991 CO Cal						
10/29/02 12:05	995.1		991 CO Cal						
10/29/02 12:06	621.1								
10/29/02 12:07	580.7								
10/29/02 12:08	588.0		594.4 CO Cal						
10/29/02 12:09	588.0		594.4 CO Cal						
10/29/02 12:10	588.0		594.4 CO Cal						
10/29/02 12:11	572.3								
10/29/02 12:12	279.5								
10/29/02 12:13	299.1		301.9 CO Cal						
10/29/02 12:14	299.1		301.9 CO Cal						
10/29/02 12:15	299.1		301.9 CO Cal						
10/29/02 12:16	299.1		301.9 CO Cal						
10/29/02 12:17	299.1		301.9 CO Cal						
10/29/02 12:18	234.7								
10/29/02 12:19	10.2								
10/29/02 12:20	4.0		0 CO Cal						
10/29/02 12:21	4.6								
10/29/02 12:22	454.3								
10/29/02 12:23	917.7								
10/29/02 12:24	994.3								
10/29/02 12:25	969.3	1		4.80	996.85	991.00	963.5	12068	54.35
10/29/02 12:26	984.3	1		4.80	996.85	991.00	978.5	12676	57.97
10/29/02 12:27	1002.7	1		4.80	996.85	991.00	996.8	12676	59.06
10/29/02 12:28	987.7	1		4.80	996.85	991.00	981.8	12676	58.17
10/29/02 12:29	981.0	1		4.80	996.85	991.00	975.2	12676	57.78
10/29/02 12:30	996.0	1		4.80	996.85	991.00	990.2	12676	58.67
10/29/02 12:31	1009.3	1		4.80	996.85	991.00	1003.5	12676	59.45
10/29/02 12:32	987.7	1		4.80	996.85	991.00	981.8	12676	58.17
10/29/02 12:33	997.7	1		4.80	996.85	991.00	991.8	12676	58.76
10/29/02 12:34	1004.3	1		4.80	996.85	991.00	998.5	12676	59.16
10/29/02 12:35	996.0	1		4.80	996.85	991.00	990.2	12676	58.67
10/29/02 12:36	992.7	1		4.80	996.85	991.00	986.8	12676	58.47
10/29/02 12:37	976.0	1		4.80	996.85	991.00	970.2	12676	57.48
10/29/02 12:38	961.0	1		4.80	996.85	991.00	955.2	12676	56.59
10/29/02 12:39	954.3	1		4.80	996.85	991.00	948.5	12676	56.20
10/29/02 12:40	972.7	1		4.80	996.85	991.00	966.8	12676	57.28
10/29/02 12:41	959.3	1		4.80	996.85	991.00	953.5	12676	56.50
10/29/02 12:42	949.3	1		4.80	996.85	991.00	943.5	12676	55.90
10/29/02 12:43	977.7	1		4.80	996.85	991.00	971.8	12676	57.58
10/29/02 12:44	971.0	1		4.80	996.85	991.00	965.2	12676	57.19
10/29/02 12:45	974.3	1		4.80	996.85	991.00	968.5	12676	57.39
10/29/02 12:46	981.0	1		4.80	996.85	991.00	975.2	12676	57.78
10/29/02 12:47	956.0	1		4.80	996.85	991.00	950.2	12676	56.30
10/29/02 12:48	966.0	1		4.80	996.85	991.00	960.2	12676	56.89
10/29/02 12:49	957.7	1		4.80	996.85	991.00	951.9	12676	56.40

**Georgia Pacific - Palatka, Florida**  
**Bleach Plant Carbon Monoxide Test**

October 29, 2002  
**DATA RECORDER PRINTOUT and TEST SUMMARY**

Time	CO, ppm	Run Number	COMMENTS	CO C <sub>1</sub>	CO C <sub>2</sub>	CO C <sub>3</sub>	CO, ppm Drift Corrected	Flow, SCFM-Dry	CO, pounds per hour
10/29/02 12:50	926.0	1		4.80	996.85	991.00	920.2	12676	54.52
10/29/02 12:51	937.7	1		4.80	996.85	991.00	931.9	12676	55.21
10/29/02 12:52	906.0	1		4.80	996.85	991.00	900.2	12676	53.34
10/29/02 12:53	934.3	1		4.80	996.85	991.00	928.5	12676	55.02
10/29/02 12:54	926.0	1		4.80	996.85	991.00	920.2	12676	54.52
10/29/02 12:55	887.7	1		4.80	996.85	991.00	881.9	12676	52.25
10/29/02 12:56	912.7	1		4.80	996.85	991.00	906.9	12676	53.73
10/29/02 12:57	921.0	1		4.80	996.85	991.00	915.2	12676	54.23
10/29/02 12:58	929.3	1		4.80	996.85	991.00	923.6	12676	54.72
10/29/02 12:59	962.7	1		4.80	996.85	991.00	956.9	12676	56.69
10/29/02 13:00	956.0	1		4.80	996.85	991.00	950.2	12676	56.30
10/29/02 13:01	979.3	1		4.80	996.85	991.00	973.5	12676	57.68
10/29/02 13:02	979.3	1		4.80	996.85	991.00	973.5	12676	57.68
10/29/02 13:03	1002.7	1		4.80	996.85	991.00	996.8	12676	59.06
10/29/02 13:04	1026.0	1		4.80	996.85	991.00	1020.1	12676	60.44
10/29/02 13:05	1011.0	1		4.80	996.85	991.00	1005.1	12676	59.55
10/29/02 13:06	1012.7	1		4.80	996.85	991.00	1006.8	12676	59.65
10/29/02 13:07	1014.3	1		4.80	996.85	991.00	1008.5	12676	59.75
10/29/02 13:08	996.0	1		4.80	996.85	991.00	990.2	12676	58.67
10/29/02 13:09	1014.3	1		4.80	996.85	991.00	1008.5	12676	59.75
10/29/02 13:10	1026.0	1		4.80	996.85	991.00	1020.1	12676	60.44
10/29/02 13:11	1007.7	1		4.80	996.85	991.00	1001.8	12676	59.36
10/29/02 13:12	1036.0	1		4.80	996.85	991.00	1030.1	12676	61.03
10/29/02 13:13	1024.3	1		4.80	996.85	991.00	1018.5	12676	60.34
10/29/02 13:14	1001.0	1		4.80	996.85	991.00	995.1	12676	58.96
10/29/02 13:15	1017.7	1		4.80	996.85	991.00	1011.8	12676	59.95
10/29/02 13:16	1032.7	1		4.80	996.85	991.00	1026.8	12676	60.84
10/29/02 13:17	1027.7	1		4.80	996.85	991.00	1021.8	12676	60.54
10/29/02 13:18	1011.0	1		4.80	996.85	991.00	1005.1	12676	59.55
10/29/02 13:19	1024.3	1		4.80	996.85	991.00	1018.5	12676	60.34
10/29/02 13:20	1026.0	1		4.80	996.85	991.00	1020.1	12676	60.44
10/29/02 13:21	1036.0	1		4.80	996.85	991.00	1030.1	12676	61.03
10/29/02 13:22	1051.0	1		4.80	996.85	991.00	1045.1	12676	61.92
10/29/02 13:23	1034.3	1		4.80	996.85	991.00	1028.4	12676	60.93
10/29/02 13:24	1034.3	1		4.80	996.85	991.00	1028.4	12676	60.93
10/29/02 13:25	1037.7			<b>Run 1 Average</b>			<b>979.0</b>		<b>57.96</b>
10/29/02 13:26	771.0								
10/29/02 13:27	54.0								
10/29/02 13:28	13.8								
10/29/02 13:29	13.8								
10/29/02 13:30	5.6		CO Cal						
10/29/02 13:31	723.3								
10/29/02 13:32	1990.0								
10/29/02 13:33	1993.1		CO Cal						
10/29/02 13:34	1993.1		CO Cal						
10/29/02 13:35	1993.1		CO Cal						
10/29/02 13:36	1521.4								
10/29/02 13:37	978.7								
10/29/02 13:38	998.3		CO Cal						

**Georgia Pacific - Palatka, Florida**  
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**DATA RECORDER PRINTOUT and TEST SUMMARY**

Time	CO, ppm	Run Number	COMMENTS	CO C <sub>1</sub>	CO C <sub>2</sub>	CO C <sub>3</sub>	CO, ppm Drift Corrected	Flow, SCFM-Dry	CO, pounds per hour
10/29/02 13:39	645.1								
10/29/02 13:40	587.4		594.4 CO Cal						
10/29/02 13:41	464.9								
10/29/02 13:42	282.6								
10/29/02 13:43	300.1		301.9 CO Cal						
10/29/02 13:44	204.3								
10/29/02 13:45	212.6								
10/29/02 13:46	1138.3								
10/29/02 13:47	1186.7								
10/29/02 13:48	1184.7								
10/29/02 13:49	1186.7								
10/29/02 13:50	1190.9								
10/29/02 13:51	1201.2								
10/29/02 13:52	1212.5								
10/29/02 13:53	1192.9								
10/29/02 13:54	1207.3								
10/29/02 13:55	1193.9								
10/29/02 13:56	1187.8								
10/29/02 13:57	1191.9								
10/29/02 13:58	1190.9								
10/29/02 13:59	1208.4								
10/29/02 14:00	1241.3								
10/29/02 14:01	1223.8								
10/29/02 14:02	1219.7								
10/29/02 14:03	1213.5								
10/29/02 14:04	1212.5								
10/29/02 14:05	1235.1								
10/29/02 14:06	1251.6								
10/29/02 14:07	1234.1								
10/29/02 14:08	1223.8								
10/29/02 14:09	1224.8								
10/29/02 14:10	1227.9								
10/29/02 14:11	1269.1								
10/29/02 14:12	1271.2								
10/29/02 14:13	1253.7								
10/29/02 14:14	1269.1								
10/29/02 14:15	1250.6								
10/29/02 14:16	1227.9								
10/29/02 14:17	1246.5								
10/29/02 14:18	1245.4								
10/29/02 14:19	1193.9								
10/29/02 14:20	1220.7								
10/29/02 14:21	1215.6								
10/29/02 14:22	1155.8								
10/29/02 14:23	1162.0								
10/29/02 14:24	1153.8								
10/29/02 14:25	1111.6								
10/29/02 14:26	1081.7								
10/29/02 14:27	1051.8								

**Georgia Pacific - Palatka, Florida**  
**Bleach Plant Carbon Monoxide Test**

October 29, 2002

**DATA RECORDER PRINTOUT and TEST SUMMARY**

Time	CO, ppm	Run Number	COMMENTS	CO C <sub>s</sub>	CO C <sub>m</sub>	CO C <sub>wa</sub>	CO, ppm Drift Corrected	Flow, SCFM-Dry	CO, pounds per hour
10/29/02 14:28	1024.0								
10/29/02 14:29	1026.1								
10/29/02 14:30	1002.4								
10/29/02 14:31	1007.6								
10/29/02 14:32	978.7								
10/29/02 14:33	961.2	2		4.05	997.8	991	954.5	12068	53.84
10/29/02 14:34	960.2	2		4.05	997.8	991	953.5	12068	53.78
10/29/02 14:35	933.4	2		4.05	997.8	991	926.8	12068	52.28
10/29/02 14:36	940.6	2		4.05	997.8	991	934.0	12068	52.68
10/29/02 14:37	930.3	2		4.05	997.8	991	923.7	12068	52.10
10/29/02 14:38	905.6	2		4.05	997.8	991	899.1	12068	50.71
10/29/02 14:39	923.1	2		4.05	997.8	991	916.5	12068	51.70
10/29/02 14:40	895.3	2		4.05	997.8	991	888.8	12068	50.13
10/29/02 14:41	897.4	2		4.05	997.8	991	890.8	12068	50.25
10/29/02 14:42	901.5	2		4.05	997.8	991	894.9	12068	50.48
10/29/02 14:43	890.2	2		4.05	997.8	991	883.7	12068	49.84
10/29/02 14:44	897.4	2		4.05	997.8	991	890.8	12068	50.25
10/29/02 14:45	880.9	2		4.05	997.8	991	874.4	12068	49.32
10/29/02 14:46	887.1	2		4.05	997.8	991	880.6	12068	49.67
10/29/02 14:47	853.1	2		4.05	997.8	991	846.7	12068	47.76
10/29/02 14:48	857.2	2		4.05	997.8	991	850.8	12068	47.99
10/29/02 14:49	862.4	2		4.05	997.8	991	855.9	12068	48.28
10/29/02 14:50	840.7	2		4.05	997.8	991	834.4	12068	47.06
10/29/02 14:51	856.2	2		4.05	997.8	991	849.8	12068	47.93
10/29/02 14:52	834.5	2		4.05	997.8	991	828.2	12068	46.72
10/29/02 14:53	811.9	2		4.05	997.8	991	805.6	12068	45.44
10/29/02 14:54	821.2	2		4.05	997.8	991	814.8	12068	45.96
10/29/02 14:55	807.8	2		4.05	997.8	991	801.5	12068	45.21
10/29/02 14:56	802.6	2		4.05	997.8	991	796.4	12068	44.92
10/29/02 14:57	789.2	2		4.05	997.8	991	783.0	12068	44.17
10/29/02 14:58	765.6	2		4.05	997.8	991	759.4	12068	42.84
10/29/02 14:59	768.6	2		4.05	997.8	991	762.5	12068	43.01
10/29/02 15:00	756.3	2		4.05	997.8	991	750.2	12068	42.31
10/29/02 15:01	778.9	2		4.05	997.8	991	772.7	12068	43.59
10/29/02 15:02	772.8	2		4.05	997.8	991	766.6	12068	43.24
10/29/02 15:03	763.5	2		4.05	997.8	991	757.3	12068	42.72
10/29/02 15:04	749.1	2		4.05	997.8	991	743.0	12068	41.91
10/29/02 15:05	728.5	2		4.05	997.8	991	722.4	12068	40.75
10/29/02 15:06	730.5	2		4.05	997.8	991	724.5	12068	40.87
10/29/02 15:07	732.6	2		4.05	997.8	991	726.5	12068	40.98
10/29/02 15:08	722.3	2		4.05	997.8	991	716.3	12068	40.40
10/29/02 15:09	736.7	2		4.05	997.8	991	730.6	12068	41.21
10/29/02 15:10	731.6	2		4.05	997.8	991	725.5	12068	40.92
10/29/02 15:11	742.9	2		4.05	997.8	991	736.9	12068	41.56
10/29/02 15:12	727.4	2		4.05	997.8	991	721.4	12068	40.69
10/29/02 15:13	735.7	2		4.05	997.8	991	729.6	12068	41.16
10/29/02 15:14	742.9	2		4.05	997.8	991	736.8	12068	41.56
10/29/02 15:15	735.7	2		4.05	997.8	991	729.6	12068	41.16
10/29/02 15:16	737.7	2		4.05	997.8	991	731.7	12068	41.27

**Georgia Pacific - Palatka, Florida**  
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**DATA RECORDER PRINTOUT and TEST SUMMARY**

Time	CO, ppm	Run Number	COMMENTS	CO C <sub>s</sub>	CO C <sub>a</sub>	CO C <sub>ua</sub>	CO, ppm Drift Corrected	Flow, SCFM-Dry	CO, pounds per hour
10/29/02 15:17	730.5	2		4.05	997.8	991	724.5	12068	40.87
10/29/02 15:18	715.1	2		4.05	997.8	991	709.1	12068	40.00
10/29/02 15:19	731.6	2		4.05	997.8	991	725.5	12068	40.92
10/29/02 15:20	739.8	2		4.05	997.8	991	733.7	12068	41.39
10/29/02 15:21	732.6	2		4.05	997.8	991	726.5	12068	40.98
10/29/02 15:22	730.5	2		4.05	997.8	991	724.5	12068	40.87
10/29/02 15:23	720.2	2		4.05	997.8	991	714.2	12068	40.29
10/29/02 15:24	708.9	2		4.05	997.8	991	702.9	12068	39.65
10/29/02 15:25	723.3	2		4.05	997.8	991	717.3	12068	40.46
10/29/02 15:26	732.6	2		4.05	997.8	991	726.5	12068	40.98
10/29/02 15:27	713.0	2		4.05	997.8	991	707.0	12068	39.88
10/29/02 15:28	706.9	2		4.05	997.8	991	700.9	12068	39.53
10/29/02 15:29	714.1	2		4.05	997.8	991	708.0	12068	39.94
10/29/02 15:30	704.8	2		4.05	997.8	991	698.8	12068	39.42
10/29/02 15:31	740.8	2		4.05	997.8	991	734.7	12068	41.44
10/29/02 15:32	749.1	2		4.05	997.8	991	743.0	12068	41.91
10/29/02 15:33	737.7			Run 2 Average			788.7		44.49
10/29/02 15:34	739.8								
10/29/02 15:35	731.6								
10/29/02 15:36	720.2								
10/29/02 15:37	726.4								
10/29/02 15:38	723.3								
10/29/02 15:39	500.9								
10/29/02 15:40	6.6								
10/29/02 15:41	2.5		0 CO Cal						
10/29/02 15:42	2.5		0 CO Cal						
10/29/02 15:43	2.5		0 CO Cal						
10/29/02 15:44	8.7								
10/29/02 15:45	758.3								
10/29/02 15:46	996.2		991 CO Cal						
10/29/02 15:47	998.3		991 CO Cal						
10/29/02 15:48	850.0								
10/29/02 15:49	731.6								
10/29/02 15:50	716.1								
10/29/02 15:51	716.1								

Georgia Pacific - Palatka, Florida  
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DATA RECORDER PRINTOUT and TEST SUMMARY

Time	CO, ppm	Run Number	COMMENTS	CO C <sub>1</sub>	CO C <sub>2</sub>	CO C <sub>3A</sub>	CO, ppm Drift Corrected	Flow, SCFM-Dry	CO, pounds per hour
10/31/02 7:13	684.2								
10/31/02 7:14	691.4								
10/31/02 7:15	698.6								
10/31/02 7:16	687.3								
10/31/02 7:17	679.0								
10/31/02 7:18	229.0								
10/31/02 7:19	15.9								
10/31/02 7:20	8.7		0 cal						
10/31/02 7:21	8.7								
10/31/02 7:22	111.6								
10/31/02 7:23	896.3								
10/31/02 7:24	1019.9								
10/31/02 7:25	1022.0		991 cal						
10/31/02 7:26	1022.0		991 cal						
10/31/02 7:27	1022.0		991 cal						
10/31/02 7:28	1022.0		991 cal						
10/31/02 7:29	1022.0		991 cal						
10/31/02 7:30	1730.5								
10/31/02 7:31	1993.1		1994 cal						
10/31/02 7:32	1993.1		1994 cal						
10/31/02 7:33	1993.1		1994 cal						
10/31/02 7:34	1993.1		1994 cal						
10/31/02 7:35	1993.1		1994 cal						
10/31/02 7:36	1971.4								
10/31/02 7:37	1009.6								
10/31/02 7:38	610.1								
10/31/02 7:39	602.8		594 cal						
10/31/02 7:40	602.8								
10/31/02 7:41	599.8								
10/31/02 7:42	657.4								
10/31/02 7:43	558.6								
10/31/02 7:44	322.7								
10/31/02 7:45	309.4		301 cal						
10/31/02 7:46	309.4								
10/31/02 7:47	315.5								
10/31/02 7:48	583.3						#DIV/0!		#DIV/0!
10/31/02 7:49	679.0								
10/31/02 7:50	680.1								
10/31/02 7:51	688.3								
10/31/02 7:52	679.0								
10/31/02 7:53	673.9								
10/31/02 7:54	676.0								
10/31/02 7:55	661.5								
10/31/02 7:56	670.8								
10/31/02 7:57	582.1								
10/31/02 7:58	687.3								
10/31/02 7:59	683.2								
10/31/02 8:00	666.7								
10/31/02 8:01	683.2								

**Georgia Pacific - Palatka, Florida**  
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**DATA RECORDER PRINTOUT and TEST SUMMARY**

Time	CO, ppm	Run Number	COMMENTS	CO C <sub>1</sub>	CO C <sub>2</sub>	CO C <sub>3</sub>	CO, ppm Drift Corrected	Flow, SCFM-Dry	CO, pounds per hour
10/31/02 8:02	678.0								
10/31/02 8:03	673.9								
10/31/02 8:04	681.1								
10/31/02 8:05	692.4								
10/31/02 8:06	672.9								
10/31/02 8:07	692.4								
10/31/02 8:08	698.6								
10/31/02 8:09	680.1								
10/31/02 8:10	687.3								
10/31/02 8:11	685.2								
10/31/02 8:12	680.1								
10/31/02 8:13	689.3								
10/31/02 8:14	691.4								
10/31/02 8:15	682.1								
10/31/02 8:16	690.4								
10/31/02 8:17	688.3								
10/31/02 8:18	690.4								
10/31/02 8:19	688.3								
10/31/02 8:20	674.9								
10/31/02 8:21	682.1								
10/31/02 8:22	697.6								
10/31/02 8:23	682.1								
10/31/02 8:24	682.1								
10/31/02 8:25	693.5								
10/31/02 8:26	687.3								
10/31/02 8:27	692.4								
10/31/02 8:28	680.1								
10/31/02 8:29	689.3								
10/31/02 8:30	694.5								
10/31/02 8:31	681.1								
10/31/02 8:32	687.3								
10/31/02 8:33	687.3								
10/31/02 8:34	667.7								
10/31/02 8:35	664.6								
10/31/02 8:36	667.7								
10/31/02 8:37	655.4								
10/31/02 8:38	670.8								
10/31/02 8:39	667.7								
10/31/02 8:40	674.9								
10/31/02 8:41	691.4								
10/31/02 8:42	693.5								
10/31/02 8:43	704.8								
10/31/02 8:44	717.2								
10/31/02 8:45	717.2								
10/31/02 8:46	728.5								
10/31/02 8:47	721.3								
10/31/02 8:48	720.2								
10/31/02 8:49	719.2								
10/31/02 8:50	719.2								

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**DATA RECORDER PRINTOUT and TEST SUMMARY**

Time	CO, ppm	Run Number	COMMENTS	CO C <sub>1</sub>	CO C <sub>2</sub>	CO C <sub>3A</sub>	CO, ppm Drift Corrected	Flow, SCFM-Dry	CO, pounds per hour
10/31/02 8:51	714.1								
10/31/02 8:52	708.9								
10/31/02 8:53	699.6								
10/31/02 8:54	702.7								
10/31/02 8:55	688.3								
10/31/02 8:56	698.6								
10/31/02 8:57	700.7								
10/31/02 8:58	695.5								
10/31/02 8:59	705.8								
10/31/02 9:00	707.9								
10/31/02 9:01	701.7								
10/31/02 9:02	711.0								
10/31/02 9:03	709.9								
10/31/02 9:04	705.8								
10/31/02 9:05	721.3								
10/31/02 9:06	681.1								
10/31/02 9:07	678.0								
10/31/02 9:08	681.1								
10/31/02 9:09	679.0								
10/31/02 9:10	679.0								
10/31/02 9:11	680.1								
10/31/02 9:12	673.9								
10/31/02 9:13	680.1								
10/31/02 9:14	674.9								
10/31/02 9:15	673.9								
10/31/02 9:16	676.0								
10/31/02 9:17	663.6								
10/31/02 9:18	667.7								
10/31/02 9:19	664.6								
10/31/02 9:20	648.2								
10/31/02 9:21	642.0								
10/31/02 9:22	633.7								
10/31/02 9:23	618.3								
10/31/02 9:24	616.2								
10/31/02 9:25	609.0								
10/31/02 9:26	597.7								
10/31/02 9:27	566.8								
10/31/02 9:28	553.4								
10/31/02 9:29	78.7								
10/31/02 9:30	6.6								
10/31/02 9:31	16.9								
10/31/02 9:32	263.0								
10/31/02 9:33	614.2								
10/31/02 9:34	685.2								
10/31/02 9:35	680.1								
10/31/02 9:36	689.3								
10/31/02 9:37	685.2								
10/31/02 9:38	673.9								
10/31/02 9:39	599.6								



Georgia Pacific - Palatka, Florida  
Bleach Plant Carbon Monoxide Test

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**DATA RECORDER PRINTOUT and TEST SUMMARY**

Time	CO, ppm	Run Number	COMMENTS	CO C <sub>1</sub>	CO C <sub>2</sub>	CO C <sub>3</sub>	CO, ppm Drift Corrected	Flow, SCFM-Dry	CO, pounds per hour
10/31/02 9:40	700.7								
10/31/02 9:41	686.3								
10/31/02 9:42	686.3								
10/31/02 9:43	690.4								
10/31/02 9:44	673.9								
10/31/02 9:45	679.0								
10/31/02 9:46	691.4								
10/31/02 9:47	680.1								
10/31/02 9:48	696.6								
10/31/02 9:49	689.3								
10/31/02 9:50	680.1								
10/31/02 9:51	679.0								
10/31/02 9:52	676.0								
10/31/02 9:53	671.8								
10/31/02 9:54	681.1								
10/31/02 9:55	670.8								
10/31/02 9:56	678.0								
10/31/02 9:57	668.8								
10/31/02 9:58	661.5								
10/31/02 9:59	661.5								
10/31/02 10:00	660.5								
10/31/02 10:01	654.3								
10/31/02 10:02	666.7								
10/31/02 10:03	664.6								
10/31/02 10:04	658.5								
10/31/02 10:05	674.9								
10/31/02 10:06	671.8								
10/31/02 10:07	666.7								
10/31/02 10:08	677.0								
10/31/02 10:09	685.2								
10/31/02 10:10	673.9								
10/31/02 10:11	671.8								
10/31/02 10:12	659.5								
10/31/02 10:13	662.6								
10/31/02 10:14	666.7								
10/31/02 10:15	650.2								
10/31/02 10:16	656.4								
10/31/02 10:17	660.5								
10/31/02 10:18	649.2								
10/31/02 10:19	658.5								
10/31/02 10:20	661.5								
10/31/02 10:21	654.3								
10/31/02 10:22	663.6								
10/31/02 10:23	662.6								
10/31/02 10:24	659.5								
10/31/02 10:25	678.0								
10/31/02 10:26	672.9								
10/31/02 10:27	667.7								
10/31/02 10:28	671.8								

**Georgia Pacific - Palatka, Florida**  
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October 31, 2002

**DATA RECORDER PRINTOUT and TEST SUMMARY**

Time	CO, ppm	Run Number	COMMENTS	CO C <sub>1</sub>	CO C <sub>2</sub>	CO C <sub>3</sub>	CO, ppm Drift Corrected	Flow, SCFM-Dry	CO, pounds per hour
10/31/02 10:29	670.8								
10/31/02 10:30	676.0								
10/31/02 10:31	680.1								
10/31/02 10:32	670.8								
10/31/02 10:33	660.5								
10/31/02 10:34	664.6								
10/31/02 10:35	658.5								
10/31/02 10:36	664.6								
10/31/02 10:37	662.6								
10/31/02 10:38	658.5								
10/31/02 10:39	672.9								
10/31/02 10:40	662.6								
10/31/02 10:41	653.3								
10/31/02 10:42	666.7								
10/31/02 10:43	664.6								
10/31/02 10:44	678.0								
10/31/02 10:45	678.0								
10/31/02 10:46	671.8								
10/31/02 10:47	680.1								
10/31/02 10:48	684.2								
10/31/02 10:49	672.9								
10/31/02 10:50	681.1								
10/31/02 10:51	677.0								
10/31/02 10:52	666.7								
10/31/02 10:53	667.7								
10/31/02 10:54	661.5								
10/31/02 10:55	656.4								
10/31/02 10:56	655.4								
10/31/02 10:57	652.3								
10/31/02 10:58	662.6								
10/31/02 10:59	649.2								
10/31/02 11:00	657.4								
10/31/02 11:01	661.5								
10/31/02 11:02	661.5								
10/31/02 11:03	678.0								
10/31/02 11:04	666.7								
10/31/02 11:05	654.3								
10/31/02 11:06	673.9								
10/31/02 11:07	672.9								
10/31/02 11:08	669.8								
10/31/02 11:09	676.0								
10/31/02 11:10	666.7								
10/31/02 11:11	680.1								
10/31/02 11:12	674.9								
10/31/02 11:13	666.7								
10/31/02 11.14	679.0								
10/31/02 11:15	580.1								
10/31/02 11:16	672.9								
10/31/02 11:17	682.1								

Georgia Pacific - Palatka, Florida  
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October 31, 2002  
**DATA RECORDER PRINTOUT and TEST SUMMARY**

Time	CO, ppm	Run Number	COMMENTS	CO C <sub>s</sub>	CO C <sub>w</sub>	CO C <sub>max</sub>	CO, ppm Drift Corrected	Flow, SCFM-Dry	CO, pounds per hour
10/31/02 11:18	673.9								
10/31/02 11:19	687.3								
10/31/02 11:20	691.4								
10/31/02 11:21	679.0								
10/31/02 11:22	690.4								
10/31/02 11:23	686.3								
10/31/02 11:24	681.1								
10/31/02 11:25	691.4								
10/31/02 11:26	693.5								
10/31/02 11:27	699.6								
10/31/02 11:28	704.8								
10/31/02 11:29	700.7								
10/31/02 11:30	695.5								
10/31/02 11:31	700.7								
10/31/02 11:32	694.5								
10/31/02 11:33	697.6								
10/31/02 11:34	697.6								
10/31/02 11:35	701.7								
10/31/02 11:36	699.6								
10/31/02 11:37	687.3								
10/31/02 11:38	680.1								
10/31/02 11:39	688.3								
10/31/02 11:40	686.3								
10/31/02 11:41	689.3								
10/31/02 11:42	700.7								
10/31/02 11:43	695.5								
10/31/02 11:44	699.6								
10/31/02 11:45	695.5								
10/31/02 11:46	703.8								
10/31/02 11:47	701.7								
10/31/02 11:48	706.9								
10/31/02 11:49	700.7								
10/31/02 11:50	705.8								
10/31/02 11:51	697.6								
10/31/02 11:52	701.7								
10/31/02 11:53	704.8								
10/31/02 11:54	698.6								
10/31/02 11:55	695.5								
10/31/02 11:56	704.8								
10/31/02 11:57	693.5								
10/31/02 11:58	694.5								
10/31/02 11:59	698.6								
10/31/02 12:00	686.3								
10/31/02 12:01	694.5								
10/31/02 12:02	699.6								
10/31/02 12:03	689.3								
10/31/02 12:04	703.8								
10/31/02 12:05	699.6								
10/31/02 12:06	699.6								

**Georgia Pacific - Palatka, Florida  
Bleach Plant Carbon Monoxide Test**

October 31, 2002

**DATA RECORDER PRINTOUT and TEST SUMMARY**

Time	CO, ppm	Run Number	COMMENTS	CO C <sub>s</sub>	CO C <sub>w</sub>	CO C <sub>aa</sub>	CO, ppm Drift Corrected	Flow, SCFM-Dry	CO, pounds per hour
10/31/02 12:07	704.8								
10/31/02 12:08	711.0								
10/31/02 12:09	697.6								
10/31/02 12:10	706.9								
10/31/02 12:11	715.1								
10/31/02 12:12	709.9								
10/31/02 12:13	693.5								
10/31/02 12:14	708.9								
10/31/02 12:15	712.0								
10/31/02 12:16	702.7								
10/31/02 12:17	708.9								
10/31/02 12:18	701.7								
10/31/02 12:19	760.4								
10/31/02 12:20	988.0								
10/31/02 12:21	1000.3		Interim Cal 991						
10/31/02 12:22	1000.3								
10/31/02 12:23	789.2								
10/31/02 12:24	56.0								
10/31/02 12:25	4.5		Interim Cal 0						
10/31/02 12:26	3.5								
10/31/02 12:27	103.4								
10/31/02 12:28	628.6								
10/31/02 12:29	717.2								
10/31/02 12:30	702.7								
10/31/02 12:31	705.8								
10/31/02 12:32	708.9								
10/31/02 12:33	708.9								
10/31/02 12:34	696.6								
10/31/02 12:35	702.7								
10/31/02 12:36	700.7								
10/31/02 12:37	699.6								
10/31/02 12:38	695.5								
10/31/02 12:39	702.7								
10/31/02 12:40	706.9								
10/31/02 12:41	703.8								
10/31/02 12:42	699.6								
10/31/02 12:43	700.7								
10/31/02 12:44	692.4								
10/31/02 12:45	701.7								
10/31/02 12:46	714.1								
10/31/02 12:47	706.9								
10/31/02 12:48	730.5								
10/31/02 12:49	719.2								
10/31/02 12:50	719.2								
10/31/02 12 51	735.7								
10/31/02 12 52	729.5								
10/31/02 12 53	723.3								
10/31/02 12 54	738.8								
10/31/02 12 55	753.2								

Georgia Pacific - Palatka, Florida  
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October 31, 2002  
**DATA RECORDER PRINTOUT and TEST SUMMARY**

Time	CO, ppm	Run Number	COMMENTS	CO C <sub>1</sub>	CO C <sub>2</sub>	CO C <sub>3</sub>	CO, ppm Drift Corrected	Flow, SCFM-Dry	CO, pounds per hour
10/31/02 12:56	764.5								
10/31/02 12:57	791.3								
10/31/02 12:58	805.7								
10/31/02 12:59	824.2								
10/31/02 13:00	852.1								
10/31/02 13:01	875.7								
10/31/02 13:02	887.1								
10/31/02 13:03	900.5								
10/31/02 13:04	941.6								
10/31/02 13:05	969.4								
10/31/02 13:06	981.8								
10/31/02 13:07	1003.4								
10/31/02 13:08	1006.5								
10/31/02 13:09	1008.6								
10/31/02 13:10	1039.5								
10/31/02 13:11	1036.4								
10/31/02 13:12	1032.3								
10/31/02 13:13	1035.4								
10/31/02 13:14	1015.8								
10/31/02 13:15	1006.5								
10/31/02 13:16	1027.1								
10/31/02 13:17	1038.4								
10/31/02 13:18	1039.5								
10/31/02 13:19	1047.7								
10/31/02 13:20	1064.2								
10/31/02 13:21	1057.0								
10/31/02 13:22	1073.5								
10/31/02 13:23	1094.1								
10/31/02 13:24	1092.0								
10/31/02 13:25	1104.4								
10/31/02 13:26	1106.4								
10/31/02 13:27	1111.56								
10/31/02 13:28	1142.453								
10/31/02 13:29	1165.109								
10/31/02 13:30	1159.96	1	<i>Begin Run 1</i>	6.25	1008	991	1141.3	13401	71.49
10/31/02 13:31	1182.615	1		6.25	1008	991	1163.7	13401	72.89
10/31/02 13:32	1194.973	1		6.25	1008	991	1176.0	13401	73.66
10/31/02 13:33	1188.794	1		6.25	1008	991	1169.9	13401	73.28
10/31/02 13:34	1167.168	1		6.25	1008	991	1148.5	13401	71.94
10/31/02 13:35	1166.139	1		6.25	1008	991	1147.4	13401	71.87
10/31/02 13:36	1157.9	1		6.25	1008	991	1135.3	13401	71.36
10/31/02 13:37	1151.722	1		6.25	1008	991	1133.2	13401	70.98
10/31/02 13:38	1162.02	1		6.25	1008	991	1143.4	13401	71.62
10/31/02 13:39	1171.288	1		6.25	1008	991	1152.5	13401	72.19
10/31/02 13:40	1135.245	1		6.25	1008	991	1116.9	13401	69.96
10/31/02 13:41	1149.662	1		6.25	1008	991	1131.1	13401	70.85
10/31/02 13:42	1164.079	1		6.25	1008	991	1145.4	13401	71.75
10/31/02 13:43	1155.841	1		6.25	1008	991	1137.3	13401	71.24
10/31/02 13:44	1170.258	1		6.25	1008	991	1151.5	13401	72.10

**Georgia Pacific - Palatka, Florida**  
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**DATA RECORDER PRINTOUT and TEST SUMMARY**

Time	CO, ppm	Run Number	COMMENTS	CO C <sub>1</sub>	CO C <sub>2</sub>	CO C <sub>3</sub>	CO, ppm Drift Corrected	Flow, SCFM-Dry	CO, pounds per hour
10/31/02 13:45	1171.288	1		6.25	1008	991	1152.5	13401	72.19
10/31/02 13:46	1153.781	1		6.25	1008	991	1135.2	13401	71.11
10/31/02 13:47	1178.496	1		6.25	1008	991	1159.7	13401	72.64
10/31/02 13:48	1194.973	1		6.25	1008	991	1176.0	13401	73.66
10/31/02 13:49	1194.973	1		6.25	1008	991	1176.0	13401	73.66
10/31/02 13:50	1215.569	1		6.25	1008	991	1196.3	13401	74.94
10/31/02 13:51	1181.585	1		6.25	1008	991	1162.7	13401	72.83
10/31/02 13:52	1190.854	1		6.25	1008	991	1171.9	13401	73.40
10/31/02 13:53	1165.109	1		6.25	1008	991	1146.4	13401	71.81
10/31/02 13:54	1147.602	1		6.25	1008	991	1129.1	13401	70.72
10/31/02 13:55	1141.424	1		6.25	1008	991	1123.0	13401	70.34
10/31/02 13:56	1135.245	1		6.25	1008	991	1116.9	13401	69.96
10/31/02 13:57	1142.453	1		6.25	1008	991	1124.0	13401	70.41
10/31/02 13:58	1144.513	1		6.25	1008	991	1126.0	13401	70.53
10/31/02 13:59	1130.096	1		6.25	1008	991	1111.8	13401	69.64
10/31/02 14:00	1141.424	1		6.25	1008	991	1123.0	13401	70.34
10/31/02 14:01	1115.679	1		6.25	1008	991	1097.5	13401	68.75
10/31/02 14:02	1139.364	1		6.25	1008	991	1121.0	13401	70.21
10/31/02 14:03	1142.453	1		6.25	1008	991	1124.0	13401	70.41
10/31/02 14:04	1132.156	1		6.25	1008	991	1113.8	13401	69.77
10/31/02 14:05	1147.602	1		6.25	1008	991	1129.1	13401	70.72
10/31/02 14:06	1182.615	1		6.25	1008	991	1163.7	13401	72.89
10/31/02 14:07	1173.347	1		6.25	1008	991	1154.6	13401	72.32
10/31/02 14:08	1190.854	1		6.25	1008	991	1171.9	13401	73.40
10/31/02 14:09	1227.926	1		6.25	1008	991	1208.6	13401	75.70
10/31/02 14:10	1205.271	1		6.25	1008	991	1186.2	13401	74.30
10/31/02 14:11	1191.883	1		6.25	1008	991	1172.9	13401	73.47
10/31/02 14:12	1225.866	1		6.25	1008	991	1206.5	13401	75.57
10/31/02 14:13	1212.479	1		6.25	1008	991	1193.3	13401	74.74
10/31/02 14:14	1186.734	1		6.25	1008	991	1167.8	13401	73.15
10/31/02 14:15	1221.747	1		6.25	1008	991	1202.5	13401	75.32
10/31/02 14:16	1196.003	1		6.25	1008	991	1177.0	13401	73.72
10/31/02 14:17	1157.9	1		6.25	1008	991	1139.3	13401	71.36
10/31/02 14:18	1186.734	1		6.25	1008	991	1167.8	13401	73.15
10/31/02 14:19	1186.734	1		6.25	1008	991	1167.8	13401	73.15
10/31/02 14:20	1178.496	1		6.25	1008	991	1159.7	13401	72.64
10/31/02 14:21	1200.122	1		6.25	1008	991	1181.1	13401	73.98
10/31/02 14:22	1172.317	1		6.25	1008	991	1153.6	13401	72.26
10/31/02 14:23	1178.496	1		6.25	1008	991	1159.7	13401	72.64
10/31/02 14:24	1200.122	1		6.25	1008	991	1181.1	13401	73.98
10/31/02 14:25	1184.675	1		6.25	1008	991	1165.8	13401	73.02
10/31/02 14:26	1194.973	1		6.25	1008	991	1176.0	13401	73.66
10/31/02 14:27	1195.734	1		6.25	1008	991	1167.8	13401	73.15
10/31/02 14:28	1135.705	1		6.25	1008	991	1166.8	13401	73.09
10/31/02 14:29	1218.658	1		6.25	1008	991	1199.4	13401	75.13
10/31/02 14:30	1220.718								
				<b>Run 1 Average</b>			<b>1155.1</b>		<b>72.35</b>
10/31/02 14:31	1206.3								
10/31/02 14:32	1235.164								
10/31/02 14:33	1118.768								

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**DATA RECORDER PRINTOUT and TEST SUMMARY**

Time	CO, ppm	Run Number	COMMENTS	CO C <sub>s</sub>	CO C <sub>w</sub>	CO C <sub>MA</sub>	CO, ppm Drift Corrected	Flow, SCFM-Dry	CO, pounds per hour
10/31/02 14:34	159.004								
10/31/02 14:35	6.5951								
10/31/02 14:36	3.5057		Zero CO Cal						
10/31/02 14:37	3.5057		Zero CO Cal						
10/31/02 14:38	8.6546								
10/31/02 14:39	656.3926								
10/31/02 14:40	989.0148								
10/31/02 14:41	995.1935		991 CO Cal						
10/31/02 14:42	995.1935		991 CO Cal						
10/31/02 14:43	1068.309								
10/31/02 14:44	1213.509								
10/31/02 14:45	1194.973								
10/31/02 14:46	1191.883								
10/31/02 14:47	1166.139								
10/31/02 14:48	1138.334								
10/31/02 14:49	1182.615								
10/31/02 14:50	1179.526								
10/31/02 14:51	1163.049								
10/31/02 14:52	1172.317								
10/31/02 14:53	1160.99								
10/31/02 14:54	1174.377								
10/31/02 14:55	1160.99								
10/31/02 14:56	1171.288								
10/31/02 14:57	1190.854								
10/31/02 14:58	1191.883								
10/31/02 14:59	1176.437								
10/31/02 15:00	1190.854								
10/31/02 15:01	1192.913								
10/31/02 15:02	1191.883								
10/31/02 15:03	1215.569								
10/31/02 15:04	1186.734								
10/31/02 15:05	1169.228								
10/31/02 15:06	1178.496								
10/31/02 15:07	1181.585								
10/31/02 15:08	1187.764								
10/31/02 15:09	1217.628								
10/31/02 15:10	1228.956								
10/31/02 15:11	1193.943								
10/31/02 15:12	1201.151								
10/31/02 15:13	1210.42								
10/31/02 15:14	1228.956								
10/31/02 15:15	1200.122								
10/31/02 15:16	1233.075								
10/31/02 15:17	1228.956								
10/31/02 15:18	1199.092								
10/31/02 15:19	1219.688								
10/31/02 15:20	1237.194								
10/31/02 15:21	1208.36								
10/31/02 15:22	1221.747								

**Georgia Pacific - Palatka, Florida**  
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October 31, 2002  
**DATA RECORDER PRINTOUT and TEST SUMMARY**

Time	CO, ppm	Run Number	COMMENTS	CO C <sub>1</sub>	CO C <sub>2</sub>	CO C <sub>3</sub>	CO, ppm Drift Corrected	Flow, SCFM-Dry	CO, pounds per hour
10/31/02 15:23	1214.539								
10/31/02 15:24	1203.211								
10/31/02 15:25	1205.271								
10/31/02 15:26	1229.986								
10/31/02 15:27	1212.479								
10/31/02 15:28	1200.122								
10/31/02 15:29	1242.343								
10/31/02 15:30	1227.926								
10/31/02 15:31	1227.926								
10/31/02 15:32	1243.373								
10/31/02 15:33	1216.598								
10/31/02 15:34	1221.747								
10/31/02 15:35	1202.181								
10/31/02 15:36	1218.658								
10/31/02 15:37	1213.509								
10/31/02 15:38	1211.449								
10/31/02 15:39	1221.747								
10/31/02 15:40	1209.39								
10/31/02 15:41	1217.628								
10/31/02 15:42	1234.105								
10/31/02 15:43	1216.598								
10/31/02 15:44	1205.271								
10/31/02 15:45	1209.39								
10/31/02 15:46	1194.973		<i>Begin Run 2</i>						
10/31/02 15:47	1190.854	2		4	995.5	991	1186.3	13171	73.03
10/31/02 15:48	1209.39	2		4	995.5	991	1204.8	13171	74.17
10/31/02 15:49	1221.747	2		4	995.5	991	1217.1	13171	74.93
10/31/02 15:50	1209.39	2		4	995.5	991	1204.8	13171	74.17
10/31/02 15:51	1240.284	2		4	995.5	991	1235.7	13171	76.07
10/31/02 15:52	1235.135	2		4	995.5	991	1230.5	13171	75.75
10/31/02 15:53	1231.015	2		4	995.5	991	1226.4	13171	75.50
10/31/02 15:54	1245.432	2		4	995.5	991	1240.8	13171	76.39
10/31/02 15:55	1211.449	2		4	995.5	991	1206.8	13171	74.30
10/31/02 15:56	1201.151	2		4	995.5	991	1196.5	13171	73.66
10/31/02 15:57	1229.986	2		4	995.5	991	1225.4	13171	75.44
10/31/02 15:58	1215.569	2		4	995.5	991	1211.0	13171	74.55
10/31/02 15:59	1216.598	2		4	995.5	991	1212.0	13171	74.61
10/31/02 16:00	1223.807	2		4	995.5	991	1219.2	13171	75.06
10/31/02 16:01	1196.003	2		4	995.5	991	1191.4	13171	73.35
10/31/02 16:02	1197.032	2		4	995.5	991	1192.4	13171	73.41
10/31/02 16:03	1182.615	2		4	995.5	991	1178.0	13171	72.52
10/31/02 16:04	1170.258	2		4	995.5	991	1165.7	13171	71.76
10/31/02 16:05	1185.705	2		4	995.5	991	1181.1	13171	72.71
10/31/02 16:06	1177.466	2		4	995.5	991	1172.9	13171	72.21
10/31/02 16:07	1186.734	2		4	995.5	991	1182.1	13171	73.08
10/31/02 16:08	1192.913	2		4	995.5	991	1188.3	13171	73.76
10/31/02 16:09	1198.062	2		4	995.5	991	1193.5	13171	74.47
10/31/02 16:10	1226.896	2		4	995.5	991	1222.3	13171	75.25
10/31/02 16:11	1211.449	2		4	995.5	991	1206.8	13171	74.30



**Georgia Pacific - Palatka, Florida**  
**Bleach Plant Carbon Monoxide Test**

October 31, 2002

**DATA RECORDER PRINTOUT and TEST SUMMARY**

Time	CO ppm	Run Number	COMMENTS	CO C <sub>1</sub>	CO C <sub>2</sub>	CO C <sub>3</sub>	CO ppm Drift Corrected	Flow, SCFM-Dry	CO, pounds per hour
10/31/02 16:12	1214.539	2		4	995.5	991	1209.9	13171	74.49
10/31/02 16:13	1219.688	2		4	995.5	991	1215.1	13171	74.80
10/31/02 16:14	1215.569	2		4	995.5	991	1211.0	13171	74.55
10/31/02 16:15	1200.122	2		4	995.5	991	1195.5	13171	73.60
10/31/02 16:16	1198.062	2		4	995.5	991	1193.5	13171	73.47
10/31/02 16:17	1194.973	2		4	995.5	991	1190.4	13171	73.28
10/31/02 16:18	1206.3	2		4	995.5	991	1201.7	13171	73.98
10/31/02 16:19	1210.42	2		4	995.5	991	1205.8	13171	74.23
10/31/02 16:20	1221.747	2		4	995.5	991	1217.1	13171	74.93
10/31/02 16:21	1216.598	2		4	995.5	991	1212.0	13171	74.61
10/31/02 16:22	1208.36	2		4	995.5	991	1203.8	13171	74.11
10/31/02 16:23	1199.092	2		4	995.5	991	1194.5	13171	73.54
10/31/02 16:24	1219.688	2		4	995.5	991	1215.1	13171	74.80
10/31/02 16:25	1216.598	2		4	995.5	991	1212.0	13171	74.61
10/31/02 16:26	1207.33	2		4	995.5	991	1202.7	13171	74.04
10/31/02 16:27	1217.628	2		4	995.5	991	1213.0	13171	74.68
10/31/02 16:28	1211.449	2		4	995.5	991	1206.8	13171	74.30
10/31/02 16:29	1224.837	2		4	995.5	991	1220.2	13171	75.12
10/31/02 16:30	1244.403	2		4	995.5	991	1239.8	13171	76.32
10/31/02 16:31	1240.284	2		4	995.5	991	1235.7	13171	76.07
10/31/02 16:32	1235.135	2		4	995.5	991	1230.5	13171	75.75
10/31/02 16:33	1241.313	2		4	995.5	991	1236.7	13171	76.13
10/31/02 16:34	1231.015	2		4	995.5	991	1226.4	13171	75.50
10/31/02 16:35	1238.224	2		4	995.5	991	1233.6	13171	75.94
10/31/02 16:36	1251.611	2		4	995.5	991	1247.0	13171	76.77
10/31/02 16:37	1236.164	2		4	995.5	991	1231.5	13171	75.82
10/31/02 16:38	1234.105	2		4	995.5	991	1229.5	13171	75.69
10/31/02 16:39	1234.105	2		4	995.5	991	1229.5	13171	75.69
10/31/02 16:40	1232.045	2		4	995.5	991	1227.4	13171	75.56
10/31/02 16:41	1222.777	2		4	995.5	991	1218.2	13171	74.99
10/31/02 16:42	1225.866	2		4	995.5	991	1221.2	13171	75.18
10/31/02 16:43	1233.075	2		4	995.5	991	1228.5	13171	75.63
10/31/02 16:44	1225.866	2		4	995.5	991	1221.2	13171	75.18
10/31/02 16:45	1233.075	2		4	995.5	991	1228.5	13171	75.63
10/31/02 16:46	1241.313	2		4	995.5	991	1236.7	13171	76.13
10/31/02 16:47	1240.284								
10/31/02 16:48	1232.045								
10/31/02 16:49	1254.701								
10/31/02 16:50	1280.445								
10/31/02 16:51	1276.326								
10/31/02 16:52	1218.658								
10/31/02 16:53	982.836								
10/31/02 16:54	996.2233		991 CO Cal						
10/31/02 16:55	996.2233								
10/31/02 16:56	862.3506								
10/31/02 16:57	81.7697								
10/31/02 16:58	4.5355								
10/31/02 16:59	4.5355		0 CO Cal						
10/31/02 17:00	4.5355								
<b>Run 2 Average</b>							<b>1212.2</b>	<b>13171</b>	<b>74.6</b>

**Georgia Pacific - Palatka, Florida**  
**Bleach Plant Carbon Monoxide Test**

October 31, 2002

**DATA RECORDER PRINTOUT and TEST SUMMARY**

Time	CO, ppm	Run Number	COMMENTS	CO C <sub>1</sub>	CO C <sub>2</sub>	CO C <sub>3</sub>	CO, ppm Drift Corrected	Flow, SCFM-Dry	CO, pounds per hour
10/31/02 17:01	4.5355								
10/31/02 17:02	4.5355								
10/31/02 17:03	713.031								
10/31/02 17:04	1258.82								
10/31/02 17:05	1270.147								
10/31/02 17:06	1279.416								
10/31/02 17:07	1303.101								
10/31/02 17:08	1293.833								
10/31/02 17:09	1296.922		<i>Begin Run 3</i>						
10/31/02 17:10	1322.667	3		4.5	996.5	991	1316.8	12999	80.01
10/31/02 17:11	1314.428	3		4.5	996.5	991	1308.6	12999	79.51
10/31/02 17:12	1292.803	3		4.5	996.5	991	1287.0	12999	78.20
10/31/02 17:13	1296.922	3		4.5	996.5	991	1291.1	12999	78.45
10/31/02 17:14	1282.505	3		4.5	996.5	991	1276.7	12999	77.57
10/31/02 17:15	1256.76	3		4.5	996.5	991	1251.0	12999	76.01
10/31/02 17:16	1223.807	3		4.5	996.5	991	1218.1	12999	74.01
10/31/02 17:17	1246.462	3		4.5	996.5	991	1240.7	12999	75.38
10/31/02 17:18	1213.509	3		4.5	996.5	991	1207.8	12999	73.38
10/31/02 17:19	1224.837	3		4.5	996.5	991	1219.1	12999	74.07
10/31/02 17:20	1255.73	3		4.5	996.5	991	1250.0	12999	75.95
10/31/02 17:21	1256.76	3		4.5	996.5	991	1251.0	12999	76.01
10/31/02 17:22	1245.432	3		4.5	996.5	991	1239.7	12999	75.32
10/31/02 17:23	1259.849	3		4.5	996.5	991	1254.1	12999	76.20
10/31/02 17:24	1260.879	3		4.5	996.5	991	1255.1	12999	76.26
10/31/02 17:25	1267.058	3		4.5	996.5	991	1261.3	12999	76.63
10/31/02 17:26	1287.654	3		4.5	996.5	991	1281.9	12999	77.88
10/31/02 17:27	1280.445	3		4.5	996.5	991	1274.7	12999	77.45
10/31/02 17:28	1263.969	3		4.5	996.5	991	1258.2	12999	76.45
10/31/02 17:29	1277.356	3		4.5	996.5	991	1271.6	12999	77.26
10/31/02 17:30	1294.862	3		4.5	996.5	991	1289.1	12999	78.32
10/31/02 17:31	1281.475	3		4.5	996.5	991	1275.7	12999	77.51
10/31/02 17:32	1269.118	3		4.5	996.5	991	1263.3	12999	76.76
10/31/02 17:33	1268.088	3		4.5	996.5	991	1262.3	12999	76.70
10/31/02 17:34	1252.641	3		4.5	996.5	991	1246.9	12999	75.76
10/31/02 17:35	1231.015	3		4.5	996.5	991	1225.3	12999	74.45
10/31/02 17:36	1248.522	3		4.5	996.5	991	1242.8	12999	75.51
10/31/02 17:37	1234.105	3		4.5	996.5	991	1228.4	12999	74.63
10/31/02 17:38	1242.343	3		4.5	996.5	991	1236.6	12999	75.13
10/31/02 17:39	1253.671	3		4.5	996.5	991	1247.9	12999	75.82
10/31/02 17:40	1234.105	3		4.5	996.5	991	1228.4	12999	74.63
10/31/02 17:41	1227.926	3		4.5	996.5	991	1222.2	12999	74.26
10/31/02 17:42	1250.581	3		4.5	996.5	991	1244.8	12999	75.63
10/31/02 17:43	1240.284	3		4.5	996.5	991	1234.8	12999	75.01
10/31/02 17:44	1247.492	3		4.5	996.5	991	1241.7	12999	75.45
10/31/02 17:45	1254.701	3		4.5	996.5	991	1248.9	12999	75.82
10/31/02 17:46	1238.224	3		4.5	996.5	991	1232.5	12999	74.82
10/31/02 17:47	1240.284	3		4.5	996.5	991	1234.8	12999	75.01
10/31/02 17:48	1256.76	3		4.5	996.5	991	1251.0	12999	76.01
10/31/02 17:49	1249.552	3		4.5	996.5	991	1242.8	12999	75.51

**Georgia Pacific - Palatka, Florida**  
**Bleach Plant Carbon Monoxide Test**

October 31, 2002

**DATA RECORDER PRINTOUT and TEST SUMMARY**

Time	CO, ppm	Run Number	COMMENTS	CO C <sub>1</sub>	CO C <sub>2</sub>	CO C <sub>3</sub>	CO, ppm Drift Corrected	Flow, SCFM-Dry	CO, pounds per hour
10/31/02 17:50	1278.386	3		4.5	996.5	991	1272.6	12999	77.32
10/31/02 17:51	1292.803	3		4.5	996.5	991	1287.0	12999	78.20
10/31/02 17:52	1252.641	3		4.5	996.5	991	1246.9	12999	75.76
10/31/02 17:53	1244.403	3		4.5	996.5	991	1238.7	12999	75.26
10/31/02 17:54	1267.058	3		4.5	996.5	991	1261.3	12999	76.63
10/31/02 17:55	1237.194	3		4.5	996.5	991	1231.5	12999	74.82
10/31/02 17:56	1227.926	3		4.5	996.5	991	1222.2	12999	74.26
10/31/02 17:57	1244.403	3		4.5	996.5	991	1238.7	12999	75.26
10/31/02 17:58	1236.164	3		4.5	996.5	991	1230.4	12999	74.76
10/31/02 17:59	1232.045	3		4.5	996.5	991	1226.3	12999	74.51
10/31/02 18:00	1203.211	3		4.5	996.5	991	1197.5	12999	72.76
10/31/02 18:01	1145.543	3		4.5	996.5	991	1139.9	12999	69.26
10/31/02 18:02	1080.666	3		4.5	996.5	991	1075.1	12999	65.32
10/31/02 18:03	1049.772	3		4.5	996.5	991	1044.2	12999	63.45
10/31/02 18:04	1069.338	3		4.5	996.5	991	1063.8	12999	64.63
10/31/02 18:05	1129.066	3		4.5	996.5	991	1123.4	12999	68.26
10/31/02 18:06	1173.347	3		4.5	996.5	991	1167.7	12999	70.95
10/31/02 18:07	1174.377	3		4.5	996.5	991	1168.7	12999	71.01
10/31/02 18:08	1167.168	3		4.5	996.5	991	1161.5	12999	70.57
10/31/02 18:09	1150.692	3		4.5	996.5	991	1145.0	12999	69.57
10/31/02 18:10	1134.215								
10/31/02 18:11	1163.049								
10/31/02 18:12	350.5449								
10/31/02 18:13	17.9228								
10/31/02 18:14	4.5355		0 CO Cal						
10/31/02 18:15	4.5355								
10/31/02 18:16	149.7359								
10/31/02 18:17	894.274								
10/31/02 18:18	997.2531		991 CO Cal						
10/31/02 18:19	998.2829								
10/31/02 18:20	968.4189								
<b>Run 3 Average</b>							<b>1231.0</b>		<b>74.8</b>

**APPENDIX - C**

**Laboratory Analysis**

# TECHNICAL SERVICES, INC.

## ENVIRONMENTAL CONSULTANTS

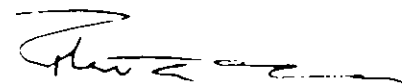
For Ambient Air Services, Inc.  
106 AMBIENT AIR WAY  
STARKE, FL 32091  
Contact: Joe Cooksey

Report Date 11-Nov-02  
Date Received 11/01/2002 @ 16:15  
Purchase Order #

### CERTIFICATE OF ANALYSIS

LAB SAMPLE DESCRIPTION	MATRIX	SAMPLE DATE	SAMPLE TIME	SAMPLED BY
02110037 GP/PALATKA, BLEACH PLANT, RUN 1	IMP. CATCH	10/31/2002	UNKNOWN	
02110038 GP/PALATKA, BLEACH PLANT, RUN 2	IMP. CATCH	10/31/2002	UNKNOWN	
02110039 GP/PALATKA, BLEACH PLANT, RUN 3	IMP. CATCH	10/31/2002	UNKNOWN	
02110040 GP/PALATKA, BLEACH PLANT, RUN 1	IMP. CATCH	10/29/2002	UNKNOWN	
02110041 GP/PALATKA, BLEACH PLANT, RUN 2	IMP. CATCH	10/29/2002	UNKNOWN	
02110042 GP/PALATKA, BLEACH PLANT, RUN 3	IMP. CATCH	10/29/2002	UNKNOWN	
02110043 GP/PALATKA, BLEACH PLANT, FIELD BLANK		UNKNOWN	UNKNOWN	

Respectfully submitted,  
Technical Services, Inc



Air and Water Pollution Sampling, Surveys, Testing and Analytical Services

2301 Danese Street • Jacksonville, Florida 32216 • 904-353-5761 • FAX 904-358-2338

Ambient Air Services, Inc

Lab No	Parameter	Result		Code	Method	Detection Limit
02110037	Chloride in base	214.2	ug/ml Cl-	A	Method 26A	0.02
02110038	Chloride in base	134.3	ug/ml Cl-		Method 26A	0.02
02110039	Chloride in base	151.1	TOTAL UG		Method 26A	0.02
02110040	Chloride in base	438.9	TOTAL UG		Method 26A	0.02
02110041	Chloride in base	320.0	TOTAL UG		Method 26A	0.02
02110042	Chloride in base	354.6	TOTAL UG		Method 26A	0.02
02110043	Chloride in base	104.3	TOTAL UG	A	Method 26A	0.02

Ambient Air Services, Inc

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Lab No	Parameter	Date of Analysis	Analysis Time	Analyst	Prep Date
02110037	Chloride in base	11/11/2002		CRB	
02110038	Chloride in base	11/11/2002		CRB	
02110039	Chloride in base	11/11/2002		CRB	
02110040	Chloride in base	11/11/2002		CRB	
02110041	Chloride in base	11/11/2002		CRB	
02110042	Chloride in base	11/11/2002		CRB	
02110043	Chloride in base	11/11/2002		CRB	

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**APPENDIX - D**

- Equipment Calibration Data**
- Carbon Monoxide Analyzer Calibration
    - Annual Meter Calibration
    - Post Test Meter Calibration
    - Pitot Tube Calibration
    - Thermocouple Calibration





Georgia Pacific - Palatka, Florida  
 Bleach Plant Carbon Monoxide Test  
 0  
 October 29, 2002  
 Calibration Sheet

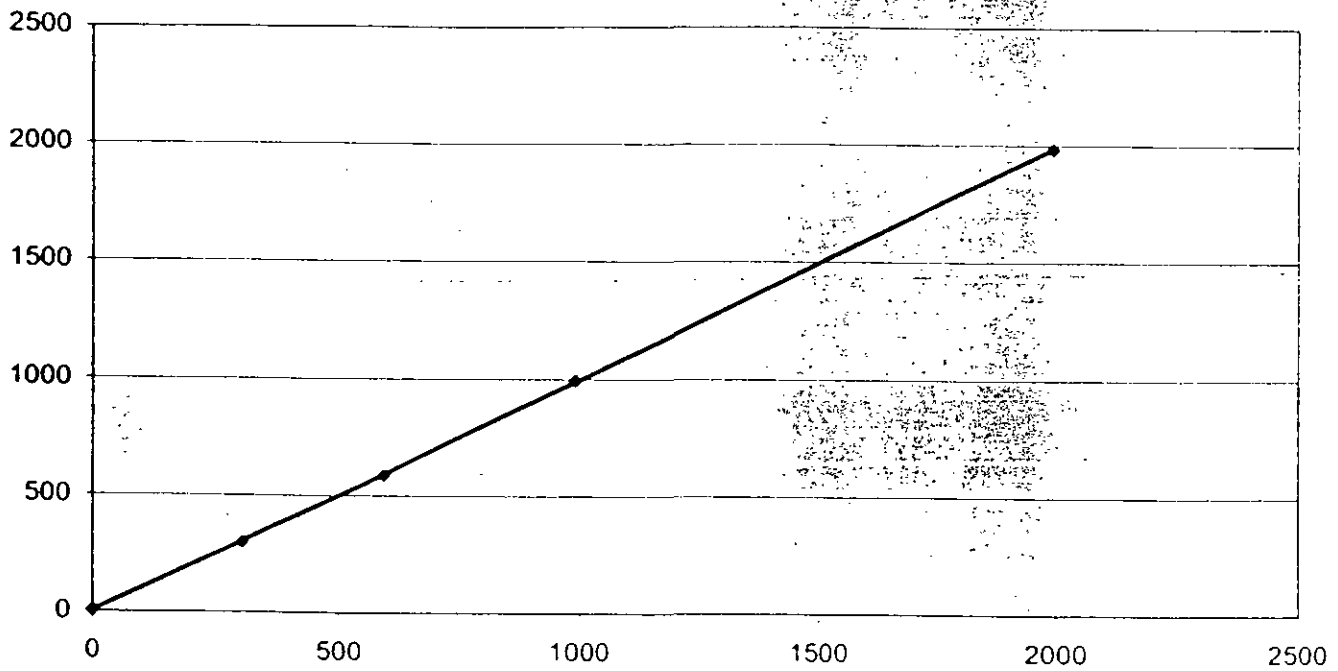
**Initial Calibration  
 Response Table**

Inject (ppm)		Time	Response (ppm)
Gas	Conc.		CO
Zero	0	12:00	4
CO	991	12:00	995.4
CO	1994	12:00	1982.2
CO	594.4	12:00	588
CO	301.9	12:00	299.1

**% Error of Range Table**

Inject (ppm)		Time	% Error of Range
Gas	Conc.		CO
Zero	0	12:00	0.20%
CO	991	12:00	0.22%
CO	1994	12:00	-0.59%
CO	594.4	12:00	-0.32%
CO	301.9	12:00	-0.14%

**Calibration Error Check**       $y = 0.9941x + 2.0399$   
 CO       $R^2 = 1$



Georgia Pacific - Palatka, Florida  
 Bleach Plant Carbon Monoxide Test  
 0  
 October 29, 2002  
 Calibration Sheet

**Calibration - Post Run 1**

**Response Table**

Inject (ppm)		Time	Response (ppm)
Gas	Conc.		CO
Zero	0	13:30	5.6
CO	991	13:30	998.3

**Drift Analysis From Initial Calibrations to the End of Run 1**

Inject (ppm)		Time	Drift Analysis (%)
Gas	Conc.		CO
Zero	0	13:30	0.08%
CO	991	13:30	0.14%

**Drift Variables for Run 1**

Variable	CO
Co	4.80
Cm	996.85
Cma	991.00

**Calibration - Post Run 2**

**Response Table**

Inject (ppm)		Time	Response (ppm)
Gas	Conc.		CO
Zero	0		2.5
CO	991		997.3

**Drift Analysis From Initial Calibrations to the End of Run 2**

Inject (ppm)		Time	Drift Analysis (%)
Gas	Conc.		CO
Zero	0	0:00	-0.08%
CO	991	0:00	0.09%

**Drift Variables for Run 2**

Variable	CO
Co	4.05
Cm	997.80
Cma	991

**Calibration - Post Run 3**

**Response Table**

Inject (ppm)		Time	Response (ppm)
Gas	Conc.		CO
Zero	0		
CO	991		

**Drift Analysis From Initial Calibrations to the End of Run 3**

Inject (ppm)		Time	Drift Analysis (%)
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**Georgia Pacific - Palatka, Florida**  
**Bleach Plant Carbon Monoxide Test**  
 0  
 October 29, 2002  
**Calibration Sheet**

Gas	Conc.		CO
Zero	0	0.00	-0.20%
CO	991	0.00	-49.77%

**Drift Variables for Run 3**

Variable	CO	
Co	1.25	
Cm	498.65	
Cma	991	



Georgia Pacific - Palatka, Florida  
 Bleach Plant Carbon Monoxide Test  
 0  
 October 31, 2002  
 Calibration Sheet

**Initial Calibration  
 Response Table**

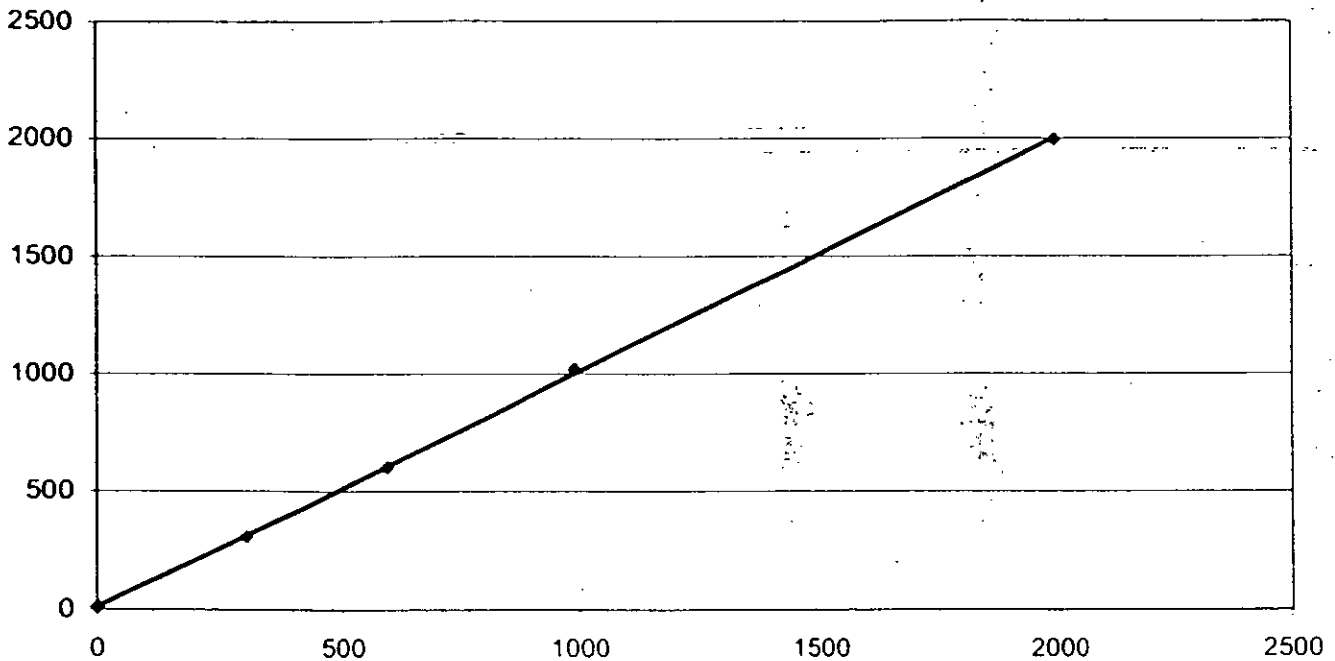
Inject (ppm)		Time	Response (ppm)
Gas	Conc.		CO
Zero	0	12:00	9
CO	991	12:00	1021
CO	1994	12:00	1994
CO	594.4	12:00	602
CO	301.9	12:00	309

**% Error of Range Table**

Inject (ppm)		Time	% Error of Range
Gas	Conc.		CO
Zero	0	12:00	0.45%
CO	991	12:00	1.50%
CO	1994	12:00	0.00%
CO	594.4	12:00	0.38%
CO	301.9	12:00	0.36%

**Calibration Error Check  
 CO**

$y = 0.9978x + 12.46$   
 $R^2 = 0.9998$



Georgia Pacific - Palatka, Florida  
 Bleach Plant Carbon Monoxide Test  
 0  
 October 31, 2002  
 Calibration Sheet

**Calibration - Post Run 1**

**Response Table**

Inject (ppm)		Time	Response (ppm)
Gas	Conc.		CO
Zero	0	14:36	3.5
CO	991	14:42	995

**Drift Analysis From Initial Calibrations to the End of Run 1**

Inject (ppm)		Time	Drift Analysis (%)
Gas	Conc.		CO
Zero	0	14:36	-0.28%
CO	991	14:42	-1.30%

**Drift Variables for Run 1**

Variable	CO
Co	6.25
Cm	1008.00
Cma	991.00

**Calibration - Post Run 2**

**Response Table**

Inject (ppm)		Time	Response (ppm)
Gas	Conc.		CO
Zero	0	16:59	4.5
CO	991	16:54	996

**Drift Analysis From Initial Calibrations to the End of Run 2**

Inject (ppm)		Time	Drift Analysis (%)
Gas	Conc.		CO
Zero	0	16:59	-0.23%
CO	991	16:54	-1.25%

**Drift Variables for Run 2**

Variable	CO
Co	4
Cm	995.50
Cma	991

**Calibration - Post Run 3**

**Response Table**

Inject (ppm)		Time	Response (ppm)
Gas	Conc.		CO
Zero	0	18:14	4.5
CO	991	18:18	997

**Drift Analysis From Initial Calibrations to the End of Run 3**

Inject (ppm)	Time	Drift Analysis (%)
--------------	------	--------------------

Georgia Pacific - Palatka, Florida  
Bleach Plant Carbon Monoxide Test  
0  
October 31, 2002  
Calibration Sheet

Gas	Conc.		CO
Zero	0	18:14	-0.23%
CO	991	18:18	-1.20%

Drift Variables for Run 3

Variable	CO	
Co	4.5	
Cm	996.50	
Cma	991	



Ambient Air Services, Inc. - Method 5 Dry Gas Meter Annual Calibration

USING CALIBRATED CRITICAL ORIFICES

5-POINT ENGLISH UNITS

Meter Console Information	
Console Model Number	AASI
Console Serial Number	Box 10
DGM Model Number	8847372
DGM Serial Number	

Calibration Conditions			
Date	Time	5-Sep-02	10:00
Barometric Pressure		29.8	in Hg
Theoretical Critical Vacuum <sup>1</sup>		14.1	in Hg
Calibration Technician		JOE ELLIOTT	

Factors/Conversions	
Std Temp	528 °R
Std Press	29.92 in Hg
K <sub>c</sub>	17.647

<sup>1</sup>For valid test results, the Actual Vacuum should be 1 to 2 in. Hg greater than the Theoretical Critical Vacuum shown above.

<sup>2</sup>The Critical Orifice Coefficient, K', must be entered in English units, (ft<sup>3</sup>R<sup>1/2</sup>)/(in.Hg<sup>1/2</sup>min).

Calibration Data										
Run Time	Metering Console					Critical Orifice				
	DGM Orifice ΔH (P <sub>in</sub> ) in H <sub>2</sub> O	Volume Initial (V <sub>in</sub> ) cubic feet	Volume Final (V <sub>out</sub> ) cubic feet	Outlet Temp Initial (t <sub>in</sub> ) °F	Outlet Temp Final (t <sub>out</sub> ) °F	Serial Number	Coefficient K'	Amb Temp Initial (t <sub>amb</sub> ) °F	Amb Temp Final (t <sub>amb</sub> ) °F	Actual Vacuum in Hg
14.1	2.8	55.603	67.154	92	92	63	0.6213	89	89	21
6.0	4.6	67.154	75.011	98	98	73	0.8486	83	80	19
11.7	1.4	75.011	82.876	99	98	55	0.4793	81	79	22
11.4	0.8	82.876	88.974	98	99	48	0.3740	79	77	24
18.4	0.4	88.974	95.110	99	99	40	0.2511	77	77	24

Standardized Data				Results				
Dry Gas Meter		Critical Orifice		Calibration Factor		Dry Gas Meter		
(V <sub>meter</sub> ) cubic feet	(Q <sub>meter</sub> ) cfm	(V <sub>cor</sub> ) cubic feet	(Q <sub>cor</sub> ) cfm	Value (Y)	Variation (ΔY)	Flowrate Std & Corr (Q <sub>meter</sub> ) cfm	ΔH @ (ΔH@) in H <sub>2</sub> O	Variation (ΔΔH@)
11.080	0.786	11.142	0.790	1.006	0.007	0.790	2.438	0.388
7.409	1.248	8.520	1.087	0.871	-0.128	1.087	2.114	0.083
7.431	0.635	7.191	0.615	0.968	-0.031	0.615	1.978	-0.072
5.753	0.429	6.439	0.481	1.119	0.121	0.481	1.890	-0.160
5.778	0.314	5.941	0.323	1.028	0.030	0.323	1.832	-0.219
				0.998	Y Average		2.050	ΔH@ Average

Note: The Calibration Factor Y, the ratio of the reading of the calibration meter to the dry gas meter, acceptance tolerance of individual values from the average is ±0.02

I certify that the above Dry Gas Meter was calibrated in accordance with USEPA Methods, CFR 40 Part 60, using the Precision Wet Test Meter # 11AE6, which in turn was calibrated using the American Bell Prohm # 3785 certificate # F107, which is traceable to the National Bureau of Standards (NIST)

Signature	<i>Joe Elliott</i>	Date	3 Sept 02
Quality Assurance Data Review	<i>[Signature]</i>	Date	3 Sept 02

**Ambient Air Services, Inc. - Method 5 Post Test Dry Gas Meter Calibration  
USING CALIBRATED CRITICAL ORIFICES  
3-POINT ENGLISH UNITS**

Meter Console Information	
Console Model Number	AASI
Console Serial Number	Box 10
Pre Test Y Value	0.989
DGM Serial Number	*****

Calibration Conditions			
Date	Time	1-Nov-02	13:12
Barometric Pressure		29.9	in Hg
Theoretical Critical Vacuum <sup>1</sup>		14.1	in Hg
Calibration Technician		JE	

Factors/Conversions		
Std Temp	72.8	°F
Std Press	29.92	in Hg
K <sub>1</sub>	17.647	(in Hg) <sup>2</sup>

<sup>1</sup>For valid test results, the Actual Vacuum should be 1 to 2 in. Hg greater than the Theoretical Critical Vacuum shown above.

<sup>2</sup>The Critical Orifice Coefficient, K<sub>1</sub>, must be entered in English units, (in<sup>3</sup>R<sup>1/2</sup>)/(in Hg<sup>1/2</sup>min).

Calibration Data										
Run Time	Metering Console					Critical Orifice				
Elapsed (H)	DGM Orifice (P <sub>m</sub> )	Volume Initial (V <sub>m</sub> )	Volume Final (V <sub>m</sub> )	Outlet Temp Initial (t <sub>m</sub> )	Outlet Temp Final (t <sub>m</sub> )	Serial Number	Coefficient (K <sub>1</sub> )	Amb Temp Initial (t <sub>amb</sub> )	Amb Temp Final (t <sub>amb</sub> )	Actual Vacuum
min	in H <sub>2</sub> O	cubic feet	cubic feet	°F	°F		see above <sup>2</sup>	°F	°F	in Hg
7.5	2.3	401.578	407.667	72	75	63	0.6213	71	72	21
62.9	2.3	407.667	459.392	75	76	63	0.6213	73	74	21
14.5	2.3	459.392	471.442	79	79	63	0.6213	74	75	21

Results								
Standardized Data				Dry Gas Meter				
Dry Gas Meter		Critical Orifice		Calibration Factor		Flowrate	ΔH @	
(Q <sub>DM</sub> )	(Q <sub>DM</sub> )	(V <sub>CR</sub> )	(Q <sub>CR</sub> )	Value (Y)	Variation (ΔY)	(Q <sub>DM</sub> )	0.75 SCFM (ΔH <sub>0</sub> )	Variation (ΔΔH <sub>0</sub> )
cubic feet	cfm	cubic feet	cfm			cfm	in H <sub>2</sub> O	
6.056	0.808	6.043	0.806	0.998	0.009	0.806	1.995	0.003
51.259	0.815	50.589	0.804	0.987	-0.002	0.804	1.995	0.003
11.861	0.818	11.651	0.804	0.982	-0.007	0.804	1.985	-0.006
				0.989	Y Average		1.992	ΔH <sub>0</sub> Average

Note: <sup>1</sup>The Calibration Factor Y, the ratio of the reading of the calibration meter to the dry gas meter, acceptable tolerance of individual values from the average is ±0.02.

I certify that the above Dry Gas Meter was calibrated in accordance with USEPA Methods, CFR 40 Part 60, using the Precision Wet Test Meter # 11AE6, which in turn was calibrated using the American Bell Prover # 3766, Certificate # F107, which is traceable to the National Bureau of Standards (N.I.S.T.)

Signature: <i>Joe Elliott</i>	Date: 11-01-02
Signature: <i>Donna Swartzell</i>	Date: 11-01-02

PITOT TUBE CALIBRATION MEASUREMENTS

DATE CALIBRATED 11/02/02 PITOT TUBE 6B

Pitot tube assembly level? Yes  No

Pitot tube openings damaged? Yes (explain below)  No

$\alpha_1 = \underline{10}^\circ (<10^\circ)$ ,  $\alpha_2 = \underline{0.5}^\circ (<10^\circ)$ ,  $\beta_1 = \underline{00}^\circ (<5^\circ)$ ,

$\beta_2 = \underline{00}^\circ (<5^\circ)$

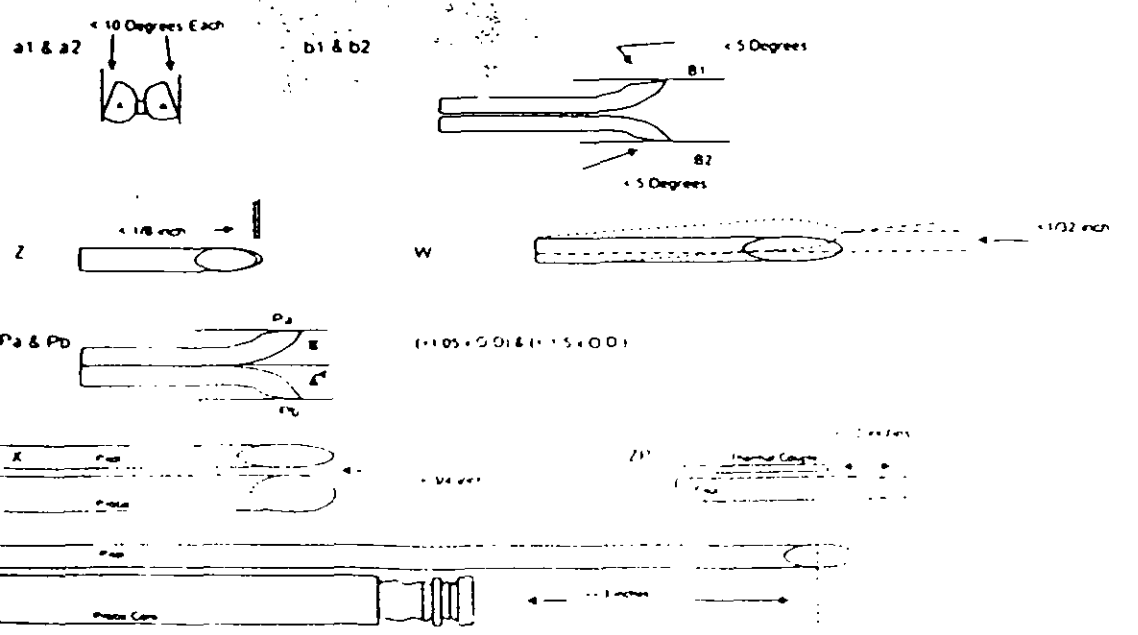
$\gamma = \underline{15}^\circ$ ,  $\theta = \underline{.5}^\circ$ ,  $A = \underline{1202}$  in. =  $(P_a + P_b)$

$z = A \sin \gamma = \underline{0031}$  in.;  $<0.32 / <1/8$  in.

$w = A \sin \theta = \underline{0010}$  in.;  $<0.08 / <1/32$  in.

$P_a = \underline{600}$  in.  $P_b = \underline{602}$  in.  $D_c = \underline{375}$

Calibration required? Yes  No



# THERMOCOUPLE CALIBRATION FORM

Calibration Date: 11/02/04 Time: 08:30  
 Ambient Temperature: 79 Source: CIP PLANT  
 Barometric Pressure: 30.05 Source: \_\_\_\_\_  
 Technician's Signature: [Signature]

Standard Thermometer Type: MERCURY IN GLASS  
 Manufacturer: PRINCO  
 Serial Number: 0932  
 Pyrometer Manufacturer: ATKINS Model: 3965  
 Serial Number: AAST #4 Meter Box: # 0

TEMPERATURE SOURCE (A)													
REFERENCE THERMOMETER	Actual Reading	<u>AMBIENT AIR</u>			<u>BOILING H<sub>2</sub>O</u>			<u>ICE BATH</u>					
	Corrected Temperature	<u>79°</u>			<u>212°</u>			<u>32°</u>					
CALIBRATED THERMOCOUPLE		Indicated Temp	Difference (B)	Percent Diff. (C)	Indicated Temp.	Difference	Percent Diff.	Indicated Temp.	Difference	Percent Diff.	Indicated Temp	Difference	Percent Diff.
Serial Number	Location												
<u>JB</u>	<u>Stack</u>	<u>79</u>	<u>0</u>		<u>212</u>	<u>0</u>		<u>32</u>	<u>0</u>				
<u>OX 10</u>	<u>Filter</u>	<u>78</u>	<u>-1</u>		<u>211</u>	<u>-1</u>		<u>32</u>	<u>0</u>				
<u>OX 4</u>	<u>Impinger</u>	<u>80</u>	<u>+1</u>		<u>212</u>	<u>0</u>		<u>31</u>	<u>-1</u>				
<u>OX 10</u>	<u>Meter In</u>	<u>79</u>	<u>0</u>		<u>212</u>	<u>0</u>		<u>32</u>	<u>0</u>				
<u>OX 10</u>	<u>Meter Out</u>	<u>79</u>	<u>0</u>		<u>213</u>	<u>+1</u>		<u>33</u>	<u>+1</u>				

Tolerance Tolerances: Stack = 1.5% of value, Filter Box = ±5.4°F, Impinger = ±2°F, Meter = ±5.4°F (40CFR Pt 60, App. A Method 5, and QA Handbook Section 3.4, Method 5, page 13, Rev 0)

Type of calibration system used: (B) Reference - Indicated = Difference

$$\left[ \frac{(\text{ref. temp. } ^\circ\text{F} - 460) - (\text{indicated temp. } ^\circ\text{F} - 460)}{(\text{reference temp. } ^\circ\text{F} - 460)} \right] \times 100$$

**APPENDIX – E**

**Sample Chain of Custody**

Technical Services, Inc.  
 2901 Danese St., Jacksonville, FL 32206  
 (904) 353-5761 / fax (904) 358-2908

02110001-1  
 thru  
 02110043

## CHAIN of CUSTODY RECORD

CLIENT NAME & ADDRESS (REPORT TO BE SENT TO) <i>Ambient Air Services, Inc.</i>				REMARKS  <i>Na2SO3 added in sampling @ TS</i>			
PROJ. NO.		PROJECT NAME/ ADDRESS:		BOTTLE MAKEUP			
		<i>GP/ProHca</i>		TOTAL NO of Containers <i>0.1 N NaOH</i> <i>1/2 N Poly</i> <i>AMBER GLASS</i> <i>1/2 N NaOH</i> <i>1/2 Gal Poly w/NaOH</i>			
		<i>Bleach Plant</i>					
SAMPLERS: (SIGNATURE)							
Sample Location ID	SAMPLE DATE	TIME	COMP	GRAB	PARAMETERS		
<i>Run 1 Imp Cch</i>	<i>10/31/02</i>				<i>Cl- / BASE</i>		
<i>2</i>	<i>↓</i>						
<i>3</i>	<i>↓</i>						
<i>Run 1 Imp Cch</i>	<i>10/29/02</i>						
<i>2</i>	<i>↓</i>						
<i>3</i>	<i>↓</i>						
<i>FIELD Blank</i>							
RELINQUISHED BY		DATE/TIME		RECEIVED BY			
RELINQUISHED BY		DATE/TIME		RECEIVED BY			
				<i>H. C. Brown 11/30/02</i>			
RELINQUISHED BY		DATE/TIME		RECEIVED BY			
<i>H. C. Brown</i>		<i>11/30/02</i>		<i>H. C. Brown 11/30/02</i>			
				RECEIVED FOR LABORATORY BY / DATE TIME			
				<i>Valerie P. Carter 11/30/02</i>			

Technical Services, Inc.  
 2901 Danese St., Jacksonville, FL 32206  
 (904) 353-5761 / fax (904) 358-2908

02110037 1

thru

02110043-1

### CHAIN of CUSTODY RECORD

CLIENT NAME & ADDRESS (REPORT TO BE SENT TO)				REMARKS			
Ambient Air Services, Inc.							
PROJ NO	PROJECT NAME/ ADDRESS			TOTAL NO of Containers	BOTTLE MAKEUP		
	GP/Polk Black Plant				0.1 N ALCOH 3/4 AL POLY 1 NUMBER GLASS 2/1 CLIN VIAL		
SAMPLERS (SIGNATURE)							
Sample Location ID	SAMPLE DATE	TIME	COMPGRADE	PARAMETERS			
Run 1 Imp Cts	10/31/02		1	CI - BASE			
2	↓		1	↓			
3	↓		1	↓			
Run 1 Imp Cts	10/29/02		1	↓			
2	↓		1	↓			
3	↓		1	↓			
FIELD BLANK				↓			
RELINQUISHED BY		DATE/TIME	RECEIVED BY	DATE/TIME			
P. S. S. Williams		10-30-02	D. W. S. Williams	10/30/02 09:00			
RELINQUISHED BY		DATE/TIME	RECEIVED BY	DATE/TIME			
D. W. S. Williams		11/01/02	H. S. Gray	11/01/02			
RELINQUISHED BY		DATE/TIME	RECEIVED BY	DATE/TIME			
H. S. Gray		11-1-02					
				RECEIVED FOR LABORATORY BY:	DATE/TIME		
				K. S. Williams	11/1/02 1615		

**APPENDIX - F**

**Calibration Gas Certificates**



# CERTIFICATE OF ANALYSIS / EPA PROTOCOL GAS

CUSTOMER **PRAXAIR SOUTHEAST** P.O NUMBER **333045 00**

## REFERENCE STANDARD

COMPONENT CARBON MONOXIDE 503 2PPM GMIS VS	NIST SRM NO. 1680B	CYLINDER NO. CLM-009396	CONCENTRATION 4.0 ± 0.05 PPM
---	-----------------------	----------------------------	---------------------------------

## ANALYZER READINGS

**R=REFERENCE STANDARD                      Z=ZERO GAS                      C=GAS CANDIDATE**

1. COMPONENT	CARBON MONOXIDE 503 2PPM GMIS	ANALYZER MAKE-MODEL/S/N	Siemens Ultramat SE S/N B8-900
ANALYTICAL PRINCIPLE	NON DISPERSIVE INFRARED	LAST CALIBRATION DATE	12 31 00
FIRST ANALYSIS DATE	12 07 00	SECOND ANALYSIS DATE	
Z	R 503	C 503	CONC 4.0
R 502	Z 0	C 502	CONC 3.0 ± 0.1
Z 0	C 502	R 503	CONC 3.0 ± 0.1
U/M ppm	MEAN TEST ASSAY	U/M ppm	MEAN TEST ASSAY

VALUES NOT VALID BELOW 100 PPM  
 UNCERTAINTY OF CARBON MONOXIDE ± 0.1 PPM

THIS CYLINDER NO. <b>0014901</b>	<b>CERTIFIED CONCENTRATION</b>
IT HAS BEEN CERTIFIED ACCORDING TO SECTION <b>1.1</b>	CARBON MONOXIDE <b>4.0 ± 0.05 PPM</b>
OF TRACEABILITY PROTOCOL NO. <b>EPA 821-F-97-001</b>	AIR <b>BALANCE</b>
PROCEDURE <b>01</b>	
CERTIFIED ACCURACY <b>± 0.1</b> & NIST TRACEABLE	
CYLINDER PRESSURE <b>1000 PSIG</b>	
CERTIFICATION DATE <b>12 07 00</b>	
EXPIRATION DATE <b>12 31 00</b> TERM <b>24 MONTHS</b>	

ANALYZED BY \_\_\_\_\_

CERTIFIED BY \_\_\_\_\_

DATE: 12/07/00

REV: 01/98/01

# CERTIFICATE OF ANALYSIS / EPA PROTOCOL GAS

CUSTOMER PRAXAIR SOUTHEAST

P.O NUMBER 333045-00

## REFERENCE STANDARD

COMPONENT	NIST SRM NO.	CYLINDER NO.	CONCENTRATION
CARBON MONOXIDE 503.2PPM GMIS VS	1680B	CLM 009396	450.4 PPM

## ANALYZER READINGS

R=REFERENCE STANDARD

Z=ZERO GAS

C=GAS CANDIDATE

I. COMPONENT	CARBON MONOXIDE 503.2PPM GMIS	ANALYZER MAKE-MODEL-S/N	Siemens Ultramat SE S/N 88-900
ANALYTICAL PRINCIPLE	NON-DISPERSIVE INFRARED	LAST CALIBRATION DATE	12/31/00
FIRST ANALYSIS DATE	12/27/00	SECOND ANALYSIS DATE	01/03/01
Z 0	R 503	C 595	CONC. 595.6
R 503	Z 0	C 595	CONC. 595.6
Z 0	C 595	R 503	CONC. 595.6
UM EST		MEAN TEST ASSAY	595.3

VALUES NOT VALID BELOW 150 PSIG  
 UNCERTAINTY OF CARBON MONOXIDE: ± 2PPM

THIS CYLINDER NO. SA12251	CERTIFIED CONCENTRATION
HAS BEEN CERTIFIED ACCORDING TO SECTION 2.2	CARBON MONOXIDE 503.2PPM
OF TRACEABILITY PROTOCOL NO EPA 800-P-07-001	
PROCEDURE	
CERTIFIED ACCURACY ± 1% NIST TRACEABLE	
CYLINDER PRESSURE 2000 PSIG	
CERTIFICATION DATE 01/03/01	
EXPIRATION DATE 01/03/02 TERM	

ANALYZED BY

CERTIFIED BY



# CERTIFICATE of ANALYSIS

Interference-Free Multi-Component EPA Protocol Gases

Cyl. Number: CC121974	Cyl. Pressure: 1667 psig	Document Number: 9032348	COMPONENT Name Carbon Monoxide	REQUESTED Concentration 1000 ppm	ASSAY Concentration 991 ±15 ppm
Assay Date: 07/23/01	Expiration Date: 07/22/04	Item Number:	Nitrogen	Balance	Balance
Customer: Technical Services	P.O. Number: 070601	Notes:			

\*Mixture is valid only to 150 psig

EPA Protocol Section No. 2.2

### REFERENCE STANDARD EMPLOYED FOR ANALYSIS

NOTE: Analytical uncertainty and NIST traceability are in compliance with EPA-600/R-97/123

Std Name	Std Conc	Units	Std Error	Comp	Balance	Cyl No	Exp Date	Sample	
GMIS91	GMIS91	1500.0	ppm	21.0	CO	N2	CC113811	06/22/03	N/A

Component 1: Carbon Monoxide Gas Analyzer Employed	Component 2: None Gas Analyzer Employed	Component 3: None Gas Analyzer Employed
Manufacturer: KVB/Analect	Manufacturer:	Manufacturer:
Model Number: EN3024	Model Number:	Model Number:
Serial Number: 3024	Serial Number:	Serial Number:
Analytical Principle: FTIR	Analytical Principle:	Analytical Principle:
MPC Calibrated: 07/05/01	MPC Calibrated:	MPC Calibrated:

07/16/01	Trial 1	Trial 2	Trial 3	Units	07/23/01	Trial 1	Trial 2	Trial 3	Units
Zero	-0.11	-0.33	-0.28		Zero	-0.02	0.05	0.16	
Reference 1	1614.16	1639.01	1648.95		Reference 1	1673.01	1678.36	1674.41	
Reference 2					Reference 2				
Calibrate	1061.20	1082.36	1088.32		Calibrate	1113.28	1105.85	1105.95	
Result	974.23	993.65	999.12	ppm	Result	996.79	990.14	990.23	ppm
Mean Result: 989.00				ppm	Mean Result: 992.39				ppm

Analyst *[Signature]*



# CERTIFICATE of ANALYSIS

Interference-Free Multi-Component EPA Protocol Gases

Cyl. Number: CC70989	Cyl. Pressure: 1667 psig	Document Number: 9032348	<b>COMPONENT</b> Name	<b>REQUESTED</b> Concentration	<b>ASSAY</b> Concentration
Assay Date: 07/23/01	Expiration Date: 07/22/04	Rem Number:	Carbon Monoxide	2000 ppm	1994 ±3% ppm
Customer: Technical Services	P.O. Number: 070601	Notes:	Nitrogen	Balance	Balance

EPAS Protocol Section No. 2.8  
 NOTE: Analytical uncertainty and NIST traceability are in compliance with EPA-600/R-97/123

REFERENCE STANDARD EMPLOYED FOR ANALYSIS									
Standard	Std. No.	Concn.	Units	Std. Error	Comp.	Balance	Cyl. No.	Exp. Date	Sample No.
GMS91	GMS91	1500.0	ppm	21.0	CO	N2	CC113811	06/22/03	N.A.

<b>Component 1:</b> Carbon Monoxide <i>Gas Analyzer Employed</i>	<b>Component 2:</b> None <i>Gas Analyzer Employed</i>	<b>Component 3:</b> None <i>Gas Analyzer Employed</i>
Manufacturer: KVB/Analect	Manufacturer:	Manufacturer:
Model Number: EN3024	Model Number:	Model Number:
Serial Number: 3024	Serial Number:	Serial Number:
Analytical Principle: FTIR	Analytical Principle:	Analytical Principle:
MPC Calibrated: 07/05/01	MPC Calibrated:	MPC Calibrated:

07/16/01				07/23/01			
Trial 1	Trial 2	Trial 3	Units	Trial 1	Trial 2	Trial 3	Units
Zero	-0.11	-0.33	-0.28	Reference 1	-0.02	0.05	0.16
Reference 1	1614.16	1639.01	1648.95	Reference 2	1673.01	1678.36	1674.41
Reference 2	2132.25	2176.69	2193.10	Candidate	2226.87	2236.96	2235.43
Result	1957.28	1998.07	2013.12	Result	1993.92	2002.95	2001.58
Mean Result: 1969.49 ppm				Mean Result: 1999.49 ppm			

Analyst

## Certificate of Analysis: E.P.A. Protocol Gas Mixture

Certification performed in accordance with "EPA Traceability Protocol (Sept. 1997)"  
 using assay procedures listed.

Cylinder No:	<u>SG9140092BAL</u>	Order No:	<u>008973-00</u>
Certification Date:	<u>09/9/2002</u>	Expiration Date:	<u>09/9/2005</u>
Cylinder Pressure:	<u>2000</u>	Part No:	<u>E02NI95E15A0077</u>

\*Do not use cylinder below 150 psig.

Component	Certified Concentration	Unit of Measure	Accuracy	Procedure	Analytical Principle
Carbon Dioxide	5.049	%	1%	G-1	NDIR
Nitrogen	Balance				

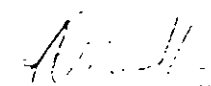
Nox  
 (Reference Value Only) ppm

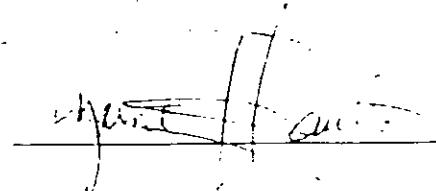
### Reference Standard Information

Type	Component	Concentration	Unit	Cylinder Number
Nlrm	Carbon Dioxide	4.204	%	SG9169571BAL

### Analytical Data

Component 1	<u>Carbon Dioxide</u>				
1st Analysis Date:	<u>09/9/2002</u>				
Zero	<u>0.000</u>	Cand	<u>5.046</u>	Ref	<u>4.202</u>
Zero	<u>0.000</u>	Cand	<u>5.045</u>	Ref	<u>4.200</u>
Zero	<u>0.000</u>	Cand	<u>5.046</u>	Ref	<u>4.201</u>
2nd Analysis Date:	_____				
Zero	_____	Cand	_____	Ref	_____
Zero	_____	Cand	_____	Ref	_____
Zero	_____	Cand	_____	Ref	_____

Analyzed by: 

Approved by: 

APPENDIX – G

Process Data

**PRODUCTION DATA FOR OCTOBER 29 AND 31, 2002 CO TESTING**

<b>DATE</b>	10/29/02		10/31/02		
<b>RUN</b>	1	2	1	2	3
<b>TIME</b>	1225-1324	1433-1532	1330-1429	1547-1646	1710-1809

Notes: ADTBPH is air-dried tons of bleached pulp per hour  
 Kappa is the pre-washer kappa  
 %ClO2 is the %ClO2 applied in that stage

Run	ADTBPH	%SW	Do Stage		%ClO2	Eop Stage		%SW	D1 Stage	
			%HW	Kappa		%HW	%ClO2		%HW	%ClO2
1 (29th)	49.8	100	0	22.0	2.0	100	0	100	0	0.5
2 (29th)	30.1	100	0	22.4	2.0	100	0	100	0	0.6
1 (31st)	50.0	100	0	22.8	2.2	100	0	100	0	0.7
2 (31st)	50.2	100	0	23.3	2.2	100	0	100	0	0.7
3 (31st)	50.1	100	0	23.3	2.2	100	0	100	0	0.7

**THE KAPPA AND %ClO2 APPLIED ARE CONFIDENTIAL BUSINESS INFORMATION.**

## PRODUCTION AND SCRUBBER DATA FOR OCTOBER 29 AND 31, 2002 CHLORINATED HAP (METHOD 26A) TESTS

DATE	10/29/02	10/31/02	
RUN	1      2      3	1      2      3	
TIME	1218-1323   1433-1538   1700-1802	1332-1443   1550-1656   1710-1816	

Notes: ADTBPH is air-dried tons of bleached pulp per hour  
 Kappa is the pre-washer kappa  
 %ClO<sub>2</sub> is the %ClO<sub>2</sub> applied in that stage

Run	ADTBPH	Do Stage				Eop Stage		D1 Stage		
		%SW	%HW	Kappa	%ClO <sub>2</sub>	%SW	%HW	%SW	%HW	%ClO <sub>2</sub>
1 (29th)	49.8	100.0	0.0	21.9	2.0	100.0	0.0	100.0	0.0	0.5
2 (29th)	30.1	100.0	0.0	22.4	2.0	100.0	0.0	100.0	0.0	0.7
3 (29th)	30.0	100.0	0.0	22.9	1.6	100.0	0.0	100.0	0.0	0.7
1 (31st)	49.8	100.0	0.0	21.9	2.2	100.0	0.0	100.0	0.0	0.5
2 (31st)	49.8	100.0	0.0	21.9	2.2	100.0	0.0	100.0	0.0	0.5
3 (31st)	49.8	100.0	0.0	21.9	2.2	100.0	0.0	100.0	0.0	0.5

**THE KAPPA AND %ClO<sub>2</sub> APPLIED ARE CONFIDENTIAL BUSINESS INFORMATION.**

Run	Flow, gpm	pH	Fan Load, %	Fan Amps	Fan Differential, in. H <sub>2</sub> O
1 (29th)	1262	9.2	84	15.0	20.8
2 (29th)	1207	8.9	84	15.1	20.8
3 (29th)	1153	9.0	85	15.2	21.1
1 (31st)	1252	9.3	85	15.4	21.3
2 (31st)	1258	9.3	85	15.4	21.3
3 (31st)	1263	9.2	86	15.4	21.4



### Cl2 Testing Raw Scrubber Data

Run 1      10/29/02      1218-1323

	Flow, gpm	pH	Fan Load, %	Fan Amps	Scrubber Differential, in H2O
1218-1233	1263	9.2	85	15.2	20.9
1233-1248	1263	9.1	84	15.1	20.9
1248-1303	1263	9.1	84	15.1	20.8
1303-1318	1262	9.0	83	15.0	20.8
Average	1262	9.1	84	15.1	20.9

**Cl2 Testing Raw Scrubber Data**

Run 2      10/29/02      1433-1538

	Flow, gpm	pH	Fan Load, %	Fan Amps	Scrubber Differential in H2O
1433-1448	1239	8.9	83	15.0	20.8
1448-1503	1228	8.9	83	15.0	20.8
1503-1518	1217	8.9	83	15.0	20.8
1518-1533	1207	8.9	84	15.1	20.9
Average	1223	8.9	84	15.0	20.8

### Cl2 Testing Raw Scrubber Data

Run 3      10/29/02      1700-1802

	Flow, gpm	pH	Fan Load, %	Fan Amps	Scrubber Differential, in H2O
1700-1715	1163	9.0	84	15.2	21.1
1715-1730	1159	9.0	84	15.2	21.1
1730-1745	1156	9.0	85	15.2	21.1
1745-1800	1153	9.0	85	15.2	21.1
Average	1158	9.0	84	15.2	21.1

### Cl2 Testing Raw Scrubber Data

Run 1      10/31/02      1332-1443

	Flow, gpm	pH	Fan Load, %	Fan Amps	Scrubber Differential, in H2O
1332-1347	1252	9.3	86	15.4	21.4
1347-1402	1252	9.3	85	15.4	21.3
1402-1417	1252	9.3	85	15.4	21.3
1417-1432	1254	9.3	86	15.4	21.3
1432-1447	1254	9.3	86	15.4	21.3
Average	1253	9.3	85	15.4	21.3

### Cl2 Testing Raw Scrubber Data

	Run 2	10/31/02	1550-1656			
	Flow, gpm	pH	Fan Load, %	Fan Amps	Scrubber Differential in H2O	
1550-1605	1258	9.3	85	15.4	21.3	
1605-1620	1258	9.3	85	15.4	21.4	
1620-1635	1259	9.3	85	15.4	21.4	
1635-1650	1259	9.3	86	15.4	21.4	
Average	1259	9.3	85	15.4	21.4	

### Cl2 Testing Raw Scrubber Data

Run 3      10/31/02      1710-1816

	Flow, gpm	pH	Fan Load, %	Fan Amps	Scrubber Differential in H2O
1710-1725	1261	9.3	86	15.5	21.4
1725-1740	1261	9.3	86	15.4	21.4
1740-1755	1262	9.3	86	15.5	21.5
1755-1810	1263	9.2	86	15.4	21.5
Average	1262	9.3	86	15.4	21.4

APPENDIX - H

Project Participants

Joe Cooksey of AASI	Report Review
Randy L Weston of AASI	Project Manager Report Preparation Field Testing
George Hawkins of AASI	Field Testing
Roger Dilinger of AASI	Field Testing
Joe Taylor of GP	Testing Support

**ATTACHMENT C**



**Subsection K. This section addresses the following emissions unit(s).**

E.U.

<u>ID No.</u>	<u>Brief Description</u>
036	Elemental Chlorine Free (ECF) No. 3 Bleach Plant

Emissions Unit 036 consists of an ECF bleach plant. This plant uses chlorine dioxide in the bleaching process. Emissions are controlled by a wet scrubber. This emissions unit is regulated under 40 CFR 63 Subpart S - National Emission Standards for Hazardous Air Pollutants for Pulp Mills, adopted and incorporated by reference in Rule 62-204.800, F.A.C.; Rule 212.400(5), F.A.C., Prevention of Significant Deterioration (PSD): Permit(s) No. PSD-FL-264; Rule 62-212.400(6), F.A.C., and Best Available Control Technology (BACT) Determination, dated June 30, 1999.

**The following specific conditions apply to the emissions unit(s) listed above:**

**Operational Parameters**

**K.0.** The Permittee shall meet the compliance milestones stated in Appendix CP-Compliance Plan.

**K.1. Permitted Capacity.** Until compliance is demonstrated with the air construction permit issued pursuant to the PSD review identified in the Compliance Schedule of the Compliance Plan, Appendix CP, Condition X.1, the maximum production rate of this emissions unit shall not exceed 840 tons per day of air-dried bleached pulp (ADBP) as a maximum monthly average. [Consent Order OGC File No. 02-1886]

**K.2. Hours of Operation.** The hours of operation are not restricted, i.e. 8,760 hours per year. [Rules 62-4.1610(2) and 62-210.200(PTE), F.A.C., Construction Permit No. 1070005-006-AC/PSD/FL-264]

**Operating Standards**

**K.3. Bleaching Stage Equipment.** The equipment at each bleaching stage, of the No. 3 Bleach Plant, where chlorinated compounds are introduced shall be enclosed and vented into a closed-vent system and routed to the wet scrubber stack for control. The enclosures and closed-vent system shall meet the requirements specified in Condition K.5. [63.445(b)]

**K.4. Chloroform air emissions.** To reduce chloroform air emissions to the atmosphere, the No. 3 Bleach Plant shall not use hypochlorite or chlorine for bleaching in the bleaching system or line. [63.445(d)(2), Construction Permit No. 1070005-006-AC/PSD-FL-264]

*Please reference the Permit No., Facility ID No., and appropriate Emissions Unit(s) ID No(s), on all correspondence, test report submittals, applications, etc.*

**K.5. Enclosures and Closed-Vent Systems.** The enclosure and closed-vent system specified in Condition K.3 for capturing and transporting vent streams that contain HAP shall meet the following requirements:

- (a) Each enclosure shall maintain negative pressure at each enclosure or hood opening as demonstrated by the procedures specified in Condition K.18. Each enclosure or hood opening closed during the initial performance test specified in 40 CFR 63.457(a) shall be maintained in the same closed and sealed position as during the performance test at all times except when necessary to use the opening for sampling, inspection, maintenance, or repairs.
- (b) Each component of the closed-vent system used to comply with Condition K.3. that is operated at positive pressure and located prior to a control device shall be designed for and operated with no detectable leaks as indicated by an instrument reading of less than 500 parts per million by volume above background, as measured by the procedures specified in Condition K.17..
- (c) Each bypass line in the closed-vent system that could divert vent streams containing HAP to the atmosphere without meeting the emission limitations in 40 CFR 63.445 shall comply with either of the following requirements:
  - (1) On each bypass line, the owner or operator shall install, calibrate, maintain, and operate according to manufacturer's specifications a flow indicator that provides a record of the presence of gas stream flow in the bypass line at least once every 15 minutes. The flow indicator shall be installed in the bypass line in such a way as to indicate flow in the bypass line; or
  - (2) For bypass line valves that are not computer controlled, the owner or operator shall maintain the bypass line valve in the closed position with a car seal or a seal placed on the valve or closure mechanism in such a way that valve or closure mechanism cannot be opened without breaking the seal.

[63.450]

### **Emission Limitations and Standards**

{Permitting note: Table 1-1, Summary of Air Pollutant Standards and Terms, summarizes information for convenience purposes only. This table does not supersede any of the terms or conditions of this permit.}

{Permitting Note: Unless otherwise specified, the averaging time for this condition is based on the specified averaging time of the applicable test method.}

**K.6. Carbon Monoxide.** Carbon monoxide emissions shall not exceed 46 lbs/hr and 201 tons per year<sup>1</sup>. Carbon monoxide emissions shall be minimized to the extent practicable by efficient bleaching operations.

<sup>1</sup> Compliance issues associated with CO emissions from this emissions unit are addressed within Consent Order OGC File No. 02-1886 until compliance is demonstrated with the air construction permit issued pursuant to the PSD review identified in the Compliance Schedule of the Compliance Plan. Appendix CP. Condition X.1.

[Rule 62-212.410, F.A.C., Construction Permit No. 1070005-006-AC/PSD-FL-264, Consent Order OGC File No. 02-1886]

*Please reference the Permit No., Facility ID No., and appropriate Emissions Unit(s) ID No(s). on all correspondence, test report submittals, applications, etc.*

**K.7. Total Chlorinated HAPs.** The total chlorinated HAP outlet concentration shall not exceed 10 parts per million by volume  
[63.445(c)(2); Construction Permit No. 1070005-006-AC/PSD-FL-264]

**K.8. Visible Emissions.** Visible Emissions from this emissions unit shall not exceed 20% opacity. The visible emissions limit shall only be effective if the visible emission measurement can be made without being substantially affected by plume mixing or moisture condensation.  
[Rule 62-296.320, F.A.C.; Rule 62-296.404(2)(b), F.A.C.; Construction Permit No. 1070005-006-AC/PSD-FL-264]

#### **Excess Emissions**

**K.9.** Excess emissions resulting from startup, shutdown or malfunction of any source shall be permitted providing (1) best operational practices to minimize emissions are adhered to and (2) the duration of excess emissions shall be minimized but in no case exceed two hours in any 24 hour period unless specifically authorized by the Department for longer duration.  
[62-201.700(1), F.A.C.]

**K.10.** Excess emissions which are caused entirely or in part by poor maintenance, poor operation, or any other equipment or process failure which may reasonably be prevented during startup, shutdown, or malfunction shall be prohibited.  
[Rule 62-210.700(4), F.A.C.]

**K.11.** Considering operational variations in types of industrial equipment operations affected by this rule, the Department may adjust maximum and minimum factors to provide reasonable and practical regulatory controls consistent with the public interest.  
[Rule 62-210.700(5), F.A.C.]

**K.12.** In case of excess emissions resulting from malfunctions, each source shall notify the Department or the appropriate Local program in accordance with Rule 62-4.130, F.A.C. A full written report on the malfunctions shall be submitted in a quarterly report, if requested by the Department.  
[Rule 62-210.700(6), F.A.C.]

#### **Test Methods and Procedures**

{Permitting note: Table 2-1, Summary of Compliance Requirements, summarizes information for convenience purposes only. This table does not supersede any of the terms or conditions of this permit.}

**K.13. Carbon Monoxide.** The test method for carbon monoxide emissions shall be EPA Method 10 as incorporated in 40 CFR 60, Appendix A. The compliance testing shall be conducted annually with a frequency base date of 05/25<sup>1</sup>.

<sup>1</sup> Compliance issues associated with CO emissions from this emissions unit are addressed within Consent Order OGC File No. 02-1886 until compliance is demonstrated with the air construction permit issued pursuant to the PSD review identified in the Compliance Schedule of the Compliance Plan. Appendix CP, Condition X.1.  
[Construction Permit No. 1070005-006-AC/PSD-FL-264, Rule 62-204.800, F.A.C., Consent Order OGC File No. 02-1886]

*Please reference the Permit No., Facility ID No., and appropriate Emissions Unit(s) ID No(s). on all correspondence, test report submittals, applications, etc.*

**K.14. Total Chlorinated HAPs.** The test method for total chlorinated HAPs shall be EPA Method 26A as incorporated in 40 CFR 60, Appendix A. The compliance testing shall be conducted annually with a frequency base date of 05/26.

[Construction Permit No. 1070005-006-AC/PSD-FL-264; Rule 62-297.310(7)(a)(4.c., F.A.C.)]

**K.15. Visible Emissions.** The test method for visible emissions shall be EPA Method 9 as incorporated in 40 CFR 60, Appendix A. The compliance testing shall be conducted annually with a frequency base date of 05/25.

[Construction Permit No. 1070005-006-AC/PSD-FL-264; Rule 62-204.800, F.A.C.]

**K.16. Vent sampling port locations and gas stream properties.** For purposes of selecting vent sampling port locations and determining vent gas stream properties, required in 40 CFR 63.445, the owner or operator shall comply with the following procedures:

(1) Method 1 or 1A of part 60, appendix A, as appropriate, shall be used for selection of the sampling site as follows:

(i) To sample for vent gas concentrations and volumetric flow rates, the sampling site shall be located prior to dilution of the vent gas stream and prior to release to the atmosphere:

(ii) For determining compliance with percent reduction requirements, sampling sites shall be located prior to the inlet of the control device and at the outlet of the control device; measurements shall be performed simultaneously at the two sampling sites; and

(iii) For determining compliance with concentration limits or mass emission rate limits, the sampling site shall be located at the outlet of the control device.

(2) No traverse site selection method is needed for vents smaller than 0.10 meter (4.0 inches) in diameter.

(3) The vent gas volumetric flow rate shall be determined using Method 2, 2A, 2C, or 2D of part 60, appendix A, as appropriate.

(4) The moisture content of the vent gas shall be measured using Method 4 of part 60, appendix A.

(5) To determine vent gas concentrations, the owner or operator shall collect a minimum of three test runs that are representative of normal conditions and average the resulting pollutant concentrations using the following procedures.

(i) Method 308 in Appendix A of this part shall be used to determine the methanol concentration.

(ii) Except for the modifications specified in paragraphs (b)(5)(ii)(A) through (b)(5)(ii)(K) of this section, Method 26A of part 60, appendix A shall be used to determine chlorine concentration in the vent stream.

(A) *Probe/Sampling Line.* A separate probe is not required. The sampling line shall be an appropriate length of 0.64 cm (0.25 in) OD Teflon® tubing. The sample inlet end of the sampling line shall be inserted into the stack in such a way as to not entrain liquid condensation from the vent gases. The other end shall be connected to the impingers. The length of the tubing may vary from one sampling site to another, but shall be as short as possible in each situation. If sampling is conducted in sunlight, opaque tubing shall be used. Alternatively, if transparent tubing is used, it shall be covered with opaque tape.

(B) *Impinger Train.* Three 30 milliliter (ml) capacity midget impingers shall be connected in series to the sampling line. The impingers shall have regular tapered stems.

*Please reference the Permit No., Facility ID No., and appropriate Emissions Unit(s) ID No(s), on all correspondence, test report submittals, applications, etc.*

Silica gel shall be placed in the third impinger as a desiccant. All impinger train connectors shall be glass and/or Teflon®.

(C) *Critical Orifice.* The critical orifice shall have a flow rate of 200 to 250 ml/min and shall be followed by a vacuum pump capable of providing a vacuum of 640 millimeters of mercury (mm Hg). A 45 millimeter diameter in-line Teflon® 0.8 micrometer filter shall follow the impingers to project the critical orifice and vacuum pump.

(D) The following are necessary for the analysis apparatus:

- (1) Wash bottle filled with deionized water;
- (2) 25 or 50 ml graduated burette and stand;
- (3) Magnetic stirring apparatus and stir bar;
- (4) Calibrated pH Meter;
- (5) 150-250 ml beaker or flask; and
- (6) A 5 ml pipette.

(E) The procedures listed in paragraphs (b)(5)(ii)(E)(1) through (b)(5)(ii)(E)(7) of this section shall be used to prepare the reagents.

- (1) To prepare the 1 molarity (M) potassium dihydrogen phosphate solution, dissolve 13.61 grams (g) of potassium dihydrogen phosphate in water and dilute to 100 ml.
- (2) To prepare the 1 M sodium hydroxide solution (NaOH), dissolve 4.0 g of sodium hydroxide in water and dilute to 100 ml.
- (3) To prepare the buffered 2 percent potassium iodide solution, dissolve 20 g of potassium iodide in 900 ml water. Add 50 ml of the 1 M potassium dihydrogen phosphate solution and 30 ml of the 1 M sodium hydroxide solution. While stirring solution, measure the pH of solution electrometrically and add the 1 M sodium hydroxide solution to bring pH to between 6.95 and 7.05.
- (4) To prepare the 0.1 normality (N) sodium thiosulfate solution, dissolve 25 g of sodium thiosulfate, pentahydrate, in 800 ml of freshly boiled and cooled distilled water in a 1-liter volumetric flask. Dilute to volume. To prepare the 0.01 N sodium thiosulfate solution, add 10.0 ml standardized 0.1 N sodium thiosulfate solution to a 100 ml volumetric flask, and dilute to volume with water.
- (5) To standardize the 0.1 N sodium thiosulfate solution, dissolve 3.249 g of anhydrous potassium bi-iodate, primary standard quality, or 3.567 g potassium iodate dried at 103 +/- 2 degrees Centigrade for 1 hour, in distilled water and dilute to 1000 ml to yield a 0.1000 N solution. Store in a glass-stoppered bottle. To 80 ml distilled water, add, with constant stirring, 1 ml concentrated sulfuric acid, 10.00 ml 0.1000 N anhydrous potassium bi-iodate, and 1 g potassium iodide. Titrate immediately with 0.1 N sodium thiosulfate titrant until the yellow color of the liberated iodine is almost discharged. Add 1 ml starch indicator solution and continue titrating until the blue color disappears. The normality of the sodium thiosulfate solution is inversely proportional to the ml of sodium thiosulfate solution consumed.

*Please reference the Permit No., Facility ID No., and appropriate Emissions Unit(s) ID No(s), on all correspondence, test report submittals, applications, etc.*

$$\text{Normality of Sodium Thiosulfate} = \frac{1}{\text{ml Sodium Thiosulfate Consumed}}$$

- (6) To prepare the starch indicator solution, add a small amount of cold water to 5 g starch and grind in a mortar to obtain a thin paste. Pour paste into 1 L of boiling distilled water, stir, and let settle overnight. Use clear supernate for starch indicator solution.
  - (7) To prepare the 10 percent sulfuric acid solution, add 10 ml of concentrated sulfuric acid to 80 ml water in an 100 ml volumetric flask. Dilute to volume.
- (F) The procedures specified in paragraphs (b)(5)(ii)(F)(1) through (b)(5)(ii)(F)(5) of this section shall be used to perform the sampling.
- (1) Preparation of Collection Train. Measure 20 ml buffered potassium iodide solution into each of the first two impingers and connect probe, impingers, filter, critical orifice, and pump. The sampling line and the impingers shall be shielded from sunlight.
  - (2) Leak and Flow Check Procedure. Plug sampling line inlet tip and turn on pump. If a flow of bubbles is visible in either of the liquid impingers, tighten fittings and adjust connections and impingers. A leakage rate not in excess of 2 percent of the sampling rate is acceptable. Carefully remove the plug from the end of the probe. Check the flow rate at the probe inlet with a bubble tube flow meter. The flow should be comparable or slightly less than the flow rate of the critical orifice with the impingers off-line. Record the flow and turn off the pump.
  - (3) Sample Collection. Insert the sampling line into the stack and secure it with the tip slightly lower than the port height. Start the pump, recording the time. End the sampling after 60 minutes, or after yellow color is observed in the second in-line impinger. Record time and remove the tubing from the vent. Recheck flow rate at sampling line inlet and turn off pump. If the flow rate has changed significantly, redo sampling with fresh capture solution. A slight variation (less than 5 percent) in flow may be averaged. With the inlet end of the line elevated above the impingers, add about 5 ml water into the inlet tip to rinse the line into the first impinger.
  - (4) Sample Analysis. Fill the burette with 0.01 N sodium thiosulfate solution to the zero mark. Combine the contents of the impingers in the beaker or flask. Stir the solution and titrate with thiosulfate until the solution is colorless. Record the volume of the first endpoint (TN, ml). Add 5 ml of the 10 percent sulfuric acid solution, and continue the titration until the contents of the flask are again colorless. Record the total volume of titrant required to go through the first and to the second endpoint (TA, ml). If the volume of neutral titer is less than 0.5 ml, repeat the testing for a longer period of time. It is important that sufficient lighting be present to clearly see the endpoints, which are

*Please reference the Permit No., Facility ID No., and appropriate Emissions Unit(s) ID No(s), on all correspondence, test report submittals, applications, etc.*

determined when the solution turns from pale yellow to colorless. A lighted stirring plate and a white background are useful for this purpose.

- (5) Interferences. Known interfering agents of this method are sulfur dioxide and hydrogen peroxide. Sulfur dioxide, which is used to reduce oxidant residuals in some bleaching systems, reduces formed iodine to iodide in the capture solution. It is therefore a negative interference for chlorine, and in some cases could result in erroneous negative chlorine concentrations. Any agent capable of reducing iodine to iodide could interfere in this manner. A chromium trioxide impregnated filter will capture sulfur dioxide and pass chlorine and chlorine dioxide. Hydrogen peroxide, which is commonly used as a bleaching agent in modern bleaching systems, reacts with iodide to form iodine and thus can cause a positive interference in the chlorine measurement. Due to the chemistry involved, the precision of the chlorine analysis will decrease as the ratio of chlorine dioxide to chlorine increases. Slightly negative calculated concentrations of chlorine may occur when sampling a vent gas with high concentrations of chlorine dioxide and very low concentrations of chlorine.
- (6) The minimum sampling time for each of the three test runs shall be 1 hour in which either an integrated sample or four grab samples shall be taken. If grab sampling is used, then the samples shall be taken at approximately equal intervals in time, such as 15 minute intervals during the test run.
- (G) The following calculation shall be performed to determine the

corrected sampling flow rate:

$$S_c = \frac{S_u(BP - PW)(293)}{(760)(273 + t)}$$

where:

$S_c$  = Corrected (dry standard) sampling flow rate, liters per minute;  
 $S_u$  = Uncorrected sampling flow rate, L/min;  
BP = Barometric pressure at time of sampling;  
PW = Saturated partial pressure of water vapor, mm Hg at temperature;  
and  
t = Ambient temperature, °C.

(H) The following calculation shall be performed to determine the moles of chlorine in the sample:

$$\text{Cl}_2 \text{ Moles} = 1/8000 (5 T_N - T_A) \times N_{\text{Thio}}$$

where:

$T_N$  = Volume neutral titer, ml;  
 $T_A$  = Volume acid titer (total), ml; and  
 $N_{\text{Thio}}$  = Normality of sodium thiosulfate titrant.

(I) The following calculation shall be performed to determine the concentration of chlorine in the sample:

*Please reference the Permit No., Facility ID No., and appropriate Emissions Unit(s) ID No(s), on all correspondence, test report submittals, applications, etc.*

$$\text{ClO}_2 \text{ Moles} = 1 / 4000 (T_A - T_N) \times N_{\text{Thio}}$$

where:

$T_A$  = Volume acid titer (total), ml;

$T_N$  = Volume neutral titer, ml; and

$N_{\text{Thio}}$  = Normality of sodium thiosulfate titrant.

(K) The following calculation shall be performed to determine the concentration of chlorine dioxide in the sample:

$$\text{ClO}_2 \text{ ppmv} = \frac{6010(T_A - T_N) \times N_{\text{Thio}}}{S_c \times t_s}$$

where:

$S_c$  = Corrected (dry standard) sampling flow rate, liters per minute;

$t_s$  = Time sampled, minutes;

$T_A$  = Volume acid titer (total), ml;

$T_N$  = Volume neutral titer, ml; and

$N_{\text{Thio}}$  = Normality of sodium thiosulfate titrant.

(iii) Any other method that measures the total HAP or methanol concentration that has been demonstrated to the Administrator's satisfaction.

(6) The minimum sampling time for each of the three runs per method shall be 1 hour in which either an integrated sample or four grab samples shall be taken. If grab sampling is used, then the samples shall be taken at approximately equal intervals in time, such as 15 minute intervals during the run.

[63.457(b)]

**K.17. Detectable leak procedures.** To measure detectable leaks for closed-vent systems as specified in Condition K.5., the owner or operator shall comply with the following:

(1) Method 21, of Part 60, Appendix A; and

(2) The instrument specified in Method 21 shall be calibrated before use according to the procedures specified in Method 21 on each day that leak checks are performed. The following calibration gases shall be used:

(i) Zero air (less than 10 parts per million by volume of hydrocarbon in air); and

(ii) A mixture of methane or n-hexane and air at a concentration of approximately, but less than, 10,000 parts per million by volume methane or n-hexane.

[63.457(d)]

**K.18. Negative pressure procedures.** To demonstrate negative pressure at process equipment enclosure openings as specified in Condition K.5., the owner or operator shall use one of the following procedures:

(1) An anemometer to demonstrate flow into the enclosure opening;

(2) Measure the static pressure across the opening;

(3) Smoke tubes to demonstrate flow into the enclosure opening; or

(4) Any other industrial ventilation test method demonstrated to the Administrator's satisfaction.

[63.457(e)]

Please reference the Permit No., Facility ID No., and appropriate Emissions Unit(s) ID No(s) on all correspondence, test report submittals, applications, etc.



**K.19. Bleaching HAP concentration measurement.** For purposes of complying with the bleaching system requirements in § 63.445, the owner or operator shall measure the total HAP concentration as the sum of all individual chlorinated HAPs or as chlorine.  
[63.457(h)]

**Continuous Monitoring Requirements**

**K.20.** The permittee shall install, calibrate, certify, operate, and maintain according to the manufacturer's specifications, a continuous monitoring system (CMS, as defined in §63.2) as specified in Condition K.21. The CMS shall include a continuous recorder.  
[63.453(a), Construction Permit No. 1070005-006-AC/PSD-FL-264]

**K.21.** A CMS shall be operated to measure the following parameters:

- (1) The pH or the oxidation/reduction potential of the gas scrubber effluent;
- (2) Fan amperage of the bleaching system vent gas fan; and
- (3) The gas scrubber liquid influent flow rate.

EPA Approved Alternative Monitoring Parameter dated December 22, 2000.  
[63.453(c), Construction Permit No. 1070005-006-AC/PSD-FL-264]

**K.22. Enclosure and Closed-Vent System.** The enclosure and closed-vent system shall comply with the following requirements:

- (1) For each enclosure opening, a visual inspection of the closure mechanism specified in K.5.(a) shall be performed at least once every 30 days to ensure the opening is maintained in the closed position and sealed.
- (2) The closed-vent system shall be visually inspected every 30 days and at other times as requested by the Administrator. The visual inspection shall include inspection of ductwork, piping, enclosures, and connections to covers for visible evidence of defects.
- (3) For positive pressure closed-vent systems or portions of closed-vent systems, demonstrate no detectable leaks as specified in Condition K.5.(b) measured initially and annually by the procedures in Condition K.17..
- (4) Demonstrate initially and annually that each enclosure opening is maintained at negative pressure as specified in Condition K.18..
- (5) The valve or closure mechanism specified in Condition K.5.(c)(2) shall be inspected at least once every 30 days to ensure that the valve is maintained in the closed position and the emission point gas stream is not diverted through the bypass line.
- (6) If an inspection required by paragraphs (1) through (5) of this Condition identifies visible defects in ductwork, piping, enclosures or connections to covers required by Condition K.5., or if an instrument reading of 500 parts per million by volume or greater above background is measured, or if enclosure openings are not maintained at negative pressure, then the following corrective actions shall be taken as soon as practicable.
  - (i) A first effort to repair or correct the closed-vent system shall be made as soon as practicable but no later than 5 calendar days after the problem is identified.
  - (ii) The repair or corrective action shall be completed no later than 15 calendar days after the problem is identified. Delay of repair or corrective action is allowed if the repair or corrective action is technically infeasible without a process unit shutdown or if the owner or

*Please reference the Permit No., Facility ID No., and appropriate Emissions Unit(s) ID No(s) on all correspondence, test report submittals, applications, etc.*

operator determines that the emissions resulting from immediate repair would be greater than the emissions likely to result from delay of repair. Repair of such equipment shall be completed by the end of the next process unit shutdown.

[63.453(k)]

**K.23. Wet Scrubber Operating Parameters.** The wet scrubber shall be operated in a manner consistent with the minimum pH of the scrubbing medium effluent at 9.1 s.u., the minimum fan motor loading of 85% (15.3 amps), and the minimum scrubber recirculation flow rate of 1,229 gpm. Operation of the wet scrubber below these minimum operating parameter values or failure to perform procedures required by 40 CFR 63 Subpart S shall constitute a violation of Condition K.7. and be reported as a period of excess emissions.

{Permitting Note: Unless otherwise specified, the averaging time for this condition is based on the specified averaging time of the applicable test method.}

[63.453(o), Applicant Request dated 12/20/02]

### **Recordkeeping Requirements**

**K.24.** The permittee shall maintain daily records of the following information in order to document continuous compliance with Condition Nos. K.1., K.6., K.7., and K.21.:

- Quantity of pulp processed through the No. 3 Bleach Plant in air-dried bleach tons.
- Scrubber parameters monitored per Condition K.21.

**K.25.** The permittee shall comply with the recordkeeping requirements of 40 CFR 63.10, as shown in Table 1 of 40 CFR Part 63 Subpart S.

[63.454(a)]

**K.26. Enclosure Opening, Closed-Vent System and Closed Collection System.** For each applicable enclosure opening, closed-vent system, and closed collection system, the owner or operator shall prepare and maintain a site-specific inspection plan including a drawing or schematic of the components of applicable affected equipment and shall record the following information for each inspection:

- (1) Date of inspection;
- (2) The equipment type and identification;
- (3) Results of negative pressure tests for enclosures;
- (4) Results of leak detection tests;
- (5) The nature of the defect or leak and the method of detection (i.e., visual inspection or instrument detection);
- (6) The date the defect or leak was detected and the date of each attempt to repair the defect or leak;
- (7) Repair methods applied in each attempt to repair the defect or leak;
- (8) The reason for the delay if the defect or leak is not repaired within 15 days after discovery;
- (9) The expected date of successful repair of the defect or leak if the repair is not completed within 15 days;
- (10) The date of successful repair of the defect or leak;

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- (11) The position and duration of opening of bypass line valves and the condition of any valve seals; and
  - (12) The duration of the use of bypass valves on computer controlled valves.
- [63.454(b)]

**K.27. New affected Process Equipment.** The permittee shall record the CMS parameters specified in §63.453 and meet the requirements specified in Condition K.25. for any new affected process equipment that becomes subject to the standards of 40 CFR Part 63 Subpart S due to a process change or modification.

[63.454(d)]

### **Reporting Requirements**

**K.28.** The permittee shall comply with the reporting requirements of 40 CFR Part 63, Subpart A as specified in Table 1 of Subpart S.

[63.455(a)]

### **Common Conditions - F.A.C. Test Requirements**

**K.29.** This emissions unit is also subject to applicable F.A.C. Test Requirements in Subsection N.

### **Common Conditions - Periodic Monitoring**

**K.30.** This emissions unit is also subject to applicable Periodic Monitoring Requirements in Subsection P.

*Please reference the Permit No., Facility ID No., and appropriate Emissions Unit(s) ID No(s). on all correspondence, test report submittals, applications, etc.*

### Appendix CP- Compliance Plan

X.1. Compliance Schedule. The following dates shall be met to satisfy measurable progress milestones for the facility to come into compliance with Conditions A.10., K.6., and K.7.

E.U. ID. No.	Milestone	Milestone Date
036 014	Responsible Official to enter into a consent order agreement with Department concerning the No. 3 ECF Bleach Plant, and initiate agreements concerning any other non-compliant conditions.	November 12, 2002
036	Facility to submit a complete application, including completed responses to Department requests for additional information, for an air construction permit/PSD Determination.	February 1, 2003
Facility	Responsible Official to submit "Certification of Compliance", addressing the entire facility, indicating what is not in compliance, when non-compliance started, the degree or amount of non-compliance, the duration of non-compliant operations, steps taken to identify and correct non-compliant conditions, and actions (with time table), to correct any current non-compliant conditions and achieve compliance.	March 1, 2003
036	Initiation of on-site construction and/or installation of emission control equipment or process change authorized by air construction permit	No later than 3 months from the date of issuance of the resulting air construction permit/PSD Determination
036	Completion of on-site construction or installation of emission control equipment or process change authorized by air construction permit	No later than 9 months from the date of issuance of the resulting air construction permit/PSD Determination
036	Compliance Testing conducted and test reports submitted pursuant to requirements of air construction permit	Pursuant to the timeframes established in the air construction permit/PSD Determination
014	Compliance Testing conducted and test reports submitted for the No. 4 Power Boiler	April 1, 2003
036	Submittal of Title V Operation Permit Revision for the incorporation of the air construction permit/PSD Determination for the No. 3 ECF Bleach Plant	At least 90 days prior to expiration of air construction permit, but no later than 180 days after commencement of operation

036	Final Compliance	No later than 11 months from the date of issuance of the resulting air construction permit/PSD Determination
Facility	Responsible Official to submit "Certification of Compliance", addressing the entire facility, indicating what is not in compliance, when non-compliance started, the degree or amount of non-compliance, the duration of non-compliant operations, steps taken to identify and correct non-compliant conditions, and actions (with time table), to correct any current non-compliant conditions and achieve compliance.	No later than 12 months from the date of issuance of the resulting air construction permit/PSD Determination

**X.2. Permitted Capacity.** Until compliance is demonstrated with the air construction permit issued pursuant to the PSD review identified in the Compliance Schedule of Condition X.1, above, the maximum throughput rate of this emissions unit shall not exceed 840 tons per day of air-dried bleached pulp (ADBP) as a maximum monthly average.  
[Consent Order OGC File No. 02-1886]

**X.3. Recordkeeping.** The Permittee shall maintain material throughput logs that indicate the type and amount of material used daily.  
[Consent Order OGC File No. 02-1886]