Walker, Elizabeth (AIR)

From: Osbourn, Scott [Scott_Osbourn@golder.com]

Sent: Friday, July 11, 2008 11:12 AM
To: Read, David; Linero, Alvaro
Subject: BG&E Draft Documents

Attachments: Emissions Standards rev2.doc; RAI Emission Calcs rev2.xls

These are the remaining attachments referred to in the draft RAI response package. We can also touch on these during our 2 PM call, if you've had time to review.

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BG&E TALLAHASSEE RENEWABLE ENERGY CENTER

ESTIMATED EMISSIONS

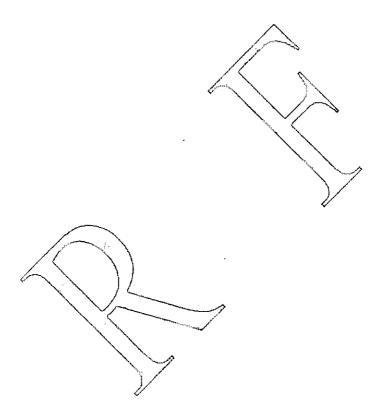
Pollutant	Fuel	Method of Operation ^a	Stack (3-Run /		CEMS ^c Compliance	Estimated Emissions (Informational purposes only)
		10 1501	lb/hr	ppmvd @ 15% O ₂	lb/hr ^d	
		СТ	32.5 🤇	1/	32.5	18.4
	Product Gas	CT/DB	32.5		32.5	19.2
NO _X	N 10 6	CT	25.0	\	25.0	8.8
	Natural Gas ^c	CT/DB			1.	
	P. 1. C	CT	50.0		50.0	17.2
	Product Gas	CT/DB	50.0		50.0	21.4
CO		CT				12.1
	Natural Gas e CT/DB	CT/DB				
		CŢ/	>			4.9
	Product Gas	CT/DB\	7 - /			6.5
VOC		ст 🌾	<i>V</i>			0.4
	Natural Gas e	atural Gas ^e CT/DB				
:		CT	V			6.7
PM	Product Gas	CT/DB				7.2
PM		CT				1.0
	Natural Gas ^e	CT/DB				
	Product Gas	CT	0.06			8.8
SO ₂	/ / J	CT/DB	0.06			11.3
(lb/MMBtu)	Natural Gas e	CT	0.06			8.8
<u> </u>		CT/DB	0.06			11.3

a. CT means operation of CT in combined cycle mode without use of the DB. CT & DB means operation in combined cycle mode and using the DB.

c. CEMS for NO_x and CO will be installed on the HRSG stacks. Correction to 15% O₂ is required for NO_x, consistent with the provisions of 40 CFR 60, Subpart KKKK. Compliance with the continuous NO_x and CO standards will be demonstrated based on data collected by the required CEMS. NOx compliance will be based on a 4- hour rolling average for natural gas firing and a 30-day rolling average for product gas firing. CO compliance will be based on a 30-day rolling average. Compliance will be based on all periods, except startup, shutdown, fuel switching or documented malfunction. The CTs will operate above 80% load, or the lowest load at which compliance is demonstrated during initial testing.

b. The initial and annual U.S. EPA Reference Method tests associated with the certification of the NOx and CO CEMS instruments may also be used to demonstrate compliance with the individual standards for product gas and natural gas. Compliance with the NOx standards will be demonstrated by conducting tests in accordance with EPA Method 7E. Compliance with the CO standards will be demonstrated by conducting tests in accordance with EPA Method 10.

- d. The mass emission rate estimates are based on a turbine inlet condition of 59° F and may be adjusted to actual test conditions in accordance with the performance curves and/or equations on file with the Department.
- e. Limits for natural gas firing are imposed for NOx and SO₂ only, as required by the New Source Performance Standards pursuant to 40 CFR 60, Subpart KKKK. The natural gas fired values provided for other pollutants are for informational purposes only.



Calculate SO2 for the CT firing on natural gas (which would only be used for SU). Assume:

• 2 gr/100 scf and heat input of 147 MMBtu/hr for the CT —need SO2 rate in lb/hr

Calculate SO2 for the CT/DB based on use of product gas. Calculate based on H25 content of 5 ppm (mass basis) in product gas. Assume:

- . Stack exhaust flow rate of 410,210 lb/hr for CT/DB combined and temp of 364 F
- Assume 100% conversion of H2S to SO2

Natural Gas Firing (C1 Only)

- the heating value of the product gas is 435 Btu/cf (LHV)
- The gas will be flared if not used in the CT/DB--for the flare emissions, assume flaring of all product gas generated (~ 378 MMBtu/hr--LHV)

Calculate SO2 emissions, given the product gas H2S content. The product gas will either be fired in combustion turbines or in a flare. Issues:

• Would the calculation be the same for both the CT and for the flare?

The calculation would be the same, except for conversion efficiency, if there is known difference in conversion efficiency between a CT and a flare.

Sulfur Content 2 gr/100 scf]	Based on 5ppm concentration				
Heat Input	СТ	147 MMBtu/hr				<u> </u>	
	DB	MMBtu/hr		Conc.	5 ppm		
	Total	147 MMBtu/hr		stack flow rate	403,569 lb/hr	@ 364 deg. F	
		•		Heating Value of product gas	435 btu/cf	- -	
Heating value		1040 btu/cf		Temperature	823,67 deg R		
Fuel use		141,346.15 cf/hr		Heat Input	3.78E+08 Btu/hr		
		1,413.46 100 cf/hr		Volumetric flowrate	142,444 88 acfm	@ 364 deg F	
S		0 40 lb/hr				Assumed MW gas 28.4	
SO2		0.81 lb/hr	7	SO2	4,55 lb/hr	_	
			_		0.03 Ib/MMI	Stu	
				$lb/hr = (ppm/10^6) \times 2,116.8 \times (66)$	0xV) x (MW/1545 6) x (1/f)	_	
Emission Factors	CO	8 2E-02 lb/MMBtu	AP-42 Table 3 1-1	, , , , , , , , , , , , , , , , , , , ,			
	VOC	2.1 E-03 lb/MMBtu	AP-42 Table 3 1-2a	ppm = parts per million l	by volume		
PMtot		6 6E-03 lb/MMBtu AP-42 Table					
		0 01 05 ID:::IMI/I	12 14010 3,1-24	MW = molecular weight		SO2	
co		12.05 lb/hr	٦	T = temperature of ga			
VOC		0.31 lb/hr	1	l .c.mperature or ga		¥ : = :	
PMtot		0.97 lb/hr	4				
 -			J	Product Gas Firing (CT/DB, F	H= 189 MMRtu/hr) \$02		
NOx Conc 25 ppm			Based on 5ppm concentration				
Volumetric flowra	ate	142,444.90 acfm		maste on applia tolicelli ation			
Stack Temperature		1.074 F	assumed	Conc.	5 ppm		
MW	•	46	assaurea	stack flow rate	410,210 lb/hr	@ 364 deg F	
		40		Heating Value of product gas	435 btu/cf	C. W. dek	
NOx		8,78 lb/hr	7	Temperature	823.67 deg. R		
		0.70 10/81	_	Heat Input	3,78E+08 Btu/hr		
				Volumetric flowrate	144,788 90 acfm	@ 364 deg F	
				volumetric nowrate	194,700 30 aCIII	Assumed MW gas 28.4	
				SO2	4.62 lh/hr	Assumed M W gas 28.4	
				1752	0.02 lb/MME		
				lb/hr =(ppm/10 ⁶) x 2,116 8 x (60xV) x (MW/1545 6) x (1/T)			
				ppm = parts per million by volume			
					ate in acfm or dscfm		
				MW = molecular weight	= 64	SO2	
				M w = molecular weight	- 04	302	

Product Gas Firing (CT Only) SO2