



October 18, 1993

F21.816

Mr. Willard Hanks  
Bureau of Air Regulation  
Florida Department of Environmental Protection  
Twin Towers Office Building  
2600 Blair Stone Road  
Tallahassee, Florida 32399-2400

RECEIVED  
OCT 20 1993  
Division of Air  
Resources Management

**Foamex, L.P.**  
**Application for Permit to Construct**  
**a Flexible Polyurethane Foam Manufacturing Facility**

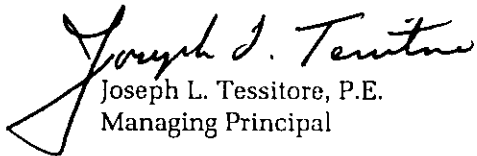
Dear Mr. Hanks:

As you requested, please find enclosed the completed form for waiver of the 90 day time limit for permit application no. AC48-214902, for Foamex, L.P.. This form is provided in addition to the letter request for extension submitted on September 22, 1993.

Please do not hesitate to contact me should you have any questions or comments concerning this matter.

Yours very truly,

HLA-C/TA

  
Joseph L. Tessitore, P.E.  
Managing Principal

JLT/PKR  
c21001.doc

cc: Mr. Dennis Nester, Orange County Environmental Protection Division (OCEPD)  
Mr. Charles Collins, P.E., FDER - Central Florida District  
Mr. Charles Eavenson, Foamex L.P.  
Mr. Art Pereira, Foamex, L.P.

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OCT 13 1993

CROSS/TESSITORE

WAIVER OF 90 DAY TIME LIMIT  
UNDER SECTIONS 120.60(2) and 403.0876, FLORIDA STATUTES

License (Permit, Certification) Application No. AC48-214902

Applicant's Name: Foamex, L. P.

With regard to the above referenced application, the applicant hereby with full knowledge and understanding of applicant's rights under Sections 120.60(2) and 403.0876, Florida Statutes, waives the right to have the application approved or denied by the State of Florida Department of Environmental Regulation within the 90 day time period prescribed by law. Said waiver is made freely and voluntarily by the applicant, with full knowledge, and without any pressure or coercion by anyone employed by the State of Florida Department of Environmental Regulation.

This waiver shall expire on the 21 day of December 1993.

The undersigned is authorized to make this waiver on behalf of the applicant.

*Charles W. Eavenson*

Signature

*Charles W. Eavenson*

Name (Please Type or Print)

# Florida Department of Environmental Protection



Lawton Chiles  
Governor

Twin Towers Office Building  
2600 Blair Stone Road  
Tallahassee, Florida 32399-2400

Virginia B. Wetherell  
Secretary

October 6, 1993

CERTIFIED MAIL - RETURN RECEIPT REQUESTED

Mr. Joseph L. Tessitore  
Cross/Tessitore & Associates  
4763 South Conway Road  
Orlando, Florida 32812

Re: Foamex, L.P.

Dear Mr. Tessitore:

The Department acknowledges receipt of your September 22, 1993, letter, granting another waiver of the 90 day time limit to process the application for permit to construct Foamex, L.P.'s flexible polyurethane foam manufacturing facility in Orlando, Orange County, Florida. We request you complete the Department's official form for this and future waivers. A copy of the form was faxed to your office on September 30, 1993.

We also confirm that the additional information requested in our June 9, 1993, meeting in Tallahassee on the application for Foamex, L.P., is needed before we can recommend a permit be issued for this plant. Basically, the needed information is the plan, schedule, and emissions proposed to bring this plant into compliance with the Department's regulation.

If you have any questions on this matter, please write to me or call Willard Hanks at (904) 488-1344.

Sincerely,

A handwritten signature in cursive script, appearing to read "John C. Brown, Jr.".

John C. Brown, Jr., P.E.  
Administrator  
Air Permitting and Standards

JB/WH/bjb

cc: Charles Collins, CFD  
Dennis Nester, OCEPD  
Charles Eavenson, Foamex, L.P.

Is your RETURN ADDRESS completed on the reverse side?

**SENDER:**

- Complete items 1 and/or 2 for additional services.
- Complete items 3, and 4a & b.
- Print your name and address on the reverse of this form so that we can return this card to you.
- Attach this form to the front of the mailpiece, or on the back if space does not permit.
- Write "Return Receipt Requested" on the mailpiece below the article number.
- The Return Receipt will show to whom the article was delivered and the date delivered.

I also wish to receive the following services (for an extra fee):

- 1.  Addressee's Address
  - 2.  Restricted Delivery
- Consult postmaster for fee.

3. Article Addressed to:  
 Mr. Joseph L. Tessitore  
 Cross/Tessitore & Associates  
 4763 South Conway Road  
 Orlando, Florida 32812

4a. Article Number  
 P 230 524 310

- 4b. Service Type
- Registered  Insured
  - Certified  COD
  - Express Mail  Return Receipt for Merchandise

7. Date of Delivery

5. Signature (Addressee)  
*Joseph L. Tessitore*

6. Signature (Agent)  
*[Signature]* 10/8/92

8. Addressee's Address (Only if requested and fee is paid)

Thank you for using Return Receipt Service.

PS Form 3810, December 1991 U.S. GPO: 1992-323-402

**DOMESTIC RETURN RECEIPT**

P 230 524 310



**Receipt for Certified Mail**

No Insurance Coverage Provided  
 Do not use for International Mail  
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Sent to Mr. Joseph L. Tessitore	
Street and No. 4763 South Conway Road	
P.O., State and ZIP Code Orlando, Florida 32812	
Postage	\$
Certified Fee	
Special Delivery Fee	
Restricted Delivery Fee	
Return Receipt Showing to Whom & Date Delivered	
Return Receipt Showing to Whom, Date, and Addressee's Address	
TOTAL Postage & Fees	\$
Postmark or Date Mailed: 10/5/93 Foamex, L.P. AC48-214902	

PS Form 3800, June 1991



September 22, 1993

F21.816

Mr. Willard Hanks  
Bureau of Air Regulation  
Florida Department of Environmental Protection  
Twin Towers Office Building  
2600 Blair Stone Road  
Tallahassee, Florida 32399-2400

Foamex, L.P.  
Application for Permit to Construct  
a Flexible Polyurethane Foam Manufacturing Facility

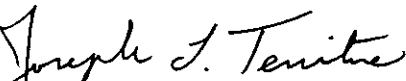
Dear Mr. Hanks:

As you are aware, HLA-C/TA is developing technical information to be submitted as an addendum to the existing Foamex, L.P. Application for Permit to Construct a Flexible Polyurethane Foam Manufacturing Facility currently under FDEP review. This information is being prepared to address the issues discussed during our meeting on June 9, 1993. It is estimated that the submittal document will be finalized in late October, however the current review schedule requires FDEP to act on the application by October 6, 1993. Considering the time that will be required for completion of the submittal document, an extension of 90 days is requested.

Please do not hesitate to contact me should you have any questions or comments concerning this matter.

Yours very truly,

HLA-C/TA

  
Joseph L. Tessitore, P.E.  
Managing Principal

JLT/PKR  
c21001.doc

cc: Mr. Dennis Nester, Orange County Environmental Protection Division (OCEPD)  
Mr. Charles Collins, P.E., FDER - Central Florida District  
Mr. Charles Eavenson, Foamex L.P.  
Mr. Art Pereira, Foamex, L.P

RECEIVED  
OCT 1 1993  
Division of Air  
Resources Management

Memorandum

Florida Department of  
Environmental Protection

TO: Patrick Wong, Dade County DERM  
FROM: Tom Tittle, FDEP/SED *TT*  
DATE: August 3, 1993  
SUBJECT: Urethane Foam Manufacturing Facilities

RECEIVED

AUG 08 1993

Division of Air  
Resources Management

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As a result of Tallahassee's visit to our respective offices, Willard Hanks asked us to look into emissions from Omni Foam Inc, Flexible Foam and Flori Foam which have been identified as Dade County facilities operating without Department air permits. Please send us what information you have about these facilities to assist us in determining whether or not these facilities need Department air permits.

cc: Willard Hanks, DARM, Tallahassee



CROSS/TESSITORE & ASSOCIATES, P.A.

4763 SOUTH CONWAY ROAD  
ORLANDO, FLORIDA 32812  
407/851-1484

July 6, 1993

RECEIVED

JUL 12 1993

Division of Air  
Resources Management

Mr. Willard Hanks  
Bureau of Air Regulation  
Florida Department of Environmental Regulation  
Twin Towers Office Building  
2600 Blair Stone Road  
Tallahassee, Florida 32399-2400

Subject: Foamex, L.P.  
(C/TA # F21.816)


Dear Mr. Hanks:

I would like to thank you for providing me with the opportunity to meet with you on Wednesday, June 9 along with Mr. Art Pereira, Mr. Charles Eavenson and Mr. Joseph Lunderville of Foamex, L.P.

Through our discussion during this meeting, it was clear that the Bureau of Air Regulation (BAR) feels that additional information should be submitted in support of the construction permit application currently under review for the Foamex Facility in Orlando. C/TA and Foamex have already begun to compile and develop the information requested, however, the completion of a document for submittal will require several more weeks. Considering the additional time required for BAR review of such a submittal document, an extension of the permit review schedule seems necessary. As the current schedule require FDER to act on the application by July 12, C/TA requests an extension of 90 days to provide sufficient time for submittal and review of the information requested by FDER.

Please do not hesitate to contact me should you have any questions or comments concerning this matter.

Sincerely,

  
Joseph L. Tessitore, P.E.  
Vice President

JLT/kp

cc: Mr. Dennis Nester, OCEPD  
Mr. Charles Collins, P.E., FDER - Central Florida District  
Mr. Charles Eavenson, Foamex, L.P.  
Mr. Art Pereira, Foamex, L.P.

C5993.Doc

Florida Department of Environmental Protection

Meeting Sign-In Sheet

Re: Florida Gas Transmission

Date: 5/26/93

Name	Representing	Telephone
Barry Andrews	Florida Gas Trans. (ENSK)	(205) 740-8263
<del>W. Duane Pierce</del>	<del>.....</del>	<del>713 853-3568</del>
Arthur R. Tuttle	FOAMEX L.P.	401-438-0900
JOSEPH H. LUNDERVILLE	FOAMEX L.P.	401-438-0900
Charles Eavenson	FOAMEX Orlando	407-857-2510
Iol Tessitore	C/TA	407-851-1484
PASTOR LEWIS	FDER - AIR PERMITTING	(904) 488-1344
SYED ARIF	FDER - AIR PERMITTING	(904) 488-1344
WILLARD HANISS	" "	"

FOAMEX  
6/9/93





CROSS/TESSITORE & ASSOCIATES, P.A.

4763 SOUTH CONWAY ROAD  
ORLANDO, FLORIDA 32812  
407/851-1484

June 2, 1993

Mr. C. H. Fancy, P.E.  
Chief  
Bureau of Air Regulation  
Florida Department of Environmental Regulation  
Twin Towers Office Building  
2600 Blair Stone Road  
Tallahassee, Florida 32399-2400

Subject: Foamex, L.P.  
(C/TA #F21.816)

Dear Mr. Fancy:

This letter is to confirm a meeting scheduled with your staff on Wednesday, June 9, at 1:30 p.m. to discuss the Construction Permit application currently under review for the Foamex, L.P. facility located in Orlando. This meeting was scheduled during a phone conversation with Mr. Willard Hanks of your staff on Thursday, May 30, and will be attended by Mr. Joe Tessitore of C/TA, Mr. Art Pereira of Foamex, and Mr. Charles Eavenson of Foamex.

Please do not hesitate to contact me should you have any questions concerning this matter.

Sincerely,

A handwritten signature in cursive script that reads "Patricia Kay Rykowski".

Patricia Kay Rykowski  
Project Engineer

cc: Mr. Art Pereira, Foamex, L.P.  
Mr. Charles Eavenson, Foamex, L.P.

foamex3.doc  
PKR/tbm



CROSS/TESSITORE & ASSOCIATES, P.A.

4763 SOUTH CONWAY ROAD  
ORLANDO, FLORIDA 32812  
407/851-1484

April 12, 1993 RECEIVED

APR 14 1993

Bureau of  
Air Regulation

Mr. John C. Brown, Jr., P.E.  
Administrator, Air Permitting and Standards  
Florida Department of Environmental Regulation  
2600 Blair Stone Road  
Tallahassee, Fl 32399-2400

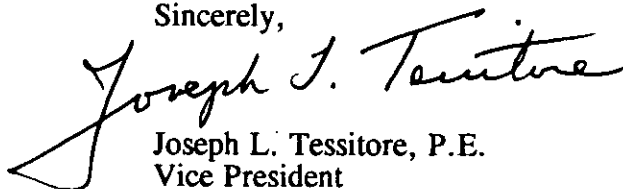
Subject: Application for Permits to Construct a Flexible Polyurethane Foam  
Manufacturing Facility (Ref: Letter, J.C. Brown to C. Eavenson,  
12/22/92)  
(C/TA #F21.816)

Dear Mr. Brown:

Please find enclosed three (3) bound copies of the response developed to address the comments included in your letter of December 22, 1992 regarding the Foamex, L.P. facility in Orlando. This document contains a letter which provides an itemized response to your comments, as well as supporting information and analysis.

Please do not hesitate to contact me should you have any questions or comments concerning this information.

Sincerely,

  
Joseph L. Tessitore, P.E.  
Vice President

cc:

Mr. Dennis Nester, OCEPD  
Mr. Charles Collins, P.E., FDER -Central Florida District  
Mr. Art Pereira, Foamex, L.P.  
Mr. Charles Eavenson, Foamex, L.P.  
Mr. Clifford A. Schulman, Greenberg and Traurig

F21.816/foamex1.doc

REGISTERED PROFESSIONAL ENGINEERS

Federal ID # 59-1638534

Copy given to  
W H and CH  
4/14/93

**RESPONSE TO FDER REVIEW COMMENTS**

**FOAMEX, L.P.  
Application for Permit to Construct  
a Flexible Polyurethane Foam  
Manufacturing Facility**

**April 7, 1993**

*Prepared for:*

**Foamex, L.P.  
1351 Gemini Boulevard  
Orlando, Florida 32821**

*Prepared by:*

**Cross/Tessitore & Associates, P.A.  
4763 South Conway Road, Suite F.  
Orlando, Florida 32812  
(407) 851-1484 FAX: (407) 855-0369  
C5951.Doc / F21.816**

April 7, 1993

**CERTIFIED MAIL - RETURN RECEIPT REQUESTED:**

Mr. John C. Brown, Jr., P.E.  
Administrator, Air Permitting and Standards  
Florida Department of Environmental Regulation  
2600 Blair Stone Road  
Tallahassee, Florida 32399-2400

Dear Mr. Brown:

Re: Application for Permits to Construct a Flexible Polyurethane Foam Manufacturing Facility (Ref: Letter, J. C. Brown to C. Eavenson, 12/22/92)

The following paragraphs provide an itemized response to the December 22, 1992 letter from Mr. Brown regarding the preliminary review conducted by FDER of the December 2, 1992 application submittal.

1. Where is the toluene diisocyanate incinerator located? If in Florida, does it have a Department air permit? If Foamex is the operator of this incinerator in Florida, please provide either the permit number or an application for permit for it.

Response:

ThermalKEM, an American NuKEM subsidiary located in Rock Hill, South Carolina operates a Part B permitted incineration plant (Permit Number: SCD 044 442 333). Other permitted hazardous waste incinerators may also be used in the future, depending on waste disposal requirements.

2. What are the 8-hour, 24-hour, and annual ambient air impacts of toluene diisocyanate emissions from the polyurethane foam facility?

Response:

Table I shows the results of the ISCST2 Modeling for the Foamex toluene diisocyanate (TDI) emissions. This table shows that the maximum off property TDI ground level concentrations are less than the FDER "No Threat Levels" for 8-hour, 24-hour, and annual averaging times. The details of the modeling results are presented in Attachment 1.

3. On Page 1-30 (VI. Foam Fabrication Operation) please clarify the 43.7 foot stack diameter listed in Section H.

Response:

The stack diameter on this page was inadvertently listed as 43.7 feet rather than 43.7 inches, or 3.64 feet.

4. Please provide a more detailed schedule on the company's investigation to use either another process or add air pollution control at this facility. We want to know what the ongoing studies are, what is expected to be learned from the study, and by what date.

Response:

In general, Foamex is working with other members of the industry through the Polyurethane Foam Association (PFA) to evaluate emission control technologies. Development work on various mechanical and chemical solutions for the industry is underway at several companies.

The PFA is formally evaluating emission control strategies and will present an update on the work at the annual PFA meeting in May, 1993. In addition, chemical suppliers are also developing alternative polyol technologies and additives to minimize the amount of auxiliary blowing agent necessary for foam production.

Specifically, Foamex is evaluating various options for emission control on a company-wide basis. These options are as follows:

- 1) Limitation of product mixture produced with blowing agents.
- 2) Capture and treatment of emissions.
- 3) Process and equipment modifications to reduce emissions.

The first option, to limit the product mixture produced, is based on the fact that not all foam grades require the use of auxiliary blowing agents. However, this is not a desired option for all facilities, since it would reduce the sales volume and thus mandate reductions in the plant work force. At a facility such as the Foamex Orlando Plant, which produces a significant amount of blown foam, the loss of this sales volume and subsequent market loss could have a serious impact.

The second option is to consider the capture and treatment of blowing agent emissions. The most promising approach being considered by the PFA, based on industry data and experience, is carbon adsorption. One PFA member has done pilot plant work on a carbon adsorption system, as discussed in question #7. Foamex will continue to follow this work and the development of other industry pilot systems and evaluate their application to emission control at the Orlando Facility. Foamex will also consider other applicable control options should they become available in the next 18 months.

The third option involves the use of several types of process equipment which are currently under development and which have the goal of producing a wide range of flexible urethane foams with little or no emissions of auxiliary blowing agents. These processes are described as follows:

- a) The Rapid Cooling process involves the rapid cooling of a block of foam with the potential of recovering any volatile blowing agent.
- b) The Environmental Cure process involves the elimination of blowing agents and produces water blown foam.
- c) The Variable Pressure Foaming (VPF) process which allows the production of a wide range of flexible urethane foams without the use of blowing agents.

The processes described under a) and b) above, are best suited to plants in which the foam may be manufactured in short blocks to meet customer specifications, which are unlike the typical Foamex plants at this stage. Currently, Foamex is committed to the VPF system which is a new technology and is based on the fact that as the air pressure is reduced within the mold, a given amount of foam will occupy a greater space under normal air pressure. This approach results in the production of greater foam volume with no blowing agent, and allows the density of the foam to be varied based on the changes in the process pressure.

While this technology has been employed in Europe for batch production, it has not been practically demonstrated on a continuous foam line. Foamex has scheduled the installation of this type of process in one of their plants during the latter part of 1993. Several months after installation and startup, Foamex hopes to optimize the foam production variables and begin elimination of the auxiliary blowing agents.

Based on the above discussion of emission control and process modification options, and the fact that OSHA may seriously restrict the use of methylene chloride, and/or EPA may restrict the use of alternate blowing agents such as 1,1,1-Trichloroethane,, and HCFC-141b, Foamex estimates that a final decision concerning emission control measures for the Orlando plant can be made by December, 1994.

In order to keep FDER informed as to the status of the previously discussed emission control and process modification options, a reporting schedule is being proposed as shown in Attachment 2. This schedule, which assumes that a FDER Permit is issued during June 1993, shows that Foamex will submit semi-annual progress reports until December 1994 at which time a decision will be made. Details of the information to be submitted in the semi-annual progress reports are presented in Attachment 3. According to this schedule, Foamex will submit a permit application in March of 1995 identifying the selected emission control configuration and/or process modification which is consistent with the existing OSHA and EPA regulations. This system or equipment will then be installed on a schedule consistent with FDER's approval.

5. Why does the boiler operate longer than the slabstock polyurethane foam production facility? Is it on "stand-by" or do other operations at the facility use steam?

Response:

Currently, the boiler operates only to support the rebond polyurethane foam production facility. The intent of requesting longer boiler operating hours was to insure boiler availability for other plant operations such as environmental heating and/or steam production.

6. What means are used to contain spills and minimize fugitive emissions during process chemical storage and handling?

Response:

All bulk storage tanks currently in use are provided with secondary containment, which can contain at least 115% of the volume in the largest tank. Spill pigs and other absorbent materials are available to contain chemical spills within the building. The chemical suppliers provide training videotapes and standard procedures for bulk materials handling, which acts to minimize spills.

The piping system for toluene diisocyanate includes welded piping, where possible, to prevent spills and minimize fugitive emissions. All drums containing chemicals are tightly closed when not in use.

7. Can any of the blowing agents captured by a carbon adsorption system be recycled at the facility? If so, what is the value of the agent recovered? How does this affect the economics of the BACT determination?

Response:

It may be possible to recycle captured methylene chloride or other auxiliary blowing agents for reuse in the process. A Foamex competitor has worked on a pilot plant scale carbon adsorption unit. They reported that more work had to be done to determine whether the lack of stabilizer in recycled methylene chloride would cause acid buildup in storage or damage foam quality.

In general, as discussed in Item 4, Foamex will continue to pursue the development of collection and treatment options and the semi-annual report will provide an updated status of the viability of carbon adsorption based on PFA studies and data. Currently, it does not appear from the industry pilot plant data that the carbon adsorption process is applicable with the existing blowing agents. However, future changes in blowing agents may cause this situation to be reevaluated.

8. Please describe the equipment cleaning practices at this facility. How much and what types of solvents are used? What is done to minimize emissions of these solvents? How are the used solvents disposed of?

Response:

Typical equipment cleaning practices are described in the following paragraphs. Foamex is continuously working to refine these procedures. The goal is to use effective cleaning methods while minimizing emissions and waste generation.

Polyol is currently used for cleaning the mixhead on the foam machine during production runs. This material is collected and used as a raw material in the rebond foam production process. Approximately 30 gallons per month are used. Due to the low volatility of polyol, no special measures are necessary to minimize emissions.

Small quantities of isopropyl alcohol are used for soaking production equipment pieces. It is estimated that one to two gallons per month are used; the alcohol is replenished as needed. The material is kept in a small covered container. Isopropyl alcohol is also used as a hand cleaner. It is estimated that 387 gallons of isopropyl alcohol were utilized in 1992. N-propyl alcohol is also used as a solvent in an ink used at the plant, and in the cleaner.

Methylene chloride is used to clean the foam line trough after completion of production activities. Approximately three gallons of material will remain after cleaning. This material is transferred to a small covered container where it is kept for reuse. This material may also be used for the soaking of small equipment pieces. The amount of methylene chloride emitted due to cleaning activities, is a small fraction of the amount used in foam production.

The methylene chloride is generally replenished as necessary and reused until it evaporates, but if it does not meet the requirements for use as a cleaner (i.e., if the solids content is too great) it is declared as a hazardous waste and transferred to a hazardous waste satellite drum. The waste is then disposed of in accordance with RCRA requirements, typically by recycling.

A mixture of 1,1,1-trichloroethane and silicone is used as a saw blade lubricant. Approximately 5,770 pounds of 1,1,1-trichloroethane were utilized in 1992. A substitute for this material will be found in a timely manner, because the material will soon become unavailable since it has been classified as a Class 1 ozone depleting compound. The status of identifying a substitute material will be discussed and updated in the semi-annual reports, as discussed in Item 4. However, current Foamex plans are to adopt an alternate procedure and the use of this chemical will be eliminated within three (3) months.

The maintenance and loop slitter department also uses reclaimed mineral spirits supplied by Safety Kleen (105 Solvent MS) for equipment cleaning. Records for 1992 indicate that 292.5 pounds of spent material were returned to Safety Kleen for recycling and 97.5 pounds were emitted. The Safety Kleen "solvent use" workstation is designed to maximize capture of volatile material and minimize emissions.

9. Under the Clean Air Act Amendment of 1990, use of HCFC for non-insulating foams is prohibited after January 1, 1994 (page 6-A-45 of the Application). Any permit issued will reflect that limitation. What will be used after this date?

Response:

Several options are being considered for the replacement of HCFCs. Testing is underway to optimize the use of additives and alternative polyols to replace a portion of the auxiliary blowing agent.

The replacement of banned HCFCs will be considered in the semi-annual reports in context with the entire emissions control options. As discussed in Item 4, Foamex will continue to pursue the best combination of chemical substitution, emission and capture and control, and process or equipment modification which will result in the lowest ground level concentration which is consistent with OSHA and FDER/EPA regulatory requirements and the Orlando plant production economics.



Please contact Joseph Tessitore of C/TA, if you have any questions or comments concerning this information.

Sincerely,

*Charles W. Eavenson*

Charles W. Eavenson  
Plant Manager

LJS 92-257

cc: Clifford Schulman, Greenberg Traurig  
Joseph L. Tessitore, P.E., Cross/Tessitore & Assoc.  
Arthur R. Pereira, Foamex L.P.  
Linda J. Spellmon, Foamex L.P.

**ATTACHMENT 1**  
**FOAMEX L.P.**  
**ISCST2 Modeling Results**  
**(Orlando Flexible Polyurethane Foam Manufacturing Facility)**

## **Foamex ISCST2 Modeling of Toluene Diisocyanate (TDI) Emissions**

The 8-hour, 24-hour, and annual ambient air impacts of the toluene diisocyanate (TDI) emissions from the Foamex facility were estimated using the EPA Industrial Source Complex - Short Term (version 92062) model (ISCST2). This analysis was based on the same methodology and assumptions used in Section 7.0 of the original permit application. The only sources of TDI emissions from the facility are the foam line stack and the two (2) rebond process exhaust fans. The input parameters used this analysis are presented in Table 1. The locations of the foam line stack and rebond process exhausts are shown in Figure 1. A downwash analysis of the three sources was conducted as outlined in Table 7-4 of the permit application and the output listing of this analysis is presented in Attachment A. Table 1 also presents the results of the TDI modeling analysis and a comparison with the FDER No Threat Levels for TDI. The ISCST2 output listings are presented in Attachment B. The results show that in all cases the predicted maximum ambient air impact of TDI emissions from the Foamex facility are below the FDER No Threat Levels for TDI.

**TABLE 1**  
**Foamex ISCST2 Modeling**  
**of Toluene Diisocyanate (TDI) Emissions**

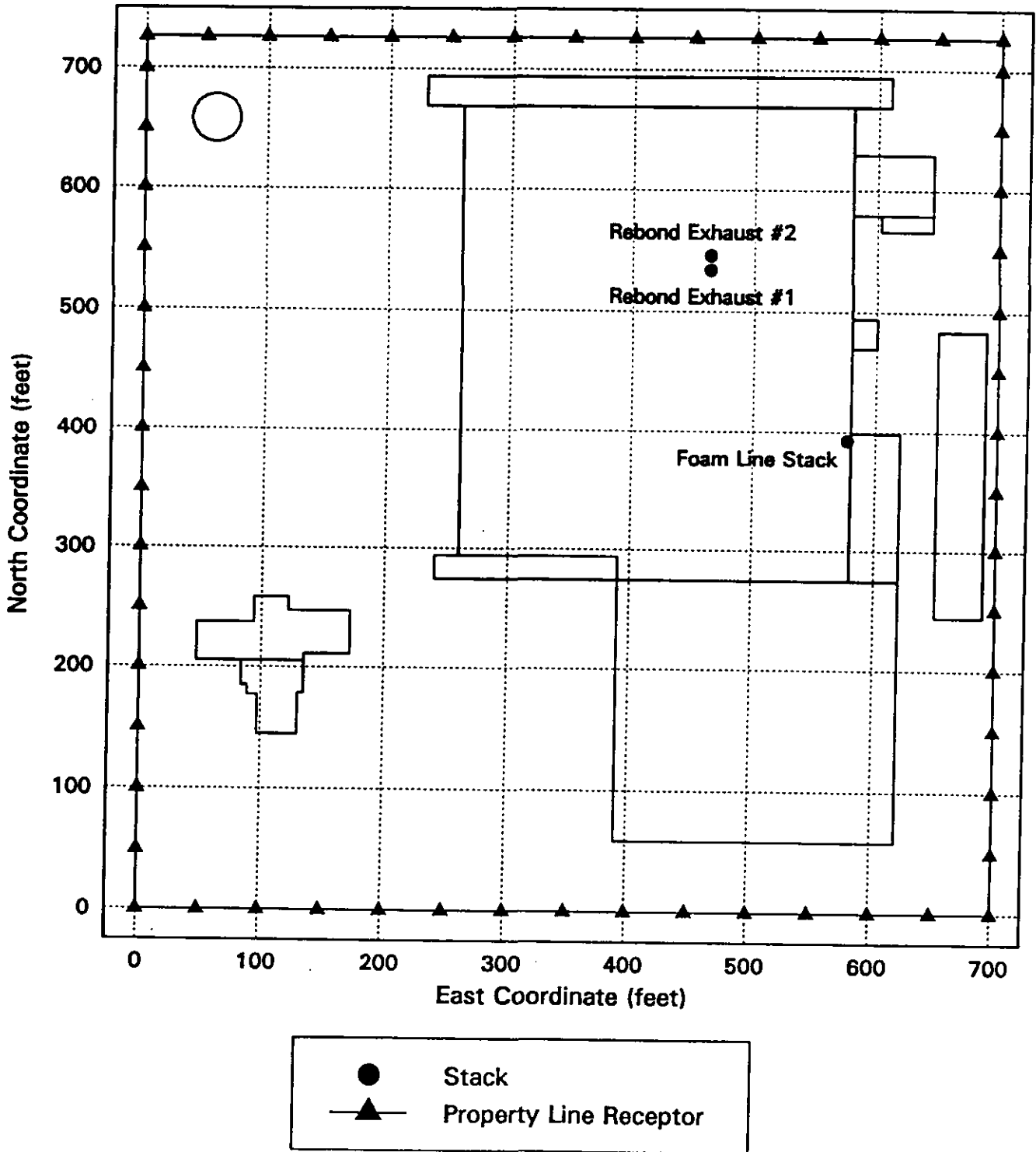
**Source Input Parameters**

Parameter	Units	Foam Line Stack	Rebond Exhaust #1	Rebond Exhaust #2
Stack Height	feet	125	41	41
Stack Inside Diameter	feet	2.303294	2.5	2.5
Stack Gas Flow Rate	ACFM	20000	1000	1000
Stack Gas Exit Velocity	ft/sec	80	3.395305	3.395305
Stack Gas Exit Temperature	°F	80	80	80
Stack Location East Coordinate	feet	577	464	464
Stack Location North Coordinate	feet	393	534	546
Hours of Operation per Day	hours/day	3	12	12
Hours of Operation per Year	hours/year	624	3744	3744
Maximum Hourly TDI Emission Rate	lb/hr	0.37	0.0023	0.0023
8-hour Average TDI Emission Rate	lb/hr	0.13875	0.0023	0.0023
24-hour Average TDI Emission Rate	lb/hr	0.04625	0.00115	0.00115
Annual Average TDI Emission Rate	lb/hr	0.026356	0.000983	0.000983

**Modeling Results and**  
**Comparison with FDER No Threat Levels for TDI**

Averaging Time	Maximum Off Property TDI Ground Level Concentration	FDER TDI No Threat Level
8-hour	0.32 $\mu\text{g}/\text{m}^3$	0.36 $\mu\text{g}/\text{m}^3$
24-hour	0.084 $\mu\text{g}/\text{m}^3$	0.0864 $\mu\text{g}/\text{m}^3$
Annual	0.0089 $\mu\text{g}/\text{m}^3$	N/A

**Figure 1**  
**Foamex ISCST2 Modeling of TDI Emissions**  
**Source Locations and Property Line Receptor Locations**



**Attachment A**  
**BREEZE WAKE Output Listing**  
**for Sources of TDI Emissions**

1 RBRZWAKE  
 IBM-PC VERSION (2.1 )  
 (C) COPYRIGHT 1989, TRINITY CONSULTANTS, INC.  
 SERIAL NUMBER 6681 SOLD TO CROSS TESSITORE  
 RUN NAME: FMXTDI  
 RUN BEGAN ON 01-20-93 AT 13:07:26

1  
 BREEZE WAKE DOWNWASH ANALYSIS

The following options have been chosen:

- (1) Calculations are made for the ISCST model.
- (2) All stacks must be within 5L to be considered for direction specific downwash.
- (3) Downwash is calculated in 360 radial directions.
- (4) Buildings are combined.

Note: This analysis determines the direction specific downwash parameters for the flow vector pointing in the direction listed.

Round figures are converted into 8-sided figures for the downwash analysis.

Algorithms:

- 
- 0 = No Downwash
  - 1 = Huber-Snyder Downwash
  - 2 = Schulman-Scire Downwash
- 

1

Input Buildings

Description	Bldg #	Bldg Ht(m)	# of Corners	X(m)	Y(m)
Office A	1	4.27	10	29.57	44.20
				39.62	44.20
				39.62	54.56
				41.15	54.56
				41.15	62.49
				25.60	62.49
				25.60	56.39
				27.13	56.39
				27.13	53.95
				29.57	53.95

Offices B	2	4.27	10	14.33	62.49
				41.15	62.49
				41.15	64.31
				52.43	64.31
				52.43	75.29
				37.19	75.29
				37.19	78.64
				28.65	78.64
				28.65	72.24
				14.33	72.24
Tank	3	9.75	8	21.99	204.87
				23.78	200.56
				21.99	196.25
				17.68	194.46
				13.37	196.25
				11.58	200.56
				13.37	204.87
				17.68	206.66
Long Bun Storage Rm	4	15.24	4	118.87	17.98
				188.98	17.98
				188.98	83.52
				118.87	83.52
East Section 40 ft	5	12.19	4	176.79	83.52
				188.98	83.52
				188.98	121.62
				176.79	121.62
Loading Dock	6	4.88	4	73.15	83.52
				118.87	83.52
				118.87	89.61
				73.15	89.61
Main Roof 35 ft	7	10.67	6	79.25	89.61
				118.87	89.61
				118.87	83.52
				176.79	83.52
				176.79	203.91
				79.25	203.91
East Section 12 ft	8	3.66	4	176.79	142.95
				182.88	142.95
				182.88	150.57
				176.79	150.57
Storage Tanks	9	10.97	4	176.79	176.48
				196.60	176.48
				196.60	191.72
				176.79	191.72



North Section 16 ft	10	4.88	4	70.11	203.91
				185.93	203.91
				185.93	211.53
				70.11	211.53
Storage Bldg	11	6.71	4	198.12	74.37
				210.32	74.37
				210.32	147.53
				198.12	147.53
Methylene Chloride	12	3.05	4	183.80	172.52
				196.60	172.52
				196.60	176.48
				183.80	176.48

1

### Input Stacks

Stack ID #	Stack #	Stack Ht(m)	X(m)	Y(m)
1	1	38.10	175.87	119.79
2	2	12.50	141.43	162.77
3	3	12.50	141.43	166.42

1

### Downwash Structures

Structure 1: Ht= 15.24 m, MPW= 95.97 m, GEP= 38.10 m

Contains the following buildings:

Building # 4: Long Bun Storage Rm

The following stacks are within 5L:

Stack # 1: 1

Structure 2: Ht= 12.19 m, MPW= 125.12 m, GEP= 30.48 m

Contains the following buildings:

Building # 4: Long Bun Storage Rm

Building # 5: East Section 40 ft

The following stacks are within 5L:

Stack # 1: 1

Stack # 2: 2

Stack # 3: 3

Structure 3: Ht= 10.97 m, MPW= 25.00 m, GEP= 27.43 m

Contains the following buildings:

Building # 9: Storage Tanks

The following stacks are within 5L:

Stack # 2: 2

Stack # 3: 3

Structure 4: Ht= 10.67 m, MPW= 215.90 m, GEP= 26.67 m

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Contains the following buildings:

- Building # 4: Long Bun Storage Rm
- Building # 5: East Section 40 ft
- Building # 7: Main Roof 35 ft
- Building # 9: Storage Tanks

The following stacks are within 5L:

- Stack # 1: 1
- Stack # 2: 2
- Stack # 3: 3

Structure 5: Ht= 9.75 m, MPW= 12.19 m, GEP= 24.38 m

---

Contains the following buildings:

- Building # 3: Tank

The following stacks are within 5L:

Structure 6: Ht= 6.71 m, MPW= 215.90 m, GEP= 16.76 m

---

Contains the following buildings:

- Building # 4: Long Bun Storage Rm
- Building # 5: East Section 40 ft
- Building # 7: Main Roof 35 ft
- Building # 9: Storage Tanks
- Building # 11: Storge Bldg

The following stacks are within 5L:

- Stack # 1: 1
- Stack # 2: 2
- Stack # 3: 3

Structure 7: Ht= 4.88 m, MPW= 227.14 m, GEP= 12.19 m

---

Contains the following buildings:

- Building # 4: Long Bun Storage Rm
- Building # 5: East Section 40 ft
- Building # 6: Loading Dock
- Building # 7: Main Roof 35 ft
- Building # 9: Storage Tanks
- Building # 10: North Section 16 ft
- Building # 11: Storge Bldg

The following stacks are within 5L:

- Stack # 1: 1
- Stack # 2: 2
- Stack # 3: 3

Structure 8: Ht= 4.27 m, MPW= 40.19 m, GEP= 10.67 m

---

Contains the following buildings:

- Building # 1: Office A
- Building # 2: Offices B

The following stacks are within 5L:

Structure 9: Ht= 3.66 m, MPW= 227.14 m, GEP= 9.14 m

---

Contains the following buildings:

- Building # 4: Long Bun Storage Rm
- Building # 5: East Section 40 ft
- Building # 6: Loading Dock
- Building # 7: Main Roof 35 ft
- Building # 8: East Section 12 ft
- Building # 9: Storage Tanks
- Building # 10: North Section 16 ft
- Building # 11: Storge Bldg

The following stacks are within 5L:

- Stack # 1: 1
- Stack # 2: 2
- Stack # 3: 3

Structure 10: Ht= 3.05 m, MPW= 227.14 m, GEP= 7.62 m

---

Contains the following buildings:

- Building # 4: Long Bun Storage Rm
- Building # 5: East Section 40 ft
- Building # 6: Loading Dock
- Building # 7: Main Roof 35 ft
- Building # 8: East Section 12 ft
- Building # 9: Storage Tanks
- Building # 10: North Section 16 ft
- Building # 11: Storge Bldg
- Building # 12: Methylene Chloride

The following stacks are within 5L:

- Stack # 1: 1
- Stack # 2: 2
- Stack # 3: 3

NUMBER OF SOURCES = 3

1

Stack ID # 1, Stack # 1

The Dominant Structure Within 5L is:  
STRUC= 1 H= 15.24 W= 95.97 GEP= 38.10

Direction Specific Building Downwash					
Degree	Structure #	Height	Width	GEP	Algorithm
10	1	15.24	84.68	38.10	1
20	1	15.24	91.23	38.10	1
30	1	15.24	95.01	38.10	1
40	1	15.24	95.96	38.10	1
50	1	15.24	95.84	38.10	1
60	1	15.24	93.53	38.10	1
70	0	.00	.00	.00	0
80	0	.00	.00	.00	0
90	0	.00	.00	.00	0
100	0	.00	.00	.00	0
110	0	.00	.00	.00	0
120	0	.00	.00	.00	0
130	0	.00	.00	.00	0
140	0	.00	.00	.00	0
150	1	15.24	93.84	38.10	1
160	1	15.24	90.70	38.10	1
170	1	15.24	83.88	38.10	1
180	0	.00	.00	.00	0
190	0	.00	.00	.00	0
200	1	15.24	91.23	38.10	1
210	1	15.24	95.01	38.10	1
220	1	15.24	95.96	38.10	1
230	1	15.24	95.84	38.10	1
240	1	15.24	93.53	38.10	1
250	0	.00	.00	.00	0
260	0	.00	.00	.00	0
270	0	.00	.00	.00	0
280	0	.00	.00	.00	0
290	0	.00	.00	.00	0
300	0	.00	.00	.00	0
310	0	.00	.00	.00	0
320	0	.00	.00	.00	0
330	1	15.24	93.84	38.10	1
340	1	15.24	90.70	38.10	1
350	1	15.24	83.88	38.10	1
360	1	15.24	75.55	38.10	1

1

Stack ID # 2, Stack # 2

The Dominant Structure Within 5L is:  
STRUC= 2 H= 12.19 W= 125.12 GEP= 30.48

Direction Specific Building Downwash					
Degree	Structure #	Height	Width	GEP	Algorithm
10	2	12.19	84.68	30.48	2
20	2	12.19	88.29	30.48	2
30	4	10.67	196.53	26.67	2
40	4	10.67	209.06	26.67	2
50	4	10.67	215.24	26.67	2
60	4	10.67	215.89	26.67	2
70	4	10.67	214.49	26.67	2
80	4	10.67	206.95	26.67	2
90	4	10.67	193.13	26.67	2
100	4	10.67	194.58	26.67	2
110	4	10.67	194.74	26.67	2
120	4	10.67	192.50	26.67	2
130	4	10.67	186.24	26.67	2
140	4	10.67	176.60	26.67	2
150	4	10.67	161.59	26.67	2
160	4	10.67	148.74	26.67	2
170	4	10.67	138.57	26.67	2
180	4	10.67	125.52	26.67	2
190	4	10.67	154.11	26.67	2
200	2	12.19	88.29	30.48	2
210	4	10.67	196.53	26.67	2
220	3	10.97	24.84	27.43	2
230	3	10.97	24.73	27.43	2
240	3	10.97	23.71	27.43	2
250	3	10.97	21.98	27.43	2
260	3	10.97	19.58	27.43	2
270	4	10.67	193.13	26.67	2
280	4	10.67	194.58	26.67	2
290	4	10.67	194.74	26.67	2
300	4	10.67	192.50	26.67	2
310	2	12.19	125.05	30.48	2
320	2	12.19	122.42	30.48	2
330	2	12.19	116.07	30.48	2
340	2	12.19	106.20	30.48	2
350	2	12.19	93.09	30.48	2
360	2	12.19	77.16	30.48	2

1

Stack ID # 3, Stack # 3

The Dominant Structure Within 5L is:  
 STRUC= 2 H= 12.19 W= 125.12 GEP= 30.48

Direction Specific Building Downwash					
Degree	Structure #	Height	Width	GEP	Algorithm
10	2	12.19	84.68	30.48	2
20	2	12.19	87.62	30.48	2
30	4	10.67	196.53	26.67	2
40	4	10.67	209.06	26.67	2
50	4	10.67	215.24	26.67	2
60	4	10.67	215.89	26.67	2
70	4	10.67	214.49	26.67	2
80	4	10.67	206.95	26.67	2
90	4	10.67	193.13	26.67	2
100	4	10.67	194.58	26.67	2
110	4	10.67	194.74	26.67	2
120	4	10.67	192.50	26.67	2
130	4	10.67	186.24	26.67	2
140	4	10.67	176.60	26.67	2
150	4	10.67	161.59	26.67	2
160	4	10.67	148.74	26.67	2
170	4	10.67	138.57	26.67	2
180	4	10.67	125.52	26.67	2
190	4	10.67	154.11	26.67	2
200	4	10.67	178.03	26.67	2
210	4	10.67	196.53	26.67	2
220	4	10.67	209.06	26.67	2
230	3	10.97	24.58	27.43	2
240	3	10.97	23.71	27.43	2
250	3	10.97	21.98	27.43	2
260	3	10.97	19.58	27.43	2
270	4	10.67	193.13	26.67	2
280	4	10.67	194.58	26.67	2
290	4	10.67	194.74	26.67	2
300	4	10.67	192.50	26.67	2
310	2	12.19	124.83	30.48	2
320	2	12.19	122.42	30.48	2
330	2	12.19	116.07	30.48	2
340	2	12.19	106.20	30.48	2
350	2	12.19	93.09	30.48	2
360	2	12.19	77.16	30.48	2

1

Stack # 1

Stack ID: 1, Building Height: 15.240, Building Width: 95.965  
 15.24015.24015.24015.24015.24015.240.00000.00000.00000.00000.00000.00000  
 .00000.0000015.24015.24015.240.00000.0000015.24015.24015.24015.240  
 .00000.00000.00000.00000.00000.00000.00000.00000.0000015.24015.24015.24015.240  
 84.67791.23295.01595.96595.84093.532.00000.00000.00000.00000.00000.00000  
 .00000.0000093.84490.69983.876.00000.0000091.23295.01595.96595.84093.532  
 .00000.00000.00000.00000.00000.00000.00000.00000.0000093.84490.69983.87675.550

Stack # 2

Stack ID: 2, Building Height: 12.192, Building Width: 125.12  
 12.19212.19210.66810.66810.66810.66810.66810.66810.66810.66810.66810.668  
 10.66810.66810.66810.66810.66810.66810.66812.19210.66810.97310.97310.973  
 10.97310.97310.66810.66810.66810.66812.19212.19212.19212.19212.192  
 84.67788.291196.53209.06215.24215.89214.49206.95193.13194.58194.74192.50  
 186.24176.60161.59148.74138.57125.52154.1188.291196.5324.83924.72623.714  
 21.98219.581193.13194.58194.74192.50125.05122.42116.07106.2093.09477.163

Stack # 3

Stack ID: 3, Building Height: 12.192, Building Width: 125.12  
 12.19212.19210.66810.66810.66810.66810.66810.66810.66810.66810.66810.668  
 10.66810.66810.66810.66810.66810.66810.66810.66810.66810.97310.973  
 10.97310.97310.66810.66810.66810.66812.19212.19212.19212.19212.192  
 84.67787.621196.53209.06215.24215.89214.49206.95193.13194.58194.74192.50  
 186.24176.60161.59148.74138.57125.52154.11178.03196.53209.0624.58323.714  
 21.98219.581193.13194.58194.74192.50124.83122.42116.07106.2093.09477.163

1

RUN ENDED ON 01-20-93 AT 13:07:32

**Attachment B**  
**ISCST2 Output Listings**  
**for Modeling of TDI Emissions**



**Run: FMXTDI8**  
**TDI 8-hour Average Emission Rates**

ISCST2 EXTENDED MODEL - (DATED 92062)

IBM-PC VERSION (1.01)

(C) COPYRIGHT 1992, TRINITY CONSULTANTS, INC.

SERIAL NUMBER 8025 SOLD TO CROSS TESSITORE & ASSOCIATES

RUN BEGAN ON 01/21/93 AT 10:40:44

STARTING

CO TITLEONE Foamex TDI Sources: Foam Line Stack & Rebond Process Exhaust

CO TITLETWO 8-hour Average Emission Rates

MODELOPT DFAULT CONC RURAL

CO AVERTIME 8

CO POLLUTID OTHER

RUNORNOT RUN

FINISHED

STARTING

\*\* Source Location Cards:

**	SRCID	SRCTYP	XS	YS	ZS
SO	LOCATION	1 POINT	175.8720	119.7880	.0000
SO	LOCATION	2 POINT	141.4290	162.7650	.0000
SO	LOCATION	3 POINT	141.4290	166.4230	.0000

\*\* Source Parameter Cards:

**	POINT:	SRCID	QS	HS	TS	VS	DS
**	VOLUME:	SRCID	QS	HS	SYINIT	SZINIT	
**	AREA:	SRCID	QS	HS	XINIT		
SO	SRCPARAM	1	.0174822	38.1000	299.8200	24.3810	.7021
SO	SRCPARAM	2	.0002898	12.4968	299.8200	1.0348	.7620
SO	SRCPARAM	3	.0002898	12.4968	299.8200	1.0348	.7620

\* NOTE: Direction-Specific Building Heights Used for Non-SS Source 1

SO	BUILDHGT	1	15.24	15.24	15.24	15.24	15.24	15.24	
SO	BUILDHGT	1	.00	.00	.00	.00	.00	.00	
SO	BUILDHGT	1	.00	.00	15.24	15.24	15.24	.00	
SO	BUILDHGT	1	.00	15.24	15.24	15.24	15.24	15.24	
SO	BUILDHGT	1	.00	.00	.00	.00	.00	.00	
SO	BUILDHGT	SO BUILDHGT	1	.00	.00	15.24	15.24	15.24	15.24
SO	BUILDHGT	2	12.19	12.19	10.67	10.67	10.67	10.67	
SO	BUILDHGT	2	10.67	10.67	10.67	10.67	10.67	10.67	
SO	BUILDHGT	2	10.67	10.67	10.67	10.67	10.67	10.67	
SO	BUILDHGT	2	10.67	12.19	10.67	10.97	10.97	10.97	
SO	BUILDHGT	2	10.97	10.97	10.67	10.67	10.67	10.67	
SO	BUILDHGT	2	12.19	12.19	12.19	12.19	12.19	12.19	
SO	BUILDHGT	3	12.19	12.19	10.67	10.67	10.67	10.67	
SO	BUILDHGT	3	10.67	10.67	10.67	10.67	10.67	10.67	
SO	BUILDHGT	3	10.67	10.67	10.67	10.67	10.67	10.67	
SO	BUILDHGT	3	10.67	10.67	10.67	10.67	10.67	10.67	
SO	BUILDHGT	3	10.67	10.67	10.67	10.67	10.97	10.97	
SO	BUILDHGT	3	10.97	10.97	10.67	10.67	10.67	10.67	
SO	BUILDHGT	3	12.19	12.19	12.19	12.19	12.19	12.19	

\*\* NOTE: Direction-Specific Building Widths Used for Non-SS Source 1

SO	BUILDWID	1	84.68	91.23	95.01	95.96	95.84	93.53
----	----------	---	-------	-------	-------	-------	-------	-------

SO BUILDWID	1	.00	.00	.00	.00	.00	.00
SO BUILDWID	1	.00	.00	93.84	90.70	83.88	.00
SO BUILDWID	1	.00	91.23	95.01	95.96	95.84	93.53
SO BUILDWID	1	.00	.00	.00	.00	.00	.00
SO BUILDWID	1	.00	.00	93.84	90.70	83.88	75.55
SO BUILDWID	2	84.68	88.29	196.53	209.06	215.24	215.89
SO BUILDWID	2	214.49	206.95	193.13	194.58	194.74	192.50
SO BUILDWID	2	186.24	176.60	161.59	148.74	138.57	125.52
SO BUILDWID	2	154.11	88.29	196.53	24.84	24.73	23.71
SO BUILDWID	2	21.98	19.58	193.13	194.58	194.74	192.50
SO BUILDWID	2	125.05	122.42	116.07	106.20	93.09	77.16
SO BUILDWID	3	84.68	87.62	196.53	209.06	215.24	215.89
SO BUILDWID	3	214.49	206.95	193.13	194.58	194.74	192.50
SO BUILDWID	3	186.24	176.60	161.59	148.74	138.57	125.52
SO BUILDWID	3	154.11	178.03	196.53	209.06	24.58	23.71
SO BUILDWID	3	21.98	19.58	193.13	194.58	194.74	192.50
SO BUILDWID	3	124.83	122.42	116.07	106.20	93.09	77.16

SO ENISUNIT .100000E+07 (GRAMS/SEC) (MICROGRAMS/CUBIC-METER)

SACGROUP ALL  
FINISHED

STARTING

GRIDPOLR POL1 STA  
 RE GRIDPOLR POL1 ORIG 106.68 110.6424  
 RE GRIDPOLR POL1 DIST 150. 200. 250. 300. 350. 400. 450. 500. 550.  
 RE GRIDPOLR POL1 DIST 600. 650. 700. 750. 800. 850. 900. 950. 1000.  
 RE GRIDPOLR POL1 GDIR 36 10. 10.  
 RE GRIDPOLR POL1 END

DISCCART	.00	.00
DISCCART	15.24	.00
RE DISCCART	30.48	.00
RE DISCCART	45.72	.00
RE DISCCART	60.96	.00
RE DISCCART	76.20	.00
RE DISCCART	91.44	.00
RE DISCCART	106.68	.00
RE DISCCART	121.92	.00
RE DISCCART	137.16	.00
RE DISCCART	152.40	.00
RE DISCCART	167.64	.00
RE DISCCART	182.88	.00
RE DISCCART	198.12	.00
RE DISCCART	213.36	.00
RE DISCCART	213.36	15.24
RE DISCCART	213.36	30.48
RE DISCCART	213.36	45.72
RE DISCCART	213.36	60.96
RE DISCCART	213.36	76.20
RE DISCCART	213.36	91.44
RE DISCCART	213.36	106.68
RE DISCCART	213.36	121.92
RE DISCCART	213.36	137.16
RE DISCCART	213.36	152.40
RE DISCCART	213.36	167.64
RE DISCCART	213.36	182.88
RE DISCCART	213.36	198.12
RE DISCCART	213.36	213.36

RE DISCCART 213.36 221.29  
RE DISCCART 198.12 221.29  
RE DISCCART 182.88 221.29  
RE DISCCART 167.64 221.29  
RE DISCCART 152.40 221.29  
RE DISCCART 137.16 221.29  
RE DISCCART 121.92 221.29  
RE DISCCART 106.68 221.29  
RE DISCCART 91.44 221.29  
RE DISCCART 76.20 221.29  
RE DISCCART 60.96 221.29  
RE DISCCART 45.72 221.29  
RE DISCCART 30.48 221.29  
RE DISCCART 15.24 221.29  
RE DISCCART .00 221.29  
RE DISCCART .00 213.36  
RE DISCCART .00 198.12  
RE DISCCART .00 182.88  
RE DISCCART .00 167.64  
RE DISCCART .00 152.40  
RE DISCCART .00 137.16  
RE DISCCART .00 121.92  
RE DISCCART .00 106.68  
RE DISCCART .00 91.44  
RE DISCCART .00 76.20  
RE DISCCART .00 60.96  
RE DISCCART .00 45.72  
RE DISCCART .00 30.48  
RE DISCCART .00 15.24  
FINISHED

STARTING  
ME IMPUTFIL C:\modELS\iscst2\ORLTMP86.BIN UNFORM  
ME AMENHGHT 10.000 METERS  
ME SURFDATA 12815 1986 SURFNAME  
ME UAIRDATA 12842 1986 UAIRNAME  
ME WINDCATS 1.54 3.09 5.14 8.23 10.80  
FINISHED

OU STARTING  
OU RECTABLE 8 FIRST SECOND  
OU MAXTABLE 8 50  
OU FINISHED

\*\*\*\*\*  
\*\*\* SETUP Finishes Successfully \*\*\*  
\*\*\*\*\*

\*\*\*      MODEL SETUP OPTIONS SUMMARY      \*\*\*

\*Model Is Setup For Calculation of Average CONCentration Values.

\*\*Model Uses RURAL Dispersion.

\*Model Uses Regulatory DEFAULT Options:

1. Final Plume Rise.
2. Stack-tip Downwash.
3. Buoyancy-Induced Dispersion.
4. Use Calms Processing Routine.
5. Not Use Missing Data Processing Routine.
6. Default Wind Profile Exponents.
7. Default Vertical Potential Temperature Gradients.
8. "Upper Bound" Values for Supersquat Buildings.
9. No Exponential Decay for RURAL Mode

\*Model Assumes Receptors on FLAT Terrain.

\*Model Assumes No FLAGPOLE Receptor Heights.

\*\*Model Calculates 1 Short Term Average(s) of: 8-HR

\*\*This Run Includes: 3 Source(s); 1 Source Group(s); and 706 Receptor(s)

\*\*The Model Assumes A Pollutant Type of: OTHER

\*Model Set To Continue RUNNING After the Setup Testing.

\*\*Output Options Selected:

- Model Outputs Tables of Highest Short Term Values by Receptor (RECTABLE Keyword)
- Model Outputs Tables of Overall Maximum Short Term Values (MAXTABLE Keyword)

\*\*NOTE: The Following Flags May Appear Following CONC Values:

- c for Calm Hours
- m for Missing Hours
- b for Both Calm and Missing Hours

\*\*Asc. Inputs: Anem. Hgt. (m) = 10.00 ; Decay Coef. = 0.0000 ; Rot. Angle = 0.0  
Emission Units = (GRAMS/SEC) ; Emission Rate Unit Factor = 0.10000E+07  
Output Units = (MICROGRAMS/CUBIC-METER)

\*\*Input Runstream File: D:\MODEL\ISCST2\FOAMEX\FMXTD18.NEW ; \*\*Output Print File: D:\MODEL\ISCST2\FOAMEX\FMXTD18.LST

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* POINT SOURCE DATA \*\*\*

SOURCE ID	NUMBER PART. CATS.	EMISSION RATE (USER UNITS)	X (METERS)	Y (METERS)	BASE	STACK	STACK	STACK	STACK	BUILDING	EMISSION RATE
					ELEV. (METERS)	HEIGHT (METERS)	TEMP. (DEG.K)	EXIT VEL. (M/SEC)	DIAMETER (METERS)	EXISTS	SCALAR VARY BY
1	0	0.17482E-01	175.9	119.8	0.0	38.10	299.82	24.38	0.70	YES	
2	0	0.28980E-03	141.4	162.8	0.0	12.50	299.82	1.03	0.76	YES	
3	0	0.28980E-03	141.4	166.4	0.0	12.50	299.82	1.03	0.76	YES	

\*\*\* ISCST2 - VERSION 92062 \*\*\*

\*\*\* Foamex TDI Sources: Foam Line Stack & Rebond Process Exhaust  
\*\*\* 8-hour Average Emission Rates

\*\*\* 01/21/93  
\*\*\* 10:40:45  
PAGE 3

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* SOURCE IDs DEFINING SOURCE GROUPS \*\*\*

GROUP ID

SOURCE IDs

ALL 1 , 2 , 3 ,

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* DIRECTION SPECIFIC BUILDING DIMENSIONS \*\*\*

SOURCE ID: 1

IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK				
1	15.2,	84.7,	0	2	15.2,	91.2,	0	3	15.2,	95.0,	0	4	15.2,	96.0,	0	5	15.2,	95.8,	0	6	15.2,	93.5,	0
7	0.0,	0.0,	0	8	0.0,	0.0,	0	9	0.0,	0.0,	0	10	0.0,	0.0,	0	11	0.0,	0.0,	0	12	0.0,	0.0,	0
13	0.0,	0.0,	0	14	0.0,	0.0,	0	15	15.2,	93.8,	0	16	15.2,	90.7,	0	17	15.2,	83.9,	0	18	0.0,	0.0,	0
19	0.0,	0.0,	0	20	15.2,	91.2,	0	21	15.2,	95.0,	0	22	15.2,	96.0,	0	23	15.2,	95.8,	0	24	15.2,	93.5,	0
25	0.0,	0.0,	0	26	0.0,	0.0,	0	27	0.0,	0.0,	0	28	0.0,	0.0,	0	29	0.0,	0.0,	0	30	0.0,	0.0,	0
31	0.0,	0.0,	0	32	0.0,	0.0,	0	33	15.2,	93.8,	0	34	15.2,	90.7,	0	35	15.2,	83.9,	0	36	15.2,	75.6,	0

SOURCE ID: 2

IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK				
1	12.2,	84.7,	0	2	12.2,	88.3,	0	3	10.7,	196.5,	0	4	10.7,	209.1,	0	5	10.7,	215.2,	0	6	10.7,	215.9,	0
7	10.7,	214.5,	0	8	10.7,	206.9,	0	9	10.7,	193.1,	0	10	10.7,	194.6,	0	11	10.7,	194.7,	0	12	10.7,	192.5,	0
13	10.7,	186.2,	0	14	10.7,	176.6,	0	15	10.7,	161.6,	0	16	10.7,	148.7,	0	17	10.7,	138.6,	0	18	10.7,	125.5,	0
19	10.7,	154.1,	0	20	12.2,	88.3,	0	21	10.7,	196.5,	0	22	11.0,	24.8,	0	23	11.0,	24.7,	0	24	11.0,	23.7,	0
25	11.0,	22.0,	0	26	11.0,	19.6,	0	27	10.7,	193.1,	0	28	10.7,	194.6,	0	29	10.7,	194.7,	0	30	10.7,	192.5,	0
31	12.2,	125.1,	0	32	12.2,	122.4,	0	33	12.2,	116.1,	0	34	12.2,	106.2,	0	35	12.2,	93.1,	0	36	12.2,	77.2,	0

SOURCE ID: 3

IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK				
1	12.2,	84.7,	0	2	12.2,	87.6,	0	3	10.7,	196.5,	0	4	10.7,	209.1,	0	5	10.7,	215.2,	0	6	10.7,	215.9,	0
7	10.7,	214.5,	0	8	10.7,	206.9,	0	9	10.7,	193.1,	0	10	10.7,	194.6,	0	11	10.7,	194.7,	0	12	10.7,	192.5,	0
13	10.7,	186.2,	0	14	10.7,	176.6,	0	15	10.7,	161.6,	0	16	10.7,	148.7,	0	17	10.7,	138.6,	0	18	10.7,	125.5,	0
19	10.7,	154.1,	0	20	10.7,	178.0,	0	21	10.7,	196.5,	0	22	10.7,	209.1,	0	23	11.0,	24.6,	0	24	11.0,	23.7,	0
25	11.0,	22.0,	0	26	11.0,	19.6,	0	27	10.7,	193.1,	0	28	10.7,	194.6,	0	29	10.7,	194.7,	0	30	10.7,	192.5,	0
31	12.2,	124.8,	0	32	12.2,	122.4,	0	33	12.2,	116.1,	0	34	12.2,	106.2,	0	35	12.2,	93.1,	0	36	12.2,	77.2,	0



\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* GRIDDED RECEPTOR NETWORK SUMMARY \*\*\*

\*\*\* NETWORK ID: POL1 ; NETWORK TYPE: GRIDPOLR \*\*\*

\*\*\* ORIGIN FOR POLAR NETWORK \*\*\*

X-ORIG = 106.68 ; Y-ORIG = 110.64 (METERS)

\*\*\* DISTANCE RANGES OF NETWORK \*\*\*

(METERS)

150.0,	200.0,	250.0,	300.0,	350.0,	400.0,	450.0,	500.0,	550.0,	600.0,
650.0,	700.0,	750.0,	800.0,	850.0,	900.0,	950.0,	1000.0,		

\*\*\* DIRECTION RADIALS OF NETWORK \*\*\*

(DEGREES)

10.0,	20.0,	30.0,	40.0,	50.0,	60.0,	70.0,	80.0,	90.0,	100.0,
110.0,	120.0,	130.0,	140.0,	150.0,	160.0,	170.0,	180.0,	190.0,	200.0,
210.0,	220.0,	230.0,	240.0,	250.0,	260.0,	270.0,	280.0,	290.0,	300.0,
310.0,	320.0,	330.0,	340.0,	350.0,	360.0,				

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* DISCRETE CARTESIAN RECEPTORS \*\*\*  
(X-COORD, Y-COORD, ZELEV, ZFLAG)  
(METERS)

( 0.0, 0.0, 0.0, 0.0);	( 15.2, 0.0, 0.0, 0.0);
( 30.5, 0.0, 0.0, 0.0);	( 45.7, 0.0, 0.0, 0.0);
( 61.0, 0.0, 0.0, 0.0);	( 76.2, 0.0, 0.0, 0.0);
( 91.4, 0.0, 0.0, 0.0);	( 106.7, 0.0, 0.0, 0.0);
( 121.9, 0.0, 0.0, 0.0);	( 137.2, 0.0, 0.0, 0.0);
( 152.4, 0.0, 0.0, 0.0);	( 167.6, 0.0, 0.0, 0.0);
( 182.9, 0.0, 0.0, 0.0);	( 198.1, 0.0, 0.0, 0.0);
( 213.4, 0.0, 0.0, 0.0);	( 213.4, 15.2, 0.0, 0.0);
( 213.4, 30.5, 0.0, 0.0);	( 213.4, 45.7, 0.0, 0.0);
( 213.4, 61.0, 0.0, 0.0);	( 213.4, 76.2, 0.0, 0.0);
( 213.4, 91.4, 0.0, 0.0);	( 213.4, 106.7, 0.0, 0.0);
( 213.4, 121.9, 0.0, 0.0);	( 213.4, 137.2, 0.0, 0.0);
( 213.4, 152.4, 0.0, 0.0);	( 213.4, 167.6, 0.0, 0.0);
( 213.4, 182.9, 0.0, 0.0);	( 213.4, 198.1, 0.0, 0.0);
( 213.4, 213.4, 0.0, 0.0);	( 213.4, 221.3, 0.0, 0.0);
( 198.1, 221.3, 0.0, 0.0);	( 182.9, 221.3, 0.0, 0.0);
( 167.6, 221.3, 0.0, 0.0);	( 152.4, 221.3, 0.0, 0.0);
( 137.2, 221.3, 0.0, 0.0);	( 121.9, 221.3, 0.0, 0.0);
( 106.7, 221.3, 0.0, 0.0);	( 91.4, 221.3, 0.0, 0.0);
( 76.2, 221.3, 0.0, 0.0);	( 61.0, 221.3, 0.0, 0.0);
( 45.7, 221.3, 0.0, 0.0);	( 30.5, 221.3, 0.0, 0.0);
( 15.2, 221.3, 0.0, 0.0);	( 0.0, 221.3, 0.0, 0.0);
( 0.0, 213.4, 0.0, 0.0);	( 0.0, 198.1, 0.0, 0.0);
( 0.0, 182.9, 0.0, 0.0);	( 0.0, 167.6, 0.0, 0.0);
( 0.0, 152.4, 0.0, 0.0);	( 0.0, 137.2, 0.0, 0.0);
( 0.0, 121.9, 0.0, 0.0);	( 0.0, 106.7, 0.0, 0.0);
( 0.0, 91.4, 0.0, 0.0);	( 0.0, 76.2, 0.0, 0.0);
( 0.0, 61.0, 0.0, 0.0);	( 0.0, 45.7, 0.0, 0.0);
( 0.0, 30.5, 0.0, 0.0);	( 0.0, 15.2, 0.0, 0.0);



\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* THE FIRST 24 HOURS OF METEOROLOGICAL DATA \*\*\*

FILE: C:\models\iscst2\ORLTMP86.BIN      FORMAT: UNIFORM  
 SURFACE STATION NO.: 12815      UPPER AIR STATION NO.: 12842  
 NAME: SURFNAME      NAME: UAIRNAME  
 YEAR: 1986      YEAR: 1986

YEAR	MONTH	DAY	HOUR	FLOW	SPEED	TEMP	STAB	MIXING HEIGHT (M)	
				VECTOR	(M/S)	(K)	CLASS	RURAL	URBAN
86	1	1	1	1.0	3.60	289.3	4	639.0	639.0
86	1	1	2	168.0	5.14	288.7	4	639.0	639.0
86	1	1	3	124.0	3.09	288.2	4	639.0	639.0
86	1	1	4	353.0	2.57	288.2	4	639.0	639.0
86	1	1	5	333.0	2.57	288.7	4	639.0	639.0
86	1	1	6	332.0	2.57	288.7	4	639.0	639.0
86	1	1	7	335.0	3.09	288.7	4	639.0	639.0
86	1	1	8	3.0	3.60	289.3	4	639.0	639.0
86	1	1	9	347.0	3.60	289.8	4	639.0	639.0
86	1	1	10	1.0	5.14	292.0	4	639.0	639.0
86	1	1	11	14.0	4.63	292.6	4	639.0	639.0
86	1	1	12	16.0	4.12	294.3	4	639.0	639.0
86	1	1	13	73.0	3.09	295.4	4	639.0	639.0
86	1	1	14	49.0	3.60	297.0	4	639.0	639.0
86	1	1	15	142.0	2.06	296.5	4	639.0	639.0
86	1	1	16	144.0	2.06	295.9	4	639.0	639.0
86	1	1	17	261.0	2.06	295.4	4	639.0	639.0
86	1	1	18	257.0	2.06	292.6	4	644.0	644.0
86	1	1	19	274.0	3.60	291.5	4	655.0	655.0
86	1	1	20	227.0	3.09	290.9	4	666.0	666.0
86	1	1	21	230.0	3.09	290.9	4	678.0	678.0
86	1	1	22	252.0	2.57	290.4	5	689.0	477.0
86	1	1	23	290.0	2.06	290.4	4	700.0	700.0
86	1	1	24	290.0	1.00	290.4	4	712.0	712.0

\*\*\* NOTES: STABILITY CLASS 1=A, 2=B, 3=C, 4=D, 5=E AND 6=F.  
 FLOW VECTOR IS DIRECTION TOWARD WHICH WIND IS BLOWING.

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* THE 1ST HIGHEST 8-HR AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: ALL
INCLUDING SOURCE(S): 1 , 2 , 3 ,

\*\*\* NETWORK ID: POL1 ; NETWORK TYPE: GRIDPOLR \*\*\*

\*\* CONC OF OTHER IN (MICROGRAMS/CUBIC-METER) \*\*

Table with columns: DIRECTION (DEGREES), 150.00, 200.00, 250.00, 300.00, 350.00. Rows range from 10.0 to 360.0 degrees. Each cell contains a concentration value and a source ID in parentheses.

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* THE 1ST HIGHEST 8-HR AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: ALL  
 INCLUDING SOURCE(S): 1 , 2 , 3 ,

\*\*\* NETWORK ID: POL1 ; NETWORK TYPE: GRIDPOLR \*\*\*

\*\* CONC OF OTHER IN (MICROGRAMS/CUBIC-METER) \*\*

RECTION (DEGREES)	DISTANCE (METERS)				
	400.00	450.00	500.00	550.00	600.00
10.0	0.13069 (86071316)	0.11716 (86071316)	0.10267 (86071316)	0.08905 (86091116)	0.08436 (86080316)
20.0	0.09285 (86010216)	0.09605 (86010216)	0.09601 (86010216)	0.09348 (86010216)	0.08942 (86010216)
30.0	0.08980 (86080416)	0.09174 (86080416)	0.08985 (86080416)	0.08552 (86080416)	0.07984 (86080416)
40.0	0.11713 (86080416)	0.11475 (86080416)	0.10770 (86080416)	0.09813 (86080416)	0.08798 (86080416)
50.0	0.10987 (86072616)	0.10836 (86072616)	0.10468 (86100416)	0.10542 (86100416)	0.10299 (86100416)
60.0	0.13375 (86100416)	0.14933 (86100416)	0.15519 (86100416)	0.15369 (86100416)	0.14717 (86100416)
70.0	0.11294 (86072016)	0.12729 (86081816)	0.13759 (86081816)	0.14070 (86081816)	0.13864 (86081816)
80.0	0.12359 (86091216)	0.11959 (86091216)	0.11071 (86091216)	0.09953 (86091216)	0.08822 (86022616)
90.0	0.09695 (86071916)	0.10038 (86071916)	0.09858 (86071916)	0.09345 (86071916)	0.08664 (86071916)
100.0	0.08125c(86071416)	0.08390 (86071916)	0.08487 (86071916)	0.08244 (86071916)	0.07804 (86071916)
110.0	0.13621 (86042916)	0.15372 (86042916)	0.16120 (86042916)	0.16094 (86042916)	0.15581 (86042916)
120.0	0.12399 (86090216)	0.11767 (86090216)	0.11476 (86091316)	0.10961 (86052216)	0.10709 (86012816)
130.0	0.13147 (86042616)	0.12894 (86042616)	0.12138 (86042616)	0.11118 (86042616)	0.11271 (86012816)
140.0	0.09855 (86042816)	0.09875 (86042816)	0.09435 (86042816)	0.08728 (86042816)	0.08061 (86030516)
150.0	0.16069 (86101616)	0.17285 (86101616)	0.17565 (86101616)	0.17174 (86101616)	0.16377 (86101616)
160.0	0.09119 (86110316)	0.09291 (86101616)	0.09850 (86101616)	0.10114 (86101616)	0.10162 (86101616)
170.0	0.14256 (86110316)	0.14035 (86110316)	0.13280 (86110316)	0.12270 (86110316)	0.11180 (86110316)
180.0	0.11295 (86110316)	0.12011 (86110316)	0.12203 (86110316)	0.12036 (86110316)	0.11641 (86110316)
190.0	0.09723c(86082316)	0.08501 (86102116)	0.08268 (86102116)	0.07866 (86102116)	0.07387 (86102116)
200.0	0.12067 (86120416)	0.12557 (86120416)	0.12534 (86120416)	0.12176 (86120416)	0.11622 (86120416)
210.0	0.11567c(86082316)	0.10536 (86111316)	0.10009 (86111316)	0.09384 (86111316)	0.08730 (86111316)
220.0	0.12182c(86082316)	0.10779c(86082316)	0.10777 (86060516)	0.10694 (86060516)	0.10437 (86060516)
230.0	0.09623 (86051116)	0.08885 (86091616)	0.08143 (86091616)	0.07653 (86102216)	0.07754 (86102216)
240.0	0.09868 (86062616)	0.09502 (86091616)	0.09097 (86091616)	0.09087 (86033116)	0.09110 (86033116)
250.0	0.12666 (86091516)	0.12633 (86091516)	0.12272 (86091516)	0.11723 (86091516)	0.11081 (86091516)
260.0	0.10867 (86062616)	0.10289 (86062616)	0.09580 (86062616)	0.08838 (86062616)	0.08113 (86062616)
270.0	0.08931 (86051316)	0.08685c(86082616)	0.08307c(86082616)	0.07850c(86082616)	0.07366c(86082616)
280.0	0.10950 (86062316)	0.10835 (86062316)	0.10527 (86062316)	0.10114 (86062316)	0.09652 (86062316)
290.0	0.12132 (86062316)	0.12227 (86062316)	0.12082 (86062316)	0.11786 (86062316)	0.11395 (86062316)
300.0	0.13655 (86040616)	0.12721 (86040616)	0.11649 (86040616)	0.10574 (86040616)	0.09561 (86040616)
310.0	0.14170 (86040616)	0.12681 (86040616)	0.11213 (86040616)	0.10036 (86100316)	0.09430 (86100316)
320.0	0.12506 (86112516)	0.12394 (86112516)	0.11884 (86112516)	0.11167 (86112516)	0.10366 (86112516)
330.0	0.11710 (86082516)	0.11813 (86082516)	0.11567 (86082516)	0.11085 (86082516)	0.10471 (86082516)
340.0	0.11067 (86082516)	0.10154 (86082516)	0.10725 (86031216)	0.11338 (86031216)	0.11627 (86031216)
350.0	0.12914 (86100916)	0.13043 (86100916)	0.12675 (86100916)	0.12013 (86100916)	0.11215 (86100916)
360.0	0.13541 (86071316)	0.12530 (86071316)	0.12019 (86112616)	0.12475 (86112616)	0.12649 (86112616)

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* THE 1ST HIGHEST 8-HR AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: ALL \*\*\*  
 INCLUDING SOURCE(S): 1 , 2 , 3 ,

\*\*\* NETWORK ID: POL1 ; NETWORK TYPE: GRIDPOLR \*\*\*

\*\* CONC OF OTHER IN (MICROGRAMS/CUBIC-METER) \*\*

RECTION (DEGREES)	DISTANCE (METERS)				
	650.00	700.00	750.00	800.00	850.00
10.0	0.07936 (86080316)	0.07416 (86080316)	0.06901 (86080316)	0.06407 (86080316)	0.06440 (86073008)
20.0	0.08816 (86072316)	0.08808 (86072316)	0.08677 (86072316)	0.08459 (86072316)	0.08196 (86072316)
30.0	0.07718 (86062916)	0.07482 (86062916)	0.07176 (86062916)	0.06832 (86062916)	0.06616 (86021116)
40.0	0.07829 (86080416)	0.06947 (86080416)	0.06281 (86030416)	0.06251 (86030416)	0.06147 (86030416)
50.0	0.09865 (86100416)	0.09330 (86100416)	0.08755 (86100416)	0.08176 (86100416)	0.07614 (86100416)
60.0	0.13811 (86100416)	0.12807 (86100416)	0.11797 (86100416)	0.10828 (86100416)	0.09925 (86100416)
70.0	0.13346 (86081816)	0.12660 (86081816)	0.11900 (86081816)	0.11125 (86081816)	0.10367 (86081816)
80.0	0.08209 (86022616)	0.07571 (86022616)	0.06952 (86022616)	0.06372 (86022616)	0.06254 (86020716)
90.0	0.07936 (86071916)	0.07224 (86071916)	0.06560 (86071916)	0.05954 (86071916)	0.05409 (86071916)
100.0	0.07276 (86071916)	0.06726 (86071916)	0.06189 (86071916)	0.05683 (86071916)	0.05305 (86090616)
110.0	0.14802 (86042916)	0.13900 (86042916)	0.12962 (86042916)	0.12040 (86042916)	0.11161 (86042916)
120.0	0.10329 (86012816)	0.09883 (86012816)	0.09413 (86012816)	0.08998 (86022016)	0.08771 (86022016)
130.0	0.11192 (86012816)	0.10895 (86012816)	0.10466 (86012816)	0.09966 (86012816)	0.09435 (86012816)
140.0	0.07552 (86030516)	0.06996 (86030516)	0.06438 (86030516)	0.05903 (86030516)	0.05409 (86032116)
150.0	0.15364 (86101616)	0.14264 (86101616)	0.13156 (86101616)	0.12093 (86101616)	0.11086 (86101616)
160.0	0.10056 (86101616)	0.09845 (86101616)	0.09567 (86101616)	0.10099 (86111508)	0.10743 (86111508)
170.0	0.10107 (86110316)	0.10010 (86012408)	0.10574 (86012408)	0.11007 (86012408)	0.11174 (86012408)
180.0	0.11116 (86110316)	0.10525 (86110316)	0.09911 (86110316)	0.09302 (86110316)	0.08712 (86110316)
190.0	0.06886 (86102116)	0.06395 (86102116)	0.05931 (86102116)	0.05754 (86111324)	0.05647 (86111324)
200.0	0.10969 (86120416)	0.10278 (86120416)	0.09589 (86120416)	0.08924 (86120416)	0.08492 (86020908)
210.0	0.08083 (86111316)	0.07467 (86111316)	0.07297 (86032716)	0.07243 (86032716)	0.07130 (86032716)
220.0	0.10069 (86060516)	0.09634 (86060516)	0.09169 (86060516)	0.08693 (86060516)	0.08216 (86060516)
230.0	0.07787 (86102216)	0.07761 (86102216)	0.07857 (86050924)	0.08137 (86050924)	0.08308 (86050924)
240.0	0.09685 (86111416)	0.10186 (86111416)	0.10528 (86111416)	0.10772 (86111416)	0.10852 (86111416)
250.0	0.10406 (86091516)	0.09733 (86091516)	0.09085 (86091516)	0.08472 (86091516)	0.07900 (86091516)
260.0	0.07670 (86121416)	0.07651 (86091016)	0.07654 (86091016)	0.07684 (86091016)	0.07607 (86091016)
270.0	0.07619 (86031008)	0.08120 (86031008)	0.08507 (86031008)	0.08843 (86031008)	0.09034 (86031008)
280.0	0.09324 (86040416)	0.09321 (86040416)	0.09234 (86040416)	0.09132 (86040416)	0.08924 (86040416)
290.0	0.10949 (86062316)	0.10475 (86062316)	0.09990 (86062316)	0.09508 (86062316)	0.09057 (86062316)
300.0	0.09145 (86030924)	0.09424 (86030924)	0.09554 (86030924)	0.09564 (86030924)	0.09541 (86030924)
310.0	0.08789 (86100316)	0.08151 (86100316)	0.07649 (86122316)	0.07685 (86122316)	0.07654 (86122316)
320.0	0.09555 (86112516)	0.08774 (86112516)	0.08044 (86112516)	0.07373 (86112516)	0.06762 (86112516)
330.0	0.09799 (86082516)	0.09114 (86082516)	0.08447 (86082516)	0.07814 (86082516)	0.07222 (86082516)
340.0	0.11672 (86031216)	0.11538 (86031216)	0.11280 (86031216)	0.10953 (86031216)	0.10556 (86031216)
350.0	0.10382 (86100916)	0.09569 (86100916)	0.08807 (86100916)	0.08107 (86100916)	0.07478 (86100916)
360.0	0.12604 (86112616)	0.12397 (86112616)	0.12076 (86112616)	0.11676 (86112616)	0.11255 (86112616)

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* THE 1ST HIGHEST 8-HR AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: ALL
INCLUDING SOURCE(S): 1 , 2 , 3 ,

\*\*\* NETWORK ID: POL1 ; NETWORK TYPE: GRIDPOLR \*\*\*

\*\* CONC OF OTHER IN (MICROGRAMS/CUBIC-METER) \*\*

Table with columns: DIRECTION (DEGREES), 900.00, 950.00, 1000.00. Rows list direction angles from 10.0 to 360.0 and corresponding concentration values in parentheses.



MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* THE 1ST HIGHEST 8-HR AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: ALL \*\*\*  
 INCLUDING SOURCE(S): 1 , 2 , 3 ,

\*\*\* DISCRETE CARTESIAN RECEPTOR POINTS \*\*\*

\*\* CONC OF OTHER IN (MICROGRAMS/CUBIC-METER) \*\*

X-COORD (M)	Y-COORD (M)	CONC	(YYMMDDHH)	X-COORD (M)	Y-COORD (M)	CONC	(YYMMDDHH)
0.00	0.00	0.21329	(86091908)	15.24	0.00	0.18996c	(86090108)
30.48	0.00	0.12733c	(86090108)	45.72	0.00	0.20776	(86091808)
60.96	0.00	0.13814c	(86020108)	76.20	0.00	0.13234	(86091708)
91.44	0.00	0.15818	(86121408)	106.68	0.00	0.13769	(86060524)
121.92	0.00	0.21851c	(86011608)	137.16	0.00	0.20422	(86122208)
152.40	0.00	0.15148	(86012408)	167.64	0.00	0.16729	(86120408)
182.88	0.00	0.22097	(86032408)	198.12	0.00	0.18065	(86032808)
213.36	0.00	0.19322	(86090808)	213.36	15.24	0.15092	(86062608)
213.36	30.48	0.17086c	(86111308)	213.36	45.72	0.19673c	(86111308)
213.36	60.96	0.23567c	(86041408)	213.36	76.20	0.16224c	(86090408)
213.36	91.44	0.27136c	(86031124)	213.36	106.68	0.28134	(86102624)
213.36	121.92	0.27821	(86060608)	213.36	137.16	0.23556c	(86012524)
213.36	152.40	0.19908c	(86101508)	213.36	167.64	0.28253c	(86101108)
213.36	182.88	0.31579c	(86100508)	213.36	198.12	0.18158	(86120224)
213.36	213.36	0.28075	(86072508)	213.36	221.29	0.24429	(86072508)
198.12	221.29	0.23913c	(86071608)	182.88	221.29	0.20568c	(86082508)
167.64	221.29	0.26836c	(86082508)	152.40	221.29	0.25970c	(86081824)
137.16	221.29	0.31468	(86012608)	121.92	221.29	0.21545	(86121008)
106.68	221.29	0.24831	(86031208)	91.44	221.29	0.15822	(86031908)
76.20	221.29	0.28161	(86050708)	60.96	221.29	0.22547	(86050708)
45.72	221.29	0.22299c	(86081224)	30.48	221.29	0.17618c	(86120208)
15.24	221.29	0.13924c	(86120208)	0.00	221.29	0.11061	(86080924)
0.00	213.36	0.13680c	(86100324)	0.00	198.12	0.15725	(86092924)
0.00	182.88	0.18367c	(86110508)	0.00	167.64	0.20693	(86112808)
0.00	152.40	0.19605c	(86100108)	0.00	137.16	0.13477c	(86050508)
0.00	121.92	0.21523c	(86060308)	0.00	106.68	0.17226c	(86021708)
0.00	91.44	0.14078c	(86080708)	0.00	76.20	0.16022c	(86092908)
0.00	60.96	0.14339	(86091524)	0.00	45.72	0.13282	(86091524)
0.00	30.48	0.14484c	(86100208)	0.00	15.24	0.22442	(86091908)

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* THE 2ND HIGHEST 8-HR AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: ALL      \*\*\*  
 INCLUDING SOURCE(S): 1 , 2 , 3 ,

\*\*\* NETWORK ID: POL1 ; NETWORK TYPE: GRIDPOLR \*\*\*

\*\* CONC OF OTHER IN (MICROGRAMS/CUBIC-METER) \*\*

DIRECTION (DEGREES)	DISTANCE (METERS)				
	150.00	200.00	250.00	300.00	350.00
10.0	0.16966c(86071508)	0.14052c(86041208)	0.12332 (86071316)	0.11064 (86091116)	0.11990 (86091116)
20.0	0.19723c(86081824)	0.12854c(86061808)	0.09006 (86091308)	0.07674 (86060816)	0.08572 (86010216)
30.0	0.20840c(86121124)	0.13425c(86121124)	0.10600c(86100508)	0.09047c(86100508)	0.08038c(86072008)
40.0	0.22433c(86090708)	0.12986 (86100608)	0.11487c(86100508)	0.09592c(86100508)	0.09504 (86100608)
50.0	0.20144 (86022008)	0.15246 (86111808)	0.13448 (86040808)	0.08966c(86071908)	0.10238 (86072616)
60.0	0.20129 (86040808)	0.11228 (86030624)	0.11607 (86030624)	0.07620c(86060908)	0.08755 (86072016)
70.0	0.14720 (86071408)	0.12809c(86092808)	0.09034 (86020716)	0.09461 (86090308)	0.09251c(86100508)
80.0	0.12854c(86070624)	0.12496 (86042508)	0.08883 (86081524)	0.09585 (86091216)	0.08652c(86071908)
90.0	0.13272c(86101024)	0.10533 (86011308)	0.07507c(86122524)	0.06240 (86071916)	0.08257 (86071516)
100.0	0.14632c(86101508)	0.12633c(86012308)	0.07484c(86012524)	0.07079c(86101424)	0.07199 (86050816)
110.0	0.13258 (86102624)	0.10331c(86012308)	0.08096 (86102624)	0.07714 (86052216)	0.09469 (86052216)
120.0	0.15721c(86041408)	0.09769 (86041808)	0.07812 (86102624)	0.09587 (86042616)	0.10793 (86042616)
130.0	0.13487c(86011608)	0.10793 (86021408)	0.10627c(86041408)	0.08333c(86090408)	0.09149 (86042816)
140.0	0.14026 (86101708)	0.11988 (86062608)	0.08614 (86011408)	0.07152 (86042816)	0.07907c(86111308)
150.0	0.17614c(86041408)	0.12645c(86041408)	0.07935c(86092408)	0.09067 (86032808)	0.07902 (86101516)
160.0	0.12025 (86012408)	0.08653 (86033008)	0.08148 (86110316)	0.09699 (86110316)	0.08908c(86041408)
170.0	0.12111c(86090208)	0.13935 (86122208)	0.09791 (86122208)	0.11616c(86082316)	0.10567c(86082316)
180.0	0.11966c(86092308)	0.14012c(86092308)	0.11507c(86082316)	0.09120c(86011608)	0.09985 (86110316)
190.0	0.11594 (86111008)	0.09770c(86092208)	0.09087c(86090208)	0.08731 (86092716)	0.09092 (86120416)
200.0	0.09193c(86020108)	0.07358 (86102824)	0.08211 (86111316)	0.09065 (86111316)	0.10872c(86082316)
210.0	0.13988 (86051408)	0.12837c(86082316)	0.11930 (86091808)	0.10522 (86091808)	0.10825 (86111316)
220.0	0.14202 (86091908)	0.12535 (86091908)	0.13690c(86082316)	0.12147c(86090108)	0.10745c(86090108)
230.0	0.12635c(86090108)	0.10501c(86100208)	0.09976c(86100208)	0.10390 (86062616)	0.10074 (86062616)
240.0	0.12537c(86051708)	0.09118 (86062616)	0.09082 (86091524)	0.09379 (86091616)	0.09726 (86091616)
250.0	0.13939c(86092908)	0.10548 (86092724)	0.08907 (86091516)	0.10971 (86091516)	0.11427 (86062616)
260.0	0.11108c(86021708)	0.09746c(86060308)	0.10184 (86062616)	0.09487c(86060308)	0.08683 (86121416)
270.0	0.14405c(86042008)	0.07139 (86091016)	0.07707 (86092216)	0.08569 (86092216)	0.08882c(86082616)
280.0	0.11210 (86081108)	0.10536 (86112324)	0.10194c(86100108)	0.10482 (86070616)	0.10756 (86062316)
290.0	0.14534 (86092624)	0.11241c(86021708)	0.09847c(86110508)	0.09718 (86043016)	0.10309c(86090516)
300.0	0.13093 (86052724)	0.10250 (86092924)	0.10348 (86093016)	0.11245 (86093016)	0.11364 (86093016)
310.0	0.11657c(86092508)	0.10835 (86093016)	0.12981 (86093016)	0.13742 (86093016)	0.13390 (86093016)
320.0	0.12682 (86092424)	0.12001 (86040616)	0.11792 (86040616)	0.11637 (86081016)	0.11974 (86112516)
330.0	0.13409 (86112524)	0.11514 (86052916)	0.08776 (86051816)	0.09935 (86082516)	0.09991 (86080816)
340.0	0.13136c(86041308)	0.09101 (86080816)	0.09685 (86080816)	0.10118 (86080816)	0.10720 (86082716)
350.0	0.13757 (86062008)	0.09817c(86020808)	0.10285 (86082716)	0.10534 (86100916)	0.11140 (86031216)
360.0	0.14533c(86020408)	0.10377 (86061624)	0.09597 (86061416)	0.10562 (86100916)	0.10665 (86100916)

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* THE 2ND HIGHEST 8-HR AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: ALL \*\*\*  
INCLUDING SOURCE(S): 1 , 2 , 3 ,

\*\*\* NETWORK ID: POL1 ; NETWORK TYPE: GRIDPOLR \*\*\*

\*\* CONC OF OTHER IN (MICROGRAMS/CUBIC-METER) \*\*

SECTION (DEGREES)	400.00	450.00	500.00	550.00	600.00
10.0	0.11856 (86091116)	0.11095 (86091116)	0.10042 (86091116)	0.08879 (86080316)	0.08196 (86110516)
20.0	0.08678 (86101416)	0.08894 (86101416)	0.08699 (86101416)	0.08287 (86072316)	0.08657 (86072316)
30.0	0.07368 (86061716)	0.07809 (86061716)	0.07826 (86061716)	0.07776 (86062916)	0.07837 (86062916)
40.0	0.08863 (86072616)	0.08827 (86072616)	0.08434 (86072616)	0.07858 (86072616)	0.07414 (86070208)
50.0	0.09144 (86100416)	0.10021 (86100416)	0.10229 (86072616)	0.09394 (86072616)	0.08488 (86072616)
60.0	0.09290 (86072016)	0.09554 (86070116)	0.10213 (86070116)	0.10503 (86070116)	0.10511 (86070116)
70.0	0.10872 (86081816)	0.11569 (86072016)	0.11284 (86072016)	0.10669 (86072016)	0.09897 (86072016)
80.0	0.08675 (86022616)	0.09435 (86022616)	0.09596 (86022616)	0.09331 (86022616)	0.08784 (86091216)
90.0	0.08366 (86091216)	0.08775 (86091216)	0.08689 (86091216)	0.08260 (86091216)	0.07650 (86091216)
100.0	0.07822 (86071916)	0.08002c(86071416)	0.07438c(86071416)	0.06892 (86042916)	0.06423 (86030516)
110.0	0.10130 (86042816)	0.09970 (86042816)	0.09415 (86042816)	0.09639 (86012316)	0.09609 (86012316)
120.0	0.11393 (86091316)	0.11716 (86091316)	0.11328 (86042816)	0.10949 (86012816)	0.10385 (86052216)
130.0	0.09617 (86042816)	0.09426 (86042816)	0.10284 (86012816)	0.11016 (86012816)	0.10046 (86042616)
140.0	0.07502 (86030516)	0.08326 (86030516)	0.08590 (86030516)	0.08447 (86030516)	0.07932 (86042816)
150.0	0.08918 (86101516)	0.09242 (86101516)	0.09038 (86101516)	0.08510 (86101516)	0.07835 (86101516)
160.0	0.08476c(86041408)	0.08122 (86110316)	0.07784 (86101516)	0.07976 (86101516)	0.07965 (86101516)
170.0	0.10077 (86110416)	0.09422 (86110416)	0.08551 (86011216)	0.08004 (86011216)	0.08298 (86012408)
180.0	0.10822c(86082316)	0.09829 (86110416)	0.09950 (86110416)	0.09773 (86110416)	0.09411 (86110416)
190.0	0.09016 (86120416)	0.08495c(86082316)	0.07645 (86120416)	0.06804 (86120416)	0.06005 (86120416)
200.0	0.09678 (86092716)	0.09358 (86092716)	0.08787 (86092716)	0.08125 (86102016)	0.07947 (86102016)
210.0	0.10859 (86111316)	0.09881c(86082316)	0.09140 (86042416)	0.08770 (86042416)	0.08297 (86042416)
220.0	0.10078 (86060516)	0.10605 (86060516)	0.09353c(86082316)	0.09339 (86112116)	0.09254 (86112116)
230.0	0.09516 (86091616)	0.08714 (86051116)	0.07802 (86051116)	0.07390 (86091616)	0.07019 (86112116)
240.0	0.09738 (86091616)	0.09013 (86062616)	0.08929 (86033116)	0.08618 (86091616)	0.09001 (86111416)
250.0	0.10837 (86062616)	0.10011 (86062616)	0.09115 (86062616)	0.08274 (86091716)	0.08057 (86091716)
260.0	0.08960 (86121416)	0.08949 (86121416)	0.08752 (86121416)	0.08443 (86121416)	0.08071 (86121416)
270.0	0.08911c(86082616)	0.08487 (86092216)	0.08078 (86092216)	0.07621 (86092216)	0.07155 (86092216)
280.0	0.10921 (86070616)	0.10499 (86070616)	0.09875 (86070616)	0.09170 (86070616)	0.09218 (86040416)
290.0	0.10682c(86090516)	0.10574c(86090516)	0.10163c(86090516)	0.09592c(86090516)	0.08951c(86090516)
300.0	0.11040 (86093016)	0.10423 (86093016)	0.09665 (86093016)	0.08871 (86093016)	0.08692 (86030924)
310.0	0.12491 (86093016)	0.11322 (86093016)	0.10541 (86100316)	0.09866 (86040616)	0.08676 (86040616)
320.0	0.10538 (86052916)	0.09453 (86052816)	0.08675 (86052816)	0.08231 (86081116)	0.07806 (86081116)
330.0	0.09926 (86080816)	0.09466 (86080816)	0.08826 (86080816)	0.08054 (86080816)	0.07355 (86081116)
340.0	0.10697 (86082716)	0.10106 (86082716)	0.09275 (86082716)	0.08524 (86100916)	0.08314 (86100916)
350.0	0.11670 (86031216)	0.11478 (86031216)	0.10848 (86031216)	0.10026 (86031216)	0.09167 (86031216)
360.0	0.10902 (86091116)	0.11215 (86112616)	0.11326 (86071316)	0.10951 (86102516)	0.10766 (86102516)

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* THE 2ND HIGHEST 8-HR AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: ALL \*\*\*  
 INCLUDING SOURCE(S): 1 , 2 , 3 ,

\*\*\* NETWORK ID: POL1 ; NETWORK TYPE: GRIDPOLR \*\*\*

\*\* CONC OF OTHER IN (MICROGRAMS/CUBIC-METER) \*\*

RECTION (DEGREES)	DISTANCE (METERS)				
	650.00	700.00	750.00	800.00	850.00
10.0	0.07627 (86110616)	0.07082 (86110616)	0.06542 (86110616)	0.06363 (86073008)	0.06290 (86113016)
20.0	0.08456 (86010216)	0.07936 (86010216)	0.07501 (86112916)	0.07353 (86112916)	0.07427 (86031108)
30.0	0.07366 (86080416)	0.06756 (86080416)	0.06474 (86021116)	0.06578 (86021116)	0.06474 (86062916)
40.0	0.07045 (86070208)	0.06654 (86070208)	0.06259 (86070208)	0.05874 (86070208)	0.05509 (86070208)
50.0	0.07851 (86073116)	0.07418 (86073116)	0.07420 (86112016)	0.07470 (86112016)	0.07420 (86112016)
60.0	0.10334 (86070116)	0.10042 (86070116)	0.09721 (86031116)	0.09625 (86031116)	0.09459 (86031116)
70.0	0.09089 (86072016)	0.08306 (86072016)	0.07639 (86031116)	0.07271 (86031116)	0.06884 (86031116)
80.0	0.07675 (86091216)	0.06710 (86091216)	0.05885 (86091216)	0.06065 (86020716)	0.05839 (86022616)
90.0	0.06954 (86091216)	0.06282 (86091216)	0.05663 (86091216)	0.05271 (86041616)	0.05202c(86022116)
100.0	0.05964 (86030516)	0.05495 (86030516)	0.05081 (86060616)	0.05124 (86090616)	0.05216 (86071916)
110.0	0.09358 (86012316)	0.08976 (86012316)	0.08524 (86012316)	0.08043 (86012316)	0.07560 (86012316)
120.0	0.09696 (86052216)	0.09395 (86022016)	0.09220 (86022016)	0.08942 (86012816)	0.08491 (86012816)
130.0	0.09023 (86042616)	0.09003 (86121716)	0.08998 (86121716)	0.08889 (86121716)	0.08725 (86121716)
140.0	0.07143 (86042816)	0.06408 (86042816)	0.05889c(86072416)	0.05581 (86032116)	0.05405 (86030516)
150.0	0.07120 (86101516)	0.06695 (86032108)	0.07025 (86032108)	0.07280 (86032108)	0.07389 (86032108)
160.0	0.07808 (86101516)	0.08322 (86111508)	0.09216 (86111508)	0.09252 (86101616)	0.09311 (86101608)
170.0	0.09241 (86012408)	0.09102 (86110316)	0.08186 (86110316)	0.07535 (86120508)	0.07769 (86120508)
180.0	0.08943 (86110416)	0.08427 (86110416)	0.07912 (86122616)	0.07769 (86122616)	0.07550 (86032216)
190.0	0.05575 (86111324)	0.05735 (86111324)	0.05779 (86111324)	0.05504 (86102116)	0.05410 (86122616)
200.0	0.07690 (86102016)	0.07390 (86102016)	0.07571 (86020908)	0.08108 (86020908)	0.08296 (86120416)
210.0	0.07781 (86042416)	0.07373 (86120416)	0.07034 (86120416)	0.06682 (86120416)	0.06566 (86010716)
220.0	0.09059 (86112116)	0.08788 (86112116)	0.08469 (86112116)	0.08130 (86112116)	0.07770 (86112116)
230.0	0.06961 (86050924)	0.07448 (86050924)	0.07708 (86102216)	0.07590 (86102216)	0.07439 (86102216)
240.0	0.09028 (86033116)	0.08870 (86033116)	0.08658 (86033116)	0.08459 (86102908)	0.08793 (86102908)
250.0	0.07783 (86091716)	0.07477 (86091716)	0.07154 (86091716)	0.06838 (86091716)	0.06512 (86091716)
260.0	0.07605 (86091016)	0.07261 (86121416)	0.06857 (86121416)	0.06700 (86122308)	0.06818 (86122308)
270.0	0.07029c(86020824)	0.07170 (86122224)	0.07426 (86122224)	0.07661 (86122224)	0.07747 (86122224)
280.0	0.09173 (86062316)	0.08696 (86062316)	0.08232 (86062316)	0.07788 (86062316)	0.07370 (86062316)
290.0	0.08297c(86090516)	0.07662c(86090516)	0.07062c(86090516)	0.06507c(86090516)	0.06445 (86120816)
300.0	0.08637 (86040616)	0.07807 (86040616)	0.07070 (86040616)	0.06708 (86030916)	0.06741 (86122316)
310.0	0.07808 (86030916)	0.07558 (86030916)	0.07539 (86100316)	0.06965 (86100316)	0.06640 (86030916)
320.0	0.07337 (86081116)	0.06860 (86081116)	0.06394 (86081116)	0.05951 (86081116)	0.05675 (86110616)
330.0	0.06950 (86081116)	0.06528 (86081116)	0.06328 (86031308)	0.06371 (86031308)	0.06337 (86031308)
340.0	0.08005 (86100916)	0.07962 (86070516)	0.08071 (86070516)	0.08110 (86070516)	0.08042 (86070516)
350.0	0.08351 (86031216)	0.07611 (86031216)	0.07112 (86052008)	0.07340 (86052008)	0.07476 (86052008)
360.0	0.10365 (86102516)	0.09842 (86102516)	0.09259 (86102516)	0.08661 (86102516)	0.08175 (86110516)

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* THE 2ND HIGHEST 8-HR AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: ALL
INCLUDING SOURCE(S): 1 , 2 , 3 ,

\*\*\* NETWORK ID: POL1 ; NETWORK TYPE: GRIDPOLR \*\*\*

\*\* CONC OF OTHER IN (MICROGRAMS/CUBIC-METER) \*\*

Table with columns: DIRECTION (DEGREES), 900.00, 950.00, 1000.00. Rows list direction angles from 10.0 to 360.0 and corresponding concentration values in parentheses.

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* THE 2ND HIGHEST 8-HR AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: ALL  
 INCLUDING SOURCE(S): 1 , 2 , 3 ,

\*\*\* DISCRETE CARTESIAN RECEPTOR POINTS \*\*\*

\*\* CONC OF OTHER IN (MICROGRAMS/CUBIC-METER) \*\*

X-COORD (M)	Y-COORD (M)	CONC (YYMMDDHH)	X-COORD (M)	Y-COORD (M)	CONC (YYMMDDHH)
0.00	0.00	0.17491c (86090108)	15.24	0.00	0.14330c (86083008)
30.48	0.00	0.12390c (86051808)	45.72	0.00	0.18048 (86051408)
60.96	0.00	0.13151 (86051408)	76.20	0.00	0.12125 (86111108)
91.44	0.00	0.13690 (86111008)	106.68	0.00	0.11127c (86020208)
121.92	0.00	0.21092c (86092308)	137.16	0.00	0.18946c (86090208)
152.40	0.00	0.13475 (86021608)	167.64	0.00	0.13660 (86033008)
182.88	0.00	0.21414c (86041408)	198.12	0.00	0.13373 (86111508)
213.36	0.00	0.13759 (86062608)	213.36	15.24	0.14814 (86090808)
213.36	30.48	0.14666c (86011608)	213.36	45.72	0.16608 (86041908)
213.36	60.96	0.19107c (86090408)	213.36	76.20	0.15887 (86031708)
213.36	91.44	0.16733 (86031708)	213.36	106.68	0.20817c (86101508)
213.36	121.92	0.24649c (86012308)	213.36	137.16	0.22109 (86011308)
213.36	152.40	0.16935 (86012108)	213.36	167.64	0.25824c (86071908)
213.36	182.88	0.23934c (86041608)	213.36	198.12	0.18122c (86060808)
213.36	213.36	0.26135 (86040808)	213.36	221.29	0.19209c (86061408)
198.12	221.29	0.22060c (86090708)	182.88	221.29	0.20538c (86071908)
167.64	221.29	0.25651c (86121124)	152.40	221.29	0.25892c (86061808)
137.16	221.29	0.25898c (86071508)	121.92	221.29	0.19857c (86020408)
106.68	221.29	0.20993c (86020408)	91.44	221.29	0.12852 (86110616)
76.20	221.29	0.18755 (86031908)	60.96	221.29	0.17141 (86112524)
45.72	221.29	0.17407c (86120208)	30.48	221.29	0.14688 (86092424)
15.24	221.29	0.13625c (86051808)	0.00	221.29	0.10776c (86100808)
0.00	213.36	0.12868 (86081024)	0.00	198.12	0.15227 (86092624)
0.00	182.88	0.15071 (86052724)	0.00	167.64	0.19770 (86092924)
0.00	152.40	0.15239 (86112324)	0.00	137.16	0.12358 (86112508)
0.00	121.92	0.19064c (86042008)	0.00	106.68	0.16152c (86060308)
0.00	91.44	0.11608 (86092724)	0.00	76.20	0.16020 (86092724)
0.00	60.96	0.11636c (86042324)	0.00	45.72	0.12607c (86051708)
0.00	30.48	0.14137 (86092608)	0.00	15.24	0.16133c (86090108)

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* THE MAXIMUM 50 8-HR AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: ALL  
INCLUDING SOURCE(S): 1 , 2 , 3 ,

\*\* CONC OF OTHER IN (MICROGRAMS/CUBIC-METER) \*\*

RANK	CONC (YYMMDDHH) AT	RECEPTOR (XR,YR) OF TYPE	RANK	CONC (YYMMDDHH) AT	RECEPTOR (XR,YR) OF TYPE
1.	0.31579c(86100508) AT (	213.36, 182.88) DC	26.	0.23567c(86041408) AT (	213.36, 60.96) DC
2.	0.31468 (86012608) AT (	137.16, 221.29) DC	27.	0.23556c(86012524) AT (	213.36, 137.16) DC
3.	0.28253c(86101108) AT (	213.36, 167.64) DC	28.	0.22555 (86071708) AT (	137.16, 221.29) DC
4.	0.28161 (86050708) AT (	76.20, 221.29) DC	29.	0.22547 (86050708) AT (	60.96, 221.29) DC
5.	0.28134 (86102624) AT (	213.36, 106.68) DC	30.	0.22442 (86091908) AT (	0.00, 15.24) DC
6.	0.28075 (86072508) AT (	213.36, 213.36) DC	31.	0.22433c(86090708) AT (	203.10, 225.55) GP
7.	0.27821 (86060608) AT (	213.36, 121.92) DC	32.	0.22299c(86081224) AT (	45.72, 221.29) DC
8.	0.27136c(86031124) AT (	213.36, 91.44) DC	33.	0.22249 (86111808) AT (	213.36, 213.36) DC
9.	0.26836c(86082508) AT (	167.64, 221.29) DC	34.	0.22243 (86012608) AT (	132.73, 258.36) GP
10.	0.26135 (86040808) AT (	213.36, 213.36) DC	35.	0.22228c(86071808) AT (	167.64, 221.29) DC
11.	0.25970c(86081824) AT (	152.40, 221.29) DC	36.	0.22117c(86010324) AT (	137.16, 221.29) DC
12.	0.25898c(86071508) AT (	137.16, 221.29) DC	37.	0.22109 (86011308) AT (	213.36, 137.16) DC
13.	0.25892c(86061808) AT (	152.40, 221.29) DC	38.	0.22097 (86032408) AT (	182.88, 0.00) DC
14.	0.25824c(86071908) AT (	213.36, 167.64) DC	39.	0.22060c(86090708) AT (	198.12, 221.29) DC
15.	0.25651c(86121124) AT (	167.64, 221.29) DC	40.	0.22014c(86061008) AT (	167.64, 221.29) DC
16.	0.25550c(86050808) AT (	152.40, 221.29) DC	41.	0.21945c(86072008) AT (	181.68, 240.55) GP
17.	0.25190c(86100508) AT (	236.58, 185.64) GP	42.	0.21851c(86011608) AT (	121.92, 0.00) DC
18.	0.24831 (86031208) AT (	106.68, 221.29) DC	43.	0.21842 (86072324) AT (	152.40, 221.29) DC
19.	0.24649c(86012308) AT (	213.36, 121.92) DC	44.	0.21696 (86030408) AT (	213.36, 213.36) DC
20.	0.24429 (86072508) AT (	213.36, 221.29) DC	45.	0.21545 (86121008) AT (	121.92, 221.29) DC
21.	0.24198c(86013008) AT (	152.40, 221.29) DC	46.	0.21523c(86060308) AT (	0.00, 121.92) DC
22.	0.23934c(86041608) AT (	213.36, 182.88) DC	47.	0.21472c(86053108) AT (	137.16, 221.29) DC
23.	0.23913c(86071608) AT (	198.12, 221.29) DC	48.	0.21414c(86041408) AT (	182.88, 0.00) DC
24.	0.23625c(86071608) AT (	203.10, 225.55) GP	49.	0.21378c(86051208) AT (	167.64, 221.29) DC
25.	0.23584 (86072308) AT (	167.64, 221.29) DC	50.	0.21332c(86041208) AT (	152.40, 221.29) DC

RECEPTOR TYPES: GC = GRIDCART  
GP = GRIDPOLR  
DC = DISCCART  
DP = DISCPOLR  
BD = BOUNDARY

\*\*\* ISCST2 - VERSION 92062 \*\*\*

\*\*\* Foamex TDI Sources: Foam Line Stack & Rebond Process Exhaust

\*\*\* 01/21/93

\*\*\* 8-hour Average Emission Rates

\*\*\* 10:40:45

PAGE 20

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* THE SUMMARY OF HIGHEST 8-HR RESULTS \*\*\*

\*\* CONC OF OTHER IN (MICROGRAMS/CUBIC-METER) \*\*

GROUP ID	AVERAGE CONC	DATE (YYMMDDHH)	RECEPTOR (XR, YR, ZELEV, ZFLAG)	OF TYPE	NETWORK GRID-ID
ALL	HIGH 1ST HIGH VALUE IS	0.31579c ON 86100508: AT (	213.36, 182.88, 0.00,	0.00)	DC
	HIGH 2ND HIGH VALUE IS	0.26135 ON 86040808: AT (	213.36, 213.36, 0.00,	0.00)	DC

- \*\* RECEPTOR TYPES:
- GC = GRIDCART
  - GP = GRIDPOLR
  - DC = DISCCART
  - DP = DISCPOLR
  - BD = BOUNDARY



\*\*\* ISCST2 - VERSION 92062 \*\*\*      \*\*\* Foamex TDI Sources: Foam Line Stack & Rebond Process Exhaust  
                                         \*\*\* 8-hour Average Emission Rates

\*\*\* 01/21/93  
\*\*\* 10:40:45  
PAGE 21

\*\*\* MODELING OPTIONS USED: CONC    RURAL    FLAT                    DFAULT

\*\*\* Message Summary For ISC2 Model Execution \*\*\*

----- Summary of Total Messages -----

A Total of                    0 Fatal Error Message(s)  
Total of                      0 Warning Message(s)  
Total of                      328 Informational Message(s)  
  
Total of                      328 Calm Hours Identified

\*\*\*\*\* FATAL ERROR MESSAGES \*\*\*\*\*  
          \*\*\* NONE \*\*\*

\*\*\*\*\* WARNING MESSAGES \*\*\*\*\*  
          \*\*\* NONE \*\*\*

\*\*\*\*\*  
\*\*\* ISCST2 Finishes Successfully \*\*\*  
\*\*\*\*\*

**Run: FMXTDI8**  
**TDI 24-hour Average Emission Rates**

ISCST2 EXTENDED MODEL - (DATED 92062)

IBM-PC VERSION (1.01)

(C) COPYRIGHT 1992, TRINITY CONSULTANTS, INC.

SERIAL NUMBER 8025 SOLD TO CROSS TESSITORE & ASSOCIATES

RUN BEGAN ON 01/21/93 AT 10:56:06

CO STARTING

CO TITLEONE Foamex TDI Sources: Foam Line Stack & Rebond Process Exhaust

CO TITLETWO 24-hour Average Emission Rates

CO MODELOPT DFAULT CONC RURAL

CO AVERTIME 24

CO POLLUTID OTHER

CO RUNORNOT RUN

CO FINISHED

CO STARTING

\*\* Source Location Cards:

	SRCID	SRCTYP	XS	YS	ZS
SO LOCATION	1	POINT	175.8720	119.7880	.0000
SO LOCATION	2	POINT	141.4290	162.7650	.0000
SO LOCATION	3	POINT	141.4290	166.4230	.0000

\*\* Source Parameter Cards:

	POINT:	SRCID	QS	HS	TS	VS	DS
SO VOLUME:	SRCID	QS	HS	SYINIT	SZINIT		
** AREA:	SRCID	QS	HS	XINIT			
SO SRCPARAM	1	.0058274	38.1000	299.8200	24.3810	.7021	
SO SRCPARAM	2	.0001449	12.4968	299.8200	1.0348	.7620	
SO SRCPARAM	3	.0001449	12.4968	299.8200	1.0348	.7620	

NOTE: Direction-Specific Building Heights Used for Non-SS Source 1

SO BUILDHGT	1	15.24	15.24	15.24	15.24	15.24	15.24
BUILDHGT	1	.00	.00	.00	.00	.00	.00
BUILDHGT	1	.00	.00	15.24	15.24	15.24	.00
SO BUILDHGT	1	.00	15.24	15.24	15.24	15.24	15.24
BUILDHGT	1	.00	.00	.00	.00	.00	.00
BUILDHGT	1	.00	.00	15.24	15.24	15.24	15.24
SO BUILDHGT	2	12.19	12.19	10.67	10.67	10.67	10.67
SO BUILDHGT	2	10.67	10.67	10.67	10.67	10.67	10.67
BUILDHGT	2	10.67	10.67	10.67	10.67	10.67	10.67
SO BUILDHGT	2	10.67	12.19	10.67	10.97	10.97	10.97
SO BUILDHGT	2	10.97	10.97	10.67	10.67	10.67	10.67
BUILDHGT	2	12.19	12.19	12.19	12.19	12.19	12.19
BUILDHGT	3	12.19	12.19	10.67	10.67	10.67	10.67
SO BUILDHGT	3	10.67	10.67	10.67	10.67	10.67	10.67
BUILDHGT	3	10.67	10.67	10.67	10.67	10.67	10.67
BUILDHGT	3	10.67	10.67	10.67	10.67	10.97	10.97
SO BUILDHGT	3	10.97	10.97	10.67	10.67	10.67	10.67
SO BUILDHGT	3	12.19	12.19	12.19	12.19	12.19	12.19

NOTE: Direction-Specific Building Widths Used for Non-SS Source 1

SO BUILDWID	1	84.68	91.23	95.01	95.96	95.84	93.53
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SO BUILDWID	1	.00	.00	.00	.00	.00	.00
SO BUILDWID	1	.00	.00	93.84	90.70	83.88	.00
SO BUILDWID	1	.00	91.23	95.01	95.96	95.84	93.53
SO BUILDWID	1	.00	.00	.00	.00	.00	.00
SO BUILDWID	1	.00	.00	93.84	90.70	83.88	75.55
SO BUILDWID	2	84.68	88.29	196.53	209.06	215.24	215.89
SO BUILDWID	2	214.49	206.95	193.13	194.58	194.74	192.50
SO BUILDWID	2	186.24	176.60	161.59	148.74	138.57	125.52
SO BUILDWID	2	154.11	88.29	196.53	24.84	24.73	23.71
SO BUILDWID	2	21.98	19.58	193.13	194.58	194.74	192.50
SO BUILDWID	2	125.05	122.42	116.07	106.20	93.09	77.16
SO BUILDWID	3	84.68	87.62	196.53	209.06	215.24	215.89
SO BUILDWID	3	214.49	206.95	193.13	194.58	194.74	192.50
SO BUILDWID	3	186.24	176.60	161.59	148.74	138.57	125.52
SO BUILDWID	3	154.11	178.03	196.53	209.06	24.58	23.71
SO BUILDWID	3	21.98	19.58	193.13	194.58	194.74	192.50
SO BUILDWID	3	124.83	122.42	116.07	106.20	93.09	77.16

SO EMISUNIT .100000E+07 (GRAMS/SEC) (MICROGRAMS/CUBIC-METER)

SO SRCGROUP ALL

SO FINISHED

SO STARTING

SO GRIDPOLR POL1 STA

RE GRIDPOLR POL1 ORIG 106.68 110.6424

RE GRIDPOLR POL1 DIST 150. 200. 250. 300. 350. 400. 450. 500. 550.

RE GRIDPOLR POL1 DIST 600. 650. 700. 750. 800. 850. 900. 950. 1000.

RE GRIDPOLR POL1 GDIR 36 10. 10.

RE GRIDPOLR POL1 END

SO DISCCART .00 .00

SO DISCCART 15.24 .00

RE DISCCART 30.48 .00

RE DISCCART 45.72 .00

RE DISCCART 60.96 .00

RE DISCCART 76.20 .00

RE DISCCART 91.44 .00

RE DISCCART 106.68 .00

RE DISCCART 121.92 .00

RE DISCCART 137.16 .00

RE DISCCART 152.40 .00

RE DISCCART 167.64 .00

RE DISCCART 182.88 .00

RE DISCCART 198.12 .00

RE DISCCART 213.36 .00

RE DISCCART 213.36 15.24

RE DISCCART 213.36 30.48

RE DISCCART 213.36 45.72

RE DISCCART 213.36 60.96

RE DISCCART 213.36 76.20

RE DISCCART 213.36 91.44

RE DISCCART 213.36 106.68

RE DISCCART 213.36 121.92

RE DISCCART 213.36 137.16

RE DISCCART 213.36 152.40

RE DISCCART 213.36 167.64

RE DISCCART 213.36 182.88

RE DISCCART 213.36 198.12

RE DISCCART 213.36 213.36

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RE DISCCART 213.36 221.29
RE DISCCART 198.12 221.29
RE DISCCART 182.88 221.29
RE DISCCART 167.64 221.29
RE DISCCART 152.40 221.29
RE DISCCART 137.16 221.29
RE DISCCART 121.92 221.29
RE DISCCART 106.68 221.29
RE DISCCART 91.44 221.29
RE DISCCART 76.20 221.29
RE DISCCART 60.96 221.29
RE DISCCART 45.72 221.29
RE DISCCART 30.48 221.29
RE DISCCART 15.24 221.29
RE DISCCART .00 221.29
RE DISCCART .00 213.36
RE DISCCART .00 198.12
RE DISCCART .00 182.88
RE DISCCART .00 167.64
RE DISCCART .00 152.40
RE DISCCART .00 137.16
RE DISCCART .00 121.92
RE DISCCART .00 106.68
RE DISCCART .00 91.44
RE DISCCART .00 76.20
RE DISCCART .00 60.96
RE DISCCART .00 45.72
RE DISCCART .00 30.48
RE DISCCART .00 15.24
RE FINISHED
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```
M STARTING
ME INPUTFIL C:\models\iscst2\ORLTMP86.BIN UNIFORM
ME ANERHGT 10.000 METERS
M SURFDATA 12815 1986 SURFNAME
M UAIIDATA 12842 1986 UAIRNAME
ME WINDCATS 1.54 3.09 5.14 8.23 10.80
M FINISHED
```

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OU STARTING
OU RECTABLE 24 FIRST SECOND
OU MAXTABLE 24 50
OU FINISHED
```

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*****
*** SETUP Finishes Successfully ***
*****
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\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* MODEL SETUP OPTIONS SUMMARY \*\*\*

Model Is Setup For Calculation of Average CONCentration Values.

\*\*Model Uses RURAL Dispersion.

Model Uses Regulatory DEFAULT Options:

- 1. Final Plume Rise.
- 2. Stack-tip Downwash.
- 3. Buoyancy-induced Dispersion.
- 4. Use Calms Processing Routine.
- 5. Not Use Missing Data Processing Routine.
- 6. Default Wind Profile Exponents.
- 7. Default Vertical Potential Temperature Gradients.
- 8. "Upper Bound" Values for Supersquat Buildings.
- 9. No Exponential Decay for RURAL Mode

\*\*Model Assumes Receptors on FLAT Terrain.

Model Assumes No FLAGPOLE Receptor Heights.

\*\*Model Calculates 1 Short Term Average(s) of: 24-HR

This Run Includes: 3 Source(s); 1 Source Group(s); and 706 Receptor(s)

The Model Assumes A Pollutant Type of: OTHER

\*\*Model Set To Continue RUNNING After the Setup Testing.

Output Options Selected:

Model Outputs Tables of Highest Short Term Values by Receptor (RECTABLE Keyword)

Model Outputs Tables of Overall Maximum Short Term Values (MAXTABLE Keyword)

NOTE: The Following Flags May Appear Following CONC Values: c for Calm Hours  
 m for Missing Hours  
 b for Both Calm and Missing Hours

\*\*Misc. Inputs: Anem. Hgt. (m) = 10.00 ; Decay Coef. = 0.0000 ; Rot. Angle = 0.0  
 Emission Units = (GRAMS/SEC) ; Emission Rate Unit Factor = 0.10000E+07  
 Output Units = (MICROGRAMS/CUBIC-METER)

\*\*Input Runstream File: D:\MODEL DAT\ISCST2\FOAMEX\FMXTD124.NEW ; \*\*Output Print File: D:\MODEL DAT\ISCST2\FOAMEX\FMXTD124.LST

\*\*\* ISCST2 - VERSION 92062 \*\*\*

\*\*\* Foamex TDI Sources: Foam Line Stack & Rebond Process Exhaust

\*\*\*

01/21/93

\*\*\* 24-hour Average Emission Rates

\*\*\*

10:56:07

PAGE 2

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* POINT SOURCE DATA \*\*\*

SOURCE ID	NUMBER	EMISSION RATE			BASE ELEV.	STACK HEIGHT	STACK TEMP.	STACK EXIT VEL.	STACK DIAMETER	BUILDING EXISTS	EMISSION RATE SCALAR	VARY BY
	PART. CATS.	(USER UNITS)	X (METERS)	Y (METERS)	(METERS)	(METERS)	(DEG.K)	(M/SEC)	(METERS)			
1	0	0.58274E-02	175.9	119.8	0.0	38.10	299.82	24.38	0.70	YES		
2	0	0.14490E-03	141.4	162.8	0.0	12.50	299.82	1.03	0.76	YES		
3	0	0.14490E-03	141.4	166.4	0.0	12.50	299.82	1.03	0.76	YES		

\*\*\* ISCST2 - VERSION 92062 \*\*\*

\*\*\* Foamex TDI Sources: Foam Line Stack & Rebond Process Exhaust

\*\*\*

01/21/93

\*\*\* 24-hour Average Emission Rates

\*\*\*

10:56:07

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\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* SOURCE IDs DEFINING SOURCE GROUPS \*\*\*

GROUP ID

SOURCE IDs

ALL 1 , 2 , 3 ,



\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DEFAULT

\*\*\* DIRECTION SPECIFIC BUILDING DIMENSIONS \*\*\*

SOURCE ID: 1

IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK
1	15.2,	84.7,	0	2	15.2,	91.2,	0	3	15.2,	95.0,	0	4	15.2,	96.0,	0	5	15.2,	95.8,	0	6	15.2,	93.5,	0
7	0.0,	0.0,	0	8	0.0,	0.0,	0	9	0.0,	0.0,	0	10	0.0,	0.0,	0	11	0.0,	0.0,	0	12	0.0,	0.0,	0
13	0.0,	0.0,	0	14	0.0,	0.0,	0	15	15.2,	93.8,	0	16	15.2,	90.7,	0	17	15.2,	83.9,	0	18	0.0,	0.0,	0
19	0.0,	0.0,	0	20	15.2,	91.2,	0	21	15.2,	95.0,	0	22	15.2,	96.0,	0	23	15.2,	95.8,	0	24	15.2,	93.5,	0
25	0.0,	0.0,	0	26	0.0,	0.0,	0	27	0.0,	0.0,	0	28	0.0,	0.0,	0	29	0.0,	0.0,	0	30	0.0,	0.0,	0
31	0.0,	0.0,	0	32	0.0,	0.0,	0	33	15.2,	93.8,	0	34	15.2,	90.7,	0	35	15.2,	83.9,	0	36	15.2,	75.6,	0

SOURCE ID: 2

IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK
1	12.2,	84.7,	0	2	12.2,	88.3,	0	3	10.7,	196.5,	0	4	10.7,	209.1,	0	5	10.7,	215.2,	0	6	10.7,	215.9,	0
7	10.7,	214.5,	0	8	10.7,	206.9,	0	9	10.7,	193.1,	0	10	10.7,	194.6,	0	11	10.7,	194.7,	0	12	10.7,	192.5,	0
13	10.7,	186.2,	0	14	10.7,	176.6,	0	15	10.7,	161.6,	0	16	10.7,	148.7,	0	17	10.7,	138.6,	0	18	10.7,	125.5,	0
19	10.7,	154.1,	0	20	12.2,	88.3,	0	21	10.7,	196.5,	0	22	11.0,	24.8,	0	23	11.0,	24.7,	0	24	11.0,	23.7,	0
25	11.0,	22.0,	0	26	11.0,	19.6,	0	27	10.7,	193.1,	0	28	10.7,	194.6,	0	29	10.7,	194.7,	0	30	10.7,	192.5,	0
31	12.2,	125.1,	0	32	12.2,	122.4,	0	33	12.2,	116.1,	0	34	12.2,	106.2,	0	35	12.2,	93.1,	0	36	12.2,	77.2,	0

SOURCE ID: 3

IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK
1	12.2,	84.7,	0	2	12.2,	87.6,	0	3	10.7,	196.5,	0	4	10.7,	209.1,	0	5	10.7,	215.2,	0	6	10.7,	215.9,	0
7	10.7,	214.5,	0	8	10.7,	206.9,	0	9	10.7,	193.1,	0	10	10.7,	194.6,	0	11	10.7,	194.7,	0	12	10.7,	192.5,	0
13	10.7,	186.2,	0	14	10.7,	176.6,	0	15	10.7,	161.6,	0	16	10.7,	148.7,	0	17	10.7,	138.6,	0	18	10.7,	125.5,	0
19	10.7,	154.1,	0	20	10.7,	178.0,	0	21	10.7,	196.5,	0	22	10.7,	209.1,	0	23	11.0,	24.6,	0	24	11.0,	23.7,	0
25	11.0,	22.0,	0	26	11.0,	19.6,	0	27	10.7,	193.1,	0	28	10.7,	194.6,	0	29	10.7,	194.7,	0	30	10.7,	192.5,	0
31	12.2,	124.8,	0	32	12.2,	122.4,	0	33	12.2,	116.1,	0	34	12.2,	106.2,	0	35	12.2,	93.1,	0	36	12.2,	77.2,	0

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* GRIDDED RECEPTOR NETWORK SUMMARY \*\*\*

\*\*\* NETWORK ID: POL1 ; NETWORK TYPE: GRIDPOLR \*\*\*

\*\*\* ORIGIN FOR POLAR NETWORK \*\*\*

X-ORIG = 106.68 ; Y-ORIG = 110.64 (METERS)

\*\*\* DISTANCE RANGES OF NETWORK \*\*\*  
(METERS)

150.0,	200.0,	250.0,	300.0,	350.0,	400.0,	450.0,	500.0,	550.0,	600.0,
650.0,	700.0,	750.0,	800.0,	850.0,	900.0,	950.0,	1000.0,		

\*\*\* DIRECTION RADIALS OF NETWORK \*\*\*  
(DEGREES)

10.0,	20.0,	30.0,	40.0,	50.0,	60.0,	70.0,	80.0,	90.0,	100.0,
110.0,	120.0,	130.0,	140.0,	150.0,	160.0,	170.0,	180.0,	190.0,	200.0,
210.0,	220.0,	230.0,	240.0,	250.0,	260.0,	270.0,	280.0,	290.0,	300.0,
310.0,	320.0,	330.0,	340.0,	350.0,	360.0,				

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* DISCRETE CARTESIAN RECEPTORS \*\*\*

(X-COORD, Y-COORD, ZELEV, ZFLAG)

(METERS)

( 0.0, 0.0, 0.0, 0.0);	( 15.2, 0.0, 0.0, 0.0);
( 30.5, 0.0, 0.0, 0.0);	( 45.7, 0.0, 0.0, 0.0);
( 61.0, 0.0, 0.0, 0.0);	( 76.2, 0.0, 0.0, 0.0);
( 91.4, 0.0, 0.0, 0.0);	( 106.7, 0.0, 0.0, 0.0);
( 121.9, 0.0, 0.0, 0.0);	( 137.2, 0.0, 0.0, 0.0);
( 152.4, 0.0, 0.0, 0.0);	( 167.6, 0.0, 0.0, 0.0);
( 182.9, 0.0, 0.0, 0.0);	( 198.1, 0.0, 0.0, 0.0);
( 213.4, 0.0, 0.0, 0.0);	( 213.4, 15.2, 0.0, 0.0);
( 213.4, 30.5, 0.0, 0.0);	( 213.4, 45.7, 0.0, 0.0);
( 213.4, 61.0, 0.0, 0.0);	( 213.4, 76.2, 0.0, 0.0);
( 213.4, 91.4, 0.0, 0.0);	( 213.4, 106.7, 0.0, 0.0);
( 213.4, 121.9, 0.0, 0.0);	( 213.4, 137.2, 0.0, 0.0);
( 213.4, 152.4, 0.0, 0.0);	( 213.4, 167.6, 0.0, 0.0);
( 213.4, 182.9, 0.0, 0.0);	( 213.4, 198.1, 0.0, 0.0);
( 213.4, 213.4, 0.0, 0.0);	( 213.4, 221.3, 0.0, 0.0);
( 198.1, 221.3, 0.0, 0.0);	( 182.9, 221.3, 0.0, 0.0);
( 167.6, 221.3, 0.0, 0.0);	( 152.4, 221.3, 0.0, 0.0);
( 137.2, 221.3, 0.0, 0.0);	( 121.9, 221.3, 0.0, 0.0);
( 106.7, 221.3, 0.0, 0.0);	( 91.4, 221.3, 0.0, 0.0);
( 76.2, 221.3, 0.0, 0.0);	( 61.0, 221.3, 0.0, 0.0);
( 45.7, 221.3, 0.0, 0.0);	( 30.5, 221.3, 0.0, 0.0);
( 15.2, 221.3, 0.0, 0.0);	( 0.0, 221.3, 0.0, 0.0);
( 0.0, 213.4, 0.0, 0.0);	( 0.0, 198.1, 0.0, 0.0);
( 0.0, 182.9, 0.0, 0.0);	( 0.0, 167.6, 0.0, 0.0);
( 0.0, 152.4, 0.0, 0.0);	( 0.0, 137.2, 0.0, 0.0);
( 0.0, 121.9, 0.0, 0.0);	( 0.0, 106.7, 0.0, 0.0);
( 0.0, 91.4, 0.0, 0.0);	( 0.0, 76.2, 0.0, 0.0);
( 0.0, 61.0, 0.0, 0.0);	( 0.0, 45.7, 0.0, 0.0);
( 0.0, 30.5, 0.0, 0.0);	( 0.0, 15.2, 0.0, 0.0);

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* METEOROLOGICAL DAYS SELECTED FOR PROCESSING \*\*\*  
 (1=YES; 0=NO)

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1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
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1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
    
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NOTE: METEOROLOGICAL DATA ACTUALLY PROCESSED WILL ALSO DEPEND ON WHAT IS INCLUDED IN THE DATA FILE.

\*\*\* UPPER BOUND OF FIRST THROUGH FIFTH WIND SPEED CATEGORIES \*\*\*  
 (METERS/SEC)

1.54, 3.09, 5.14, 8.23, 10.80,

\*\*\* WIND PROFILE EXPONENTS \*\*\*

STABILITY CATEGORY	WIND SPEED CATEGORY					
	1	2	3	4	5	6
A	.70000E-01	.70000E-01	.70000E-01	.70000E-01	.70000E-01	.70000E-01
B	.70000E-01	.70000E-01	.70000E-01	.70000E-01	.70000E-01	.70000E-01
C	.10000E+00	.10000E+00	.10000E+00	.10000E+00	.10000E+00	.10000E+00
D	.15000E+00	.15000E+00	.15000E+00	.15000E+00	.15000E+00	.15000E+00
E	.35000E+00	.35000E+00	.35000E+00	.35000E+00	.35000E+00	.35000E+00
F	.55000E+00	.55000E+00	.55000E+00	.55000E+00	.55000E+00	.55000E+00

\*\*\* VERTICAL POTENTIAL TEMPERATURE GRADIENTS \*\*\*  
 (DEGREES KELVIN PER METER)

STABILITY CATEGORY	WIND SPEED CATEGORY					
	1	2	3	4	5	6
A	.00000E+00	.00000E+00	.00000E+00	.00000E+00	.00000E+00	.00000E+00
B	.00000E+00	.00000E+00	.00000E+00	.00000E+00	.00000E+00	.00000E+00
C	.00000E+00	.00000E+00	.00000E+00	.00000E+00	.00000E+00	.00000E+00
D	.00000E+00	.00000E+00	.00000E+00	.00000E+00	.00000E+00	.00000E+00
E	.20000E-01	.20000E-01	.20000E-01	.20000E-01	.20000E-01	.20000E-01
F	.35000E-01	.35000E-01	.35000E-01	.35000E-01	.35000E-01	.35000E-01

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* THE FIRST 24 HOURS OF METEOROLOGICAL DATA \*\*\*

FILE: C:\models\iscst2\ORLTMP86.BIN

FORMAT: UNIFORM

SURFACE STATION NO.: 12815

UPPER AIR STATION NO.: 12842

NAME: SURFNAME

NAME: UAIRNAME

YEAR: 1986

YEAR: 1986

YEAR	MONTH	DAY	HOUR	FLOW	SPEED	TEMP	STAB	MIXING HEIGHT (M)	
				VECTOR	(M/S)	(K)	CLASS	RURAL	URBAN
86	1	1	1	1.0	3.60	289.3	4	639.0	639.0
86	1	1	2	168.0	5.14	288.7	4	639.0	639.0
86	1	1	3	124.0	3.09	288.2	4	639.0	639.0
86	1	1	4	353.0	2.57	288.2	4	639.0	639.0
86	1	1	5	333.0	2.57	288.7	4	639.0	639.0
86	1	1	6	332.0	2.57	288.7	4	639.0	639.0
86	1	1	7	335.0	3.09	288.7	4	639.0	639.0
86	1	1	8	3.0	3.60	289.3	4	639.0	639.0
86	1	1	9	347.0	3.60	289.8	4	639.0	639.0
86	1	1	10	1.0	5.14	292.0	4	639.0	639.0
86	1	1	11	14.0	4.63	292.6	4	639.0	639.0
86	1	1	12	16.0	4.12	294.3	4	639.0	639.0
86	1	1	13	73.0	3.09	295.4	4	639.0	639.0
86	1	1	14	49.0	3.60	297.0	4	639.0	639.0
86	1	1	15	142.0	2.06	296.5	4	639.0	639.0
86	1	1	16	144.0	2.06	295.9	4	639.0	639.0
86	1	1	17	261.0	2.06	295.4	4	639.0	639.0
86	1	1	18	257.0	2.06	292.6	4	644.0	644.0
86	1	1	19	274.0	3.60	291.5	4	655.0	655.0
86	1	1	20	227.0	3.09	290.9	4	666.0	666.0
86	1	1	21	230.0	3.09	290.9	4	678.0	678.0
86	1	1	22	252.0	2.57	290.4	5	689.0	477.0
86	1	1	23	290.0	2.06	290.4	4	700.0	700.0
86	1	1	24	290.0	1.00	290.4	4	712.0	712.0

\*\*\* NOTES: STABILITY CLASS 1=A, 2=B, 3=C, 4=D, 5=E AND 6=F.  
 FLOW VECTOR IS DIRECTION TOWARD WHICH WIND IS BLOWING.

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* THE 1ST HIGHEST 24-HR AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: ALL \*\*\*  
 INCLUDING SOURCE(S): 1 , 2 , 3 ,

\*\*\* NETWORK ID: POL1 ; NETWORK TYPE: GRIDPOLR \*\*\*

\*\* CONC OF OTHER IN (MICROGRAMS/CUBIC-METER) \*\*

DIRECTION (DEGREES)	DISTANCE (METERS)				
	150.00	200.00	250.00	300.00	350.00
10.0	0.04591 (86081324)	0.03682 (86071724)	0.03102 (86071724)	0.02864c(86071324)	0.02690c(86071324)
20.0	0.06087 (86072324)	0.03891 (86072324)	0.02666 (86072324)	0.02055 (86072324)	0.01782 (86072324)
30.0	0.07349c(86012924)	0.04670c(86012924)	0.03465c(86060824)	0.02897c(86060824)	0.02419c(86060824)
40.0	0.05995 (86030324)	0.03962 (86030324)	0.02664c(86021824)	0.02037c(86021824)	0.01881 (86070224)
50.0	0.05003 (86121824)	0.04339 (86040824)	0.03321c(86072524)	0.03094c(86072524)	0.02659c(86072524)
60.0	0.04383c(86100524)	0.03103c(86081824)	0.02778 (86030624)	0.02013c(86060924)	0.01867c(86072024)
70.0	0.06169c(86071924)	0.02643c(86071424)	0.02137 (86090324)	0.02393 (86040824)	0.01955c(86072024)
80.0	0.03072c(86122524)	0.02404c(86042524)	0.02692c(86071924)	0.03181c(86071924)	0.03089c(86071924)
90.0	0.02844c(86012524)	0.02629c(86122524)	0.01663c(86122524)	0.01491c(86071424)	0.01472c(86071924)
100.0	0.03678c(86012324)	0.03305c(86012324)	0.01448c(86012524)	0.01878 (86042924)	0.02038 (86042924)
110.0	0.03082c(86031124)	0.03092c(86012324)	0.01968c(86012324)	0.02050c(86012324)	0.02371c(86012324)
120.0	0.02823c(86012824)	0.02181c(86012524)	0.01885c(86031124)	0.01736 (86102624)	0.01682 (86102624)
130.0	0.02821c(86111324)	0.02167c(86012824)	0.01773c(86012824)	0.01604 (86042624)	0.01810 (86042624)
140.0	0.03117 (86101624)	0.03089c(86090824)	0.01634 (86011424)	0.01635c(86111324)	0.01450c(86111324)
150.0	0.04299 (86120424)	0.02392 (86101624)	0.02280 (86101624)	0.02234 (86101624)	0.02298 (86101624)
160.0	0.03116 (86012424)	0.02258c(86103024)	0.02695 (86120424)	0.02694 (86120424)	0.02103 (86120424)
170.0	0.03212c(86122624)	0.02572 (86122224)	0.02440 (86122124)	0.02370 (86110324)	0.02506 (86110324)
180.0	0.02488 (86060524)	0.02188c(86090224)	0.02273c(86090224)	0.02093c(86090224)	0.01826c(86090224)
190.0	0.02592 (86121424)	0.01829 (86121424)	0.01634c(86041424)	0.01492c(86041424)	0.01344 (86060524)
200.0	0.02313 (86102824)	0.01870 (86102824)	0.01610 (86121624)	0.01571 (86042424)	0.01507 (86042424)
210.0	0.02939 (86091824)	0.02457 (86091824)	0.02104 (86091824)	0.01891c(86092724)	0.01808c(86092724)
220.0	0.03815c(86090124)	0.03252c(86090124)	0.02883c(86090124)	0.02599c(86090124)	0.02355c(86090124)
230.0	0.03102 (86091924)	0.02133 (86091924)	0.01970c(86100224)	0.01853c(86100224)	0.01752c(86100224)
240.0	0.03332 (86091524)	0.03046 (86091524)	0.02794 (86091524)	0.02573 (86091524)	0.02360 (86091524)
250.0	0.03901c(86092724)	0.03342c(86092724)	0.02523c(86092724)	0.01954c(86092724)	0.01827 (86091524)
260.0	0.02663c(86060324)	0.02344c(86051324)	0.02684c(86092724)	0.02616c(86092724)	0.02305c(86092724)
270.0	0.03014c(86092724)	0.02032 (86110924)	0.02209c(86051324)	0.02330c(86051324)	0.02305c(86051324)
280.0	0.03295c(86050524)	0.03193c(86051324)	0.03376c(86051324)	0.02647 (86062324)	0.02586 (86062324)
290.0	0.03959c(86051324)	0.03155 (86112824)	0.02406 (86052724)	0.02392c(86093024)	0.02598c(86093024)
300.0	0.03651 (86052724)	0.04266c(86093024)	0.02539c(86020424)	0.02333c(86080924)	0.02272c(86080924)
310.0	0.04088c(86020424)	0.03041c(86080924)	0.03132c(86100324)	0.02796c(86100324)	0.02441c(86100324)
320.0	0.04154c(86100324)	0.02949c(86100324)	0.02415 (86112524)	0.02046 (86112524)	0.01913c(86050724)
330.0	0.03412c(86050724)	0.03538c(86050724)	0.02798c(86052924)	0.02385c(86052924)	0.01741c(86052924)
340.0	0.03728c(86050724)	0.02055c(86082924)	0.01876 (86031224)	0.01972 (86031224)	0.01848 (86031224)
350.0	0.03448 (86031324)	0.03309c(86020424)	0.02233c(86020424)	0.02413 (86100924)	0.02567 (86100924)
360.0	0.04322 (86100924)	0.03158 (86100924)	0.02096 (86081324)	0.02045 (86081324)	0.02121c(86071324)

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DEFAULT

\*\*\* THE 1ST HIGHEST 24-HR AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: ALL \*\*\*  
 INCLUDING SOURCE(S): 1 , 2 , 3 ,

\*\*\* NETWORK ID: POL1 ; NETWORK TYPE: GRIDPOLR \*\*\*

\*\* CONC OF OTHER IN (MICROGRAMS/CUBIC-METER) \*\*

RECTION (DEGREES)	DISTANCE (METERS)				
	400.00	450.00	500.00	550.00	600.00
10.0	0.02489c(86071324)	0.02285c(86071324)	0.02091c(86071324)	0.01912c(86071324)	0.01756c(86071324)
20.0	0.01689 (86072324)	0.01681 (86072324)	0.01704 (86072324)	0.01728 (86072324)	0.01741 (86072324)
30.0	0.02072 (86071024)	0.01947 (86071024)	0.01835 (86071024)	0.01737 (86071024)	0.01652 (86071024)
40.0	0.01946 (86080424)	0.01929 (86080424)	0.01860 (86070224)	0.01857 (86070224)	0.01842 (86070224)
50.0	0.02215c(86072524)	0.02009 (86072624)	0.01882 (86072624)	0.01757 (86100424)	0.01703 (86100424)
60.0	0.02095 (86100424)	0.02201 (86100424)	0.02198 (86100424)	0.02122 (86100424)	0.02000 (86100424)
70.0	0.02266c(86081824)	0.02519c(86081824)	0.02651c(86081824)	0.02680c(86081824)	0.02639c(86081824)
80.0	0.02693c(86071924)	0.02286c(86071924)	0.01964c(86071924)	0.01715c(86071924)	0.01517c(86071924)
90.0	0.01694c(86071924)	0.01812c(86071924)	0.01861c(86071924)	0.01856c(86071924)	0.01818c(86071924)
100.0	0.01749 (86042924)	0.01414 (86042924)	0.01387c(86122524)	0.01360c(86071924)	0.01338c(86071924)
110.0	0.02316c(86012324)	0.02116 (86042924)	0.02234 (86042924)	0.02263 (86042924)	0.02235 (86042924)
120.0	0.01943c(86012324)	0.02011c(86012324)	0.01934c(86012324)	0.01854c(86052224)	0.01784c(86052224)
130.0	0.01870 (86042624)	0.01830 (86042624)	0.01730 (86042624)	0.01707c(86012824)	0.01721c(86012824)
140.0	0.01312 (86042824)	0.01388 (86042824)	0.01410 (86042824)	0.01388 (86042824)	0.01338 (86042824)
150.0	0.02377 (86101624)	0.02420 (86101624)	0.02405 (86101624)	0.02336 (86101624)	0.02230 (86101624)
160.0	0.01818 (86110324)	0.01757 (86101624)	0.01869 (86101624)	0.01968 (86101624)	0.02054 (86101624)
170.0	0.02495 (86110324)	0.02403 (86110324)	0.02262 (86110324)	0.02106 (86110324)	0.01950 (86110324)
180.0	0.01731 (86110324)	0.01776 (86110324)	0.01792 (86110324)	0.01788 (86110324)	0.01770 (86110324)
190.0	0.01295 (86060524)	0.01248 (86060524)	0.01208 (86060524)	0.01172 (86060524)	0.01140 (86060524)
200.0	0.01461 (86120424)	0.01499 (86120424)	0.01484 (86120424)	0.01434 (86120424)	0.01431 (86102824)
210.0	0.01713c(86092724)	0.01601c(86092724)	0.01550c(86111324)	0.01496c(86111324)	0.01432c(86111324)
220.0	0.02138c(86090124)	0.01942c(86090124)	0.01766c(86090124)	0.01729 (86060524)	0.01707 (86060524)
230.0	0.01669c(86100224)	0.01596c(86100224)	0.01525c(86100224)	0.01454c(86100224)	0.01532 (86010924)
240.0	0.02156 (86091524)	0.01962 (86091524)	0.01782 (86091524)	0.01620 (86091524)	0.01525 (86010924)
250.0	0.01843 (86091524)	0.01815 (86091524)	0.01758 (86091524)	0.01683 (86091524)	0.01601 (86091524)
260.0	0.01990c(86092724)	0.01738c(86092724)	0.01551c(86092724)	0.01415c(86092724)	0.01315 (86121424)
270.0	0.02212c(86051324)	0.02103c(86051324)	0.01994c(86051324)	0.01891c(86051324)	0.01794c(86051324)
280.0	0.02336 (86062324)	0.02074 (86062324)	0.01855 (86062324)	0.01684 (86062324)	0.01547 (86062324)
290.0	0.02595c(86093024)	0.02406c(86093024)	0.02145c(86093024)	0.01890c(86093024)	0.01674c(86093024)
300.0	0.02243 (86040624)	0.02201 (86040624)	0.02069 (86040624)	0.01888 (86040624)	0.01840 (86030924)
310.0	0.02427c(86100324)	0.02363c(86100324)	0.02195c(86100324)	0.01980c(86100324)	0.01766c(86100324)
320.0	0.01747c(86050724)	0.01605 (86081124)	0.01563 (86081124)	0.01490 (86081124)	0.01409 (86081124)
330.0	0.01609c(86053024)	0.01509c(86082524)	0.01466c(86082524)	0.01397c(86082524)	0.01456 (86031324)
340.0	0.01795 (86031224)	0.01814 (86031224)	0.01852 (86031224)	0.01877 (86031224)	0.01880 (86031224)
350.0	0.02589 (86100924)	0.02508 (86100924)	0.02370 (86100924)	0.02209 (86100924)	0.02052 (86100924)
360.0	0.02097c(86071324)	0.02018c(86071324)	0.01919c(86071324)	0.01810c(86071324)	0.01708c(86071324)

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* THE 1ST HIGHEST 24-HR AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: ALL \*\*\*  
INCLUDING SOURCE(S): 1 , 2 , 3 ,

\*\*\* NETWORK ID: POL1 ; NETWORK TYPE: GRIDPOLR \*\*\*

\*\* CONC OF OTHER IN (MICROGRAMS/CUBIC-METER) \*\*

RECTION (DEGREES)	DISTANCE (METERS)				
	650.00	700.00	750.00	800.00	850.00
10.0	0.01628c(86071324)	0.01565 (86082024)	0.01613 (86082024)	0.01647 (86082024)	0.01680 (86082024)
20.0	0.01739 (86072324)	0.01719 (86072324)	0.01685 (86072324)	0.01640 (86072324)	0.01594 (86072324)
30.0	0.01579 (86071024)	0.01518 (86071024)	0.01474 (86071024)	0.01429 (86071024)	0.01395 (86071024)
40.0	0.01814 (86070224)	0.01774 (86070224)	0.01724 (86070224)	0.01668 (86070224)	0.01607 (86070224)
50.0	0.01637 (86100424)	0.01567 (86100424)	0.01497 (86100424)	0.01429 (86100424)	0.01363 (86100424)
60.0	0.01857 (86100424)	0.01710 (86100424)	0.01575 (86100424)	0.01442 (86100424)	0.01321 (86100424)
70.0	0.02558c(86081824)	0.02456c(86081824)	0.02347c(86081824)	0.02237c(86081824)	0.02130c(86081824)
80.0	0.01356c(86071924)	0.01221c(86071924)	0.01110c(86071924)	0.01011c(86071924)	0.00925c(86071924)
90.0	0.01766c(86071924)	0.01708c(86071924)	0.01656c(86071924)	0.01602c(86071924)	0.01553c(86071924)
100.0	0.01294c(86071924)	0.01238c(86071924)	0.01176c(86071924)	0.01112c(86071924)	0.01049c(86071924)
110.0	0.02175 (86042924)	0.02099 (86042924)	0.02015 (86042924)	0.01929 (86042924)	0.01845 (86042924)
120.0	0.01688c(86052224)	0.01591 (86022024)	0.01569 (86022024)	0.01542 (86022024)	0.01515 (86022024)
130.0	0.01703c(86012824)	0.01663c(86012824)	0.01608c(86012824)	0.01544c(86012824)	0.01478c(86012824)
140.0	0.01271 (86042824)	0.01196 (86042824)	0.01119 (86042824)	0.01054 (86032124)	0.01050 (86032124)
150.0	0.02101 (86101624)	0.01960 (86101624)	0.01816 (86101624)	0.01679 (86101624)	0.01546 (86101624)
160.0	0.02128 (86101624)	0.02181 (86101624)	0.02217 (86101624)	0.02251 (86101624)	0.02256 (86101624)
170.0	0.01945 (86012424)	0.01982 (86120524)	0.02053 (86120524)	0.02109 (86120524)	0.02119 (86120524)
180.0	0.01742 (86110324)	0.01705 (86110324)	0.01768 (86122824)	0.01850 (86122824)	0.01893 (86122824)
190.0	0.01113 (86060524)	0.01082 (86060524)	0.01074c(86122624)	0.01129c(86122624)	0.01161c(86122624)
200.0	0.01465 (86102824)	0.01494 (86102824)	0.01512 (86102824)	0.01531 (86102824)	0.01538 (86102824)
210.0	0.01361c(86111324)	0.01289c(86111324)	0.01216c(86111324)	0.01229 (86010724)	0.01245 (86010724)
220.0	0.01666 (86060524)	0.01627 (86010824)	0.01670 (86010824)	0.01695 (86010824)	0.01696 (86010824)
230.0	0.01604 (86010924)	0.01656 (86010924)	0.01697 (86010924)	0.01726 (86010924)	0.01729 (86010924)
240.0	0.01606 (86010924)	0.01667 (86010924)	0.01709 (86010924)	0.01751 (86010924)	0.01761 (86010924)
250.0	0.01519 (86091524)	0.01439 (86091524)	0.01362 (86091524)	0.01292 (86091524)	0.01227 (86091524)
260.0	0.01286c(86091024)	0.01285c(86091024)	0.01279c(86091024)	0.01286c(86091024)	0.01270c(86091024)
270.0	0.01706c(86051324)	0.01621c(86051324)	0.01540c(86051324)	0.01467c(86051324)	0.01396c(86051324)
280.0	0.01522 (86052724)	0.01481 (86052724)	0.01437 (86052724)	0.01395 (86052724)	0.01353 (86052724)
290.0	0.01580 (86062324)	0.01534 (86062324)	0.01487 (86062324)	0.01439 (86062324)	0.01395 (86062324)
300.0	0.01895 (86030924)	0.01921 (86030924)	0.01922 (86030924)	0.01904 (86030924)	0.01885 (86030924)
310.0	0.01638 (86122324)	0.01680 (86122324)	0.01703 (86122324)	0.01720 (86122324)	0.01716 (86122324)
320.0	0.01319 (86081124)	0.01232 (86081124)	0.01150 (86081124)	0.01076 (86081124)	0.01008 (86081124)
330.0	0.01546 (86031324)	0.01617 (86031324)	0.01669 (86031324)	0.01717 (86031324)	0.01733 (86031324)
340.0	0.01858 (86031224)	0.01817 (86031224)	0.01762 (86031224)	0.01699 (86031224)	0.01628 (86031224)
350.0	0.01902 (86100924)	0.01768 (86100924)	0.01650 (86100924)	0.01546 (86100924)	0.01460 (86100924)
360.0	0.01649 (86112624)	0.01602 (86112624)	0.01551 (86112624)	0.01545 (86082024)	0.01621 (86082024)



\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* THE 1ST HIGHEST 24-HR AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: ALL \*\*\*  
 INCLUDING SOURCE(S): 1 , 2 , 3 ,

\*\*\* NETWORK ID: POL1 ; NETWORK TYPE: GRIDPOLR \*\*\*

\*\* CONC OF OTHER IN (MICROGRAMS/CUBIC-METER) \*\*

RECTION (DEGREES)	DISTANCE (METERS)		
	900.00	950.00	1000.00
10.0	0.01687 (86082024)	0.01684 (86082024)	0.01672 (86082024)
20.0	0.01536 (86072324)	0.01476 (86072324)	0.01415 (86072324)
30.0	0.01363 (86071024)	0.01334 (86071024)	0.01307 (86071024)
40.0	0.01547 (86070224)	0.01482 (86070224)	0.01418 (86070224)
50.0	0.01305 (86100424)	0.01259 (86112024)	0.01247 (86122024)
60.0	0.01268c(86022624)	0.01223c(86022624)	0.01178c(86022624)
70.0	0.02037c(86081824)	0.01939c(86081824)	0.01847c(86081824)
80.0	0.00860c(86081824)	0.00870c(86020724)	0.00883c(86122524)
90.0	0.01513c(86071924)	0.01473c(86071924)	0.01437c(86071924)
100.0	0.00988c(86071924)	0.00930c(86071924)	0.00875c(86071924)
110.0	0.01763 (86042924)	0.01684 (86042924)	0.01610 (86042924)
120.0	0.01480 (86022024)	0.01444 (86022024)	0.01406 (86022024)
130.0	0.01409c(86012824)	0.01341c(86012824)	0.01281 (86102624)
140.0	0.01034 (86032124)	0.01042 (86122924)	0.01061 (86122924)
150.0	0.01420 (86101624)	0.01304 (86101624)	0.01215 (86032124)
160.0	0.02250 (86101624)	0.02234 (86101624)	0.02208 (86101624)
170.0	0.02108 (86120524)	0.02081 (86120524)	0.02040 (86120524)
180.0	0.01919 (86122824)	0.01928 (86122824)	0.01919 (86122824)
190.0	0.01186c(86122624)	0.01202c(86122624)	0.01205c(86122624)
200.0	0.01540 (86102824)	0.01537 (86102824)	0.01521 (86102824)
210.0	0.01252 (86010724)	0.01249 (86010724)	0.01227 (86010724)
220.0	0.01686 (86010824)	0.01666 (86010824)	0.01628 (86010824)
230.0	0.01722 (86010924)	0.01704 (86010924)	0.01668 (86010924)
240.0	0.01759 (86010924)	0.01743 (86010924)	0.01711 (86010924)
250.0	0.01195 (86092024)	0.01173 (86092024)	0.01144 (86092024)
260.0	0.01253c(86091024)	0.01229c(86091024)	0.01197c(86091024)
270.0	0.01329c(86051324)	0.01266c(86051324)	0.01205c(86051324)
280.0	0.01312 (86052724)	0.01271 (86052724)	0.01228 (86052724)
290.0	0.01348 (86062324)	0.01301 (86062324)	0.01252 (86062324)
300.0	0.01841 (86030924)	0.01790 (86030924)	0.01726 (86030924)
310.0	0.01694 (86122324)	0.01664 (86122324)	0.01615 (86122324)
320.0	0.00947 (86081124)	0.00892 (86081124)	0.00841 (86081124)
330.0	0.01737 (86031324)	0.01730 (86031324)	0.01708 (86031324)
340.0	0.01554 (86031224)	0.01479 (86031224)	0.01404 (86031224)
350.0	0.01379 (86100924)	0.01308 (86100924)	0.01243 (86100924)
360.0	0.01672 (86082024)	0.01713 (86082024)	0.01744 (86082024)

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* THE 1ST HIGHEST 24-HR AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: ALL \*\*\*  
 INCLUDING SOURCE(S): 1 , 2 , 3 ,

\*\*\* DISCRETE CARTESIAN RECEPTOR POINTS \*\*\*

\*\* CONC OF OTHER IN (MICROGRAMS/CUBIC-METER) \*\*

X-COORD (M)	Y-COORD (M)	CONC (YYMMDDHH)	X-COORD (M)	Y-COORD (M)	CONC (YYMMDDHH)
0.00	0.00	0.03610 (86091924)	15.24	0.00	0.03959c (86090124)
30.48	0.00	0.02851c (86090124)	45.72	0.00	0.03711 (86091824)
60.96	0.00	0.02797 (86121624)	76.20	0.00	0.02887 (86102824)
91.44	0.00	0.03132 (86121424)	106.68	0.00	0.03219 (86060524)
121.92	0.00	0.04024c (86090224)	137.16	0.00	0.03926c (86122624)
152.40	0.00	0.03791 (86012424)	167.64	0.00	0.03625 (86120424)
182.88	0.00	0.03683 (86032424)	198.12	0.00	0.03384 (86101624)
213.36	0.00	0.03985c (86090824)	213.36	15.24	0.03298c (86090824)
213.36	30.48	0.03203c (86111324)	213.36	45.72	0.03549c (86111324)
213.36	60.96	0.03934c (86012824)	213.36	76.20	0.04058c (86012524)
213.36	91.44	0.04134c (86031124)	213.36	106.68	0.05893c (86012324)
213.36	121.92	0.07088c (86012324)	213.36	137.16	0.05953 (86042924)
213.36	152.40	0.03582 (86012724)	213.36	167.64	0.07934c (86071924)
213.36	182.88	0.05142c (86100524)	213.36	198.12	0.04799 (86030624)
213.36	213.36	0.06052c (86072524)	213.36	221.29	0.04996c (86072524)
198.12	221.29	0.06355 (86030324)	182.88	221.29	0.04340 (86080424)
167.64	221.29	0.06227c (86012924)	152.40	221.29	0.08421 (86072324)
137.16	221.29	0.06731 (86082024)	121.92	221.29	0.06723 (86100924)
106.68	221.29	0.05521 (86031224)	91.44	221.29	0.04201c (86052924)
76.20	221.29	0.06746c (86050724)	60.96	221.29	0.04846c (86050724)
45.72	221.29	0.04364c (86100324)	30.48	221.29	0.04755c (86100324)
15.24	221.29	0.03981c (86100324)	0.00	221.29	0.03648c (86080924)
0.00	213.36	0.03930c (86080924)	0.00	198.12	0.05046c (86093024)
0.00	182.88	0.04227 (86052724)	0.00	167.64	0.04849 (86112824)
0.00	152.40	0.04116c (86051324)	0.00	137.16	0.03204c (86050524)
0.00	121.92	0.04036c (86092724)	0.00	106.68	0.03545c (86060324)
0.00	91.44	0.03779c (86092724)	0.00	76.20	0.04001c (86092724)
0.00	60.96	0.03688 (86091524)	0.00	45.72	0.03182 (86091524)
0.00	30.48	0.02886c (86100224)	0.00	15.24	0.03828 (86091924)

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DEFAULT

\*\*\* THE 2ND HIGHEST 24-HR AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: ALL \*\*\*  
 INCLUDING SOURCE(S): 1 , 2 , 3 ,

\*\*\* NETWORK ID: POL1 ; NETWORK TYPE: GRIDPOLR \*\*\*

\*\* CONC OF OTHER IN (MICROGRAMS/CUBIC-METER) \*\*

RECTION (DEGREES)	150.00	200.00	250.00	300.00	350.00
10.0	0.04366 (86082024)	0.03297c(86071324)	0.03026c(86071324)	0.02592c(86041224)	0.02154c(86041224)
20.0	0.04814c(86081824)	0.03265c(86081824)	0.02439c(86090624)	0.01983c(86090624)	0.01644c(86090624)
30.0	0.05515c(86060824)	0.04226c(86060824)	0.03333c(86012924)	0.02624c(86012924)	0.02221 (86071024)
40.0	0.04342c(86021824)	0.03597c(86021824)	0.02587 (86030324)	0.02031 (86100624)	0.01866 (86080424)
50.0	0.04268 (86042824)	0.03651 (86030424)	0.03012 (86040824)	0.02110 (86071024)	0.02059 (86071024)
60.0	0.04019 (86040824)	0.02732 (86030624)	0.02068c(86081824)	0.01890 (86030624)	0.01838 (86100424)
70.0	0.04259c(86071424)	0.02517 (86090324)	0.01850 (86040824)	0.01686c(86100524)	0.01893 (86040824)
80.0	0.02668c(86071424)	0.02267 (86012024)	0.02265 (86012024)	0.02072c(86071424)	0.01689c(86101124)
90.0	0.02690c(86042524)	0.02351 (86011324)	0.01574c(86071424)	0.01310c(86060224)	0.01252 (86100624)
100.0	0.03089 (86102624)	0.03104c(86060624)	0.01439c(86101024)	0.01595 (86082424)	0.01608 (86011324)
110.0	0.02551 (86102624)	0.02660 (86102624)	0.01722c(86060624)	0.01948c(86060624)	0.02153c(86060624)
120.0	0.02813c(86090424)	0.01803 (86031724)	0.01529 (86102624)	0.01320c(86090224)	0.01601c(86012324)
130.0	0.02348 (86011424)	0.01915 (86021424)	0.01746c(86090424)	0.01589 (86042824)	0.01604 (86042824)
140.0	0.03090 (86032824)	0.01998 (86062624)	0.01518c(86111324)	0.01227 (86050324)	0.01304 (86050324)
150.0	0.03218 (86101724)	0.02278 (86032424)	0.02223 (86032824)	0.01986 (86032824)	0.01522 (86032824)
160.0	0.02808 (86122124)	0.01874 (86021224)	0.01819 (86110324)	0.01964 (86110324)	0.01962 (86110324)
170.0	0.02928 (86110224)	0.02559 (86122124)	0.02050 (86110324)	0.02163 (86122124)	0.01923 (86012424)
180.0	0.02187c(86011624)	0.02139c(86011624)	0.01824c(86032724)	0.01620c(86032724)	0.01657 (86110324)
190.0	0.02295 (86091724)	0.01614 (86111024)	0.01383c(86092224)	0.01377 (86060524)	0.01314 (86102124)
200.0	0.02194 (86121624)	0.01773 (86121624)	0.01584 (86102824)	0.01533 (86121624)	0.01487c(86111324)
210.0	0.02861 (86121624)	0.02339 (86121624)	0.02037 (86121624)	0.01858 (86121624)	0.01738 (86121624)
220.0	0.03237 (86103124)	0.02556 (86103124)	0.02075 (86103124)	0.01778 (86091924)	0.01619 (86091924)
230.0	0.02332c(86090124)	0.02069c(86100224)	0.01723 (86092624)	0.01636c(86082324)	0.01568c(86082324)
240.0	0.02723c(86051724)	0.02218 (86112224)	0.02105 (86112224)	0.01982 (86112224)	0.01849 (86112224)
250.0	0.02793 (86102924)	0.01861 (86102924)	0.01739 (86062624)	0.01763 (86091524)	0.01696 (86062624)
260.0	0.02338c(86082224)	0.02237c(86092724)	0.02052c(86102424)	0.01787c(86102424)	0.01508 (86062624)
270.0	0.02646c(86060324)	0.01841c(86051324)	0.01851c(86050524)	0.02004c(86082624)	0.02056c(86082624)
280.0	0.02566c(86082624)	0.02402c(86082624)	0.02269 (86062324)	0.02636c(86051324)	0.02011c(86092924)
290.0	0.03429 (86062724)	0.02729 (86052724)	0.02345c(86100824)	0.02037c(86100824)	0.01979 (86040624)
300.0	0.03216c(86100824)	0.02761 (86040624)	0.02395c(86093024)	0.02141 (86081024)	0.02191 (86040624)
310.0	0.03511c(86082624)	0.02854 (86040624)	0.02695c(86051824)	0.02393c(86080924)	0.02137c(86093024)
320.0	0.03822c(86051824)	0.02614c(86093024)	0.02152c(86093024)	0.01983c(86050724)	0.01752 (86112524)
330.0	0.03208 (86112524)	0.02372c(86052924)	0.02091c(86050724)	0.01723c(86053024)	0.01726c(86053024)
340.0	0.03247c(86052924)	0.02048c(86052924)	0.01753c(86080824)	0.01841c(86080824)	0.01775c(86080824)
350.0	0.03425 (86031224)	0.02796 (86121024)	0.02108 (86100924)	0.02148c(86082724)	0.02053c(86082724)
360.0	0.03959 (86121024)	0.02596 (86113024)	0.01970 (86100924)	0.02043c(86071324)	0.01896 (86081324)

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* THE 2ND HIGHEST 24-HR AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: ALL \*\*\*  
 INCLUDING SOURCE(S): 1 , 2 , 3 ,

\*\*\* NETWORK ID: POL1 ; NETWORK TYPE: GRIDPOLR \*\*\*

\*\* CONC OF OTHER IN (MICROGRAMS/CUBIC-METER) \*\*

RECTION (DEGREES)	DISTANCE (METERS)				
	400.00	450.00	500.00	550.00	600.00
10.0	0.01812c(86041224)	0.01572c(86060924)	0.01477c(86061124)	0.01441c(86061124)	0.01428 (86082024)
20.0	0.01465 (86111724)	0.01362 (86111724)	0.01343 (86081724)	0.01366 (86081724)	0.01357 (86081724)
30.0	0.02021c(86060824)	0.01710c(86060824)	0.01466c(86060824)	0.01372c(86081924)	0.01373c(86081924)
40.0	0.01852 (86070224)	0.01855 (86070224)	0.01849 (86080424)	0.01731 (86080424)	0.01595 (86080424)
50.0	0.02074 (86072624)	0.01836c(86072524)	0.01787 (86100424)	0.01735 (86072624)	0.01585 (86072624)
60.0	0.01982c(86072024)	0.02007c(86072024)	0.01963c(86072024)	0.01880c(86072024)	0.01776c(86072024)
70.0	0.02191c(86072024)	0.02226c(86072024)	0.02146c(86072024)	0.02014c(86072024)	0.01867c(86072024)
80.0	0.01648c(86101124)	0.01577c(86090724)	0.01415c(86101124)	0.01295c(86101124)	0.01190c(86022624)
90.0	0.01315c(86022624)	0.01257c(86022624)	0.01173c(86030524)	0.01154c(86041624)	0.01170c(86041624)
100.0	0.01450 (86011324)	0.01337c(86122524)	0.01350c(86071924)	0.01340c(86122524)	0.01286c(86030524)
110.0	0.02154c(86060624)	0.02097c(86012324)	0.01889c(86012324)	0.01717c(86012324)	0.01575c(86012324)
120.0	0.01668c(86052224)	0.01822c(86052224)	0.01877c(86052224)	0.01808c(86012324)	0.01682c(86012324)
130.0	0.01626 (86042824)	0.01605 (86042824)	0.01647c(86012824)	0.01594 (86042624)	0.01448 (86042624)
140.0	0.01290 (86050324)	0.01255c(86061024)	0.01250c(86061024)	0.01216c(86030524)	0.01172 (86042624)
150.0	0.01566c(86090824)	0.01554c(86090824)	0.01429c(86090824)	0.01269c(86090824)	0.01149 (86032124)
160.0	0.01634 (86101624)	0.01617 (86110324)	0.01428 (86032324)	0.01367 (86032324)	0.01295 (86032324)
170.0	0.01871 (86012424)	0.01850 (86012424)	0.01858 (86012424)	0.01885 (86012424)	0.01916 (86012424)
180.0	0.01569c(86122624)	0.01582c(86122624)	0.01595c(86122624)	0.01601c(86122624)	0.01598c(86122624)
190.0	0.01295 (86102124)	0.01247 (86102124)	0.01186 (86102124)	0.01121 (86102124)	0.01058 (86102124)
200.0	0.01442c(86111324)	0.01374 (86121624)	0.01364 (86102824)	0.01397 (86102824)	0.01365 (86120424)
210.0	0.01644 (86121624)	0.01589c(86111324)	0.01483c(86092724)	0.01392 (86121624)	0.01316 (86121624)
220.0	0.01609 (86060524)	0.01690 (86060524)	0.01726 (86060524)	0.01611c(86090124)	0.01486 (86010824)
230.0	0.01483c(86082324)	0.01415 (86033024)	0.01419 (86102224)	0.01443 (86010924)	0.01452 (86102224)
240.0	0.01716 (86112224)	0.01622c(86092724)	0.01589c(86092724)	0.01539c(86092724)	0.01488c(86092724)
250.0	0.01593 (86062624)	0.01472 (86062624)	0.01349 (86062624)	0.01270c(86082224)	0.01239c(86082224)
260.0	0.01452 (86062624)	0.01415 (86121424)	0.01392 (86121424)	0.01357 (86121424)	0.01312c(86092724)
270.0	0.01911c(86082624)	0.01729c(86082624)	0.01639 (86112324)	0.01606 (86112324)	0.01547 (86112324)
280.0	0.01968 (86112824)	0.01794 (86112824)	0.01587 (86112824)	0.01557 (86052724)	0.01542 (86052724)
290.0	0.01910 (86040624)	0.01728 (86062324)	0.01702 (86062324)	0.01665 (86062324)	0.01624 (86062324)
300.0	0.02033c(86080924)	0.01759c(86080924)	0.01630 (86052624)	0.01751 (86030924)	0.01695 (86040624)
310.0	0.02148c(86093024)	0.02079c(86093024)	0.01919c(86093024)	0.01708c(86093024)	0.01576 (86122324)
320.0	0.01610 (86112524)	0.01542c(86050724)	0.01404 (86112524)	0.01302 (86112524)	0.01201 (86112524)
330.0	0.01518c(86082524)	0.01438c(86053024)	0.01308 (86101324)	0.01348 (86031324)	0.01315c(86082524)
340.0	0.01671c(86020424)	0.01728c(86020424)	0.01701c(86020424)	0.01624c(86020424)	0.01523c(86020424)
350.0	0.01855c(86082724)	0.01662 (86031224)	0.01558 (86031224)	0.01434 (86031224)	0.01382 (86082124)
360.0	0.01729 (86112624)	0.01748 (86112624)	0.01744 (86112624)	0.01723 (86112624)	0.01690 (86112624)

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* THE 2ND HIGHEST 24-HR AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: ALL INCLUDING SOURCE(S): 1 , 2 , 3 ,

\*\*\* NETWORK ID: POL1 ; NETWORK TYPE: GRIDPOLR \*\*\*

\*\* CONC OF OTHER IN (MICROGRAMS/CUBIC-METER) \*\*

DIRECTION (DEGREES)	DISTANCE (METERS)				
	650.00	700.00	750.00	800.00	850.00
10.0	0.01502 (86082024)	0.01512c(86071324)	0.01413c(86071324)	0.01370 (86121224)	0.01377 (86121224)
20.0	0.01326 (86081724)	0.01279 (86081724)	0.01223 (86081724)	0.01198 (86011024)	0.01239 (86011024)
30.0	0.01353c(86081924)	0.01316c(86081924)	0.01270c(86081924)	0.01215c(86081924)	0.01157c(86081924)
40.0	0.01459 (86080424)	0.01329 (86080424)	0.01213 (86080424)	0.01106 (86080424)	0.01129 (86021024)
50.0	0.01446 (86072624)	0.01321 (86072624)	0.01250 (86112024)	0.01264 (86112024)	0.01268 (86112024)
60.0	0.01667c(86072024)	0.01560c(86072024)	0.01460c(86072024)	0.01368c(86072024)	0.01309c(86022624)
70.0	0.01726c(86072024)	0.01599c(86072024)	0.01494c(86072024)	0.01397c(86072024)	0.01314c(86072024)
80.0	0.01118c(86022624)	0.01041c(86022624)	0.00966c(86022624)	0.00902c(86081824)	0.00880c(86081824)
90.0	0.01173c(86041624)	0.01165c(86041624)	0.01171 (86012024)	0.01170 (86012024)	0.01157 (86012024)
100.0	0.01224c(86030524)	0.01157c(86030524)	0.01086c(86030524)	0.01016c(86030524)	0.00950c(86030524)
110.0	0.01452c(86012324)	0.01347c(86012324)	0.01248c(86012324)	0.01157c(86012324)	0.01076c(86012324)
120.0	0.01595 (86022024)	0.01582c(86052224)	0.01472c(86052224)	0.01366c(86052224)	0.01308c(86012324)
130.0	0.01306 (86042624)	0.01175 (86042624)	0.01139c(86121724)	0.01126 (86102624)	0.01180 (86102624)
140.0	0.01144 (86042624)	0.01113 (86042624)	0.01079 (86042624)	0.01043 (86042624)	0.01011 (86042624)
150.0	0.01197 (86032124)	0.01233 (86032124)	0.01256 (86032124)	0.01274 (86032124)	0.01273 (86032124)
160.0	0.01266 (86011124)	0.01359 (86011124)	0.01440 (86011124)	0.01517 (86011124)	0.01565 (86011124)
170.0	0.01878 (86120524)	0.01956 (86012424)	0.01952 (86012424)	0.01946 (86012424)	0.01912 (86012424)
180.0	0.01595c(86122624)	0.01680 (86122824)	0.01662 (86110324)	0.01620 (86110324)	0.01575 (86120524)
190.0	0.01001 (86102124)	0.01022c(86122624)	0.01051 (86060524)	0.01025 (86060524)	0.00995 (86060524)
200.0	0.01314 (86121624)	0.01311 (86121624)	0.01310 (86121624)	0.01306 (86121624)	0.01295 (86121624)
210.0	0.01247 (86121624)	0.01198 (86101924)	0.01195 (86101924)	0.01189 (86101924)	0.01168 (86101924)
220.0	0.01568 (86010824)	0.01613 (86060524)	0.01553 (86060524)	0.01491 (86060524)	0.01423 (86060524)
230.0	0.01461 (86102224)	0.01466 (86102224)	0.01470 (86102224)	0.01466 (86102224)	0.01454 (86102224)
240.0	0.01461 (86102924)	0.01519 (86102924)	0.01570 (86102924)	0.01633 (86102924)	0.01665 (86102924)
250.0	0.01238 (86092024)	0.01237 (86092024)	0.01231 (86092024)	0.01227 (86092024)	0.01212 (86092024)
260.0	0.01275 (86121424)	0.01228 (86121424)	0.01188 (86110924)	0.01178 (86110924)	0.01160 (86110924)
270.0	0.01475 (86112324)	0.01396 (86112324)	0.01318 (86112324)	0.01242 (86112324)	0.01217 (86051524)
280.0	0.01434 (86062324)	0.01337 (86062324)	0.01275c(86040324)	0.01245 (86040424)	0.01218 (86040424)
290.0	0.01501c(86093024)	0.01366c(86093024)	0.01279 (86052624)	0.01250 (86052624)	0.01222 (86052624)
300.0	0.01577 (86052624)	0.01531 (86052624)	0.01476 (86052624)	0.01417 (86052624)	0.01416 (86122324)
310.0	0.01573c(86100324)	0.01407c(86100324)	0.01305 (86112524)	0.01243 (86112524)	0.01179 (86112524)
320.0	0.01104 (86112524)	0.01013 (86112524)	0.00929 (86112524)	0.00853 (86112524)	0.00784c(86053024)
330.0	0.01227c(86082524)	0.01139c(86082524)	0.01054c(86082524)	0.00973c(86082524)	0.00957 (86031224)
340.0	0.01413c(86020424)	0.01305c(86020424)	0.01233c(86102524)	0.01270c(86102524)	0.01286c(86102524)
350.0	0.01331 (86082124)	0.01278 (86082124)	0.01224 (86082124)	0.01221 (86052024)	0.01223 (86052024)
360.0	0.01616c(86071324)	0.01535c(86071324)	0.01476 (86082024)	0.01497 (86112624)	0.01448 (86112624)

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* THE 2ND HIGHEST 24-HR AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: ALL \*\*\*  
 INCLUDING SOURCE(S): 1 , 2 , 3 ,

\*\*\* NETWORK ID: POL1 ; NETWORK TYPE: GRIDPOLR \*\*\*

\*\* CONC OF OTHER IN (MICROGRAMS/CUBIC-METER) \*\*

RECTION (DEGREES)	DISTANCE (METERS)		
	900.00	950.00	1000.00
10.0	0.01361 (86121224)	0.01335 (86121224)	0.01303 (86121224)
20.0	0.01253 (86011024)	0.01256 (86011024)	0.01248 (86011024)
30.0	0.01099c(86081924)	0.01054 (86072824)	0.01029 (86072824)
40.0	0.01154 (86021024)	0.01158 (86021024)	0.01154 (86021024)
50.0	0.01270 (86112024)	0.01247 (86100424)	0.01243 (86112024)
60.0	0.01213 (86100424)	0.01177 (86121824)	0.01164 (86121824)
70.0	0.01244c(86072024)	0.01180c(86072024)	0.01123c(86072024)
80.0	0.00858c(86020724)	0.00867c(86122524)	0.00880c(86020724)
90.0	0.01140 (86012024)	0.01113 (86012024)	0.01082 (86012024)
100.0	0.00887c(86030524)	0.00858c(86090624)	0.00873c(86090624)
110.0	0.01002c(86012324)	0.00934c(86012324)	0.00882 (86011324)
120.0	0.01266c(86012324)	0.01231c(86012324)	0.01200c(86012324)
130.0	0.01219 (86102624)	0.01254 (86102624)	0.01275c(86012824)
140.0	0.01014 (86122924)	0.01013 (86032124)	0.01054c(86012524)
150.0	0.01260 (86032124)	0.01240 (86032124)	0.01198 (86101624)
160.0	0.01600 (86011124)	0.01623 (86011124)	0.01634 (86111524)
170.0	0.01870 (86012424)	0.01820 (86012424)	0.01773c(86103024)
180.0	0.01621 (86110224)	0.01678 (86110224)	0.01719 (86110224)
190.0	0.00968 (86060524)	0.00955 (86122724)	0.00961 (86122724)
200.0	0.01280 (86121624)	0.01262 (86121624)	0.01249 (86010724)
210.0	0.01142 (86101924)	0.01112 (86101924)	0.01074 (86101924)
220.0	0.01356 (86060524)	0.01333 (86111424)	0.01318 (86111424)
230.0	0.01438 (86102224)	0.01419 (86092024)	0.01414 (86092024)
240.0	0.01691 (86102924)	0.01702 (86102924)	0.01695 (86102924)
250.0	0.01167 (86091524)	0.01112 (86091524)	0.01066c(86082224)
260.0	0.01142 (86110924)	0.01124 (86020924)	0.01104 (86020924)
270.0	0.01193 (86051524)	0.01179c(86091024)	0.01157c(86091024)
280.0	0.01188 (86040424)	0.01153 (86040424)	0.01113 (86040424)
290.0	0.01183 (86052624)	0.01143 (86052624)	0.01098 (86052624)
300.0	0.01440 (86122324)	0.01452 (86122324)	0.01444 (86122324)
310.0	0.01116 (86112524)	0.01056 (86112524)	0.01014 (86031824)
320.0	0.00750c(86110624)	0.00737c(86110624)	0.00719c(86110624)
330.0	0.00988 (86031224)	0.01014 (86031224)	0.01029 (86031224)
340.0	0.01293c(86102524)	0.01293c(86102524)	0.01282c(86102524)
350.0	0.01209 (86052024)	0.01189 (86052024)	0.01162 (86052024)
360.0	0.01391 (86112624)	0.01336 (86112624)	0.01281 (86112624)

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* THE 2ND HIGHEST 24-HR AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: ALL \*\*\*  
 INCLUDING SOURCE(S): 1 , 2 , 3 ,

\*\*\* DISCRETE CARTESIAN RECEPTOR POINTS \*\*\*

\*\* CONC OF OTHER IN (MICROGRAMS/CUBIC-METER) \*\*

X-COORD (M)	Y-COORD (M)	CONC	(YYMMDDHH)	X-COORD (M)	Y-COORD (M)	CONC	(YYMMDDHH)
0.00	0.00	0.02892c	(86090124)	15.24	0.00	0.03397	(86103124)
30.48	0.00	0.02639	(86103124)	45.72	0.00	0.03157	(86121624)
60.96	0.00	0.02405	(86102824)	76.20	0.00	0.02741	(86091724)
91.44	0.00	0.02796	(86091724)	106.68	0.00	0.02414	(86122724)
121.92	0.00	0.03310c	(86122624)	137.16	0.00	0.03795	(86122224)
152.40	0.00	0.03785	(86122124)	167.64	0.00	0.03299c	(86103024)
182.88	0.00	0.03098	(86101724)	198.12	0.00	0.03345	(86032824)
213.36	0.00	0.02293	(86062624)	213.36	15.24	0.02515	(86062624)
213.36	30.48	0.02578	(86011424)	213.36	45.72	0.02768	(86041924)
213.36	60.96	0.03214c	(86041424)	213.36	76.20	0.03050c	(86012824)
213.36	91.44	0.03675c	(86012524)	213.36	106.68	0.05417	(86102624)
213.36	121.92	0.06106c	(86060624)	213.36	137.16	0.05314	(86011324)
213.36	152.40	0.03318c	(86042524)	213.36	167.64	0.05123c	(86071424)
213.36	182.88	0.04826c	(86041624)	213.36	198.12	0.03941c	(86020724)
213.36	213.36	0.05963	(86040824)	213.36	221.29	0.04659	(86100424)
198.12	221.29	0.04759c	(86021824)	182.88	221.29	0.04200	(86072624)
167.64	221.29	0.05682c	(86090624)	152.40	221.29	0.06444c	(86081824)
137.16	221.29	0.06526	(86081324)	121.92	221.29	0.06302	(86121024)
106.68	221.29	0.05402	(86031324)	91.44	221.29	0.03699c	(86050724)
76.20	221.29	0.03316	(86031924)	60.96	221.29	0.04123	(86112524)
45.72	221.29	0.03915c	(86081224)	30.48	221.29	0.04186c	(86080924)
15.24	221.29	0.03966c	(86051824)	0.00	221.29	0.02989c	(86100324)
0.00	213.36	0.03325c	(86100324)	0.00	198.12	0.03496c	(86020424)
0.00	182.88	0.03683c	(86100824)	0.00	167.64	0.04150c	(86092924)
0.00	152.40	0.03317c	(86082624)	0.00	137.16	0.02762	(86110924)
0.00	121.92	0.03577c	(86060324)	0.00	106.68	0.02939c	(86051324)
0.00	91.44	0.02701	(86111124)	0.00	76.20	0.03446	(86102924)
0.00	60.96	0.02615c	(86082224)	0.00	45.72	0.02612c	(86051724)
0.00	30.48	0.02476	(86092624)	0.00	15.24	0.02709c	(86090124)

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* THE MAXIMUM 50 24-HR AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: ALL  
 INCLUDING SOURCE(S): 1 , 2 , 3 ,

\*\* CONC OF OTHER IN (MICROGRAMS/CUBIC-METER) \*\*

RANK	CONC (YYMMDDHH) AT	RECEPTOR (XR,YR) OF TYPE	RANK	CONC (YYMMDDHH) AT	RECEPTOR (XR,YR) OF TYPE
1.	0.08421 (86072324) AT (	152.40, 221.29) DC	26.	0.05556 (86063024) AT (	137.16, 221.29) DC
2.	0.07934c(86071924) AT (	213.36, 167.64) DC	27.	0.05521 (86031224) AT (	106.68, 221.29) DC
3.	0.07349c(86012924) AT (	181.68, 240.55) GP	28.	0.05515c(86060824) AT (	181.68, 240.55) GP
4.	0.07088c(86012324) AT (	213.36, 121.92) DC	29.	0.05485c(86041224) AT (	152.40, 221.29) DC
5.	0.06746c(86050724) AT (	76.20, 221.29) DC	30.	0.05417 (86102624) AT (	213.36, 106.68) DC
6.	0.06731 (86082024) AT (	137.16, 221.29) DC	31.	0.05402 (86031324) AT (	106.68, 221.29) DC
7.	0.06723 (86100924) AT (	121.92, 221.29) DC	32.	0.05392 (86030424) AT (	213.36, 213.36) DC
8.	0.06526 (86081324) AT (	137.16, 221.29) DC	33.	0.05314 (86011324) AT (	213.36, 137.16) DC
9.	0.06444c(86081824) AT (	152.40, 221.29) DC	34.	0.05243 (86113024) AT (	121.92, 221.29) DC
10.	0.06355 (86030324) AT (	198.12, 221.29) DC	35.	0.05217 (86022224) AT (	167.64, 221.29) DC
11.	0.06302 (86121024) AT (	121.92, 221.29) DC	36.	0.05215c(86061124) AT (	152.40, 221.29) DC
12.	0.06227c(86012924) AT (	167.64, 221.29) DC	37.	0.05200 (86111724) AT (	152.40, 221.29) DC
13.	0.06169c(86071924) AT (	247.63, 161.95) GP	38.	0.05198 (86071224) AT (	137.16, 221.29) DC
14.	0.06106c(86060624) AT (	213.36, 121.92) DC	39.	0.05190c(86071324) AT (	137.16, 221.29) DC
15.	0.06087 (86072324) AT (	157.98, 251.60) GP	40.	0.05142c(86100524) AT (	213.36, 182.88) DC
16.	0.06052c(86072524) AT (	213.36, 213.36) DC	41.	0.05129 (86112624) AT (	137.16, 221.29) DC
17.	0.05995 (86030324) AT (	203.10, 225.55) GP	42.	0.05129 (86071724) AT (	137.16, 221.29) DC
18.	0.05991 (86012624) AT (	137.16, 221.29) DC	43.	0.05123c(86071424) AT (	213.36, 167.64) DC
19.	0.05963 (86040824) AT (	213.36, 213.36) DC	44.	0.05114 (86020524) AT (	152.40, 221.29) DC
20.	0.05953 (86042924) AT (	213.36, 137.16) DC	45.	0.05079c(86102524) AT (	121.92, 221.29) DC
21.	0.05893c(86012324) AT (	213.36, 106.68) DC	46.	0.05066c(86050824) AT (	152.40, 221.29) DC
22.	0.05730 (86072724) AT (	152.40, 221.29) DC	47.	0.05046c(86093024) AT (	0.00, 198.12) DC
23.	0.05682c(86090624) AT (	167.64, 221.29) DC	48.	0.05003 (86121824) AT (	221.59, 207.06) GP
24.	0.05643 (86061324) AT (	167.64, 221.29) DC	49.	0.04996c(86072524) AT (	213.36, 221.29) DC
25.	0.05603 (86072324) AT (	167.64, 221.29) DC	50.	0.04955 (86112724) AT (	137.16, 221.29) DC

\*\* RECEPTOR TYPES: GC = GRIDCART  
 GP = GRIDPOLR  
 DC = DISCCART  
 DP = DISCPOLR  
 BD = BOUNDARY



\*\*\* ISCST2 - VERSION 92062 \*\*\*

\*\*\* Foamex TDI Sources: Foam Line Stack & Rebond Process Exhaust

\*\*\*

01/21/93

\*\*\* 24-hour Average Emission Rates

\*\*\*

10:56:07

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\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* THE SUMMARY OF HIGHEST 24-HR RESULTS \*\*\*

\*\* CONC OF OTHER IN (MICROGRAMS/CUBIC-METER) \*\*

GROUP ID	AVERAGE CONC	DATE		RECEPTOR (XR, YR, ZELEV, ZFLAG)	NETWORK	
		(YYMMDDHH)			OF TYPE	GRID-ID
L	HIGH 1ST HIGH VALUE IS	0.08421	ON 86072324: AT (	152.40,	221.29,	0.00, 0.00) DC
	HIGH 2ND HIGH VALUE IS	0.06526	ON 86081324: AT (	137.16,	221.29,	0.00, 0.00) DC

\*\*\* RECEPTOR TYPES:

- GC = GRIDCART
- GP = GRIDPOLR
- DC = DISCCART
- DP = DISCPOLR
- BD = BOUNDARY

\*\*\* ISCST2 - VERSION 92062 \*\*\*      \*\*\* Foamex TDI Sources: Foam Line Stack & Rebond Process Exhaust  
                                         \*\*\* 24-hour Average Emission Rates

\*\*\* 01/21/93  
\*\*\* 10:56:07  
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\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* Message Summary For ISC2 Model Execution \*\*\*

----- Summary of Total Messages -----

Total of            0 Fatal Error Message(s)  
Total of            0 Warning Message(s)  
X Total of           328 Informational Message(s)  
  
Total of            328 Calm Hours Identified

\*\*\*\*\* FATAL ERROR MESSAGES \*\*\*\*\*  
          \*\*\* NONE \*\*\*

\*\*\*\*\* WARNING MESSAGES \*\*\*\*\*  
          \*\*\* NONE \*\*\*

\*\*\*\*\*  
\*\*\* ISCST2 Finishes Successfully \*\*\*  
\*\*\*\*\*

**Run: FMXTDI8**

**TDI Annual Average Emission Rates**

ISCST2 EXTENDED MODEL - (DATED 92062)

IBM-PC VERSION (1.01)

(C) COPYRIGHT 1992, TRINITY CONSULTANTS, INC.

SERIAL NUMBER 8025 SOLD TO CROSS TESSITORE & ASSOCIATES

RUN BEGAN ON 01/21/93 AT 11:11:26

CO STARTING

CO TITLEONE Foamex TDI Sources: Foam Line Stack & Rebond Process Exhaust

CO TITLETWO Annual Average Emission Rates

CO MODELOPT DFAULT CONC RURAL

CO AVERTIME PERIOD

CO POLLUTID OTHER

CO RUNORNOT RUN

CO FINISHED

STARTING

\*\* Source Location Cards:

	SRCID	SRCTYP	XS	YS	ZS
SO LOCATION	1	POINT	175.8720	119.7880	.0000
LOCATION	2	POINT	141.4290	162.7650	.0000
LOCATION	3	POINT	141.4290	166.4230	.0000

Source Parameter Cards:

POINT:	SRCID	QS	HS	TS	VS	DS
** VOLUME:	SRCID	QS	HS	SYINIT	SZINIT	
** AREA:	SRCID	QS	HS	XINIT		
SO SRCPARAM	1	.0033208	38.1000	299.8200	24.3810	.7021
SO SRCPARAM	2	.0001239	12.4968	299.8200	1.0348	.7620
SO SRCPARAM	3	.0001239	12.4968	299.8200	1.0348	.7620

\*\* NOTE: Direction-Specific Building Heights Used for Non-SS Source 1

BUILDHGT	1	15.24	15.24	15.24	15.24	15.24	15.24
BUILDHGT	1	.00	.00	.00	.00	.00	.00
SO BUILDHGT	1	.00	.00	15.24	15.24	15.24	.00
SO BUILDHGT	1	.00	15.24	15.24	15.24	15.24	15.24
BUILDHGT	1	.00	.00	.00	.00	.00	.00
SO BUILDHGT	1	.00	.00	15.24	15.24	15.24	15.24
SO BUILDHGT	2	12.19	12.19	10.67	10.67	10.67	10.67
BUILDHGT	2	10.67	10.67	10.67	10.67	10.67	10.67
BUILDHGT	2	10.67	10.67	10.67	10.67	10.67	10.67
SO BUILDHGT	2	10.67	12.19	10.67	10.97	10.97	10.97
BUILDHGT	2	10.97	10.97	10.67	10.67	10.67	10.67
BUILDHGT	2	12.19	12.19	12.19	12.19	12.19	12.19
SO BUILDHGT	3	12.19	12.19	10.67	10.67	10.67	10.67
SO BUILDHGT	3	10.67	10.67	10.67	10.67	10.67	10.67
BUILDHGT	3	10.67	10.67	10.67	10.67	10.67	10.67
SO BUILDHGT	3	10.67	10.67	10.67	10.67	10.97	10.97
SO BUILDHGT	3	10.97	10.97	10.67	10.67	10.67	10.67
BUILDHGT	3	12.19	12.19	12.19	12.19	12.19	12.19

NOTE: Direction-Specific Building Widths Used for Non-SS Source 1

SO BUILDWID	1	84.68	91.23	95.01	95.96	95.84	93.53
-------------	---	-------	-------	-------	-------	-------	-------

SO BUILDWID	1	.00	.00	.00	.00	.00	.00
SO BUILDWID	1	.00	.00	93.84	90.70	83.88	.00
SO BUILDWID	1	.00	91.23	95.01	95.96	95.84	93.53
SO BUILDWID	1	.00	.00	.00	.00	.00	.00
SO BUILDWID	1	.00	.00	93.84	90.70	83.88	75.55
SO BUILDWID	2	84.68	88.29	196.53	209.06	215.24	215.89
SO BUILDWID	2	214.49	206.95	193.13	194.58	194.74	192.50
SO BUILDWID	2	186.24	176.60	161.59	148.74	138.57	125.52
SO BUILDWID	2	154.11	88.29	196.53	24.84	24.73	23.71
SO BUILDWID	2	21.98	19.58	193.13	194.58	194.74	192.50
SO BUILDWID	2	125.05	122.42	116.07	106.20	93.09	77.16
SO BUILDWID	3	84.68	87.62	196.53	209.06	215.24	215.89
SO BUILDWID	3	214.49	206.95	193.13	194.58	194.74	192.50
SO BUILDWID	3	186.24	176.60	161.59	148.74	138.57	125.52
SO BUILDWID	3	154.11	178.03	196.53	209.06	24.58	23.71
SO BUILDWID	3	21.98	19.58	193.13	194.58	194.74	192.50
SO BUILDWID	3	124.83	122.42	116.07	106.20	93.09	77.16
SO EMISUNIT		.100000E+07 (GRAMS/SEC)		(MICROGRAMS/CUBIC-METER)			
SO SRCGROUP	ALL						
SO FINISHED							

STARTING

GRIDPOLR POL1 STA  
 RE GRIDPOLR POL1 ORIG 106.68 110.6424  
 GRIDPOLR POL1 DIST 150. 200. 250. 300. 350. 400. 450. 500. 550.  
 GRIDPOLR POL1 DIST 600. 650. 700. 750. 800. 850. 900. 950. 1000.  
 RE GRIDPOLR POL1 GDIR 36 10. 10.  
 RE GRIDPOLR POL1 END

DISCCART	.00	.00
RE DISCCART	15.24	.00
RE DISCCART	30.48	.00
DISCCART	45.72	.00
DISCCART	60.96	.00
RE DISCCART	76.20	.00
DISCCART	91.44	.00
DISCCART	106.68	.00
RE DISCCART	121.92	.00
RE DISCCART	137.16	.00
DISCCART	152.40	.00
RE DISCCART	167.64	.00
RE DISCCART	182.88	.00
DISCCART	198.12	.00
DISCCART	213.36	.00
RE DISCCART	213.36	15.24
RE DISCCART	213.36	30.48
DISCCART	213.36	45.72
RE DISCCART	213.36	60.96
RE DISCCART	213.36	76.20
DISCCART	213.36	91.44
RE DISCCART	213.36	106.68
RE DISCCART	213.36	121.92
DISCCART	213.36	137.16
DISCCART	213.36	152.40
RE DISCCART	213.36	167.64
RE DISCCART	213.36	182.88
DISCCART	213.36	198.12
RE DISCCART	213.36	213.36

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RE DISCCART      213.36    221.29
RE DISCCART      198.12    221.29
RE DISCCART      182.88    221.29
RE DISCCART      167.64    221.29
RE DISCCART      152.40    221.29
RE DISCCART      137.16    221.29
RE DISCCART      121.92    221.29
RE DISCCART      106.68    221.29
RE DISCCART       91.44    221.29
RE DISCCART       76.20    221.29
RE DISCCART       60.96    221.29
RE DISCCART       45.72    221.29
RE DISCCART       30.48    221.29
RE DISCCART       15.24    221.29
RE DISCCART        .00    221.29
RE DISCCART        .00    213.36
RE DISCCART        .00    198.12
RE DISCCART        .00    182.88
RE DISCCART        .00    167.64
RE DISCCART        .00    152.40
RE DISCCART        .00    137.16
RE DISCCART        .00    121.92
RE DISCCART        .00    106.68
RE DISCCART        .00     91.44
RE DISCCART        .00     76.20
RE DISCCART        .00     60.96
RE DISCCART        .00     45.72
RE DISCCART        .00     30.48
RE DISCCART        .00     15.24
RE FINISHED

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STARTING
ME INPUTFIL C:\models\iscst2\ORLTP86.BIN UNIFORM
ANEMHGHT 10.000 METERS
SURFDATA 12815 1986 SURFNAME
ME UAIRDATA 12842 1986 UAIRNAME
ME WINDCATS 1.54 3.09 5.14 8.23 10.80
FINISHED

```

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STARTING
FINISHED

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*****
* SETUP Finishes Successfully ***
*****

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\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* MODEL SETUP OPTIONS SUMMARY \*\*\*

\*\*Model Is Setup For Calculation of Average CONCentration Values.

\*\*Model Uses RURAL Dispersion.

\*\*Model Uses Regulatory DEFAULT Options:

1. Final Plume Rise.
2. Stack-tip Downwash.
3. Buoyancy-induced Dispersion.
4. Use Calms Processing Routine.
5. Not Use Missing Data Processing Routine.
6. Default Wind Profile Exponents.
7. Default Vertical Potential Temperature Gradients.
8. "Upper Bound" Values for Supersquat Buildings.
9. No Exponential Decay for RURAL Mode

\*\*Model Assumes Receptors on FLAT Terrain.

\*\*Model Assumes No FLAGPOLE Receptor Heights.

\*\*Model Calculates PERIOD Averages Only

\*\*This Run Includes: 3 Source(s); 1 Source Group(s); and 706 Receptor(s)

\*\*The Model Assumes A Pollutant Type of: OTHER

\*\*Model Set To Continue RUNNING After the Setup Testing.

Output Options Selected:

Model Outputs Tables of PERIOD Averages by Receptor

NOTE: The Following Flags May Appear Following CONC Values: c for Calm Hours  
m for Missing Hours  
b for Both Calm and Missing Hours

Misc. Inputs: Anem. Hgt. (m) = 10.00 ; Decay Coef. = 0.0000 ; Rot. Angle = 0.0  
Emission Units = (GRAMS/SEC) ; Emission Rate Unit Factor = 0.10000E+07  
Output Units = (MICROGRAMS/CUBIC-METER)

\*\*Input Runstream File: D:\MODEL DAT\ISCST2\FOAMEX\FMXTDIA.NEW ; \*\*Output Print File: D:\MODEL DAT\ISCST2\FOAMEX\FMXTDIA.LST

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* POINT SOURCE DATA \*\*\*

SOURCE ID	NUMBER PART. CATS.	EMISSION RATE (USER UNITS)	X (METERS)	Y (METERS)	BASE	STACK	STACK	STACK	STACK	BUILDING EXISTS	EMISSION RATE	
					ELEV. (METERS)	HEIGHT (METERS)	TEMP. (DEG.K)	EXIT VEL. (M/SEC)	DIAMETER (METERS)		SCALAR	VARY BY
1	0	0.33208E-02	175.9	119.8	0.0	38.10	299.82	24.38	0.70	YES		
2	0	0.12390E-03	141.4	162.8	0.0	12.50	299.82	1.03	0.76	YES		
3	0	0.12390E-03	141.4	166.4	0.0	12.50	299.82	1.03	0.76	YES		



\*\*\* ISCST2 - VERSION 92062 \*\*\*

\*\*\* Foamex TDI Sources: Foam Line Stack & Rebond Process Exhaust

\*\*\*

01/21/93

\*\*\* Annual Average Emission Rates

\*\*\*

11:11:26

PAGE 3

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* SOURCE IDs DEFINING SOURCE GROUPS \*\*\*

GROUP ID

SOURCE IDs

ALL 1 , 2 , 3 ,

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* DIRECTION SPECIFIC BUILDING DIMENSIONS \*\*\*

SOURCE ID: 1

IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK
1	15.2	84.7	0	2	15.2	91.2	0	3	15.2	95.0	0	4	15.2	96.0	0	5	15.2	95.8	0	6	15.2	93.5	0
7	0.0	0.0	0	8	0.0	0.0	0	9	0.0	0.0	0	10	0.0	0.0	0	11	0.0	0.0	0	12	0.0	0.0	0
13	0.0	0.0	0	14	0.0	0.0	0	15	15.2	93.8	0	16	15.2	90.7	0	17	15.2	83.9	0	18	0.0	0.0	0
19	0.0	0.0	0	20	15.2	91.2	0	21	15.2	95.0	0	22	15.2	96.0	0	23	15.2	95.8	0	24	15.2	93.5	0
25	0.0	0.0	0	26	0.0	0.0	0	27	0.0	0.0	0	28	0.0	0.0	0	29	0.0	0.0	0	30	0.0	0.0	0
31	0.0	0.0	0	32	0.0	0.0	0	33	15.2	93.8	0	34	15.2	90.7	0	35	15.2	83.9	0	36	15.2	75.6	0

SOURCE ID: 2

IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK
1	12.2	84.7	0	2	12.2	88.3	0	3	10.7	196.5	0	4	10.7	209.1	0	5	10.7	215.2	0	6	10.7	215.9	0
7	10.7	214.5	0	8	10.7	206.9	0	9	10.7	193.1	0	10	10.7	194.6	0	11	10.7	194.7	0	12	10.7	192.5	0
13	10.7	186.2	0	14	10.7	176.6	0	15	10.7	161.6	0	16	10.7	148.7	0	17	10.7	138.6	0	18	10.7	125.5	0
19	10.7	154.1	0	20	12.2	88.3	0	21	10.7	196.5	0	22	11.0	24.8	0	23	11.0	24.7	0	24	11.0	23.7	0
25	11.0	22.0	0	26	11.0	19.6	0	27	10.7	193.1	0	28	10.7	194.6	0	29	10.7	194.7	0	30	10.7	192.5	0
31	12.2	125.1	0	32	12.2	122.4	0	33	12.2	116.1	0	34	12.2	106.2	0	35	12.2	93.1	0	36	12.2	77.2	0

SOURCE ID: 3

IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK	IFV	BH	BW	WAK
1	12.2	84.7	0	2	12.2	87.6	0	3	10.7	196.5	0	4	10.7	209.1	0	5	10.7	215.2	0	6	10.7	215.9	0
7	10.7	214.5	0	8	10.7	206.9	0	9	10.7	193.1	0	10	10.7	194.6	0	11	10.7	194.7	0	12	10.7	192.5	0
13	10.7	186.2	0	14	10.7	176.6	0	15	10.7	161.6	0	16	10.7	148.7	0	17	10.7	138.6	0	18	10.7	125.5	0
19	10.7	154.1	0	20	10.7	178.0	0	21	10.7	196.5	0	22	10.7	209.1	0	23	11.0	24.6	0	24	11.0	23.7	0
25	11.0	22.0	0	26	11.0	19.6	0	27	10.7	193.1	0	28	10.7	194.6	0	29	10.7	194.7	0	30	10.7	192.5	0
31	12.2	124.8	0	32	12.2	122.4	0	33	12.2	116.1	0	34	12.2	106.2	0	35	12.2	93.1	0	36	12.2	77.2	0

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* GRIDDED RECEPTOR NETWORK SUMMARY \*\*\*

\*\*\* NETWORK ID: POL1 ; NETWORK TYPE: GRIDPOLR \*\*\*

\*\*\* ORIGIN FOR POLAR NETWORK \*\*\*

X-ORIG = 106.68 ; Y-ORIG = 110.64 (METERS)

\*\*\* DISTANCE RANGES OF NETWORK \*\*\*

(METERS)

150.0,	200.0,	250.0,	300.0,	350.0,	400.0,	450.0,	500.0,	550.0,	600.0,
650.0,	700.0,	750.0,	800.0,	850.0,	900.0,	950.0,	1000.0,		

\*\*\* DIRECTION RADIALS OF NETWORK \*\*\*

(DEGREES)

10.0,	20.0,	30.0,	40.0,	50.0,	60.0,	70.0,	80.0,	90.0,	100.0,
110.0,	120.0,	130.0,	140.0,	150.0,	160.0,	170.0,	180.0,	190.0,	200.0,
210.0,	220.0,	230.0,	240.0,	250.0,	260.0,	270.0,	280.0,	290.0,	300.0,
310.0,	320.0,	330.0,	340.0,	350.0,	360.0,				

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* DISCRETE CARTESIAN RECEPTORS \*\*\*

(X-COORD, Y-COORD, ZELEV, ZFLAG)

(METERS)

( 0.0, 0.0, 0.0, 0.0);	( 15.2, 0.0, 0.0, 0.0);
( 30.5, 0.0, 0.0, 0.0);	( 45.7, 0.0, 0.0, 0.0);
( 61.0, 0.0, 0.0, 0.0);	( 76.2, 0.0, 0.0, 0.0);
( 91.4, 0.0, 0.0, 0.0);	( 106.7, 0.0, 0.0, 0.0);
( 121.9, 0.0, 0.0, 0.0);	( 137.2, 0.0, 0.0, 0.0);
( 152.4, 0.0, 0.0, 0.0);	( 167.6, 0.0, 0.0, 0.0);
( 182.9, 0.0, 0.0, 0.0);	( 198.1, 0.0, 0.0, 0.0);
( 213.4, 0.0, 0.0, 0.0);	( 213.4, 15.2, 0.0, 0.0);
( 213.4, 30.5, 0.0, 0.0);	( 213.4, 45.7, 0.0, 0.0);
( 213.4, 61.0, 0.0, 0.0);	( 213.4, 76.2, 0.0, 0.0);
( 213.4, 91.4, 0.0, 0.0);	( 213.4, 106.7, 0.0, 0.0);
( 213.4, 121.9, 0.0, 0.0);	( 213.4, 137.2, 0.0, 0.0);
( 213.4, 152.4, 0.0, 0.0);	( 213.4, 167.6, 0.0, 0.0);
( 213.4, 182.9, 0.0, 0.0);	( 213.4, 198.1, 0.0, 0.0);
( 213.4, 213.4, 0.0, 0.0);	( 213.4, 221.3, 0.0, 0.0);
( 198.1, 221.3, 0.0, 0.0);	( 182.9, 221.3, 0.0, 0.0);
( 167.6, 221.3, 0.0, 0.0);	( 152.4, 221.3, 0.0, 0.0);
( 137.2, 221.3, 0.0, 0.0);	( 121.9, 221.3, 0.0, 0.0);
( 106.7, 221.3, 0.0, 0.0);	( 91.4, 221.3, 0.0, 0.0);
( 76.2, 221.3, 0.0, 0.0);	( 61.0, 221.3, 0.0, 0.0);
( 45.7, 221.3, 0.0, 0.0);	( 30.5, 221.3, 0.0, 0.0);
( 15.2, 221.3, 0.0, 0.0);	( 0.0, 221.3, 0.0, 0.0);
( 0.0, 213.4, 0.0, 0.0);	( 0.0, 198.1, 0.0, 0.0);
( 0.0, 182.9, 0.0, 0.0);	( 0.0, 167.6, 0.0, 0.0);
( 0.0, 152.4, 0.0, 0.0);	( 0.0, 137.2, 0.0, 0.0);
( 0.0, 121.9, 0.0, 0.0);	( 0.0, 106.7, 0.0, 0.0);
( 0.0, 91.4, 0.0, 0.0);	( 0.0, 76.2, 0.0, 0.0);
( 0.0, 61.0, 0.0, 0.0);	( 0.0, 45.7, 0.0, 0.0);
( 0.0, 30.5, 0.0, 0.0);	( 0.0, 15.2, 0.0, 0.0);



\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* THE FIRST 24 HOURS OF METEOROLOGICAL DATA \*\*\*

FILE: C:\models\iscst2\ORLTMP86.BIN  
 SURFACE STATION NO.: 12815  
 NAME: SURFNAME  
 YEAR: 1986

FORMAT: UNFORM  
 UPPER AIR STATION NO.: 12842  
 NAME: UAIRNAME  
 YEAR: 1986

YEAR	MONTH	DAY	HOUR	FLOW	SPEED	TEMP	STAB	MIXING HEIGHT (M)	
				VECTOR	(M/S)	(K)	CLASS	RURAL	URBAN
86	1	1	1	1.0	3.60	289.3	4	639.0	639.0
86	1	1	2	168.0	5.14	288.7	4	639.0	639.0
86	1	1	3	124.0	3.09	288.2	4	639.0	639.0
86	1	1	4	353.0	2.57	288.2	4	639.0	639.0
86	1	1	5	333.0	2.57	288.7	4	639.0	639.0
86	1	1	6	332.0	2.57	288.7	4	639.0	639.0
86	1	1	7	335.0	3.09	288.7	4	639.0	639.0
86	1	1	8	3.0	3.60	289.3	4	639.0	639.0
86	1	1	9	347.0	3.60	289.8	4	639.0	639.0
86	1	1	10	1.0	5.14	292.0	4	639.0	639.0
86	1	1	11	14.0	4.63	292.6	4	639.0	639.0
86	1	1	12	16.0	4.12	294.3	4	639.0	639.0
86	1	1	13	73.0	3.09	295.4	4	639.0	639.0
86	1	1	14	49.0	3.60	297.0	4	639.0	639.0
86	1	1	15	142.0	2.06	296.5	4	639.0	639.0
86	1	1	16	144.0	2.06	295.9	4	639.0	639.0
86	1	1	17	261.0	2.06	295.4	4	639.0	639.0
86	1	1	18	257.0	2.06	292.6	4	644.0	644.0
86	1	1	19	274.0	3.60	291.5	4	655.0	655.0
86	1	1	20	227.0	3.09	290.9	4	666.0	666.0
86	1	1	21	230.0	3.09	290.9	4	678.0	678.0
86	1	1	22	252.0	2.57	290.4	5	689.0	477.0
86	1	1	23	290.0	2.06	290.4	4	700.0	700.0
86	1	1	24	290.0	1.00	290.4	4	712.0	712.0

NOTES: STABILITY CLASS 1=A, 2=B, 3=C, 4=D, 5=E AND 6=F.  
 FLOW VECTOR IS DIRECTION TOWARD WHICH WIND IS BLOWING.

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* THE PERIOD ( 8760 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: ALL \*\*\*  
 INCLUDING SOURCE(S): 1 , 2 , 3 ,

\*\*\* NETWORK ID: POL1 ; NETWORK TYPE: GRIDPOLR \*\*\*

\*\* CONC OF OTHER IN (MICROGRAMS/CUBIC-METER) \*\*

DIRECTION (DEGREES)	150.00	200.00	250.00	DISTANCE (METERS)		400.00	450.00	500.00	550.00
				300.00	350.00				
10.00	0.00575	0.00420	0.00319	0.00261	0.00226	0.00203	0.00187	0.00174	0.00163
20.00	0.00602	0.00373	0.00276	0.00229	0.00201	0.00183	0.00169	0.00158	0.00148
30.00	0.00538	0.00354	0.00260	0.00213	0.00186	0.00166	0.00152	0.00140	0.00131
40.00	0.00444	0.00302	0.00230	0.00194	0.00172	0.00158	0.00146	0.00137	0.00129
50.00	0.00471	0.00340	0.00253	0.00206	0.00178	0.00159	0.00145	0.00134	0.00126
60.00	0.00379	0.00294	0.00230	0.00188	0.00165	0.00151	0.00141	0.00133	0.00126
70.00	0.00253	0.00200	0.00171	0.00157	0.00147	0.00140	0.00134	0.00128	0.00123
80.00	0.00237	0.00174	0.00126	0.00114	0.00113	0.00111	0.00108	0.00103	0.00099
90.00	0.00270	0.00182	0.00123	0.00107	0.00106	0.00104	0.00099	0.00094	0.00089
100.00	0.00271	0.00201	0.00144	0.00129	0.00122	0.00114	0.00106	0.00098	0.00090
110.00	0.00204	0.00168	0.00157	0.00146	0.00142	0.00137	0.00129	0.00121	0.00114
120.00	0.00225	0.00155	0.00123	0.00118	0.00122	0.00124	0.00124	0.00122	0.00119
130.00	0.00231	0.00162	0.00142	0.00128	0.00122	0.00118	0.00113	0.00108	0.00103
140.00	0.00262	0.00200	0.00152	0.00131	0.00120	0.00112	0.00106	0.00102	0.00097
150.00	0.00270	0.00203	0.00172	0.00153	0.00141	0.00131	0.00123	0.00115	0.00108
160.00	0.00248	0.00188	0.00172	0.00163	0.00152	0.00139	0.00128	0.00120	0.00112
170.00	0.00301	0.00248	0.00205	0.00174	0.00154	0.00139	0.00129	0.00121	0.00115
180.00	0.00257	0.00225	0.00202	0.00184	0.00169	0.00157	0.00147	0.00139	0.00133
190.00	0.00248	0.00207	0.00182	0.00163	0.00149	0.00137	0.00127	0.00119	0.00113
200.00	0.00225	0.00188	0.00167	0.00154	0.00143	0.00133	0.00126	0.00119	0.00113
210.00	0.00299	0.00249	0.00218	0.00196	0.00178	0.00164	0.00153	0.00143	0.00135
220.00	0.00313	0.00266	0.00236	0.00214	0.00196	0.00182	0.00169	0.00158	0.00149
230.00	0.00313	0.00269	0.00243	0.00224	0.00208	0.00196	0.00184	0.00175	0.00166
240.00	0.00339	0.00293	0.00262	0.00239	0.00222	0.00208	0.00196	0.00186	0.00177
250.00	0.00365	0.00301	0.00260	0.00233	0.00214	0.00199	0.00186	0.00175	0.00165
260.00	0.00352	0.00285	0.00248	0.00226	0.00209	0.00194	0.00181	0.00170	0.00160
270.00	0.00352	0.00280	0.00240	0.00217	0.00201	0.00188	0.00178	0.00169	0.00162
280.00	0.00328	0.00289	0.00273	0.00241	0.00212	0.00190	0.00175	0.00163	0.00154
290.00	0.00403	0.00286	0.00243	0.00224	0.00207	0.00188	0.00172	0.00159	0.00148
300.00	0.00366	0.00296	0.00239	0.00202	0.00179	0.00167	0.00160	0.00153	0.00146
310.00	0.00358	0.00271	0.00245	0.00211	0.00186	0.00169	0.00155	0.00142	0.00132
320.00	0.00378	0.00281	0.00219	0.00186	0.00165	0.00148	0.00133	0.00122	0.00112
330.00	0.00353	0.00239	0.00185	0.00156	0.00140	0.00130	0.00121	0.00113	0.00105
340.00	0.00309	0.00223	0.00193	0.00170	0.00153	0.00141	0.00132	0.00124	0.00117
350.00	0.00344	0.00274	0.00236	0.00207	0.00186	0.00170	0.00158	0.00148	0.00139
360.00	0.00462	0.00330	0.00256	0.00219	0.00198	0.00183	0.00172	0.00163	0.00155

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* THE PERIOD ( 8760 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: ALL \*\*\*  
 INCLUDING SOURCE(S): 1 , 2 , 3 ,

\*\*\* NETWORK ID: POL1 ; NETWORK TYPE: GRIDPOLR \*\*\*

\*\* CONC OF OTHER IN (MICROGRAMS/CUBIC-METER) \*\*

DIRECTION (DEGREES)	600.00	650.00	700.00	750.00	800.00	850.00	900.00	950.00	1000.00
10.00	0.00154	0.00147	0.00140	0.00134	0.00129	0.00124	0.00120	0.00115	0.00111
20.00	0.00141	0.00134	0.00128	0.00123	0.00118	0.00114	0.00109	0.00105	0.00101
30.00	0.00123	0.00116	0.00111	0.00106	0.00101	0.00097	0.00094	0.00091	0.00088
40.00	0.00122	0.00116	0.00111	0.00106	0.00102	0.00098	0.00095	0.00091	0.00088
50.00	0.00118	0.00112	0.00107	0.00102	0.00098	0.00094	0.00091	0.00088	0.00085
60.00	0.00121	0.00116	0.00111	0.00108	0.00104	0.00101	0.00098	0.00095	0.00092
70.00	0.00118	0.00113	0.00108	0.00105	0.00101	0.00097	0.00094	0.00091	0.00088
80.00	0.00094	0.00089	0.00085	0.00082	0.00078	0.00075	0.00072	0.00069	0.00067
90.00	0.00083	0.00078	0.00074	0.00070	0.00066	0.00063	0.00060	0.00057	0.00054
100.00	0.00083	0.00077	0.00072	0.00068	0.00064	0.00060	0.00057	0.00054	0.00052
110.00	0.00106	0.00100	0.00094	0.00089	0.00085	0.00081	0.00077	0.00073	0.00070
120.00	0.00115	0.00110	0.00106	0.00101	0.00097	0.00093	0.00089	0.00085	0.00082
130.00	0.00098	0.00092	0.00088	0.00083	0.00079	0.00076	0.00072	0.00069	0.00066
140.00	0.00093	0.00089	0.00086	0.00082	0.00078	0.00075	0.00072	0.00069	0.00066
150.00	0.00102	0.00097	0.00093	0.00089	0.00085	0.00082	0.00079	0.00076	0.00073
160.00	0.00107	0.00103	0.00099	0.00096	0.00093	0.00090	0.00088	0.00085	0.00083
170.00	0.00110	0.00106	0.00102	0.00099	0.00096	0.00093	0.00090	0.00087	0.00085
180.00	0.00128	0.00124	0.00120	0.00117	0.00115	0.00112	0.00109	0.00106	0.00104
190.00	0.00107	0.00103	0.00099	0.00095	0.00093	0.00090	0.00087	0.00085	0.00082
200.00	0.00108	0.00104	0.00100	0.00096	0.00093	0.00090	0.00087	0.00085	0.00082
210.00	0.00128	0.00122	0.00117	0.00112	0.00108	0.00104	0.00101	0.00097	0.00094
220.00	0.00141	0.00134	0.00128	0.00122	0.00117	0.00113	0.00109	0.00105	0.00101
230.00	0.00159	0.00152	0.00146	0.00141	0.00136	0.00131	0.00127	0.00122	0.00118
240.00	0.00170	0.00164	0.00158	0.00152	0.00148	0.00143	0.00138	0.00134	0.00129
250.00	0.00157	0.00150	0.00144	0.00138	0.00133	0.00128	0.00123	0.00119	0.00114
260.00	0.00152	0.00145	0.00138	0.00132	0.00127	0.00122	0.00118	0.00113	0.00109
270.00	0.00156	0.00151	0.00146	0.00141	0.00137	0.00133	0.00129	0.00124	0.00120
280.00	0.00146	0.00140	0.00135	0.00130	0.00126	0.00122	0.00118	0.00114	0.00110
290.00	0.00140	0.00132	0.00126	0.00120	0.00115	0.00111	0.00106	0.00102	0.00098
300.00	0.00139	0.00133	0.00128	0.00122	0.00117	0.00113	0.00109	0.00105	0.00100
310.00	0.00123	0.00116	0.00109	0.00104	0.00099	0.00095	0.00091	0.00087	0.00083
320.00	0.00104	0.00097	0.00091	0.00086	0.00081	0.00077	0.00073	0.00070	0.00067
330.00	0.00099	0.00093	0.00088	0.00083	0.00080	0.00076	0.00073	0.00070	0.00067
340.00	0.00112	0.00107	0.00102	0.00098	0.00094	0.00091	0.00088	0.00085	0.00082
350.00	0.00132	0.00125	0.00119	0.00114	0.00110	0.00106	0.00102	0.00098	0.00094
360.00	0.00148	0.00142	0.00136	0.00131	0.00127	0.00123	0.00119	0.00115	0.00112



\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* THE PERIOD ( 8760 HRS) AVERAGE CONCENTRATION VALUES FOR SOURCE GROUP: ALL  
 INCLUDING SOURCE(S): 1 , 2 , 3 ,

\*\*\* DISCRETE CARTESIAN RECEPTOR POINTS \*\*\*

\*\* CONC OF OTHER IN (MICROGRAMS/CUBIC-METER) \*\*

X-COORD (M)	Y-COORD (M)	CONC	X-COORD (M)	Y-COORD (M)	CONC
0.00	0.00	0.00302	15.24	0.00	0.00322
30.48	0.00	0.00321	45.72	0.00	0.00332
60.96	0.00	0.00286	76.20	0.00	0.00274
91.44	0.00	0.00301	106.68	0.00	0.00308
121.92	0.00	0.00351	137.16	0.00	0.00375
152.40	0.00	0.00313	167.64	0.00	0.00281
182.88	0.00	0.00294	198.12	0.00	0.00272
213.36	0.00	0.00257	213.36	15.24	0.00262
213.36	30.48	0.00259	213.36	45.72	0.00264
213.36	60.96	0.00291	213.36	76.20	0.00303
213.36	91.44	0.00300	213.36	106.68	0.00353
213.36	121.92	0.00427	213.36	137.16	0.00397
213.36	152.40	0.00340	213.36	167.64	0.00361
213.36	182.88	0.00470	213.36	198.12	0.00500
213.36	213.36	0.00508	213.36	221.29	0.00447
198.12	221.29	0.00468	182.88	221.29	0.00544
167.64	221.29	0.00663	152.40	221.29	0.00850
137.16	221.29	0.00887	121.92	221.29	0.00727
106.68	221.29	0.00551	91.44	221.29	0.00462
76.20	221.29	0.00451	60.96	221.29	0.00455
45.72	221.29	0.00455	30.48	221.29	0.00425
15.24	221.29	0.00392	0.00	221.29	0.00344
0.00	213.36	0.00342	0.00	198.12	0.00403
0.00	182.88	0.00423	0.00	167.64	0.00473
0.00	152.40	0.00444	0.00	137.16	0.00417
0.00	121.92	0.00450	0.00	106.68	0.00443
0.00	91.44	0.00443	0.00	76.20	0.00438
0.00	60.96	0.00400	0.00	45.72	0.00364
0.00	30.48	0.00337	0.00	15.24	0.00318

\*\*\* ISCST2 - VERSION 92062 \*\*\*

\*\*\* Foamex TDI Sources: Foam Line Stack & Rebond Process Exhaust  
\*\*\* Annual Average Emission Rates

\*\*\* 01/21/93  
\*\*\* 11:11:26  
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\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* THE SUMMARY OF MAXIMUM PERIOD ( 8760 HRS) RESULTS \*\*\*

\*\* CONC OF OTHER IN (MICROGRAMS/CUBIC-METER) \*\*

GROUP ID	AVERAGE CONC	RECEPTOR (XR, YR, ZELEV, ZFLAG)	OF TYPE	NETWORK GRID-ID
L	1ST HIGHEST VALUE IS 0.00887 AT (	137.16, 221.29, 0.00, 0.00)	DC	
	2ND HIGHEST VALUE IS 0.00850 AT (	152.40, 221.29, 0.00, 0.00)	DC	
	3RD HIGHEST VALUE IS 0.00727 AT (	121.92, 221.29, 0.00, 0.00)	DC	
	4TH HIGHEST VALUE IS 0.00663 AT (	167.64, 221.29, 0.00, 0.00)	DC	
	5TH HIGHEST VALUE IS 0.00602 AT (	157.98, 251.60, 0.00, 0.00)	GP	POL1
	6TH HIGHEST VALUE IS 0.00575 AT (	132.73, 258.36, 0.00, 0.00)	GP	POL1

\*\* RECEPTOR TYPES: GC = GRIDCART  
GP = GRIDPOLR  
DC = DISCCART  
DP = DISCPOLR  
BD = BOUNDARY

\*\*\* ISCST2 - VERSION 92062 \*\*\*      \*\*\* Foamex TDI Sources: Foam Line Stack & Rebond Process Exhaust  
                                         \*\*\* Annual Average Emission Rates

\*\*\* 01/21/93  
\*\*\* 11:11:26  
PAGE 13

\*\*\* MODELING OPTIONS USED: CONC RURAL FLAT DFAULT

\*\*\* Message Summary For ISC2 Model Execution \*\*\*

----- Summary of Total Messages -----

Total of            0 Fatal Error Message(s)  
Total of            0 Warning Message(s)  
Total of            328 Informational Message(s)  
  
Total of            328 Calm Hours Identified

\*\*\*\*\* FATAL ERROR MESSAGES \*\*\*\*\*  
          \*\*\* NONE \*\*\*

\*\*\*\*\* WARNING MESSAGES \*\*\*\*\*  
          \*\*\* NONE \*\*\*

\*\*\*\*\*  
\*\*\* ISCST2 Finishes Successfully \*\*\*  
\*\*\*\*\*

**ATTACHMENT 2**

**FOAMEX L.P.**

**Progress Report & Emission Control Schedule**

**(Orlando Flexible Polyurethane Foam Manufacturing Facility)**

## **ATTACHMENT 2**

### **Foamex L.P. Progress Report & Emission Control Schedule (Orlando Flexible Polyurethane Foam Manufacturing Facility)**

<b>FDER Permit Issued</b>	<b>June 1993</b>
<b>Submission to FDER 1st Progress Report</b>	<b>October 1993</b>
<b>Submission to FDER 2nd Progress Report</b>	<b>June 1994</b>
<b>Submission to FDER 3rd Progress Report</b>	<b>December 1994</b>
<b>Submission to FDER Permit Modification</b>	<b>March 1995</b>
<b>Begin Installation of Final Selection</b>	<b>June 1995</b>
<b>Submission to FDER of Certificate of Completion</b>	<b>December 1995</b>

**ATTACHMENT 3**  
**FOAMEX L.P.**  
**Progress Report Content**  
**(Orlando Flexible Polyurethane Foam Manufacturing Facility)**

## ATTACHMENT 3

### Foamex L.P. Progress Report Content

#### (Orlando Flexible Polyurethane Foam Manufacturing Facility)

##### 1st Progress Report

December 1993

- a) Status of engineering/design for Capture and Disperse concepts.
- b) Current status of industry and EPA data for Capture and Treat concepts.
- c) Current status of Process and Equipment Modification approaches. This report will include status of Foamex installation of VPF system.

##### 2nd Progress Report

June 1994

- a) Preliminary engineering/design drawings for Capture and Disperse concept.
- b) Updated status of industry and EPA data for Capture and Treat concepts.
- c) Updated status of Process and Equipment Modification approaches, including current operational data from Foamex VPF system.

##### 3rd Progress Report

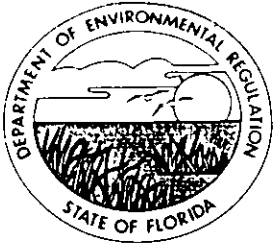
December 1994

- a) Final engineering/design drawings for Capture and Disperse concept.
- b) Final status of industry and EPA data for Capture and Treat concept.
- c) Final status of Process and Equipment Modification approaches, including current operational data from Foamex VPF system.
- d) Selection of final concept which may include any of the above concepts and/or combinations. This final selection will be based on existing criteria, including: 1) economics, 2) performance, and 3) current OSHA, FDER, and EPA regulations.

##### Submission of FDER Construction Permit Modification

March 1995

Based on the final selection of December 1994, a final permit application will be prepared and submitted. This application will reflect the final configuration including any of the studies concepts or combinations of controls, chemical substitution, and/or process or equipment modification.



# Florida Department of Environmental Regulation

Twin Towers Office Bldg. • 2600 Blair Stone Road • Tallahassee, Florida 32399-2400

Lawton Chiles, Governor

Carol M. Browner, Secretary

December 22, 1992

CERTIFIED MAIL - RETURN RECEIPT REQUESTED

Mr. Charles Eavenson, Plant Manager  
Foamex, L.P.  
1351 Gemini Boulevard  
Orlando, Florida 32821

Dear Mr. Eavenson:

Re: Applications for Permits to Construct a Flexible Polyurethane  
Foam Manufacturing Facility

The Bureau of Air Regulation has made a preliminary review of your December 2, 1992, applications for permits to construct a slabstock polyurethane foam production line, a rebond polyurethane foam production line, tank storage area, steam boiler, environmental heating systems, and foam fabrication operation.

Please provide the following additional information to complete these applications.

1. Where is the toluene diisocyanate incinerator located? If in Florida, does it have a Department air permit? If Foamex is the operator of this incinerator in Florida, please provide either the permit number or an application for permit for it.
2. What are the 8-hr, 24-hr, and annual ambient air impacts of toluene diisocyanate emissions from the polyurethane foam facility?
3. On page 1-30 (VI. Foam Fabrication Operation) please clarify the 43.7 foot stack diameter listed in Section H.
4. Please provide a more detailed schedule on the company's investigation to use either another process or add air pollution control at this facility. We want to know what the ongoing studies are, what is expected to be learned from the study, and by what date.
5. Why does the boiler operate longer than the slabstock polyurethane foam production facility? Is it on "stand-by" or do other operations at the facility use steam?

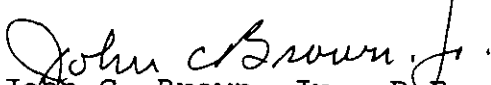


Mr. Charles Eavenson  
Foamex, L. P.  
Page 2

6. What means are used to contain spills and minimize fugitive emissions during process chemical storage and handling?
7. Can any of the blowing agents captured by a carbon adsorption system be recycled at the facility? If so, what is the value of the agent recovered? How does this affect the economics of the BACT determination?
8. Please describe the equipment cleaning practices at this facility. How much and what types of solvents are used? What is done to minimize emissions of these solvents? How are the used solvents disposed of?
9. Under the Clean Air Act Amendment of 1990, use of HCFC for non-insulating foams is prohibited after January 1, 1994 (page 6-A-45 of the application). Any permit issued will reflect that limitation. What will be used after this date?

The Department will resume processing your applications after receipt of the requested information. Please write to me or call Willard Hanks at (904) 488-1344, if you have any questions on this matter.

Sincerely,

  
John C. Brown, Jr., P.E.  
Administrator  
Air Permitting and Standards

JCB/WH/plm

cc: Charles Collins, CD  
Joe Tessitore, P.E.

PS Form 3811, July 1983 447-845

**SENDER: Complete items 1, 2, 3 and 4.**

Put your address in the "RETURN TO" space on the reverse side. Failure to do this will prevent this card from being returned to you. The return receipt fee will provide you the name of the person delivered to and the date of delivery. For additional fees the following services are available. Consult postmaster for fees and check box(es) for service(s) requested.

- 1.  Show to whom, date and address of delivery.
- 2.  Restricted Delivery.

3. Article Addressed to:  
 Charles E. Evanson, Plant Mag.  
 Dorman, R.P.  
 1351 Gemini Blvd  
 Orlando, FL 32821

4. Type of Service:	Article Number
<input type="checkbox"/> Registered <input type="checkbox"/> Insured <input checked="" type="checkbox"/> Certified <input type="checkbox"/> COD <input type="checkbox"/> Express Mail	P062921936

Always obtain signature of addressee or agent and **DATE DELIVERED.**

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X

6. Signature - Agent  
X N. Bowser

7. Date of Delivery  
12/24/92

8. Addressee's Address (ONLY if requested and fee paid)

DOMESTIC RETURN RECEIPT

PS Form 3800, June 1991

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P 062 921 936



Receipt for Certified Mail

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Charles E. Evanson  
Dorman  
Orlando, FL