

KA 124-97-03

August 11, 1998

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BUREAU OF AIR REGULATION

Mr. John Reynolds
Florida Department of
 Environmental Protection
Twin Towers Office Building
2600 Blair Stone Road
Tallahassee, FL 32399-2400

Subject: IMC-Agrico Company (New Wales)

Multifos Plant Production Increase

DEP File No. 1050059-024-AC, PSD-FL-244

Dear Mr. Reynolds:

We would like to thank both you and Al Linero for meeting with us last week to discuss IMC-Agrico's concerns regarding the draft permit for the above project. We truly appreciate your willingness to consider the issues of concern to us and to work with us to resolve them in an expeditious manner.

Our comments on the draft permit are provided below. Most of the comments are inter-related and correspond to just a few key issues.

### TECHNICAL EVALUATION & PRELIMINARY DETERMINATION

### 1. Page 2 of 13, Section IIA, Paragraph 2:

A scrubber will not be required for the mixed feed storage building given the minimal amount of fluorides present in the building. Additional information on this process is provided in Attachment 1, along with references and test data.

### 2. Page 2 of 13, Section IIA, Paragraph 2:

Only one caustic scrubber, for the new kiln, will be required for the proposed project. No changes are proposed to the existing kilns.

### 3. Page 3 of 13, Paragraph 1:

IMC-Agrico requests that installation of a new stack be provided for in the permit, as an alternative to ducting the third kiln to the existing stack. A new stack for the third kiln may be necessary if back-pressure becomes an issue.

Please note that a separate stack is not required for compliance testing purposes as it will be possible to test the new kiln by sampling in the duct leading to the main stack, if required. The existing system can be tested by sampling prior to the point at which the new duct connects to the main stack.

### 4. Pages 3 and 4 of 13:

We do not feel that such an extensive explanation for the completeness date for the project is necessary.

### 5. Page 4 of 13, Paragraph 2:

The chemical reactions associated with the mixed feed process do not require curing during storage. The material is, however, kept in storage for a period of time to allow for a reduction in the excess moisture.

### 6. Page 4 of 13, Paragraph 3 (table):

Based on recent nitrogen oxides emissions measurements, it seems that the proposed project will trigger PSD review for NOx. The recent measurements indicate a tentative limit of 15 pounds per hour (66 tpy), to be refined upon completion of construction.

### 7. Page 5 of 13, Paragraph 1 (table):

The table should not include the existing kilns A and B and their associated scrubbers and baghouses as they are not part

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of the proposed modification. A discussion on the proposed modification is provided in Attachment 2.

### 8. Page 5 of 13, Paragraph 3:

The emission increases associated with SO2 are expected to be less than the PSD threshold, given that the existing kilns are not being modified. We agree that the proposed project should be subject to PSD review for NOx.

### 9. Page 6 of 13, Paragraph 2:

The 1981 permitted production increase was accommodated with corresponding emission decreases within the plant (see Attachment 3). There was no change in the production rate of 25 tph in 1995, simply a correction in the corresponding raw material input rate referenced in the operation permit. A copy of the corresponding construction permit, issued in 1981, is presented in Attachment 3.

### 10. Page 7 of 13, Paragraph 2:

It should be noted that the application was prepared based on information available on total fluoride emissions as no information is available on hydrogen fluoride. We agree with the Department's opinion that the proposed project is not major for HAPs.

### 11. Page 7 of 13, Last Paragraph:

The proposed project is not subject to PSD for SO2. The modeling was conducted merely to determine if the predicted SO2 impacts were significant, given FDEP's concern about SO2 in the SW area of Florida. Please note that the ISC3 modeling was updated to reflect the option of an alternate new stack for the new kiln. The results indicate lower predicted SO2 impacts from the proposed project if a separate stack is used. The modeling results are summarized in Attachment 4. A disk, containing the modeling output, is enclosed.

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### 12. Page 13 of 13. Conclusion:

We do not object to providing FDEP with information on the new kiln design (when available), however, we do not feel that the kiln design requires FDEP approval.

We understand and prefer that the TEPD not be revised based on our comments. Changes are requested to the conditions of the final permit and BACT.

### PERMIT CONDITIONS

### 13. Reference to Permit Number:

The permit number, in the header from page 3 onward, needs to be corrected.

### 14. Facility Description:

Please note that 55 tph corresponds to the maximum material input rate to the kilns.

### 15. Page 4 of 8, List of Emission Units:

As previously discussed, please remove EU Nos. 032, 033, 034, 035 and 038 from the list of affected units, as they are not part of the proposed modification.

### 16. Page 4 of 8, Specific Condition 2:

Please remove existing kilns A and B and their associated scrubbers and baghouses from the table, as they are not part of the proposed modification. Also, we suggest a NOx emission limit of 15 pounds per hour for the new kiln, based on measurements on the existing kilns (see Attachment 5). It may be appropriate to set a final NOx limit based on testing of the new kiln, upon completion of construction.

### 17. Page 4 of 8, Specific Condition 3:

Based on conversations with design and process staff, the maximum mixed feed preparation plant rate should reflect 100 tph. Compliance testing will be conducted at 90-100 percent of the allowable operating rate.

### 18. Page 4 of 8, Specific Condition 4:

The rates tabulated by FDEP are representative only of material input to the kilns, as the raw material rates vary depending on moisture, etc. The tabulated rates are appropriate, however, it is requested that the preceding wording reflect that these are kiln input rates.

### 19. Page 5 of 8, Specific Condition 6:

As discussed during our meeting, it is requested that the condition be re-worded to reflect that the pollution control system for kiln C shall be designed for 99.9+% fluorides removal and that testing will not required to determine the system efficiency. Also, kilns A and B should not be included in this condition.

### 20. Page 5 and 6 of 8, Specific Conditions 7, 8 and 9:

As discussed during our meeting, the emissions limits set by FDEP will be met by IMC-Agrico. Consequently, these three conditions should be deleted. We do not object to a condition which prohibits the release of the caustic scrubber water to the existing process pond water to ensure that the captured SO2 and F will not be liberated to the atmosphere.

### 21. Page 7 of 8, Specific Condition 11:

It is requested that the higher operation period be for 30 days to allow for the 15-day prior testing notification, required by rule. This would be consistent with similar conditions for many facilities' Title V permit provisions.

### 22. Page 7 of 8, Specific Condition 14:

It is requested that the permit allow the use of both fuels for cost leveraging and operational flexibility purposes. It should be noted that the emissions limits, FDEP's primary concern, will be met in either case. Also, it is requested that reference to kilns A and B be removed as they are not part of the proposed modification.

### BACT DETERMINATION

### 23. Page BD-1, Paragraph 1:

The 30 and 55 tph values correspond to kiln input rates. Also, the last sentence should read "avoid" or "escape" PSD review, not circumvent. The former is specifically allowed by rule while the latter is prohibited.

### 24. Page BD-1, Paragraph 2:

The stated production rates are actually kiln feed rates. Also, the AP-42 NOx emissions factor is based on fuel so the annual NOx emissions are dependent upon fuel use, not tons of material processed. Regardless, the NOx emissions from the proposed project will be subject to PSD review based on recent measurements on the existing kilns (see Attachment 5).

### 25. Pages BD-1 and BD-2:

As explained to FDEP, the two existing kilns will not be modified or debottlenecked (see Attachment 2). Therefore, they are not subject to PSD review. Consequently, the calculations of net emissions increase would be different. However, the issue is moot.

### 26. <u>Page BD-5</u>:

Fluorides are not expected to be emitted in any significant quantity from the mixed feed operation or storage building,

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unlike TSP, due to differences in the material composition and reaction. Additional information on the mixed feed operation is presented in Attachment 1. Also included are results of measurements conducted in the storage building which reflect extremely low fluoride concentrations.

Please note that the pug mill will be vented to the existing equipment scrubber primarily for control of particulates, as is the case for the existing feed preparation operation.

### 27. <u>Page BD-6</u>:

We agree with the Department that BACT for NOx emissions should focus on combustion controls. Presently, the kiln exit measurements reflect 1.5% oxygen level. These low excess air conditions effectively reduce the amount of NOx generated. Therefore, IMC-Agrico proposes the use of low excess air, (using cooler air as secondary combustion air) as BACT for NOx. A preliminary NOx limit of 15 pounds per hour would be acceptable with a provision to set the final limit after testing upon completion of construction.

### 28. <u>Pages BD-7 to BD-10</u>:

As discussed with FDEP during our meeting, we are not in complete agreement over the data used in calculating fluoride emissions and the corresponding scrubber efficiencies. However, no further discussion is warranted as the issue is moot. Based on the commitment made during our meeting, the air pollution control system will be designed for 99.9+% of fluorides and 98% removal of SO2, combination of the crossflow pond water scrubber and the caustic scrubber; and, the respective emission limits will be met (see Attachment 6). We do not object to a condition which prohibits the release of the caustic scrubber water to the existing process pond water to ensure that the captured SO2 and F will not be liberated to the atmosphere. approach allows the disposal or beneficial use of the stream without compromising FDEP's intent.

### 29. Pages BD-12 to BD-14:

The BACT determination should not apply to the existing kilns A and B and their associated scrubbers and baghouses, as previously discussed.

We appreciate the opportunity to submit the above comments. It is our understanding that FDEP will review these comments and then finalize the permit and BACT, as appropriate. As you are aware, the request of extension of time expires around the conclusion of the 30-day public notice period. Consequently, we would appreciate your prompt feedback on any issue where additional information is required.

If you have any questions, or feel that a follow up meeting is required to resolve any issues, please call Pradeep Raval or me.

Very truly yours,

KOOGLER & ASSOCIATES

oba B Koogler, Ph.D., P.E.

par encl.

c: C. Dave Turley, IMC-Agrico

CC: C. Holladay, BAR SWP POLK CO. EPA NPS

### ATTACHMENT 1

- A. PROCESS INFORMATION
- B. TEST DATA
- C. REFERENCE INFORMATION

### A. PROCESS INFORMATION

### MULTIFOS MIXED FEED vs. TRIPLE SUPER PHOSPHATE BLENDING AND STORAGE OPERATION

The FDEP evaluation compared the mixed feed process to the triple super phosphate process, assuming that there is fluoride generation in the storage area. However, the two processes are very different because of the proportions of acid to rock and the presence of soda ash (a strong base) in the mixed feed process.

The triple super phosphate process uses 2.5 tons of  $P_2O_5$  from acid for each ton of  $P_2O_5$  from the rock. This contrasts with the mixed feed process which uses only 0.42 tons of  $P_2O_5$  from acid for each ton of  $P_2O_5$  from the rock. Additionally, in the mixed feed process, 0.85 tons of soda ash is used for each ton of  $P_2O_5$  from phosphoric acid. This works out to be about 1.14 moles of  $Na_2O$  for each mole of acid  $P_2O_5$ . The soda ash is enough to form monosodium phosphate with all of the phosphoric acid present, and then form some disodium phosphate, which is alkaline and has a solution pH of 9.1 (Merck Index). Samples of mixed feed have been measured to have a pH of 6.5 immediately after mixing, while GTSP samples have been measured to have a pH of 3.1.

In summary, the neutral pH of the mixed feed prevents the fluorapetite from being dissolved by the acid, which is the reaction that occurs in TSP storage that generates fluorides. Consequently, fluorides are not generated in the mixed feed storage area, as there is practically no ongoing reaction involving the rock. Results of fluoride measurements in the storage area are attached.

The mixed feed, however, is allowed to dry over a period of a couple of days to reduce the moisture content. The fuel consumption can be reduced by reducing the amount of moisture in the feed material.

### Run 1 Calculations and Results

Facility: New Walos

Plant: Multifus Mixed Feed Storage Building

Company ID:

0

FDFP AIRS & Pt. ID:

0

Test Team: DC/ML

Date: 7/31/98 mm/dd/yy

Start Time:

840

End Time:

1040

Standard Meter Volume Vms:

70.91 dscf

### **Emission Calculations**

I'luoride Total mg: 0.15 mg
0.0021 mg/dscf
0.0869 ambient ppm Dry Basis
0.00276 lb/hr at 10000 cfm

Ambient Data					
		Start	1 Hour	lind	Avg
At Sample Level					
Dry Bulb		93	95	98	
Wet Bulb	•	85	85	88	
Relative Humidity		72	66	67	68
At Floor					
Dry Bulb		87	88	90	
Wet Bulb		13	81	81	
Relative Humidity		76	74	<b>6</b> 8	73
At Bay Door					
Dry Bulb		85	87	92	
Wet Bulh		80	85	82	
Relative Humidity		81	92	65	79

### Sample Collection Site Description

The catwalk above the warehouse at the mid point of the warehouse.

Material to the west of the sample point was 1-3 days old.

Material was entering the building east of the sample point.

Kiln feed was being removed directly below the sample point

Run 1 Data

l'acility: New Wales

Plant: Multifos Mixed Feed Storage Building

Company ID:

FDEP AIRS & Pt. ID:

0 Test Team: DC/ML

> 7/31/98 mm/dd/yy Datc:

Start Time:

840

lind Time:

1040

Number at Traverse Points:

Dwell Time/Point:

1 60 min.

Total Test Time:

60 min.

Stack Diameter:

0 inches

Stack Area:

0.00 sq. ft.

Molecular Weight Dry Md:

28,969

Volume of Water Vapor Condensed:

56 ml

Weight of Water Collected in Silica Gel:

17.3 gram

Moisture Volume Fraction Bwo: Moisture Volume Saturated Bwo: 0.0464

Moisture Percent Saturation:

0.0556

83

Moisture Used for Calculations: Stack Molecular Weight Ms; 0.0464 28.460

Barometric Pressure Pb;

30.16 in He

Stack Static Pressure Pv:

0.00 in [12O]

Stack Pressure Ps:

30.160 in Hg

Average Meter Delta H:

2.000 in H2O

Meter Pressure Pm:

30.307 in Hg

Console Number:

3187

Meter Delta IIa: Mcter Correction Factor:

1.754 0.9730

Average Meter Temperature:

98.7 dcg. F

Average Stack Temperature:

95.3 deg. F

35.2 dcg C

Average Square Root Delta P: 0.316

Meter Volume Vm:

76.15 cu. ft.

Probe Length/Liner:

Cp:

0

Nozzle Ident.:

0.84 0

Nozzle Diameter Dn:

0 in.

Impinger Set Number:

Average Computer K: 30.0000

### Data Page

Facility New Wales			Date:	7/31/98
Plant Multifos Mixed Feed Storage Buildin	g	1	Run 1	
Impinger Set Number:	0			
Impinger Number: 1	2	3		4
Final (grams/mls): 146	110	0	_	342.5
Initial (grams/mls):100	100	<u> </u>	<b>-</b>	325.2
Pilter Set Number:	0			
Filter Analysis	Probe Wash Analysis			
Filter Number:	Besker Number:			
Final Weight	Pinal Weight:			
Initial Weight:	Initial Weight:			÷
Fluoride Probe Wash Fluoride ppm:	Volume ml:	рН		
Impinger Fluoride ppm: 0.4	Volume ml: 370	рН	4.98	
Laboratory Results		·		
Probe Wash Pluoride mg: 0.00				
Impinger Fluoride mg:0.15_				

### Run 1 Data Sheet

Pacility: Now Wales

Plant: Multifos Mixed Feed Storage Building

Team (CB/PR): DC/ML.

Company ID: POEP AIRS & Pt. ID:

7/31/98 Date Mcter Box Number 3187 **Dwell Time** 60 min. Meter Delta IIa (in. H2O) 1.754 Pitot Check Traverse Points Meter Correction Factor 0.973 in H2O pos Nozzle Ident.: in H2O Stack Diameter inches neg 90 % Est % Saturation Nozzlo Diameter Dn: Leak Check 0,000 cfm in H2O Stack Static Pressure Impinger Set Number: cſm Barometric Pressure 30.16 in Hg Probe longth/Liner: 5 in Hg VHC Dry Molecular Weight 28.969 Filter Set Number

Point 1 2	Meter Volume 163.066 205 239.218	Delta P 0.1 0.1 0.1	840 Calc'd Delta H 2.000 2.000 2.000	Actual Delta H 2 2 2	Stack Temp 93 95 98	Probe Temp	Hot Box Temp.	Meter In Temp 84 112 118	Meter Out Temp 84 93 101	Impinger Temp	Pump Vac
End	·	0.1	Avcrage Max Min		95.3	0	0	98.7		#DIV/0! 0	0
		Time End	Range 1040			223-273	223-273	Pitot ( pos neg Leak C cfin vac		<0.020	in H2O in H2O cfm in Hg

### Moisture Data Sheet Method 13B

Facility New Wales	Date	: <b>7</b> /31/98		
Plant Multifos Mixed Food	Run	1		
Impinger Set	Number:	0 .		
Impinger Number:	1	2	3	4
l'inal (grams/mls):	146	110	0	342.5
Initial (grama/mls):	100	100	0	325.2
Difference (grams/mls):	46	10	0	17.3
Total Moisture Collected:			56 mls	17.3 gram
<u>.</u> }				

Fluoride

Laboratory mg

0.15

### Particulate and Moisture Data Sheet Method 5

Plant Multifos Mixed I	Food Storage Build	ing	Run 1		
Impingo	r Sct Number:	0			
Impinger Numbe	er: 1	2	3	4	
Final (grame/mls	): 146	110	o	342.5	
Initial (grams/mls	): 100	100	0	325.2	
Difference (grams/mls	): 46	10	0	17.3	
Total Moisture Collected	<del>i</del> :		56 mls	17.3 gran	
Filter	Sct Number:	0		<del></del>	
Filter Analysis		Probe Wash Analysis			
Filter Number:	o	Beaker Number:	0	·	
Final Weight	0.0000	Final Weight:	0.0000		
Initial Weight:	0.0000	Initial Weight:	0.0000		
Difference:	0.0000	Difference:	0.0000		

### Particulate Calculations

Particulate	Pa	rticu	late
-------------	----	-------	------

Probe Wash Particulate mg 0.0 16 liter Particulate mg: 0.0

Total Particulate mg: 0.0

### Particulate and Moisture Data Sheet Method 5 & 13B Combined

Facility New Wales			Date:	7/31/98
Plant Multifor Mixed Feed	Storage Building		Run 1	
Impinger Set	Number:	0		
Impinger Number:	1	. 2	3	4
Final (grams/mls):	146	110	O	342.5
Initial (grams/mls):	100	100	0	325.2
Difference (grams/mls):	46	10	0	17.3
Total Moisture Collected:			56 mls	17.3 ұянт
: Filter Set 1	Number: 0			
Filter Analysis		Probe Wash Analysis		
Filter Number:	0	Beaker Number:	0	•
Final Weight	0.0000	Final Weight:	0.0000	
Initial Weight:	0.000.0	Initial Weight:	0.0000	
Difference:	0,000,0	Difference;	0,0000	
	Fluoride and l	Particulate Calculation	15	
luoride Probe Wash Fluo	ride mg	0.00	`	
Impinger Fluor		0.15		
articulate	Total Fluoride mg:	0.15		
Probe Wash Particu	late mg	0.0		
Pilter Particul	atc mg:	0.0		
Tota	al Particulate mg:	0.0		

# FCI

# FERTILIZER TECHNICAL DATA BOOK

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uct is dried & screened & the fines are recycled to the granulation unit.

### Run-of-Pile Triple Superphosphate Manufacture

Nongranular superphosphate is commonly produced by continuous den processes followed by a storage curing period of up to 1 month during which chemical reactions are completed. Dens that are suitable for single superphosphate (SSP) are often also suitable for TSP. The main difference is that TSP sets more rapidly than SSP, thus the den retention time can be much shorter. If the retention time is too long, the TSP may become so hard that disintergration is difficult. Depending on the reactivity of the rock and other factors, denning times of 5-20 minutes are suitable for TSP as compared with 30 minutes to 2 hours for SSP.

After storage curing, the TSP usually is reclaimed with a power shovel and disintegrated in a cage mill to pass a 6-mesh screen. Sometimes blasting is necessary to loosen the pile of TSP before reclaiming. The disintegrated TSP may be used for making compound fertilizer by granulation processes, or it may be granulated for direct application.

For mixing of acid & rock many plants use the old TVA cone-mixer which has low mixing efficiency. FCI has designed & built continuous high speed mixers with extraordinary mixing of solids & liquid attaining highest homogeneity of material. The mixed product discharges to a belt conveyor where its retention time is in the range of 5-10 minutes. From there it is conveyed to the storage for final curing.

Cured run-of-pile TSP, 3-6 weeks old, is removed from storage and fed to a screen. The oversize is milled and recycled; the fine material is conveyed to a pugmill or rotary-drum granulator. Water is sprayed onto the bed of material, and steam is sparged underneath the bed to provide wet granular material. The wet granules are discharged to a rotary dryer. The dried granules are screened. The oversize is milled and returned with the fines to the granulator. Dust and fumes from the dryer are scrubbed in a water scrubber.

effect of Grade & P<sub>2</sub>O<sub>5</sub>: CaO Ratio of Rock on Proportions of Rock & Phosphoric Acid & on Grade of TSP

Wt. ratio	%P_2	o <sub>s in</sub>	Tons/	ton of	. %	P205
P205:CaO	produc	t from	produc	et P <sub>2</sub> O <sub>5</sub>		
in rock	rock	acid		acid	rock	product
0.588	24.0	76.0	0.73	1.40	33	47.0
0.666	27.0	73.0	0.82	1.35	33	46.1
0.740	30.2	69.8	0.92	1.29	33	45.2
0.666	27.0	73.0	0.96	1.35	28	43.0

Phosphoric acid 54% P205

# Requirements per short ton of granulor TSP made from run-of-pile and other data

Rock (72 BPL), ton	0.43
Acid (54% P <sub>2</sub> O <sub>5</sub> ), ton	0.61
Steam (25 psig minimum), lbs.	147
Fuel, Btu.	570,000
Electricity, KWH	26

### DEFLUORINATED PHOSPHATE ROCK

Most of the phosphorus in phosphate rock is present as fluorapatite,  $Ca_{10}(PO_4)_6F_2$ , a compound so stable that its phosphours cannot be utilized readily by plants or animals. Methods for the processing of phosphate rocks into animal feed supplement are designed to break that the phosphorus-fluorine fluorapatite structure 50 combination is disrupted & the phosphorus appears in a compound in which it is readily available to animal. The nutrient value of defluorinated phosphate rock, 18% P & 32% Ca(min.), is related more or less directly to the 2% citric acid solubility of the P2O5.

In defluorinating phosphate rock a mixture of ground phosphate rock 72-75 BPL (80% - 200 mesh), wet phosphoric acid (50-54%  $P_2O_5$ ) & sodium hydroxide (50%) or sodium carbonate is granulated in a pugmill & is introduced directly into a rotary kiln. However, it is preferable to dry the moist granules in a dryer & subsequently screened to uniform size. Due to structural strength & uniform size, these granules exhibit excellent flow characteristics as they progress through a kiln & are particularly suitable for use in a fluidized bed reactor. Rocks with high  $Al_2O_3$  (over 2%) must be avoided. Aluminum has great affinity for fluorine, therefore, it retards defluorination.

The factors influencing the defluorination of the mixture are; type of calciner, calcination time & temperature, particle size, the interacy of contact between the particles & gaseous atmosphere, particle porosity, gas velocity & water vapor atmosphere. In general the retention period of the mixture in a rotary kiln is between about 90 to 120 minutes, & in a fluidized bed reactor is between about 60 to 90 minutes.

)

Recommended formula for producing defluorated phosphate rock, in presence of water vapor, with high availability & P:F ratio over 100 is:

 $\frac{\text{Mols CaO+Na}_2\text{O-3P}_2\text{O}_5}{\text{Mols SiO}_2} < 1.1 \text{ (preferable between 0.4 to 0.8)}$ 

Also, the compounds added to the rock should be proportioned so that the:

 $Na_2O/acid P_2O_5$  is between 0.5-0.8

Acid  $P_2O_5$  to the mix is 7-12% of the dry mix

Total  $Na_2O$  added to the mix is 0.3-0.7 mol per mol  $P_2O_5$  in the rock

The SiO, content of the dry mix is about 2-6%

### REACTION

The simplest possible mechanism of the chemical reaction involved in making defluorinated phosphate rock for animal feed supplement from the raw materials; rock, phosphoric acid & sodium hydroxide or sodium carbonate are shown below:

(1) 3Ca <sub>3</sub> (PO <sub>4</sub> ) <sub>2</sub> .CaF <sub>2</sub> +H <sup>+</sup>	<del></del>	3Ca <sub>3</sub> (PO <sub>4</sub> ) <sub>2</sub> +CaF <sub>2</sub>
(2) CaF <sub>2</sub> +H <sub>2</sub> O		Ca(OH) <sub>2</sub> +2HF
(3) 3Ca(OH) <sub>2</sub> +2H <sub>3</sub> PO <sub>4</sub>	-	Ca <sub>3</sub> (PO <sub>4</sub> ) <sub>2</sub> +3H <sub>2</sub> O
(4) 2NaOH		Na20+H20
(5) 3Ca <sub>3</sub> (PO <sub>4</sub> ) <sub>2</sub> +Na <sub>2</sub> O+H <sub>2</sub> O		Ca <sub>9</sub> (PO <sub>4</sub> ) <sub>6</sub> .(NaOH) <sub>2</sub> Sodium Hydroxyapatite

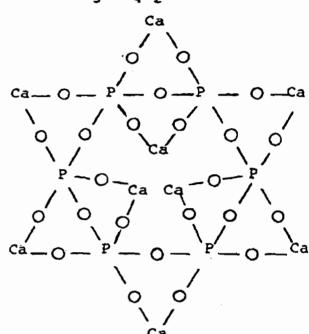
From the above reactions it is evident that defluorination takes place in accordance with reactions No. (1) and (2). The factors involved in the defluorination of phosphate rock are:

- a) Break-up of crystal lattice of the apatite by H
- b) Exposure of material to stream of hot gases in presence of  $\rm H_{2O}$ , for about 1-2 hours at 2300°F to 2700°F.

c) Particle size & particle porosity.

### STRUCTURAL FORMULAS

a- Tricalcium phosphate 3Ca3(PO4)2

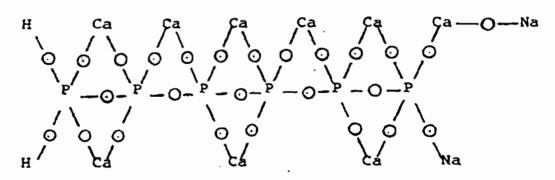


Ca/P = 1.935 wt. ratio

%P = 20.0

%Ca = 38.7

b- Sodium hydroxyapatite Ca<sub>9</sub>(PO<sub>4</sub>)<sub>6</sub>(NaOH)<sub>2</sub>



Ca/P = 1.935 wt. ratio

P = 18.4

2Ca = 35.6

 $8Na_2O = 6.1$ 

### RECOMMENDED RAW MATERIAL PER TON PRODUCT

1- 1835 1bs. of 72 BPL rock (80%-200 mesh)

2- 393 lbs. of 52% P<sub>2</sub>O5 acid

3- 335 lbs. of 50% sodium hydroxide or 222 lbs of sodium carbonate. 40%  $P_2O_5$  acid should be used when sodium carbonate is added.

Mol. ratio Calculation for rock having 32.90%  $P_2O_5$ , 48.00% CaO & 6.30% SiO<sub>2</sub>;

CaO 
$$1835\frac{0.48}{56}$$
 = 15.73 mols

$$P_2O_5 = 1835\frac{0.329}{142} + 393\frac{0.52}{142} = 5.69 \text{ mols}$$

$$Na_2O = 335 \frac{0.5}{2x40} = 2.09 \text{ mols}$$

$$SiO_2$$
 1835 $\frac{0.063}{60}$  = 1.93 mols

mol, ratio = 
$$\frac{15.73+2.09-3x5.69}{1.93} = 0.39$$

#### PRODUCT ANALYSIS

P 18.0%, Ca 32% (min.), Na<sub>2</sub>0 7% & Sio<sub>2</sub> 2%

### **PROCESS**

Defluorinated phosphate rock plant is comprised of three separate sections;

- a) Feed preparation (Fig. 1)
- b) Defluorionation Fluid bed (Fig. 2) or kiln (Fig. 3)
- c) Product sizing (Fig. 4)

### ATTACHMENT 2

### MODIFICATION DETERMINATION

As explained to FDEP, the two existing kilns will not be modified or debottlenecked. The existing mixed feed operation is capable of supplying much more material than the existing kilns can process. This surge capacity, accomodated by the storage area, is necessary to allow equipment maintenance and repair in the mixed feed operation, unlike the kilns which operate continuously. There is a definite process disconnect at storage as the material sits for a couple of days to dry. There are separate conveyors and hoppers for each kiln and these supply the kilns continuously with material from storage, for independent kiln operation. Currently, the kilns themselves are the production bottleneck. It should be noted that because the two existing kilns are not being modified, the current bottleneck will remain.

The proposed pugmill will also be operated intermittently, capable of material supply to storage well beyond the kiln capacities. This aspect of the operation will allow for the same maintenance and repair requirements. The existing kilns are not being modified and will be operated no differently as a result of the proposed project. IMC-Agrico is not opposed to recordkeeping of the material processing rates in order to document this fact. Therefore, the existing kilns are not part of the proposed modification.

This assessment is supported by guidance in mid-1980s from Wayne Aronson of EPA to Clair Fancy, Bill Thomas and Pradeep Raval, of FDEP, to exclude independent process units from modification considerations when the associated units have existing federally enforceable operation caps. While the guidance was not in the form of a letter or memorandum, this approach is logical, practical and allows for a common sense approach to PSD applicability determinations of site modifications. We are not aware of any change in EPA position on this issue.

For example, adding molten sulfur storage tanks for increased surge capacity to an existing sulfuric acid plant would not trigger PSD for the sulfuric acid plant as it would be capable of independent operation and have existing federally enforceable operation caps.

Also, in the case of a power plant with four existing coal fired units producing 1000 MW which adds an additional unit to increase site capacity to 1250 MW. the modification would address the additional unit and the

changes to the existing coal handling operation, not all five units at the site. This is because the existing four units would be capable of independent operation and have existing federally enforceable operation caps.

### ATTACHMENT 3

AVAILABLE FDEP CORRESPONDENCE
ON PAST MULTIFOS PERMITTING ACTIONS

- A. COPY OF PERMIT AC53-40084
- B. PERMIT MODIFICATION IN 1981
- C. COPY OF PERMIT AC53-267287



ITEM A

BOB GRAHAL

STATE OF FLORIDA

### DEPARTMENT OF ENVIRONMENTAL REGULATION

### SOUTHWEST DISTRICT

Polk County AP

Mr. T. H. Traylor, V.P. & Gen. Mgr. International Minerals & Chemical Corp. P.O. Box 1035 Mulberry, Fla. 33860

Dear Mr. Traylor:

	sed is Perm				3-40084	_ dated	May 18,	1981	,
	construct								
issued	pursuant	to	Section	40	,	Florida	Statutes.		

Should you object to this permit, including any and all of the conditions contained therein, you may file an appropriate petition for administrative hearing. This petition must be filed within fourteen (14) days of the receipt of this letter. Further, the petition must conform to the requirements of Section 28-5.201, Florida Administrative Code, (see reverse side of this letter). The petition must be filed with the Office of General Counsel, Department of Environmental Regulation, Twin Towers Office Building, 2600 Blair Stone Road, Tallahassee, Florida 32301.

If no petition is filed within the prescribed time, you will be deemed to have accepted this permit and waived your right to request an administrative hearing on this matter.

Acceptance of the permit constitutes notice and agreement that the Department will periodically review this permit for compliance, including site inspections where applicable, and may initiate enforcement action for violation of the conditions and requirements thereof.

Sincerely,

cc: Record Center C.A. Pflaum, P.E.

Enclosure ·

W.K. Hennessey District Manager

DER Form 17-1.122(66) Page 1 of 2

ביי אינו פינו פאר בעריעב ביין ווער אבט וביי יינו אוני אוני אוני איני עב אינייעב ביין אינייעב אבט וביי

## RULES OF THE ADMINISTRATION COMMISSION MODEL RULES OF PROCEDURE CHAPTER 28-5 DECISIONS DETERMINING SUBSTANTIAL INTERESTS

### PART II FORMAL PROCEEDINGS

### 28-5.201 Initiation of Formal Proceedings.

- (1) Initiation of formal proceedings shall be made by petition to the agency responsible for rendering final agency action. The term petition as used herein includes any application or other document which expresses a request for formal proceedings. Each petition should be printed, typewritten or otherwise duplicated in legible form on white paper of standard legal size. Unless printed, the impression shall be on one side of the paper only and lines shall be double-spaced and indented.
- (2) All petitions filed under these rules should contain:
  - (a) The name and address; of each agency affected and each agency's file or identification number, if known;
  - (b) The name and address of the petitioner or petitioners, and an explanation of how his/her substantial interests will be affected by the agency determination;
  - (c) A statement of when and how petitioner received notice of the agency decision or intent to render a decision;
  - (d) A statement of all disputed issues of material fact. If there are none, the petition must so indicate;
  - (e) A concise statement of the ultimate facts alleged, as well as the rules and statutes which entitle the petitioner to relief;
  - (f) A demand for relief to which the petitioner deems himself entitled; and
  - (g) Other information which the petitioner contends is material.

#### \*\*\*\*\*\*

A petition may be denied if the petitioner does not state adequately a material factual allegation, such as a substantial interest in the agency determination, or if the petition is untimely. (Section 28-5.201(3)(a), FAC)

#### STATE OF FLORIDA

### DEPARTMENT OF ENVIRONMENTAL REGULATION

**SOUTHWEST DISTRICT** 

7601 HIGHWAY 301 NORTH TAMPA, FLORIDA 33610



DISTRICT MANAGER

**BOB GRAHAM** 

APPLICANT:

PERMIT/CERTIFICATION

International Minerals & Chemical Corp.

P.O. Box 1035

Mulberry, Fla. 33860

NO. AC53-40084

COUNTY: Polk

PROJECT: Multiphos

Scrubbers

This permit is issued under the provisions of Chapter 403, Florida Statutes, and Chapter 17-2, Florida Administrative Code. The above named applicant, hereinafter called Permittee, is hereby authorized to perform the work or operate the facility shown on the approved drawing(s), plans, documents, and specifications attached hereto and made a part hereof and specifically described as follows:

For the construction/modification of the multifos kilns and dryer scrubbers to increase production from 14 TPH to 25 TPH with resulting offsets to DAP plant #1 and the GTSP storage scrubber to allow for particulate emission increase.

Located at Hwy 640, at Hillsborough/Polk County Line, Polk County.

UTM: 17-396.7E and 3079.4N

Replaces Permit NO: A053-16903 NEDS NO: 0059 Point ID: 36

Expires: May 1, 1982

PAGE \_\_\_\_ OF \_\_\_4

PERMIT NO .:

AC53-40084

APPLICANT:

International Minerals & Chemical Corp.

#### **GENERAL CONDITIONS:**

- 1. The terms, conditions, requirements, limitations, and restrictions set forth herein are "Permit Conditions:, and as such are binding upon the permittee and enforceable pursuant to the authority of Section 403.161(1). Florida Statutes. Permittee is hereby placed on notice that the department will review this permit periodically and may initiate court action for any violation of the "Permit Conditions" by the permittee, its agents, employees, servants or representatives.
- 2. This permit is valid only for the specific processes and operations indicated in the attached drawings or exhibits. Any unauthorized deviation from the approved drawings, exhibits, specifications, or conditions of this permit shall constitute grounds for revocation and enforcement action by the department.
- 3. If, for any reason, the permittee does not comply with or will be unable to comply with any condition or limitation specified in this permit, the permittee shall immediately notify and provide the department with the following information: (a) a description of and cause of non-compliance; and (b) the period of non-compliance, including exact dates and times; or, if not corrected, the anticipated time the non-compliance is expected to continue, and steps being taken to reduce, eliminate, and prevent recurrence of the non-compliance. The permittee shall be responsible for any and all damages which may result and may be subject to enforcement action by the department for penalties or revocation of this permit.
- 4. As provided in subsection 403.087(6), Florida Statutes, the issuance of this permit does not convey any vested rights or any exclusive privileges. Nor does it authorize any injury to public or private property or any invasion of personal rights, nor any infringement of federal, state or local laws or regulations.
- 5. This permit is required to be posted in a conspicuous location at the work site or source during the entire period of construction or operation.
- 6. In accepting this permit, the permittee understands and agrees that all records, notes, monitoring data and other information relating to the construction or operation of this permitted source, which are submitted to the department, may be used by the department as evidence in any enforcement case arising under the Florida Statutes or department rules, except where such use is proscribed by Section 403.111, F.S.
- 7. In the case of an operation permit, permittee agrees to comply with changes in department rules and Florida Statutes after a reasonable time for compliance, provided, however, the permittee does not waive any other rights granted by Florida Statutes or department rules.
- 8. This permit does not relieve the permittee from liability for harm or injury to human health or welfare, animal, plant, or aquatic life or property and penalities therefore caused by the construction or operation of this permitted source; nor does it allow the permittee to cause pollution in contravention of Florida Statutes and department rules, except where specifically authorized by an order from the department granting a variance or exception from department rules or state statutes.
- 9. This permit is not transferable. Upon sale or legal transfer of the property or facility covered by this permit, the permittee shall notify the department within thirty (30) days. The new owner must apply for a permit transfer within thirty (30) days. The permittee shall be liable for any non-compliance of the permitted source until the transferee applies for and receives a transfer of permit.
- 10. The permittee, by acceptance of this permit, specifically agrees to allow access to permitted source at reasonable times by department personnel presenting credentials for the purposes of inspection and testing to determine compliance with this permit and department rules.
- 11. This permit does not indicate a waiver of or approval of any other department permit that may be required for other aspects of the total project.
- 12. This permit conveys no title to land or water, nor constitutes state recognition or acknowledgement of title, and does not constitute authority for the reciamation of submerged lands unless herein provided and the necessary title or lessehold interests have been obtained from the state. Only the Trustees of the Internal Improvement Trust Fund may express state opinion as to title.
- 13. This permit also constitutes:

  ( ) Determination of Best Available Control Technology (BACT)

  [ ) Determination of Prevention of Significant Deterioration (PSD)

[ | Certification of Compliance with State Water Quality Standards (Section 401, PL 92-500)

PAGE	2	OF	4
PAGE		_ OF _	

PERMIT NO.: AC53-40084

APPLICANT: International Minerals & Chemical Corp.

#### SPECIFIC CONDITIONS:

- 1. Construction of this installation shall be completed by 2/28/82. Application for Permit to Operate to be submitted by 3/30/82. (Chapter 17-4.07(7), F.A.C.)
- 2. This construction permit expires on 05/01/82 following an initial period of operation for appropriate testing to determine compliance with the Rules of the Florida Dept. of Environmental Regulation Commission. (Chapter 17-4.07(7), F.A.C.)
- 3. All applicable rules of the Department including design discharge limitations specified in the application shall be adhered to. The permit holder may also need to comply with county, municipal, federal, or other state regulations prior to construction. (Chapter 17-4.07(1), F.A.C.)
- 4. Test for particulates and fluorides at an input production rate of 30 TPH, raw materials per Chapter 17-2, F.A.C. At this maximum process rate, the limit of particulate emissions will be 29.83 lbs/hr and fluoride emissions not to exceed 4.2 lbs/hr (NSPS standard of 0.37 #/ton P2O5).

PERMIT NO .: AC53-40084

APPLICANT: International Minerals & Chemical Corp.

May 1, 1982 **Expiration Date:** Pages Attached.

STATE OF FLORIDA
DEPARTMENT OF ENVIRONMENTAL REGULATION

Signature

W.K. Hennessey District Manager

#### STATE OF FLORIDA

### DEPARTMENT OF ENVIRONMENTAL REGULATION

SOUTHWEST DISTRICT

7601 NIGHWAY 301 NORTH TAMPA FLORIDA 33610





GOVERNOR XMROBOXXXX SECRETARY DISTRICT MANAGER

BOB GRAHAM

May 18, 1981

Mr. T. H. Traylor, V.P. & Gen. Mgr. International Minerals & Chemical Corp. P.O. Box 1035 Mulberry, Fla. 33860

Dear Mr. Traylor:

Modification of Conditions Permit No. A053-36916

We are in receipt of your request for a modification of the permit conditions. The conditions are changed as follows:

Condition

From

T'O

No. 4

particulates 36.3 lbs/hr 28.6 lbs/hr

Add: "This change is part of the required offset necessitated by the increase in production of the multifos plant."

This letter must be attached to your permit and becomes a part of that permit.

Robert R. Garrett

Air Engineer

RRG/rkt



### Department of BEST AVAILABLE COPY

### **Environmental Protection**

Southwest District 3804 Coconut Palm Drive Tampa, Florida 33619

Lawton Chiles Governor

PERMITTEE:

P.O. Box 2000

IMC-Agrico Company

New Wales Operation

Mulberry, Florida 33860

PERMIT/PROJECT:

Permit: AC53-267287

County: Polk

Expiration Date: 06/01/97

Project: Multifos Product ion Plant:

Dryer, Blending and Storage Operation, Kiln 'A' & Kiln 'B'

This permit is issued under the provisions of Chapter 403, Florida Statutes, and Florida Administrative Code Rules 62-200 through 297 and 62-4. The above named permittee is hereby authorized to perform the work or operate the facility shown on the application and approved drawing(s), plans and other documents, attached hereto or on file with the Department and made a part hereof and specifically described as follows:

This permit is issued for a portion of the Multifos Production Plant consisting of a phosphate rock dryer, a blending operation, and two defluorination kilns designated as Kiln 'A' (North), and Kiln 'B' Emissions from the dryer, the blending operation and the kilns are controlled by three separate Teller packed bed scrubbers connected to a common stack.

The dryer has the capability of processing 35 tons per hour of wet phosphate rock and is fired at a maximum heat input rate of 12.5 MMBtu per hour with either natural gas or new, No. 6 or a better grade fuel oil. The dried phosphate rock is normally stored in a hopper prior to the blending operation.

The blending operation is a batch operation which combines the dried phosphate rock with soda ash and a phosphoric acid into a mixed feed which is then sent to the mixed feed storage building for a period of time in order to age.

From storage, the mixed feed is transferred to the common kiln feed conveyor at a maximum rate of 11.35 tons per hour 100% P2Os (approximately 30 tons per hour mixed feed rate). Each kiln is capable of being fired at a maximum heat input rate of 56 MMBtu per hour by either natural gas, on-specification used oil from on-site sources, only, or new, No. 6 or a better grade fuel oil.

Emissions from both the dryer and the batch blending operation are controlled by the same scrubber. Emissions from each kiln are controlled by a separate scrubber.

Page 1 of 8

"Protect, Conserve and Manage Florido's Environment and Natural Resources"

Printed on recycled paper.

Location: New Wales Operations, Highway 640 and County Line

Road South of Mulberry

UTM: 17-396.7 km East 3078.9 km North

NEDS No: 0059 Point ID: 36

Facility ID: 40TPA530059

Replaces Permit: AC53-40084 and AC53-5132

Modifies Permit: A053-206083

#### SPECIFIC CONDITIONS:

1. A part of this permit is the attached GENERAL CONDITIONS.

2. Issuance of this permit does not relieve the permittee from complying with applicable emission limiting standards or other requirements of Chapters 62-2 through 62-297, F.A.C. or any other requirements under federal, state or local law.
[Rule 62-200.300, F.A.C.]

### EMISSION LIMITATIONS

- 3. The particulate matter emission rate from the stack common to the Multifos Production Plant dryer, batch blending operation, kiln 'A' and kiln 'B' scrubbers shall not exceed 29.83 pounds per hour. This particulate matter emission rate limitation qualifies the facility for the PM-RACT exemption per Rule 62-296.700(2)(b), F.A.C. [Permit AC53-40084, Rules 62-296.310(1) and 62-296.700(2)(b), F.A.C.]
- 4. The fluoride emission rate from the stack common to the Multifos Production Plant dryer, batch blending operation, kiln 'A' and kiln 'B' scrubbers shall not exceed 4.2 pounds per hour as fluorides (water soluble or gaseous atomic weight 19). At a total, combined input rate to the kilns of less than 11.35 tons per hour  $100\% P_2O_5$  (approximately 30 tons per hour mixed feed rate), the maximum allowable fluoride emission rate is 0.37 pounds per ton  $100\% P_2O_5$  input. [Permit AC53-40084 and Rule 62-296.403(1)(h), F.A.C.]
- 5. Visible emissions shall not be equal to or greater than 20% opacity. [Rule 62-296.310(2)(a), F.A.C.]

Allowable

SPECIFIC CONDITIONS: (Continued)

### OPERATION LIMITATIONS

- 6. The fuels burned shall be limited to those shown below:
  - A. Dryer
    - i. natural gas; or
    - ii. new, No. 6 fuel oil, or better grade fuel oil. (1)
  - B. Kilns
    - i. natural gas; or

Constituent/Property

- ii. on-specification used oil<sup>(2)</sup> (generated on-site, only, see Specific Condition No. 7); or
- iii. new, No. 6 fuel oil, or better grade fuel oil. (1)

[Permit A053-206083 and request by KOOGLER & ASSOCIATES, March 14, 1995]

7. The used oil (generated on-site, only) to be fired in the kilns shall meet the following on-specification used oil requirements:

Cadmium	2	ppm	maximum	
Arsenic			maximum	
Chromium	10	ppm	maximum	٠.
Lead	100	ppm	maximum	
Total Halogens	1000	ppm	maximum	#
Polychlorinated Byphenyls(PCB's)	50		maximum	
Flash Point	100	·F	minimum	

\* Used oil containing more than 1000 ppm and up to a maximum of 4000 ppm total halogens can be burned only if the permittee can show that the used oil does not contain any halogenated hazardous wastes.

[Federal Specifications contained in 40 CFR 266.40].

- 8. Each batch of used oil collected for use as fuel shall be sampled and analyzed for all of the constituents/properties listed in Specific Condition No. 7 using EPA/DEP or ASTM approved methods. Split samples of the used oil shall be retained for 3 months after the analysis for further testing if necessary. The results of each analysis shall be retained for at least 5 years and made available to the Department of Environmental Protection upon request. If used oil is being fired during the stack test then results of the most recent batch analysis shall be submitted along with the test report. [Rule 62-4.070(3), F.A.C. and A053-127484]
- 9. The sources covered by this permit are allowed to operate continuously (8760 hours per year). [Permit AC53-5132]

10. The total, combined input rate to the kilns shall not exceed 11.35 tons per hour 100%  $P_2O_5$  (approximately 30 tons per hour mixed feed rate). [Based on 4.2 pounds per hour maximum fluoride emission rate, permit AC53-40084]

#### TESTING AND COMPLIANCE REQUIREMENTS

- 11. Test the stack common to the Multifos Production Plant dryer, batch blending operation, kiln 'A' and kiln 'B' scrubbers, annually, for particulate matter emissions, fluoride emissions and visible emissions. The due date for the annual test will be set by the operation permit for this emission unit. [Rules 62-297.340(1)(a), and 62-297.570(3), F.A.C. and request by KOOGLER & ASSOCIATES, March 14, 1995]
- 12. Compliance with the emission limitations of Specific Condition Nos. 3, 4, and 5 shall be determined using EPA Methods 1, 2, 3, 4, 5, 9, and 13A or 13B as contained in 40 CFR 60, Appendix A and adopted by reference in Chapter 62-297, F.A.C. The minimum requirements for stack sampling facilities, source sampling and reporting, shall be in accordance with Chapter 62-297, F.A.C. and 40 CFR 60, Appendix A.
- 13. The visible emissions test shall be conducted by a certified observer and be a minimum of 60 minutes in duration. The test observation period shall include the period during which the highest opacity emissions can reasonably be expected to occur. A visible emissions test shall be conducted during the same testing period as the particulate matter test and the fluoride emission test.

  [Rules 62-297.330(1)(b), and 62-4.070, F.A.C.]
- 14. Testing of emissions should be accomplished while simultaneously operating within 90% 100% of each of the following:
- (1) the maximum total, combined input rate to the kilns of 11.35 tons per hour 100%  $P_2O_5$  (approximately 30 tons per hour mixed feed rate).
- (2) the maximum heat input rate to the dryer of 12.5 million Btu per hour.
- (3) the maximum heat input rate for each of the kilns of 56.0 million Btu per hour.

(Specific Condition No. 14, Continued on Next Page)

### 14. (Continued)

- If it is not practical to test at the maximum rates in (1), (2) or (3), above, then the source may be tested at less than the maximum rates. In this case, subsequent source operation is then limited to 110 percent of the test rate(s) until a new test is conducted. Once the source is so limited, then operation at a higher rate is only allowed for no more than 15 consecutive days for the purpose of additional compliance testing in order to regain a maximum permitted rate in this permit. Acceptance of a test by the Department of Environmental Protection will automatically amend this permit to the new rate(s), plus 10%, but shall not exceed the maximum rates in (1) through (3), above. Failure to submit the actual rates, the type of fuel burned, or operating under conditions during testing which are not representative of normal operating conditions, may invalidate the test. [Rules 62-297.340 and 62-4.070(3), F.A.C.]
- 15. Compliance testing shall be conducted while firing oil, if oil of any type (new, fuel oil, or on-specification used oil), has been used in the rock dryer and/or the kilns for a sum total of more than 400 hours from the previous test. If a test is conducted while firing natural gas, and in the 12 month period following the test, oil of any type is burned for a sum total of more than 400 hours, then an additional visible emission test per Specific Condition No. 5 shall be conducted, while burning oil in that source, within 30 days of having exceeded the 400 hour oil burning limit. A compliance test submitted using a better grade of oil, than No. 6 grade, will automatically amend the operation permit to only allow subsequent operation on only that better grade oil or a higher ranked oil.

  [Rules 62-297.340(2), and 62-4.070(3), F.A.C.]

### NOTIFICATION REQUIREMENTS

- 16. In case of excess emissions resulting from a malfunction, IMC-Agrico Company shall immediately notify the Air Compliance Section of the Southwest District Office of the Department of Environmental Protection in accordance with Rule 62-4.130, F.A.C. If requested, IMC-Agrico Company shall submit a full written report on the malfunction. [Rule 62-210.700, F.A.C.]
- 17. The permittee shall notify the Air Compliance Section of the Southwest District Office of the Department of Environmental Protection at least 15 days prior to the date on which each formal compliance test is to begin of the date, time, and place of each test, and the test contact person who will be responsible for coordinating the test. [Rule 62-2.700(2)(a)9., F.A.C.]

### RECORDKEEPING REQUIREMENTS

- 18. A record log(s) shall be established and maintained to document, at a minimum, the following:
- (1) the quantity of the new, fuel oil and the on-specification used oil utilized in the dryer and the kilns.
- (2) the sulfur content (percent, by weight) of the new, fuel oil and the on-specification used oil utilized in the dryer and the kilns.

The log(s) shall be updated, at a minimum, on a monthly basis and shall be retained at the facility for a minimum of 5 years. The log(s) shall be made available to the Department of Environmental Protection, upon request. [Permit A053-206083 Amendment, 06/23/94 and Rules 62-4.070(3), and 62-213.440(b)2.b., F.A.C.]

#### OTHER REQUIREMENTS

19. Reasonable precautions shall be taken to prevent and control generation of unconfined emissions of particulate matter in accordance with the provision in Rule 62-296.310(3), F.A.C. These provisions are applicable to any source, including, but not limited to, vehicular movement, transportation of materials, construction, alterations, demolition or wrecking, or industrial related activities such as loading, unloading, storing and handling.

### REPORTING REQUIREMENTS

20. Submit to the Southwest District Office, Air Compliance Section of the Department of Environmental Protection, each calendar year, on or before March 1, completed DEP Form 62-210.900(5), Annual Operating Report for Air Pollutant Emitting Facility, including the "Emissions Report", for the preceding year. Include in this report the total quantity of all fuels utilized, including a summary of the range of analysis values for each constituent/property referenced in Specific Condition Nos. 7 and 8. [Rule 62-210.370(3), F.A.C.]

21. All tests reports shall be submitted to the Air Compliance Section of the Southwest District Office of the Department of Environmental Protection within 45 days of testing. Each report shall reference, at a minimum, the "Project", "Facility ID" and "Point ID". The following information, or equivalent, shall be included in each report submitted:

Project: Multifos Production Plant: Dryer, Blending and Storage

Operations, and Kiln 'A' & Kiln 'B'

Facility ID: 40TPA530059

Point ID: 36

[Rules 62-297.570(2) and 62-4.070, F.A.C.]

### PERMITTING REQUIREMENTS

22. IMC-Agrico Company is subject to the permitting requirements of Rule 62-213.400 and shall apply for a Title V operation permit by submitting a completed application, DEP Form 62-210.900(1), to the Air Permitting Section of the Southwest District Office of the Department of Environmental Protection by the appropriate date referenced in Rule 62-213.420(1)(a), F.A.C.

STATE OF FLORIDA DEPARTMENT OF ENVIRONMENTAL PROTECTION

Richard D. Garrity, Ph.D.

Director of District Management

Southwest District

5imc287c.pmt(2)

### DEFINITIONS:

### (1) Better Grade Fuel Oil

A better grade fuel oil is defined as a fuel oil with a higher ranking in the following list:

### Better Grade (Top of list)

```
new, No. 2 fuel oil, or No. 2 on-specification fuel oil new, No. 3 fuel oil, or No. 3 on-specification fuel oil new, No. 4 fuel oil, or No. 4 on-specification fuel oil new, No. 5 fuel oil, or No. 5 on-specification fuel oil new, No. 6 fuel oil, or No. 6 on-specification fuel oil
```

### (2) "On-Specification" Used Oil

"On-specification" used oil is defined as used oil that meets all of the requirements in Specific Condition Nos. 7 and 8 in this permit. Used oil that does not meet all the requirements of Specific Condition Nos. 7 and 8 in this permit is defined as "off-specification" used oil and shall not be burned.

# ATTACHMENT 4

SUMMARY OF MODELING RESULTS USING NEW STACK FOR NEW KILN

# ALTERNATE AIR QUALITY MODELING PARAMETERS MULTIFOS PLANT EXPANSION

# IMC-AGRICO COMPANY (NEW WALES) POLK COUNTY, FLORIDA

Stack	Pollutant	Emissions (g/s)	Ht (m)	Dia (m)	Vel Temp (mps) (°K)
Kiln	PM SO2 NOx	1.80 1.10 1.90	52.4	0.91	18.00 314
Cooler	PM	0.79	26.2	0.91	32.30 394
Screen & Mills	РМ	0.23	27.44	0.46	34.45 327

### NOTES:

(1) Proposed alternate parameters, with a new Kiln C stack.

### SUMMARY OF SIGNIFICANT IMPACT ANALYSES FOR PM/PM10, SO2 and NOx USING ALTERNATE AIR QUALITY MODELING PARAMETERS

MET	MAX. PREDICTED AMBIENT AIR IMPACTS (ug/m3) (1) PM10 SO2 NOx								
YEAR	24-hr	Annual	3-hr	24-hr	Annual	Annua 1			
CLASS I AREA IMPACTS									
1987	0.08	0.002	0.11	0.02	0.001	0.001			
1988	0.07	0.003	0.10	0.02	0.001	0.002			
1989	0.07	0.005	0.11	0.03	0.002	0.003			
1990	0.06	0.002	0.12	0.02	0.001	0.001			
1991	0.05	0.002	0.09	0.02	0.001	0.001			
EPA SIG. (2)	0.3	0.2	1.0	0.2	0.1	0.01			
SIGNIFICANT?	NO	NO	NO	NO	NO	NO			
CLASS II AREA IMPA	ACTS								
1987	6.5	0.54	11.0	3.1	0.22	0.38			
1988	5.2	0.35	8.9	1.9	0.14	0.24			
1989	7.3	0.54	11.2	2.9	0.17	0.30			
1990	7.6	0.53	10.1	3.4	0.20	0.34			
1991	6.8	0.51	11.2	2.7	0.21	0.36			
EPA SIG.(2)	5	1	25	5	1	1			
SIGNIFICANT?	YES	NO	NO	NO	NO	NO			

NOTES:(1) The above impacts represent the highest-high impacts from the proposed project.

<sup>(2)</sup> Significant impact levels proposed by EPA.

<sup>(3)</sup> Above impacts predicted when using a new Kiln C stack.

### SUMMARY OF REFINED MODELING ANALYSES FOR PM10 USING ALTERNATE AIR QUALITY MODELING PARAMETERS

MET YEAR	MAX. PREDICTED AMBIENT AIR IMPACTS (ug/m3) (1)  PM10 24-hr
FAAQS ANALYSIS	
1987	59.4
1988	41.4
1989	54.7
1990	73.5
1991	64.2
MAXIMUM w/Bkgd.	94.5
FAAQS	150
STD. EXCEEDED?	NO
CLASS II PSD INCRE	MENT ANALYSIS
1987	25.1
1988	15.7
1989	24.9
1990	26.6
1991	26.3
INCREMENT	30
EXCEEDED?	NO

### NOTES:

- (1)
- The above impacts represent the highest-second high impacts. A background concentration of 21 ug/m3 for PM10 is included. Above impacts predicted when using a new Kiln C stack. (2)
- (3)

THIS DISK CONTAINS SULFUR DIOXIDE (SO2) AND PARTICULATE MATTER (PM10) AND OXIDES OF NITROGEN (NOX) MODELING FILES FOR THE IMC NEW WALES PHOSPHATES FACILITY IN NEW WALES FLORIDA. THE FOLLOWING FILES ARE IN SELF EXTRACTING ARCHIVE FORMAT.

C1ASI.EXE 102,796 08-10-98 CLASS 1 SIGNIFICANT IMPACT ANALYSIS (SIA)
C2ASI.EXE 499,592 08-10-98 CLASS 2 SIGNIFICANT IMPACT ANALYSIS
C2&FQS.EXE 157,854 08-10-98 CLASS 2 INCREMENT & AIR QUALITY STANDARD
DYRNG.EXE 25,390 08-10-98 DAYS & RECEPTORS OF SIGNIFICANT IMPACT
NW-DWNWH.EXE 21,491 01-08-98 BPIP BUILDING WAKE EFFECT

TO UNARCHIVE THESE FILES COPY THEM TO A HARD DISK DRIVE AND TYPE THE FILE NAME. FOR EXAMPLE TO UNARCHIVE THE CLASS 1 SIA ISCST3 OUTPUT FILES, TYPE "C1ASI" AND PRESS ENTER. THE FILES WILL AUTOMATICALLY UNARCHIVE TO THE HARD DISK DRIVE. THESE ARCHIVED FILES CONTAIN THE MODELING AND ANALYSIS FILES IN ASCII AND LOTUS FORMAT DESCRIBED AS FOLLOWS;

IN THE FILE C1ASI.EXE IS ISCST3 MODELING OF SIGNIFICANT IMPACT (SIA) FOR CHASSAHOWITZKA NWR PSD CLASS 1 AREA.

C1N87.OUT	29,532	08-07-98	NOX MODELING FOR 1987
C1N88.OUT	29,532	08-07-98	NOX MODELING FOR 1988
C1N89.OUT	29,532	08-07-98	NOX MODELING FOR 1989
C1N90.OUT	29,532	08-07-98	NOX MODELING FOR 1990
C1N91.OUT	29,532	08-07-98	NOX MODELING FOR 1991
	ŕ		
C1P87.OUT	45,903	08-07-98	PM10 MODELING FOR 1987
C1P88.OUT	45,903	08-07-98	PM10 MODELING FOR 1988
C1P89.OUT	45,903	08-07-98	PM10 MODELING FOR 1989
C1P90.OUT	45,903	08-07-98	PM10 MODELING FOR 1990
C1P91.OUT	45,903	08-07-98	PM10 MODELING FOR 1991
C1S87.OUT	50,514	08-07-98	SO2 MODELING FOR 1987
C1S88.OUT	50,514	08-07-98	SO2 MODELING FOR 1988
C1S89.OUT	50,514	08-07-98	SO2 MODELING FOR 1989
C1S90.OUT	50,514	08-07-98	SO2 MODELING FOR 1990
C1S91.OUT	50,514	08-07-98	SO2 MODELING FOR 1991

# IN THE FILE C2ASI.EXE IS ISCST3 MODELING OF SIGNIFICANT IMPACT ANALYSIS (SIA) FOR SIA OF CLASS 2 AREA:

```
C2N87 4.OUT
                184,300 08-07-98 NOX MODELING FOR 1987
C2N88 4.OUT
                184,300 08-07-98 NOX MODELING FOR 1988
C2N89 4.OUT
                184,300 08-07-98 NOX MODELING FOR 1989
C2N90 4.OUT
                184,300 08-07-98 NOX MODELING FOR 1990
C2N91 4.OUT
                184,300 08-07-98 NOX MODELING FOR 1991
C2P87 4.OUT
                302,991 08-07-98 PM10 MODELING FOR 1987
C2P88 4.OUT
                302,991 08-07-98 PM10 MODELING FOR 1988
C2P89 4.OUT
                302,991 08-07-98 PM10 MODELING FOR 1989
                302,991 08-07-98 PM10 MODELING FOR 1990
C2P90 4.OUT
C2P91 4.OUT
                302,991 08-07-98 PM10 MODELING FOR 1991
               409.002 08-07-98 SO2 MODELING FOR 1987
C2S87 4.OUT
C2S88 4.OUT
               409,002 08-07-98 SO2 MODELING FOR 1988
                409,002 08-07-98 SO2 MODELING FOR 1989
C2S89 4.OUT
                409,002 08-07-98 SO2 MODELING FOR 1990
C2S90 4.OUT
C2S91 4.OUT
                409,002 08-07-98 SO2 MODELING FOR 1991
```

THERE ARE RECEPTORS AT 100 METER INTERVALS ALONG THE PROPERTY LINE, DISCRETE POLAR RECEPTORS FROM 1500 METERS TO 6000 METERS AND A POLAR RECEPTOR GRID AT 7000, 8000, 9000, 10,000, 12,000, 14,000, 16,000, 18,000 METERS.

POLAR RECEPTORS ARE CENTERED AT X=0 Y=0 THE LOCATION OF THE KILN STACK OR UTMS 396,803 METERS EAST, 3,079,435 METERS NORTH. NO SIGNIFICANCE WAS FOUND FOR THE PSD CLASS 1 RECEPTORS, HOWEVER, CLASS 2 SIA INDICATED

IN THE FILE C1ASI.EXE IS CLASS 2 AREA INCREMENT AND FLORIDA AMBIENT AIR QUALITY STANDARD (FAAQS) ANALYSIS FOR THE 24-HOUR PM10 STANDARD:

#### CLASS 2: 101,378 08-10-98 PM10 MODELING FOR 1987 C2PP87.OUT C2PP88.OUT 96,575 08-10-98 PM10 MODELING FOR 1988 99,776 08-10-98 PM10 MODELING FOR 1989 C2PP89.OUT C2PP90.OUT 100,443 08-10-98 PM10 MODELING FOR 1990 C2PP91.OUT 98,174 08-10-98 PM10 MODELING FOR 1991 **FAAOS:** FQP87.OUT 126,359 08-10-98 PM10 MODELING FOR 1987 121,556 08-10-98 PM10 MODELING FOR 1988 FOP88.OUT FQP89.OUT 124,757 08-10-98 PM10 MODELING FOR 1989 FOP90.OUT 125,558 08-10-98 PM10 MODELING FOR 1990 FOP91.OUT 123,423 08-10-98 PM10 MODELING FOR 1991

THAT INCREMENT ANALYSIS WAS REQUIRED.

TO DETERMINE THE DAYS AND RECEPTORS OF SIGNIFICANCE, THE FOLLOWING FILES PROVIDED IN "DYRNG.EXE" WERE ANALYZED.

C2P87\_4.PRN 3,635 08-10-98 HIGH 50 TABLE FOR 1987 C2P88\_4.PRN 3,635 08-10-98 HIGH 50 TABLE FOR 1988 C2P89\_4.PRN 3,635 08-10-98 HIGH 50 TABLE FOR 1989 C2P90\_4.PRN 3,635 08-10-98 HIGH 50 TABLE FOR 1990 C2P91\_4.PRN 3,635 08-10-98 HIGH 50 TABLE FOR 1991

DYRNG.WK1 13,760 08-10-98 SORT OF DAYS & RECEPTORS REC&DYS1.PRN 7,122 08-10-98 FINAL INPUT TO MODEL

BUILDING INPUT PROFILE PROGRAM (BPIP) FILES ARE PROVIDED IN NW-DWNWH.EXE, THESE BUILDING DOWNWASH CALCULATIONS ARE USED IN ALL MODELING. THE FOLLOWING
BPIP FILES ARE PROVIDED:

IMC2BPI INP 1,678 11-13-97 INPUT IMC2BPI OUT 4,867 11-13-97 OUTPUT IMC2BPI SUM 86,715 11-13-97 SUMMARY

AND:

READ ME 5,326 08-10-98 THIS FILE

IF I MAY PROVIDE ADDITIONAL FILES, OR CLARIFICATION PLEASE CONTACT ME.

AUGUST 10, 1998 MARK KOLETZKE KOOGLER AND ASSOCIATES (352) 377-5822 KOOGLER@WORLDNET.ATT.NET

# ATTACHMENT 5

### SUMMARY OF NITROGEN OXIDES MEASUREMENTS ON EXISTING KILN B

- A. TESTING CONDUCTED MAY 1998
- B. TESTING CONDUCTED AUGUST 1998

# Southern Environmental Sciences, Inc.

1204 North Wheeler Street ☐ Plant City, Florida 33566-2354 ☐ (813) 752-5014

May 19, 1998

l TEM A

Mr. John Upton **IMC-AGRICO COMPANY** New Wales Operations P.O. Box 2000 Mulberry, Florida 33860-1100

Re:

Multiphos Stack

Dear John:

The following are the results of the nitrogen oxides (NOx) test performed on the above referenced source on May 12, 1998.

Time

NO<sub>X</sub> PPM

1525 - 1555

22

Enclosed is a copy of the strip chart and the calibration gas certifications. If you need any additional information please let me know.

Very truly yours,

SOUTHERN ENVIRONMENTAL

Mark S. Gierke

Environmental Specialist

MSG/bm

**Enclosures** 

Kill B optg

.,	a tarda a militar in terr	- 0			s of 19
	uititos Piant B Kili	n Operating	TAAT	dous	NG. CEM
					815
1525-1555					815
			,,,	12	-
ta P	Sqrt Delte P	Active Pt.			
0.78	0.883176	1			
0.88	0.938083	1			
0.97	0.984886	1			
1	1	1			
1.1	1.048809	1			
1.2	1.095445	1			
0.92	0.959166	1			
0.94	0.969536	1			
1	1	t			
1.05	1.024695	1			
1.2	1.095445	\$			
1.2	1.095445	1			
Avg Sqrt del	(a P 1.007891	12			
-			:		
102 (F)	562 (R)	38.88889 (C)			
89 (F)					
13					
/0.44 B =	<b>Cl</b>				
60 % 1ron	n Charus	;			
0.0686					
				•••	
			4.12 %	1120	
Pi = R ^ 2		54	15.90 Sq	uare Feet	
	LxW				
2.435 * Sqrt delta	P * Ts ^1/2		58.2 Fe	eVsec	
Stack Velocity * 60	• Cross Sectional arcs		55491 AC	TFM.	
·		<u></u>			
31680 *(1-Bws)*v	=A6/Ts(R)		49988 DS	CFM	
			22 pp	m	
		2dscm/dscf	7.9 16/	hr	
=1[b/454000mg=60	mni/hr*xxxdscfm				
	5/(2/98  1525-1555  1ta P  0.78  0.88  0.97  1  1.1  1.2  0.92  0.94  1  1.05  1.2  1.2  1.2  1.2  Avg Sqrt del  102 (F)  89 (F)  13  60 % from  0.0686  Pi * R * 2  2.435 * Sqrt delta  Stack Velocity * 60  31680 *(1-Bws)*va	1525-1555     1525-1555     1528	1525-1555     1525-1555     1528   P	1525-1555   The   1525-1555	New Wales Multifos Plant B Kiln Operating

ITEM B.

# I.M.C. NEW WALES MULTIFOS TEST SUMMARY

AUGUST 3, 1998

CONDITION No.	PPM NOX	LB/HR NOX	STACK FLOW (DSCFM)	COMMENT
1	32.50	10.82	46455 *	BURNER AIR 3375 CFM
2	36.44	12.14	46455 *	RED. BURNER AIR 2250 CFM
3	33.38	11.12	46455 *	INC. COMB. AIR 2730 CFM
4	31.62	10.53	46455 *	INC. COMB. AIR 3220 CFM
5	28.70	9.56	46455 *	INC. COMB. AIR 3700 CFM
6	30.49	10.15	46455 *	INC. COMB. AIR 3800 CFM
7	30.79	10.25	46455 *	INC. COMB. AIR 3170 CFM
8	67.81	14.57	29971	A FAN OFF

<sup>\* =</sup> AVERAGE OF FLOWS 1 & 2

LB/HR = (STACK GAS FLOW RATE) (PPM NOX) (.0000071688)

```
PAGE 2
                                469.31
              1.00
11:49:59
                                467.44
              0.97
11:50:59
                                326.56
11:51:59
              1.05
                                 18.56
              1.08
11:52:59
                                  8.35
11:53:59
              8.61
             19.17
                                  4.17
11:54:59
                                  3.29
11:55:59
             20.18
                                  2.86
11:56:59
             20.44
                                  2.53
             20.51
11:57:59
                                  1.87
11:58:59
             20.55
                                  2.09
             20.61
11:59:59
                                  1.76
12: 0:59
             20.66
                                  5.93 burner air at 3375 cfm
12: 1:59
             20.71
                                 30.42 <<< stack, flow 1 & 2
12: 2:59
             18.65
                                 33.49 Condition 1
12: 3:59
             17.48
                                                     32.50 ppm nox
                                 32.61 average =
12: 4:59
             14.82
                                 33.05
12: 5:59
             16.96
                                                     16.89 % 02
             15.98
                                 32.72 average =
12: 6:59
                                 28.55
12: 7:59
             17.39
                                 29.87
             16.17
12: 8:59
                                 30.86
12: 9:59
             15.18
             17.21
                                 31.73
12:10:59
                                 33.16
12:11:59
             17.06
             17.22
                                 32.61
12:12:59
                                 31.95
             17.29
12:13:59
                                 33.49
12:14:59
             17.31
                                 33.38
12:15:59
             16.94
                                 35.69
12:16:59
             16.94
                                 33.82
12:17:59
             17.37
                                 33.05
12:18:59
             17.39
                                 33.38
             17.01
12:19:59
                                 33.05
12:20:59
             17.44
                                 32.61
12:21:59
             17.43
             17.44
                                 33.27
12:22:59
                                 33.82
             17.46
12:23:59
                                 32.39
             16.91
12:24:59
                                 31.08
12:25:59
             16.05
                                 32.50 <<< reduced burner air - 2250 cfm
12:26:59
             17.51
                                 32.17
12:27:59
             17.50
                                 33.93 Condition 2
12:28:59
             17.50
                                                     36.44 ppm nox
                                 36.89 average =
12:29:59
             17.49
12:30:59
             17.50
                                 39.31
                                                     17.42 % 02
12:31:59
                                 39.09 average =
             17.51
                                 35.69
12:32:59
             16.50
             17.53
                                 34.92
12:33:59
                                 34.15
             17.53
12:34:59
12:35:59
             17.54
                                 35.36
                                 37.44
12:36:59
             17.52
                                 37.77
12:37:59
             17.53
                                 35.91
12:38:59
             17.56
                                 35.58
             16.72
12:39:59
                                 38.65
12:40:59
             17.60
```

```
PAGE 3
                                41.07
12:41:59
             17.49
                                39.09
12:42:59
             17.60
                                37.77 <<< inc. combuston air, 2730 cfm
             17.60
12:43:59
                                34.92
             17.61
12:44:59
                                32.94 Condition 3
            17.61
12:45:59
                                32.17 average = 33.38 ppm nox
12:46:59
             15.50
12:47:59
            16.94
                                31.18
                                                   17.05 % O2
                                33.27 average =
12:48:59
            17.60
            16.46
                                31.40
12:49:59
                                31.18 <<< inc. combuston air, 3220 cfm
             17.24
12:50:59
                                31.29
            17.64
12:51:59
                                32.39 Condition 4
            17.64
12:52:59
                                32.61 \text{ average} = 31.62 \text{ ppm nox}
            13.80
12:53:59
                                31.95
            17.62
12:54:59
                                32.39 average = 17.10 % 02
12:55:59
            17.64
                                30.97
            17.58
12:56:59
                                30.20
            17.65
12:57:59
                                30.64 <<< inc. combuston air, 3700 cfm
             15.99
12:58:59
                                29.65
            17.41
12:59:59
                                28.77 Condition 5
            17.64
13: 0:59
                                28.66 \text{ average} = 28.70 \text{ ppm nox}
13: 1:59
            17.67
13: 2:59
            16.90
                                28.66
                                28.33 average = 17.28 % O2
13: 3:59
            17.69
                                27.45
            17.68
13: 4:59
                                28.22
13: 5:59
            17.01
                                27.89
13: 6:59
            17.49
                                27.67 <<< inc. combuston air, 3800 cfm
13: 7:59
            17.69
            17.68
                                28.44
13: 8:59
                                28.22 Condition 6
13: 9:59
            17.70
                                29.98 average = 30.49 ppm nox
            17.70
13:10:59
                                30.09
            17.72
13:11:59
                                30.42 \text{ average} = 17.69 \% 02
            17.71
13:12:59
                                30.53
            17.70
13:13:59
                                30.31
13:14:59
            17.71
                                30.31
            17.70
13:15:59
                                31.95
13:16:59
             17.71
                                33.38
            17.70
13:17:59
                                32.61
            17.70
13:18:59
                                32.50
             17.58
13:19:59
                                32.06 <<< inc. combuston air, 3170 cfm
             17.69
13:20:59
                                31.18 @ 50 % DAMPER
13:21:59
            17.69
                                29.65 Condition 7
            17.71
13:22:59
                                28.22 \text{ average} = 30.79 \text{ ppm nox}
             17.19
13:23:59
                                28.00
13:24:59
             17.72
                                29.21 average = 17.62 % O2
             17.74
13:25:59
                                28.88
13:26:59
            17.75
                                29.32 average 02 for all 7 conditions
             17.18
13:27:59
                                                   17.33 % 02
                                27.67
13:28:59
            17.74
                                27.12
            17.72
13:29:59
                                29.54
13:30:59
             17.73
                                30.75
            17.73
13:31:59
                                31.84
            17.64
13:32:59
```

```
PAGE 4
                                 32.72
13:33:59
             17.73
                                 32.61
13:34:59
             17.75
                                 32.39
13:35:59
             17.73
             17.73
                                 32.83
13:36:59
                                 33.27
13:37:59
             17.73
                                 33.27
             17.77
13:38:59
             17.77
                                 33.16
13:39:59
                                 32.94
13:40:59
             17.74
13:41:59
             17.75
                                 31.73
                                 35.03
             17.55
13:42:59
                                 39.20
             17.58
13:43:59
                                 40.74
13:44:59
             17.33
             16.84
                                 38.10
13:45:59
                                 37.44
             17.70
13:46:59
                                 51.06
             17.41
13:47:59
                                 63.14 <<< A fan off, flow 3
13:48:59
             16.22
             15.57
                                 68.63
13:49:59
                                 72.14 Condition 8
13:50:59
             15.53
                                                     59.75 ppm nox
                                 72.25 average =
             15.52
13:51:59
                                 68.96
             15.37
13:52:59
                                 65.11 average =
                                                     15.42
             15.16
13:53:59
                                 62.81
13:54:59
             15.47
                                 61.93
             15.49
13:55:59
                                 62.37
13:56:59
             15.51
                                 62.26
             15.54
13:57:59
                                 65.33
             15.53
13:58:59
                                 68.41
13:59:59
             15.52
14: 0:59
             15.49
                                 83.12
                                 84.22
14: 1:59
             14.76
                                 69.84
14: 2:59
             15.51
                                 63.47
14: 3:59
             15.54
                                 63.25
14: 4:59
             15.55
                                 63.25 <<< end of testing
14: 5:59
             15.54
                                 85.21
14: 6:59
             15.65
                                  0.99
14: 7:59
             16.39
                                  0.55 <<< \text{ \text{zero air}
14: 8:59
             17.07
                                  0.44
14: 9:59
             17.50
                                122.65
14:10:59
             17.81
             18.01
                                501.59
14:11:59
                                502.25 <<< 483 ppm nox
14:12:59
             18.16
                                502.47
14:13:59
             18.36
                                510.05
14:14:59
             18.59
             18.74
                                901.18
14:15:59
                                909.08
             18.84
14:16:59
                                908.31 <<< 898 ppm nox
             18.93
14:17:59
                                907.10
14:18:59
             18.99
                                906.67
14:19:59
             19.05
                                201.71
             19.12
14:20:59
                                101.46
14:21:59
             19.19
                                492.92
             19.24
14:22:59
                                492.48
14:23:59
             19.27
                                492.70 <<< 483 ppm nox, leak check
             19.36
14:24:59
                                492.92
14:25:59
             19.53
                                492.48
             19.67
14:26:59
```

```
Company: IMC, NEW WALES
                                          Location: NEW WALES, FL
         MULTIFOS, FLOW 1
Source:
                                          Date:
                                                    AUGUST 3, 1998
         A & B FANS ON
             54.61 FT/SEC
                                             15.90 ft^2
                                     As =
    vs =
             52116 acfm - not corrected
     Q =
Q(stnd) =
             47046 dscfm - both temperature and moisture corrected
Q(moist)=
             49452 dcfm -
                           only moisture corrected
Q(temp) =
             49785 scfm -
                           only temperature corrected
                   Moisture
Vm(Std) = 45.957685
                                     Bws = 0.096263
                                                      Lower Bws
                                Bws @sat =0.055277
Vw(Std) = 4.89528
                                                       Value used
                           Percent Moist =5.527700
Emission Rates:
                     CO =
                                0.00 lb/hr
                    Nox =
                               10.79 lb/hr as NO2
                    SO2 =
                                0.00 lb/hr
                                0.00 lb/hr as Propane
                    THC =
EQUATIONS:
As = (PI*(Stack Dia/12)^2)/4
                                    --- Round Stacks
As = (Stack L/12)*(Stack W/12)
                                    --- Square Stacks
Md = (.44*\%CO2)+(.32*\%O2)+(.28*(100-(\%CO2+\%O2)))
Ms = (Md*(1-%Moist))+(18*%Moist)
P(stack) = Pb+(Ps/13.6)
vs = (85.49)*(0.85)*(Sqrt.Dp)*(Sqrt[(T(s)+460)/(Ms*P(stack))])
Q = vs * As * 60
Q(stnd) = Q*(1-%Moist)*(528/(Ts+460))*(P(stack)/29.92)
Vm (Stnd) = 17.6471 * Vm * Y * ((Pb+(dH/13.6))/(Tm+460))
Vw (Stnd) = 0.0471 * Vlc
Bws = (Vw(Stnd) / (Vm(Stnd) + Vw(Stnd))
Bws @ Sat = Vap. Pressure of H2O @ Dew Point Temp/Ps
CO (lb/hr) = ((PPM CO)*Q(stnd)*28.01*60)/(385*10^6)
NOx (1b/hr) = ((PPM NOx)*Q(stnd)*46.006*60)/(385*10^6)
SO2 (lb/hr) = ((PPM SO2)*Q(stnd)*64.0648*60)/(385*10^6)
THC (lb/hr) = ((PPM THC)*Q(temp)*44.0965*60)/(385*10^6)
```

Company: IMC, NEW WALES
MULTIFOS, FLOW 1
A & B FANS ON

Sqrt.Dp= 0.9470

T(s) =95.00 Location: NEW WALES, FL Date: AUGUST 3, 1998

12 Filename: QuickFLOW

[Alt-C]
to clear input

range

	Stack	Stack	*	02 measured by	KA O2	meter
Data	Velocity	Gas		CO2 calculated		
Point	Head	Temp.		moisture assum		
1	1.10	95		Pb =		in Hg
2	1.10	95		Ps =		in H2O
3	1.00	95		%O2 =	17.33	
4	0.78	95		%CO2 =	3.57	
5	0.73	95		%Moist =	5.50	
6	0.66	95		Stack Dia	54	in
7	0.94	95		or		
8	0.97	95		Stack L =		in
9	0.92	95		Stack $W =$		in
10	0.84	95		PPM CO =		ppm
11	0.92	95		PPM NOx =	32	ppm
12	0.86	95		PPM SO2 =	0	ppm
13	0.00	0		PPM THC =		ppm
14	0.00	0		Vm =	47.31	
15	0.00	0		dH =		in H2O
16	0.00	0		Tm =	90	F
17	0.00	0		Y =	1.002	
18	0.00	0		Vlc =	104	ml
19	0.00	0				
20	0.00	0		•		
21	0.00	0				
22	0.00	0				
23	0.00	0				
24	0.00	. 0				
25	0.00	0				
26	0.00	0				
27	0.00	0				
28	0.00	0				
29	0.00	0				
30	0.00	0				
31	0.00	0		•		
32	0.00	0				
33	0.00	0				
34	0.00	0				
35	0.00	0				
36	0.00	0				

```
Company: IMC, NEW WALES
                                          Location: NEW WALES, FL
Source: MULTIFOS, FLOW 2
                                          Date:
                                                   AUGUST 3, 1998
         A & B FANS ON
             53.91 FT/SEC
                                             15.90 ft^2
    vs =
                                     As =
     Q =
             51443 acfm - not corrected
Q(stnd) =
             45863 dscfm - both temperature and moisture corrected
Q(moist)=
             48555 dcfm - only moisture corrected
Q(temp) =
             48790 scfm - only temperature corrected
                   Moisture
Vm(Std) = 45.957685
                                     Bws =0.096263
                                                      Lower Bws
Vw(Std) = 4.89528
                                Bws @sat =0.062440 |
                                                      Value used
                           Percent Moist =6.244001
Emission Rates:
                     CO =
                                0.00 lb/hr
                               10.52 lb/hr as NO2
                    NOx =
                                0.00 lb/hr
                    SO2 =
                    THC =
                                0.00 lb/hr as Propane
EQUATIONS:
As = (PI*(Stack Dia/12)^2)/4
                                    --- Round Stacks
As = (Stack L/12)*(Stack W/12) --- Square Stacks
Md = (.44*\%CO2)+(.32*\%O2)+(.28*(100-(\%CO2+\%O2)))
Ms = (Md*(1-%Moist))+(18*%Moist)
P(stack) = Pb+(Ps/13.6)
vs = (85.49)*(0.85)*(Sqrt.Dp)*(Sqrt[(T(s)+460)/(Ms*P(stack))])
Q = vs * As * 60
Q(stnd) = Q*(1-%Moist)*(528/(Ts+460))*(P(stack)/29.92)
Vm (Stnd) = 17.6471 * Vm * Y * ((Pb+(dH/13.6))/(Tm+460))
Vw (Stnd) = 0.0471 * Vlc
Bws = (Vw(Stnd) / (Vm(Stnd) + Vw(Stnd))
Bws @ Sat = Vap. Pressure of H2O @ Dew Point Temp/Ps
CO (lb/hr) = ((PPM CO)*Q(stnd)*28.01*60)/(385*10^6)
NOx (1b/hr) = ((PPM NOx)*Q(stnd)*46.006*60)/(385*10^6)
SO2 (1b/hr) = ((PPM SO2)*Q(stnd)*64.0648*60)/(385*10^6)
THC (1b/hr) = ((PPM THC)*Q(temp)*44.0965*60)/(385*10^6)
```

```
Location: NEW WALES, FL
Company: IMC, NEW WALES
                                                       AUGUST 3, 1998
                                              Date:
         MULTIFOS, FLOW 2
         A & B FANS ON
                                              Filename:
                                     12
                                              OuickFLOW
          Sqrt.Dp=
                      0.9305
                                              [Alt-C]
                                              to clear input
              T(s)=
                       99.00
                                              range
                                        * O2 measured by KA O2 meter
                                Stack
            Stack
                                          CO2 calculated O2 - 20.9
          Velocity
                                 Gas
  Data
                                          moisture assumed saturation
                                Temp.
  Point
             Head
                                                  Pb =
                                                           30.08 in Hg
                                     99
               0.91
       1
                                                            -0.5 in H2O
                                                  Ps =
                                     99
               0.90
       2
                                                           17.33 % *
                                                 %02 =
                                     99
       3
               0.84
                                                            3.57 % *
                                                %CO2 =
                                     99
       4
               0.82
                                              %Moist =
                                                            6.00 % *
                                     99
               0.82
       5
                                                              54 in
               0.83
                                     99
                                              Stack Dia
       6
                                     99
                                                 or
               1.10
       7
                                                                 in
                                              Stack L =
                                     99
       8
               1.10
                                                                 in
                                     99
                                              Stack W =
               1.05
       9
               0.76
                                     99
                                              PPM CO =
                                                                 ppm
      10
                                     99
                                              PPM NOx =
                                                              32 ppm
               0.67
      11
                                              PPM SO2 =
                                                               0 ppm
                                     99
               0.66
      12
                                              PPM THC =
                                                                 ppm
                                      0
      13
               0.00
                                                           47.31 ft3
                                                  Vm =
                                      0
               0.00
      14
                                                            1.84 in H2O
                                                  dH =
                                      0
      15
               0.00
                                                              90 F
                                      0
                                                  Tm =
               0.00
      16
                                                   Y =
                                                           1.002
                                      0
               0.00
      17
                                                             104 ml
                                                 Vlc =
                                      0
      18
               0.00
               0.00
                                      0
      19
                                      0
      20
               0.00
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```
Location: NEW WALES
Company: IMC, NEW WALES
         MULTIFOS, FLOW 3
                                                    AUGUST 3,
Source:
                                           Date:
         A FAN OFF
             35.21 FT/SEC
                                              15.90 ft^2
    vs =
                                      As =
             33597 acfm - not corrected
     Q =
             29971 dscfm - both temperature and moisture cor
Q(stnd) =
Q(moist)=
             31730 dcfm - only moisture corrected
Q(temp) =
             31884 scfm - only temperature corrected
                   Moisture
Vm(Std) = 45.957685
                                      Bws = 0.096263
                                                       Lower
Vw(Std) = 4.89528
                                 Bws @sat =0.062401
                                                       Value
                            Percent Moist =6.240183
                                0.00 lb/hr
Emission Rates:
                     CO =
                    NOx =
                                13.75 lb/hr as NO2
                     SO2 =
                                0.00 lb/hr
                    THC =
                                0.00 lb/hr as Propane
EQUATIONS:
As = (PI*(Stack Dia/12)^2)/4
                                     --- Round Stacks
                                    --- Square Stacks
As = (Stack L/12)*(Stack W/12)
Md = (.44 * CO2) + (.32 * CO2) + (.28 * (100 - (CO2 + CO2)))
Ms = (Md*(1-%Moist))+(18*%Moist)
P(stack) = Pb+(Ps/13.6)
vs = (85.49)*(0.85)*(Sqrt.Dp)*(Sqrt[(T(s)+460)/(Ms*P(stack)))
Q = vs * As * 60
Q(stnd) = Q*(1-%Moist)*(528/(Ts+460))*(P(stack)/29.92)
Vm (Stnd) = 17.6471 * Vm * Y * ((Pb+(dH/13.6))/(Tm+460))
Vw (Stnd) = 0.0471 * Vlc
Bws = (Vw(Stnd) / (Vm(Stnd) + Vw(Stnd))
Bws @ Sat = Vap. Pressure of H2O @ Dew Point Temp/Ps
CO (lb/hr) = ((PPM CO)*Q(stnd)*28.01*60)/(385*10^6)
NOx (1b/hr) = ((PPM NOx)*Q(stnd)*46.006*60)/(385*10^6)
SO2 (lb/hr) = ((PPM SO2)*Q(stnd)*64.0648*60)/(385*10^6)
THC (lb/hr) = ((PPM THC)*Q(temp)*44.0965*60)/(385*10^6)
```

```
Location: NEW WALES, FL
Company: IMC, NEW WALES
                                                          AUGUST 3, 1998
                                               Date:
          MULTIFOS, FLOW 3
          A FAN OFF
                                               Filename:
                                      12
                                               QuickFLOW
           Sqrt.Dp=
                      0.6102
                                               [Alt-C]
                                               to clear input
              T(s)=
                        99.00
                                               range
                                          * O2 measured by KA O2 meter
                                 Stack
            Stack
                                            CO2 calculated O2 - 20.9
                                  Gas
           Velocity
  Data
                                            moisture assumed saturation
                                 Temp.
  Point
             Head
                                                             30.08 in Hg
                                      99
                                                    Pb =
                0.37
       1
                                                             -0.25 in H2O
                                      99
                                                    Ps =
       2
                0.38
                                                             15.42 % *
                                                   %02 =
                                      99
       3
                0.39
                                                              5.48 % *
                                                  %CO2 =
                                      99
                 0.4
        4
                                               %Moist =
                                                              6.00 % *
                                      99
       5
                0.35
                                                                 54 in
                                               Stack Dia
                                      99
       6
                0.34
                                      99
                                                   or
       7
                0.36
                                               Stack L =
                                                                    in
                0.37
                                      99
       8
                                                                    in
                                      99
                                               Stack W =
               0.38
       9
                                                                    ppm
                                      99
                                               PPM CO =
      10
                0.38
                                                                 64 ppm
                                               PPM NOx =
                                      99
      11
                0.37
                                               PPM SO2 =
                                                                  0 ppm
                                      99
      12
                0.38
                                               PPM THC =
                                                                    ppm
                                       0
      13
                   0
                                                             47.31 ft3
                                       0
                                                    vm =
                   0
      14
                                                    dH =
                                                              1.84 in H2O
                                       0
                   0
      15
                                                    Tm =
                                                                 90 F
                                       0
      16
                   0
                                                             1.002
                                                     Y =
                   0
                                       0
      17
                                                   Vlc =
                                                               104 ml
                                       0
                   0
      18
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```

### ATTACHMENT 6

MANUFACTURER'S EMISSION GUARANTEES FOR SULFUR DIOXIDE AND FLUORIDES

- A. GUARANTEE ON FLUORIDES
- B. GUARANTEE ON SULFUR DIOXIDE

D.R. TECHNOLOGY, INCORPORATED

POLIZITION CONTROL & ENERGY CONSERVATION
COMMINITING • DESIGN • WHIGHERING
72 FOUTH STPFFT, PURTHOLD, NEW JERSRY 07786

Telephone: 732-780-4664

ITEM A.

August 6, 1998

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1MC-Agrico Company New Wales Operations P. O. Box 2000 Mulbarry, Florida 33860-1100

Attn: Mr. Richard Harrison (P:941-428-2500 x6570/F:7191)

Subject: Performance Of SOz Scribber On "Fluoride"

D. R. Technology Reference: 98771 IMC A8936214

Dear Richard:

As stated, you may have up to 2 Lbs./Hr. of "Fluoride" in the 25,000 ACFH of gas as well as the anticipated SO2.

Be advised that this unit as is will remove 95+% of entering HF

Please feel free to contact the undersigned with questions, or to discuss.

Very truly yours, D. R. TECHROLOGY, INC.

Richard A. Schwartz,

President

RAS:dk

oc: H & B Industrial Equipment Co. (Sales Representative)

P. Q. Box 6216

4406 B. Florida Ave.

Suite 220

Lakeland, Florida 33807-6246

Attn: Luis Homandez P:941-647-5943/F:0018

B:771£6178

### D.R. TECHNOLOGY, INCORPORATED

Pollution control & energy conservation consulting • Design • Engineering 73 South Street, Freehold. New Jersey 07728

Telephone: 732-780-4664

August 11, 1998

'n

IMC-Agrico Company New Wales Operations P. O. Box 2000 Mulberry, Florida 33860-1100

Attn: Mr. Richard Harrison (P:941-428-2500 x6570/F:7191)

Subject: Performance of SO2 Scrubber

D. R. Technology Reference: 98771

IMC A8936214

Dear Mr. Harrison:

Per our conversation, we have reviewed the process requirements for 98% SD2 removal.

Be advised that this unit with additional packing will remove 98% of the entering SO2.

Please feel free to contact the undersigned with questions, or to discuss!

Very truly yours, D. R. TECHNOLOGY, INC.

Richard A. Schwartz, MCS

President

RAS:dk

cc: H & B Industrial Equipment Co. (Sales Representative)
P. O. Box 6246
4406 S. Florida Ave.
Suite 220
Lakeland, Florida 33807-6346
Attn: Luis Hernandez
P:941-647-5943/F:0018

B:771L8118