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FROM:

PREVENTION OF SIGNIFICANT
DETERIORATION PERMIT
APPLICATION FOR PROPOSED
MODIFICATIONS AT GARDINIER, INC.'S
TAMPA CHEMICAL PLANT

Submitted By: Gardinier Inc. P.O. Box 3269 Tampa, Florida 33608

Submitted To:
U.S. Environmental Protection Agency
Region IV



GARDINIER INC.

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RUDY J. CABINA VICE PRESIDENT

November 26, 1979

U.S. Environmental Protection Agency, Region IV Air and Hazardous Materials Division Air Facilities Branch 345 Courtland Street, N.E. Atlanta, Georgia 30308

Attention: Mr. Tommie A. Gibbs, Branch Chief

Re: Prevention of Significant
Deterioration Permit Application
for Proposed Modifications
At Gardinier, Inc's Tampa
Chemical Plant

Dear Mr. Gibbs:

Attached is a Prevention of Significant Deterioration (PSD) permit application for proposed modifications at Gardinier's Tampa Chemical Plant. This project has previously been discussed with you and your staff at meetings held on October 5, 1979, and on October 29, 1979. Representing Gardinier at these meetings was Al Morrison, Superintendent of Environmental and Chemical Services, and our environmental consultant, Dames & Moore. The attached application incorporates suggestions and recommendations made during these meetings (and during related telephone discussions), including suggestions made at the October 29 meeting by Jeff Shumaker who represents your contractor, TRW Inc.

Based on information received from EPA, it is our understanding that Gardinier's proposed project will be reviewed under existing PSD regulations and, under these regulations, will be subject to Tier 1 requirements only. The content of our application, particularly with regard to evaluation of control technology and air quality impacts, is structured in accordance with this understanding.

U.S. Environmental Protection Agency, Region IV November 26, 1979 Page Two

As agreed to at the October 29 meeting, we are simultaneously submitting permit application copies to EPA, TRW, and the Florida Department of Environmental Regulation. Should your staff or TRW have any questions concerning the application, please direct them to Al Morrison at the Tampa Chemical Plant (813-677-9111). Since time is an important consideration on this project, we would appreciate a conclusion of the completeness review as soon as possible and immediate notification if it appears that the application might be considered incomplete. We will be pleased to meet with your representatives or otherwise provide additional information at any time if this will assist in EPA and TRW's review.

Sincerely,

Zuly J. Rabina Rudy J. Cabina Vice President

Attachment

Jeff Shumaker, TRW Inc.

Steve Smallwood, Florida DER

TABLE OF CONTENTS

| Sect | <u>tion</u> | Page |
|------|---|------|
| LIST | T OF TABLES | ii |
| | T OF FIGURES | ii |
| | APPLICANT INFORMATION | 1-1 |
| 1. | 1.1 GENERAL INFORMATION | 1-1 |
| | | |
| | 1.2 PROJECT SCHEDULE OBJECTIVES | 1-1 |
| | 1.3 EXPECTED NORMAL OPERATING SCHEDULE | 1-1 |
| 2. | SITE INFORMATION | 2-1 |
| | 2.1 GENERAL INFORMATION | 2-1 |
| | 2.2 SITE PLAN | 2-1 |
| 3. | DESCRIPTION OF MODIFICATIONS AND NEW FACILITIES | 3-1 |
| | 3.1 GENERAL INFORMATION | 3-1 |
| | 3.2 FUEL CONSUMPTION | 3-2 |
| | 3.3 PROCESS FLOW DIAGRAMS | 3-2 |
| 4. | EMISSION SOURCE INFORMATION | 4-1 |
| | 4.1 IDENTIFICATION OF EMISSION SOURCES | 4-1 |
| | 4.2 DERIVATION OF EMISSION RATE ESTIMATES | 4-7 |
| | 4.3 TIMING OF EMISSION SOURCE CHANGES | 4-8 |
| | REGULATORY CONSIDERATIONS | 5-1 |
| | | 6-1 |
| | | |
| | AMBIENT AIR QUALITY IMPACT | 7-1 |
| | 7.1 GENERAL | 7-1 |
| | 7.2 PSD CLASS I AREA IMPACT | 7-2 |
| 8. | STATE OF FLORIDA PERMIT APPLICATIONS | 8-1 |
| 9. | CONCLUSIONS | 9-1 |
| | | |

APPENDIX

LIST OF TABLES

| <u>Table</u> | Description | Page |
|---------------|--|-------------|
| 4-1 | Summary of Affected Particulate Matter Emission Sources | 4-2 |
| 4-2 | Summary of Affected Fluoride Emission Sources | 4-3 |
| 4-3 | Summary of Affected Sulfur Dioxide Emission Sources | 4-4 |
| 4-4 | Summary of Affected Nitrogen Dioxide Emission Sources | 4-5 |
| 4-5 | Summary of Net Change in Annual Emissions Resulting from Proposed Modifications . | 4-6 |
| 6-1 | Comparison of Actual Facility Emissions Versus Applicable Emission Limitation Standards | 6-2 |
| | LIST OF FIGURES | |
| <u>Figure</u> | <u>Description</u> | <u>Page</u> |
| 2-1 | Relative Location of Gardiner's Tampa Chemical Plant | 2-2 |
| 2-2 | Relative Location of New and Modified Facilities | 2-3 |
| 4-1 | Proposed Project Development Schedule | 4-10 |
| | | |

APPLICANT INFORMATION

1.1 GENERAL INFORMATION

COMPANY NAME: GARDINIER, INC.

Tampa Chemical Plant

ADDRESS: Post Office Box 3269

Tampa, Florida 33601

<u>TELEPHONE</u>: (813) 677-9111

RESPONSIBLE OFFICERS: Rudy J. Cabina, Vice President

Allen E. Morrison, Superintendent, Environmental

Chemical Services

SOURCE LOCATION: The location of the Tampa Chemical Plant operated by Gardinier, Inc. is approximately 8 km south of the city of Tampa at the intersection of U.S. Highway 41 and Riverview Drive. The facility is situated at UTM co-ordinates 362.9 E, 3082.5 N.

NATURE OF THE PROPOSED PROJECT: Gardinier, Inc. plans to modify its existing phosphate processing plant to allow approximately a 20 percent increase in production of P_2O_5 on a yearly basis.

DISTANCE TO NEAREST PSD CLASS I AREA: The nearest PSD Class I area is the Chassahowitzka National Wilderness Area (NWA) located 90 km to the north of the plant site. The only other Class I areas in Florida are the St. Marks NWA located 300 km to the northwest, the Everglades National Park located 300 km to the south-southeast and the Bradwell Bay NWA which is 320 km to the northwest.

1.2 PROJECT SCHEDULE OBJECTIVES

Start Construction: April-July 1980

Start Operation: Within two years of starting construction.

1.3 EXPECTED NORMAL OPERATING SCHEDULE

(See copies of construction permit applications in Appendix.)

2. SITE INFORMATION

2.1 GENERAL INFORMATION

The Tampa Chemical Plant, operated by Gardinier, Inc., is located approximately 8 km south of Tampa on the west side of U.S. Highway 41 at the intersection of Riverview Drive. The relative location of the plant site is shown in Figure 2-1.

2.2 SITE PLAN

The site plan of Gardinier's Tampa Chemical Plant is shown in Figure 2-2. The figure shows the location of proposed modifications and additions to this facility as described herein.

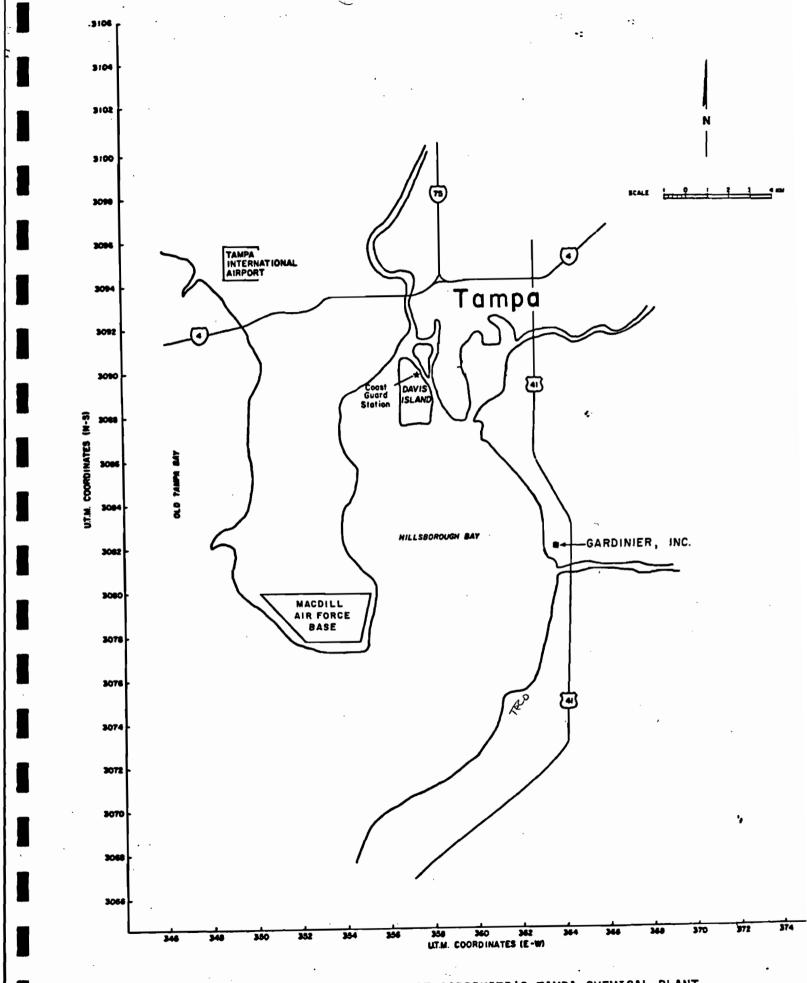
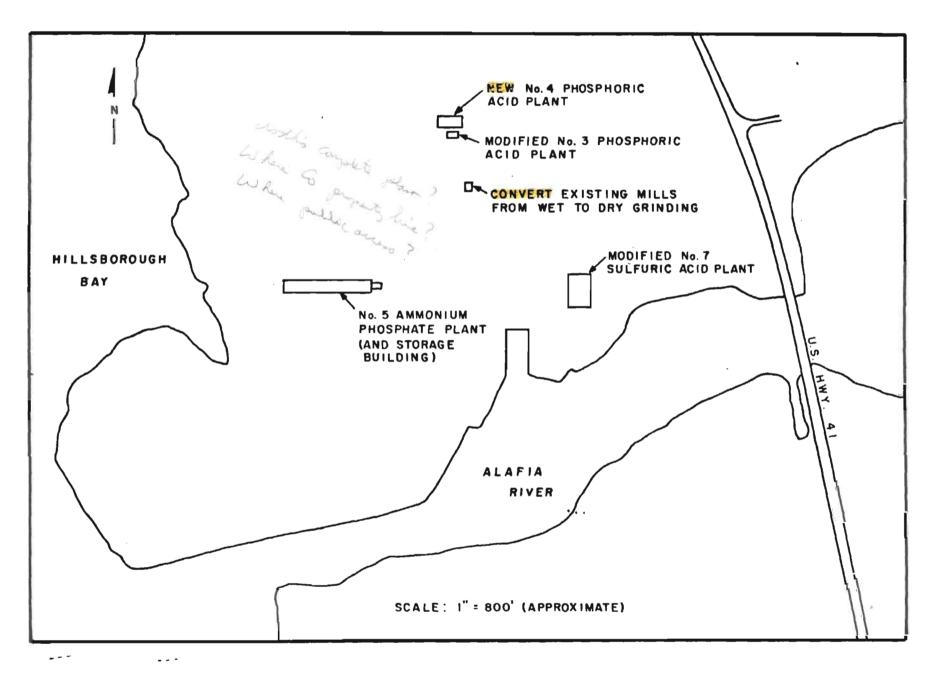


FIGURE 2-1. RELATIVE LOCATION OF GARDINIER'S TAMPA CHEMICAL PLANT



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Figure 2-2. Relative Location of New and Modified Facilities.

3. DESCRIPTION OF MODIFICATIONS AND NEW FACILITIES

3.1 GENERAL INFORMATION

Gardinier's planned modifications to its existing facilities as well as the construction of a new diammonium phosphate production unit will result in an expanded production from 600,000 to 720,000 tons of P_2O_5 per year. The primary changes in the physical plant which will occur are as follows:

- ° Conversion of the present NG. 3 Phosphoric Acid Plant to handle wet rock (as opposed to the currently processed dry rock) as well as the elimination of a dilution cooler, the addition of a flash cooler, and the modification of the cross-flow packed scrubber.
- Replacement of the present No. 2 Phosphoric Acid Plant with a new plant (to be designated the No. 4 Phosphoric Acid Plant).
- ° Construction of a new wet rock mill and the conversion of three existing dry rock mills to the wet rock process.
- ° Construction of a new 50 ton/h diammonium phosphate production unit (to be designated as the No. 5 Ammonium Phosphate Plant) and associated storage building.
- ° Modification of the existing No. 7 Sulfuric Acid Plant to facilitate an increase in production capacity from 1,380 tons of H_2SO_4/day to 1,750 tons/day.

In addition to these modifications, the following facilities will be shut down:

- ° No. 6, 7, 8, 10 rock grinding mills.
- ° No. 11, 12 KVS rock mills.
- ° 68BPL rock unloading and storage.
- ° South No. 2, 3 rock transfer airslides.
- ° North No. 2 rock transfer airslide
- ° Center No. 3 rock transfer airslide.
- ° No. 3 rock transfer airslide bin.



- ° No. 2, 3 filter buildings.
- Normal superphosphate plant (presently not in operation; see Section 4. for additional discussion).

3.2 FUEL CONSUMPTION

Of the above-mentioned modifications and additions, only the operation of the new Ammonium Phosphate Plant will involve the utilization of combustible fuel. This new facility will consume approximately 150 gal/h of No. 6 fuel oil in order to provide 21.9 MMBTU/h heat input to the rotary dryer.

3.3 PROCESS FLOW DIAGRAMS

Process flow diagrams for each of the new or modified processes are contained in the Appendix. These flow diagrams are included as part of the construction permit applications previously submitted to the Florida Department of Environmental Regulation (DER). Flow diagrams are provided for each of the following processes:

- ° No. 3 Phosphoric Acid Plant (modification to existing plant)
- On No. 4 Phosphoric Acid Plant (replaces No. 2 Phosphoric Acid Plant)
- ° No. 7 Sulfuric Acid Plant (modification to existing plant)
- ° No. 5 Ammonium Phosphate Plant (new plant)

4. EMISSION SOURCE INFORMATION

4.1 IDENTIFICATION OF EMISSION SOURCES

Tables 4-1 through 4-5 set forth the emission status of all proposed new or modified emission sources for the Tampa Chemical Plant. These tables contain information on emission rates and emission source characteristics for each affected source of emission, including sources which will be removed from service upon project completion. Table 4-5 presents an overall summary of annual emission changes for affected pollutants assuming continuous operation of all emission sources (see footnote at bottom of table).

From Table 4-5 it can be seen that the <u>allowable</u> emissions of fluorides will decrease as a result of the proposed project, although the net change in potential fluoride emissions will be greater than 100 tons/year thereby requiring that a PSD permit be obtained. Both particulate matter and sulfur dioxide net emission changes (potential as well as allowable) are emission <u>reductions</u> as a result of shutting down several emission sources and installing current technology control equipment on new and modified sources. Potential and allowable emissions of nitrogen dioxide are also estimated to be less than 50 tons/year.

There will also be an additional factor not reflected in Tables 4-1 and 4-5 which further supports the improvement in particulate matter air quality which will be gained if the proposed project is approved: namely, conversion to a wet-rock process will eliminate a considerable amount of fugitive dust for which no credit is taken in this application. The Hillsborough County Environmental Protection Commission has estimated that present fugitive dust emissions generated by Gardinier's Tampa Chemical plant are approximately 2,200 tons/year.

For better understanding of Tables 4-1, 4-2, and 4-5, it should be noted that the Normal Superphosphate Plant is a permitted emission source but is not presently operating. When the No. 5 Ammonium Phosphate Plant is started up, there will not be an adequate supply of raw materials to allow simultaneous operation of both it and the Superphosphate plant. Therefore, as part of the proposed project, this

TABLE 4-1 SUMMARY OF AFFECTED PARTICULATE MATTER EMISSION SOURCES

| | Potential ^a Particulate Emission | Permitted or Allowable Particulate Emission | Stack Helght | Stack Dlameter | Exit Velocity | Exl† Temperature | Exit Volumetric Flow |
|--|---|--|-----------------|-------------------|------------------|---------------------|----------------------------|
| Emission Source Description | Rate (lb/h) | Rate (lb/h) | (ft) | (ft) | (ft/s) | (°F) | (ft ³ /mln) |
| 1. Existing Facilities Which Will Be Shut Down | 2-22139 | | | | | | |
| No. 6, 7, 8, Rock Grinding Mills | s ^c 100 | 39.3 ^b | 95 | 2.0 | 95.5 | 152 | 18,000 |
| No. (11 KVS Rock MIII - 22179 | 400 | 30.6 ^b | 76 | 1.6 | 44.3 | 145 | 5,340 |
| No. 12 KVS Rock MIIIC - 22141 | 80 | 32.9 ^b | 71 | 1.6 | 70.7 | 148 | 8,530 |
| 68BPL Rock Unloading and Storage | | 42.5 ^b | 30 | 1.7 | 97.8 | 100 | 13,320 |
| South No. 2 Rock Transfer Airslide | 7 464210 | 18.2 ^b | 96 | 1.0 | 54.5 | 105 | 2,570 |
| North No. 2 Rock Transfer Airslide | 210 | 18.2 ^b | 85 | 0.4 | 83.6 | 102 | 630 |
| ⊳South No. 3 Rock Transfer Airslide | 102 | 9.65 ^D | 96 | 1.2 | 21.1 | 132 | 1,430 |
| Center No. 3 Rock Transfer Alrsilde | | 9.65 ^b | 115 | 1.2 | 22.7 | 118 | 1,540 |
| Morth No. 3 Rock Transfer A!rslide | 105 | 9•65 ^b | 82 | 1.2 | 14.4 | 97 | 980 |
| Mo. 3 Rock Transfer Airslide Bin ^C | 105 | 9•65 ^b | 108 | 1.2 | 21.5 | 128 | 1,460 |
| Normal Superphosphate - 13812 | 20 | 19•4 ^b | 73 | 2.5 | 49.8 | 86 | 14,670 |
| Total | 1616 | 239.7 | | | | | |
| 2. New Facilities | 2110 | 4 | | | | | |
| No. 5 Ammonium Phosphate | 7210 | 10 ^d | 90 | 8.0 | 45.1 | 140 | 136,000 |
| Net Emissions | -1406 ^e | −229•7 ^Θ | | | | | |
| a | +484 | | | | | | |

d_{Maximum} based on available data.

 $^{^{}m e}$ Represents a net emission reduction.

TABLE 4-2 SUMMARY OF AFFECTED FLUORIDE EMISSION SOURCES

| Emission Source Description | Potentlal Fluoride Emission Rate (lb/h) | Permitted or Allowable Fluoride Emission Rate (lb/h) | Stack Helght (ft) | Stack Dlameter (ft) | Exit Velocity (ft/s) | Exl† Temperature (°F) | Exit Volumetric Flow (ft ³ /mln) |
|---|--|--|-------------------------|---------------------------|----------------------------|-----------------------------|---|
| 1. Existing Facilities Which | | | | | | | |
| WIII Be Shut Down or ModIfled | 68 65 C CO | | | | | | |
| No. 2 Phosphoric Acid (shut down) | 6.0a | 1.12 | 110 | 4.0 | 37.3 | 154 | 28,120 |
| No. 2 Phosphoric Acid (shut down) No. 2 Filter Building (shut down) No. 3 Phosphoric Acid (modified) | 752 5.4a | 0.37 | 59 | 4.75 | 32.1 | 97 | 34,130 |
| No. 2 Filter Building (shut down). No. 3 Phosphoric Acid (modified). No. 3 Filter Building (shut down). | 25.0a | 0.94 | 93 | 4.0 | 29.4 | 124 | 22,170 |
| No. 3 Filter Building (shut down) | 18.6ª | 0.83 | 51 | 4.5 | 40.6 | 108 | 38,740 |
| Normal Superphosphate -13012 | _0.5 | 0.50 | 73 | 2.5 | 49.8 | 86 | 14,670 |
| Total | 57.5 | 3.76 | | | | | |
| 2. New or Modified Facilities | | | | | | | |
| No. 3 Phosphoric Acid (modified) | 25•0 ^b | 0.9 | 93 | 4.0 | 15.9 | 135 | 11,990 |
| No. 4 Phosphoric Acid (new) | 32.2 ^b | 1.2 | 115 | 4.0 | 15.9 | 135 | 11,990 |
| No. 5 Ammonium Phosphate (new) | 176.0b | 1.4 | 90 | 8.0 | 45.1 | 140 | 136,000 |
| Total | 233.2 | 3.5 | | | | | |
| 1334 # F-/Pa v | | | | | | | |
| Net Emissions | +175.7 | -0.26 | | | | | |
| #7 H204 - 5585 | | | | | | | |

 $^{^{\}rm a}$ Potential emissions in the absence of control equipment, based on estimated control efficiency. $^{\rm b}$ Based on typical scrubber water analysis.

TABLE 4-3
SUMMARY OF AFFECTED SULFUR DIOXIDE EMISSION SOURCES

| Emission Source Description | Potential Sul. Dlox. Emission Rate (lb/h) | Permitted or Allowable Sul. Diox. Emission Rate (lb/h) | Stack Helght (ft) | Stack Dlameter (ft) | Exit Velocity (ft/s) | Exit Temperature (°F) | Exit Volumetric Flow (ft ² /min) |
|---|--|--|-------------------------|---------------------------|----------------------------|-----------------------------|---|
| 1. Existing Facilities Which Will Be Modified | | | | | | | |
| No. 7 Sulfuric Acid | а | 575 | 150 | 7.5 | 27.1 | 153 | 71,830 |
| 2. Modified Facility | | | | | | | |
| No. 7 Sulfuric Acid | а | 292 | 150 | 7.5 | 33.9 | 155 | 89,860 |
| Net Emissions | a | -283 ^b | | | | | |

^aPotential emissions are difficult to define in this case because control method (double-absorption process) is an integral part of unit and not an add-on flue gas sulfur removal method.

^bRepresents a net emission <u>reduction</u>.

TABLE 4-4
SUMMARY OF AFFECTED NITROGEN DIOXIDE EMISSION SOURCES

| Emission Source Description | Potential Nit. Diox. Emission Rate (lb/h) | Permitted or Allowable Nit. Diox. Emission Rate (lb/h) | Stack Helght (ft) | Stack Diameter (ft) | Exit Velocity (ft/s) | Exit Temperature (°F) | Exit Volumetric Flow (ft ⁵ /min) |
|--|--|--|-------------------------|---------------------------|----------------------------|-----------------------------|--|
| 1. New Facility No. 5 Ammonium Phosphate | 9.0ª | 9•0 ^a | 90 | 8.0 | 45.1 | 140 | 136,000 |

Promis

 $^{^{}m a}$ Based on AP-42 emission factors for industrial bollers of 60 lb NO $_2$ per 1000 gal of residual fuel oll.

TABLE 4-5

SUMMARY OF NET CHANGE IN ANNUAL EMISSIONS
RESULTING FROM PROPOSED MODIFICATIONS

| Emission Type | Particulate <u>Matter (t/y)</u> | Fluorides (t/y) | Sulfur <u>Dioxide (t/y)</u> | Nitrogen Dioxide (t/y) |
|-------------------------------------|------------------------------------|-----------------|--------------------------------|---------------------------|
| Potential Emissions ^a | -6158 | +770 | -1240 ^b | +40 |
| Allowable Emissions ^a | -1006 | -1 | -1240 ^b | +40 |

aBased on the assumption that emission sources operate continuously throughout the year. Continuous operation is not actually possible, of course. However, the normal operating hours of offsetting fluoride emission sources are such that assuming continuous operation assures no underestimation of annual potential or allowable fluoride emissions. The continuous operation assumption also provides an upper limit on nitrogen dioxide emissions from the No. 5 Ammonium Phosphate Plant.

^bSulfur dioxide emissions result from operation of the No. 7 Sulfuric Acid Plant. Since emission controls are integral to the acid production process, potential and allowable emissions are assumed to be equivalent.

Superphosphate Plant will be dismantled and will no longer be even a potential source of emissions.

As a concluding note, there will also be sulfuric acid mist emissions from the No. 7 Sulfuric Acid Plant. Allowable emissions will decrease from the present limit of 17.3 lb/h (72 tons/year) to 10.9 lb/h (46 tons/year) after modifications have been completed. (The annual rate is based on an operating schedule of approximately 8300 hours/year.) This amounts to a net reduction of approximately 26 tons/year.

4.2 <u>DERIVATION OF EMISSION RATE ESTIMATES</u>

Existing Emission Sources

The allowable emission rates shown in Tables 4-1 through 4-3 for existing emission sources scheduled to be shut down or modified are the limits specified in current state permits.

New Particulate Matter Emission Source

The only new particulate matter emission source involved in the proposed project is the No. 5 Ammonium Phosphate Plant. At present there is not a specific federal New Source Performance Standard or a Florida emission limiting standard for particulate emissions from diammonium phosphate production units. The estimated maximum emission rate of 10 lb/h shown in Table 4-1 is based on performance data for comparable new equipment operated elsewhere within the Florida phosphate industry. The allowable emission rate based solely on Florida process weight rate standards would be much higher than 10 lb/h (see Table 6-1), but Gardinier is confident of achieving an emission rate of no greater than 10 lb/h and is willing to accept this rate as a condition of state and federal permits.

New and Modified Fluoride Emission Sources

The allowable fluoride emission rates listed in Table 4-2 for new and modified facilities are based strictly on the rates allowed by

federal New Source Performance Standards and Florida emission limiting standards specific to these types of facilities (wet-process phosphoric acid plants and diammonium phosphate plants). Applicable standards and equivalent P_2O_5 process quantities used to develop emission rates are presented in a later section (in Table 6-1). Actual emission rates are expected to be somewhat less than allowed by emission standards (see Table 6-1), but Gardinier requests that permit emission restrictions be no more stringent than required by performance standards for new sources.

XF

Modified Sulfur Dioxide Emission Source

The only source of sulfur dioxide affected by the proposed project is the No. 7 Sulfuric Acid Plant. The emission rate shown in Table 4-3 for the modified facility is derived from the federal New Source Performance Standard and Florida emission limiting standard for new sources as shown in Table 6-1.

New Nitrogen Dioxide Emission Source

The only new source of nitrogen dioxide emissions is the No. 5 Ammonium Phosphate Plant. Relatively low emissions of NO_X are expected to result from combustion of No. 6 fuel oil in the dryer. Specific state or federal NO_X emission standards for this type of combustion do not exist. The emission rate shown in Table 4-4 is derived from the AP-42 emission factor for industrial boilers which is 60 lb NO_2 per thousand gallons of residual fuel oil burned. Based on an expected fuel combustion rate of 150 gal/h, the resulting emission rate estimate is 9 lb/h.

4.3 TIMING OF EMISSION SOURCE CHANGES

Particulate Matter Emission Sources

The only new source of particulate matter emissions is the No. 5

Ammonium Phosphate Plant. At least one of the dry rock grinding mills 10

listed in Table 4-1 with sufficient emissions to offset the No. 5 Ammonium Phosphate Plant will have shut down by the time the No. 5 Plant

becomes operational. All of the existing facilities scheduled for shut down as listed in Table 4-1 will have ceased operation within nine months of the startup of the No. 5 Ammonium Phosphate Plant. In summary, there will not be any period when allowable emissions of particulate matter will exceed those presently in effect.

Sulfur Dioxide Emission Source

The only sulfur dioxide emission source involved in the proposed project is the No. 7 Sulfuric Acid Plant. This plant will be out of service while undergoing final modifications (a phase which will last approximately 6 weeks), and when started back up will be operating at a lower allowable emission rate than at present.

Flouride Emission Sources

The present schedule for shutting down, modifying, and adding the fluoride emission sources listed in Table 4-2 is somewhat complicated. Before getting into the details of this schedule, however, it should be recognized that even if all of the new and modified emission sources were operating at full capacity simultaneously with sources slated to be shut down (a situation which will not occur), the total allowable fluoride emission rate would only be 6.4 pounds per hour (equivalent to an annual rate of 28 tons). The question of overlapping operating periods is therefore not particularly significant.

The total period scheduled for adding, modifying, and shutting down sources is approximately 23 months after construction permits are obtained. During this time there may be overlapping periods when fluoride emission sources not presently in operation will be operating simultaneously with existing sources before modification or shut down. The current development schedule showing maximum periods of overlap is presented in Figure 4-1.

This figure should be evaluated with three considerations in mind. First, the periods of overlap include testing phases for the No. 3 Phosphoric Acid Plant, No. 4 Phosphoric Acid Plant, and No. 5 Ammonium Phosphate Plant. The testing phase for each plant will last

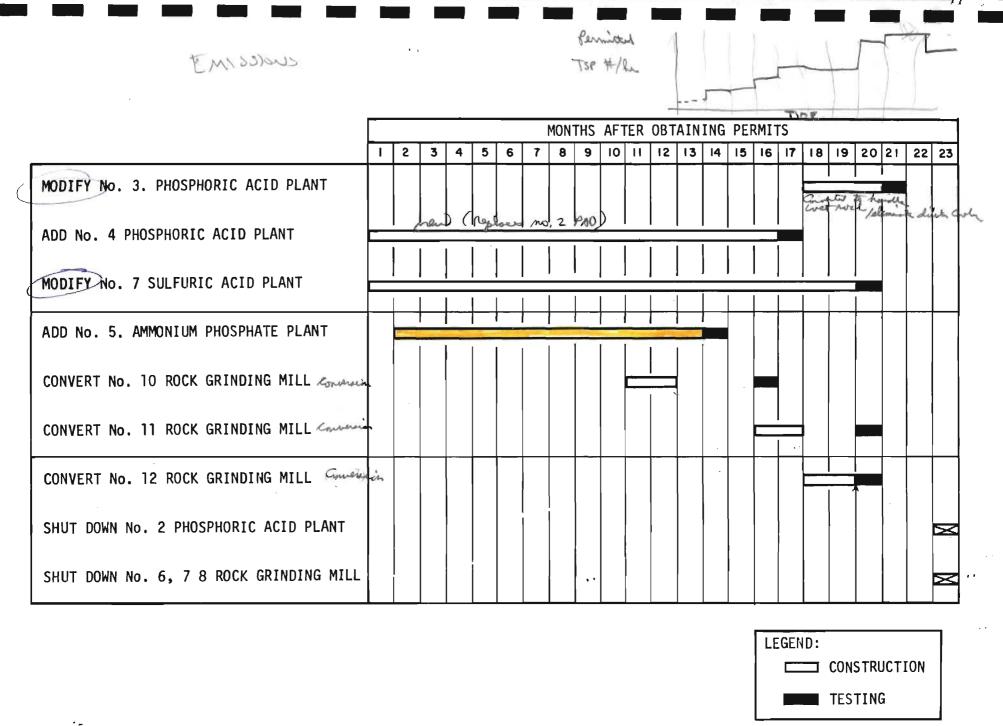


Figure 4-1. Proposed Project Development Schedule.

approximately one month, during which time fluoride emissions will be intermittent rather than continuous. Second, the raw material supply available for the entire plant complex will not allow each existing and new facility to be operated simultaneously at full capacity. As a result, total fluoride emissions even during overlap periods will be essentially equal to present emissions. Third, the schedule for development of the No. 5 Ammonium Phosphate Plant is somewhat flexible and could be adjusted to reduce the duration of overlap periods if necessary.

REGULATORY CONSIDERATIONS

Under the existing regulations governing PSD, new or modified sources with allowable emissions of less than 50 tons/year are exempt from full PSD review. In accordance with these regulations, such sources need not: demonstrate the use of Best Available Control Technology (BACT); demonstrate that the source would not cause or contribute to violations of applicable PSD increments or the national ambient air quality standards (NAAQS); assess direct or indirect effects of the source on visibility, soils or vegetation; or provide ambient air quality monitoring data, unless the source is expected to impact a PSD Class I area or an area where an applicable increment or standard is known to be violated. An applicant must, however, demonstrate that the source would meet all applicable emission limitations regulated under the state implementation plan (SIP) and all applicable emission standards and new source performance standards (NSPS) under 40 CFR, parts 60 and 61.

In discussing Gardinier's project with EPA, a question arose as to whether or not the proposed modification of the No. 7 Sulfuric Acid Plant requires a BACT analysis. Allowable SO₂ emissions from the modified facility will exceed 50 tons per year, but in comparison with allowable $S0_2$ emissions from the existing facility there will be a decrease in allowable emissions of 1240 tons per year (as shown in Table 4-5). Gardinier recognizes that achieving internal emission offsets does not provide an exemption from BACT review when there is an increase in emissions of 50 tons per year or more at one facility and an offsetting emissions reduction at an entirely separate facility within the same plant complex. In the present case, however, the offset is being achieved as a result of modifying a single facility, the No. 7 Sulfuric Acid Plant. In this situation, Gardinier feels that section 52.21 (j)(3) of the existing PSD regulations is governing. This section states that "In the case of modification, the requirement for best available control technology shall apply only to each new or modified facility which would increase the allowable emissions of an

applicable pollutant." (The term facility is defined as "an identifiable piece of process equipment.") However, since the question of BACT applicability has not been resolved, a further discussion of modifications proposed for the No. 7 Sulfuric Acid Plant is provided in Section 6 in the event that EPA requires further assurance on planned emission controls.

Inasmuch as all allowable net increases in emissions for the proposed additions and modifications to this plant complex are less than 50 tons/year (see Table 4-5), and furthermore in that the allowable emissions from individual new and modified facilities are less than 50 tons/year without offsets (except for the No. 7 Sulfuric Acid Plant as discussed above), it is expected that the proposed changes will be exempt from full PSD review. Regarding the demonstration of compliance with state and federal emission limitation standards, this will be shown in Section 6.

At the present time, the area of Hillsborough County in which the Tampa Chemical Plant is located is officially designated as a nonattainment area for particulate matter. In view of this situation, it is necessary to ensure that there will be no adverse air quality impact on this nonattainment area as a result of the proposed modifications.

Ambient air quality considerations are discussed in Section 7.

6. EMISSION CONTROL

As discussed in the previous section, a demonstration of BACT is not expected to be required for the permitting of these facilities since all allowable net changes in contaminant emissions are less than 50 tons/year. It should be noted, however, that all new and modified facilities will be equipped with technologically current emission control devices to ensure that the best available emission control technology is in fact being utilized.

Because the Tampa Chemical Plant is located within a nonattainment area for total suspended particulates, particulate matter emissions are of special concern. As shown in Table 4-1, there will be a net <u>reduction</u> in allowable particulate matter emissions of about 210 lb/h (920 ton/yr) as a result of these modifications (not counting reduction in fugitive dust emissions). The primary reason for the large reduction in particulate matter emissions is the conversion to wet-rock processing and consequent elimination of dry-rock grinding and handling.

As required under the regulations governing PSD, it is necessary to demonstrate compliance with all applicable state and Federal emission limitation standards. Table 6-1 sets forth these standards, compared with the expected maximum emission rates for each facility. As shown in the table, emission standards for this facility apply to fluorides (No. 3 and No. 4 Phosphoric Acid Plants and the No. 5 Ammonium Phosphate Plant), particulates (No. 5 Ammonium Phosphate Plant), as well as sulfur dioxide and sulfuric acid mist (No. 7 Sulfuric Acid Plant). All of these emissions are shown to be lower than or equal to the applicable emission standard.

Comments were made in Section 5. on the question of whether or not a BACT analysis is required for the No. 7 Sulfuric Acid Plant. Without discussing further the regulatory aspects of this question, additional information on modifications proposed for this facility is provided below. This information is taken in part from the construction permit application copy contained in the appendix.

TABLE 6-1

COMPARISON OF ACTUAL FACILITY EMISSIONS VERSUS
APPLICABLE EMISSION LIMITATION STANDARDS

| <u>Facility</u> | Product | Process Rate (1b/h) | Contaminant | Expected Maximum Emission Rate (lb/h) | Applicablea Emission Standard (lb/ton) | Emission Limitation (1b/h) |
|-----------------------------------|--------------------------------|--|--|---------------------------------------|---|----------------------------------|
| No. 3 Phosphoric Acid Plant | Phosphoric Acid | 93,000 (P ₂ 0 ₅) | Fluorides | 0.83 | 0.02 1b/ton of P ₂ 0 ₅ | 0.9 |
| No. 4 Phosphoric Acid Plant | Phosphoric Acid | 120,000 (P ₂ 0 ₅) | Fluorides | 0.83 | 0.02 1b/ton of P ₂ 0 ₅ | 1.2 |
| No. 5 Ammonium Phosphate Plant | Di-Ammonium Phosphate | 46,000 (P ₂ 0 ₅) | Fluorides | 1.4 | 0.06 1b/ton of P ₂ 0 ₅ | 1.4 |
| n | II | 100,000 (Process input) | Particulates | 10.0 | 17.31P ^{0.16b} | 32.4 |
| No. 7 Sulfuric Acid Plant | H ₂ S0 ₄ | 145,833 (H ₂ SO ₄) | s0 ₂ | 291.7 | 4 lb/ton of H ₂ SO ₄ | 291.7 |
| н | и | п | H ₂ SO ₄ (mist) | 10.9 | 0.15 lb/ton of H ₂ SO ₄ | 10.9 |

^aState and Federal standards are equivalent except where noted.

^bState standard only. "P" represents process feed rate in tons per hour.

The modifications undertaken will increase plant capacity from 1380 tons of 100% sulfuric acid per day to 1750 tons per day. This will be accomplished by the following changes:

- Drying Tower Replace packed spray catcher with a mesh pad; remaining tower internals will not be changed.
- 2. <u>Sulfur Burner</u> Change sulfur sprays to handle 60 gallons per minute (gpm) of sulfur.
- 3. Sulfur Pumps Increase capacity to 60 gpm.
- 4. No. 1 Waste Heat Boiler New boiler required.
- 5. Converter Installation of an additional 21,000 liters of Type 210 catalyst will keep SO_2 emission levels below 4.0 lb/ton H_2SO_4 .
- 6. <u>Superheaters</u> No. 2 superheater must be retubed. Allowance was made in the original design to accommodate sufficient additional surface area without rebuilding the converter internals.
- Economizer One additional section must be added.
- 8. <u>Interpass Absorption Tower</u> Install additional HVM mist eliminators in spaces provided. Remainder of interpass tower and internals are adequate. (It is expected that no additional mist eliminators will be required upstream of booster blower.)
- 9. <u>Booster Blower</u> Install new booster blower between interpass absorption tower and shell side of No. 1 cold heat exchanger. Blower to handle 69,000 SCFM at approximately 75 inches w.g. and approximately 175°F.
- 10. <u>Mesh Pad and Vessel</u> Install new S.S. mesh pad in new vessel at discharge of booster blower to protect cold heat exchanger.

- 11. <u>Acid Coolers</u> Rearrange existing radiator coolers to provide seven cooler banks for D.T. circuit duty, sixteen cooler banks for IPAT circuit duty, and two cooler banks for product acid duty.
- 12. Acid Pumps Increase D.T. acid pump capacity to 3,700 gpm and IPAT acid pump capacity to 5,000 gpm.

Sulfur dioxide emissions control is accomplished as an integral part of the acid production process within the double-absorption converter. Improvements in the system will permit the modified plant to achieve compliance with federal New Source Performance Standards. Although it is theoretically conceivable that additional emissions control could be achieved by some add-on stack flue gas desulfurization system, discussion with vendors confirms that double-absorption is sufficient to achieve emission standards for new sources and that flue gas controls are neither practical nor necessary.

It is recognized that BACT decisions are not based solely on compliance with emission standards but must be made on a "case-by-case" basis which may suggest emission limits more stringent than allowed by emission standards. In this regard, an important point to consider for Gardiner's project is that compliance with new source standards will result in a decrease in allowable emissions on both a pound of SO_2 per ton of acid basis and on a total tons per year of SO_2 basis. Therefore, in this "case," defining BACT as equivalent to NSPS will result in air quality improvement. Defining BACT any more stringently than this does not seem justified.

7. AMBIENT AIR QUALITY

7.1 GENERAL

Since net emission changes (for any pollutant) will not exceed 50 tons/year, the existing regulations governing PSD do not require that an estimate of air quality impact be made. It should be noted, moreover, that only emissions of nitrogen dioxide will be increased as a result of facility modifications. Nitrogen dioxide emissions will result from the operation of the No. 5 Ammonium Phosphate Plant at an estimated maximum rate of 40 tons/year (9 lb/h); however, such a small emission rate should have an almost negligible effect on ambient levels of NO₂ in relation to the ambient standard for NO₂ which is an annual average standard.

Because the Tampa Chemical Plant is located in a particulate matter nonattainment area, there may be some concern about whether or not proposed particulate emission reductions will also result in reduced ambient concentrations. By reference to Table 4-1, it can easily be seen that the effective stack height (physical stack height plus plume rise) of the new particulate matter source (No. 5 Ammonium Phosphate) will exceed that of sources which will be shut down. This difference in effective stack height results from the much greater volumetric flow of the new source coupled with a stack height and exit temperature which are comparable to those of the sources which will be shut down. According to standard Gaussian modeling concepts, a higher effective stack height will necessarily lead to reduced ground-level impacts provided emissions do not increase.

As an example of differences in effective stack height, consider the No.5 Ammonium Phosphate Plant in comparison with the outlet handling emissions from the No. 6, 7, 8, 10 Rock Grinding Mills. (The No. 6, 7, 8, 10 Rock Grinding Mills outlet is selected for comparison because it has the highest effective stack height of the existing particulate emission source due to temperature and volumetric flow characteristics.) The physical stack heights of these two emission points

are nearly the same (90 ft and 95 ft); therefore, any difference in effective stack height will be due to plume rise. Using the Briggs plume rise calculation method commonly applied in evaluations of this type, the expected plume rise of the No. 5 Ammonium Phosphate Plant plume is four times greater than the plume rise of the Rock Grinding Mills during unstable and neutral atmospheric conditions, and two times greater during stable conditions. Coupled with reduced particulate emissions, the increase in effective stack height should result in lower ground-level concentrations.

7.2 PSD CLASS I AREA IMPACT

The nearest Class I area to Gardinier's Tampa Chemical Plant site is the Chassahowitzka NWA located 90 km to the north. This area is far beyond any expected range of influence for this plant complex (for any pollutant) and consequently there will be no adverse impact on it as a result of the proposed modifications.

8. STATE OF FLORIDA PERMIT APPLICATIONS

The proposed modifications and additions to Gardinier's Tampa Chemical Plant are currently undergoing review by the Florida DER. (In fact, a construction permit for the No. 3 Phosphoric Acid Plant has already been issued.) Copies of construction permit applications submitted to DER are included in the Appendix for the following sources:

- ° No. 3 Phosphoric Acid Plant
- ° No. 4 Phosphoric Acid Plant
- ° No. 7 Sulfuric Acid Plant
- ° No. 5 Ammonium Phosphate Plant

9. CONCLUSIONS

It has been shown previously that the <u>net</u> change in allowable emission rates as a result of proposed modifications will not exceed 50 tons/year for any pollutant thereby presumably exempting this application from full (tier 2) PSD review. Moreover, it is evident from the previous discussion that the proposed modifications and additions to this facility will not result in any adverse air quality impacts either in the surrounding area or in any PSD Class I area. It has further been shown that contaminant emissions will comply with the applicable state and federal emission limitation standards for the particular processes in question.

APPENDIX

This apendix contains relevant portions of construction permit applications as submitted to the Florida Department of Environmental Regulation (DER) for the following facilities:

No. 3 Phosphoric Acid Plant NEW MOD, NEW ENCEL. EQUIP.

No. 4 Phosphoric Acid Plant NOD. 502 & AC, AO

No. 7 Sulfuric Acid Plant NOD. 502 & AC, AO

No. 5 Ammonium Phosphate Plant NEW MOD.

HAVE MODEL RESULTS.

NO. 3 PHOSPHORIC ACID PLANT





STATE OF FLORIDA

DEPARTMENT OF ENVIRONMENTAL REGULATION

APPLICATION TO OPERATE/CONSTRUCT AIR POLLUTION SOURCES

| <u> </u> | | | <u> </u> | | |
|---|---|--|---|--|--|
| arca Type: rpe application: | Air Pollution [X] | Incinerator [] [X] Construction | | | |
| mpany Name: | [] New Gardinier, Inc | [] Existing | [X] Modification | _ County: Hillsborough | |
| ource identification | n: No. 3 Phosphor | ic Acid Plant | | | |
| urce Location: St | U.S. Highway | 41 and Rivery | iew Drive | _ City: South of Tampa | |
| UTM: East _ | 362.9 | | North | 3082.5 | |
| ol, Name and Tit | Rudy J. Cabi | na, Vice Presid | dent | | |
| opl. Address: | P.O. Box 326 | 9, Tampa, Flori | ida 33601 | | |
| | | STATEMENTS BY | APPLICANT AND ENG | INEER - | |
| APPLICANT | | | | | |
| | rsigned owner or authoriz | | | | |
| I certify that t | the statements made in th | is application for a | Construction | | permit are |
| pollution contions of the D | mol facilities in such a m | anner as to comply withereof, I also understa | ith the provisions of Cha and that a permit, if grant | to maintain and operate the pollution contribute 403, Florida Statutes, and all the rule ted by the Department, will be nontransferated. | s and regula- |
| | | By: | Roul | Colonie Vice Presid | ent |
| 1 | | | Signalure of th | he Owner or Authorized Representative and | Title |
| | | | Date: 6/8/7 | 7.9 Telephone No.: 813- | 677-9111 |
| | | | | tanding must be submitted with application. Tallahassee, Florida 32304. | . This may be |
| PROFESSION | IAL ENGINEER REGIST | ERED IN FLORIDA | • | • | |
| formity with There is reason discharge an e also agreed th | modem engineering prin nable assurance, in my pr officient that complies wi | ciples applicable to the rofessional judgment, the all applicable statute furnish the applicant is | e treatment and dispose that the pollution controllers of the State of Florid | been designed/examined by me and found at of politizants characterized in the permit of facilities, when properly maintained and it and the rules and regulation of the Depthe proper maintenance and operation of | t application. operated, will artment, It is |
| Signature: | CofDan | herly | Mailing Adores | P.O. Box 3269, Tampa, Flo | <u>rida 336</u> 0 |
| Neme: | C. S. Daug (Please Ty | | | | |
| Company Nam | e: Gardinier, | Inc. | Telephone No. | 813-677-9111 | |
| Florida Registi | ration Number: 2115 | 0 | Date: | 6/8/79 | |
| | (Affix Seal) | | | | |

DETAILED DESCRIPTION OF SOURCE

| 2 Phosphort | c Acid Plant will be | modified to process wet ground Phosphate rock. |
|--|---------------------------------------|---|
| odifications t | o the existing cross | flow scrubber will be performed to handle increase |
| | | gestion system. |
| 1407146 670146 | 2011 2102 2110 10011 427 | Beerzen Byereet |
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| | | • |
| chequie of Project Cov | erec in this Application (Constru | uction Permit Application Only). |
| | | |
| State of Controlstics | n: April | 1, 1980 |
| Completion of Cons | mustion: April | 1, 1983 |
| Completion of Cons | rection. | • |
| | | |
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| | | |
| or this source indicate | any previous DER permits, orde | ers, and notices; including issuance dates and expiration dates. |
| | • | ers, and notices; including issuance dates and expiration dates. |
| ermit | Issued | ers, and notices; including issuance dates and expiration dates. Expire |
| ermit | • | ers, and notices; including issuance dates and expiration dates. |
| ermit | Issued | ers, and notices; including issuance dates and expiration dates. Expire 7/15/83 |
| ermit | Issued | Expire 7/15/83 |
| ermit | Issued | Expire 7/15/83 |
| ermit | Issued | Expire 7/15/83 |
| ermit | Issued | Expire 7/15/83 |
| ermit | Issued | Expire 7/15/83 |
| or this source indicate Permit A029-6752 | Issued | Expire 7/15/83 |
| Permit A029-6752 | Issued | Expire 7/15/83 |

22F-2, Florida Administrative Code? _____ Yes __X_ No

father than incinerators) **BEST AVAILABLE COPY** Identification of Air Contaminants: of 1 1 Other (Identify) el [] Smoke bl [] Fly Ash 21 [] Sulfur Compounds e) [] Other (identify) b) [] Reduced Sulfur as H2S 3) [] Nitrogen Compounds 3 Other (identity) PHU [] [4] Acid Mist 1 Volatile Organic Compounds Raw Materials and Chemicals Used (Be Specific): Approximate Utilization Contaminant Relate to Content Rate Flow Diagram be Ins. % W. Type Y 3.5 310,000 Fluoride B· 238,960 • 276,950 C 548,960 lb/hr X85XXXXX 1b/hr P205

Process Rate:

hrs. Jday:

Water .

1) [] Particulates

a) [] \$0, a: \$0,7

a) [] NO, as NO2

7) I | Hydrocarbons

1 Other (Specify):

Description

Phosphate Rock

Sulfuric Acid

4) [X] Fluorides

al [] Dust

- 1) Total Process Input Rate (Units*): 88,350 ·

- H sessonal describe: not seasonal 7,600 hr/yr 3) Normal Operating Time: 20.8 days/wk:
- Airporne Contaminants Discharged:

| Name of | Actual** Discharge | | Discharge Criteria | Allowable Discharge | Relate to Flow Diagram |
|-------------|--------------------|-------|-----------------------|------------------------|------------------------|
| Conseninant | . I>iJhr. | T/y:. | Rate* | lbs.Jhr. | LIOM DISÉLUM |
| | 1 | | 1 | | 1 |
| Fluoride | 0.83 | 3.2 | 10.02 1b F/ton Pool | 0.9 | l D |
| | 1 | | 1 input | | 1 |
| | <u> </u> | • | 1 | | 1 |
| | 1 | | 1 | | 1. |
| | 1 | | 1 | | 1 |
| | 1 | | 1 | | 1 |

fer to Chapter 17-2.04(2), Florida Administrative Code. (Discharge Criteria: Rate = tbs./ton F2Os. lbs./M BTU/nr_etc.)

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***This figure is revised from figure originally submitted to DER.

| Name and Type [Model and Serial No.] | Contaminant | Efficiency* | Conditions of Operations | Basis for Efficiency Operational Data, Test, Design, Data |
|---|-----------------------|--------------------|---------------------------------------|---|
| | | | · · · · · · · · · · · · · · · · · · · | |
| Teller Crossflow | Fluoride | 99+ | 1 | Design |
| | | | | |
| | <u> </u> | | <u> </u> | |
| · | | | 1 | |
| | | | | |
| | 1 | | | |
| | | • | 1 | |
| required supplement. Jude any test data and/or design da Fuels: No fuels are u | | tantistion) | • | |
| Type (Be Specific) | | Consumption | ١• | Maximum Heat Input |
| | Lava . | h:. | Max,/hr. | MMBTU/hr. |
| | | | | |
| • | | 1 | • | |
| | | · | | to a transfer of the second |
| • | | | | |
| Fuel Analysis: Percent Surfur: Density: Heat Capacity: Other Fuel Contaminants: | Oils, Coal — Ibs.Jhr. | Perci | | BTU/s |
| Indicate liquid or solid wates p | | | to the in-plan | nt water recycle system. |
| | | | | |
| | | | | |
| • | | • . | | |
| Emission Stack Geometry and F Stack Height: 9 | | provide data for e | sch stack): Stack Diamete | 4.0 |
| | 9 000 | | | 105 |
| Gzs Flow Rate:4 | | AC | FM Gas Exit Temp | perature: |
| Water Vapor Content: | <u>.</u> | * | | • |

Please Provide the Following Required Supplements For All Pollution Sources:

- . Total process input rate and product weight show derivation. See below.
- 2. Efficiency estimation show derivation. See below.
- . An 8%" x 11" flow diagram, which will, without revealing trade secrets, identify the individual operations and/or processes. Indicate where raw materials enter, where solid and liquid waste exit, where gaseous emissions and/or airborne particles are evolved and where finished products are obtained.

 See attached.
- . An 8%" x 11" plot plan showing the exact location of manufacturing processes and outlets for airborne emissions. Relate all flows to the flow diagram. See attached.
- i. An BX" x 11" plot plan showing the exact location of the establishment, and points of airborne emissions in relation to the surrounding area, residences and other permanent structures and roadways. See attached.
- Description and sketch of storm water control measures taken both during and after construction.

Process Input Rate

Product Weight

Phosphate Rock - 310,000 lb/hr 29% P205

Phosphoric Acid, 29% P205

Sulfuric Acid - 238,960 lb/hr

 $310,000 \times .29 = 89,900^{+} lb/hr P205$

Water - 276,950 lb/hr

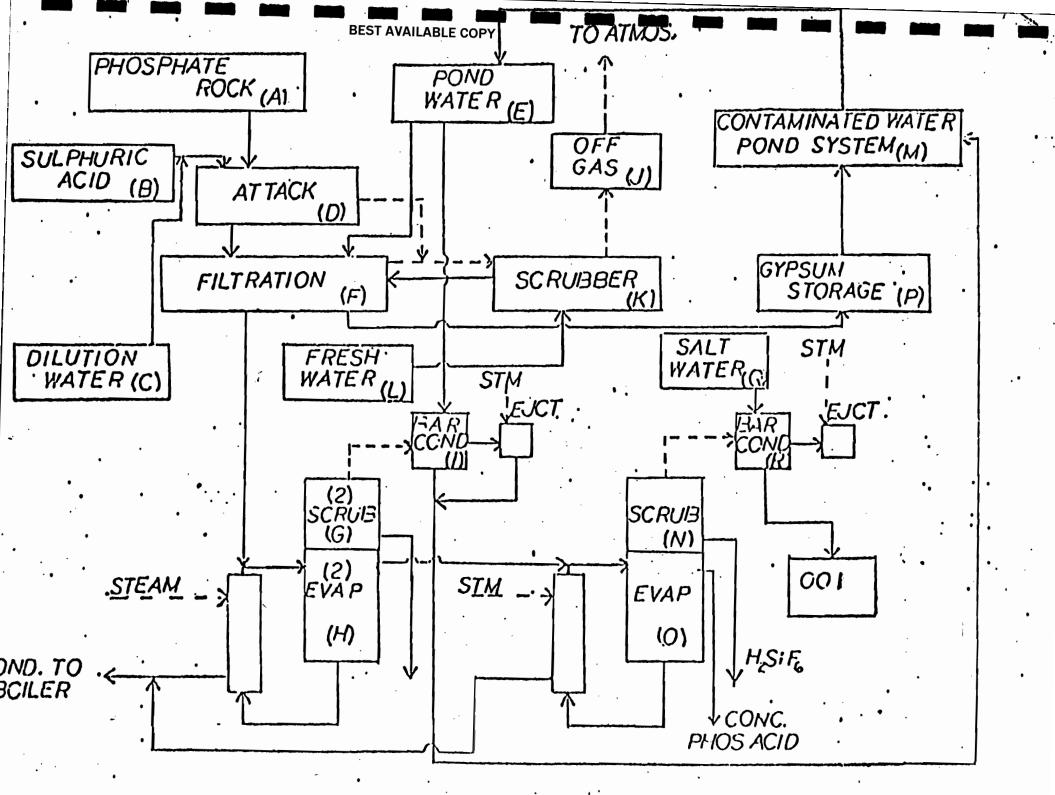
89,900 + .29 = 310,000 lb/hr 29% P205 Acid

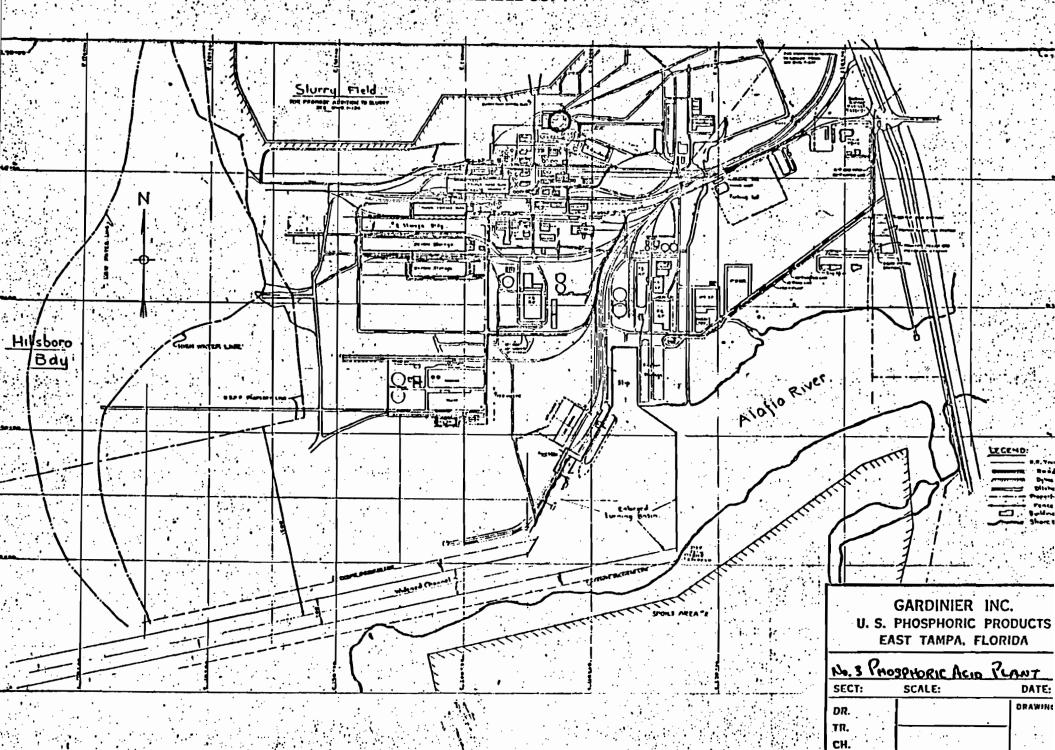
310,000 X .95 = 294,500 lb/hr 29% P205 Ac.

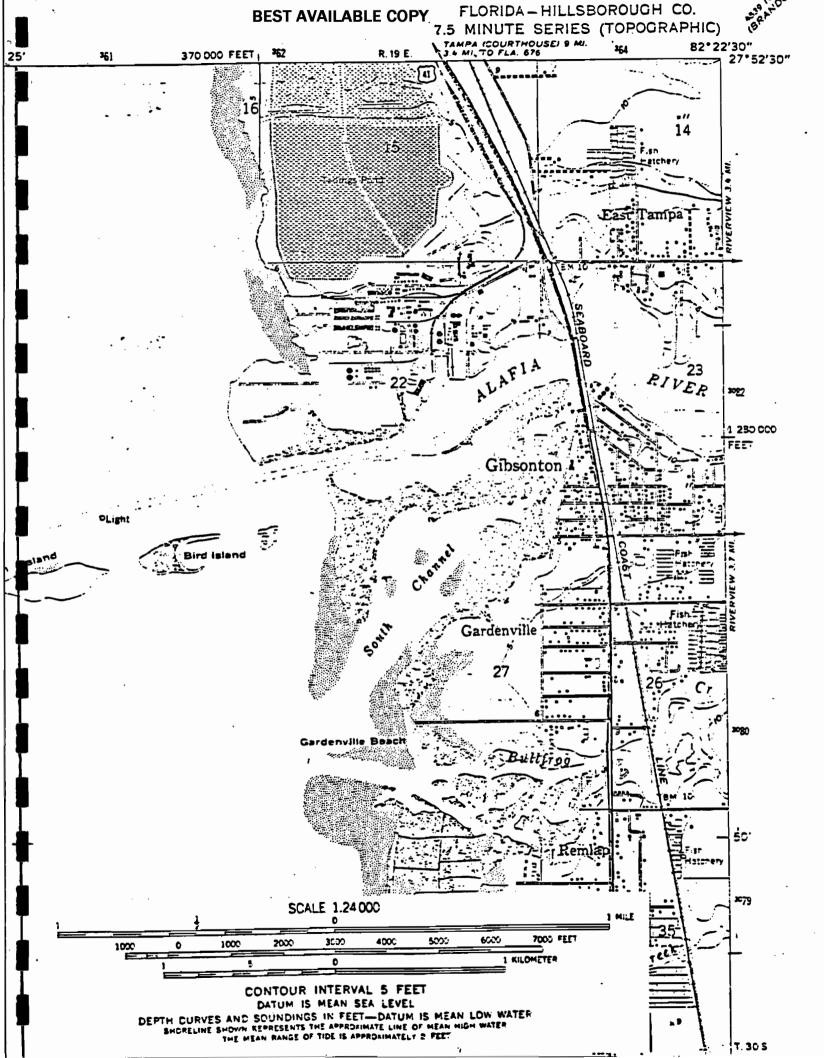
. = 85,405 lb/hr P205 Recovered

Only scrubber exit loadings are measured. Efficiency cannot be measured.

 $^{\star}\mathrm{P_{2}0_{5}}$ process input rate has been revised to 93,000 lb/hr.







NO. 4 PHOSPHORIC ACID PLANT





STATE OF FLORIDA DEPARTMENT OF ENVIRONMENTAL REGULATION

APPLICATION TO OPERATE/CONSTRUCT AIR POLLUTION SOURCES

| Turce Type: Air Pollution (X) Incin | perator [] | | • . • |
|--|--|--|---|
| pe application: [] Operation [X] | Construction | | • |
| mpany Name: Gardinier, Inc. | Existing [] Modification | Hillsbor | eough : |
| Ource Identification: No. 4 Phosphoric A | cid Plant | County: | |
| urce Location: Street: U.S. Highway 41 | South | City: South of | Татра |
| UTM: East 362.9 | North | 3082.5 | • |
| pol. Name and Title: Rudy J. Cabina, | Vice President | · · · · · · · · · · · · · · · · · · · | |
| P.O. Box 3269, | Tampa, Florida 33601 | | |
| STA | ATEMENTS BY APPLICANT AND | ENGINEER . | |
| APPLICANT | • | | • |
| I am the undersigned owner or authorized repr | esentative of <u>Gardinier</u> , I | Inc. | • |
| I certify that the statements made in this applic | cation for m. Construction | 1 | Dermit are |
| true, correct and complete to the best of my pollution control facilities in such a manner a tions of the Department and revisions thereof promptly notify the Department upon sale or i | is to comply with the provisions of . I also understand that a permit, if | Chapter 403, Florids Statutes, granted by the Department, will inhumant. | and all the rules and regula- |
| | · | of the Cwner or Authorized Re | |
| - | Date: | I . | No.: 813-677-9111 |
| *Attach a letter of authorization, If applicant in obtained for a \$5.00 charge from the Secretary | - | od Standing must be submitted v | with application. This may be |
| PROFESSIONAL ENGINEER REGISTERED | IN FLORIDA | | • |
| This is to certify that the engineering features formity with modern engineering principles a There is reasonable assurance, in my profession discharge an effluent that complies with all a also agreed that the undersigned will furnish control facilities and, if applicable, pollution so | explicable to the treatment and displicable to the treatment and displicable statutes of the State of Figure applicant a set of instructions | sposal of pollutants characteriz ontrol facilities, when properly r florida and the rules and regula | ed in the permit application, maintained and operated, will tion of the Department. It is |
| Signature: C. S. Daugherty | Mailing Ad | • | 22501 |
| Name: C. S. Daugherev (Please Type) | | Tampa, Florida | 10001 |
| | - | <u> </u> | |
| Company Name: Gardinier, Inc. | Telephone | No.: 813-677-9111 | |
| Fiorida Registration Number: 211 | 150 Date: | 6/8/79 | |
| : | | . / / | |

DETAILED DESCRIPTION OF SOURCE

| | ure and extent of the project. Refer to existing pollution control facilities, expected improvement in performance of the fether the project will result in full compliance. Attach additional sheet if necessary. |
|------------------|--|
| This plant | will replace the existing No. 2 Phosphoric Acid System. The existing system |
| three scri | bbers will be replaced by one emission point. Emissions of fluoride will be |
| | om a permitted level of 55.7 lbs/day to approximately 20 lbs/day. The No. 4 |
| | Acid Plant will utilize best available control technology. |
| r noopnozze | |
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| Schedule of Pro | ect Covered in this Application (Construction Permit Application Only). |
| | A |
| | trustion: April 1, 1980 |
| Completion | f Construction: April 1, 1983 |
| | |
| | |
| Packed Cro | ssflow Scrubber with attendant equipment - \$1,000,000 |
| Packed Cro | ssflow Scrubber with attendant equipment - \$1,000,000 |
| Packed Cro | ssflow Scrubber with attendant equipment - \$1,000,000 |
| Packed Cro | ssflow Scrubber with attendant equipment - \$1,000,000 |
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| Packed Cro | ssflow Scrubber with attendant equipment - \$1,000,000 |
| Packed Cro | |
| Packed Cro | ssflow Scrubber with attendant equipment - \$1,000,000 |
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| | |
| or this source i | |
| | |

AIR POLLUTION SOURCES & CONTROL DEVICES (other than incinerators)

| 1) [] Particulates a) [] Dust | γl |
|---|----|
| a) [] SO _X as SO ₂ b) [] Reduced Sulfur as H ₂ S c) [] Other (Identify) 3) [] Nitrogen Compounds a) [] NO _X as NO ₂ b) [] NH ₃ c) [] Other (Identify) 4) [X] Fluorides 5) [] Acid Mist 6) [] Odor 7) [] Hydrocarbons 8) [] Volatile Organic Compounds 9) [] Other (Specify): w Materials and Chemicals Used (Be Specific): Description Utilization Rate Ibs./hr. Type % Wt. Osphate Rock 400,000 Fluoride 3.5 A | |
| a) [] SO _X as SO ₂ b) [] Reduced Sulfur as H ₂ S c) [] Other (Identify) 3) [] Nitrogen Compounds a) [] NO _X as NO ₂ b) [] NH ₃ c) [] Other (Identify) 4) [X] Fluorides S) [] Acid Mist 6) [] Odor 7) [] Hydrocarbons 8) [] Volatile Organic Compounds 9) [] Other (Specify): w Materials and Chemicals Used (Be Specific): Description Utilization Rate Ibs./hr. Type % Wt. Psphate Rock 400,000 Fluoride 3.5 A | |
| a) [] NO _X as NO ₂ b) [] NH ₃ c) [] Other (Identify) 4) [X] Fluorides 5) [] Acid Mist 6) [] Odor 7) [] Hydrocarbons 8) !] Volatile Organic Compounds 9) [] Other (Specify): w Materials and Chemicals Used (Be Specific): Description Utilization Rete Ibs./hr. Type % Wt. Sphate Rock 400,000 Fluoride 3.5 A | |
| 4) [X] Fluorides 5) [] Acid Mist 6) [] Odor 7) [] Hydrocarbons 8) [] Volatile Organic Compounds 9) [] Other (Specify): w Materials and Chemicals Used (Be Specific): Description Utilization Rete Contaminant Content Flow Diagram Type % Wt. sphate Rock 400,000 Fluoride 3.5 A | |
| 7) [] Hydrocarbons 8) [] Volatile Organic Compounds 9) [] Other (Specify): w Materials and Chemicals Used (Be Specific): Description Utilization Contaminant Contaminant | |
| 9) [] Other (Specify): w Materials and Chemicals Used (Be Specific): Description Description Description Utilization Rate Ibs./hr. Type Wt. Sphate Rock 400,000 Fluoride 3.5 A Provide Specific Plan Content Flow Diagram Approximate - Content Flow Diagram Flow Diagram A | |
| Materials and Chemicals Used (Be Specific): Description | |
| W Materials and Chemicals Used (Be Specific): Description | |
| osphate Rock 400,000 Fluoride 3.5 A | |
| osphate Rock 400,000 Fidoride 500 | |
| Efuric Acid, 100% 308,333 B | |
| | |
| cer 357,357 - C | |
| | |

D. - Airborne Contaminants Discharged:

| Name of Contaminant | Actual** Discharge | | Discharge Criteria | Allowable Discharge | Relate to Flow Diagram | |
|---------------------|-----------------------|------|-----------------------|------------------------|------------------------|--|
| Contaminant | Lbs./hr. T/yr. | | , Rate* | lbs./hr. | Plow Diagram | |
| Fluoride | 0.83 | 3.17 | 10.02 #F/ton P205 f | nput 1.2 | J | |
| | | | | | • | |
| | | - | <u> </u> | <u> </u> | | |
| | <u> </u> | • | <u> </u> | <u> </u> | | |
| | | | | | | |
| , | | | | | | |

*Refer to Chapter 17-2.04(2), Florida Administrative Code.

(Discharge Criteria: Plate = Ibs./ton P2O5, Ibs./M BTU/hr., etc.)

** Estimate only if this is an application to construct.

***This figure is revised from figure originally submitted to DER.

| | | | | | <u> </u> | | | |
|--|--|--------------|--------------------|--------------|---|---|-------|---------------------|
| Name and Type (Model and Serial No.) | Contaminant | Efficiency | • : | Conditions : | | Basis for Eff Operationa Test, Design | Data. | |
| acked Crossflow | Fluoride | 99+ | Sa | turated 120 | φ _F | Desi | gn | |
| | | | | | | | | |
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| · | | | | | | | | |
| de any test data and/or design d | | antiation) | • | | • | | | |
| <u> </u> | | Consumpt | rion* | | | Maximus | | |
| Type (Be Specific) | Lave | hr. | Mı | ex.fhr. | • | Heat Inpo | | |
| | | | - | | | , | | |
| | | | | : • | • | | | |
| | | | | <u> </u> | | | | |
| | | • • • | | : | * | | • | |
| | | • . • | | | · | yeer in two | • | • • |
| s: Natural Gas — MCG/hr.; Fuel | Oils, Coal — lbs./hr. | | | <i></i> | 5 . 3v | ç⊷ 1. '∀'; | | |
| Fuel Analysis: | • | İ | | | | | | |
| Fuel Analysis: Percent Surfur: | . | İ | ercent Ash | 1: | * | | | |
| Fuel Analysis: | •••• | Pe | • | | | | | |
| Fuel Analysis: Percent Surfur: Density: | •••• | | • | 1: | | | | |
| Fuel Analysis: Percent Surfur: Density: | | | Jgal. | 1: | | | | |
| Fuel Analysis: Percent Surfur: Density: Heat Capacity: | | | Jgal. | 1: | | | | |
| Fuel Analysis: Percent Surfur: Density: Heat Capacity: | | Pe | Jgal. | 1: | | | | |
| Fuel Analysis: Percent Surfur: Density: Heat Capacity: Other Fuel Contaminants: | generated and method (| Pe tb B' | o./ga1. TU/i5. | | | | | |
| Fuel Analysis: Percent Surfur: Density: Heat Capacity: Other Fuel Contaminants: Indicate liquid or solid wastes (| generated and method (| Pe tb B' | o./ga1. TU/i5. | | | | tem. | |
| Fuel Analysis: Percent Surfur: Density: Heat Capacity: Other Fuel Contaminants: Indicate liquid or solid wastes (| generated and method (| Pe tb B' | o./ga1. TU/i5. | | | | | |
| Fuel Analysis: Percent Surfur: Density: Heat Capacity: Other Fuel Contaminants: Indicate liquid or solid wastes (| generated and method (| Pe tb B' | o./ga1. TU/i5. | | | | tem. | |
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| Fuel Analysis: Percent Surfur: Density: Heat Capacity: Other Fuel Contaminants: Indicate liquid or solid westes of Liquid and solid was | generated and method of astes will be d | of disposal: | Jgs!. TU/ib. | e in-plant | water re | | tem. | |
| Fuel Analysis: Percent Surfur: Density: Heat Capacity: Other Fuel Contaminants: Indicate liquid or solid wastes of Liquid and solid wastes of Liquid an | generated and method of astes will be described by the second of the sec | of disposal: | to the cach start. | e in-plant | water re | cycle sys | tem. | _ BTU/ ₁ |

Please Provide the Following Required Supplements For All Pollution Sources:

- 1. Total process input rate and product weight show derivation. See below.
- 2. Efficiency estimation show derivation. See below.
- 3. An 8%" x 11" flow diagram, which will, without revealing trade secrets, identify the individual operations and/or processes. Indicate where raw materials enter, where solid and liquid waste exit, where gaseous emissions and/or airborne particles are evolved and where finished products are obtained.
- An 8%" x 11" plot plan showing the exact location of manufacturing processes and outlets for airborne emissions. Relate all flows to the flow diagram.
- 5. An BK" x 11" plot plan showing the exact location of the establishment, and points of airborns emissions in relation to the surrounding area, residences and other permanent structures and roadways.
- 5. Description and sketch of storm water control measures taken both during and after construction.
 - See Permit No. IC29-2379

| 1. | Process | Input | Rate: |
|----|---------|-------|-------|
| | | | |

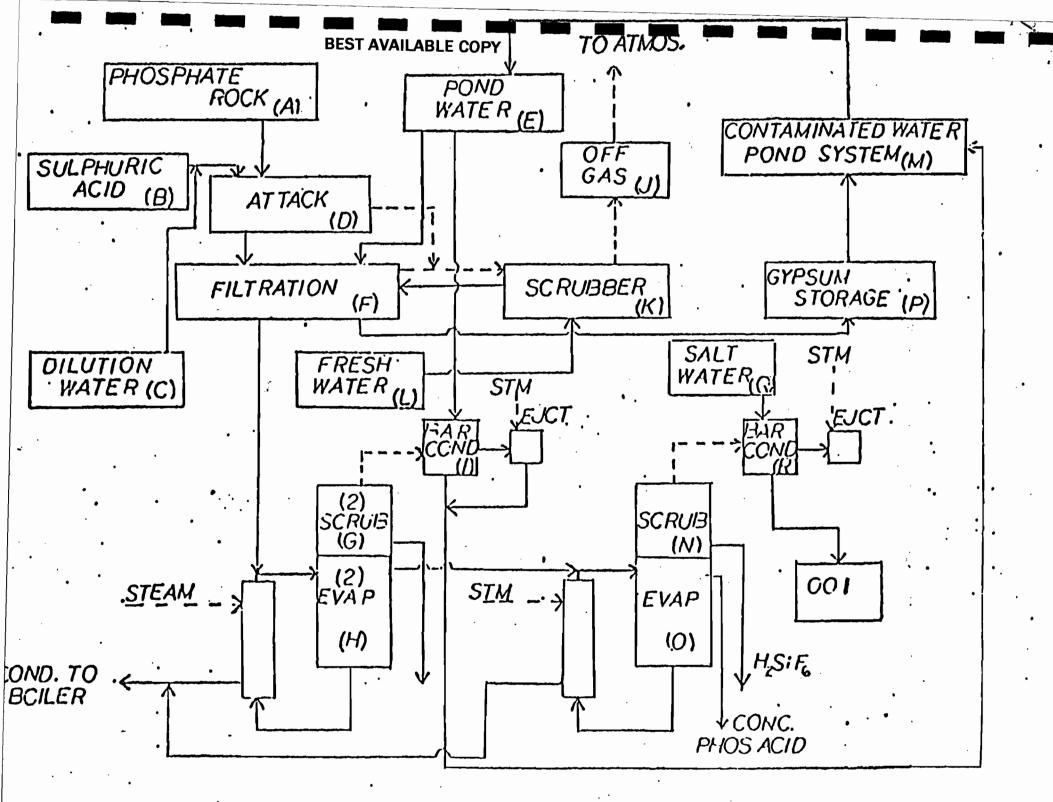
Product Weight

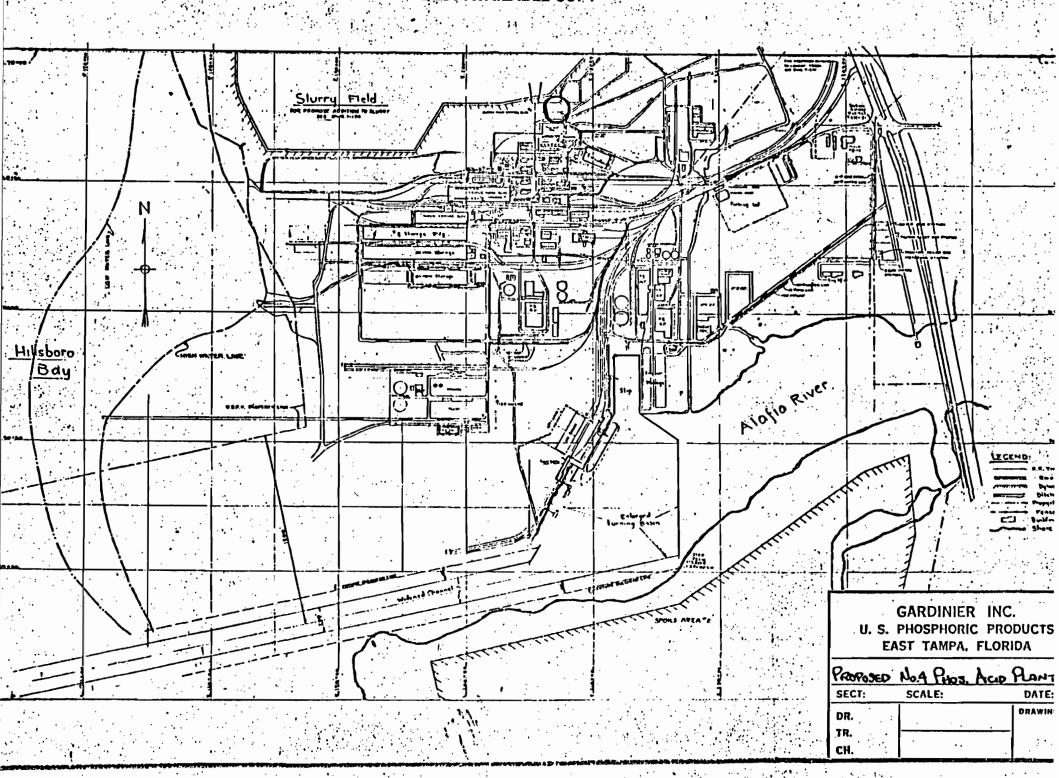
= 110,200 lb/hr P205 recovere

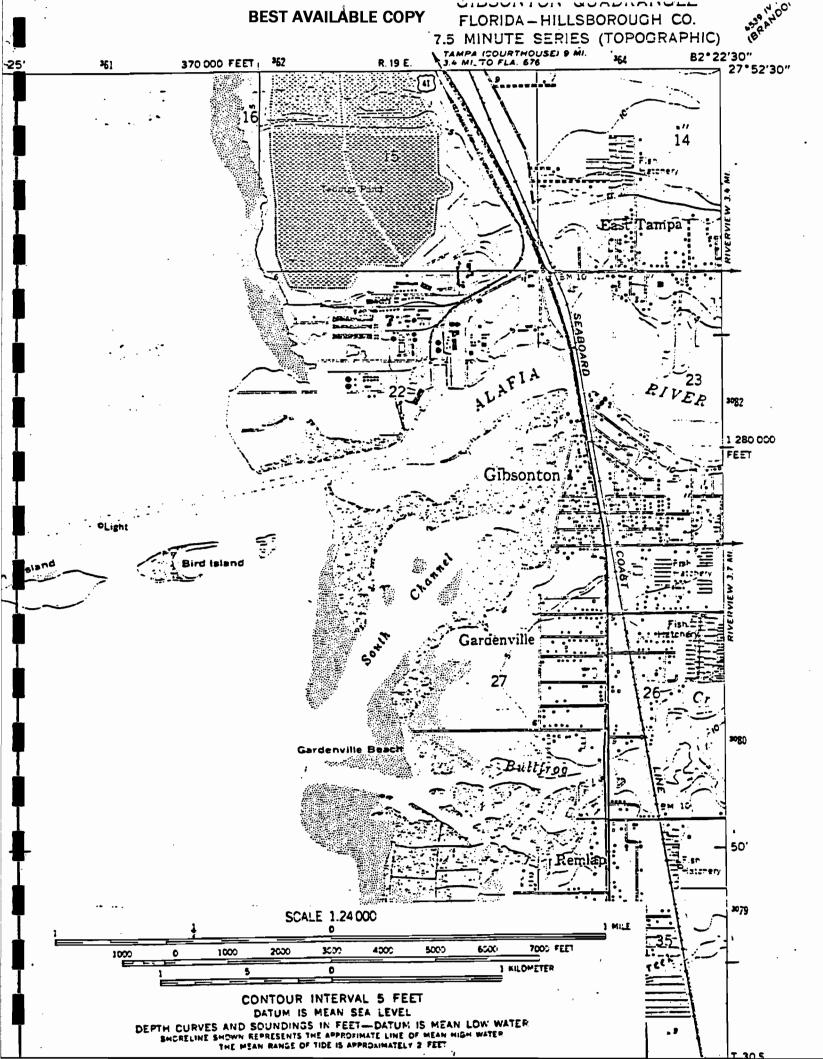
| Phosphate Rock | 400,000 lbs/hr 29% P ₂ 05 | Phosphoric Acid, 29% P205 |
|----------------|--------------------------------------|--|
| Sulfuric Acid | 308,333 lbs/hr | 400,000 x .29 = 116,000 tbs/hr P205 |
| Water | 357,357_lbs/hr | 116,000 ÷ .29 = 400,000 lbs/hr 29%-H3P04 |
| | 1.065.690 lbs/hr | 400,000 x .95 = 380,000 lbs/hr recovered |

2. Efficiency cannot be determined as only scrubber exit loadings are measured.

- *P₂0₅ process input rate has been revised to 120,000 lb/hr.







NO. 7 SULFURIC ACID PLANT



STATE OF FLORIDA DEPARTMENT OF ENVIRONMENTAL REGULATION

APPLICATION TO OPERATE/CONSTRUCT AIR POLLUTION SOURCES

| purce Type: Air Pollution [X] Incinerator [] | |
|---|---|
| ype application: [] Operation [X] Construction | |
| ompany Name: Gardinier, Inc. | Modification : Hillsborough |
| ource Identification: #7 Sulfuric Acid Plant . | County: |
| ource Location: Street: U.S. Highway 41 and Riverview | Drive City: South of Tampa |
| UTM: Eas: 363.2 | Nerth 3082.2 |
| pol. Name and Time: Rudy J. Cabina, Vice President | |
| P.O. Box 3269, Tampa, Florida | 33601 |
| STATEMENTS BY APPLIS | CANT AND ENGINEER |
| APPLICANT | • |
| I am the undersigned owner or authorized representative of Gard | linier, Inc. |
| I certify that the statements made in this application for aCons | struction permit are |
| pollution control facilities in such a manner as to comply with the p | Further, I agree to maintain and oberate the pollution control source and provisions of Chapter 403, Florida Statutes, and all the rules and regula- a permit, if granted by the Department, will be nontransferable and I will nitted establishment. |
| Ву: | Colone Vice President |
| Date: _ | Signature of the pwner or Authorized Representative and Title 6/8/79 Telephone No.: 813-677-9111 |
| *Attach a letter of authorization. If applicant is a corporation, a Certi obtained for a \$5.00 charge from the Secretary of State, Bureau of Co | ficate of Good Standing must be submitted with application. This may be reporate Records, Taliahassee, Florida 32304. |
| PROFESSIONAL ENGINEER REGISTERED IN FLORIDA | • |
| formity with modern engineering principles applicable to the treatrement is reasonable assurance, in my professional judgment, that the discharge an effluent that complies with all applicable statutes of the | rol project have been designed/examined by me and found to be in con- nent and disposal of pollutants characterized in the permit application, pollution control facilities, when properly maintained and operated, will be State of Florida and the rules and regulation of the Department. It is instructions for the proper maintenance and operation of the pollution |
| Signature:CLDaugher | Mailing Address: P.O. Box 3269 |
| C. S. Daugherty | Tampa, Florida 33601 |
| Neme: (Piesse Type) | |
| Company Name: Gardinier, Inc. | Telephone No.: 813-677-9111 |
| Florida Registration Number: 21150 | Date: 6/8/79 |
| AAF- Parth | / / |

DETAILED DESCRIPTION OF SOURCE

| | | ce. Attach additional sheet if necessary. |
|--|---|--|
| | | "add-on" Leonard-Monsanto double absorption, dou |
| | | ease its capacity from 1380 tons 100% sulfuric a |
| | | id per day. The Plant is currently permitted to |
| | | 00 # per day. After modification the plant will |
| ew source stand | ards of 4# SO2 per ton | of H2SO4 or 7,000 # per day. The plant will be |
| | | of Florida and Hillsborough County regulations. |
| etails are atta | ched. | |
| | | |
| | | |
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| | | • |
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| | | • |
| | | · |
| chedule of Project Cover | red in this Application (Construction | on Permit Application Only) |
| | | |
| Stan of Construction: | April 1. 1980 | |
| | | 33 |
| Completion of Constr | uetion: | • • |
| | | |
| iditional Catal | yst - \$50,000 | |
| dditional Catal | yst - \$50,000 | |
| dditional Catal | yst - \$50,000 | |
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| dditional Catal | yst - \$50,000 | |
| | | and notices; including issuance dates and expiration dates. |
| or this source indicate at | ny previous DER permits, orders, a | and notices; including issuance dates and expiration dates. |
| or this source indicate at | ny previous DER permits, orden, a Issued | and notices; including issuance dates and expiration dates. Expires |
| or this source indicate at ermit 029-2180 | ny previous DER permits, orders, a Issued 5/25/73 | Expires 7/1/75 |
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| or this source indicate at ermit 029-2180 C29-2384 | ny previous DER permits, orders, a Issued 5/25/73 | Expires 7/1/75 |
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| ermit 029-2180 C29-2384 | Issued 5/25/73 | Expires 7/1/75 3/1/77 |
| ermit 029-2180 | Issued 5/25/73 | Expires 7/1/75 3/1/77 |
| | Issued 5/25/73 | Expires 7/1/75 3/1/77 |
| ermit 029-2180 | Issued 5/25/73 | Expires 7/1/75 3/1/77 |
| ermit 029-2180 | Issued 5/25/73 | Expires 7/1/75 3/1/77 |
| ermit 029-2180 | Issued 5/25/73 | Expires 7/1/75 3/1/77 |

AIR POLLUTION SOURCES & CONTROL DEVICES .

(other than incinerators)

| Name of Contaminant | | | Criteria Rate* | Disch Ibs | _ | Flow Diagram |
|---|----------------------|---------------------|----------------------------|------------------|---------------|--------------------------|
| | | mai** | Discharge | Allow | | Relate to |
| Airporne Conteminant | s Discharged: | | | | | |
| hrs./day: | 22.8 | days/wk | _ | | s/yr.: 52 | |
| 3) Normal Operating | Time: | 8322 hr | s/yr if sea | sonal describe: | | asonal |
| 2) Product Weight (U) | | 145,833 | | | | |
| Process Rate: 1) Total Process Input | Dava / I taise*). | 146,135 | 5.6 #/hr | • | | |
| | | | | | | <u> </u> |
| ater | 2 | 26795.5 | · : 😑 · | - | · · · · · · · | С |
| tmospheric Oxygen | 1 7 | 1521.2 | - | - | | B |
| ulfur | 4 | 7818.9 | Sulfur | 100 | | A |
| · · · · · · · · · · · · · · · · · · · | | lbs./hr. | Type | % W1. | | " |
| Description | | Utilization Rate | Approxi Consens Cons | inant | F | Relate to low Diagram |
| Raw Materials and Chemic | ials Used (Be Specif | ic): | | | | |
| 9) [X] Other (Speci | y): <u>Opacit</u> | 3' | | | | |
| 7) [] Hydrocarbon | s 8) [] | Volatile Organic | Compounds | | | • |
| 4) [] Fluorides | 5) [X] | Acid Mist | . 61 [] | Odor | | |
| a) [] NO _x as NO ₂ | | NH ₃ | e) [] (a | Other (Identify) | | |
| 3)] Nitrogen Cor | | • | • | •• | | |
| 2) [X] Sutfur Comp a) [X] SO _x at SO ₂ | | Reduced Sulfur | as HoS c) [] | Other (Identify) | | • |
| | | | | | | |
| a) [] Dust | ы [] | Fly Ash | e) [] : | Smoke | a) [] C | other (Identify) |

| Name of Conteminant | Disc | harge | Criteria | Allowable Discharge | Relate to Flow Disprem |
|---------------------|----------|--------|--|------------------------|---------------------------|
| | lbs./hr. | T/yr. | . Rate* | lbs./hr. | Tion Disgrain |
| Sulfur Dioxide | 291.7 | 1213.6 | 4#/Ton H ₂ SO ₄ | 291.7 | D, |
| Sulfur Trioxide | and | 1 | | | |
| Acid Mist | 10.9 | 45.5 | 0.15#/ton H ₂ SO ₄ | 10.9 | D |
| Opacity | 10% | | 10% | 10% | D |
| | | 1 | · | | 1 |

Refer to Chapter 17-2.04(2), Florida Administrative Code.

Discharge Criteria: Plate = Ibs./ton P2O5, Ibs./M BTU/hr., etc.)

*Estimate only if this is an application to construct.

| Name and Type (Model and Serial No.) Contaminant Efficiency of Operations of Operations Design Design Design Design Design Design Trioxide 6 Acid Mist Acid Mist Type (Be Specific) Consumption* Maximum Met Hoor. Avg./hr. Max./hr. Max./hr. Max./hr. Max./hr. Mist Hoor. Full Analysis: Percent Surfur: Percent Surfur: Density: Design Trioxide 6 Acid Mist Consumption* Maximum Met Hoor. MMSTU/hr. Max./hr. Max./hr. Max./hr. Mist Hoor. Density: Density | Control Devices: | | | | |
|--|------------------------------------|-----------------------|--------------------|---|--|
| al Absorber Sulfur 99.99 Dry 180° Design Trioxide 6 Acid Mist Acid Mist Idea and the supplement. Idea and the supplement the supplement. Idea and the supplement the supplement. Idea and the supplement the supplement. Idea and the supplement the supplement. Idea and the supplement the supplement. Idea and the supple | | Contaminant | · Efficiency* | • | Operational Data, |
| Trioxide & Acid Mist Acid Mist Acid Mist Required supplement. Inde any ter: data and/or design data for efficiency substramisation) Fuelt: No fuels are used. Consumption* Avg./hr. Max./hr. Mistrum Hest input Mistrum Hest input Mistrum Hest input Mistrum Mistrum Hest input Mistrum al Converter | Sulfur Dioxi | ie 99.8 | Dry 450° | Design |
| Trioxide & Acid Mist Acid Mist Acid Mist Treating any ter, data and/or design data for efficiency subcramiation) Fusit: No fuels are used. Type (Be Specific) Consumption* Maximum Heat input MMSTU/hr. MMSTU/hr. MMSTU/hr. Fusi Analysis: Percent Surfur: Percent Surfur: Density: Density: Ib/gal. Heat Capacity: Dother Fusi Contaminant: Indicate inquist or solid wastes penerated and method of disposal: Cooling tower and boiler blowdown are discharged from plant Outfall 005. Turbine blocondenser water is discharged from plant Outfall 001. There are no solid wastes generated and method of disposal: Condenser water is discharged from plant Outfall 001. There are no solid wastes generated and state of the state of | | | | - | |
| Acid Mist Acid Mist | al Absorber | Sulfur | 99.99 | Dry 180° | Design |
| required supplement. ude any test data and/or design data for efficiency substantiation) Fuelt: No fuels are used. Type (Be Specific) Avg_/hr. Max_/hr. Max_/hr. Mest input MMSTU/hr. Fuel Analysis: Percent Surfur: Percent Surfur: Percent Surfur: Density: 1b /gai. Hes: Capacity: STU/lb. Condenser water is discharged from plant Outfall 005. Turbine bld condenser water is discharged from plant Outfall 001. There are no solid wastes gend Emission Stack Geometry and Flow Characteristics, (provide data for each stack): Stack Heiph:: 150 7.0 | | Trioxide & | | | |
| Fuels: No fuels are used. Type (Be Specific) Consumption* Max./hr. Max./hr. Max./hr. Mist Input Mist Inp | | Acid Mist | | 1 | 1 |
| Fuels: No fuels are used. Type (Be Specific) Consumption* Avg./hr. Max./hr. Max./hr. Max./hr. MidETU/hr. Es: Natural Gas — MCG/nr.: Fuel Dils, Coal — Ibs./hr. Fuel Analysis: Percent Surfur: Density: Ib./gai. Hes: Capacity: ETU/Ib. Dither Fuel Contaminants: Indicate liquid or solid wastes penerated and method of disposal: Cooling tower and boiler blowdown are discharged from plant Outfall 005. Turbine blocondenser water is discharged from plant Outfall 001. There are no solid wastes generated and Flow Characteristics, (provide data for each stack): Stack Height: 150 †1. Stack Dismeter: 7.0 | <u> </u> | | | | · |
| Type (Be Specific) Avg./hr. Avg./hr. Max./hr. Max./hr. Max./hr. Max./hr. MMBTU/hr. Ex: Natural Gas - MCG/hr.; Fuel Dils, Coal - tbx./hr. Fuel Analysis: Percent Surfur: Percent Ash: Density: Ib./gai. Hest Capacity: BTU/lb. Stack Geometry and boiler blowdown are discharged from plant Outfall 005. Turbine block condenser water is discharged from plant Outfall 001. There are no solid wastes gent Emission Stack Geometry and Flow Characteristics, (provide data for each stack): Stack Height: 150 ft. Stack Diameter: 7.0 | de any test data and/or design dat | • | rantiation} | | |
| Avg_/hr. Max_/hr. MMBTU/hr. TX: Natural Gas = MCG/hr.; Fuel Dils, Coal = lbt_/hr. Fuel Analysis: Percent Surfur: Percent Ash: Density: BTU/lb. Differ Fuel Contaminants: Indicate liquid or solid wastes generated and method of disposal: Cooling tower and boiler blowdown are discharged from plant Outfall 005. Turbine blocondenser water is discharged from plant Outfall 001. There are no solid wastes generated and method of disposal: Cooling tower and boiler blowdown are discharged from plant Outfall 005. Turbine blocondenser water is discharged from plant Outfall 001. There are no solid wastes generated and method of disposal: Cooling tower and boiler blowdown are discharged from plant Outfall 001. There are no solid wastes generated and method of disposal: Cooling tower and boiler blowdown are discharged from plant Outfall 001. There are no solid wastes generated and method of disposal: Cooling tower and boiler blowdown are discharged from plant Outfall 001. There are no solid wastes generated and method of disposal: Cooling tower and boiler blowdown are discharged from plant Outfall 005. Turbine blocondenser water is discharged from plant Outfall 001. There are no solid wastes generated and method of disposal: Cooling tower and boiler blowdown are discharged from plant Outfall 005. Turbine blocondenser water is discharged from plant 001. There are no solid wastes generated and method of disposal. | Toron (D. Constilla) | | Consumption | on* | • |
| Emission Stack Geometry and Flow Characteristics, (provide data for each stack): Stack Height: | Type (Be Specific) | Avg | /hr. | Max.Jhr. | |
| Ex: Natural Gas — MCG/nr.; Fuel Dits, Coal — Ibt./hr. Fuel Analysis: Percent Surfur: Density: Density: BTU/Ib. STU/Ib. Dits Fuel Contaminants: Cooling tower and boiler blowdown are discharged from plant Outfall 005. Turbine blowdown are discharged from plant Outfall 005. Turbine blowdown are discharged from plant Outfall 005. Turbine blowdown are discharged from plant Outfall 005. Turbine blowdown are discharged from plant Outfall 001. There are no solid wastes generated and formal outfall 001. There are no solid wastes generated and formal outfall 001. There are no solid wastes generated and formal outfall 001. There are no solid wastes generated and formal outfall 001. There are no solid wastes generated and formal outfall 001. There are no solid wastes generated and formal outfall 001. There are no solid wastes generated and formal outfall 001. There are no solid wastes generated and formal outfall 001. There are no solid wastes generated and formal outfall 001. There are no solid wastes generated and formal outfall 001. There are no solid wastes generated and formal outfall 001. There are no solid wastes generated and formal outfall 001. There are no solid wastes generated and formal outfall 001. There are no solid wastes generated and formal outfall 001. There are no solid wastes generated and formal outfall 002. There are no solid wastes generated and formal outfall 002. | | | | | |
| EX: Natural Gas — MCG/nr.; Fuel Dils, Coal — Ibs./hr. Fuel Analysis: Percent Surfur: Percent Ash: Density: Ib /gal. Hea: Capacity: BTU/Ib. Other Fuel Conteminants: Cooling tower and boiler blowdown are discharged from plant Outfall 005. Turbine blowdown are discharged from plant Outfall 005. Turbine blowdown are discharged from plant Outfall 005. Turbine blowdown are discharged from plant Outfall 005. Turbine blowdown are discharged from plant Outfall 005. Turbine blowdown are discharged from plant 001. There are no solid wastes generated and matter is discharged from plant 001. There are no solid wastes generated and for each stack): Emission Stack Geometry and Flow Characteristics, (provide data for each stack): Stack Height: 150 ft. Stack Diameter: 7.0 | · | | . | · ! | • |
| Fuel Analysis: Percent Surfur: Percent Ash: Density: Ib Jgal. Hea: Capacity: BTU/Ib. Stack Geometry and Flow Characteristics, (provide data for each stack): Stack Height: 150 1 b Jgal. Percent: Ash: Percent: Ash: Percent: Ash: BTU/Ib. BTU/I | • • | <u> </u> | · . · | | the collection of the collecti |
| Fuel Analysis: Percent Surfur: Percent Ash: Density: Ib Jgal. Hea: Capacity: BTU/Ib. Stack Geometry and Flow Characteristics, (provide data for each stack): Stack Height: 150 1 b Jgal. Percent: Ash: Percent: Ash: Percent: Ash: BTU/Ib. BTU/I | s: Natural Gas — MCG/hr.; Fuel C | Dils, Coal — Ibs./hr. | | | |
| Density: Ib Jgsl. | | | • | | |
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| Indicate liquid or solid wastes generated and method of disposal: Cooling tower and boiler blowdown are discharged from plant Outfall 005. Turbine blocondenser water is discharged from plant Outfall 001. There are no solid wastes generated as the stack of the stac | Hes: Capacity: | - | BTL | J/1b | BTU |
| Cooling tower and boiler blowdown are discharged from plant Outfall 005. Turbine blocondenser water is discharged from plant Outfall 001. There are no solid wastes generally because the condenser water is discharged from plant Outfall 001. There are no solid wastes generally because the condenser water is discharged from plant Outfall 001. There are no solid wastes generally because the condenser water is discharged from plant Outfall 001. There are no solid wastes generally because the condenser water is discharged from plant Outfall 001. There are no solid wastes generally because the condenser water is discharged from plant Outfall 001. There are no solid wastes generally because the condenser water is discharged from plant Outfall 001. There are no solid wastes generally because the condense water is discharged from plant Outfall 001. There are no solid wastes generally because the condense water is discharged from plant Outfall 001. There are no solid wastes generally because the condense water is discharged from plant Outfall 001. There are no solid wastes generally because the condense water is discharged from plant Outfall 001. There are no solid wastes generally because the condense water is discharged from plant Outfall 001. There are no solid wastes generally because the condense water is discharged from plant Outfall 001. There are no solid wastes generally because the condense water is discharged from plant Outfall 001. There are no solid wastes generally because the condense water is discharged from plant Outfall 001. There are no solid wastes generally because the condense water is discharged from plant Outfall 001. There are no solid wastes generally because the condense water is discharged from plant Outfall 001. The condense water is discharged from plant Outfall 001. The condense water is discharged from plant Outfall 001. The condense water is discharged from plant Outfall 001. The condense water is discharged from plant Outfall 001. The condense water is discharged from plant Outfall 001. T | Other Fuel Conteminants: | | | | • |
| Cooling tower and boiler blowdown are discharged from plant Outfall 005. Turbine blocondenser water is discharged from plant Outfall 001. There are no solid wastes generally because the condenser water is discharged from plant Outfall 001. There are no solid wastes generally because the condense of th | Other Fuel Conteminants: | ~ | | | • |
| Emission Stack Geometry and Flow Characteristics, (provide data for each stack): Stack Height: | Cooling tower and bo | iler blowdow | n are disch | | |
| Stack Height: | condenser water is | lischarged fr | om plant Ou | tfall 001. The | ere are no solid wastes gene |
| Stack Height: | · · | | | | |
| Stack Height: | Emission Study Garmany and E | low Change in the | man ido dos dos | P.maskl | |
| | 1.5 | | provide data for (| | |
| | | | | | |

Please Provide the Following Required Supplements For All Pollution Sources:

- 1. Total process input rate and product weight show derivation. See below.
- 2. Efficiency estimation show derivation. See below.
- 3. An 8%" x 11" flow diagram, which will, without revealing trade secrets, identify the individual operations and/or processes. Indicate where raw materials enter, where solid and liquid waste exit, where gaseous emissions and/or airborne particles are evolved and where finished products are obtained.
- 4. An 8%" x 11" plot plan showing the exact location of manufacturing processes and outlets for airborne emissions. Relate all flows to the flow diagram.
- 5. An BK" x 11" plot plan showing the exact location of the establishment, and points of airborne emissions in relation to the surrounding area, residences and other permanent structures and roadways.
- 6. Description and sketch of storm water control measures taken both during and after construction.
- Storm water runoff is captured by plant ditches 001 and 005 (see attached general plant layout diagram).

1. Process Input and Product Rates

Product:

$$H_2SO_4 = 1750 \text{ T/D} = 1750 (2000/24) = 154,833 \#/hr$$

Acid Mist =
$$1750 \times 0.15 = 262.5 \#/D = 262.5/24 = 10.9 \#/hr$$

$$SO_2 = 1750 \times 4 = 7000 \#/D = 7000/24 = 291.7$$
.

Input:

Sulfur =
$$(145,833 + 10.9)(32.06/98.08) + 291.7(32.06/64.06) = 47818.9 \#$$

Water =
$$(145,833 + 10.9)(18.02/98.08) = 26795.5 \#/hr$$

Atmospheric Oxygen =
$$(145,833 + 10.9)(48/98.08) + 291.7(32/64.06) = 71521.1 #/hr$$

2. Efficiency Estimate:

Converter -
$$(2000/(2000 + 4)) \times 100 = 98.80\%$$

Aboseption -
$$(2000/(200 + .15)) \times 100 = 99.99\%$$

Item A

Modifications Necessary to Increase No. 7 Plant Capacity to 1750 STPD

1. Drying Tower

Replace packed spray catcher with a mesh pad. Remaining tower internals are adequate.

2. Sulfur Burner

Change sulfur sprays to handle 60 gpm of sulfur.

3. Sulfur Pumps

Increase capacity to 60 gpm.

4. No. 1 Waste Heat Boiler

New boiler required.

5. Converter

Installation of an additional 21,000 liters of Type 210 catalyst will keep S02 emissions levels below 4.0 lbs/ton of H_2S04 . (Note: This assumes existing catalyst is in as new condition.)

6. Superheaters

No. 2 superheater must be retubed. Allowance was made in the original design to accommodate sufficient additional surface area without rebuilding the converter internals.

7. Economizer

One additional section must be added.

8. Interpass Absorption Tower

Install additional HVM mist eliminators in spaces provided. (Note: It is expected that no additional mist eliminators will be required upstream of the booster blower.) The remainder of the interpass tower and internals is adequate.

9. Booster Blower

Install new booster blower between interpass absorption tower and shell side of No. 1 cold heat exchanger. Blower to handle 69,000 SCFM at approximately 75 inches w.g. and approximately 175°E (Exact conditions will depend on detailed design.)

10. Mesh Pad and Vessel

Install new S.S. mesh pad in new vessel at discharge of booster blower. This is to protect the cold heat exchanger.

Item A, Cont -

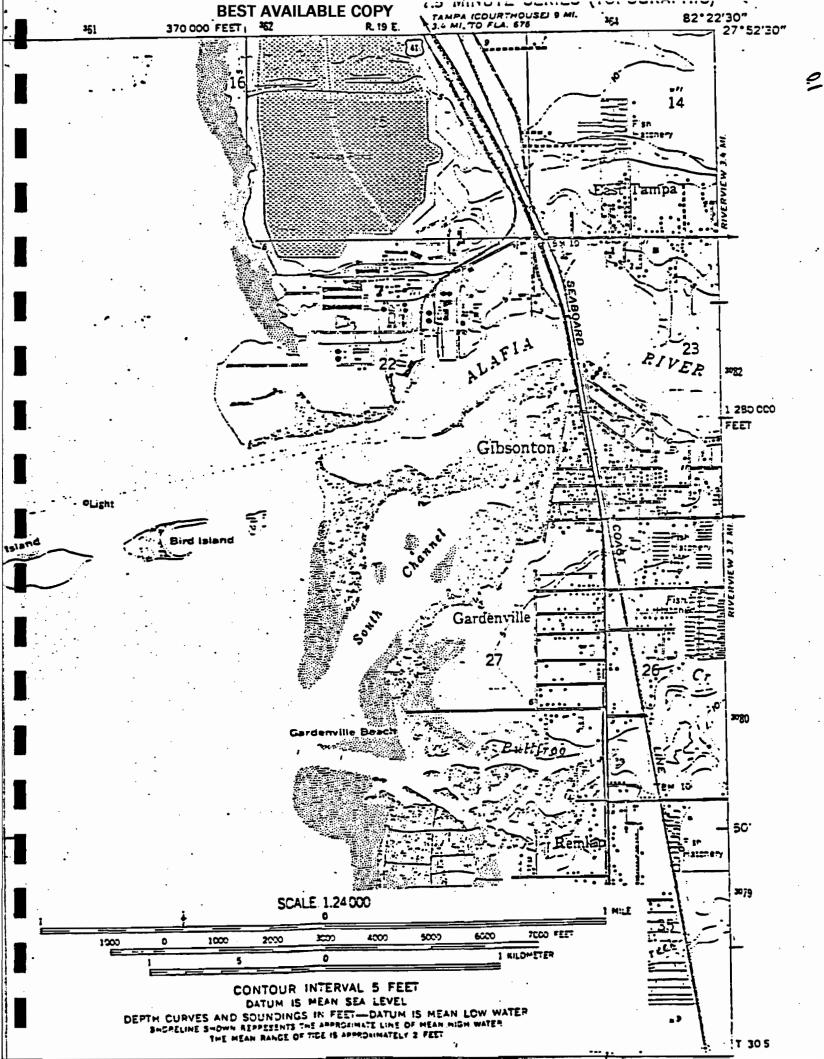
11. Acid Coolers

By rearranging existing radiator coolers as follows, there should be adequate cooler area for the D.T. and IPAT circuits plus product acid:

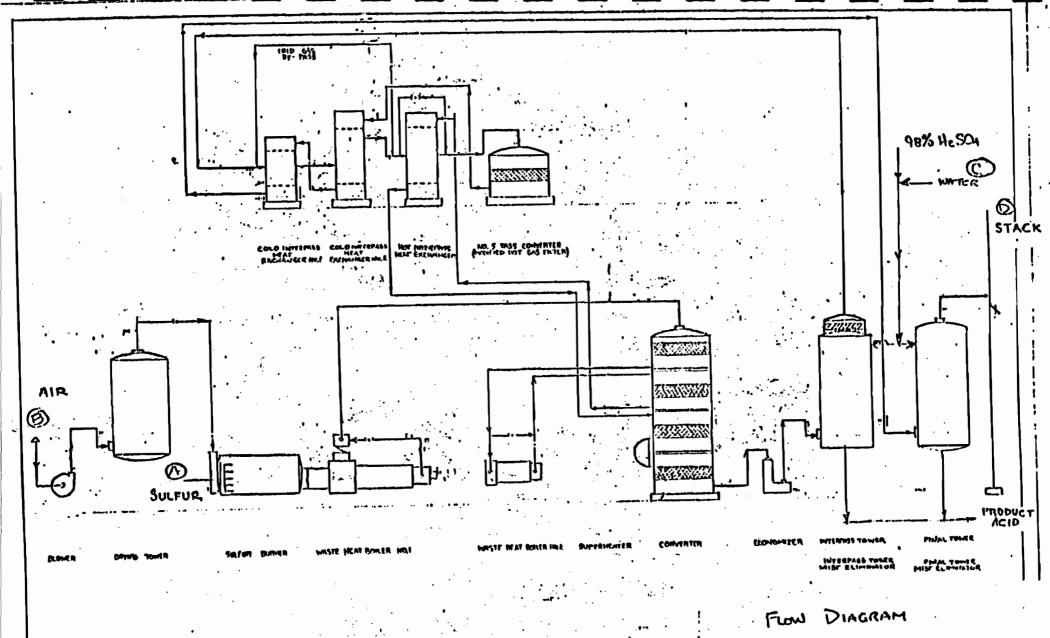
- a. Seven cooler banks for D.T. circuit duty.
- b. Sixteen cooler banks for IPAT circuit duty.
- c. Two cooler banks for product acid duty.

12. Acid Pumps

Increase D.T. acid pump capacity to 3,700 gpm. Increase IPAT acid pump capacity to 5,000 gpm.



BEST AVAILABLE COPY Sturry Field CALL STREET Hysboro Bdy Kiofio River GARDINIER INC. . U. S. PHOSPHORIC PRODUCTS EAST TAMPA, FLORIDA SULFURIC ACID No.7 SCALE: SECT: DATE DRAWIN DR.



No. 7 CONTACT ACID PLANT

NO. 5 AMMONIUM PHOSPHATE PLANT





STATE OF FLORIDA

DEPARTMENT OF ENVIRONMENTAL REGULATION

APPLICATION TO OPERATE/CONSTRUCT AIR POLLUTION SOURCES

| ource Type: | Air Pollution [X] | Incinerator [] | | | | |
|--|---|--|---|--|---|--|
| Type application: | [] Operation | [X] Construction | | | | |
| ource Statut: | [X] New | [] Existing | [] Modification | | | |
| sompany Name: | Gardinier, I | ic. | | County: _ | Hillsborough | |
| Source Identification | No. 5 Ammonia | m Phosphate Plan | ıt | | | |
| ource Location: S | treet: U.S. High | way 41 and River | view Drive | City: | South of Tampa | · B |
| UTM: East _ | | | North | | 3082.5 | |
| ool. Name and Tis | Rudy J. (| Cabina, Vice Pres | sident | - | | |
| Appl. Address: | P.O. Box | 3269, Tampa, Flo | rida 33601 | | | |
| | | STATEMENTS BY | APPLICANT AND EN | GINEER | | |
| L APPLICANT | | | • | | | |
| - I am the unde | rsigned owner or autho | rized representative of | Gardinier, Inc | • | | • |
| l certify that I | the statements made in | this application for a | Construction | | <u> </u> | permit are |
| tions of the D | Department and revision | | nd that a permit, if gra | nted by the Dep | rida Statutes, and all the partment, will be nontransi | ierable and i will |
| | | ٠,٠٠ | Signature of | the Owner or A | authorized Representative | |
| • | | | - L/81- | 79 | Telephone No.: _81 | 3_677_0111 |
| | | applicant is a corporation, Secretary of State, Burea | | - | be submitted with applicati lorida 32304. | ion. This may be |
| . PROFESSION | IAL ENGINEER REGI | STERED IN FLORIDA | | | | |
| formity with There is reaso discharge an e also agreed th | modern engineering pi nable assurance, in my effluent that complies | inciples applicable to the professional judgment, the with all applicable statuted furnish the applicant a | e treatment and disponant the pollution contress of the State of Flor | sal of pollutant rol facilities, which and the rule | /examined by me and fours characterized in the persent properly maintained at example regulation of the Daintenance and operation | mit application. nd operated, will department. It is |
| | a 0 D | 111 | | | | |
| Signature: —_ | Ceca | -greeny | Mailing Addre | | Box 3269 | |
| Name: | C. S. Daughe | | | Tamp | a, Florida 33601 | |
| | (Piezse | і үреі | •= | | | |
| Company Nav | ne: Gardinie | r, Inc. | Telephone No | 813- | 677-9111 | |
| | . 21 | 150 | | 6 | 18/19 | |
| riorida Regist | ration Number:21 | | Dete: | 7 | / / / | |
| | IAAGu Caall | | | , | | |

DETAILED DESCRIPTION OF SOURCE Describe the nature and extent of the project. Refer to existing pollution control facilities, expected improvement in performance of the facilities and state whether the project will result in full compliance. Attach additional sheet if necessary. This is an application to construct an entirely new ammonium phosphate production facility. A "TVA" type plant is proposed and will utilize all latest reasonably available control technology to achieve lowest achievable emission rates. (LAER) Schedule of Project Covered in this Application (Construction Permit Application Only). April 1980 Start of Construction: _ April 1984 Completion of Construction: -Costs of Construction (Show a breakdown of estimated costs for individual components/units of the project serving pollution control purpose only), information on actual costs shall be furnished with the application for operation permit. Venturi -Packed Crossflow - \$1,000,000 + \$400,000 Water Line For this source indicate any previous DER permits, orders, and notices; including issuance dates and expiration dates. None

is this application associated with or part of a Development of Regional Impact (DRI) pursuant to Chapter 380, Florida Statutes, and Chapter

DER Form PERM 12-1 (Apr 76) Page 2 of 6

22F-2, Florida Administrative Code? _____ Yes X No

AIR POLLUTION SOURCES & CONTROL DEVICES

(other than incinerators)

| Fluoride | 1.4 | | | | 1.4 | С |
|--|--|------------------|---|---------------------|------------------|------------------|
| Particulate *** | 10 / | 38 5.32 | lp.16 <u>X17.31 1b</u> 0.061bF/ton P | | 32.4 | С |
| Conteminent | lbs./hr/ | T/yr. | corfert Rate | lt. | s.Jhr. | Flow Diagram |
| Name of | | ual** | Discharge Criteria | | owabie charpe | Relate to |
| D. Airporne Conteminants Disc | therged: Es | timated | 0.24/4 | DKP | | |
| hrs./day: 20 | .8 | Days/wk | <u>: 7</u> | | wks/yr.: | . 52 |
| - 3) Normal Operating Time: | | 7600 hrs | /yr, if se | easonal describe: _ | not seaso | nal |
| 2) Product Weight (Units*) | | 100,000 1 | o/hr | 23TP205 | | |
| C. Process Rate: 1) Total Process Input Rate | (Unitr*): | 100,206 11 | o/hr (dry) | | | CB ^p |
| Sulfuric Acid, 100% | | 3,213 | Farticulate | | | |
| | <u>l</u> | 3,213 | Particulate | 100% | <u> </u> | D |
| Anhydrous Ammonia | - | 22,885 | Ammonia | 100% | | В |
| Dry, plus Solids | | 74,108 | Fluoride | 1.8% | | |
| Phosphoric Acid, 100% | Happi | | | <u> </u> | i . | |
| Description | | Rate Ibu/hr. | Type | ænτ % Wt. | - | Flow Disgrato |
| | | Utilization | Contai | ximate - minant | - | Relate to |
| B. Raw Materials and Chemicals U | sec (Be Specif | ic): | Jo 302 P.O. ? | | | |
| 9)] Dther (Specify):_ | | | | | | |
| 7) [] Hydrocarbons | 8) [] | Volatile Organic | Compounds | | | • |
| 4) [X] Fluorides | 5) [] | Acid Mist | e) [] | Odor | | |
| al [] NO _X as NO ₂ | P) [X] | NH ₃ | c) [] | Other (identify) | | |
| 31 [] Nitropen Compou | | • | - · | · | | |
| 2) [] Sulfur Compound a) [] SO _x at SO ₂ | | Reduced Sulfur a | ns H ₂ S _ e) [] | Other (Identify) | | • |
| a) [] Dust | P) [] | Fly Ash | [] (a | Smoke | d) [] | Other (Identify) |
| 1) [X] Particulates | | | | ı | • | |
| A. Identification of Air Contar | ninants: | • | | | | |
| | | | | | | |

Refer to Chapter 17-2.04(2), Florida Administrative Code.

(Discharge Criteria: Rate = Ibs./ton P205, Ibs./M BTU/hr., etc.)

*Estimate only if this is an application to construct.

2.1

7.98

None

***Revised from figures originally submitted to DER.

No limit

DER FORM PERMISSI (An. 30) Bank 2 of 6

Ammonia

| Name and Type (Model and Serial No.) | Contaminant | Efficiency* | Conditions of Operations | Basis for Efficiency Operational Data, Test, Design, Data |
|--|--|---|---|---|
| avy Powergas | Particulate | 99+ | Saturated 140 F | Design |
| | Fluoride | 99+ | | Design |
| | Ammonia | 99+ | | Design |
| | Soz · | | | |
| | | | | |
| | | | | |
| | | | | |
| | | | | |
| Fuels: Type (Be Specific) | Avg./h | Consumption | Max/hr. | Maximum Heat Input MMBTU/hr. |
| o, 6 Fuel Oil | - | 1275*** | / | 26.3 |
| 501 | 1 . | 1275 | · · | |
| | · · · · · · · · · · · · · · · · · · · | | | |
| • .• . | l | · . · | | Control of the second |
| re: Namural Gas - MCG/hr : Fun | el Dits Coal — the Inc | | .] | . Dogres - Marie - |
| Percent Solidi. | el Diis, Coal — Ibs./hr. | ***] | his figure will be revised permit applient Ash: | supplied to DER in a |
| Fuel Analysis: Percent Surfur: Density: 8 Heat Capacity: | . 5 | *** Perci | his figure will be revised permit appliant Ash: 146,000 | supplied to DER in a cation. BT Tele system. |
| Percent Surfur: 2 Density: 8 Heat Capacity: Other Fuel Conteminants: Indicate liquid or solid wastes | .0 s generated and method of will be consumed | *** Perce Ib Jg BTU of dispose!: if in the pl | his figure will be revised permit applicant Ash: 146,000 ant-wide water recy | supplied to DER in a cation. |
| Percent Surfur: Density: Neat Capacity: Other Fuel Conteminants: Indicate liquid or solid wastes Scrubber effluent to Emission Stack Geometry and Stack Height: | s generated and method of will be consumed of Flow Characteristics, (p. 90 | *** Perciple to Japan BTU of disposal: if in the pl provide data for e ft. | This figure will be revised permit applicant Ash: 146,000 ant-wide water recy | supplied to DER in a cation. BT Tole system. 8.0 |

600 °K

DER Form PERM 12-1 (Apr 76) Page 4 of 6

= 8.2 H/h

Please Provide the Following Required Supplements For All Pollution Sources:

- 1. Total process input rate and product weight show derivation. See below.
 - . Efficiency estimation show derivation. See below.
- 3. An 8%" x 11" flow diagram, which will, without revealing trade secrets, identify the individual operations and/or processes. Indicate where raw materials enter, where solid and liquid waste exit, where gaseous emissions and/or airborne particles are evolved and where finished products are obtained. See Attached.
- 4. An 8%" x 11" plot plan showing the exact location of manufacturing processes and outlets for airborne emissions. Relate all flows to the flow diagram. See Attached.
- 5. An 8%" x 11" plot plan showing the exact location of the establishment, and points of airborne amissions in relation to the surrounding area, residences and other permanent structures and roadways. See attached.
- Description and sketch of storm water control measures taken both during and after construction.See Permit IC29-2379

Phosphoric Acid, 100% + Solids - 74,108 lb/hr = 46,904 lb/hr P₂0₅

1. Process Input Rate and Product Weight

Input

23.5 TPH 1200

Product Weight
(from design information)
100,000 lb/hr @ 1.5% H20

Anhydrous Ammonia

- 22,885 lb/hr

= 98,500 lb/hr dry.

Sulfuric Acid, 100%

- 3.213 lb/hr

= 46,000 lb/hr P205

100,206 lb/hr

 $= 21,857 \text{ lb/hr NH}_3$

(Does not include uncombined water)

(Differences due to scrubber losses)

- Efficiency Estimation
 - Fluroride

Input - 74,108 X .018 = 1334 lb fluoride input per hour

Output - 1.4 1b fluoride per hour in stack gas

 $100 - (1.4 \times 100) = 99.89\%$ Efficiency

