

## UNITED STATES ENVIRONMENTAL PROTECTION AGENCY

#### REGION IV

345 COURTLAND STREET, N.E. ATLANTA, GEORGIA 30365

**4APT-AEB** 

JUN 18 1993

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JUN. 23 1993

Division of Air Resources Management

Mr. Clair H. Fancy, P.E., Chief Bureau of Air Regulation Florida Department of Environmental Regulation

Twin Towers Office Building 2600 Blair Stone Road Tallahassee, Florida 32399-2400

RE: Central Florida Power Limited Partnership, Tiger Bay Cogeneration Plant (PSD-FL-190)

Dear Mr. Fancy:

This is to acknowledge receipt of the final determination and Prevention of Significant Deterioration (PSD) permit for the above referenced facility, by your correspondence dated May 19, 1993. The proposed facility will be a 258 megawatt combined cycle cogeneration power plant. The proposed project consists of one advanced technology heavy-duty industrial gas turbine electric generating unit, with a duct burner-fired heat recovery steam generator, and a steam turbine generator.

Your determination proposes to limit NO<sub>x</sub> emissions from the combustion turbine through advanced dry low-NO<sub>x</sub> combustors and water injection, to limit NO<sub>x</sub> emissions from the duct burner through combustion design, to limit CO and VOC emissions from the combustion turbine and duct burner through combustion control, and to limit PM/PM<sub>10</sub>, Be, and As emissions from the combustion turbine through combustion control and the use of clean fuels. In addition, this facility will meet revised, lower NO<sub>x</sub> limits no later than December 31, 1997, through advanced combustor technology or the use of selective catalytic reduction.

We have reviewed the package as submitted and have no adverse comments. Thank you for the opportunity to review and comment on the package. If you have any questions or comments, please contact Mr. Scott Davis of my staff at (404) 347-5014.

Sincerely yours.

Brian L. Beals, Chief Source Evaluation Unit

Air Enforcement Branch Air, Pesticides, and Toxics

Management Division

cc: D. Heron

C. Helonday B. Ikomaci Gudint Q. Bunyak, NPS X. Horak, P.E., KBN X. novak, Palk Co

40TPA530223 Oentul Florida



March 11, 1993

Mr. Clair H. Fancy, P.E. Chief, Bureau of Air Regulation Florida Department of Environmental Regulation Twin Towers Office Building 2600 Blair Stone Road Tallahassee, Florida 3299-2400 R T E I V E D

Resources menedanismi

RE: Centr

Central Florida Power Limited Partnership (CFPLP)

Tiger Bay Cogeneration Plant AC 53-214903; PSD-FL-190

### Dear Clair:

This correspondence provides technical information for the Department's consideration concerning the comments received from the U.S. Fish and Wildlife Service (USFWS) dated February 5, 1993 on the above referenced project. Specifically, the USFWS suggested the final permit for the project include a statement that selective catalytic reduction (SCR) be installed if the 15 ppmvd (corrected to 15 percent oxygen) emission limit is not met and that the Department re-establish an allowable emissions limit as best available control technology (BACT) if actual emissions are tested less than 15 ppmvd. The information contained herein and in the permit record clearly suggest that the final permit should not contain the suggestions made by the USFWS. The rationale is presented below.

## **Mandating SCR**

12018A1/15

Modifying the proposed language of the permit to include a provision mandating SCR is unwarranted. The condition as proposed by the Department clearly recognizes that it will be at the determination of the Department whether SCR will be installed. This allows flexibility to incorporate other design features to meet the 15 ppmvd NOx emission limit if desired by the Department. As "pollution prevention" technology progresses over the next several years there may be other options of lowering NOx to meet emission limits. For example, the combined use of dry-low NOx combustion and wet injection may prove to be a viable technique. Research is also being performed in the area of fuel additives. Mandating the installation of SCR, if a permit limit is not met, does not recognize the development of future technologies and does not provide the Department or CFPLP the inherent flexibility to make an appropriate decision.

## Lowering the Permit/BACT Limit

Incorporating a provision in the permit that will require the lowering the BACT limit is not appropriate for several reasons. First, there have been no criteria proposed for establishing such a lower limit. While the initial performance tests may find a NOx emission rate lower than 15 ppmvd corrected, this tested rate will only be an accurate representation of NOx emissions that occurred during the specific conditions observed during the tests. Combustion turbines are sensitive to ambient meteorological

KBN ENGINEERING AND APPLIED SCIENCES, INC.



conditions such as temperature and relative humidity. Changes in meteorological conditions, for which CFPLP will have no control, may cause changes in NOx emissions. Such conditions are recognized in the margins incorporated into the design features of the control equipment. An example of how operational conditions can affect NOx emissions was previously supplied to the Department for the Orlando CoGen Limited, L.P. Project. Information was supplied to the Department that indicated that actual NOx tested as low as 9 to 13 ppmvd for the combustion turbine proposed for the project. However, the vendor would only guarantee 15 ppmvd since margins are required to assure compliance with the permit limits under all operating scenarios. The Department accepted this rationale in this permit decision.

Second, the proposed project is being designed for operation in late 1994 to early 1995. While it is recognized that combustion turbine units proposed for operation in the future (> 1997) have proposed lower limits, equipment proposed for these projects may not be applicable to the proposed project. The earlier commercial operation date for the CFPLP facility suggests that differences in equipment may result.

Third, all equipment degrades whether it be dry low-NOx combustors, SCR or a fabric filter. The emission margins built into all control equipment recognizes this fact and an appropriate emission limit must be established to account for emission changes as a result of equipment degradation.

## Apparent Preference for Technology Comments by USFWS

The State of Florida has full authority for implementing the federally mandated Prevention of Significant Deterioration program through approval of its regulations and State Implementation Plan (SIP). The federal agencies comment on the PSD applications and have differing authority. The USFWS which is the designated Federal Land Manager for National Wilderness Areas Class I areas has review authority of air quality related values in such areas. The Environmental Protection Agency has authority in establishing the implementing regulations for PSD review and approval, and establishing guidelines for modeling and control technology review. For the CFPLP project, the EPA comments (see letter dated February 16, 1993), suggest that the Department's permitting decision was appropriate. The EPA is clearly the appropriate agency regarding control technology issues. In contrast, the USFWS which is the appropriate agency for air quality related values, had no adverse comments regarding the NOx impacts in the Class I area. Indeed, the USFWS indicated that the NOx impacts at the emission limits proposed by the Department were not significant. The USFWS comments should be viewed in this context; i.e., lowering the NOx emission limit will not change the conclusion reached regarding impacts (i.e., impacts will still not be significant). Moreover, the EPA comments concerning control technology (as well as emission limits) should take preference over USFWS comments.

## Conclusion

The technical information presented herein and the permit record clearly indicate that the emission limits proposed by the Department in the draft permit are appropriate. Taken together with the commercial concerns expressed by CFPLP (see letter of March 10, 1993, from Destec Energy the controlling partner), we respectively request the Department not incorporate the comments made by the USFWS into the final permit.



As always, the assistance of you and your staff are greatly appreciated. Please call if you have any questions.

Sincerely,

Thurmand 7. 14 why Kennard F. Kosky, P.E.

President and Principal Engineer Florida Registration No. 14996

cc:

Terrsa Heron

Preston Lewis

R. Chatham

attachment Narper, EPA
KFK/mlb J. Dunyak, WPS
B. Shomas, 5000



March 10, 1993

DESTEC ENERGY, INC. 2500 CITYWEST BLVD., SUITE 150 P.O. BOX 4411 HOUSTON, TEXAS 77210-4411 (713) 735-4000

Mr. C. H. Fancy Chief, Bureau of Air Regulation Florida Department of Environmental Regulation Twin Towers Office Building 2600 Blair Stone Road Tallahassee, Florida 32399-2400

VIA FEDERAL EXPRESS

Re: Central Florida Power, L.P. - DER No. AC53-214903 & PSD-FL-190

Dear Mr. Fancy:

On behalf of Central Florida Power, L.P. (CFPLP), I respectfully request the following comments be entered into the Department's record:

We have given serious consideration to the issue of revising emission limits after performance testing and emission data if such a lower rate is achievable. Our experience with lenders indicates that they would be unlikely to commit funds to a project with such a permit condition. We, as well as the financial community, are well aware that the regulatory agencies have the authority to impose new requirements on existing facilities. This "regulatory risk" is taken into account during the development of the project financing. A specific condition in the permit stating the Department's authority to revise the allowable emission limit would bring the "reliance on" the permit into question. Therefore, we request that no such condition be in the final permit for a change in the emission limits based on actual emission rates and that the Department rely on the regulation to provide for revision to the allowable limits.

We respectfully request that you consider our comment and would be pleased to address any other questions or concerns you might have. We appreciate the efforts on the part of the Department in reviewing our permit application and we look forward to receiving our permit.

Sincerely.

Frost W. Cochran

Project Finance Manager

FWC/nl

cc:

**Bob Taylor** 

Ken Kosky

I. Alyon FWC/nlC. Holloday RECEIVED

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Division of Air Resources Management







# UNITED STATES ENVIRONMENTAL PROTECTION AGENCY REGION IV - ATLANTA, GEORGIA

AIR, PESTICIDES & TOXICS MANAGEMENT DIVISION

## AIR ENFORCEMENT BRANCH FACSIMILE TRANSMISSION SHEET

DATE: 2/15/93	# OF PAGES:
TO: Clare H. Fancy	PHONE #:
ADDRESS: FO€R	
FROM: Scott DAVIS	
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SPECIAL INSTRUC	TIONS FOR RECEIVER:
	AND STREET, N.E. EORGIA 30365

FAX (404) 347-3059



#### UNITED STATES ENVIRONMENTAL PROTECTION AGENCY

#### REGION IV

345 COURTLAND STREET, N.E. ATLANTA, GEORGIA 30365

4APT-AEB

FEB 16 1993

Mr. Clair H. Fancy, P.E., Chief **Bureau of Air Regulation** Florida Department of Environmental Regulation Twin Towers Office Building 2600 Blair Stone Road Tallahassee, Florida 32399-2400

RE: Central Florida Power Limited Partnership, Tiger Bay Cogeneration Plant (PSD-FL-190)

Dear Mr. Fancy:

This is to acknowledge receipt of the preliminary determination and draft Prevention of Significant Deterioration (PSD) permit for the above referenced facility, by your letter dated January 15, 1993. The proposed facility will be a 258 megawatt combined cycle cogeneration power plant. The proposed project consists of one advanced technology heavy-duty industrial gas turbine electric generating unit, with a duct burner-fired heat recovery steam generator, and a steam turbine generator.

Your determination proposes to limit NO, emissions from the combustion turbine through advanced dry low-NO<sub>x</sub> combustors and water injection, to limit NO<sub>x</sub> emissions from the duct burner through combustion design, to limit CO and VOC emissions from the combustion turbine and duct burner through combustion control, and to limit PM/PM<sub>10</sub>, Be, and As emissions from the combustion turbine through combustion control and the use of clean fuels. In addition, this facility will meet revised, lower NO<sub>x</sub> limits no later than December 31, 1997, through advanced combustor technology or the use of selective catalytic reduction.

We have reviewed the package as submitted and have no adverse comments. Thank you for the opportunity to review and comment on the package. If you have any questions or comments, please contact Mr. Scott Davis of my staff at (404) 347-5014.

Sincerely yours

Brian L. Beals, Chief

Source Evaluation Unit Air Enforcement Branch

Air, Pesticides, and Toxics

Management Division

Cl: J. Meron

C. Holladay

B. Shomas, Sw Dist

Q. Bunnak, NPS

X. Kosky, KBN

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Division of Air Resources Management



February 8, 1993

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Division of Air Resources Management

Mr. Clair H. Fancy
Bureau of Air Regulation
Florida Department of Environmental Regulation
Twin Towers Office Building
2600 Blair Stone Road
Tallahassee, FL 32399-2400

Re: Central Florida Power Limited Partnership Tiger Bay Cogeneration Plant PSD-FL-190 AC 53-214903

Dear Mr. Fancy:

Enclosed please find the Affidavit of Publication for advertisement of the Notice of Intent to Issue Permit for this project. As shown, the advertisement was published in The Polk County Democrat on February 4, 1993 and satisfies the publication requirements of the Intent to Issue.

If you have any questions concerning this material, please call me at your earliest convenience.

Sincerely,

Kennard F. Kosky, P.E.

President

Enclosure

12018A1/Ĭ4

cc:

Robert I. Taylor, Central Florida Power, L.P.

Robert Chatham, Destec Energy, Inc.

B. dignias Sw Dist

Teresa Heron, FDER

Project File

Rowalk BN ENGINEERING AND APPLIED SCIENCES. INC.

1034 Northwest 57th Street Gainesville, Florida 32605 904/331-9000 FAX: 904/332-4189

## AFFIDAVIT OF PUBLICATION

## The Polk County Democra Coconut Palm Drive, Tampe,

Published Semi-Weekly Bartow, Polk County, Florida

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STATE OF FLORIDA		determination.  Further, a public he
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matter of Central Florid		iii tile
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Affiant further says that The Bartow, in said Polk County, Florida ously published in said Polk County entered as second class matter at the period of one year next preceding ment; and affiant further says that he corporation any discount, rebate, considerable advertisement for publication in second Signary The foregoing instrument was acknown.	a, and that said newspaper has y, Florida, each Monday and post office in Bartow, in said I the first publication of the at the has neither paid nor promommission, or refund for the aid newspaper.	s heretofore been continu- l Thursday, and has been Polk County, Florida, for a tached copy of advertise- ised any person, firm, or purpose of securing this
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-	Teresa M. Pacetti	
(	Printed or typed name of	Notary Public) Notary Public
My Commission Expires:	Notar Polar	y Public, State of Ejorida

quent intervention will only be at the approval of the presiding officer upon motion filed pursuant to Rule 28-5.207, F.A.C.

The application is available for ablic inspection during normal business hours, 8:00 a. m. to 5:00 p. m., Monday through Friday, except legal holidays, at Depart-ment of Environmental Regulation, Bureau of Air Regulation, 2600 Blair Stone Road, Tallahassee, Florida 32399-2400, Department of Environmental Regula-Florida '33619-8218

Any person may send written comments on the proposed action to Mr. Preston Lewis at the Department's Tellehauses \* received ublication sidered in s 'final

ering can person(s), submitted notice.

TERESA M. PACETTI

My Comm, Exp. Dec. 19, 1995 Comm. No. CC 169402

STATE OF FLORIDA DEPARTMENT OF ENVIRONMENTAL REGULATION NOTICE OF INTENT TO ISSUE PERMIT

The Department of Environ cental Regulation gives notice of mental Registers gives a PSD permit to ...
Central Florida Power. Limited:
Partnership (CFPLP), County
Road 630, 5 miles west of Ft.
Meade, Polk County, Florida, to estruct a 258 MW cogeneration facility. A determination of Best Available Control Technology (BACT) was required. The Department is issuing this Intent to Issue for the reasons stated in the Technical Evaluation and Preliminary Determination.

. A person whose substantial interests are affected by the Department's proposed permitting decision may petition for an administrative proceeding (hearing) in accordance with Section 120.57, Florida Statutes. The petition must contain the information set forth below and must be filed (received) in the Office of General Counsel of the Department at 2600 Blair Stone Road, Tallahasses, Florida 32399-2400, within (14) days of publication of this notice. Petitioner shall mail a copy of the petition to the applicant at the address indicated above at the time of filing. Failure to file a petition within this time period shall constitute a waiver of any right such person may have to request an administrative determination (hearing) under Section 190.57, Florida Statutes.

The Petition shall contain the

following information; (a) The name, address; and telephone number of each petitioner, the applicant's name and addre Department Permit File Number and the county in which the project is proposed; (b) A stateent of how and when each petitioner received notice of the Department's action or proposed action; (c) A statement of how each petitioner's substantial interests are affected by the Department's action or proposed action; (d) A statement of the material facts disputed by Petitioner, if any; (e) A statement of facts which peti-A statement of sites which post-tioner contends warrant reversal or modification of the Depart-ment's action or proposed action; (f) A statement of which rules or statutes petitioner contends require reversal or modification of the Department's action or proposed action; and (g) A statement of the relief sought by petitioner, stating precisely the action petitioner wants the Department to take with respect to the Department's action or proposed action.
If a petition is filed, the admini-

strative hearing process is designed to formulate agency action. Accordingly, the Department's final action may be different from the position taken by it in this Notice. Persons . who substantial interests will be affected by any decision of the Department with regard to the application have the right to petition to become a party to the preceeding. The patition must conform to the requirements specified above and be filed (received) within 14 days of publication of this notice in the Office of General Counsel at the above address of the Department. Failure to p tion within the allowed time frame constitutes a waiver of any right such person has to request a hearing under Section 120.57, P.S., and to participate as a party



## United States Department of the Interior



FISH AND WILDLIFE SERVICE 75 Spring Street, S.W. Atlanta, Georgia 30303

February 5, 1993

Mr. C. H. Fancy Chief, Bureau of Air Regulation Florida Department of Environmental Regulation Twin Towers Office Building 2600 Blair Stone Road Tallahassee, Florida 32399-2400 RECEIVED

FEB 0 8 1993

Division of Air Resources Management

Dear Mr. Fancy:

We have completed our review of Central Florida Power's (CFP) permit application and the Florida Department of Environmental Regulation's (FDER) Technical Evaluation and Preliminary Determination document regarding the proposed 258 MW Tiger Bay cogeneration project. This facility would be located near Ft. Meade, approximately 120 km southeast of the Chassahowitzka Wilderness Area (WA), a Class I air quality area administered by the Fish and Wildlife Service. The proposed project would be a significant emitter of particulate matter (PM), beryllium (Be), carbon monoxide (CO), arsenic (As), and nitrogen oxides (NOx). In addition, small amounts of sulfur dioxide (SO2), volatile organic compounds (VOC), mercury (Hg), lead (Pb), and sulfuric acid mist (H2SO4) would be emitted. We are pleased to see that CFP would minimize SO2 and H2SO4 emissions by burning natural gas as the primary fuel, and fuel oil with a maximum sulfur content of 0.05 percent as the backup fuel. This fuel choice allows CFP to avoid the Class I SO, increment consumption issue faced by new, high sulfur fuel-burning projects in the vicinity of the Chassahowitzka WA.

CFP proposes to further minimize emissions from the combustion turbine by using proper combustion controls, water injection, and advanced dry low-NO $_{\rm x}$  combustors. We agree that using proper combustion controls and burning a low sulfur fuel represent best available control technology (BACT) for PM, Be, As, CO, VOC, SO $_{\rm 2}$ , and H $_{\rm 2}$ SO $_{\rm 4}$ . For NO $_{\rm x}$ , we still believe that either dry low-NO $_{\rm x}$  combustors, or water injection in combination with Selective Catalytic Reduction (SCR), is BACT for new combined cycle combustion turbine projects. Dry low-NO $_{\rm x}$  combustors can reduce NO $_{\rm x}$  levels to less than 15 parts per million (ppm) when firing natural gas, while SCR can achieve flue gas NO $_{\rm x}$  concentrations as low as 6 ppm when burning gas and 9 ppm when burning oil.

Company Name: Central Florida P Permit Number: AC-53-1214903 PSD Number: County: PSI PSD-FL-RO Permit Engineer: Feresa Others involved:		Mosphoto	7/14/92	2.
Application:  Initial Application  Incompleteness Letters  Responses  Final Application (if applicable)  Waiver of Department Action  Department Response				
Intent to Issue Notice to Public Technical Evaluation BACT Determination Unsigned Permit Attachments:  Correspondence with: EPA Park Services County Other Proof of Publication Petitions - (Related to extensions, hearings, extensions)	etc.)			
Final Determination:  Final Determination  Signed Permit  BACT Determination  Post Permit Correspondence:  Extensions  Amendments/Modifications  Response from EPA  Response from County  Response from Park Services				

It is evident that the BACT process is driving emissions from combustion turbines downward, and that applicants are looking for ways to inherently lower emissions, rather than opting for add-on flue gas cleaning technologies. The advantages of this approach are obvious. For example, with dry low-NO<sub>x</sub> combustors, the potential problems often cited with SCR (i.e., ammonia slip, disposal of spent catalyst, accidental release of stored ammonia, etc.) would not be a factor. Assuming this process continues, and inherently lower emitting systems are developed, such an approach may be preferred from a total environmental standpoint.

Regardless of which control technology is used, we believe that permit conditions should reflect the minimum achievable NO, The Technical Evaluation and Preliminary emission rates. Determination document for the Tiger Bay project mentions that General Electric (GE) is developing processes, using either steam/water injection or dry-low NO<sub>x</sub> combustor technology, to achieve a NO, control level of 15 ppm when firing natural gas. Accordingly, the FDER proposes to accept CFP's low-NO, burner design with a maximum NO, emission limit of 25 ppm (while burning gas) until December 31, 1997. After that date, the maximum permitted limit would be lowered to 15 ppm. In fact, it is our understanding that GE is hoping to design combustors that achieve an even lower rate, 9 ppm. Therefore, while we do not object to the FDER allowing CFP to emit at the 25 ppm NO, rate until GE develops the combustors, we feel that draft permit condition Number 15 should be revised. As written now, it suggests that SCR may be required if the lower NO, emission limit of 15 ppm cannot be met. We recommend that this permit condition require CFP to install SCR if the dry low-NO, combustors cannot meet the 15 ppm rate, and also that it include the statement that the FDER may revise and lower the allowable BACT limit to less than 15 ppm if such a lower rate is achievable.

Regarding CFP's analyses of Tiger Bay's potential impacts on the Chassahowitzka WA, CFP performed a Level I VISCREEN analysis and showed that there would be low potential for plume impacts in the In addition, CFP addressed potential effects on wilderness area. aquatic and terrestrial resources in the Chassahowitzka WA from increased nitrogen input. As we discussed in detail in our recent letter on the Kissimmee project, we are concerned about increased nitrogen input into the wilderness area and potential problems associated with nutrient enrichment in the aquatic ecosystem. However, because CFP's modeling shows that the annual average nitrogen dioxide impacts in the wilderness area from the Tiger Bay facility alone would be 0.014 micrograms per cubic meter (ug/m³), less than our proposed significant impact level of 0.025 uq/m³, we would not expect the project to contribute significantly to this problem.

If you have any questions regarding this matter, please contact Ms. Tonnie Maniero of our Air Quality office in Denver at 303/969-2071.

Sincerely yours,

James W. Pulliam, Jr. Regional Director

B. Storner, Swilest B. Eunyah, NFS & novak, Palh Co, K. Kasky, KBN G. Harper, EPA

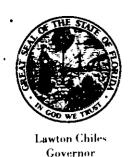
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8. Addressee's Address (Only if requested and fee is paid)



## Florida Department of Environmental Protection

Twin Towers Office Building 2600 Blair Stone Road Tallahassee, Florida 32399-2400

Virginia B. Wetherell Secretary

August 5, 1993

Mr. Robert S. Chatam, P.E. DESTEC ENERGY, INC. 2500 Citywest Blvd., Suite 150 P.O. Box 4411 Houston, Texas 77210-4411

Dear Mr. Chatam:

RE: Central Florida Power L.P.
Permit No. AC53-214903, PSD -FL-190

The Department is in receipt of your letter dated July 30, 1993 regarding several design changes to your proposed Tiger Bay Cogeneration facility.

We have reviewed your letter and have no adverse comments. An "as built" plot and site plan should be included with the Certificate of Completion when you apply for an operation permit for this facility. Thank you for the opportunity to review and comment on this letter.

Sincerely,

C. H. Fancy, P.E.

Chief

Bureau of Air Regulation

CHF/TH/bjb



## Florida Department of Environmental Protection

Twin Towers Office Building 2600 Blair Stone Road Tallahassee, Florida 32399-2400

Virginia B. Wetherell Secretary

October 11, 1993

Mr. Kennard F. Kosky, P.E. President KBN Engineering and Applied Sciences, Inc. 1034 N.W. 57th Street Gainesville, Florida 32605

Dear Mr. Kosky:

This in response to your recent letter notifying the Department of a design change for the Tiger Bay Cogeneration Facility (PSD-FL-190) consisting of a lower operating load of 60 percent. This design change will neither increase emissions nor result in a substantially different ambient impact. This operation will have no impact as far as the construction permit emission limits are concerned. Consequently, a construction permit modification is not required for this design change. However, it is required that this and all other substantive changes in the final design and construction be reported in the operation permit application.

If you have further questions, please contact Preston Lewis, Teresa Heron or Cleve Holladay at (904-488-1344).

Sincerely,

C. H. Fancy, P.

Chief

Bureau of Air Regulation

CHF/CH

cc: Robert Chatham, Destec Energy, Inc. Robert I. Taylor, Tiger Bay L.P. Bill Thomas, SWD



January 30, 1993

Mr. Clair H. Fancy
Bureau of Air Regulation
Florida Department of Environmental Regulation
Twin Towers Office Building
2600 Blair Stone Road
Tallahassee, FL 32399-2400

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Division of Air Resources Management

Re: Central Florida Power Limited Partnership Tiger Bay Cogeneration Plant PSD-FL-190 AC 53-214903

Dear Mr. Fancy:

After review of the Technical Evaluation and Preliminary Determination (TEPD) for this project, dated January 15, 1993, several items in the draft permit were discussed with Ms. Teresa Heron for clarifications or corrections. These items, which were sent by facsimile to Teresa on January 21, 1993, are included as an attachment to this letter. From those discussions, the revisions, which were not considered significant by Teresa, are summarized as follows:

- 1. Specific Condition No. 5, page 5 of 10, TEPD- the operating parameters are for the 184 MW Combustion Turbine. Therefore, the wording, 74 MW Steam Turbine, can be eliminated from the heading.
- 2. Specific Condition No. 8, page 7 of 10, TEPD- Method 201, Method 12, Method 101A, and Method 8, as referenced, are either not applicable or were inadvertantly inserted in this condition. These methods should be deleted.

Method 202, Determination of Condensible Particulate Emissions from Stationary Sources, should be inserted and will be used with Method 201A.

- 3. Specific Condition No. 9, page 7 of 10, TEPD- Method 201A and Method 201 are listed for determining the initial compliance status of particulate matter emissions. This should be changed to Method 201A and Method 202.
- 4. Specific Condition No. 13, page 7 of 10, TEPD- Reference to the "proposed" NOx standard should be revised to the "NSPS" NOx standard since the standard is a final regulation.

ERIE!	ESTIONS? CALL BOO 238-5355 TOL	FREE.	AIRBILL PACKAGE TRACKING NUMBER	102882	53Pg
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- 5. Table 1, TEPD- Several corrections regarding the emission rates and wording:
  - a. For CO(CT), oil-change 98 lbs/hr to 98.4 lbs/hr
  - b. For opacity, oil- insert footnote D
  - c. For Hg, As, Be, Pb- include emission rate in lb/hr and TPY
  - d. For Hg, As, Be, Pb- change factor of 10<sup>-12</sup> to 10<sup>-6</sup>
  - e. In footnote A- delete No. 2 in reference to distillate oil
  - f. In footnote B- include emission rate of 97.2 lb/hr in reference to the NOx emission limit of 15 ppmvd; 15 ppmv should be ppmvd
- 6. Best Available Control Technology (BACT) Determination, Table on page 9:
  - a. For NOx(CT)- include lb/hr emission rates and correct ppmv to ppmvd
  - b. For CO(CT)- change 98 lbs/hr to 98.4 lbs/hr
  - c. For Hg, As, Be, Pb- include emission rate in lb/hr and TPY
  - d. For Hg, As, Be, Pb- change factor of 10<sup>-12</sup> to 10<sup>-6</sup>
  - e. In footnote b- delete No. 2 in reference to distillate oil
  - f. in footnote c- change 8460 hours per year to 8760
  - g. in footnote c- delete 300 hours per year and insert 3,742,327 gallons per calendar year

Items that remained as issues to be addressed include the following.

- 1. The PM10 emission limits for the CT firing natural gas and oil are currently expressed in units of lbs/MMBtu. However, based on the manufacturer's guarantee, the emission limits were presented in the application in units of lb/hr (see recommended changes in Table 1 of the TEPD; page 3 and table on page 9 of the BACT Determination). As shown in the attached KBN Table 1, the PM emission rate may exceed 0.01 lbs/MMBtu for oil-firing at base load and high temperature conditions and at 70 percent load for the range of temperatures. Although the emission limit of 0.01 lbs/MMBtu is based on base load and ambient temperature of 27 °F in the tables, the text does not mention the operating condition or temperature. To avoid this potential confusion, it is recommended that the CT emission limit for firing natural gas and fuel oil be expressed as 9 and 17 lb/hr, respectively.
- 2. On page 7 of the BACT Determination, it is stated that General Electric (GE) is currently developing programs using both steam/water injection and dry low NOx combustor to achieve NOx emission control level of 9 ppm when firing natural gas. From recent discussions with GE, it is our undersatnding that the emission control level that they are attempting to achieve is 15 ppm.
- 3. To be consistent with emission rates presented for most pollutants, it is recommended that the limits for sulfuric acid mist (H<sub>2</sub>SO<sub>4</sub>) should be expressed to 3 three significant digits (see Table 1 of the TEPD and the table on page 9 of the BACT Determination.



We appreciate your efforts in preparing the draft permit and reviewing our comments. Please call me if there any further questions on the material submitted.

Sincerely, Herma (7. )Grahy

Kennard F. Kosky, P.E.

President

Enclosure

cc: Robert I. Taylor, Central Florida Power, L.P.

Robert Chatham, Destec Energy, Inc.

Teresa Heron, FDER C. Holladay



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## Florida Department of Environmental Regulation

Twin Towers Office Bldg. • 2600 Blair Stone Road • Tallahassee, Florida 32399-2400 Lawton Chiles, Governor Carol M. Browner, Secretary

October 9, 1992

CERTIFIED MAIL - RETURN RECEIPT REQUESTED

Mr. Robert I. Taylor, Project Manager Central Florida Power, L.P. 2500 City West Blvd., Suite 150 Houston, Texas 77042

Dear Mr. Taylor:

This letter is to confirm the Department's conversation with Mr. Ken Kosky that additional information (updated process flow diagram showing the volumetric flow rates) is needed to complete your application for permit to construct the Tiger Bay Cogeneration Plant (File No. AC53-214903/PSD-FL-190). We are working directly with Mr. Kosky to obtain the needed information and will resume processing this application when it is complete.

If you have any questions on this matter, please write to me or call Mirza Baig, review engineer, at (904) 488-1344.

Sincerely,

for of H. Fancy, P.E.

Chief

Bureau of Air Regulation

CHF/MB/plm

cc: Ken Kosky, KBN

B. Shomas, swhist Q. Harper EPA B. Mitchell, NPS



October 23, 1992

Mr. G. Preston Lewis, P.E. Bureau of Air Regulation Florida Department of Environmental Regulation Twin Towers Office Building 2600 Blair Stone Road Tallahassee, Florida 32399-2400

RE: Central Florida Power Limited Partnership Tiger Bay cogeneration plant PSD-FL-190 AC 53-214903

Dear Mr. Lewis,

Deres (713) 735-4000

MTR Z A

The talk

P. O. BOX 4411

DESTEC ENGINEERING, INC. 2500 CITYWEST BLVD., SUITE 150

HOUSTON, TEXAS 77210-4411

Prestor

Per our conversation on October 22, I want to personally thank you for your involvement and decision to determine our application as administratively complete as of October 9, 1992 and your commitment to issue the draft permit by December 9, 1992. KBN and I look forward to working with Mr. Mirza Baig and your department in the review and processing of our application and final issuance of the permit.

Please call me at (713) 735-4087 should you or your department have questions or comments about our application.

Sincerely,

Robert S. Chatham, P.E. Senior Environmental Engineer

Rath Chathan

RSC:tk

plewis.wpR

cc:Mr. Mirza Baig - FDER, Tallahassee

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OCT 2 4 1992

Division of Air Resources ivianagement



October 9, 1992

Mr. Clair H. Fancy, Chief Bureau of Air Regulation Florida Department of Environmental Regulation Twin Towers Office Building 2600 Blair Stone Road Tallahassee, Florida 32399-2400

Attention: Mirza Baig

RE: Central Florida Power Limited Partnership

Tiger Bay (formerly Central Florida) Cogeneration Plant

PSD-FL-190 AC 53-214903

Dear Mirza:

As we discussed today, we will be sending to you information relating to the volumetric flow rates in the process flow diagrams sent in our letter of August 26, 1992.

Sincerely,

Januard F. Kosky, P.E.

Principal Engineer

KFK/mlb

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OCT 1 6 1992

Division of Air Resources Management



September 9, 1992

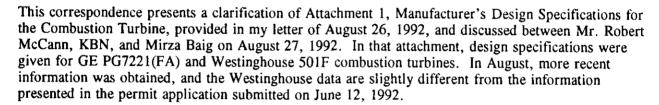
Mr. Clair H. Fancy, Chief Bureau of Air Regulation Florida Department of Environmental Regulation Twin Towers Office Building 2600 Blair Stone Road Tallahassee, FL 32399-2400

Re: Central Florida Power Limited Partnership

Tiger Bay (formerly Central Florida) Cogeneration Plant

PSD-FL-190 AC 53-214903

Dear Mr. Fancy:



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Resources Management

As shown in Tables 1 through 4, the changes in maximum emission rates for the Westinghouse turbine are minor and generally are within approximately 2 percent of the rates specified in the permit application (see Tables 5 through 8). The emission rates for other regulated and non-regulated pollutants increase slightly due to the slight increase in the heat input rate (i.e., MMBtu/hr) which generally is the basis of the emission factor for those pollutants. Comparisons of the maximum emissions for the Westinghouse and GE turbines as presented in the permit application and for the revised Westinghouse turbine are presented in Tables 9 through 12. As shown, the emission data, in tons per year (TPY), for the GE machine at 72°F ambient temperature are higher for all pollutants except VOC when compared to the Westinghouse data. The revised maximum VOC emission rate for the Westinghouse turbine is slightly higher than that presented in the permit application (45.6 TPY compared to 45.3 TPY).

Table 3-1 from the support document to the PSD permit application has been revised to reflect the worstcase emission rates for each pollutant from either turbine. The worst-case emission rates are used to determine pollutant applicability under PSD regulations by comparing the maximum allowable emissions for the project to the PSD significant emission rates.

The modeling analysis presented as part of the permit application also does not significantly change and still provides a conservative estimate of short-term and annual impacts. The impacts were based on the the worst-case emission rates from either the GE emission data or the previous Westinghouse emission data which are still higher than the updated Westinghouse emission data.

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KBN ENGINEERING AND APPLIED SCIENCES, INC.

Mr. Clair H. Fancy, Chief September 8, 1992 Page 2



Therefore, the updated design specifications for the Westinghouse turbine are not a significant change from the material presented in the original application and should not materially affect any conclusions drawn from original application.

Please call me if there any further questions on the material submitted.

Sincerely,

Kennard F. Kosky, P.E.

President

KFK/dmpm

Enclosure

Robert I. Taylor, Central Florida Power, L.P. cc:

Robert Chatham, Destec Engineering, Inc.

Mirza Baig, FDER

File (2)

6. Holladay B. Homas, SW Dist G. Murph FPA B. Mitchell, NPS

Table 3-1. Net Increase in Emissions Due To the Central Florida Cogeneration Facility Compared to the PSD Significant Emission Rates (REVISED)

	Emissions (TPY)						
		Emissic Prop Fac	ntial ons From posed ility <sup>a</sup>		Significant		
Pollutant	Permi Applicat		Rev	ised	Emission Rate	PSD Review	
Sulfur Dioxide <sup>b</sup>	33.1	(GE)	33.1	(GE)	40	No	
Particulate Matter (TSP)	45.0	(GE)	45.0	(GE)	25	Yes	
Particulate Matter (PM10)	45.0	(GE)	45.0	(GE)	15	Yes	
Nitrogen Dioxide	702.1	(GE)	702.1	(GE)	40	Yes	
Carbon Monoxide	243.1	(GE)	243.1	(GE)	100	Yes	
Volatile Organic Compounds	45.3	(W)	45.6	(W)	40	Yes	
ead	0.00219	(GE)	0.00219	(GE)	0.6	No	
ulfuric Acid Mist	4.2	(GE)	4.2	(GE)	7	No	
otal Fluorides	0.00802	(GE)	0.00802	(GE)	3	No	
otal Reduced Sulfur	NEG		neg		10	No	
educed Sulfur Compounds	NEG		NEG		10	No	
ydrogen Sulfide .	NEG		NEG		10	No	
Asbestos	NEG		NEG		0.007	No	
eryllium	0.000616	(GE)	0.000616	(GE)	0.0004	Yes	
dercury	0.000739	(GE)	0.000739	(GE)	0.1	No	
inyl Chloride	NEG		NEG		1	No	
enzene	NEG		NEG		0	No	
adionuclides	NEG		NEG		·	No	
norganic Arsenic	0.00104	(GE)	0.00104	(GE)	0	Yes	

Note: GE = General Electric.

NEG = Negligible.

W = Westinghouse.

All calculations based on 72°F base load condition.

Based on a maximum sulfur content specification of 0.05 percent in fuel oil.

Maximum annual emissions based on the gas turbine firing distillate oil and natural gas for 300 and 8,460 hours, respectively, and duct burner firing natural gas for 8,760 hours. Tables A-15 through A-18 present emissions for the GE machine while Tables A-33 through A-36 present emissions for the Westinghouse machine.

Table 1. Difference in Maximum Emissions for Criteria Pollutants for Tiger Bay Cogeneration Facility-Westinghouse 501F, Base Load, Permit Application Compared to Revised Values

Pollutant	Gas Turbin	Gas Turbine- Distillate Oil			Gas Turbine- Natural Gas			Duct Burner- Natural Gas			Emissions	
	27 of	72 oF	97 oF	27 oF	72 of	97 of	27 oF	72 oF	97 of	27 oF	72 oF	97 oF
Hours of Opera	tion	300	. <u>.</u>		8460			8760				<del></del>
Particulate:												
lb/hr TPY	-9.00E-01 -1.35E-01		0.00E+00 0.00E+00	2.00E-01 8.46E-01	1.00E-01 4.23E-01	1.00E-01 4.23E-01	0.00E+00 0.00E+00	0.00E+00 0.00E+00	0.00E+00 0.00E+00	-9.00E-01 7.11E-01	-1.00E-01 4.08E-01	0.00E+00 4.23E-01
Sulfur Dioxide	:											
lb/hr TPY		-7.94E-01 -1.19E-01	-6.95E-01 -1.04E-01	3.93E-02 1.66E-01	3.78E-02 1.60E-01	3.64E-02 1.54E-01	0.00E+00 0.00E+00	0.00E+00 0.00E+00	0.00E+00 0.00E+00	-1.70E+00 -8.86E-02	-7.94E-01 4.06E-02	-6.95E-01 4.95E-02
Nitrogen Oxide:	s:				•							
lb/hr TPY	-7.98E-01 -1.20E-01	4.82E+00 7.22E-01	4.27E+00 6.40E-01	-6.21E+00 -2.63E+01	2.49E+00 1.05E+01	2.69E+00 1.14E+01	0.00E+00 0.00E+00	0.00E+00 0.00E+00	0.00E+00 0.00E+00	-7.98E-01 -2.64E+01	4.82E+00 1.13E+01	4.27E+00 1.20E+01
Carbon Monoxid	e:											
lb/hr TPY	-2.58E+00 -3.87E-01	1.36E+00 2.05E-01	1.67E+00 2.51E-01	1.27E+00 5.37E+00	2.70E-01 1.14E+00	2.65E-01 1.12E+00	0.00E+00 0.00E+00	0.00E+00 0.00E+00	0.00E+00 0.00E+00	-2.58E+00 4.98E+00	1.36E+00 1.34E+00	1.67E+00 1.37E+00
VOCs (as methar	ne):											
lb/hr TPY	-1.21E-01 -1.82E-02	1.59E-01 2.38E-02	1.62E-01 2.43E-02	6.16E-02 2.61E-01	6.13E-02 2.59E-01	6.39E-02 2.70E-01	0.00E+00 0.00E+00	0.00E+00 0.00E+00	0.00E+00 0.00E+00	-1.21E-01 2.43E-01	1.59E-01 2.83E-01	1.62E-01 2.94E-01
Lead:												
lb/hr TPY	4.54E-06 6.81E-07	1.37E-04 2.06E-05	1.37E-04 2.05E-05	AA AA	NA NA	NA NA	NA NA	NA NA	NA NA	4.54E-06 6.81E-07	1.37E-04 2.06E-05	1.37E-04 2.05E-05

79Y.

Table 2. Difference in Maximum Emissions of Other Regulated Pollutants for Tiger Bay Cogeneration Facility Westinghouse 501F, Base Load, Permit Application Compared to Revised Values

Pollutant		Gas Turbine- Distillate Oil			Gas Turbine- Natural Gas			Duct Burner- Natural Gas			Maximum Emissions		
····		27 oF	72 oF	97 oF	27 oF	72 oF	97 of	27 oF	72 oF	97 oF	27 oF	72 oF	97 oF
Arsenic													
	lb/hr TPY	2.14E-06 3.21E-07	6.47E-05 9.71E-06	6.44E-05 9.67E-06	AA AA	NA NA	NA NA	NA NA	NA NA	NA NA	2.14E-06 3.21E-07	6.47E-05 9.71E-06	6.44E-05 9.67E-06
Beryllium	n												
21,,	lb/hr	1.27E-06	3.85E-05	3.84E-05	NA	NA NA	NA NA	NA	NA NA	NA NA	1.27E-06	3.85E-05	3.84E-05
	TPY	1.91E-07	5.78E-06	5.75E-06	NA	NA	NA	NA	NA	NA	1.91E-07	5.78E-06	5.75E-06
Mercury													
	lb/hr	1.53E-06	4.62E-05	4.60E-05	NA NA	, NA Na	NA	NA	NA	NA	1.53E-06	4.62E-05	4.60E-05
	TPY	2.29E-07	6.94E-06	6.91E-06	NA	NA	NA	NA	NA	NA	2.29E-07	6.94E-06	6.91E-06
Fluoride													
	lb/hr	1.66E-05	5.01E-04	4.99E-04	NA	NA NA	AA	NA	NA	NA	1.66E-05	5.01E-04	4.99E-04
	TPY	2.49E-06	7.52E-05	7.49E-05	NA	NA	NA	NA	NA	NA	2.49E-06	7.52E-05	7.49E-05
Sulfuric	Acid												
Mist	`lb/hr	-2.08E-01	-9.73E-02		5.07E-03	4.87E-03	4.69E-03	0.00E+00	0.00E+00	0.00E+00	-2.08E-01	-9.73E-02	-8.52E-02
	TPY	-3.12E-02	-1.46E-02	-1.28E-02	2.14E-02	2.06E-02	1.98E-02	0.00E+00	0.00E+00	0.00E+00	-9.78E-03	6.01E-03	7.06E-03

Table 3. Difference in Maximum Emissions of Non-Regulated Pollutants for Tiger Bay Cogeneration Facility-Westinghouse 501F, Base Load, Permit Application Compared to Revised Values

ollutant	Gas Turbine- Distillate Oil			Gas Turbi	Gas Turbine- Natural Gas			er- Natural	Gas	Maximum Emissions		
	 27 oF	72 of	97 of	27 oF	72 oF	97 oF	27 oF	72 of	97 oF	27 of	72 oF	97 of
Manganese												
lb/ TPY	7.14E-06 1.07E-06	2.16E-04 3.24E-05	2.15E-04 3.22E-05	NA NA	NA NA	NA NA	NA NA	' NA Na	NA NA	7.14E-06 1.07E-06	2.16E-04 3.24E-05	2.15E-04 3.22E-05
Nickel							•					
lb/ TPY	8.67E-05 1.30E-05	2.62E-03 3.93E-04	2.61E-03 3.91E-04	NA NA	NA NA	NA NA	NA NA	NA NA	NA NA	8.67E-05 1.30E-05	2.62E-03 3.93E-04	2.61E-03 3.91E-04
Cadmium												
lb/ TPY	5.35E-06 8.03E-07	1.62E-04 2.43E-05	1.61E-04 2.42E-05	NA NA	. NA NA	NA NA	NA NA	NA NA	NA NA	5.35E-06 8.03E-07	1.62E-04 2.43E-05	1.61E-04 2.42E-05
Chromium												
lb/	2.42E-05	7.32E-04	7.29E-04	NA	NA	NA	NA	NA	NA	2.42E-05	7.32E-04	7.29E-04
TPY	3.63E-06	1.10E-04	1.09E-04	NA	NA	NA	NA	NA	NA	3.63E-06	1.10E-04	1.09E-04
Copper												
lb/	1.43E-04	4.32E-03	4.30E-03	NA	NA	NA	NA	NA	NA	1.43E-04	4.32E-03	4.30E-03
TPY	2.14E-05	6.47E-04	6.44E-04	NA	NA	NA	NA	NA	NA	2.14E-05	6.47E-04	6.44E-04
Vanadium			•									
lb/	3.54E-05	1.07E-03	1.07E-03	NA	NA	NA	NA	NA	NA	3.54E-05	1.07E-03	1.07E-03
TPY	5.32E-06	1.61E-04	1.60E-04	NA	NA	NA	NA	NA	NA	5.32E-06	1.61E-04	1.60E-04
Selenium		•										
lb/	1.19E-05	3.61E-04	3.59E-04	NA.	NA	NA	NA	NA	NA	1.19E-05	3.61E-04	3.59E-04
TPY	1.79E-06	5.41E-05	5.39E-05	NA	HA	NA	NA	NA	NA	1.79E-06	5.41E-05	5.39E-05
Polycyclic												
Organic lb/	1.42E-07	4.28E-06	4.27E-06	1.45E-05	1.40E-05	1.35E-05	0.00E+00	0.00E+00	0.00E+00	1.45E-05	1.40E-05	1.35E-0
Matter TPY	2.13E-08	6.43E-07	6.40E-07	6.15E-05	5.91E-05	5.69E-05	0.00E+00	0.00E+00	0.00E+00	6.15E-05	5.98E-05	5.76E-05
Formaldehyde												
lb/	2.07E-04	6.24E-03	6.21E-03	1.15E-03	1.11E-03	1.07E-03	0.00E+00	0.00E+00	0.00E+00	2.07E-04	6.24E-03	6.21E-0
TPY	3.102-05	9.36E-04	9.32E-04	4.87E-03	4.68E-03	4.51E-03	0.00E+00	0.00E+00	0.00E+00	4.90E-03	5.62E-03	5.44E-0

Table 4. Difference in Maximum Emissions for Additional Non-Regulated Pollutant for Tiger Bay Cogeneration Facility-Westinghouse 501F, Base Load, Permit Application Compared to Revised Values

ollutant		Gas Turbin	e- Distilla	ite Oil	Gas Turbir	ne- Natural	Gas	Duct Burne	er- Natural	Gas	Maximum	Emissions	
		27 of	72 oF	97 of	27 oF	72 oF	97 oF	27 of	72 oF	97 oF	27 oF	72 oF	97 oF
Antimony	,												
	lb/hr TPY	1.11E-05 1.67E-06	3.37E-04 5.05E-05	3.35E-04 5.03E-05	NA NA	NA NA	NA NA	NA NA	NA NA	NA NA	1.11E-05 1.67E-06	3.37E-04 5.05E-05	3.35E-04 5.03E-05
		.,					****						
Barium	ĺb/hr	9.95E-06	3.01E-04	3.00E-04	NA	NA	NA	NA	NA	NA	9.95E-06	3.01E-04	3.00E-04
	TPY	1.49E-06	4.51E-05	4.49E-05	NA NA	NA	NA	NA	NA	NA	1.49E-06	4.51E-05	4.49E-05
Cobalt													
	lb/hr	4.62E-06	1.40E-04	1.39E-04	NA	, NA	NA	NA	NA	NA	4.62E-06	1.40E-04	1.39E-04
	TPY	6.93E-07	2.10E-05	2.09E-05	NA	NA	NA	NA	NA	NA	6.93E-07	2.10E-05	2.09E-05
Zinc													
	lb/hr	3.48E-04	1.05E-02	1.05E-02	NA	NA	NA	NĄ	NA	NA	3.48E-04	1.05E-02	1.05E-02
	TPY	5.23E-05	1.58E-03	1.57E-03	NA	NA	NA	NA	NA	NA	5.23E-05	1.58E-03	1.57E-03
Chlorine													
	lb/hr	-8.22E-04			NA	NA	NA	NA	NA	NA	-8.22E-04		-3.36E-04
	TPY	-1.23E-04	-5.81E-05	-5.04E-05	NA	NA	NA	NA	NA	NA	-1.23E-04	-5.81E-05	-5.04E-05

Table 5. Percent Change in Maximum Emissions for Criteria Pollutants for Tiger Bay Cogeneration Facility-Westinghouse 501F, Base Load, Permit Application Compared to Revised Values

Pollutant	Gas Turbi	ne- Disti	llate Oil	Gas Turb	oine- Natu	ıral Gas	Duct Bur	ner- Natu	ıral Gas	Maximum	Emission	ıs
	27 oF	72 of	97 oF	27 oF	72 oF	97 oF	27 oF	72 oF	97 oF	27 oF	72 oF	97 oF
Hours of Operation		300			8460	<del></del>		8760				
Particulate:												
lb/hr TPY	-2.23% -2.23%	-0.26% -0.26%	0.00%	3.12% 3.13%	1.69% 1.69%	1.79% 1.79%	0.00% 0.00%	0.00% 0.00%	0.00% 0.00%	-2.17% 1.90%	-0.25% 1.16%	0.00% 1.26%
Sulfur Dioxide:		•										
lb/hr TPY	-1.87% -1.87%	-0.91% -0.91%	-0.85% -0.85%	0.82% 0.82%	0.88% 0.88%	0.91% 0.91%	0.00% 0.00%	0.00% 0.00%	0.00%	-1.86% -0.25%	-0.91% 0.13%	-0.847 0.167
Nitrogen Oxides:						•						
lb/hr TPY	-0.27% -0.27%	1.81% 1.81%	1.72% 1.72%	-3.67% -3.67%	1.75% 1.75%	2.02% 2.02%	0.00% 0.00%	0.00% 0.00%	0.00% 0.00%	-0.27% -3.29%	1.74% 1.64%	1.657 1.877
Carbon Monoxide:												
lb/hr TPY	-1.58% -1.58%	0.87% 0.87%	1.14% 1.14%	3.79% 3.79%	0.87% 0.87%	0.92% 0.92%	0.00% 0.00%	0.00% 0.00%	0.00% 0.00%	-1.49% 2.37%	0.82% 0.68%	1.073
VOCs (as methane):			•									
lb/hr TPY	-0.64% -0.64%	0.87% 0.87%	0.94% 0.94%	0.77% 0.77%	0.87% 0.87%	0.92% 0.92%	0.00% 0.00%	0.00% 0.00%	0.00% 0.00%	-0.56% 0.49%	0.75% 0.63%	0.817 0.667
Lead:												
lb/hr TPY	0.03% 0.03%	1.00%	1.07% 1.07%	NA NA	NA NA	NA NA	NA NA	NA NA	NA NA	0.03% 0.03%	1.00% 1.00%	1.077

Table 6. Percent Change in Maximum Emissions of Other Regulated Pollutants for Tiger Bay Cogeneration Facility Westinghouse 501F, Base Load, Permit Application Compared to Revised Values

Poliutant	:	Gas Turbi	ne- Disti	llate Oil	Gas Turb	ine- Natu	ural Gas	Duct Bur	ner- Natu	ırat Gas	Maximum	n Emissior	ns
		27 of	72 oF	97 oF	27 of	72 oF	97 oF	27 oF	72 oF	97 oF	27 oF	72 of	97 of
Arsenic													
	lb/hr TPY	0.03% 0.03%	1.00%	1.07% 1.07%	NA NA	NA NA	NA NA	NA NA	NA NA	NA NA	0.03% 0.03%	1.00% 1.00%	ל1.077 ל1.077
Berylliu	m .												
,	lb/hr	0.03%	1.00%	1.07%	NA	NA	NA	NA	NA	NA	0.03%	1.00%	1.073
	TPY	0.03%	1.00%	1.07%	NA	NA	NA	NA	NA	NA	0.03%	1.00%	1.073
Mercury													
•	lb/hr	0.03%	1.00%	1.07%	NA	NA	, NA	NA	NA	NA	0.03%	1.00%	1.073
	TPY	0.03%	1.00%	1.07%	NA	NA	NA	NA	NA	NA	0.03%	1.00%	1.07%
Fluoride	<b>!</b>												
	lb/hr	0.03%	1.00%	1.07%	NA	NA	NA	NA	NA	NA	0.03%	1.00%	1.07%
	TPY	0.03%	1.00%	1.07%	NA	NA	NA	NA	NA	NA	0.03%	1.00%	1.07%
Sulfuric	Acid												
Mist	'lb/hr	-1.87%	-0.91%	-0.85%	0.82%	0.88%	0.91%	0.00%	0.00%	0.00%	-1.86%	-0.91%	-0.84%
	TPY	-1.87%	-0.91%	-0.85%	0.82%	0.88%	0.91%	0.00%	0.00%	0.00%	-0.22%	0.15%	0.18%

Table 7. Percent Change in Maximum Emissions of Non-Regulated Pollutants for Tiger Bay Cogeneration Facility-Westinghouse 501F, Base Load, Permit Application Compared to Revised Values

ollutant		Gas Turbi	ne- Disti	llate Oil	Gas Turb	ine- Natu	ıral Gas	Duct Bur	ner- Natu	ıral Gas	Maximum	Emission	ıs
		27 oF	72 of	97 oF	27 of	72 oF	97 oF	27 oF	72 oF	97 oF	27 oF	72 of	97 of
Manganes													
	lb/hr TPY	0.03% 0.03%	1.00% 1.00%	1.07% 1.07%	NA NA	NA NA	NA NA	NA NA	NA NA	NA NA	0.03% 0.03%	1.00% 1.00%	1.07
Nickel													
	lb/hr	0.03%	1.00%	1.07%	NA	NA	NA	NA	NA	NA	0.03%	1.00%	1.07
	TPY	0.03%	1.00%	1.07%	NA	NA	NA	NA	NA	NA	0.03%	1.00%	1.07
Cadmium													
	lb/hr TPY	0.03% 0.03%	1.00% 1.00%	1.07% 1.07%	NA NA	NA NA	. NA Na	NA NA	NA NA	NA NA	0.03%	1.00%	1.07 1.07
	161	0.03%	1.00%	1.07%	77	NA.	na.	NA.	NA	n/A	0.03%	1.00%	1.07
Chromium			4 000	4.039	61.6		414	***			0.07*	4 000	4 07
	lb/hr TPY	0.03% 0.03%	1.00%	1.07% 1.07%	NA NA	NA NA	NA NA	NA NA	NA NA	NA NA	0.03% 0.03%	1.00%	1.07 1.07
•													-
Copper	lb/hr	0.03%	1.00%	1.07%	NA	NA	NA	NA	NA	NA	0.03%	1.00%	1.07
	TPY	0.03%	1.00%	1.07%	NA	NA	NA	NA	NA	NA	0.03%	1.00%	1.07
Vanadium	1			1									
V	lb/hr	0.03%	1.00%	1.07%	NA	NA	NA	NA	NA	NA	0.03%	1.00%	1.07
	TPY	0.03%	1.00%	1.07%	NA	NA	NA	NA	NA	NA	0.03%	1.00%	1.07
Selenium	1			•									
	lb/hr	0.03%	1.00%	1.07%	NA	NA	NA	NA	NA	NA	0.03%	1.00%	1.07
	TPY	0.03%	1.00%	1.07%	NA	NA	NA	NA	NA	NA	0.03%	1.00%	1.07
Polycycl				· ·									
Organic Matter	lb/hr TPY	0.03% 0.03%	1.00% 1.00%	1.07% 1.07%	0.82% 0.82%	0.88% 0.88%	0.91% 0.91%	0.00%	0.00%	0.00% 0.00%	0.77% 0.76%	0.83% 0.83%	0.85
		0.05%	1100%	11.57%	0,012	0,00%	0.71%	0.00%	0.00%	0.00%	0.10%	0.00%	0.05
Formal de	hyde lb/hr	0.03%	1.00%	1.07%	0.82%	0.88%	0.91%	0.00%	0.00%	0.00%	0.03%	0.99%	1.05
	TPY	0.03%	1.00%	1.07%	0.82%	0.88%	0.91%	0.00%	0.00%	0.00%	0.67%	0.85%	0.88

Table 8. Percent Change in Maximum Emissions for Additional Non-Regulated Pollutant for DESTEC Central Florida Cogeneration Facility-Westinghouse 501F, Base Load, Permit Application Compared to Revised Values

ollutant		Gas Turbi	ne- Disti	llate Oil	Gas Turbine- Natural Gas			Duct Burner- Natural Gas			Maximum Emissions		
		27 of	72 of	97 oF	27 oF	72 oF	97 oF	27 oF	72 oF	97 oF	27 oF	72 oF	97 of
Antimon	y												
	lb/hr TPY	0.03% 0.03%	1.00%	1.07% 1.07%	NA NA	NA NA	NA NA	NA NA	NA NA	NA NA	0.03% 0.03%	1.00% 1.00%	1.07% 1.07%
Barium										•			
	lb/hr	0.03%	1.00%	1.07%	NA	NA	NA	NA	NA	NA	0.03%	1.00%	1.07%
	TPY	0.03%	1.00%	1.07%	NA	NA	NA	NA	NA	NA	0.03%	1.00%	1.07%
Cobalt													
000011	lb/hr	0.03%	1.00%	1.07%	NA	NA	. NA	NA	NA	NA	0.03%	1.00%	1.07%
	TPY	0.03%	1.00%	1.07%	NA	NA	NA	NA	NA	NA	0.03%	1.00%	1.07%
Zinc													
	lb/hr	0.03%	1.00%	1.07%	NA	NA	NA	NA	NA	NA	0.03%	1.00%	1.07%
	TPY	0.03%	1.00%	1.07%	NA	NA	NA	NA	NA	NA	0.03%	1.00%	1.07%
Chlorine	ė												
	lb/hr	-1,87%	-0.91%	-0.85%	NA	NA	NA	NA	NA	NA	-1.87%	-0.91%	-0.85%
	TPY	-1.87%	-0.91%	-0.85%	NA	NA	NA	NA	NA	NA	-1.87%	-0.91%	-0.85%

Table 9. Comparison of Maximum Emissions for Criteria Pollutants for Tiger Bay Cogeneration Facility-Permit Application for GE and Westinghouse Turbines and Revised Westinghouse Data, Base Load

Pollutant	Per	mit Appli GE PG7221	cation (FA)		mit Appli tinghouse		Revised Data Westinghouse 501F			
	27 oF	72 oF	97 of	27 oF	72 oF	97 oF	27 oF	72 oF	97 of	
Particulate:										
lb/hr TPY	18.00 45.00			41.40 37.51			40.50 38.22			
Sulfur Dioxide:										
lb/hr TPY	100.02 36.82		82.11 30.74	91.35 35.24	87.31 32.46	82.32 30.52	89.65 35.15			
Nitrogen Oxides:						•				
lb/hr TPY	336.22 777.46		278.04 655.15	300.93 802.48	276.05 685.75	258.65 644.03	300.13 776.09		262.92 656.07	
Carbon Monoxide:										
lb/hr TPY	108.41 265.12	98.62 243.12	93.20 230,91	173.49 209.97	167.04 198.55	156.99 187.82	170.91 214.95		158.66 189.19	
VOCs (as methane):			,							
lb/hr TPY	10.40 25.63		9.40 - 23.66	21.76 49.53	21.18 45.29		21.64 49.77		20.22 44.95	
Lead:										
lb/hr TPY		1.46E-02 2.19E-03			1.37E-02 2.05E-03			1.38E-02 2.07E-03		

Note: Based on firing natural gas and distillate oil for 8470 and 300 hours, respectively. Total emissions include emissions from the combustion turbine and duct burner.

Table 10. Comparison of Maximum Emissions of Other Regulated Pollutants for Tiger Bay Cogeneration Facility-Permit Application for GE and Westinghouse Turbines and Revised Westinghouse Data, Base Load

Pollutant		Maxim	um Emissi	ons	Maximum Emissions			Maximum Emissions		
		27 oF	72 oF	97 oF	27 oF	72 of	97 of	27 of	72 of	97 oF
Arsenic										
	lb/hr TPY		6.90E-03 1.04E-03			6.45E-03 9.68E-04	6.02E-03 9.04E-04			6.09E-03 9.13E-04
Beryllium	l						•			
•	lb/hr TPY		4.11E-03 6.16E-04		3.99E-03 5.98E-04					3.62E-03 5.44E-04
Mercury										
,	lb/hr TPY		4.93E-03 7.39E-04		4.79E-03 7.18E-04					4.35E-03 6.52E-04
Fluoride										
	lb/hr TPY		5.35E-02 8.02E-03		5.19E-02 7.79E-03					4.72E-02 7.08E-03
Sulfuric	Acid									
Mist	'lb/hr TPY		1.09E+01 4.18E+00		1.12E+01 4.46E+00				1.06E+01 4.11E+00	1.00E+01 3.86E+00

Note: Based on firing natural gas and distillate oil for 8470 and 300 hours, respectively. Total emissions include emissions from the combustion turbine and duct burner.

Table 11. Comparison of Maximum Emissions of Non-Regulated Pollutants for Tiger Bay Cogeneration Facility-Permit Application for GE and Westinghouse Turbines and Revised Westinghouse Data, Base Load

ollutant		Maxim	um Emissi	ons	Maxim	ım Emissi	ons	Maxim	um Emissi	ons
	<u>.</u>	27 oF	72 of	97 oF	27 oF	72 of	97 of	27 oF	72 oF	97 oF
Manganes	se									
•	lb/hr TPY	2.59E-02 3.88E-03	2.30E-02 3.45E-03	2.12E-02 3.19E-03			2.01E-02 3.01E-03	2.23E-02 3.35E-03	2.17E-02 3.26E-03	
Nickel										•
	lb/hr TPY			2.58E-01 3.87E-02	2.71E-01 4.07E-02			2.71E-01 4.07E-02	2.64E-01 3.96E-02	
Cadmium										
	lb/hr TPY		1.73E-02 2.59E-03		1.68E-02 2.51E-03			1.68E-02 2.51E-03	1.63E-02 2.44E-03	
Chromium	1									
	lb/hr TPY		7.80E-02 1.17E-02		7.58E-02 1.14E-02			7.58E-02 1.14E-02	7.37E-02 1.11E-02	
Copper										
	lb/hr TPY		4.60E-01 6.90E-02	6.37E-02	4.47E-01 6.70E-02			4.47E-01 6.70E-02		
Vanadium	1			i						
	lb/hr TPY		1.14E-01 1.71E-02		1.11E-01 1.66E-02			1.11E-01 1.66E-02		
Selenium	1			•						
	lb/hr TPY	4.33E-02 6.50E-03			3.74E-02 5.60E-03			3.74E-02 5.61E-03		
Polycycl	ic			,						
Organic Matter	lb/hr TPY	1.91E-03 8.17E-03			1.88E-03 8.05E-03			1.90E-03 8.11E-03	1.71E-03 7.31E-03	1.60E-03 6.86E-03
Formalde	hyde									
	ĺb/hr TPY	7.58E-01 7.53E-01	6.74E-01 6.79E-01	6.23E-01 6.33E-01	6.55E-01 7.29E-01			6.55E-01 7.34E-01	6.37E-01 6.68E-01	5.96E-01 6.26E-01

Note: Based on firing natural gas and distillate oil for 8470 and 300 hours, respectively. Total emissions include emissions from the combustion turbine and duct burner.

Table 12. Comparison of Maximum Emissions for Additional Non-Regulated Pollutant for Tiger Bay Facility-Permit Application for GE and Westinghouse Turbines and Revised Westinghouse Data, Base Load

Pollutant		Maxim	um Emissi	ons	Maximum Emissions			Maximum Emissions		
		27 oF		72 oF 97 oF		72 oF	72 of 97 of	27 oF 72 o	72 oF	97 oF
Antimony	,									
	lb/hr TPY		3.59E-02 5.38E-03			3.36E-02 5.03E-03			3.39E-02 5.09E-03	
Barium										•
	lb/hr		3.21E-02			3.00E-02			3.03E-02	
	TPY	5.42E-03	4.81E-03	4.44E-03	4.67E-03	4.50E-03	4.20E-03	4.67E-03	4.54E-03	4.25E-03
Cobalt										
	lb/hr	1.68E-02	1.49E-02	1.38E-02	1.45E-02	1.39E-02	1.30E-02	1.45E-02	1.41E-02	1.31E-02
	TPY	2.51E-03	2.23E-03	2.06E-03	2.17E-03	2.09E-03	1.95E-03	2.17E-03	2.11E-03	1.97E-03
2 inc										
<b>E</b> 1110	lb/hr	1.26E+00	1.12E+00	1.04E+00	1.09E+00	1.05E+00	9.80E-01	1.09E+00	1.06E+00	9.91E-01
	TPY	1.90E-01	1.68E-01	1.56E-01	1.64E-01	1.57E-01	1.47E-01	1.64E-01	1.59E-01	1.49E-01
Chlorine										
	(b/hr	4.99E-02	4.43E-02	4.09E-02	4.41E-02	4.24E-02	3.96E-02	4.32E-02	4.21E-02	3.93E-02
	TPY	7.48E-03	6.64E-03	6.14E-03	6.61E-03	6.37E-03	5.94E-03	6.49E-03	6.31E-03	5.89E-03

Note: Based on firing natural gas and distillate oil for 8470 and 300 hours, respectively. Total emissions include emissions from the combustion turbine and duct burner.



August 26, 1992

Mr. Clair H. Fancy, Chief
Bureau of Air Regulation
Florida Department of Environmental Regulation
Twin Towers Office Building
2600 Blair Stone Road
Taliahassee, FL 32399-2400

RECEIVED

AUG 27 1992

Division of Air Resources Management

Re: Central Florida Power Limited Partnership

Tiger Bay (formerly Central Florida) cogeneration plant

PSD-FL-190 AC 53-214903

Dear Mr. Fancy:

This correspondence presents the information requested by the Department's July 14, 1992, letter. The responses have been prepared based on phone conversations held on July 15, 1992, with Mr. Mirza Baig, and subsequent discussions held with Mr. Cleve Holladay and Mr. John Glunn.

1. COMMENT: Section 1-1 states the electrical output of the cogeneration facility is 206 MW. The gas turbine (GT) is rated at 147 MW and the duct burner is rated at 74 MW, giving a total of 221 MW. What is the maximum electrical output you would like to be permitted for this facility?

RESPONSE: The maximum electrical output of the cogeneration facility is 258 MW (GE machine) and 246 MW (Westinghouse machine), based on the following conditions: fuel oil firing and an ambient temperature of 27°F. The breakdown of the maximum electrical output for both machines for fuel oil is as follows:

•	Maximum Rated Electrical Output (MW)					
Fuel/Unit	GE	Westinghouse				
Combustion Turbine	184	172				
Steam Turbine	74	74				

2. COMMENT: According to Section 1-1, two types of advanced GTs are being considered for this project. The Department must know the exact type of gas turbine you propose to install so that a BACT determination can be made. Accordingly, please submit detailed information of the unit selected. We will also need any available stack test data for that unit.



RESPONSE: The combustion turbine for the project has not been selected. The candidate turbines are currently being evaluated for performance and commercial terms. The air construction application for the project was based on the advanced class of turbines, and performance and emissions are similar for the two turbines under consideration. The information on both turbines is presented in Attachment 1. The information presented in the application was based on performance and emissions characteristics that enveloped these two turbines. Since the performance and emission characteristics are similar for the turbines under consideration, a decision regarding BACT would not be substantially different regardless of which turbine was selected. A similar decision was made by the Department in the BACT determination for the Hardee Power Station. In that project, four combustion turbines were proposed by the applicant, with the Department's BACT determination made on an envelope of performance and emission characteristics.

3. COMMENT: What is the maximum sulfur content of the natural gas you propose to burn? Provide a copy of any sulfur content guarantee that you may have from the supplier.

RESPONSE: The maximum sulfur content of the natural gas proposed in the application was 1 grain of sulfur per 100 cubic feet (1 gr/100 cf). This was based on an evaluation of 9 months of sulfur content data supplied by Florida Gas Transmission (FGT). FGT is the only supplier of pipeline natural gas in Florida. The results of the evaluation are presented in Table 1. As shown in this table, the average sulfur content of natural gas was 0.43 gr/100 cf. A 130 percent contingency was used to develop the proposed emission rate of 1 gr/100 cf from the average sulfur content of 0.43 gr/100 cf reported by FGT in natural gas and would statistically account for potentially higher sulfur contents. Sulfur content information supplied by FGT for four sample analyses performed in April and May 1992 indicated a maximum sulfur content of 0.4 gr/100 cf which is within the previously supplied data (see Attachment 2).

There is no guaranteed sulfur content for natural gas that is supplied by FGT.

4. COMMENT: Submit an updated process flow diagram showing steam turbine and volumetric air flow rates.

RESPONSE: Updated process flow diagrams showing the steam turbine and the mass energy balance around the steam turbine and gas turbine are presented in Attachment 3 for natural gas and fuel oil firing.

5. COMMENT: In Section 4-12, Table 4-2, the emissions (25 ppmvd) for advance GT with dry low-NO<sub>x</sub> technology appears to be incorrect. Also, Table 4-2 should state the turbine size on which these figures are based.

RESPONSE: The 25 ppmvd listed for the dry low-NO<sub>x</sub> technology in both the conventional and advanced machines is correct. This is the actual level that would be emitted from each machine. The 22.5 ppmvd listed on page 4-11 of the report is for the advanced machine when the emission rate is adjusted based on the same amount of generation (i.e., megawatthours) as a conventional gas turbine. As described in the preceding paragraph, the advanced



machine is more efficient and will result in lower NO<sub>x</sub> emissions for each megawatt generated. This comparison would be analogous to the amount of particulate per ton of clinker produced by a cement plant.

The sizes of the turbines in Table 4-2 are: conventional--82 MW gas and 84 MW oil; advanced--147.1 MW gas and 159.2 MW oil [for GE PG7221(FA) machine at ambient temperature of 72 °F].

6. COMMENT: Submit all emission calculations and not just an example calculation. These emission calculations shall be based on the selected turbine for this project.

RESPONSE: The detailed emission calculations for the turbine proposed for this project are presented in Attachment 4 to this letter.

7. COMMENT: What is the expected maximum ambient concentrations for the metals emitted?

RESPONSE: The expected maximum ambient concentrations for toxic air pollutants, including metals, are presented in Table 7-5, page 7-9, in the PSD analysis that supports the air construction permit application. Based on the results presented in the table, the highest predicted impacts were below the no-threat levels for all pollutants and averaging times.

8. COMMENT: Please provide an air quality related analysis (AQRV) of the impact this project will have on the Chassahowitzka National Wilderness Area (CNWA) for the pollutant NO<sub>2</sub>. The AQRV analysis includes impacts to soil, vegetation, and wildlife. This analysis also includes an assessment of impacts to the aquatic environment. Since the modeling information already provided with this application shows that the predicted NO<sub>2</sub> impact at the CNWA Class I area is less than the National Park Service (NPS) recommended significance level, the NPS has verbally stated that only a literature review is needed in order to comply with the AQRV analysis requirement.

RESPONSE: KBN has performed air quality analyses to determine the Prevention of Significant Deterioration (PSD) Class I increment consumption and Air Quality Related Values (AQRV) Analyses for the Chassahowitzka National Wilderness Area (NWA) due to emissions from the Tiger Bay cogeneration facility. The facility is located approximately 120 km from the closest part of the Chassahowitzka National Wilderness Area (NWA), a PSD Class I area. The proposed facility alone had a maximum predicted annual average nitrogen dioxide (NO<sub>2</sub>) impact of 0.014  $\mu$ g/m³, which is less than the National Park Service (NPS) significant impact level of 0.025  $\mu$ g/m³.

Based on verbal communications between the Florida Department of Environmental Regulation (FDER) and NPS, the AQRV analyses for the PSD Class I area of the Chassahowitzka NWA need only address the impacts of increased NO<sub>2</sub> emissions for this project.

The Chassahowitzka NWA is characterized by vegetation which includes flatwoods, brackishwater, marine, and halophytic terrestrial species. Predominant tree species are slash pine,



laurel oak, sweetgum, and palm. Other plants in the preserve include needlegrass rush, seashore saltgrass, marsh hay, and red mangrove. NO<sub>2</sub> concentrations can injure plant tissue with symptoms usually appearing as irregular white to brown collapsed lesions between the leaf veins and near the margins. Conversely, non-injurious levels of NO<sub>2</sub> can be absorbed by plants, enzymatically transformed into ammonia, and incorporated into plant constituents such as amino acids (Matsumaru et al., 1979).

Plant damage can occur through either acute (short-term, high concentration) or chronic (long-term, relatively low concentration) exposure. For plants that have been determined to be more sensitive to  $NO_2$  exposure than others, acute (1, 4, 8 hours) exposure caused 5 percent predicted foliar injury at concentrations ranging from 3,800 to 15,000  $\mu$ g/m³ (Heck and Tingey, 1979). Chronic exposure of selected plants (some considered  $NO_2$ -sensitive) to  $NO_2$  concentrations of 2,000 to 4,000  $\mu$ g/m³ for 213 to 1,900 hours caused reductions in yield of up to 37 percent and some chlorosis (Zahn, 1975).

By comparison of published toxicity values for NO<sub>2</sub> exposure to short-term (i.e., 1-, 3-, and 8-hour averaging times) and long-term (annual averaging time) modeled concentrations, the possibility of plant damage in the preserve can be examined for both acute and chronic exposure situations, respectively. The 1-, 3-, and 8-hour estimated NO<sub>2</sub> concentrations at the point of maximum impact are 3.65, 2.14, and 1.00  $\mu$ g/m<sup>3</sup>, respectively. These concentrations are approximately 6.7 x 10<sup>-5</sup> to 9.6 x 10<sup>-4</sup> of the levels that could potentially injure 5 percent of the plant foliage. For a chronic exposure, the annual estimated NO<sub>2</sub> concentration at the point of maximum impact in the preserve (0.014  $\mu$ g/m<sup>3</sup>) is 3.5 x 10<sup>-6</sup> to 7.0 x 10<sup>-6</sup> of the levels that caused minimal yield loss and chlorosis in plant tissue.

The majority of the soil in the Class I area is classified as Weekiwachee--Durbin muck. This is an euic, hyperthermic typic sufihemist that is characterized by high levels of sulfur and organic matter. This soil is flooded daily with the advent of high tide, and the pH ranges between 6.1 and 7.8. The upper level of this soil may contain as much as 4 percent sulfur (USDA, 1991).

The greatest threat to soils from increased NO<sub>2</sub> deposition is a decrease in pH or an increase of sulfur to levels considered unnatural or potentially toxic. Although ground deposition was not calculated, it is evident that the amount of NO<sub>2</sub> deposited would be inconsequential in light of the inherent sulfur content. The regular flooding of these soils by the Gulf of Mexico regulates the pH, and any rise in acidity in the soil would be buffered by this activity.

The predicted NO<sub>2</sub> concentrations are well below the lowest observed effects levels in animals (Newman and Schreiber, 1988). Given these conditions, the proposed source's emissions pose no risk to wildlife. Because predicted levels are below those known to cause effects to vegetation, there is also no risk.



#### References

Heck, W.W. and D.T. Tingey. 1979. Nitrogen Dioxide: Time-Concentration Model to Predict Acute Foliar Injury. EPA-600/3-79-057, U.S. Environmental Protection Agency, Corvallis, OR.

Matsumaru, T., T. Yoneyama, T. Totsuka, and K. Shiratori. 1979. Absorption of Atmospheric NO<sub>2</sub> by Plants and Soils. Soil Sci. Plant Nutr. 25:255-265.

Newman, J.R. and Schreiber. 1988. Air Pollution and Wildlife Toxicology. Environmental Toxicology and Chemistry 7:381-390.

U.S. Department of Agriculture. 1991. Surveys of Hernando and Citrus Counties, Florida. USDA Soil Conservation Service in cooperation with University of Florida, Institute of Food and Agricultural Sciences, Agricultural Experiment Stations, and Soil Science Department.

Zahn, R. 1975. Gassing Experiments with NO<sub>2</sub> in Small Greenhouses. Staub Reinhalt. Luft 35:194-196.

9. COMMENT: Section 4.3.1.2, page 4-10, states that "While the increased firing temperature increases the thermal NO<sub>x</sub> generated, this NO<sub>x</sub> increase is controlled through combustion design." How much additional thermal NO<sub>x</sub> is generated due to higher temperature?

RESPONSE: The increased thermal NO<sub>x</sub> emissions, due to the higher firing temperature of the advanced combustion turbine, is about 20 percent higher than a conventional turbine when firing natural gas (from Table 4-2, 150 ppmvd, conventional, compared to 179 ppmvd, advanced) and about 13 percent higher than a conventional turbine when firing oil (from Table 4-2, 245 ppmvd, conventional, compared to 276 ppmvd, advanced).

10. COMMENT: On page 4-3, the estimated cost of SCR is reported to be about \$7,400 per ton of NO<sub>x</sub> removed and it exceeds \$10,000 per ton of pollutant removed when the net emissions of all pollutants (exclusive of CO<sub>2</sub>) are considered. Provide us with the names and addresses of all manufacturers that were contacted while developing capital and annualized cost estimates for this project.

RESPONSE: The cost for SCR was obtained from a database developed by KBN from this and other projects. The manufacturers contacted were:

Steuler International Corporation P.O. Box 38 Mertztown, PA 19539-0038 215-682-7171

Hitachi Zosen U.S.A. Ltd. 150 East 52 nd Street New York, NY 10022 212-355-5650



Mitsubishi International Corporation 2 Houston Center, Suite 3800 Houston, TX 77010 713-652-9200

W. R. Grace & Co. P.O. Box 2117 Baltimore, MD 21203-2117 410-659-9000

Norton Company P.O. Box 350 Arkon, OH 44309-0350 216-673-5860

11. COMMENT (via July 15, 1992, telephone conversation): Provide a large-scale site plan similar to Figure 2-2 of the air permit application.

**RESPONSE**: A full-scale revised plot plan is included in Attachment 5.

12. COMMENT (via July 15, 1992, telephone conversation): Please provide a diagram indicating the proposed location of the sample ports for source sampling purposes. Show these locations with respect to the proposed stack and HRSG unit.

RESPONSE: The stack sample port location is depicted in Figure 1. The sample port will be accessible by ladder from the top of the HRSG to a platform assembly near the port location.

Submittal of this information should clarify all questions raised by the Department in the completeness determination for this project. Please call me at 904-331-9000 if there are any further questions on the material submitted.

Sincerely,

Cobut C. Mc Caun In Kennard F. Kosky, P.E.

President

Enclosures KFK/dmm

cc: Mirza Baig, FDER

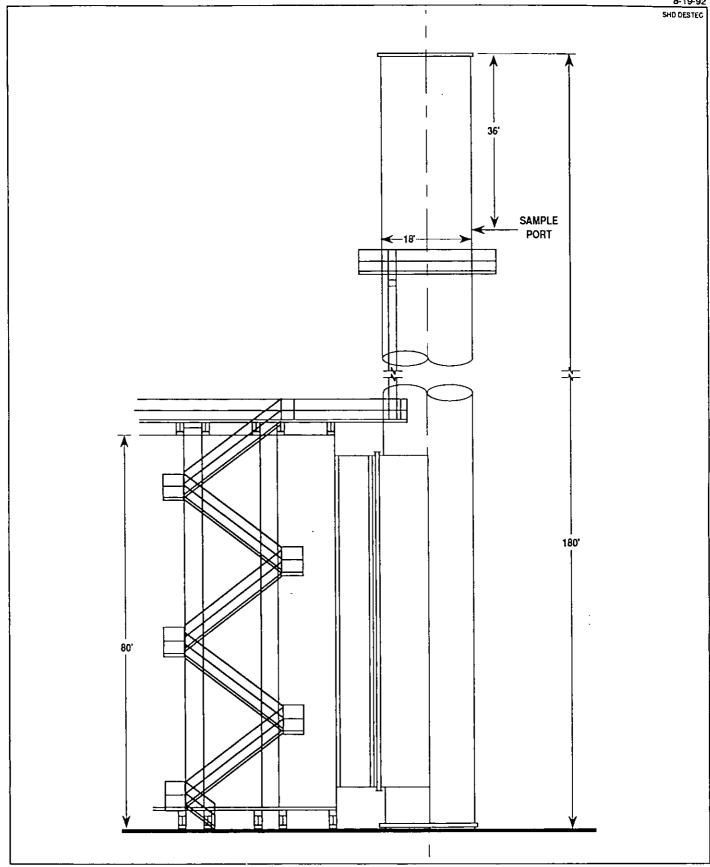
Robert I. Taylor, Central Florida Power, L.P. Robert Chatham, Destec Engineering, Inc.

File (2)

Table 1. Sulfur Content, Heat Content, and SO<sub>2</sub> Emission Factors for Natural Gas

Date	Sulfur Content (gr/100 cf)	Heat Content (Btu)	SO <sub>2</sub> Emission Factor (lb/10 <sup>6</sup> Btu)	SO <sub>2</sub> Emission Factor (lb/10 <sup>6</sup> cf)
2/6/90	0.30	1,031	0.00083	0.857
2/13/90	0.05	1,028	0.00014	0.143
2/20/90	0.35	1,025	0.00098	1.000
2/27/90	0.45	1,024	0.00126	1.286
3/6/90	0.45	1,025	0.00125	1.286
3/13/90	0.30	1,026	0.00084	0.857
3/20/90	0.35	1,026	0.00097	1.000
3/27/90	0.35	1,025	0.00098	1.000
4/3/90	0.60	1,026	0.00167	1.714
4/10/90	0.25	1,022	0.00070	0.714
4/17/90	0.40	1,026	0.00111	1.143
4/24/90	0.30	1,022	0.00084	0.857
5/1/90	0.40	1,020	0.00112	1.143
5/8/90	0.25	1,034	0.00069	0.714
5/15/90	0.20	1,023	0.00056	0.571
6/5/90	0.45	1,020	0.00126	1.286
6/12/90	0.40	1,018	0.00112	1.143
6/19/90	0.70	1,017	0.00197	2.000
6/26/90	0.45	1,019	0.00126	1.286
7/3/90	0.55	1,022	0.00154	1.571
7/10/90	0.35	1,022	0.00098	1.000
7/17/90	0.45	1,021	0.00126	1.286
7/30/90	0.30	1,021	0.00084	0.857
8/7/90	0.50	1,024	0.00140	1.429
8/14/90	0.45	1,022	0.00126	1.286
8/21/90	0.40	1,022	0.00112	1.143
8/28/90	0.70	1,022	0.00196	2.000
9/4/90	0.55	1,029	0.00153	1.571
9/11/90	0.40	1,025	0.00111	1.143
9/18/90	0.45	1,026	0.00125	1.286
9/25/90	0.40	1,026	0.00111	1,143
10/2/90	0.45	1,029	0.00125	1.286
10/9/90	0.45	1,025	0.00125	1.286
10/16/90	0.70	1,028	0.00195	2.000
10/28/90	0.80	1,024	0.00223	2.286
Average:	0.43	1,024	0.00119	1.216
Maximum:	0.80	1,034	0.00223	2.286
Minimum:	0.05	1,017	0.00014	0.143
Std. Dev.	0.15	4	0.00042	0.427

Source: Florida Gas Transmission Company, 1990.



TIGER BAY CONCEPTUAL DRAWING OF STACK AND ADJOINING STRUCTURE Figure 1



#### **ATTACHMENT 1**

# MANUFACTURER'S DESIGN SPECIFICATIONS FOR THE COMBUSTION TURBINE



LOAD CONDITION	•		BASE	90%	80%	70%	60%
AMBIENT TEMP.		-Deg F.	27	27	27	27	
OUTPUT			170700.	153200.	135300.	119900.	27
HEAT RATE (LHV)		- Btu/kWh		9770.	10240.	10770.	101400.
HEAT CONS. (LHV)	X10-6	- Btu/h	1614.8	1496.8	1385.5		11600.
EXHAUST FLOW	X10-3	– lb/h	3582.0	3228.0		1291.3	1176.2
EXHAUST TEMP	*****	- Deg F.	1078.		2958.0	2744.0	2521.0
EXHAUST ENERGY	Y10 6	- Btu/h	976.4	1118.	1150.	1177.	1200.
S.III IOOT ENEROT	V10-0	- Biwii	970.4	922.1	875.5	836.9	788.6
NOX	nomud	@ 15% O2	26	٥٥	0.5		
NOX AS NO2	- lb/h	@ 13% UZ	25.	25.	25.	25.	25.
CO	-•		162	149.	138.	128.	116.
	- ppmvd		15.	*	*	*	*
CO	– lb/h		49.	*	*	*	*
UHC	- ppmvw	•	7.	*	*	*	*
UHC	– lb/h		14.	* .	*	*	*
VOC	- ppmvw	•	1.4	*	*	*	*
VOC	lb/h		2.8	*	*	*	*
PART	– Ib/h		9.0	9.0	9.0	9.0	9.0
EXHAUST ANALYS	IS % VC	)L.					
ARGON	- <b>- -</b>		0.90	0.90	0.90	0.00	0.00
NITROGEN			75.04			0.90	0.90
OXYGEN				74.97	74.95	74.95	74.98
CARBON DIOXIDE			12.71	12.52	12.46	12.46	12.56
WATER			3.74	3.83	3.85	3.85	3.81
WAIEK			7.61	7.78	7.84	7.84	7.75
SITE CONDITIONS	•						
ELEVATION		_ fr	160				

T VALIUN 160 SITE PRESSURE 14.62 - psia INLET LOSS - in. Water 4 **EXHAUST LOSS** - in. Water 12 RELATIVE HUMIDITY - % 40 FUEL TYPE **METHANE FUEL LHV** - Btu/lb 21515

**APPLICATION** 317S HYDROGEN COOLED GENERATOR

COMBUSTION SYSTEM DRY LOW NOX II

EMISSION INFORMATION BASED ON GE RECOMMENDED MEASUREMENT METHODS. NOx EMISSIONS ARE CORRECTED TO 15% O2 WITHOUT HEAT RATE CORRECTION AND ARE NOT CORRECTED TO ISO REFERENCE CONDITIONS PER 40CFR 60.335(a)(1)(i). NOx LEVELS SHOWN WILL BE CONTROLLED BY ALGORITHMS WITHIN THE SPEEDTRONIC CONTROL SYSTEM. COMPRESSOR BLEED HEAT IS USED FOR 70% AND 60% PART LOAD OPERATION. APPROXIMATELY 10% OF THE VOC'S ARE NON-METHANE AND ETHANE.

\* DATA NOT AVAILABLE

IPS-8707 JPT 3/19/92

> Subject page NO TAGI Proposal **DESTECS**



LOAD CONDITION AMBIENT TEMP. OUTPUT HEAT RATE (LHV) HEAT CONS. (LHV) X10-6 EXHAUST FLOW X10-3 EXHAUST TEMP EXHAUST ENERGY X10-6	BASE - Deg F 64 - kW 151900 Btu/kWh 9750 Btu/h 1481 lb/h 3322 Deg F 1110 Btu/h 911.	0 3010.0 1145.	80% 64 124400. 10340. 1286.3 2810.0 1168. 816.8	70% 64 106500. 11070. 1179.0 2595.0 1195. 773.9	60% 64 89900. 11860. 1066.2 2413.0 1200. 721.3
NOX         - ppmvd           NOX AS NO2         - lb/h           CO         - ppmvd           CO         - lb/h           UHC         - ppmvd           UHC         - lb/h           VOC         - ppmvd           VOC         - lb/h           PART         - lb/h	45. v 7. 13.	* 4 * 6 *	25. 129. * * * * * * * * *	25. 118. * * * * * * *	25. 107. * * * * * * *
EXHAUST ANALYSIS % VO ARGON NITROGEN OXYGEN CARBON DIOXIDE WATER	0.1 74.1 12.1	04 73.98 56 12.41 68 3.75	0.88 73.97 12.35 3.78 9.02	0.88 73.98 12.41 3.75 8.98	0.89 74.05 12.62 3.65 8.79
SITE CONDITIONS ELEVATION SITE PRESSURE INLET LOSS EXHAUST LOSS RELATIVE HUMIDITY FUEL TYPE FUEL LHV APPLICATION	- ft 160 - psia 14.6 - in. Water 4 - in. Water 12 - % 78 - METHAN - Btu/lb 21515 - 3178 HYI		ED GENERA	TOR	

EMISSION INFORMATION BASED ON GE RECOMMENDED MEASUREMENT METHODS. NOX EMISSIONS ARE CORRECTED TO 15% O2 WITHOUT HEAT RATE CORRECTION AND ARE NOT CORRECTED TO ISO REFERENCE CONDITIONS PER 40CFR 60.335(a)(1)(i). NOX LEVELS SHOWN WILL BE CONTROLLED BY ALGORITHMS WITHIN THE SPEEDTRONIC CONTROL SYSTEM.

DRY LOW NOX II

COMPRESSOR BLEED HEAT IS USED FOR 70% AND 60% PART LOAD OPERATION. APPROXIMATELY 10% OF THE VOC'S ARE NON-METHANE AND ETHANE.

\* DATA NOT AVAILABLE

COMBUSTION SYSTEM

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Subject		page NO TAGI			
Proposal	DECTECA				



LOAD CONDITION AMBIENT TEMP. OUTPUT HEAT RATE (LHV) HEAT CONS. (LHV) X EXHAUST FLOW X EXHAUST TEMP EXHAUST ENERGY	(10–6 (10–3	- Deg F - kW - Btu/kW - Btu/h - lb/h - Deg F. - Btu/h	147100.	90% 72 131800. 10210. 1345.7 2960.0 1151. 849.0	80% 72 120500. 10550. 1271.3 2768.0 1173. 815.5	70% 72 103100. 11340. 1169.2 2560.0 1199. 776.0	60 % 72 86800. 12220. 1060.7 2383.0 1200. 726.5
NOX AS NO2 - CO - UHC - UHC - VOC - VOC -	- ppmvd ( - lb/h - ppmvd - lb/h - ppmvw - lb/h - ppmvw - lb/h - lb/h		2 25. 145 15. 44. 7. 13. 1.4 2.6 9.0	25. 134. * * * * * * * 9.0	25. 126. * * * * * * 9.0	25. 116. * * * * * * * *	25. 105. * * * * * * * 9.0
EXHAUST ANALYSI ARGON NITROGEN OXYGEN CARBON DIOXIDE WATER	IS % VC	DL.	0.89 73.73 12.51 3.66 9.21	0.88 73.68 12.37 3.73 9.34	0.89 73.67 12.32 3.75 9.38	0.87 73.68 12.39 3.72 9.34	0.88 73.76 12.63 3.61 9.12
SITE CONDITIONS ELEVATION SITE PRESSURE INLET LOSS EXHAUST LOSS RELATIVE HUMIDIT FUEL TYPE FUEL LHV APPLICATION COMBUSTION SYST		Btu/lb	er 12 75 METHANE 21515		ED GENERA	ATOR	

EMISSION INFORMATION BASED ON GE RECOMMENDED MEASUREMENT METHODS. NOx EMISSIONS ARE CORRECTED TO 15% O2 WITHOUT HEAT RATE CORRECTION AND ARE NOT CORRECTED TO ISO REFERENCE CONDITIONS PER 40CFR 60.335(a)(1)(i). NOx LEVELS SHOWN WILL BE CONTROLLED BY ALGORITHMS WITHIN THE SPEEDTRONIC CONTROL SYSTEM. COMPRESSOR BLEED HEAT IS USED FOR 70% AND 60% PART LOAD OPERATION.

APPROXIMATELY 10% OF THE VOC'S ARE NON-METHANE AND ETHANE.

\* DATA NOT AVAILABLE IPS-8707

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Proposal DESTECS



LOAD CONDITION AMBIENT TEMP. OUTPUT HEAT RATE (LHV) HEAT CONS. (LHV) X10- EXHAUST FLOW X10- EXHAUST TEMP EXHAUST ENERGY X10	Btu/kWh 6 Btu/h 3 lb/h Deg F.	BASE 79 142700. 9970. 1422.7 3202.0 1124. 886.3	90% 79 127900. 10330. 1321.2 2910.0 1157. 838.6	80% 79 116500. 10700. 1246.6 2725.0 1179. 805.2	70% 79 99500. 11510. 1145.2 2524.0 1200. 765.1	60 % 79 83900. 12390. 1039.5 2352.0 1200. 715.8
NOX — ppr NOX AS NO2 — lb/l CO — ppr CO — lb/l UHC — ppr UHC — lb/l VOC — ppr VOC — lb/l PART — lb/l	mvd h mvw h mvw h	25. 143 15. 43. 7. 13. 1.4 2.6 9.0	25. 132. * * * * * * * *	25. 124. * * * * * * * *	25. 114. * * * * * * 9.0	25. 103. * * * * * * * *
EXHAUST ANALYSIS % ARGON NITROGEN OXYGEN CARBON DIOXIDE WATER	6 VOL.	0.87 73.07 12.36 3.65 10.05	0.88 73.02 12.22 3.71 10.17	0.87 73.01 12.19 3.73 10.20	0.88 73.02 12.28 3.68 10.14	0.87 73.10 12.52 3.58 9.93
SITE CONDITIONS ELEVATION SITE PRESSURE INLET LOSS EXHAUST LOSS RELATIVE HUMIDITY FUEL TYPE FUEL LHV APPLICATION COMBUSTION SYSTEM	– Вш/lb – 3	r 12 86 METHANE 21515		ED GENERA	TOR	

EMISSION INFORMATION BASED ON GE RECOMMENDED MEASUREMENT METHODS. NOx EMISSIONS ARE CORRECTED TO 15% O2 WITHOUT HEAT RATE CORRECTION AND ARE NOT CORRECTED TO ISO REFERENCE CONDITIONS PER 40CFR 60.335(a)(1)(i). NOx LEVELS SHOWN WILL BE CONTROLLED BY ALGORITHMS WITHIN THE SPEEDTRONIC CONTROL SYSTEM.

COMPRESSOR BLEED HEAT IS USED FOR 70 AND 60% PART LOAD OPERATION APPROXIMATELY 10% OF THE VOC'S ARE NON-METHANE AND ETHANE.

\* DATA NOT AVAILABLE

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Proposal	DESTEC2		-



LOAD CONDITION	t		BASE	90%	80%	70%	60%
AMBIENT TEMP.		- Deg F.	97 <sup>1</sup>	97	97	97	97
OUTPUT			131800.	118400.	106800.	90900.	77100.
HEAT RATE (LHV)		- Btu/kWh	10230.	10600.	11070.	11890.	12780.
HEAT CONS. (LHV)	X10-6	– Btu/h	1348.3	1255.0	1182.3	1080.8	985.3
EXHAUST FLOW	X10-3	– lb/h	3077.0	2808.0	2640.0	2454.0	2293.0
EXHAUST TEMP		- Deg F.	1140.	1170.	1190.	1200.	1200.
EXHAUST ENERGY	X10-6	– Btu/h	851.5	807.0	776.1	732.0	686.5
NOX	– nomyd	@ 15% 02	25.	26	05	05	
NOX AS NO2	- lb/h	@ 15% OZ	135	25. 125.	25.	25.	25.
CO	– ppmvd		15.	123.	118.	107.	97.
co	– lb/h		41.	*	*	*	*
UHC	– ppmvw	,	7.	*	*	*	*
UHC	– lb/h		12.	*	*	*	*
VOC	– ppmvw	•	1.4	*	*	*	
VOC	– ppinvw – lb/h		2.4	*	*	*	*
PART	– 10/11 – 1b/h						*
174(1	- 10/11		9.0	9.0	9.0	9.0	9.0
EXHAUST ANALYS	SIS % VC	)L.					
ARGON			0.88	0.87	0.87	0.88	0.89
NITROGEN			73.13	73.09	73.10	73.13	73.20
OXYGEN			12.48	12.36	12.37	12.52	12.74
CARBON DIOXIDE			3.60	3.66	3.65	3.58	3.48
WATER			9.91	10.02	10.01	9.89	9.70
SITE CONDITIONS							
ELEVATION		− ft∟	160				
SITE PRESSURE		neio	14.62				

SITE PRESSURE – psia 14.62 INLET LOSS - in. Water 4 EXHAUST LOSS - in. Water 12 RELATIVE HUMIDITY - % 48 FUEL TYPE **METHANE** FUEL LHV – Btu/lb 21515

APPLICATION – 317S HYDROGEN COOLED GENERATOR

COMBUSTION SYSTEM - DRY LOW NOX II

EMISSION INFORMATION BASED ON GE RECOMMENDED MEASUREMENT METHODS. NOx EMISSIONS ARE CORRECTED TO 15% O2 WITHOUT HEAT RATE CORRECTION AND ARE NOT CORRECTED TO ISO REFERENCE CONDITIONS PER 40CFR 60.335(a)(1)(i). NOx LEVELS SHOWN WILL BE CONTROLLED BY ALGORITHMS WITHIN THE SPEEDTRONIC CONTROL SYSTEM.

COMPRESSOR BLEED HEAT IS USED FOR 70% AND 60% PART LOAD OPERATION. APPROXIMATELY 10% OF THE VOC'S ARE NON-METHANE AND ETHANE.

\* DATA NOT AVAILABLE

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Subject		page	NO TAGI
Proposal	DESTEC1		

05/06/1992 14:36 FROM GE-TURBINE TECHNOLOGY DPT TO DESTEC - GATOR COCKN \*\*\*\*\*

#### ESTINATED PERFORMANCE - PG7221(FA)

LOAD CONDITION  AMBIENT TEMP Deg F. OUTPUT - kV  HEAT RATE (LEV) - Btu/kVh  HEAT CONS. (LEV) X10-6 - Btu/kVh  EXHAUST FLOV X10-3 - lb/h  EXHAUST TEMP EXHAUST HEAT X10-6 - Btu/h  VATER FLOV - lb/h	BASE 27 183700. 10070. 10674. 1849.9 3743.0 1060. 1021.8 135390.	70x 27 129200. 11430. 12115. 1476.8 2837.0 1166. 876.8 105120.
### Description of the column	42. 327. 30. 98. 7- 15. 3.5 7.5 11. 95. 10. 17.0	42. 258. * * * * * 12. 76. 1. 5. 8. 17.0
ARGON NITROGEN	0.86 71.27	

#### SITE CONDITIONS <del>^^^</del>

CARBON

OXYGEN

DIOXIDE

\_ ft. BLEVATION 160 STIE PRESSURE peia in. Vater 14.62 INLET LOSS EXBAUST LOSS in. Vater RRIATIVE HUMIDITY PUBL TYPE PUBL LEV 18550 Btu/lb APPLICATION 317S HYDROGEN COOLED GENERATOR DRY LOW NOK II COMBUSTION SISTEM

SULFUR ENISSIONS ARE BASED ON A TOTAL FUEL SULFUR CONTENT OF 0.0.

EMISSION INFORMATION BASED ON GE RECOMMENDED MEASUREMENT METHODS. NOW EMISSIONS ARE CORRECTED TO 15% 02 VITEOUT HEAT RATE CORRECTION AND ARE NOT CORRECTED TO ISO REFERENCE CONDITIONS PER 40CFR 60.335(a)(1)(i). NOX LEVELS SHOWN WILL BE CONTROLLED BY ALCORITHMS WITHIN THE SPEEDIRONIC CONTROL SYSTEM. DISTILLATE FUBL IS ASSUMED TO HAVE .015% FUEL BOUND NITROGEN, OR LESS. FRN ANOUNTS: GREATER THAN .015% WILL ADD TO THE REPORTED NOW VALUE.

10.96

P. O. BOX 4411

ON SHIP TOWN AND THE SERVICE STATE OF THE LOAD OPERATION.

ENGINEERING

IPS\_8707 7/6/97



LOAD CONDITIO	N		BASE	70%
AMBIENT TEMP.		- Deg F.	72	72
OUTPUT		~ kW	159200.	111000,
HEAT RATE (LHV)	}	- BturkWh	10320.	11800,
HEAT CONS, (LHV	7 X10-6	Btu/h	1642.9	1309.8
EXHAUST FLOW	X10-3	lb/h	3390.0	2619.0
EXHAUST TEMP		- Dog F.	1102.	1192
<b>EXHAUST HEAT</b>	X10-6	– Buyh	932.2	801.6
WATER FLOW		lb/h	107070.	80490.
		-	10,010.	<del>40150</del> .
NOX	– comvd	I@ 15% O2	42,	42.
NOX AS NO2	Îb∕h	_	290,	229.
CO	- ppmvd	İ	30.	#.
CO	- lb/h		89.	*
UHC	- ppmvw	,	7.	
UHC	- lb/h		13.	
VOC	- ppmvw	i	3.5	*
VÕC	-lb/h		6 <u>.5</u>	*
PART	- lb/b		17.0	-
*****	XC# 13		17.0	17.0
EXHAUST ANALY	SIS % VC	)L.		
ARGON			0.86	0.86
NTTROGEN			70 <u>.5</u> 9	
OXYGEN			10.95	70,63
CARBON DIOXIDE			5.21	10.81
WATER				5.31
****			12,40	12.40

#### SITE CONDITIONS

COMMITTOM				
ELEVATION	- ft.		160	
STTE PRESSURE	– psia		14.62	
INLET LOSS	- in. Wa	iter	4	
	– in. Wa	ter	12	
RELATIVE HUMIDITY	- %		75	
	-	DIST	TLLATE	
				•
APPLICATION	-	<b>317S</b>	HYDROGEN COOK	ED GENERATOR
COMBUSTION SYSTEM	-	DRY	LOW NOX II	
	ELEVATION SITE PRESSURE INLET LOSS EXHAUST LOSS RELATIVE HUMIDITY FUEL TYPE FUEL LHY APPLICATION	ELEVATION - ft.  SITE PRESSURE - psia INLET LOSS - in. We EXHAUST LOSS - in. We EXHAUST LOSS - in. We FUEL TYPE - FUEL LHY - BUILD  APPLICATION -	ELEVATION - ft.  SITE PRESSURE - psia INLET LOSS - in. Water EXHAUST LOSS - in. Water EXHAUST LOSS - in. Water FUEL TYPE - DIST FUEL LHV - BUVID 18  APPLICATION - 317S	ELEVATION -ft. 160  SITE PRESSURE -psia 14.62  INLET LOSS -in. Water 4  EXHAUST LOSS -in. Water 12  RELATIVE HUMIDITY -% 75  FUEL TYPE - DISTILLATE  FUEL LHV -BIWID 18550  APPLICATION - 317S HYDROGEN COOK

EMISSION INFORMATION BASED ON GE RECOMMENDED MEASUREMENT METHODS. NOX EMISSIONS ARE CORRECTED TO 15% O2 WITHOUT HEAT RATE CORRECTION AND ARE NOT CORRECTED TO ISO REFERENCE CONDITIONS PER 40CFR 50.335(a)(1)(1). NOX LEVELS SHOWN WILL BE CONTROLLED BY ALGORITHMS WITHIN THE SPEEDTRONIC CONTROL SYSTEM. DISTILLATE FUEL IS ASSUMED TO HAVE 0.015% FUEL BOUND NITROGEN. OR LESS.

DISTILLATE FUEL IS ASSUMED TO HAVE 0.015% FUEL BOUND NITROGEN. OR LESS.
FUEL BOUND NITROGEN AMOUNTS GREATER THAN 0.015% WILL ADD TO THE REPORTED
NOX VALUE.

\* DATA NOT AVAILABLE

COMPRESSOR BLEED HEAT IS USED FOR PART LOAD OPERATION.

IPS~8707

JPT 4/14/92

Performance page 1

Proposal IPS-8707

TOP-2 TOTALISHINI LOUD 36, 91 846



LOAD CONDITIO	N		BASE	70%
AMBIENT TEMP.		Deg F.	97	97
OUTPUT		_ kW	142500.	98500.
HEAT RATE (LHV)	)	- But/kWh	10650.	12280.
HEAT CONS. (LHV		- Btu/h	1517.6	1209.6
EXHAUST FLOW	X10-3	– lb/h	. 3189.0	2510.0
EXHAUST TEMP	•	– Deg F.	1127.	1200;
EXHAUST HEAT	X10-6	- Btu∕h	881.7	758.7
WATER FLOW		Ib/h	92890.	68760.
NOX	– ppmvo	1@ 15% O2	42.	42.
NOX AS NO2	Ib/h	:	268.	211.
CO .	- ppmvt	1 ,	30.	*
CO	!b/h		83.	*
UHC	- ppmv1		7.	*
UHC	- 1b/h		13.	*
VOC	- ppmvv	su ·	3.5	*
VOC	- 16/h	,	6.5	· •
PART	– Ib∕iı		17.0	17.0
EXHAUST ANALY	ysis % v	OL.		
ARGON			0.85	0.85
NITROGEN			<i>7</i> 0.31	70.4 <del>9</del>
OXYGEN			11.03	11.07
CARBON DIOXID	E	•	5.11	5.11
WATER			12.71	12.48

#### SITE CONDITIONS

ELEVATION	iL	160
SITE PRESSURE	– psia	14.62
INLET LOSS	- in. Water	4
EXHAUST LOSS	- in. Water	12
RELATIVE HUMIDITY	- %	48
FUEL TYPE	- DIS	TILLATE
FUEL LHV	−Bm/lb	18550

APPLICATION - 317S HYDROGEN COOLED GENERATOR

COMBUSTION SYSTEM - DRY LOW NOX II

EMISSION INFORMATION BASED ON GE RECOMMENDED MEASUREMENT METHODS.
NOX EMISSIONS ARE CORRECTED TO 15% O2 WITHOUT HEAT RATE CORRECTION AND ARE
NOT CORRECTED TO ISO REFERENCE CONDITIONS PER 40CFR 60.335(a)(1)(i).
NOX LEVELS SHOWN WILL BE CONTROLLED BY ALGORITHMS WITHIN THE
SPEEDTRONIC CONTROL SYSTEM.
DISTILLATE FUEL IS ASSUMED TO HAVE 0.015% FUEL BOUND NITROGEN, OR LESS.

DISTILLALE FUEL IS ASSUMED TO HAVE 0.015% FUEL BOUND NITROGEN, OR LESS.
FUEL BOUND NITROGEN AMOUNTS GREATER THAN 0.015% WILL ADD TO THE REPORTED NOX VALUE.

\* DATA NOT AVAILABLE

COMPRESSOR BLEED HEAT IS USED FOR PART LOAD OPERATION. IPS-8707

IPS-8707 IPT 4/14/92

Performance

page 1

Proposal IPS-8707

DESTEC ENGINEERING ; 8-26-92;	13:45 ;	ŧu	713735	t	9043324 35254545 00000000000000000000000000000000	189
TO LOW NOX COMBUSTOR					Rev. 2	
PECTED SOIF COMBUSTION TURBINE PERFO	PAMANCE AND	EMISSIOI	NS		8/19/92	
TE CONDITIONS:						
UEL TYPE	GAS. BASE	GAS BASE	GAS BASE	gas Base	GAS BASE	
OAD LEVEL 'UEL HEATING VALUE, BTU/LB LHV	20900	20900	20900	20900	20900	
CUEL HEATING VALUE, BTU/LB HHV	23200	23200	23200	23200	23200	
MBIENT TEMPERATURE, F	27	64	72	9 25	97	
RELATIVE HUMIDITY	40	78	75	75	48	
SAROMETRIC PRESSURE, PSIA	14.015	14.015 3,7	14,615	14.615 3.5	14.615 3,4	
NLET PRESSURE LOSS, IN-WATER EXHAUST PRESSURE LOSS, IN-WATER	4.0 11.0	9.6	3.6 9.3	9.0	•	
NJEOTION FLUID	NONE	NONE	NONE	NONE	NONE	
NJECTION PATIO, LE/LB	. 0	0	0	0	0	
SENERATOR POWER FACTOR	0.85	0.85	0.85	0.65	0.85	
SENERATOR HYDROGEN PRESSURE, PSIA SENERATOR FRAME (97 X 114)	30	30	30	30	30	
OMBUSTION TURBINE PERFORMANCE:						
NET POWER OUTPUT, KW	169210	147950	143450	139560	129370	
HEAT RATE, BTU/KWH LHV	9490	9900	10000	10100	10350	
KEAT RATE, BYUKWH HHV	10530	10990	11100	11210	11500	
EXHAUST FLOW, LB/HR	3702540			3311770	3180510	•
SKHAUST TEMPEHATURE, F	1063	1086	1092	1098	1111	
TUEL FLOW, LB/HR	76830	70080	68640	67440	64130	
NJECTION RATE, LEVHR	4~	400	400	۰۵	400	
ALDRILIARY LOAD, KW HEAT INPUT, MMBTU/HR (LHV)	400 1606	400 1465	400 1435	400 1409	400 1840	
HEAT INPUT, MMBTUHR (HHV)	1782	1626	1592	1565	1488	
EXHAUST ENERGY, MMBTU/HR	1053,5	1004.8	994.1	985.4	959.0	
KHAUST GAS COMPOSITION (BY PCT VOL):						
OXYGEN	13.08	12.97	1291	12.82	12.54	
CARBON DIOXIDE	3.61	3.53	3.52	3.51	9.47	
WATER	7-26	8.45	6.82	9,32	9.56	
NITROGEN	75.00	74.11	73.61	73.41	79.20	
ARGON	0.94 28.50	0.93 28,36	0.93 28.32	0.92 28.26	0.92 28.23	
WOLECULAR WEIGHT	20.50	20,30	20.32	20.20	20.23	
MISSIONS						
√Ox, PPM√D @ 15% O2	25	25	25	25	25	
NOx, LEVHR	163	148	145	143	138	
OO, PPMVD	10 35	10	10	10	10	
CO, LB/HR	್ಷವ 1	32 1	31	31 1	29 1	
302, PPMVD 302, LB/HR	2	1	1	1	1	
rotal uhc, ppmvd	8		1 8	8	8	
TOTAL UHC, LEVHR	16	15	14	14	13	
VOC, PPMVD	4	4	4	4	4	
VOC, LB/HR	8	7	7	7	7	
PARTICULATES (PM10/TSP), LB/HR (TOTAL)	6.6	5.1	6.0	5.9	5.7	
SOOT, LEVHR	6.3	6,0	5.8	5.7	5.5	
ASH, LB/HR	0.0	0.0	0.0	0.0	0.0	
H2SO4 MIST, LB/HR	. 0.2	0.2	0.2	0.2	0,2	
202, PPMVD	40055	39729	39758	39894	39524	
DÓ2, LB/HR	212418	193677	189813	186588	177228	

i# 2

#### NOTE8:

[ RECEIVED 08/26 16:05 1992 AT 9043324189

<sup>1.</sup> The net power output is the power at the generator terminals minus turbine suxillary loads.

2. The fuel composition for natural gas is per oustomer's specification.

3. Exhaust energy is referenced to 400 degrees Rankins.

[ RECEIVED 08/26 16:09 1992 AT 9043324189 PAGE	SE 5 (PRI	INTED PAI	SE 5) 713735		8043324	189
SENT BY:DESTEC ENGINEERING : 8-26-92;  AUG-19-1992 11:08 FROM WESTINGHOUSE	13.40 1	TO			86264505	P.Ø5
DESTEC ENGINEERING - INGEN EAT PROJECT					711-269U	
. DRY LOW NOV COMPLISTOR					Rev. 2	
EXPECTED 501F COMBUSTION TURBINE PERFOR	MANCE AND	EMISSION	IS		8/19/92	
SITÉ CONDITIONS:						
*** T.P.C	GAS	GAS	GAS	GA3	GAS	
RUEL TYPE LOAD LEVEL	70%	70%	70%	70%	70%	
FUEL HEATING VALUE, BTU/LB LHV	20900	20900	20900	20900	20900	
FUEL HEATING VALUE, BTU/LB HHV	23200	23200	23200	23200	23200	
			=4	~^	^*	
AMBIENT TEMPERATURE. F	27	64 78	72 75	79 75	97 48	
RELATIVE HUMIDITY	40 14.615	14,815	14.615	14.615	14,615	
BAROMETRIC PRESSURE, PSIA	2.3	2.3	2.3	2.3	2.2	
INLET PRESSURE LOSS, IN-WATER EXHAUST PRESSURE LOSS, IN-WATER	5.7		5.9	5.8	5.5	
INJECTION FLUID	NONE	NONE	NONE	NONE	NONE	
INJECTION RATIO, LEALB	0	0	0	0	0	
GENERATOR POWER FACTOR	0.85	0.85	0,85	0.85	0.85	
GENERATOR HYDROGEN PRESSURE, PSIA	30	30	30	30	30	•
GENERATOR FRAME (97 X 114)						
			•			
COMBUSTION TURBINE PERFORMANCE:						
NET POWER OUTPUT, KW	118330	103390	100210	97490	90340	
HEAT RATE, BTU/KWH LHV	10490	11020	11150	11270	11600	
HEAT RATE, BTU/KWH HAV	11650	12230	12370	12510	12680	
EXHAUST FLOW, LEVHR	27\$4000			2619850		
EXHAUST TEMPERATURE, F	1130	1130	1130	1130	1130	
FUEL FLOW, LEYNA	59390	54520	53460	52570	50140	
INJECTION RATE, LB/HR	0	400	0	0	. O	
AUXILIARY LOAD, KW	400	400	400	400	400 1048	
HEAT INPUT, MMBTU/HR (LHV)	1241 1378	1139 1265	1117 1240	1099 1220	1163	
HEAT INPUT, MMBTU/HR (HHV) EXHAUST ENERGY, MMBTU/HR	834.4	816.3	808.4	801.9	782.8	
EXTMUST BIRTIST, MIMOTORIA	00-1	010.0	٠.٠٠	٠٠.٠	. 02.0	
EXHAUST GAS COMPOSITION (BY PCT VOL.):						
OXYGEN	13.04	13.10	13.09	13.04	13.15	
CARBON DIOXIDE	3.62	3.47	3.44	3,41	3.33	
WATER	7,30	6.32	83.8	9.12	9.29	
NITROGEN	75.08	74.16	73,87	73.50		
ARGON	0.94	0.93	0.93	0.92	0.92	
MOLECULAR WEIGHT	28.49	28,37	28.33	26.28	28,25	
EMISSIONS						
NOx, PPMVD @ 15% O2	25	25	25	25	25	
NOX, LB/HR	121	113	111	109	104	
CO, PPMVD	10	10	10	10	10	
CO, LB/HR	26	25	25	24	24	1.0
SO2, PPMVO	1	1	1	1	1	,
SO2, LB/HR	1	1	1	1	1	
TOTAL UHC, PPMVD	8	В	8	6	8	
TOTAL UHC, LB/HR	12	11	11	11	11	
VOC, PPMVD	4	4	4	4	4	
VOC, LEVHR	6	6	6	. 6	. 5	
PARTICULATES (PM10/TSP), LEVHR (TOTAL)	4.9	4.8	4.7	4.7	4.6	
SOOT, LB/HR	4.7	4,6	4.6	4.5	4.4	

0.0

0.2

40247

158710

<=10

0.0

0.2

39014

148643

<=10

0.0

0.2

38766

145662

<=10

0.0

0.2

38626

143145

<=10

0.0

0.2

37815

136547

<=10

:# 5

#### NOTES:

ASH, LB/HR

CO2, PPMVD CO2, LB/HR

OPACITY, %

H2SO4 MIST, LB/HR

<sup>1.</sup> The net power output is the power at the generator terminals minus. turbine auxiliary loads.

<sup>2.</sup> The fuel composition for natural gas is per customer's specication.3. Exhaust energy is referenced to 400 degrees Rankine.

<sup>4.</sup> Part loads are achieved by modulating igvs.

[ RECEIVED 0B/26 16:11 1992 AT 9043324189 PAGE 7 SENT BY:DESTEC ENGINEERING : 8-26-92 : 13:51	(PRINTED PAGE 7) ] ; 7137354092→	9043324189	;# 7
AUG-19-1992 11:09 FROM WESTINGHOUSE DESTEC ENGINEERING - TIGER BAY PROJECT	TO	86264505 P.07 CTT-5230	
DRY LOW NOX COMBUSTOR		Rev. 2	

8/19/92

#### SITE CONDITIONS:

SITE CONDITIONS:			
FUELTYPE	OIL	OIL	OIL
LOAD LEVEL	PART		BASE
FUEL HEATING VALUE, BYU/LB LHY	18450		18450
FUEL HEATING VALUE, BTU/LB HHY	19680	19680	19680
	••		(000
AMBIENT TEMPERATURE, F	27	72	97
RELATIVE HUMIDITY	40	75	45
Barometric Pressure, PSIA	14.515	14,615	14.615
inlet pressure loss, in—water	3.5	5,8	3.6
EXHAUST PRESSURE LOSS, IN-WATER	10.3		9.0
INJECTION FLUID	STEAM		STEAM
INJECTION RATIO, LB/LB	1.5	1.5	1.5
GENERATOR POWER FACTOR	0.85		
GENERATOR HYDROGEN PRESSURE, PSIA	30	30	30
GENERATOR FRAME (97 X 114)			
COMBUSTION TURBINE PERFORMANCE:			
MET BOWER ALTONIT YOU			
NET POWER OUTPUT, KW	171970	162330	147180
HEAT RATE, BTU/KWH LHV	9280	9560	9850
HEAT RATE, BTU/KWH HHV	9900	10190	10510
EXHAUST FLOW, LB/HR		3509380	
EXHAUST TEMPERATURE, F	1104	1104	1121
FUEL FLOW, LB/HR	86500	84110	78580
INJECTION RATE, LB/HR	129750		117870
AUXILIARY LOAD, KW	600	- • •	600
HEAT INPUT, MMBTU/HR (LHV)	1596	1552	1450
HEAT INPUT, MMBTU/HR (HHV)	1702		1546
EXHAUST ENERGY, MMBTU/HR	1054.5	1064.2	1024.3
EXHAUST GAS COMPOSITION (BY PCT VOL):			
OXYGEN	11.92	11.88	44.00
GARBON DIOXIDE	5.00	4.83	11.83 4.76
WATER	10.60	11,9(	12.57
NTROGEN	71.56	70.47	
ARGON	0.90	Q.89	69,94 0.88
MOLEÇULAR WEIGHT	28.33	28.17	28.00
2-17-2-11	20.00	20.17	20.00
EMISSIONS			
NOx, PPMVD @ 15% O2	42	42	42
NOx LB/HR	279	271	253
CO, PPMVD	50	50	60
CO, LB/HR	159	158	149
SO2, PPMVD	13	12	12
SO2, LB/HR	89	87	81
TOTAL UHC, PPMVD	20	20	20
TOTAL UHC, LB/HR	35	38	34
VOC, PPMVD	10	10	10
VOC, LB/HR	18	18	17
PARTICULATES (PM10/TSP), LB/HR (TOTAL)	39,6	39.0	36.7
SOOT, LB/HR	16.6	16.7	15.8
ASH, LB/HR	8.9	8.7	8.1
H2SO4 MIST 1 D/MD	0.3	10.7	0,1

EXPECTED 501F COMBUSTION TURBINE PERFORMANCE AND EMISSIONS

#### NOTES:

H2SO4 MIST, LB/HR

CO2, PPMVD

CO2, LB/HR

OPACITY, %

1. The net power output is the power at the generator terminals minus turbine auxiliary loads.

14.1

57653

260388

<=20

13.7

56431

<=20

272545

12.6

56099

<=20

254472

- 2. The fuel composition for distillate oil is per customer's specification.
- 3. Exhaust energy is referenced to 400 degrees Rankins.
- 4. Part loads are achived by modulating love.
  5. Power output at 27 deg. F is limited to 172 MW.

SENT BY: DESTEC ENGINEERING : 8-26-92; 13:54; 7137354
AUG-19-1992 11:11 FROM WESTINGHOUSE TO
DESTEC ENGINEERING - TOPE PAGE 20 [ RECEIVED 00/26 16:15 1992 AT 9043324189 ;#10 7137354092→ 9043324189 86264505 P. 10 じローちど30 Rev. 2 DRY LOW NOX COMBUSTOR

8/19/92

#### SITE CONDITIONS:

SITE CONDITIONS:			
0.0 705	OfL	OIL	OIL
FUEL TYPE	70%	70%	70%
LOAD LEVEL	18450	18450	18450
PUEL HEATING VALUE, BTU/LB LHV	19680	19680	19680
FUEL HEATING VALUE, BTU/LB HHV	18000	10000	1200-
AMBIENT TEMPERATURE, F	27	72	97
	40	75	48
RELATIVE HUMIDITY BAROMETRIC PRESSURE, PSIA	14,615	14.615	14,615
INLET PRESSURE LOSS, IN-WATER	2.3	2.3	2.2
EXHAUST PRESSURE LOSS, IN-WATER	7.2	0.4	5.9
INJECTION FLUID	STEAM	STEAM	STEAM
INJECTION RATIO, LB/LB	1,5	1.5	1,5
GENERATOR POWER FACTOR	0,85	0.85	0.85
GENERATOR HYDHOGEN PRESSURE, PSIA	30	30	30
GENERATOR FRAME (97 X 114)			
COMBUSTION TURBINE PERFORMANCE:			
NET POWER OUTPUT, KW	133020	113400	102810
HEAT RATE, BTU/KWH LHV	9770	10310	10680
HEAT RATE BTU/KWH HHV	10420	10990	11390
EXHAUST FLOW, LB/HR	2934960	2757580	2662180
EXHAUST TEMPERATURE, F	1130	1130	1130
PUEL FLOW, LEVHR	70440	63370	59510
INJECTION RATE, LB/HR	105660	95060	89270
AUXILIARY LOAD, KW	600	600	600
HEAT INPUT, MMBTU/HPI (LHV)	1300	1169	1098
HEAT INPUT, MMBTU/HR (HHV)	1386	1247	1171
EXHAUST ENERGY, MMBTU/HR	904.4	855 <i>.</i> 3	828.0
<b>—</b> • • • • • • • • • • • • • • • • • • •			
EXHAUST GAS COMPOSITION (BY PCT VOL):			
ÖXYGÉN	12.08	12.17	12.26
CARBON DIOXIDE	4.91	4.67	4.53
WATER	10.43	11.58	12.09
NITROGEN	71.65	70.68	70.23
ARGON	0.90	88.0	0.88
MOLECULAR WEIGHT	28.34	28.19	28.12
EMISSIONS			
NOx, PPMVD @ 15% O2	42	42	42
NOx, LB/HR	229	205	193
CO, PPMVD	50	50	50
CO, LB/HR	134	125	120
SO2, PPMVD	12	12	12
SO2, LB/HR	73	65	61
TOTAL UHC, PPMVD	20	20	20
TOTAL UHC, LEVHR	31	29	27
VOC, PPMVD	10	10	10
VOC, LB/HR	15	14	14
PARTICULATES (PM10/TSP), LEVHR (TOTAL)	32.6	30.0	28.5
SOOT, LB/HR	13.9	13.1	12,7
ASH, LE/HR	7.3	6.5	6.1
H2SO4 MIST, LB/HR	11.4	10,3	9.7
CO2, PPMVD	56460	54374	53041
CO2, LB/HR	230464	206946	194263
OPACITY %	<≂20	<=20	<=20

EXPECTED 501F COMBUSTION TURBINE PERFORMANCE AND EMISSIONS

#### NOTES:

OPACITY, %

.}

1. The net power output is the power at the generator terminals minus turbine auxiliary loads.

<=20

<=20

<=20

- 2. The fuel composition for distillate oil is per customer's specification.
- 3. Exhaust energy is referenced to 400 degrees Rankine.
- 4. Part loads are achieved by modulating igvs.

#### **ATTACHMENT 2**

#### FLORIDA GAS TRANSMISSION NATURAL GAS SAMPLE ANALYSES

.UATE: 04/28	/92	ANALYSIS TIME:	345	STREAM SEQUENCE:	12
TIME: 11 ANALYZER#:	:22 1	CYCLE TIME: MODE:	360 Run	STREAM#: 2 CYCLE START TIME	: 11:16
111111111111111111111111111111111111111	_	1.002			. ~~
COMP NAME C	OMP CODE	MOLE %	GAL/MCF**	B.T.U.*	SP. GR.
HEXANÉ +	151	0.022	0.0096	1.13	0.000
PROPANE	152	0.162	0.0446	4.08	0.002
I-RUTANE	153	7892.15-6	0.0026	0.26	0.000
N-BUTANE	154	7528.58-6	0.0024	0.25	0.000
IPENTANE	155	4220.48-6	0.0015	0.17	0.000
NPENTANE	156	4062.01-6	0.0015	0.16	0.000
NITROGEN	157	0.418	0.0000	0.00	0.004
METHANE	158	96.588	0.0000	977 <b>.78</b>	0.5549 0.538
C02	159	0.804	0.0000	0.00	0.012
ETHANE	160	1.982	0.5302	35.15	0.020
TOTALS		100.000	0.5923	1018.97	0.575

\* @ 14.730 PSIA DRY & UNCORRECTED FOR COMPRESSIBILITY

\*\* @ 14.730 & 60 DEG. F

COMPRESSIBILITY FACTOR (1/Z) = 1.0021DRY B.T.U. @ 14.730 PSIA & 60 DEG. F CORRECTED FOR (1/Z) = 1021.1 SAT B.T.U. @ 14.730 PSIA & 60 DEG. F CORRECTED FOR (1/Z) = 1003.3 REAL SPECIFIC GRAVITY = 0.5764UNNORMALIZED TOTAL 99.86

ACTIVE ALARMS

NONE

1041.8 10.5939

1041.9 ... 0.5939

TOTAL SULFUE O35 GOOD HUS 005 GO/CCF

0.8

DATE: 05/05/92 TIME: 11:25 'ANALYZER#: 137		ANALYSIS TIME: CYCLE TIME: MODE:	345 360 RUN	STREAM SEQUENCE: STREAM#121 CYCLE START TIME:	
COMP NAME C	OMP CODE	MOLE %	GAL/MCF**	B.T.U.*	SP. GR.
HEXANE +	151	0.024	0.0106	1.25	• 0.000
PROPANE	152	0.172	0.0474	4.34	0.00:
I-BUTANE	153	9949.88-6	0.0033	0.32	0.000
N-BUTANE	154	7610.23-6	0.0024	0.25	0.000
IPENTANE	155	3393.25-6	0.0012	0.14	0.000
NPENTANE	156	2694.51-6	0.0010	0.11	0.000
NITROGEN	157	Q.34B	0.0000	0.00	0.000
METHANE	158	96.786	0.0000	979 <b>.</b> 77	0.53
CO2	159	0.726	0.0000	0.00	0.01
ETHANE	160	1.919	0.5134	34.04	0.01
TOTALS		100.000	0.5793	1020.22	0.574

\* @ 14.730 PSIA DRY & UNCORRECTED FOR COMPRESSIBILITY

\*\* @ 14.730 & 60 DEG. F

COMPRESSIBILITY FACTOR (1/Z) = 1.0021

DRY B.T.U. @ 14.730 PSIA & 60 DEG. F CORRECTED FOR (1/Z) = 1022.4

SAT B.T.U. @ 14.730 PSIA & 60 DEG. F CORRECTED FOR (1/Z) = 1004.6

REAL SPECIFIC GRAVITY = 0.5752

UNNORMALIZED TOTAL = 79.80

ACTIVE ALARMS

NONE

TOTAL SULPHRO30 GRICES H25 Ox Grices

1.0 Billetonson

•

DATE: 05/12/9		. ANALYSIS TIME: CYCLE TIME:	345 360	STREAM SEQUENCE: STREAM#: 2	12
TIME: 12:1 ANALYZER#:	1	MODE:	RUN	CYCLE START TIME:	12:11
COMP NAME COM	1P CODE	MOLE %	GAL/MCF**	B.T.U.*	SP. GR.*
HEXANE +	151	0.021	0.0090	1.06	0.0007
PROPANE	152	0.177	0.0487	4.46	0.0027
I-RUTANE	153	0.014	0.0045	0.45	0.0003
N-BUTANE	154	0.012	0.0039	0.41	. 0.0003
IPENTANE	155	5825.91-6	0.0021	0.23	0.0001
NPENTANE	156	3664,47-6	0.0013	0.15	0.0001
NITROGEN	157	0.398	0.0000	0.00	0.0038
METHANE '	158	96 <b>.</b> 669	0.0000	978 <b>.</b> 59	0.5355
C02	159	0.748	0.0000	0.00	0.0114
ETHANE	160	1.952	0.5221	34.62	0.0203
TOTALS		100.000	0.5916	1019.95	0.5750

# @ 14.730 PSIA DRY & UNCORRECTED FOR COMPRESSIBILITY

\*\* @ 14.730 & 60 DEG. F

COMPRESSIBILITY FACTOR (1/Z) = 1.0021
DRY B.T.U. @ 14.730 PSIA & 60 DEG. F CORRECTED FOR (1/Z) = 1022.1
SAT B.T.U. @ 14.730 PSIA & 60 DEG. F CORRECTED FOR (1/Z) = 1004.3
REAL SPECIFIC GRAVITY = 0.5760
UNNORMALIZED TOTAL = 99.62

ACTIVE ALARMS

NONE

1041.8/0.5939

1041.9 20 0.5938

Force Suite 0.35 GYCCF" HIS OOS GYCCF

Bill Stirror

DATE: 05/19 TIME: 13 ANALYZER代記	3:02	ANALYSIS TIME: CYCLE TIME: MODE:	345 360 RUN	STREAM SEQUENCE: 12 STREAM#: TAKE 27 CYCLE START TIME: 12:	<b>ప</b> ్ర
COMP NAME (	COMP CODE .	MOLE %	GAL/MCF**	B.T.U.* S	P. GR.#
HEXANE +	151	0.024	0.0105	1.24	0.0008
PROPANE	152	0.189	0.0521	4.77	0.0029
I-BUTANE	153	0.015	0.0048	0.47	0.0003
N-BUTANE	154	0.012	0.0038	0.39	0.0002
IPENTANE	155	4932.21-6	0.0018	0.20	0.0001
NPENTANE	156	3461.10-6	0.0013	0.14	0.0001
NITROGEN	157	0.405	0.0000	0.00	0.0039
METHANE	158	96.505	0.0000	976.92	0.5345
C02	159	0.725	0.0000	0.00	0.0110
ETHANE	160	2.117	0.5662	37.54	0.0220
TOTALS		100.000	0.5404	1021.68	0.5758

\* @ 14.730 PSIA DRY & UNCORRECTED FOR COMPRESSIBILITY

\*\* @ 14.730 & 60 DEG. F

COMPRESSIBILITY FACTOR (1/Z) = 1.0021

DRY B.T.U. @ 14.730 PSIA & 60 DEG. F CORRECTED FOR (1/Z) = 1023.8

SAT B.T.U. @ 14.730 PSIA & 60 DEG. F CORRECTED FOR (1/Z) = 1006.0

REAL SPECIFIC GRAVITY = 0.5768

UNNORMALIZED TOTAL = 99.83

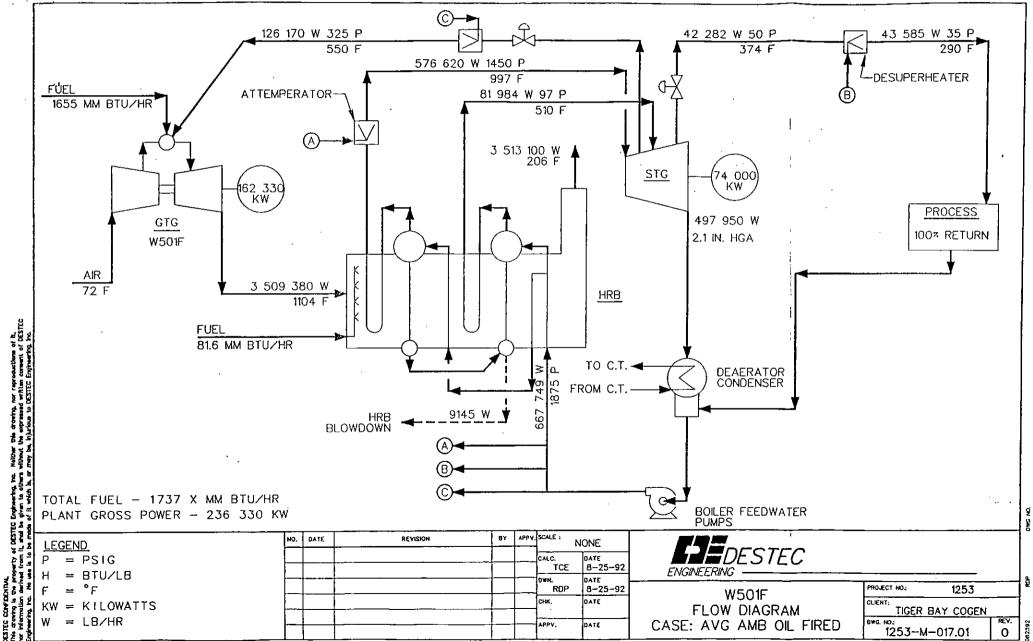
ACTIVE ALARMS

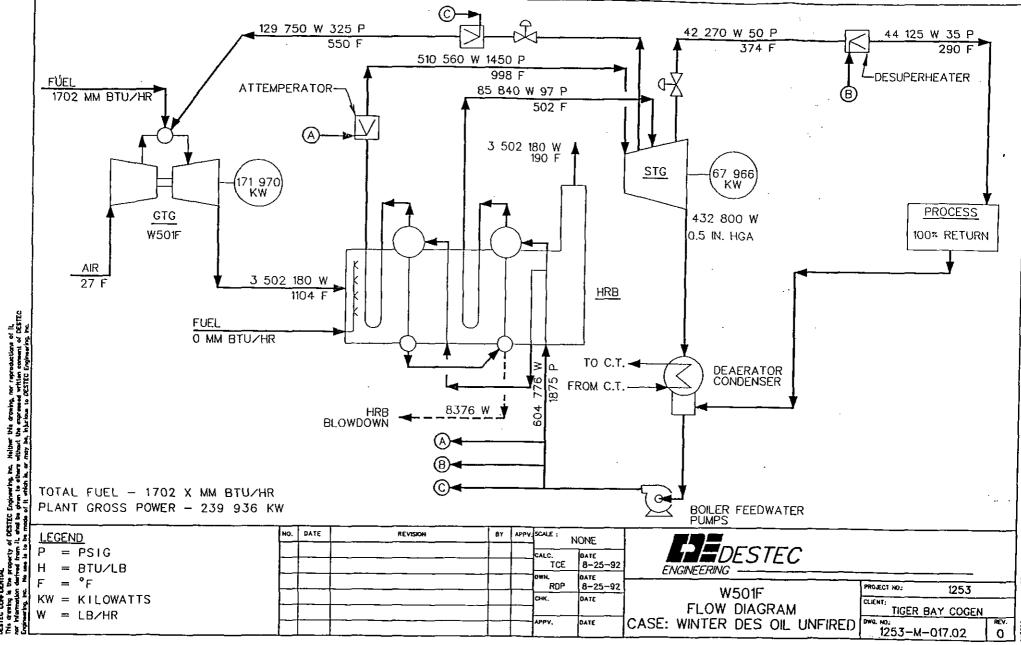
NONE

	FLORIDA GAS TRANSMISSION CO.	
	BROCKER LAB- Comm.	
	STANDARD GAS 1041.8 0,5939	<del></del>
	CERTIFIED VALUE BTU 1041.9 GRAI. 0.5939	
-	TOTAL SULFUR 0.30 GR/CCF H2SO.05 3R/CCF	
	HO /1/ #/MMCF BY BILL	

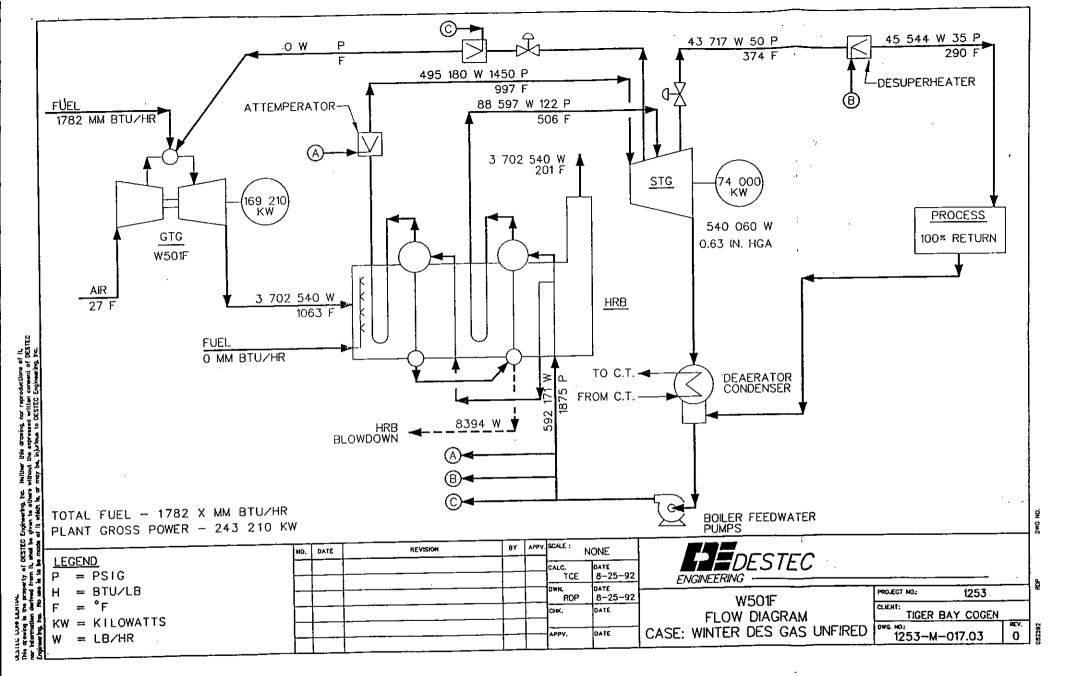
#### **ATTACHMENT 3**

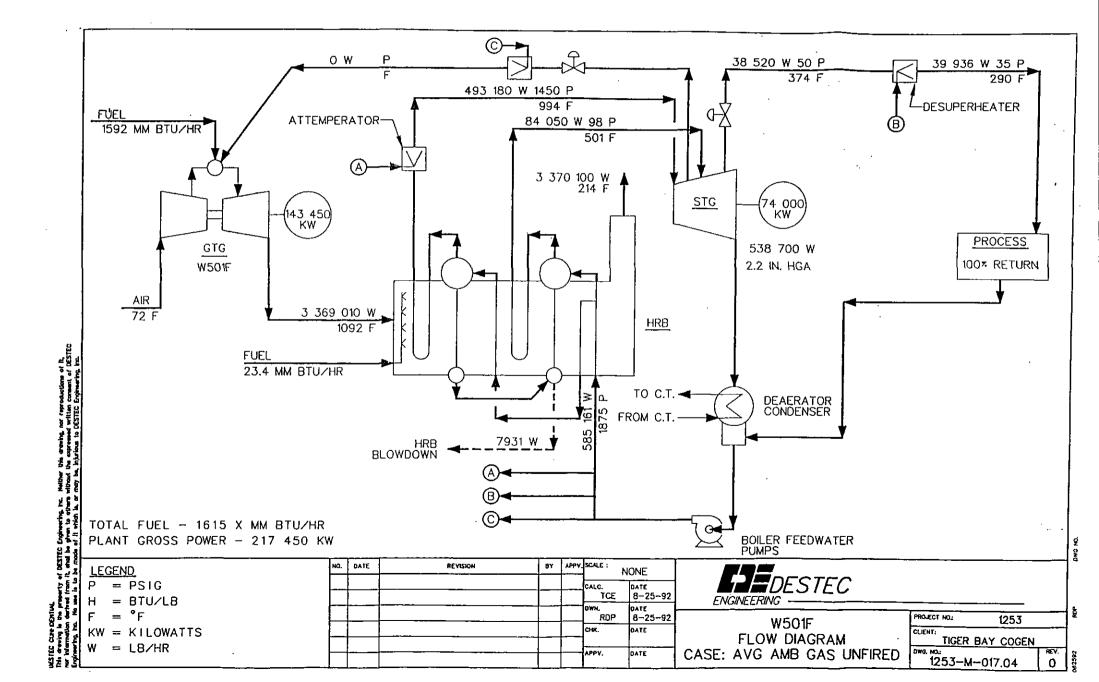
#### PROCESS FLOW DIAGRAMS FOR THE COMBUSTION TURBINE FIRING NATURAL GAS AND OIL

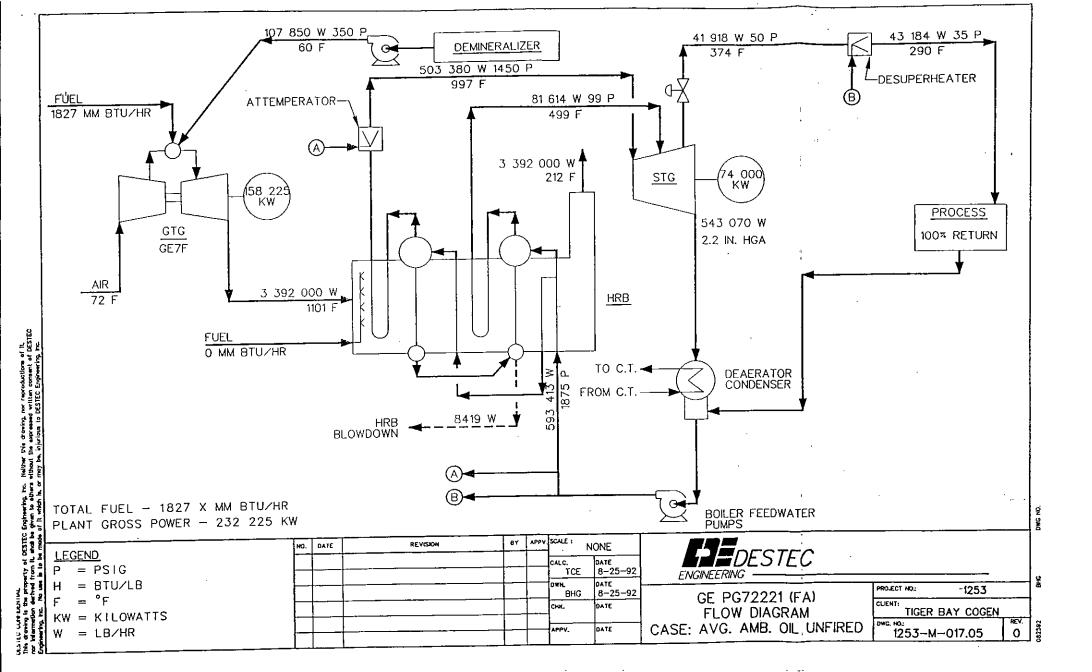


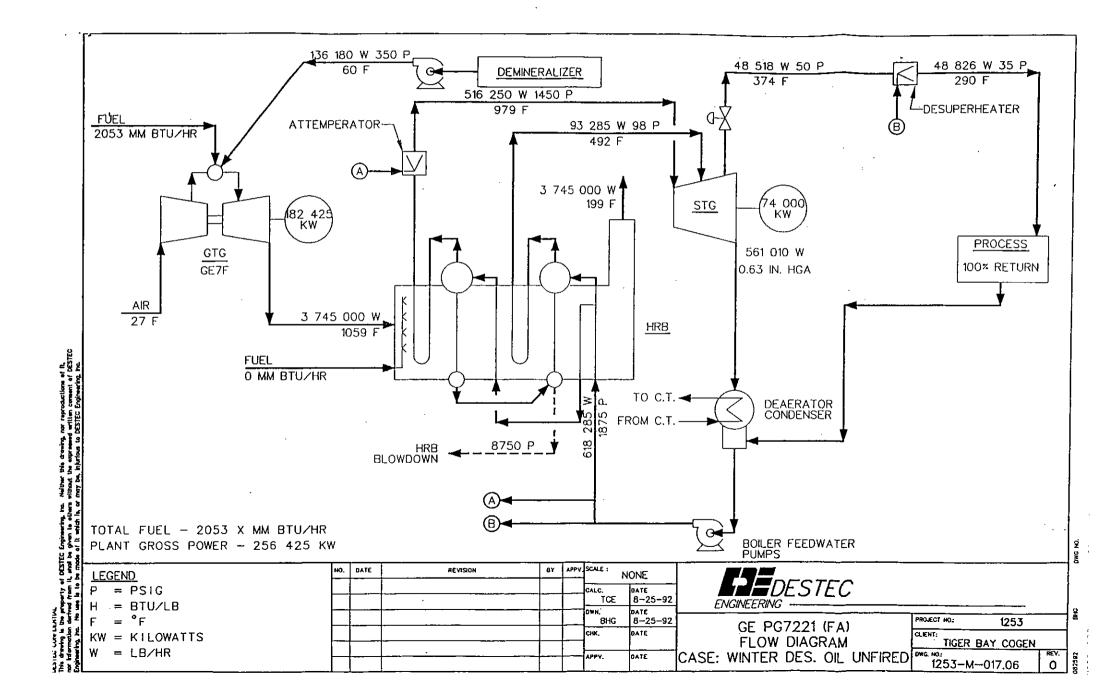


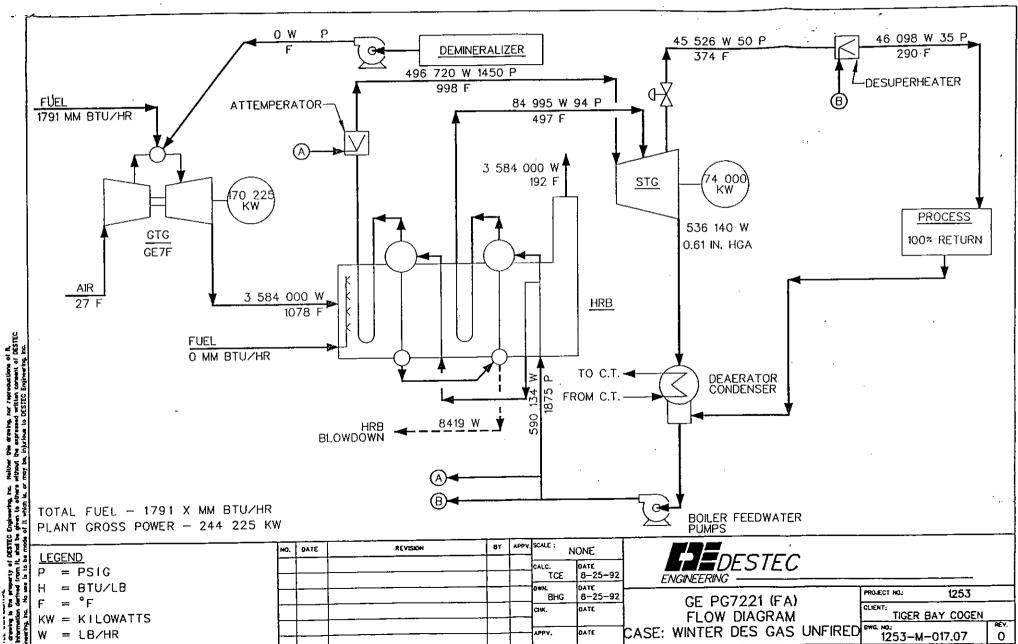
Contraction





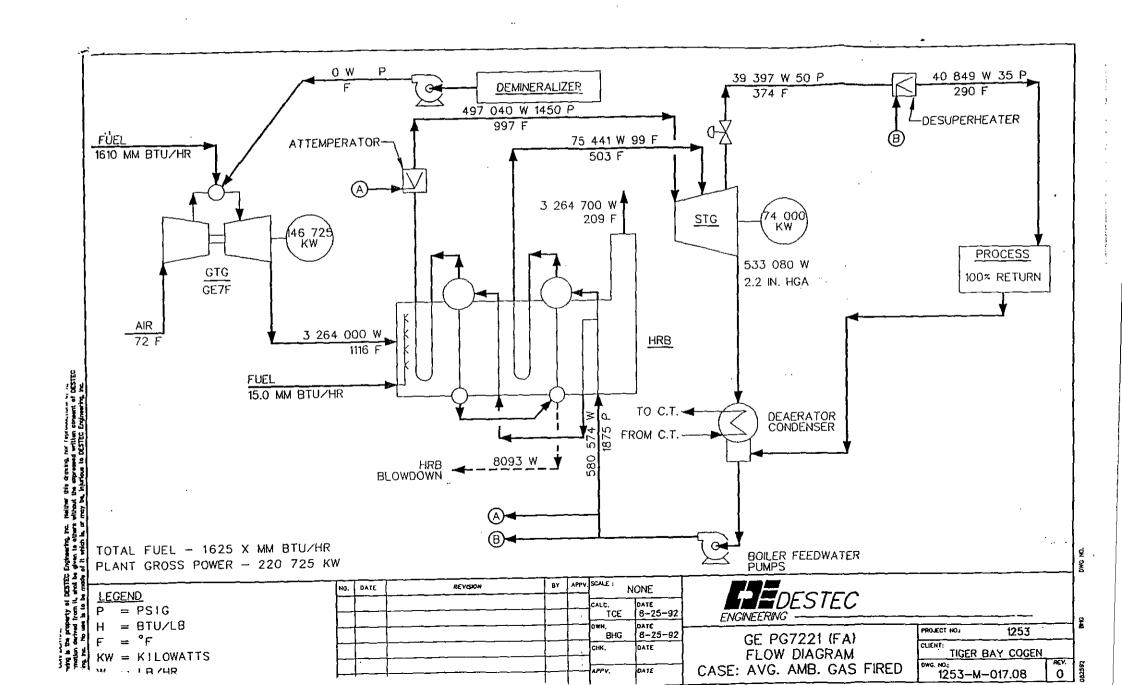






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2592 BH





# Florida Department of Environmental Regulation

Twin Towers Office Bidg. ● 2600 Blair Stone Road ● Tallahassee, Florida 32399-2400

Lawton Chiles, Governor

Carol M. Browner, Secretary

June 22, 1992

Mrs. Chris Shaver, Chief Permit Review and Technical Support Branch National Park Service-Air Quality Division Post Office Box 25287 Denver, Colorado 80225

Dear Mrs. Shaver:

RE: Central Florida Power Limited Partnership 206 MW Cogeneration Facility Polk County, PSD-FL-190

The Department has received the above referenced PSD application. Please review this package for completeness and forward your comments to the Bureau of Air Regulation by July 10, 1992. The Bureau's FAX number is (904)922-6979.

If you have any questions, please call Mirza Baig or Cleve Holladay at (904)488-1344 or write to me at the above address.

Sincerely,

WC. H. Fancy, P.E.

Chief

Bureau of Air Regulation

CHF/pa

Enclosures





# Florida Department of Environmental Regulation

Twin Towers Office Bldg. ● 2600 Blair Stone Road ● Tallahassee, Florida 32399-2400

Lawton Chiles, Governor

Carol M. Browner, Secretary

June 22, 1992

Ms. Jewell A. Harper, Chief Air Enforcement Branch U.S. EPA, Region IV 345 Courtland Street, N.E. Atlanta, Georgia 30308

Dear Ms. Harper:

RE: Central Florida Power Limited Partnership 206 MW Cogeneration Facility Polk County, PSD-FL-190

The Department has received the above referenced PSD application package. Please review this package and forward your comments to the Department's Bureau of Air Regulation by July 10, 1992. The Bureau's FAX number is (904)922-6979.

If you have any questions, please contact Mirza Baig or Cleve Holladay at (904)488-1344 or write to me at the above address.

Sincerely,

fr. H. Fancy, P.E.

Chief

Bureau of Air Regulation

CHF/pa

Enclosures





RECEIV DESTEC ENGINEERING, INC. 2500 CITYWEST BLVD., SUITE 1700 P.O. BOX 4411

JUN 25 1992 HOUSTON, TEXAS 77210-4411

JUN 25 1992 713) 974-8200

June 23, 1992

Division of Air Resources Management

Mr. Clair Fancy
Bureau of Air Regulation
Florida Department of Environmental Regulation
Twin Towers Office Building
2600 Blair Stone Road
Tallahassee, Florida 32399-2400

Re: Central Florida Power Limited Partnership

Dear Clair:

Please find enclosed a copy of the "Letter of Authorization" which was not included in our permit application and prevention of significant deterioration analysis for a 206-MW cogeneration facility. The application was submitted on June 12, 1992.

I will be contacting you in a week to review the initial comments your staff may have. In the meantime, please call if you have any questions.

Sincerely,

Robert S. Chatham, P.E.

Senior Environmental Engineer

RSC:tk

cc: Kennard F. Kosky, KBN

Barry Andrews, FDER

Mirza Baig, FDER

File



DESTEC ENGINEERING, INC. 2500 CITYWEST BLVD., SUITE 1700 P.O. BOX 4411 HOUSTON, TEXAS 77210-4411 (713) 974-8200

June 12, 1992

#### TO WHOM IT MAY CONCERN:

Subject: Letter of Authorization

Please be advised that Robert I. Taylor, Project Manager, is authorized to represent Central Florida Power Limited Partnership in matters relating to necessary permits and approvals required from federal, state, county, and local regulatory authorities in the areas of air, water and land issues.

Sincerely,

Robert O. Rogers

President, Central Florida DGE Inc.

Robert O. Kogen

Managing General Partner of

Central Florida Power Limited Partnership

tk

• 2	SENDER:
100	• Complete in
	Complete items 1 and/or 2 for additional services.     Complete items 3, and 4a & b.     Print your services.
1.8	Complete items 1 and/or 2 for additional services.     Print your name and address on the reverse of this form so     Attach this form so feel:  Attach this form so feel:
	Print your name and address on the reverse of this form so     Attach this form so
٠.:	that we can return this card to you.  Attach this form to the reverse of this form so feel:
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	Write "Return Receipt Regressed"  1. Addressee's Address  Addressee's Address
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	PS Form 3811, October 1990 alls one
	#US GPO: 1890—273-861 DOMESTIC DEPUT
	DOMESTIC RETURN RECEIPT
	THE THE RECEIPT

Certified Mail Receipt
No Insurance Coverage Provided
Do not use for International Mail
(See Reverse)

Sent to Sent to Heverse)
Mr. Robert I Tour
2500 City No. 11 10Wer, 11
Houston, TX 77042
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Postmark or Date
E Mailed: 7 1/ n
Permit: AC 53-214903
PSD-FL-190



# Florida Department of Environmental Regulation

Twin Towers Office Bldg. ● 2600 Blair Stone Road ● Tallahassee, Florida 32399-2400

Lawton Chiles, Governor

Carol M. Browner, Secretary

July 14, 1992

CERTIFIED MAIL - RETURN RECEIPT REQUESTED

Mr. Robert I. Taylor, Project Manager Central Florida Power, L.P. 2500 City West Blvd., Suite 150 Houston, Texas 77042

Dear Mr. Taylor:

On June 15, 1992, the Department received a PSD permit application to construct a 206 MW cogeneration power plant at the U.S. Agri-Chemicals Complex near Ft. Meade, Florida and deemed it incomplete. Please provide the following information:

- 1. Section 1-1 states the electrical output of the cogeneration facility is 206 MW. The gas turbine (GT) is rated at 147 MW and the duct burner is rated at 74 MW giving a total of 221 MW. What is the maximum electrical output you would like to be permitted for this facility?
- 2. According to Section 1-1, two types of advanced GTs are being considered for this project. The Department must know the exact type of gas turbine you propose to install so that a BACT determination can be made. Accordingly, please submit detailed information of the unit selected. We will also need any available stack test data for that unit.
- 3. What is the maximum sulfur content of the natural gas you propose to burn? Provide a copy of any sulfur content guarantee that you may have from the supplier.
- 4. Submit an updated process flow diagram showing steam turbine and volumetric air flow rates.
- 5. In Section 4-12, Table 4-2, the emissions (25 ppmvd) for advance GT with dry low- $NO_X$  technology appears to be incorrect. Also Table 4-2 should state the turbine size on which these figures are based.
- 6. Submit all emission calculations and not just an example calculation. These emission calculations shall be based on the selected turbine for this project.



Mr. Robert I. Taylor Page 2 of 2

- 7. What is the expected maximum ambient concentrations for the metals emitted?
- 8. Please provide an air quality related analysis (AQRV) of the impact this project will have on the Chassahowitzka National Wilderness Area (CNWA) for the pollutant NO2. The AQRV analysis includes impacts to soil, vegetation, and wild life. This analysis also includes an assessment of impacts to the adjuatic environment. Since the modeling information already provided with this application shows that the predicted NO2 impact at the CNWA Class I area is less than the National Park Service (NPS) recommended significance level, the NPS has verbally stated that only a literature review is needed in order to comply with the AQRV analysis requirement.
- 9. Section 4.3.1.2, page 4-10, states that "While the increased firing temperature increases the thermal  $NO_X$  generated, this  $NO_X$  increase is controlled through combustion design." How much additional thermal  $NO_X$  generated is due to higher temperature?
- 10. On page 4-3, the estimated cost of SCR is reported to be about \$7400 per ton of  $NO_X$  removed and it exceeds \$10,000 per ton of pollutant removed when the net emissions of all pollutants (exclusive of  $CO_2$ ) are considered. Provide us with the names and addresses of all manufacturers that were contacted while developing capital and annualized cost estimates for this project.

The processing of your application will continue upon receipt of the above requested information. If you have any questions, please contact Mr. Mirza P. Baig at (904) 488-1344.

Sincerely,

C. H. Fancy, P.E.

Chief

Bureau of Air Regulation

CHF/MB/plm

cc: Bill Thomas, SWD
 Ken Kosky, P.E., KBN Eng.
 Robert Chatham, Destec Eng.
 Jewell Harper, EPA, Atlanta
 Chris Shaver, NPS



April 9, 1992

DESTEC ENGINEERING, INC. 2500 CITYWEST BLVD., SUITE 1700 P.O. BOX 4411 HOUSTON, TEXAS 77210-4411

APIS Nº020 40 TPA53023801

Mr. Preston Lewis Bureau of Air Regulations Florida Department of Environmental Regulations 2600 Blairstone Road Tallahassee, FL - 32399-2400

Subject:

**Central Florida Cogeneration Plant** 

Fort Meade, Polk County

**Preliminary Information and Pre-Application Meeting** 

Dear Mr. Lewis:

The Central Florida Power Limited Partnership is planning a 210 MWe (nominal) cogeneration project(at)the U.S. Agri Chemicals Complex near Ft. Meade, Florida. The project will be called the Central Florida Cogeneration Plant. Destec Energy, Inc. is one of the partners, and is the developer of the project. Destec Operating Company will operate and maintain the cogeneration plant under contract to the Partnership. All pollution-emitting activities, including emission controls, will be under Destec control. Destec Engineering, Inc., an affiliate of Destec Energy, is under contract to the limited partnership to perform engineering services for the project, including air permitting.

The project will consist of one gas turbine (GT) electric generating unit, equipped with a duct burner-fired heat recovery steam generator (HRSG). The GT/HRSG unit will be primarily fired with natural gas, distillate oil will be used as the emergency backup fuel for the GT.

This letter presents a brief overview of the project, our preliminary analysis of the air emissions due to the project, and our understanding of the air permitting requirements and air regulations which apply to the project. We have concluded that a FDER construction permit will be required, and that certain NSPS will apply. We have also concluded that a PSD permit will be required for carbon monoxide (CO), nitrogen oxides (NO,), volatile organic compounds (VOC), particulate matter (PM), and particulate matter less that 10 microns (PM-10).

We understand that PSD review will not apply for sulfur dioxide (SO<sub>2</sub>) and other PSD-regulated pollutants, because the project will not cause significant emissions for these pollutants. We further understand that Nonattainment New Source Review (NNSR) will not apply to the project's emissions, because the project is not located in a nonattainment area.

We look forward to meeting at the FDER on Tuesday, April 14, 1992 at 10:00 AM to discuss the project and confirm the project's permitting requirements, procedures, and timing. We are especially interested in obtaining FDER input regarding BACT considerations for NO<sub>x</sub>, CO<sub>x</sub> VOC, PM, PM-10 and the timing of air dispersion modeling submittals. Destec Engineering.

Inc. has engaged the services of KBN Engineering (KBN) to prepare the air permit applications. Representatives of Destec, General Peat Resources and KBN will be present at the meeting.

#### **Project Schedule**

Contingent upon receipt of the necessary pre-construction approvals, construction of the Cogeneration Plant is scheduled to be financed by December 1992, construction begin by June 1993, and be operational by January 1995.

## **Project Overview**

Attachment 1 to this letter shows the general location of the project in Florida and Polk County. Polk County is classified as "attainment" or "cannot be classified" for all criteria pollutants.

Attachment 2 shows the specific project location in the U.S. Agri Chemicals Complex near Ft. Meade. The project will provide process steam to the U.S. Agri Chemicals complex. Electric power will be supplied to the public utility grid.

Destec personnel will operate and maintain the cogeneration plant under contract to the Partnership. The cogeneration plant manager will be a Destec employee. The plant will be owned by the limited partnership. An affiliate of Destec Energy, Inc., General Peat Resources and EcoEnergy will have ownership interest in the partnership.

The project is evaluating different manufacturers of gas-fired turbines. The gas turbine unit will have a nominal electrical output of about 150 MWe, a maximum heat input of about 1900 MMBtu/hr (HHV), and will be equipped with dry low NO<sub>x</sub> combustors. The gas turbine's exhaust will be routed to a duct burner-fired HRSG unit, normally unfired. The natural gas-fired duct burner for the HRSG unit is expected to have a maximum heat input of about 125 MMBtu/hr (HHV). The steam from the HRSG unit will power a steam turbine electrical generator, with a maximum output of about 74 MWe.

Approximately 40,000 lb/hr of low pressure steam will be exported to the U.S. Agri Chemical complex for use as thermal energy.

Electrical power will be sold to the public utility grid.

#### **Project Emissions**

By firing natural gas the gas turbine exhaust (entering the HRSG) will be limited to 25 ppmvd NO<sub>x</sub>, at 15% oxygen, and 15 ppmvd CO. Advanced dry low NO<sub>x</sub> technology combustors and other measures will be used to control the NO<sub>x</sub> emissions from the project's gas turbine and duct burner while firing natural gas. The duct burners will be only fired on natural gas. The duct

burner NO<sub>x</sub> emissions will be about 0.10 lb/MMBtu.

When firing distillate oil, the gas turbine exhaust entering the HRSG will be limited to 42 ppmvd  $NO_x$  at 15% oxygen and 30 ppmvd CO. Steam or water injection will be utilized for  $NO_x$  control when firing distillate oil. The annual distillate oil usage is anticipated to be approximately 350 hours per year.

The planned permit application will present calculations of maximum hourly and annual emission rates for all regulated pollutants for each emitting unit. For purposes of evaluating how PSD regulations may apply to the project, Destec has performed preliminary, worst-case emissions calculations of annual emissions. These calculations are summarized and discussed below.

Destec may present slightly different calculated emissions in the planned permit application, based on operational limitations that may be proposed to FDER as part of the requested permit.

In the preliminary, worst-case emissions calculations the single GT/HRSG is assumed to operate at maximum rated heat input, year-round. This calculational basis considerably over estimates the emissions that will actually occur, since (1) the gas turbine will at times be operated at less than maximum capacity and (2) the duct burner in the HRSG will not normally be operated. The following table summarizes the preliminary, worst-case emissions calculations and compares the calculated emissions to the PSD significance levels:

	Worst Case Project Emissions (T/yr)	PSD Significance Level (T/yr)
Carbon monoxide (CO)	324	100
Nitrogen oxides (NO <sub>x</sub> )	750	40
Sulfur dioxide (SO <sub>2</sub> )	39	40
Particulate matter (PM)* and PM-10	48	25/15
Volatile organic compounds (VOC)	58	40
Non-criteria PSD regulated pollutants	None or Negligible	Project emissions will be insignificant

The permit application will conservatively assume that PM will consist 100% of PM-10.

## **Applicability of PSD and NNSR Review**

Destec's understanding of the PSD regulations is that the planned Cogeneration Plant is not one of the 28 source types, therefore, the criterion of "major source" is 250 T/yr of any regulated pollutant. On that basis, and based on the preliminary emissions calculations summarized above, the cogeneration plant will be a major stationary source, since the plant will emit 250 T/yr or more CO and NO<sub>x</sub>. Destec understands, therefore, that PSD is applicable to all PSD-regulated pollutants which the plant will emit in significant amounts. Destec further understands that, because the cogeneration plant will be a new "stationary source" under separate control from the U.S. Agri Chemical complex, netting of contemporaneous increases and decreases is not applicable. Therefore, Destec has concluded that PSD will apply to all pollutants for which significant emissions will occur from the new cogeneration plant. As shown on the table in the preceding section, the plant will be significant for CO, NO<sub>x</sub>, VOC, PM and PM-10. Therefore, we understand that PSD review will apply to the project for CO, NO<sub>x</sub>, VOC, PM and PM-10.

The plant will have insignificant emissions of SO<sub>2</sub>, lead, and non-criteria PSD regulated pollutants. Therefore, we understand that the project will <u>not</u> be subject to PSD review for SO<sub>2</sub>, lead, and non-criteria PSD-regulated pollutants. Also, we understand that the project will not be subject to NNSR review.

## **Applicability of NSPS Regulations**

Based upon the preliminary project plans, we understand that the Cogeneration Plant will be subject to some of the New Source Performance Standards contained in:

• 40 CFR 60 Subpart GG: Stationary Gas Turbines

• 40 CFR 60 Subpart Db: Industrial - Commercial - Institutional Steam Generating Units

In addition, the project's duct burner-fired HRSG unit does not appear to not be subject to Subpart D or Da since the duct burners' maximum heat input capacity of 125 MMBtu/hr does not exceed the applicability level of 250 MMBtu/hr.

Regarding the NSPS for a gas turbine in 40 CFR 60 Subpart GG, the turbines will be subject to the Subpart GG limits for sulfur dioxide, which require that the exhaust gases do not exceed 150 ppmv SO<sub>2</sub> (at 15% O<sub>2</sub>, dry basis) and that the fuel does not contain more than 0.8 percent sulfur by weight. The turbine and fuels will easily comply with these limits. We understand that the cogeneration plant will be required to periodically monitor and report fuel sulfur content in accordance with the Subpart GG NSPS.

Regarding the NSPS for steam generating units in 40 CFR 60 Subpart Db., the project's duct burner-fired HRSG unit will be subject to the NSPS, because the maximum fuel firing rate (about 125 MMBtu/hr/duct burner (HHV)) is greater that the NSPS applicability threshold of 29 MWe (100 MMBtu/hr). The Subpart Db NSPS requires that affected duct burners meet a NO<sub>x</sub> emission limit of 0.2 lb/MMBtu heat input, which is applicable to firing natural gas in duct burners of combined cycle systems (see 40 CFR 60.44b(e)). The planned duct burners will have

no difficulty in meeting the NSPS. The duct burners will be fired only on natural gas.

#### **CO BACT Considerations**

The gas turbines dry low NO<sub>x</sub> combustors are guaranteed to limit CO to 15 ppmvd, natural gas, and limit CO to 30 ppmvd, firing distillate oil and injecting steam or water. At the CO emission rates which correspond to this low concentration, the ambient CO impacts of the project are expected to be negligible (i.e., well below FDER and EPA significance thresholds). Given the low CO emissions and negligible impacts, we currently anticipate proposing the low NO<sub>x</sub> controls as BACT for CO. We would like to obtain FDER input prior to preparing our BACT analysis and permit applications.

### **Contents of Air Permit Applications**

We plan to submit two separate permit application documents for the Cogeneration Plant:

- FDER construction permit application
- PSD application

Destec Engineering and KBN are now beginning to assemble the information and perform the analysis to be included in the permit applications.

The FDER permit application is expected to include the following information:

- Completed FDER permit application forms
- Certifications (i.e. professional engineers certification)
- Description of the project and the process, with an area map, plot plant and process flow diagram. Emphasis will be placed on sources of emissions and emission control measures.
- BACT analysis for CO, NO<sub>x</sub>, SO<sub>2</sub>, PM, PM-10 and VOC
- Description of applicable air regulatory requirements
- Appendicized emission rate calculations, along with the inputs and assumptions used.
- Dispersion modeling analysis in accordance with protocols agreed upon with FDER.

The PSD permit application will include much of the same information included in the state application, except that the PSD BACT analysis and any dispersion modeling analysis will address only CO, NO<sub>x</sub>, PM, VOC, and PM-10. The PSD application's BACT analysis for NO<sub>x</sub> and CO will be quite brief, because we understand that our planned BACT measures for NO<sub>x</sub> and CO represent the "top" level of BACT, consistent with current FDER and EPA policies. The PSD application's BACT analysis for PM and PM-10 is also expected to be quite brief, because we are aware of no control techniques (aside from modern design and good combustion

practices) for PM/PM-10 emissions from gas-fired/oil-fired gas turbines and gas-fired duct burners.

With respect to dispersion modeling, we currently anticipate submitting modeling analysis when the permit applications are submitted to FDER. We anticipate that a separate modeling protocol meeting with FDER modelers will be required to confirm specific procedures prior to performing the modeling.

We look forward to meeting with you on April 14th to confirm the air permitting requirements and timing for the project. In the interim, if there are any questions regarding the project or this letter, please call me at (713) 735-4087.

Sincerely,

DESTEC ENGINEERING, INC.

Rath Chatham

Robert S. Chatham

**Environmental** Engineer

cc:

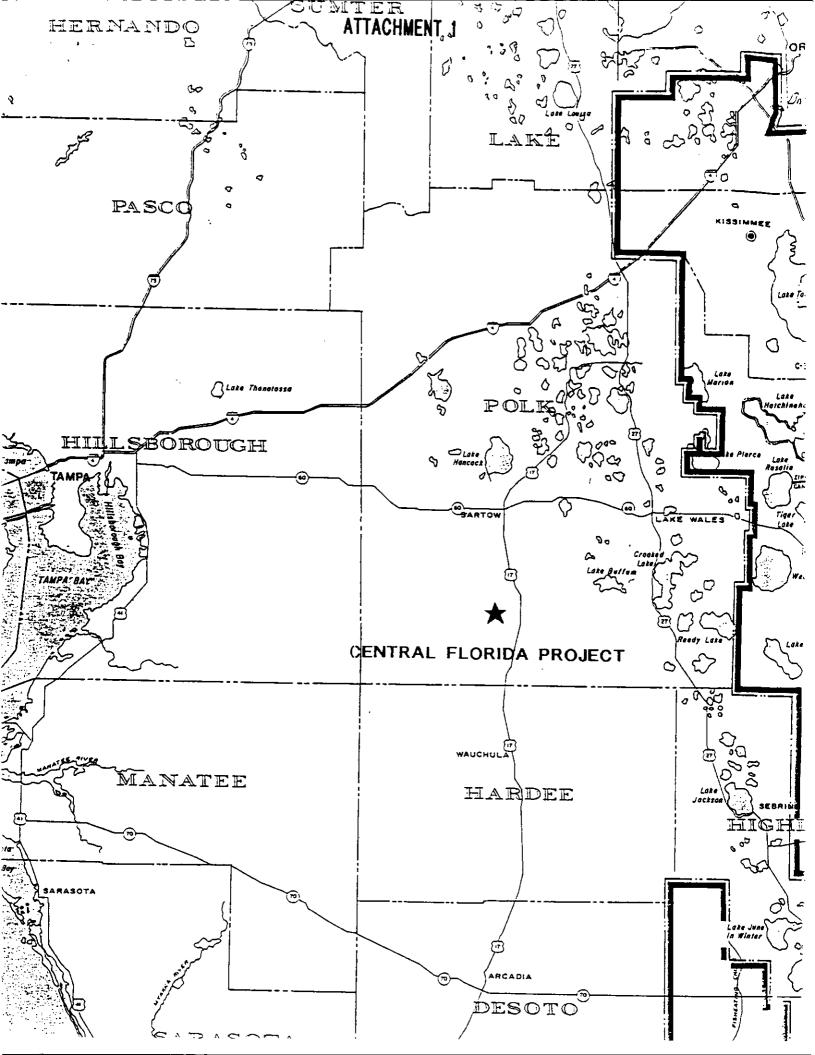
Mr. J. W. Kenny, General Peat Resources

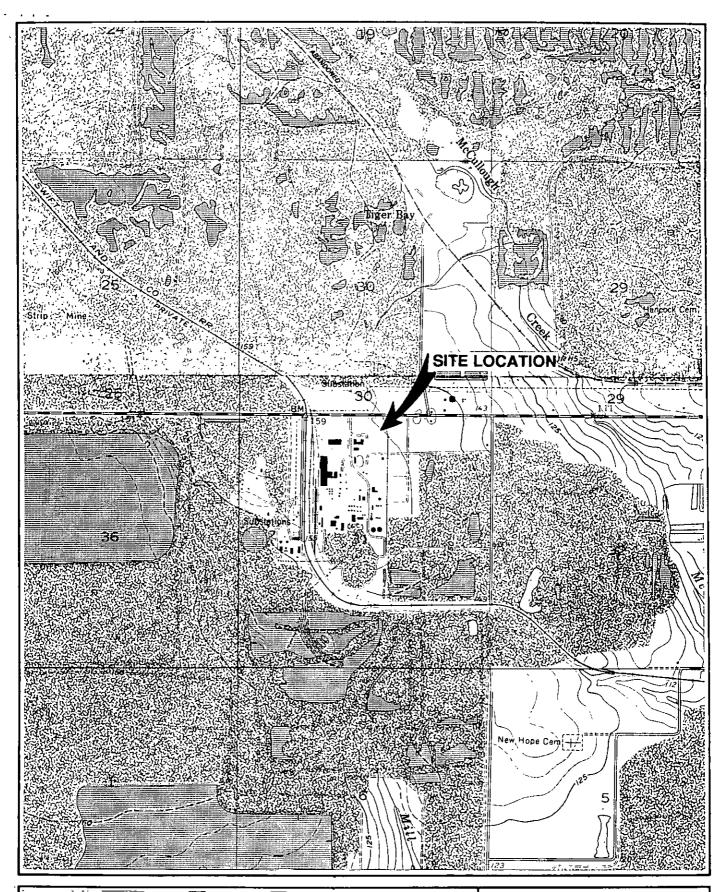
Mr. Ken Kosky, KBN

Attachments:

1 -

Project Location in Florida and Polk County Project Location within U.S. Agri Chemicals Complex





ATTACHMENT 2
PROJECT LOCATION MAP

EDESTEC ENGINEERING

SOURCES: USGS, 1987; KBN, 1992.

*.* .

# WAIVER OF 90 DAY TIME LIMIT UNDER SECTIONS 120.60(2) and 403.0876, FLORIDA STATUTES

License (Permit, Co	ertification)	Application	NO. AC 53-214903
			PSD-FL-190
Applicant's Name:	Central Florida	Power, L.P.	
	Tiger Bay Cogen	eration Plant	
hereby with full rights under Sect waives the right the State of Fl within the 90 day made freely and knowledge, and w	knowledge a ions 120.60(2 to have the orida Departmentime period voluntarily without any	and understa ) and 403.08 application ment of Env prescribed by by the a pressure or	cation, the applicant nding of applicant's 76, Florida Statutes, approved or denied by ironmental Regulation law. Said waiver is applicant, with full coercion by anyone ment of Environmental
This waiver shall	expi-re on the	15th day	of January 1993.
The undersigned i the applicant.	Ŝ	ignature Robert I. Taylor	roject Manager



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DESTEC ENGINEERING, INC. 2500 CITYWEST BLVD., SUITE 1700 PO. BOX 4411 HOUSTON, TEXAS 77210-4411 (713) 974-8200

Date: _ To:	Preston Lewis		Page \ of 2
1.	Document  Waiver of 90 Day Time	 	Date/ Job No./ Note Revision Project
2.	7	- -	
3.		- -	
4		-	
Notes:		-	
Cover			ackage c² Teresa Heroni (Fi
			c: Teresa Heroni (Fi Patti Adams (Fi
File			