

00 South Adams Street, Box A-2, Tallahassee, Florida 32301, (850) 891-4YOU (4968), talgov.com

June 6, 2006

Hamilton S. Oven, Administrator Siting Coordination Office Department of Environmental Protection 2600 Blair Stone Road Tallahassee, Florida 32399-2400 Hand Delivered

Re: Cit

City of Tallahassee Arvah B. Hopkins Generating Station Hopkins Unit 2 Request for Modification of Site Certification No. PA 74-03 RECEIVED

JUN 07 2006

BUREAU OF AIR REGULATION

Dear Mr. Oven:

Pursuant to Section 403.516, Florida Statutes, the City of Tallahassee (City) hereby requests a modification of the Site Certification for Unit No. 2 at the City's Arvah B. Hopkins Electric Generating Station (Hopkins). By this request, the City is seeking approval to "repower" the existing, certified Hopkins Unit 2 by retiring the existing oil and gas-fired boiler and installing a new combustion turbine and heat recovery steam generator.

The repowering project will not result in an increase in steam electric generating capacity at the Hopkins site. Therefore, a modification of the site certification is necessary. Detailed information regarding the repowering project is provided in the attached application for modification of site certification. The factual reasons supporting the modification and the anticipated effects of the proposed modification on the City, the public and the environment are addressed in this application.

Enclosed, please find a check in the amount of \$10,000 made payable to the Department of Environmental Protection as required under Rule 62-17.293(1)(c)2., Florida Administrative Code.

The City requests that the Florida Department of Environmental Protection (Department) undertake a review of this request for modification by consulting with the other affected agencies. Upon conclusion of that review, the City requests that the Department issue a Proposed Order of Modification for review by the parties and the public, and ultimately, a Final Order granting the requested modification of certification.

The City looks forward to working with the Department and the various agencies that will be involved in reviewing this requested modification. Should you have any questions or concerns regarding this modification request, please do not hesitate to contact me at (850) 891-8851, or Rob McGarrah, Manager of Power Production at (850) 891-5534.

Sincerely,

John K. Powell, P.E.

Interim Environmental and Safety Manager

Attachments

cc: Scott Goorland, Esq., FDEP

Parties to Hopkins Unit 2 Certification

FDEP Bureau of Air Regulation (P.E. Sealed Air Permit)

#### AIR PERMIT APPLICATION FOR THE CITY OF TALLAHASSEE ARVAH B. HOPKINS GENERATING STATION UNIT NO. 2 REPOWERING PROJECT LEON COUNTY, FLORIDA

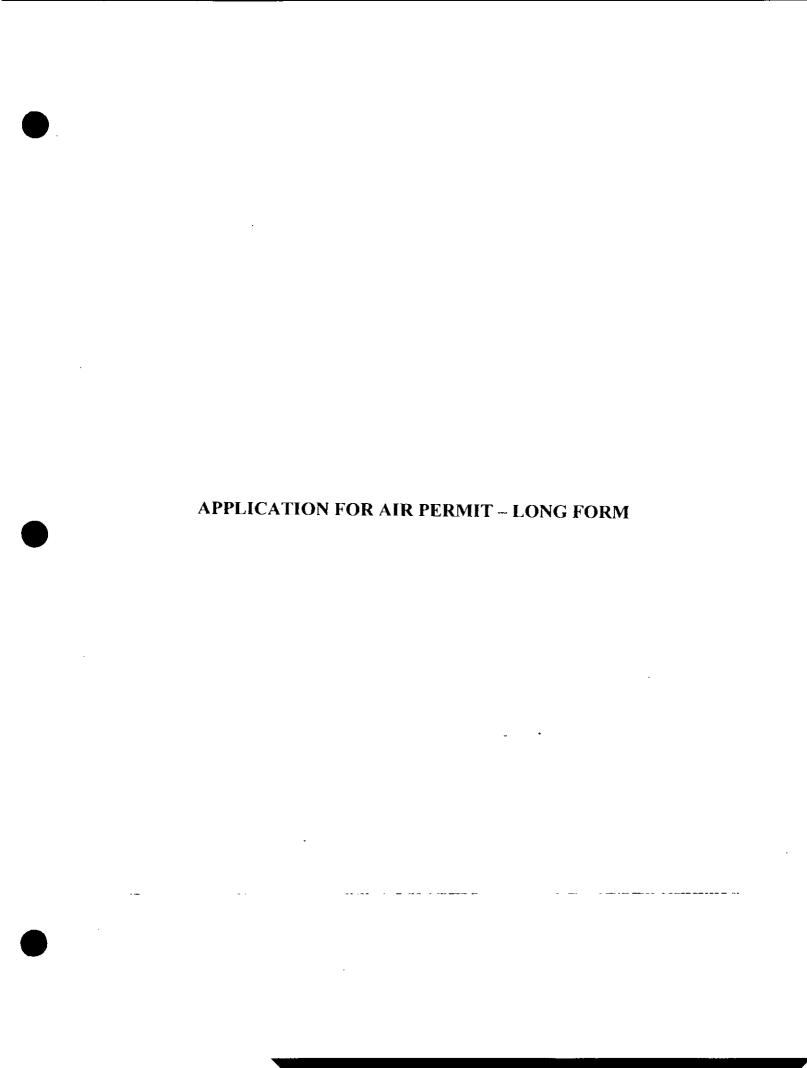
Prepared For: City of Tallahassee 300 South Adams Street Tallahassee, Florida

Prepared By: Golder Associates Inc. 6241 NW 23rd Street, Suite 500 Gainesville, Florida 32653-1500

> May 2006 063-7522

#### **DISTRIBUTION:**

- 4 Copies FDEP
- 3 Copies City of Tallahassee
- 2 Copies Golder Associates Inc.





### Department of Environmental Protection

## Division of Air Resource Management APPLICATION FOR AIR PERMIT - LONG FORM

#### I. APPLICATION INFORMATION

Air Construction Permit – Use this form to apply for an air construction permit at a facility operating under a federally enforceable state air operation permit (FESOP) or Title V air permit. Also use this form to apply for an air construction permit:

- For a proposed project subject to prevention of significant deterioration (PSD) review, nonattainment area (NAA) new source review, or maximum achievable control technology (MACT) review; or
- Where the applicant proposes to assume a restriction on the potential emissions of one or more pollutants to escape a federal program requirement such as PSD review, NAA new source review, Title V, or MACT; or
- Where the applicant proposes to establish, revise, or renew a plantwide applicability limit (PAL).

Air Operation Permit - Use this form to apply for:

- An initial federally enforceable state air operation permit (FESOP); or
- An initial/revised/renewal Title V air operation permit.

Air Construction Permit & Revised/Renewal Title V Air Operation Permit (Concurrent Processing Option) – Use this form to apply for both an air construction permit and a revised or renewal Title V air operation permit incorporating the proposed project.

To ensure accuracy, please see form instructions.

Ide	entification of Facility						
1.	Facility Owner/Company Name: City of Tallahassee, Electric Utilities						
2.	Site Name: Arvah B. Hopkins Generating St	ation					
3.	Facility Identification Number: 0730003						
4.	Facility Location: Street Address or Other Locator: Route 4, Box 450, 1125 Geddie Road (County Road 1585)						
	City: Tallahassee County: I	.eon	Zip Code: <b>32304</b>				
5.	Relocatable Facility?  ☐ Yes ☐ No	6. Existing Title   ⊠ Yes	V Permitted Facility? ☐ No				
<u>Ap</u>	plication Contact						
1.	Application Contact Name: John K. Powell	, J.D., P.E., Environm	nental Resources				
2.	Application Contact Mailing Address Organization/Firm: City of Tallahassee, Env	vironmental Resourc	:es				
	Street Address: City Hall, 300 South Ada						
	-		7: 0 1 20004 4704				
	City: Tallahassee S	tate: Florida	Zip Code: <b>32301-1731</b>				
3.	Application Contact Telephone Numbers						
	Telephone: <b>(850) 891-8851</b> ext.	Fax: (850) 891-	-8277				
4.	. Application Contact Email Address: powellj@talgov.com						
Ap	pplication Processing Information (DEP U	Jse)					

DEP Form No. 62-210.900(1) – Form Effective: 02/02/06

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1. Date of Receipt of Application: (-7-00) 3. PSD Number (if applicable):—2. Project Number(s): 0.730003-009-40 4. Siting Number (if applicable):

#### **Purpose of Application**

This application for air permit is submitted to obtain: (Check one)
Air Construction Permit  ☐ Air construction permit. ☐ Air construction permit to establish, revise, or renew a plantwide applicability limit (PAL). ☐ Air construction permit to establish, revise, or renew a plantwide applicability limit (PAL), and separate air construction permit to authorize construction or modification of one or more emissions units covered by the PAL.
Air Operation Permit  Initial Title V air operation permit.  Title V air operation permit revision.  Title V air operation permit renewal.  Initial federally enforceable state air operation permit (FESOP) where professional engineer (PE) certification is required.  Initial federally enforceable state air operation permit (FESOP) where professional engineer (PE) certification is not required.
Air Construction Permit and Revised/Renewal Title V Air Operation Permit (Concurrent Processing)  Air construction permit and Title V permit revision, incorporating the proposed project.  Air construction permit and Title V permit renewal, incorporating the proposed project.  Note: By checking one of the above two boxes, you, the applicant, are requesting concurrent processing pursuant to Rule 62-213.405, F.A.C. In such case, you must also check the following box:
☐ I hereby request that the department waive the processing time requirements of the air construction permit to accommodate the processing time frames of the Title V air operation permit.

#### **Application Comment**

This application is for repowering of Unit No. 2 with a new GE 7FA combined-cycle combustion turbine (CT). City of Tallahassee proposes to permanently shut down the boiler associated with Unit No. 2 and construct a new GE 7FA CT. The CT can operate in combined cycle mode, with and without a duct burner, and simple cycle mode firing natural gas and distillate fuel oil with exhaust gases routed to the heat recovery steam generator (HRSG) and selective catalytic reduction (SCR) system. The duct burner will be fired with natural gas. In addition, the CT can operate in simple cycle mode firing natural gas only with exhaust gases routed to an emergency bypass stack, instead of the HRSG and SCR system. Emission netting results in pollutant emission increases below the PSD significant thresholds. See Part B.

#### **Scope of Application**

Emissions Unit ID Number	Description of Emissions Unit	Air Permit Type	Air Permit Proc. Fee
CT2A	GE 7FA Combined-Cycle Combustion Turbine and Duct Burner	AC1A	N/A
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#### Owner/Authorized Representative Statement

Complete if applying for an air construction permit or an initial FESOP.

1. Owner/Authorized Representative Name:

Robert E. McGarrah, Production Superintendent

2. Owner/Authorized Representative Mailing Address...

Organization/Firm: City of Tallahassee, Electric Utilities

Street Address: 2602 Jackson Bluff Road

City: Tallahassee

State: Florida

Zip Code: 32304

3. Owner/Authorized Representative Telephone Numbers...

Telephone: (850) 891-5534

ext.

Fax:

(850) 891-5162

4. Owner/Authorized Representative Email Address: McGarraR@talgov.com

5. Owner/Authorized Representative Statement:

I, the undersigned, am the owner or authorized representative of the facility addressed in this air permit application. I hereby certify, based on information and belief formed after reasonable inquiry, that the statements made in this application are true, accurate and complete and that, to the best of my knowledge, any estimates of emissions reported in this application are based upon reasonable techniques for calculating emissions. The air pollutant emissions units and air pollution control equipment described in this application will be operated and maintained so as to comply with all applicable standards for control of air pollutant emissions found in the statutes of the State of Florida and rules of the Department of Environmental Protection and revisions thereof and all other requirements identified in this application to which the facility is subject. I understand that a permit, if granted by the department, cannot be transferred without authorization from the department, and I will promptly notify the department upon sale or legal transfer of the facility or any permitted emissions unit.

Signature

Date

6/1/06

#### **Application Responsible Official Certification**

Complete if applying for an initial/revised/renewal Title V permit or concurrent processing of an air construction permit and a revised/renewal Title V permit. If there are multiple responsible officials, the "application responsible official" need not be the "primary responsible official."

1.	Application Responsible Official Name:						
2.	Application Responsible Official Qualification (Check one or more of the following options, as applicable):						
	For a corporation, the president, secretary, treasurer, or vice-president of the corporation in charge of a principal business function, or any other person who performs similar policy or decision-making functions for the corporation, or a duly authorized representative of such person if the representative is responsible for the overall operation of one or more manufacturing, production, or operating facilities applying for or subject to a permit under Chapter 62-213, F.A.C.						
	For a partnership or sole proprietorship, a general partner or the proprietor, respectively.  For a municipality, county, state, federal, or other public agency, either a principal executive						
	officer or ranking elected official.						
3.	The designated representative at an Acid Rain source.  Application Responsible Official Mailing Address						
٦.	Organization/Firm:						
	Street Address:						
	City: State: Zip Code:						
4.	Application Responsible Official Telephone Numbers						
	Telephone: ( ) - ext. Fax: ( ) -						
5.	Application Responsible Official Email Address:						
6.	Application Responsible Official Certification:						
	I, the undersigned, am a responsible official of the Title V source addressed in this air permit application. I hereby certify, based on information and belief formed after reasonable inquiry, that the statements made in this application are true, accurate and complete and that, to the best of my knowledge, any estimates of emissions reported in this application are based upon reasonable techniques for calculating emissions. The air pollutant emissions units and air pollution control equipment described in this application will be operated and maintained so as to comply with all applicable standards for control of air pollutant emissions found in the statutes of the State of Florida and rules of the Department of Environmental Protection and revisions thereof and all other applicable requirements identified in this application to which the Title V source is subject. I understand that a permit, if granted by the department, cannot be transferred without authorization from the department, and I will promptly notify the department upon sale or legal transfer of the facility or any permitted emissions unit. Finally, I certify that the facility and each emissions unit are in compliance with all applicable requirements to which they are subject, except as identified in compliance plan(s) submitted with this application.						
	Signature Date						
	Signature Date						

Pro	ofessional Engineer Certification
1.	Professional Engineer Name: Kennard F. Kosky
	Registration Number: 14996
2.	Professional Engineer Mailing Address
	Organization/Firm: Golder Associates Inc.**
ļ	Street Address: 6241 NW 23 <sup>rd</sup> Street, Suite 500
	City: Gainesville State: FL Zip Code: 32653
3.	Professional Engineer Telephone Numbers
	Telephone: (352) 336-5600 ext.516 Fax: (352) 336-6603
4.	Professional Engineer Email Address: kkosky@golder.com
5.	Professional Engineer Statement:
	I, the undersigned, hereby certify, except as particularly noted herein*, that:
	(1) To the best of my knowledge, there is reasonable assurance that the air pollutant emissions unit(s) and the air pollution control equipment described in this application for air permit, when properly operated and maintained, will comply with all applicable standards for control of air pollutant emissions found in the Florida Statutes and rules of the Department of Environmental Protection; and
	(2) To the best of my knowledge, any emission estimates reported or relied on in this application are true, accurate, and complete and are either based upon reasonable techniques available for calculating emissions or, for emission estimates of hazardous air pollutants not regulated for an emissions unit addressed in this application, based solely upon the materials, information and calculations submitted with this application.
	(3) If the purpose of this application is to obtain a Title V air operation permit (check here , if so), I further certify that each emissions unit described in this application for air permit, when properly operated and maintained, will comply with the applicable requirements identified in this application to which the unit is subject, except those emissions units for which a compliance plan and schedule is submitted with this application.
	(4) If the purpose of this application is to obtain an air construction permit (check here ⊠, if so) or concurrently process and obtain an air construction permit and a Title V air operation permit revision or renewal for one or more proposed new or modified emissions units (check here □, if so), I further certify that the engineering features of each such emissions unit described in this application have been designed or examined by me or individuals under my direct supervision and found to be in conformity with sound engineering principles applicable to the control of emissions of the air pollutants characterized in this application.
	(5) If the purpose of this application is to obtain an initial air operation permit or operation permit revision or renewal for one or more newly constructed or modified emissions units (check here , if so). I further certify that, with the exception of any changes detailed as part of this application, each such emissions unit has been constructed or modified in substantial accordance with the information given in the corresponding application for air construction permit and with all provisions contained in such permit.    Signature   5/31/06     Date   Da
	(seal): Action of the seal of

<sup>\*</sup> Attach any exception to certification statement.

\*\* Board of Professional Engineers Certificate of Authorization #00001670

#### A. GENERAL FACILITY INFORMATION

#### **Facility Location and Type**

1.	. Facility UTM Coordinates Zone 16 East (km) 749.53 North (km) 3371.7		2.	Facility Latitude/Longitude (DD/MM/Longitude (DD/MM/Longi	(SS) <b>30/27/08</b>
3.	Governmental Facility Code: 4	4. Facility Status Code: A	5.	Facility Major Group SIC Code: 49	6. Facility SIC(s): 4911
7.	Facility Comment:	•	•		

#### **Facility Contact**

1.	Application Contact Name: John K. Powell, J.D., P.E., Environmental Resources						
2.	Application Contact Mailing Address Organization/Firm: City of Tallahassee, Environmental Resources						
	_	Street Address: City Hall, 300 South Adams Street					
		City: Tallahassee	Stat	e: Florida	Zip Code: <b>32301-1731</b>		
3.	Application Contact Telephone Numbers						
	Telephone:	(850) 891-8851	ext.	Fax: (850)	891-8277		
4.	Application Contact Email Address: powellj@talgov.com						

#### Facility Primary Responsible Official

Complete if an "application responsible official" is identified in Section I. that is not the facility "primary responsible official."

1.	Facility Primary Responsible Official Name:						
2.	Facility Primary Responsible Official Mailing Address Organization/Firm:						
	Street Address:						
	City:		State:		Zip Code:		
3.	. Facility Primary Responsible Official Telephone Numbers						
	Telephone: ( )	-	ext.	Fax: (	) -	!	
4.	Facility Primary Resp	onsible Officia	Email Add	ress:			

#### **Facility Regulatory Classifications**

Check all that would apply following completion of all projects and implementation of all other changes proposed in this application for air permit. Refer to instructions to distinguish between a "major source" and a "synthetic minor source."

1.	Small Business Stationary Source	☐ Unknown
2.	Synthetic Non-Title V Source	
3. 🛛	Title V Source	
4. 🗵	Major Source of Air Pollutants, Other than Hazardous	Air Pollutants (HAPs)
5. 🗆	Synthetic Minor Source of Air Pollutants, Other than I	HAPs
6. 🛛	Major Source of Hazardous Air Pollutants (HAPs)	
7. 🔲	Synthetic Minor Source of HAPs	
8. 🛛	One or More Emissions Units Subject to NSPS (40 CI	FR Part 60)
9.	One or More Emissions Units Subject to Emission Gu	idelines (40 CFR Part 60)
10. 🖾	One or More Emissions Units Subject to NESHAP (40	CFR Part 61 or Part 63)
11.	Title V Source Solely by EPA Designation (40 CFR 76	0.3(a)(5))
NSF to ti will mee	ility Regulatory Classifications Comment: PS - 40 CFR Part 60, Subpart GG, applies to the propose he HRSG duct burner. However, the proposed 40 CFR I replace Subpart GG. Under Subpart KKKK, the duct bu eting the requirements of Subpart Da. NESHAP- 40 CFR ly based on actual oil fuel used in a calendar year.	Part 60, Subpart KKKK, eventually irner would be exempt from

#### **List of Pollutants Emitted by Facility**

1. Pollutant Emitted	2. Pollutant Classification	3. Emissions Cap [Y or N]?
Particulate Matter - PM	Α	No
Particulate Matter with an aerodynamic diameter less than 10 microns - PM <sub>10</sub>	A	No
Sulfur Dioxide - SO <sub>2</sub>	Α	No
Nitrogen Oxides - NO <sub>x</sub>	A	No
Carbon Monoxide - CO	A	No
Volatile Organic Compounds - VOCs	A	No
Total Hazardous Air Pollutants HAPs	Α	No
Sulfuric Acid Mist – SAM	A	No
-		

#### **B. EMISSIONS CAPS**

#### Facility-Wide or Multi-Unit Emissions Caps

						Emissions Caps	or Multi-Unit		
asis for	6. Bas	Annual	5.	Hourly	4.	3. Emissions	2. Facility		1. Pollutant
missions	Em	Cap		Cap		Unit ID No.s	Wide		Subject to
ap	Cap	(ton/yr)		(lb/hr)	Ì	Under Cap	Сар	ons	<b>Emissions</b>
•						(if not all	[Y or N]?		Cap
						units)	(all units)		
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				ent:	omm	t Emissions Cap C	de or Multi-Uni	y-Wide	7. Facility-W

#### C. FACILITY ADDITIONAL INFORMATION

#### Additional Requirements for All Applications, Except as Otherwise Stated

1.	Facility Plot Plan: (Required for all permit applications, except Title V air operation permit revision applications if this information was submitted to the department within the previous five years and would not be altered as a result of the revision being sought)  ☐ Attached, Document ID: Part B☐ Previously Submitted, Date: ☐
2.	Process Flow Diagram(s): (Required for all permit applications, except Title V air operation permit revision applications if this information was submitted to the department within the previous five years and would not be altered as a result of the revision being sought)  Attached, Document ID: Part B Previously Submitted, Date:
3.	Precautions to Prevent Emissions of Unconfined Particulate Matter: (Required for all permit applications, except Title V air operation permit revision applications if this information was submitted to the department within the previous five years and would not be altered as a result of the revision being sought)  Attached, Document ID: Previously Submitted, Date:
<u>A</u> 0	Iditional Requirements for Air Construction Permit Applications
1.	Area Map Showing Facility Location:  Attached, Document ID: Not Applicable (existing permitted facility)
2.	Description of Proposed Construction, Modification, or Plantwide Applicability Limit (PAL):  ☑ Attached, Document ID: Part B
3.	Rule Applicability Analysis:  Attached, Document ID: Part B
4.	List of Exempt Emissions Units (Rule 62-210.300(3)(a) or (b)1., F.A.C.):  ☐ Attached, Document ID: Part B ☐ Not Applicable (no exempt units at facility)
5.	Fugitive Emissions Identification (Rule 62-212.400(2), F.A.C.):  Attached, Document ID: Not Applicable
6.	Air Quality Analysis (Rule 62-212.400(7), F.A.C.):  Attached, Document ID: Not Applicable
7.	Ambient Impact Analysis (Rule 62-212.400(5)(d), F.A.C.):  ☐ Attached, Document ID: ☐ Not Applicable
8.	Air Quality Impact since 1977 (Rule 62-212.400(5)(h)5., F.A.C.):  ☐ Attached, Document ID: ☐ Not Applicable
9.	Additional Impact Analyses (Rules 62-212.400(5)(e)1. and 62-212.500(4)(e), F.A.C.):  Attached, Document ID:   Not Applicable
10.	Alternative Analysis Requirement (Rule 62-212.500(4)(g), F.A.C.):  Attached, Document ID:   Not Applicable

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#### Additional Requirements for FESOP Applications 1. List of Exempt Emissions Units (Rule 62-210.300(3)(a) or (b)1., F.A.C.): Attached, Document ID:\_\_\_\_ Not Applicable (no exempt units at facility) Additional Requirements for Title V Air Operation Permit Applications 1. List of Insignificant Activities (Required for initial/renewal applications only): Attached, Document ID:\_\_\_\_ Not Applicable (revision application) 2. Identification of Applicable Requirements (Required for initial/renewal applications, and for revision applications if this information would be changed as a result of the revision being sought): Attached, Document ID: Not Applicable (revision application with no change in applicable requirements) 3. Compliance Report and Plan (Required for all initial/revision/renewal applications): Attached, Document ID: Note: A compliance plan must be submitted for each emissions unit that is not in compliance with all applicable requirements at the time of application and/or at any time during application processing. The department must be notified of any changes in compliance status during application processing. 4. List of Equipment/Activities Regulated under Title VI (If applicable, required for initial/renewal applications only): Attached, Document ID: Equipment/Activities On site but Not Required to be Individually Listed Not Applicable 5. Verification of Risk Management Plan Submission to EPA (If applicable, required for initial/renewal applications only): Attached, Document ID: 6. Requested Changes to Current Title V Air Operation Permit: ☐ Attached, Document ID:\_\_\_\_ Not Applicable Additional Requirements Comment

#### III. EMISSIONS UNIT INFORMATION

Title V Air Operation Permit Application - For Title V air operation permitting only, emissions units are classified as regulated, unregulated, or insignificant. If this is an application for Title V air operation permit, a separate Emissions Unit Information Section (including subsections A through I as required) must be completed for each regulated and unregulated emissions unit addressed in this application for air permit. Some of the subsections comprising the Emissions Unit Information Section of the form are optional for unregulated emissions units. Each such subsection is appropriately marked. Insignificant emissions units are required to be listed at Section II, Subsection C.

Air Construction Permit or FESOP Application - For air construction permitting or federally enforceable state air operation permitting, emissions units are classified as either subject to air permitting or exempt from air permitting. The concept of an "unregulated emissions unit" does not apply. If this is an application for air construction permit or FESOP, a separate Emissions Unit Information Section (including subsections A through I as required) must be completed for each emissions unit subject to air permitting addressed in this application for air permit. Emissions units exempt from air permitting are required to be listed at Section II, Subsection C.

Air Construction Permit and Revised/Renewal Title V Air Operation Permit Application — Where this application is used to apply for both an air construction permit and a revised/renewal Title V air operation permit, each emissions unit is classified as either subject to air permitting or exempt from air permitting for air construction permitting purposes and as regulated, unregulated, or insignificant for Title V air operation permitting purposes. The air construction permitting classification must be used to complete the Emissions Unit Information Section of this application for air permit. A separate Emissions Unit Information Section (including subsections A through I as required) must be completed for each emissions unit subject to air permitting addressed in this application for air permit. Emissions units exempt from air construction permitting and insignificant emissions units are required to be listed at Section II, Subsection C.

If submitting the application form in hard copy, the number of this Emissions Unit Information Section and the total number of Emissions Unit Information Sections submitted as part of this application must be indicated in the space provided at the top of each page.

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#### A. GENERAL EMISSIONS UNIT INFORMATION

#### Title V Air Operation Permit Emissions Unit Classification

1.	Regulated or Unregulated Emissions Unit? (Check one, if applying for an initial, revised or renewal Title V air operation permit. Skip this item if applying for an air construction permit or FESOP only.)								
	emission	s un	it.				Unit Information S  Unit Information S		
	unregulat	ted e	emissions unit.						
Er	nissions Unit	Des	cription and St	atus	<u> </u>				
1.			ns Unit Addresse						
	process o	r pr	ns Unit Informat oduction unit, or least one definat	act	ivity, whic	h pro	ses, as a single en oduces one or mor (stack or vent).	iissi e ai	ons unit, a single r pollutants and
	process o	r pr	ns Unit Informat oduction units ar t) but may also p	nd a	ctivities wl	nich	has at least one de	issi efina	ons unit, a group of able emission point
	more pro	cess	or production u	nits	and activit	ies v	ses, as a single em	issi itive	ons unit, one or emissions only.
2.	<ol> <li>Description of Emissions Unit Addressed in this Section:</li> <li>One nominal 188-MW GE 7-FA Combined-Cycle Combustion Turbine with HRSG Duct Firing.</li> </ol>								
3.	Emissions U	nit I	dentification Nur	mbe	er: <b>009</b>				
4.	Emissions Unit Status Code: C	5.	Commence Construction Date:	6.	Initial Startup Date:	7.	Emissions Unit Major Group SIC Code: 49	8.	Acid Rain Unit?  ☑ Yes ☐ No
9.	Package Unit				•••			l	
<u> </u>	Manufacturer: General Electric Model Number: 7-FA								
10.	. Generator N	ame	eplate Rating: 18	3 M	W				
11.	11. Emissions Unit Comment:  Based on natural gas-firing at 25°F for CT only. For distillate oil-firing, rating is 199 MW at 25°F.								
•			<del>-</del> ·				· • deple description — — — — define de		- — - · · · · · · · · ·

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#### **Emissions Unit Control Equipment**

1.	Control Equipment/Method(s) Description:  025 – Staged Combustion [Dry Low-NO <sub>x</sub> (DLN) Burners]  028 – Water Injection
	139 – Selective Catalytic Reduction (SCR)
	•
	Control Device or Method Code(s): 025, 028, 139

#### **B. EMISSIONS UNIT CAPACITY INFORMATION**

(Optional for unregulated emissions units.)

#### **Emissions Unit Operating Capacity and Schedule**

i.	. Maximum Process or Throughput Rate:			
2.	2. Maximum Production Rate: 188 MW (nominal)			
3.	Maximum Heat Input Rate: 2,66	4 million Btu/hr (HHV)	•	
4.	Maximum Incineration Rate:	pounds/hr		
		tons/day		
5.	Requested Maximum Operating	Schedule:		
		hours/day	days/week	
		weeks/year	8,760 hours/year	

6. Operating Capacity/Schedule Comment:

Maximum heat input for natural gas-firing at 25 °F, includes 1,899 MMBtu/hr (HHV) heat input from the combustion turbine and 765 MMBtu/hr (HHV) heat input from duct firing. Maximum heat input from oil firing is 2,079 MMBtu/hr (HHV) heat input from the combustion turbine plus 765 MMBtu/hr (HHV) heat input from duct firing natural gas. Heat input varies based on inlet temperature and performance. See Part B.

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## C. EMISSION POINT (STACK/VENT) INFORMATION (Optional for unregulated emissions units.)

#### **Emission Point Description and Type**

Identification of Point on Flow Diagram: Part B	Plot Plan or	2. Emission Point 7	Гуре Code:		
3. Descriptions of Emission Points Comprising this Emissions Unit for VE Tracking:					
4. ID Numbers or Descriptio	ns of Emission Ur	nts with this Emission	n Point in Common:		
<ol><li>Discharge Type Code:</li><li>V</li></ol>	<ol><li>Stack Height 150 feet</li></ol>	:	7. Exit Diameter: 18 feet		
8. Exit Temperature: 188 °F	9. Actual Volur 1,016,100 acfi	metric Flow Rate:	10. Water Vapor: 11.2 %		
<ol> <li>Maximum Dry Standard F dscfm</li> </ol>	low Rate:	12. Nonstack Emission Point Height: feet			
13. Emission Point UTM Coo Zone: 16 East (km): North (km)	749.7	14. Emission Point Latitude/Longitude Latitude (DD/MM/SS) Longitude (DD/MM/SS)			
North (km): 3371.7 Longitude (DD/MM/SS)  15. Emission Point Comment: Information at baseload conditions for natural gas-firing with the duct burner at 59°F ambient temperature. See Part B, Appendix A of the Air Permit Application for performance at various ambient temperatures and loads. The design includes a simple cycle emergency bypass stack with a stack height of 150 feet and a diameter of 18 feet.					

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#### EMISSIONS UNIT INFORMATION

Section [1] GE 7FA and Duct Burner

#### D. SEGMENT (PROCESS/FUEL) INFORMATION

Segment Description and Rate: Segment 1 of 2

1.	. Segment Description (Process/Fuel Type):				
	Internal Combustion Engine – Electric Generation; Turbine, Natural Gas				
2	Source Classification Cod	la (CCC)	12 GOOM :		
2.	. Source Classification Code (SCC): 2-01-002-01		3. SCC Units: Million Cubic Feet		
4.	Maximum Hourly Rate: 2.571	5. Maximum 18,323	Annual Rate:	6. Estimated Annual Activity Factor:	
7.	Maximum % Sulfur:	8. Maximum	% Ash:	9. Million Btu per SCC Unit: 1,036	
10	annual rate is based on to	tal of 8,760 hours pendix A, of the	of operation at	includes duct firing. Maximum 59°F, with 2,598,800 MMBtu/yr of ation for performance at various	

<u>Se</u>	Segment Description and Rate: Segment 2 of 2					
1.	Segment Description (Pro Internal Combustion Engir				, Distillate Oil	
2.	Source Classification Cod 2-01-001-01.	le (S	CC):	3. SCC Units: 1,000 gallons		
4.	Maximum Hourly Rate: 16.0	5.	Maximum . <b>53,276</b>	Annual Rate:	6. Estimated Annual Activity Factor:	
7.	Maximum % Sulfur:	8.	Maximum <sup>4</sup>	% Ash:	9. Million Btu per SCC Unit: 130	
10.	Maximum annual rate is ba (equivalent to 3,500 hours	ased of o	on maximum peration) at 5	n heat input rate 9°F ambient ten	includes maximum duct firing. of 6,926,500 MMBtu/yr perature for the CT. See Part B, t various ambient temperatures,	

#### E. EMISSIONS UNIT POLLUTANTS

#### List of Pollutants Emitted by Emissions Unit

1. Pollutant Emitted	2. Primary Control Device Code	3. Secondary Control Device Code	4. Pollutant Regulatory Code
PM/PM <sub>10</sub>		201100 0000	EL EL
SO <sub>2</sub>			EL
NO <sub>x</sub>	028	139	EL
со			EL
VOCs		-	EL
			***
,			

POLLUTANT DETAIL INFORMATION
Page [1] of [5]
Particulate Matter

## F1. EMISSIONS UNIT POLLUTANT DETAIL INFORMATION – POTENTIAL/ESTIMATED FUGITIVE EMISSIONS

(Optional for unregulated emissions units.)

#### Potential/Estimated Fugitive Emissions

Complete for each pollutant identified in Subsection E if applying for an air construction permit or concurrent processing of an air construction permit and a revised or renewal Title V permit. Complete for each emissions-limited pollutant identified in Subsection E if applying for an air operation permit.

#### POLLUTANT DETAIL INFORMATION Page [1] of [5] **Particulate Matter**

#### F2. EMISSIONS UNIT POLLUTANT DETAIL INFORMATION -**ALLOWABLE EMISSIONS**

Complete if the pollutant identified in Subsection F1 is or would be subject to a numerical emissions limitation.

A 11 ...

	IOWADIE Emissions Allowable Emissions 1 c	<u> </u>				
1.	Basis for Allowable Emissions Code: OTHER	2. Future Effective Date of Allowable Emissions:				
3.	Allowable Emissions and Units: 10% Opacity	4. Equivalent Allowable Emissions: 21.1 lb/hour 65.2 tons/year				
5.	Method of Compliance: EPA Method 9; Initial and once annually.					
	5. Allowable Emissions Comment (Description of Operating Method):  Maximum hourly rate based on natural gas-firing in CT and duct burner at 25°F and full load.  Annual emission rate based on natural gas-firing with a maximum heat input rate of 2,598,800 MMBtu/yr of duct firing at 59°F and full load. Refer to Part B.					
<u>Al</u>	lowable Emissions Allowable Emissions 2 o	ıf <u>2</u>				
1.	Basis for Allowable Emissions Code: OTHER	2. Future Effective Date of Allowable Emissions:				
3.	Allowable Emissions and Units: 10% Opacity	4. Equivalent Allowable Emissions: 38.7 lb/hour 65.8 tons/year				
5.	Method of Compliance: EPA Method 9; Initial; Annual, if >400 hr/yr.					
6.	Allowable Emissions Comment (Description of Operating Method):  Maximum hourly rate based on distillate oil-firing in CT at 59°F and full load. Annual emission rate based on maximum heat input rate of 6,926,500 MMBtu/yr (equivalent to 3,500 hours) of distillate oil-firing of CT at 59°F and full load. Refer to Part B.					
Al	lowable Emissions Allowable Emissions	of				
1.	Basis for Allowable Emissions Code:	2. Future Effective Date of Allowable Emissions:				
3.	Allowable Emissions and Units:	4. Equivalent Allowable Emissions: lb/hour tons/year				
5.	Method of Compliance:					
6.	Allowable Emissions Comment (Description	of Operating Method):				

# POLLUTANT DETAIL INFORMATION Page [2] of [5] Sulfur Dioxide

## F1. EMISSIONS UNIT POLLUTANT DETAIL INFORMATION – POTENTIAL/ESTIMATED FUGITIVE EMISSIONS

(Optional for unregulated emissions units.)

#### Potential/Estimated Fugitive Emissions

Complete for each pollutant identified in Subsection E if applying for an air construction permit or concurrent processing of an air construction permit and a revised or renewal Title V permit. Complete for each emissions-limited pollutant identified in Subsection E if applying for an air operation permit.

1. Pollutant Emitted: SO <sub>2</sub>	2. Total Perc	cent Efficiency of Control:			
3. Potential Emissions:		4. Synthetically Limited?			
111 lb/hour 211.	7 tons/year	⊠ Yes □ No			
5. Range of Estimated Fugitive Emissions (as to tons/year	applicable):				
6. Emission Factor:		7. Emissions			
Reference: See Part B, Air Permit App	olication Report	Method Code:			
8.a. Baseline Actual Emissions (if required): 1,642 tons/year	8.b. Baseline 24-month Period: From: 2/1/2004 To: 1/31/2006				
9.a. Projected Actual Emissions (if required): tons/year	9.b. Projected Monitoring Period: ☐ 5 years ☐ 10 years				
10. Calculation of Emissions:  Maximum hourly rate based on full-load oil firing in CT and duct burner firing gas at 25°F.  Annual emissions based on an equivalent 5,260 hours of natural gas firing with maximum heat input rate of 2,598,800 MMBtu/yr for duct firing at full load and 6,926,500 MMBtu/yr (equivalent to 3,500 hours) of distillate oil-firing of the CT at full load and 59°F. Refer to Part B.					
11. Pollutant Potential/Estimated Fugitive Emissions Comment:  See Section 2.0 of Part B and Appendix A for performance at various ambient temperatures and loads.					

# POLLUTANT DETAIL INFORMATION Page [2] of [5] Sulfur Dioxide

## F2. EMISSIONS UNIT POLLUTANT DETAIL INFORMATION - ALLOWABLE EMISSIONS

Complete if the pollutant identified in Subsection F1 is or would be subject to a numerical emissions limitation.

<u>Allowable Emissions</u>	Allowable	Emissions	<u>1</u> of <u>2</u>
----------------------------	-----------	-----------	----------------------

1.	Basis for Allowable Emissions Code: OTHER	2. Future Effective Date of Allowable Emissions:			
3.	Allowable Emissions and Units: 2 grains S/100 SCF	4. Equivalent Allowable Emissions:  14.7 lb/hour 50.5 tons/year			
5.	Method of Compliance: Fuel analysis				
6.	Allowable Emissions Comment (Description Maximum hourly rate based on natural gas-fit Annual emission rate based on natural gas-fit 2,598,800 MMBtu/yr of duct firing at 59°F and	ring in CT and duct burner at 25°F and full load. ring with a maximum heat input rate of			
Al	lowable Emissions Allowable Emissions 2 o	f <u>2</u>			
1.	Basis for Allowable Emissions Code: Other	2. Future Effective Date of Allowable Emissions:			
3.	Allowable Emissions and Units: 0.05% Sulfur	4. Equivalent Allowable Emissions: 107 lb/hour 178.5 tons/year			
5.	Method of Compliance: Fuel analysis				
6.	Allowable Emissions Comment (Description of Operating Method):  Maximum hourly rate based on distillate oil-firing in CT at 25°F and full load. Annual emission rate based on maximum heat input rate of 6,926,500 MMBtu/yr (equivalent to 3,500 hours) of distillate oil-firing of CT at 59°F and full load. Refer to Part B.				
Al	lowable Emissions Allowable Emissions	of			
1.	Basis for Allowable Emissions Code:	2. Future Effective Date of Allowable Emissions:			
3.	Allowable Emissions and Units:	4. Equivalent Allowable Emissions:  lb/hour tons/year			
5.	Method of Compliance:				
6.	. Allowable Emissions Comment (Description of Operating Method):				

POLLUTANT DETAIL INFORMATION
Page [3] of [5]
Nitrogen Oxides

## F1. EMISSIONS UNIT POLLUTANT DETAIL INFORMATION – POTENTIAL/ESTIMATED FUGITIVE EMISSIONS

(Optional for unregulated emissions units.)

#### **Potential/Estimated Fugitive Emissions**

Complete for each pollutant identified in Subsection E if applying for an air construction permit or concurrent processing of an air construction permit and a revised or renewal Title V permit. Complete for each emissions-limited pollutant identified in Subsection E if applying for an air operation permit.

Pollutant Emitted:     NO <sub>x</sub>	2. Total Perc	ent Efficie	ency of Control:
3. Potential Emissions:		4. Synth	etically Limited?
108.4 lb/hour 265.	7 tons/year	∑Y€	s 🗌 No
5. Range of Estimated Fugitive Emissions (as to tons/year	applicable):		
6. Emission Factor:			7. Emissions
<b>D</b> 0			Method Code:
Reference: See Part B, Air Permit App	olication Report.		0
8.a. Baseline Actual Emissions (if required):	8.b. Baseline		
843.3 tons/year	From: 5/1/2003	To: 4/30	/2005
9.a. Projected Actual Emissions (if required):	9.b. Projected	Monitorir	ng Period:
tons/year		rs 🗌 10	-
10. Calculation of Emissions:  Maximum hourly rate based on full-load oil Annual emissions based on an equivalent 8 operation at full load and 59°F with exhaupotential annual emissions for combined 5,260 hours of natural gas firing with maximum duct firing at full load and 6,926,500 MMBt firing at full load and 59°F. Refer to Part B.	,760 hours of na ust gases route cycle operation num heat input	atural gas ed to eme n are bas rate of 2,	firing for simple cycle rgency bypass stack. ed on an equivalent 598,800 MMBtu/vr for
11. Pollutant Potential/Estimated Fugitive Emis See Section 2.0 of Part B and Appendix A for and loads.			mbient temperatures

POLLUTANT DETAIL INFORMATION
Page [3] of [5]
Nitrogen Oxides

## F2. EMISSIONS UNIT POLLUTANT DETAIL INFORMATION - ALLOWABLE EMISSIONS

Complete if the pollutant identified in Subsection F1 is or would be subject to a numerical emissions limitation.

Allowable Emissions	Allowable Emissions 1 of 1

1.	Basis for Allowable Emissions Code: OTHER	2.	Future Effective Dat Emissions:	e of Allowable
3.	Allowable Emissions and Units: 5 ppmvd @ 15% O <sub>2</sub>	4.	Equivalent Allowabl 47.8 lb/hour	le Emissions: 164.9 tons/year
5.	Method of Compliance: CEMS 30-day rolling average			
6.	Allowable Emissions Comment (Descripti Maximum hourly rate based on natural gas Annual emission rate based on natural gas 2,598,800 MMBtu/yr of duct firing at 59°F ar	-firing -firing	in CT and duct burner with a maximum heat i	

#### Allowable Emissions 2 of 2

1.	Basis for Allowable Emissions Code: OTHER	2.	Future Effective Date of Allowable Emissions:
3.	Allowable Emissions and Units: 10 ppmvd @ 15% O₂ for CT	4.	Equivalent Allowable Emissions:  108.4 lb/hour 135.6 tons/year
5.	Method of Compliance: CEMS 30-day rolling average.	•	
6.	Allowable Emissions Comment (Description Maximum hourly rate based on distillate oil full load. Annual emission rate based on maximum (equivalent to 3,500 hours) of distillate oil-firm	l-firin axim	g in CT and duct burner(gas) at 25°F and um heat input rate of 6,926,500 MMBtu/yr

<u>Al</u>	lowable Emissions Allowable Emissions	(	of
1.	Basis for Allowable Emissions Code: OTHER	2.	Future Effective Date of Allowable Emissions:
3.	Allowable Emissions and Units: 9 ppmvd @ 15% O <sub>2</sub>	4.	Equivalent Allowable Emissions: 61.8 lb/hour 255.6 tons/year
5.	Method of Compliance: CEMS (see Part B)	, <b></b>	
6.	Allowable Emissions Comment (Description For simple cycle operation with emergency natural gas-firing in CT at 25°F and full load. 8,760 hours of operation at 59°F and full load.	bypa: Ann	ss stack. Maximum hourly rate based on ual emission rate based on an equivalent

# POLLUTANT DETAIL INFORMATION Page [4] of [5] Carbon Monoxide

## F1. EMISSIONS UNIT POLLUTANT DETAIL INFORMATION – POTENTIAL/ESTIMATED FUGITIVE EMISSIONS

(Optional for unregulated emissions units.)

#### Potential/Estimated Fugitive Emissions

Complete for each pollutant identified in Subsection E if applying for an air construction permit or concurrent processing of an air construction permit and a revised or renewal Title V permit. Complete for each emissions-limited pollutant identified in Subsection E if applying for an air operation permit.

Pollutant Emitted:     CO	2. Total Percent Efficiency of Control:		
3. Potential Emissions:		4. Synthetically Limited?	
<b>142.9</b> lb/hour <b>340.</b>	1 tons/year	⊠ Yes □ No	
5. Range of Estimated Fugitive Emissions (as to tons/year	applicable):		
6. Emission Factor:		7. Emissions	
		Method Code:	
Reference: See Part B, Air Permit App	olication Report	. 0	
8.a. Baseline Actual Emissions (if required):	8.b. Baseline	24-month Period:	
<b>241.1</b> tons/year	From: 1/1/2001	1 To: 12/31/2002	
9.a. Projected Actual Emissions (if required):	9.b. Projected	Monitoring Period:	
tons/year	☐ 5 yea	ars 10 years	
10. Calculation of Emissions:  Maximum hourly rate based on full-load oil to Annual emissions based on an equivalent 5, heat input rate of 2,598,800 MMBtu/yr for deguivalent to 3,500 hours) of distillate oil-full Refer to Part B.	260 hours of na uct firing at ful	atural gas firing with maximum	
11. Pollutant Potential/Estimated Fugitive Emissions See Section 2.0 of Part B and Appendix A for and loads.			

# POLLUTANT DETAIL INFORMATION Page [4] of [5] Carbon Monoxide

## F2. EMISSIONS UNIT POLLUTANT DETAIL INFORMATION - ALLOWABLE EMISSIONS

Complete if the pollutant identified in Subsection F1 is or would be subject to a numerical emissions limitation.

<b>Allowable Emissions</b>	Allowable Emissions	1	of	2

	THE WOOL SHIPS TO	* =		
1.	Basis for Allowable Emissions Code: OTHER	2.	Future Effective Date Emissions:	of Allowable
3.	Allowable Emissions and Units: 16.8 ppmvd @ 15% O <sub>2</sub>	4.	Equivalent Allowable 96.8 lb/hour	Emissions: 264.6 tons/year
5.	Method of Compliance: EPA Method 10			
6.	Allowable Emissions Comment (Description Maximum hourly rate based on natural gas-full load. Annual emission rate based on natural of 2,598,800 MMBtu/yr of duct firing at 59°F a Refer to Part B.	iring ural :	in CT and duct burner gas-firing with a maximu	um heat input rate
Al	lowable Emissions Allowable Emissions 2 o	f <u>2</u>		
1.	Basis for Allowable Emissions Code: OTHER	2.	Future Effective Date (Emissions:	of Allowable

# OTHER Emissions: 4. Equivalent Allowable Emissions: 142.9 lb/hour 143.9 tons/year 5. Method of Compliance: EPA Method 10; Initial; Annual >400 hr/yr. 6. Allowable Emissions Comment (Description of Operating Method): Maximum hourly rate based on distillate oil-firing in CT and duct burner (gas) at 25°F and full load. Annual emission rate based on maximum heat input rate of 6,926,500 MMBtu/yr (equivalent to 3,500 hours) of distillate oil-firing of CT at 59°F and full load. 17.7 ppmvd at 15% O₂ for CT only. Refer to Part B.

#### 

POLLUTANT DETAIL INFORMATION
Page [5] of [5]
Volatile Organic Compounds

## F1. EMISSIONS UNIT POLLUTANT DETAIL INFORMATION – POTENTIAL/ESTIMATED FUGITIVE EMISSIONS

(Optional for unregulated emissions units.)

#### Potential/Estimated Fugitive Emissions

Complete for each pollutant identified in Subsection E if applying for an air construction permit or concurrent processing of an air construction permit and a revised or renewal Title V permit. Complete for each emissions-limited pollutant identified in Subsection E if applying for an air operation permit

applying for an air operation permit.			
1. Pollutant Emitted:	2. Total Perc	ent Efficie	ency of Control:
VOCs			
3. Potential Emissions:		4. Synth	netically Limited?
<b>17.1</b> lb/hour <b>47</b> .	4 tons/year	⊠ Y€	es 🗌 No
5. Range of Estimated Fugitive Emissions (as	applicable):		
to tons/year			
6. Emission Factor:			7. Emissions
			Method Code:
Reference: See Part B, Air Permit Ap	plication Report		0
8.a. Baseline Actual Emissions (if required):	8.b. Baseline	24-month	Period:
19.7 tons/year	From: 1/1/2004	4 To: 12/3	31/2005
9.a. Projected Actual Emissions (if required):	9.b. Projected	Monitorii	ng Period:
tons/year	☐ 5 yea	urs 🔲 10	years
10. Calculation of Emissions:  Maximum hourly rate based on full-load oil Annual emissions based on an equivalent 5 heat input rate of 2,598,800 MMBtu/yr for o (equivalent to 3,500 hours) of distillate oil-f Part B.	,260 hours of na luct firing at ful iring in the CT	atural gas I load and at full load	firing with maximum 6,926,500 MMBtu/yr
11. Pollutant Potential/Estimated Fugitive Emis See Section 2.0 of Part B and Appendix A for and loads.			mbient temperatures

POLLUTANT DETAIL INFORMATION
Page [5] of [5]
Volatile Organic Compounds

## F2. EMISSIONS UNIT POLLUTANT DETAIL INFORMATION - ALLOWABLE EMISSIONS

Complete if the pollutant identified in Subsection F1 is or would be subject to a numerical emissions limitation.

Allowable Emissions	Allowable	Emissions :	1 of 2
			$\overline{}$

1.	Basis for Allowable Emissions Code:  OTHER	2.	Future Effective Date of Emissions:	of Allowable
3.	Allowable Emissions and Units: 5.7 ppmvd @ 15% O <sub>2</sub> for CT and HRSG	4.	Equivalent Allowable 16.7 lb/hour	Emissions: 46.8 tons/year
5.	Method of Compliance: EPA Method 25A, Initial performance test only	1.		
	Allowable Emissions Comment (Description Maximum hourly rate based on natural gas-fir Annual emission rate based on natural ga 2,598,800 MMBtu/yr of duct firing at 59°F an Refer to Part B.	ring as-fi d fu	in CT and duct burner at ring with a maximum	heat input rate of
All	lowable Emissions Allowable Emissions 2 of	f <u>2</u>		
1.	Basis for Allowable Emissions Code: OTHER	2.	Future Effective Date of Emissions:	of Allowable
3.	Allowable Emissions and Units: 5.3 ppmvd @ 15% O <sub>2</sub> for CT and DB	4.	Equivalent Allowable   17.1 lb/hour	Emissions: 13.1 tons/year
5.	Method of Compliance: EPA Method 25A, Initial performance test only	1		
6.	Allowable Emissions Comment (Description Maximum hourly rate based on distillate oil-full load. Annual emission rate based on ma (equivalent to 3,500 hours) of distillate oil-firing	irinç xim	in CT and duct burner um heat input rate of 6,9	926,500 MMBtu/yr
All	lowable Emissions Allowable Emissions	c	f	
1.	Basis for Allowable Emissions Code:	2.	Future Effective Date of Emissions:	f Allowable
3.	Allowable Emissions and Units:	4.	Equivalent Allowable I lb/hour	Emissions: tons/year
5.	Method of Compliance:			
6.	Allowable Emissions Comment (Description	of (	Operating Method):	

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#### G. VISIBLE EMISSIONS INFORMATION

Complete if this emissions unit is or would be subject to a unit-specific visible emissions limitation.

Visible Emissions Limitation: Visible Emissions Limitation 1 of 1

		· · · · · · · · · · · · · · · · · · ·	
1.	Visible Emissions Subtype: VE10	<ul><li>2. Basis for Allowable</li><li>☑ Rule</li></ul>	Opacity:  Other
3.	Allowable Opacity: Normal Conditions:  10 % Ex Maximum Period of Excess Opacity Allower	ceptional Conditions: ed:	100 % 60 min/hour
4.	Method of Compliance: EPA Method 9	•	
5.	Visible Emissions Comment: Rule 62-296.320 (4) (b). Excess emissions. F	Refer to Part B.	
Vi:	sible Emissions Limitation: Visible Emission	ons Limitation of _	
1.	Visible Emissions Subtype:	2. Basis for Allowable	Opacity:
		☐ Rule	☐ Other
	Allowable Opacity: Normal Conditions: % Ex Maximum Period of Excess Opacity Allower	ceptional Conditions:	Other  % min/hour
3.	Normal Conditions:  % Ex	ceptional Conditions:	%
<ol> <li>4.</li> </ol>	Normal Conditions: % Ex Maximum Period of Excess Opacity Allowe	ceptional Conditions:	%

#### H. CONTINUOUS MONITOR INFORMATION

Complete if this emissions unit is or would be subject to continuous monitoring.

Continuous Monitoring System: Continuous Monitor 1 of 2

1.	Parameter Code: EM	2.	Pollutant(s): NO <sub>x</sub>		
3.	CMS Requirement:	$\boxtimes$	Rule	Other	
4.	Monitor Information Manufacturer: TBD				
_	Model Number: TBD		Serial Number: TBD		
5.	Installation Date:	6.	Performance Spec	ification Test Date:	
	TBD = To be determined. CEM required pursu				
Continuous Monitoring System: Continuous Monitor 2 of 2					
1.	Parameter Code: O <sub>2</sub> or CO <sub>2</sub>		Pollutant(s):     Oxygen or Carbon Dioxide		
3.	CMS Requirement:	$\boxtimes$	Rule	Other	
4.	Manufacturer: TBD				
	Model Number: TBD		Serial Number: TBD		
5.	Installation Date:		6. Performance S	pecification Test Date:	
7.	Continuous Monitor Comment: Diluent monitor required pursuant to 40 CFR	Part	75 for NO <sub>x</sub> monitor	ing.	

#### **EMISSIONS UNIT INFORMATION**

Section [1] GE 7FA and Duct Burner

#### I. EMISSIONS UNIT ADDITIONAL INFORMATION

#### Additional Requirements for All Applications, Except as Otherwise Stated

1.	revision applications if this information was submitted to the department within the previous five years and would not be altered as a result of the revision being sought)  Attached, Document ID: Part B Previously Submitted, Date		
2.	operation permit revision applications if this information was submitted to the department within the previous five years and would not be altered as a result of the revision being sought)  Attached, Document ID: Part B Previously Submitted, Date		
3.	V air operation permit revision applications if this information was submitted to the department within the previous five years and would not be altered as a result of the revision being sought)  Attached, Document ID: Part B Previously Submitted, Date		
4.	Procedures for Startup and Shutdown (Required for all operation permit applications, except Title V air operation permit revision applications if this information was submitted to the department within the previous five years and would not be altered as a result of the revision being sought)  Attached, Document ID: Previously Submitted, Date  Not Applicable (construction application)		
5.			
6.	Compliance Demonstration Reports/Records  Attached, Document ID: Test Date(s)/Pollutant(s) Tested:		
	Previously Submitted, Date: Test Date(s)/Pollutant(s) Tested:		
	To be Submitted, Date (if known): Test Date(s)/Pollutant(s) Tested:		
	☑ Not Applicable		
	Note: For FESOP applications, all required compliance demonstration records/reports must be submitted at the time of application. For Title V air operation permit applications, all required compliance demonstration reports/records must be submitted at the time of application, or a compliance plan must be submitted at the time of application.		
7.	Other Information Required by Rule or Statute  Attached, Document ID: Not Applicable		

# **EMISSIONS UNIT INFORMATION**

Section [1]
GE 7FA and Duct Burner

# Additional Requirements for Air Construction Permit Applications

1.	Control Technology Review and Analysis (Rules 62-212.400(6) and 62-212.500(7),
	F.A.C.; 40 CFR 63.43(d) and (e))
	☐ Attached, Document ID: Part B ☑ Not Applicable
2.	Rule 62-212.500(4)(f), F.A.C.)
	☐ Attached, Document ID: Part B ☑ Not Applicable
3.	Description of Stack Sampling Facilities (Required for proposed new stack sampling facilities only)
Ac	Iditional Requirements for Title V Air Operation Permit Applications
1.	Identification of Applicable Requirements
	☐ Attached, Document ID: ⊠ Not Applicable
2.	Compliance Assurance Monitoring
	☐ Attached, Document ID: ⊠ Not Applicable
3.	Alternative Methods of Operation
	☐ Attached, Document ID: ⊠ Not Applicable
4.	Alternative Modes of Operation (Emissions Trading)
	☐ Attached, Document ID: ⊠ Not Applicable
5.	Acid Rain Part Application
	Certificate of Representation (EPA Form No. 7610-1)
	Copy Attached, Document ID:
	Acid Rain Part (Form No. 62-210.900(1)(a))
	☐ Attached, Document ID:  ☑ Previously Submitted, Date:
	Repowering Extension Plan (Form No. 62-210.900(1)(a)1.)
	Attached, Document ID:
	Previously Submitted, Date:
	☐ New Unit Exemption (Form No. 62-210.900(1)(a)2.)
	Attached, Document ID:
	Previously Submitted, Date:
	Retired Unit Exemption (Form No. 62-210.900(1)(a)3.)
	☐ Attached, Document ID: ☐ Previously Submitted, Date:
	Phase II NOx Compliance Plan (Form No. 62-210.900(1)(a)4.)
	Attached, Document ID:
	Previously Submitted, Date:
	Phase II NOx Averaging Plan (Form No. 62-210.900(1)(a)5.)
	Attached, Document ID:
	☐ Previously Submitted, Date:
	☐ Not Applicable

# Additional Requirements Comment

EMISSIONS UNIT INFORMATION

Section [1] GE 7FA and Duct Burner

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PART B

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Appendix A EXPECTED PERFORMANCE AND EMISSION INFORMATION FOR THE COMBUSTION TURBINE AND DUCT BURNER

# 1.0 INTRODUCTION

The City of Tallahassee proposes to repower the Arvah B. Hopkins Generating Station Unit No. 2, located in Leon County, Florida (see Figure 2.1-1 of the Report for the modification to the Site Certification). The repowering of Unit No. 2 will include the addition of one nominal 188-megawatt (MW) combustion turbine and the permanent shut down of the fossil fuel steam generator for Unit 2. The repowering will enhance the City's electric system reliability and help the City meet the current forecasts of growth in population and electric demand.

The Arvah B. Hopkins Generating Station is an existing generating facility presently comprised of two steam electric generating units (Units 1 and 2), two Westinghouse combustion turbines (CTs) (referred to as GT-1 and GT -2), and two General Electric (GE) LM6000 CTs (referred to as GT -3 and GT -4). GT -3 and GT -4 began operation in 2005.

The proposed combined cycle unit will consist of one GE 7FA CT and associated electric generator, heat recovery steam generator (HRSG), and the existing steam turbine-electric generator. The unit will be equipped with a bypass stack that will be used with natural gas firing only. Together, these facilities are referred to as the "Project".

The proposed CT will use dry low-nitrogen oxides [(NO<sub>x</sub>) DLN] combustion technology when operating on natural gas and water injection for NO<sub>x</sub> control when operating on distillate fuel oil. The CT/HRSG will be installed with selective catalytic reduction (SCR) to further reduce emissions of NO<sub>x</sub>. The HRSG will be equipped with duct burners that will fire natural gas.

The CT will operate a maximum of 8,760 hours per year. The CT will operate up to an equivalent of 3,500 hours per year on distillate fuel oil at full-load operating. Existing transmission and fuel supply facilities are adjacent to the proposed location of the new CT.

The Project will be a minor modification to an existing major air pollution source and requires review under the Department's air construction permit rules. Because the Project is being constructed at a certified site under the Florida Power Plant Siting Act (PPSA), a modification to the site certification is also required. The U.S. Environmental Protection Agency (EPA) and the Florida Department of Environmental Protection (FDEP) have implemented regulations requiring a Prevention of Significant Deterioration (PSD) review for new major sources or major modifications at major sources that increase air emissions above certain threshold amounts. Because the proposed

modification will not exceed the major modification threshold amounts, the Project is not subject to PSD review.

Leon County, Florida, has been designated as an attainment or unclassifiable area for all criteria pollutants [i.e., attainment: ozone (O<sub>3</sub>); sulfur dioxide (SO<sub>2</sub>); carbon monoxide (CO); and nitrogen dioxide (NO<sub>2</sub>); unclassifiable: particulate matter with an aerodynamic diameter of 10 microns or less (PM<sub>10</sub>) and lead] and is a PSD Class II area for PM<sub>10</sub>, SO<sub>2</sub>, and NO<sub>2</sub>. Therefore, the preconstruction minor modification review will follow regulations pertaining to such designations.

The air permit application is divided into three major sections:

- Section 1.0 is an introduction to the Project.
- Section 2.0 presents a description of the Project, including air emissions and stack parameters.
- Section 3.0 provides a review of the regulatory requirements applicable to the Project.

# 2.0 PROJECT DESCRIPTION

# 2.1 Site Description

The Arvah B. Hopkins Generating Station consists of approximately 232 acres and is presently comprised of two steam electric generating units (Units 1 and 2), two Westinghouse CTs (GT -1 and GT -2), and two GE LM6000 CTs (GT -3 and GT -4). The steam electric units and the CTs use oil, natural gas, and/or liquefied petroleum gas as fuel. Unit 1, which went into service in 1971, is a nominal 75-MW unit. Unit 2, which went into service in 1977, is a nominal 238-MW unit. The existing CT, HC-1, went into service in 1970 and has a nominal generating capacity of approximately 16.5 MW (nominal). The existing CT, GT -2, went into service in 1972 and has a generating capacity of approximately 25 MW (nominal). The LM6000 CTs, GT-3 and GT-4, use natural gas and distillate fuel oil. Both GT-3 and GT-4 went into service in 2005 and have a total generating capacity of approximately 94 MW (net summer rating).

The plant site is bounded by Geddie Road to the west, CSX railroad to the east, State Road 20 to the south and U.S. Highway 90. The plant elevation will be approximately 136 feet above mean sea level (ft-msl). The terrain surrounding the site is gently rolling hills.

# 2.2 Unit No. 2 Repowering Project

# 2.2.1 Shutdown of Existing Unit No. 2 Boiler

The City of Tallahassee proposes to repower existing Unit No. 2 with one combined-cycle CT with a duct burner. The repowering Project will result in the permanent shutdown of the Unit No. 2 boiler and replaced with a new combined cycle unit.

# 2.2.2 Proposed Unit

The proposed CT will be configured as a combined-cycle unit. The combined cycle unit will consist of one GE Frame 7FA CT with an associated HRSG, and the existing Unit 2 steam turbine-electric generator. The CT will use DLN combustion technology when firing natural gas and water injection when firing light oil to minimize NO<sub>x</sub> formation. SCR will be installed in the HRSG to further reduce emissions of NO<sub>x</sub>. The unit may operate in simple cycle mode; however, the exhaust gases will be routed through the HRSG and SCR system, with the same emissions achieved as those for the combined cycle mode. Natural gas and light oil will be used an alternative fuels.

In the event of a major unplanned forced outage of the HRSG or to the steam turbine, the electrical output associated with the CT would not be available to meet system reliability needs without an alternative to routing steam through the HRSG. To mitigate the system reliability impacts from such a major unplanned forced outage event, an emergency HRSG bypass system be installed as a part of the Project. The bypass stack would be physically inoperable during combined cycle operations. To utilize the bypass stack, the unit would have to be removed from service, a "blanking plate" in the duct would have to be physically removed, and a HRSG blanking plate would have to be installed. Since this would be for emergency bypass use only, the bypass stack would not be equipped with a SCR. During these emergency situations, the City would propose that the unit operate on natural gas only. Compliance with this mode of operation would be demonstrated using the NO<sub>x</sub> CEMs without the SCR operating.

Plant performance for the GE 7FA CT was developed for natural gas and oil at 100-, 75-, and 60-percent load and 25, 59, and 95 degrees Fahrenheit (°F) ambient dry bulb temperatures, respectively. Nominal part load percentages herein are relative to 100-percent load without evaporative cooling.

For the CT, the maximum heat input is 1,899 MMBtu/hr (HHV) or 1,711 MMBtu/hr (LHV) when firing natural gas (100-percent capacity, 25°F). For fuel oil firing, the maximum heat input is 2,079 MMBtu/hr (HHV) or 1,961 MMBtu/hr (LHV) (100-percent capacity, 25°F).

The HRSG will be equipped with a duct burner with a maximum heat input of 712 MMBtu/hr (HHV) when firing natural gas at 59 °F. The duct burner has a maximum heat input of 765 MMBtu/hr (HHV) when firing natural gas at 25°F.

The CT will use DLN combustion technology (when firing natural gas) and water injection (when firing distillate oil) to minimize NO<sub>x</sub> formation. SCR will be installed in the HRSG to further reduce emissions of NO<sub>x</sub>.

The SO<sub>2</sub> emissions will be controlled by the use of low-sulfur fuels. Good combustion practices and clean fuels will also minimize potential emissions of PM, CO, volatile organic compounds (VOC), and other pollutants (e.g., trace metals).

SCR reactors for the unit-will be-located in the HRSG to provide the proper operating temperature range for the required reaction between ammonia and NOx to achieve the proposed emission rate and

to assure the economical operation of the system. The  $NO_x$  is reduced by a chemical reaction with the ammonia in the presence of the catalyst. Ammonia is carried by a diluent and injected into the exhaust gas upstream of the catalyst modules. The ammonia reacts with  $NO_x$  on the surface of the catalyst to form nitrogen and water.

Natural gas is currently available at the Hopkins facility. As such, there will be minimal additional infrastructure required to support additional natural gas delivery to the site. The Hopkins facility currently has two existing 10,000 bbl diesel storage tanks and two #6 fuel oil tanks (55,000 bbl and 180,000 bbl). The City plans on converting the 180,000 bbl tank to diesel storage. The existing diesel storage tanks and the converted #6 fuel oil tank will be used for the Project, and no new fuel oil tanks will be required.

# 2.3 Proposed Source Emissions and Stack Parameters

# 2.3.1 Shutdown of Existing Unit No. 2

The permanent shutdown of the Unit No. 2 boiler will result in emission reductions. These emission reductions are used in the netting analysis for determination of PSD applicability of the Project (see Section 3.0).

To determine the bascline past actual emissions for the existing Unit No. 2, the highest emissions over a consecutive 24-month period in the last 5 years were utilized. This analysis was conducted on a pollutant-by-pollutant basis and is presented in Tables 2-1 through 2-3. The PM/PM<sub>10</sub>, CO, VOC, and lead emissions are presented in Table 2-1 and are based on fuel usage from the annual operating reports (AORs) reported to the FDEP and the latest AP-42 emission factors for natural gas and fuel oil combustion. These data are presented from 2001 to 2005 and are based on annual emissions estimated for each calendar year. The SO<sub>2</sub> and NO<sub>x</sub> emissions are presented in Tables 2-2 and 2-3, respectively, and are based on data recorded by the continuous emission monitor system (CEMS). These data are presented on a monthly basis from March 2001 to February 2006 since the CEMS data are available monthly.

For PM/PM<sub>10</sub>, VOC, lead, and mercury emissions, the highest annual average emissions occurred over the 24-month period from 2004 to 2005. For CO emissions, the highest annual average emissions occurred over the 24-month period from 2001 to 2002. For SO<sub>2</sub> emissions, the highest annual average emissions from the CEM data occurred over the 24-month period from February 2004 to January 2006. For NO<sub>x</sub> emissions, the highest annual average emissions from the CEM data

occurred over the 24-month period from May 2003 to April 2005. The annual average emission rates for those years were used to represent the actual annual average emissions for those pollutants.

# 2.3.2 Proposed Unit

The maximum estimated hourly emission rates of regulated pollutants for combined cycle operation for the CT/HRSG with and without the duct burner when firing natural gas and distillate oil at baseload conditions are presented in Tables 2-4 and 2-5, respectively. The maximum estimated hourly emission rates when the CT is firing distillate oil and the duct burner is firing natural gas are also presented in Table 2-5. The same emission rates will be achieved during simple cycle operation when the exhaust gases are routed through the HRSG and SCR system. The maximum estimated hourly emission rates of regulated pollutants for simple cycle operation when the exhaust gases are routed through the emergency bypass stack, instead of the HRSG and SCR system, are presented in Table 2-6. Only natural gas will be fired when the emergency bypass stack is used. The primary pollutants emitted by the CT/HRSG will be NO<sub>x</sub>, CO, SO<sub>2</sub>, PM, and VOC.

The maximum estimated hourly emission rates and exhaust information representative of the CT/HRSG and duct burner were determined using the manufacturer's information for the equipment proposed for the Project. The design parameters were provided for operating loads of 100- (baseload), 75-, and 60-percent capacity and for ambient temperatures of 25, 59, and 95°F, respectively. The performance and emissions data for the operating conditions are given in Appendix A for turbine inlet temperatures of 25, 59, and 95°F and various operating conditions (100-percent load and low-load operation applicable for the CT).

As shown in Tables 2-4 through 2-6, the maximum short-term emission rates [pounds per hour (lb/hr)] for base load conditions occur at 25°F operations when the CT has the greatest output and greatest fuel consumption.

The maximum potential annual emissions for the repowered unit are presented in Table 2-7. Annual emissions were based on emissions expected for baseload and ambient temperatures of 59°F. The maximum annual emissions are based on the range of operations that could occur with operating the CT on natural gas and distillate oil and the CT, operating with the duct burners firing natural gas. In addition, the maximum annual emissions were estimated for the CT operating in simple cycle mode ... with the exhaust to an emergency-bypass stack (bypass stack-would not be equipped with a SER).

The annual operation of the repowered unit will be limited so that the net emission increase of all pollutants will be less than the PSD significant emission rates. The allowable annual operation was determined from an analysis of the emissions for various operating scenarios. These scenarios are reflected in the range of operating hours and fuels (natural gas and distillate oil) shown in Table 2-7 for CT operating alone and the CT operating with maximum duct firing. The operating envelope being proposed consists of four parts that are discussed below:

- 1. CT operation mode when firing natural gas in combined cycle or simple cycle mode with the exhaust gases routed through the HRSG and SCR system is not limited (see Operating Scenarios A and E in Table 2-7). CT operation in simple cycle mode with the emergency bypass stack will be limited to natural gas firing. The emissions during this operational mode are not higher than those in the combined cycle mode for any pollutant except for NO<sub>x</sub>. NO<sub>x</sub> emissions in this mode are not limiting based on the netting analysis described in Section 3.0 and shown as Operating Scenario E in Table 2-7.
- 2. Duct firing with natural gas is proposed to be limited to 2,598,800 MMBtu/yr (HHV), which is equivalent to 3,650 hours at the maximum duct firing rate of 712 MMBtu/hr (see Operating Scenario B).
- 3. The maximum amount of distillate oil firing in the CT is proposed to be limited to 6,926,500 MMBtu/yr, which is equivalent to 3,500 hours at full load as shown in Table 2-7 as Operating Scenarios C and D.

The potential annual emissions are based on the 59°F turbine inlet temperature at 100-percent load condition, which is conservative since the annual average temperatures for the Tallahassee area are slightly higher than 70°F. Higher turbine inlet temperatures result in lower turbine performance and lower mass emissions. The conservative nature of the turbine inlet temperature combined with a 100-percent capacity factor (i.e., 8,760 hours per year at full load) result in worst-case emissions estimates.

Emission factors for hazardous air pollutants (HAPs) were evaluated based on the revised AP-42 emission factors, the EPA Combustion Turbine Emissions Database, and the CT Maximum Achievable Control Technology (MACT) standards. The HAP emissions are based on emission factors from the April 2000 revision of EPA's AP-42 emission factors for large stationary CTs. Summaries of the emission factors and emissions for light oil-firing and gas-firing are presented in Appendix A.

The MACT standard in 40 CFR, Subpart YYYY, is potentially applicable to the Project. The HAPs emissions from the Project will be less than 10 tons per year (TPY) for any single HAP and less than 25 TPY for all HAPs. However, the Hopkins Plant is a major source of HAP emissions since emissions exceed 10 TPY of a single HAP and exceed 25 TPY for all HAPs and will remain a major source of HAPs after the repowering project. Since low-sulfur light oil is proposed to be fired in the proposed CT, the proposed CT is defined as "stationary diffusion flame oil-fired combustion turbines" under the Subpart YYYY requirements. The Project, combined with two other CTs at the Hopkins facility, would have the potential for an aggregate total potential of 1,000 hours or more of oil firing during any calendar year. Actual applicability of Subpart YYYY is based on actual oil fuel used in a calendar year. The proposed Project will be required to demonstrate compliance with the CT MACT of 91-parts per billion by volume, dry (ppbvd) formaldehyde, corrected to 15-percent oxygen, if the aggregate 1,000 hours per year is exceeded. Based on the applicability of Subpart YYYY, compliance will be determined upon initial operation and annually (40 CFR Part 63, Section 63.6120, Table 3).

An emission factor for toluene of 33 pounds (lb)/10<sup>12</sup> British thermal units (Btu) for natural gas firing, was developed from the data in the EPA Combustion Turbine Emissions Database. This factor is based on the median value for loads greater than 80 percent. Similar to formaldehyde emission factors, there are no confirmed test data of toluene emissions from F Class turbines. The recent EPA emission factor, which is based on much smaller turbines than those proposed for the Project, suggests toluene emissions from gas turbines of 130 lb/10<sup>12</sup> Btu when firing natural gas at loads greater than 80 percent. For all loads, the average and median EPA factors are 94 and 19 lb/10<sup>12</sup> Btu, respectively. Since the median emission factor is about 4 to 5 times lower than the average factor, this clearly points to the large range in toluene emissions and how the individual CT characteristics can influence the results.

The emission factors for many of the other HAPs were developed by EPA in a manner similar to toluene. For these HAPs, fewer data are available and are also considered not representative of state-of-the-art DLN combustion systems. The use of AP-42 emission factors for HAPs is considered to provide conservative estimates of emissions.

The GE 7FA CT with SCR will experience excess emissions during the short startup and shutdown periods for NO<sub>x</sub> and may experience excess emissions for other pollutants. The conservative turbine inlet temperature combined with the assumption of 100-percent capacity factor provides maximum

potential emissions that would envelope operation including any excess emissions from startups and shutdowns.

# 2.4 Site Layout, Structures, and Stack Sampling Facilities

A site plan of the proposed Project is presented in Figure 2.1-2 (see the Report for the modification to the Site Certification) and a process flow diagram is presented in Figure 2-1. Stack sampling facilities will be constructed in accordance to Rule 62-297.310(6), F.A.C.

TABLE 2-1
ESTIMATED ACTUAL ANNUAL PM/PM<sub>16</sub>, CO, VOC, LEAD, AND MERCURY EMISSIONS FOR THE EXISTING HOPKINS UNIT 2 WITH LATEST AP-42 EMISSION FACTORS

	- Units						
Pollutant		2001	2002	2003	2004	2005	Maximum 2-year Perio
Total Emission	<u>s</u>					· • •	· <u> </u>
PM	TPY	32.2	26.3	111.1	126.2	146.5	136.3
PM <sub>10</sub>	TPY	24.3	20.2	79.2	90.4	104.7	97.5
со	TPY	233.8	248.4	181.2	252.8	194.1	241.1
VOC	TPY	16.3	17.0	16.6	21.7	17.7	19.7
Lead	TPY	0.0046	0.0040	0.017	0.019	0.018	0.019
Mercury	TPY	0.00032	0.00026	0.00127	0.00140	0.00135	0.0014
Residual Oil (C	Grade 6) *						
PM	TPY	27.2	20.9	108.2	121.8	143.4	
PM <sub>10</sub>	TPY	19.3	14.8	76.4	86.0	101,6	
CO	TPY	11.0	8.4	54.5	59.1	57.8	
voc ,	ŢPY .	1.7	1.3	8.3	9.0	8.8	
Lead	TPY	0.0033	0.0025	0.016	0.018	0.017	
Mercury	ТРҮ	0.00025	0.00019	0.00123	0.00134	0.00131	
S content	percent	i	1	0 73	0 77	1	
Fuel usage	1,000 gal/yr	4,383.20	3,367.20	21,799.08	23,658.40	23,109.50	
Natural Gas b	,		<u> </u>				
PM	TPY	5.0	5.4	2.9	4,4	3.1	
$PM_{10}$	ТРҮ	5.0	5.4	2.9	4.4	3.1	
CO	TPY	222.9	239.9	126.7	193.7	136.3	
VOC	TPY	14.6	15.7	8.3	12.7	8.9	
Lead	ТРҮ	0.0013	0.0014	0 0008	0.0012	0.0008	
Mercury	TPY	0.00007	0.00007	0 00004	0.00006	0.00004	
Fuel usage	million cubic fl/yr	5,306.81	5,712.80	3,016.04	4,611.60	3,245.20	

<sup>\*</sup> Emission factors for residual fuel oil (AP-42, Section 1.3, 9/98)

lb/1,000 gal	$(9.19 \times S) + 3.22$	(Filterable only)
lb/1,000 gal	$5.9 \times [(1.12 \times S) + 0.37]$	(Filterable only)
lb/1,000 gal	5.0	• • • • • • • • • • • • • • • • • • • •
lb/1,000 gal	0.76	
1b/1,000 gal	0.00151	
lb/1,000 gal	0.000113	
	ib/1,000 gal lb/1,000 gal lb/1,000 gal lb/1,000 gal	1b/1,000 gal   5.9 x [(1.12 x S) + 0.37]   1b/1,000 gal   5.0   1b/1,000 gal   0.76   1b/1,000 gal   0.00151

<sup>&</sup>lt;sup>h</sup> Emission factors for natural gas (AP-42, Section 1.4, 3/98)

PM	lb/mmcf	1.9	(Filterable only)
$PM_{10}$	lb/mmcf	1.9	(Filterable only)
CO	lb/mmcf	84	
VOC	lb/mmcf	5.5	
Lead	lb/mmcf	0.0005	
Mercury	lb/mmcf	-0.000026	

TABLE 2-2 ACTUAL SO<sub>2</sub> EMISSIONS FOR THE EXISTING HOPKINS UNIT 2 BASED ON CEMS DATA

		SO <sub>2</sub> Emissions					
		T	Tons/year (TPY) Tons/month (TPM) Average 24 months				
Year	Month	Oil	Gas	TOTAL	Average 24 months Consecutive		
aximum				438	1642		
2001	Mar	0	. 0	•			
2001	Apr	0	0.06	0 0.06	NA NA		
	May	Ö	0.28	0.28	NA NA		
	Jun	Ö	0.27	0.27	NA NA		
	Jul	Ö	0.31	0.31	NA NA		
	Aug	15.93	0.28	16.21	NA NA		
	Sep	13.64	0.23	13.87	NA.		
	Oct	0	0	0	NA NA		
	Nov	0	0	0	NA		
	Dec	0	0.03	0.03	NA		
2002	Jan	36.95	0.07	37.02	NA		
	Feb	0	0	0	NA		
	Mar	0	0.03	0.03	NA		
	Арг	0	0.22	0.22	NA		
	May	87.61	0.13	87.74	NA		
	Jun	4.42	0.22	4.64	NA		
	Jul	0	0.26	0.26	NA		
	Aug	0	0.26	0.26	NA		
	Sep	4.9	0.2	5.1	NA		
	Oct	51 44	0.07	51.51	NA		
	Nov	24.64	0.17	24.81	NA		
2003	Dec	0	0.18	0.18	NA		
.003	Jan Feb	90.14 2.31	0.07	90.21	NA 168		
	Mar	2.31 84.51	0.01 0.11	2.32	168		
	Apr	0	0.11	84.62	210		
	May	189.66	0.03	0.03 189.74	210		
	Jun	181.58	0.09	181.67	305 395		
	Jul	183.92	0.09	184.02	395 487		
	Aug	212.51	0.08	212.59	585		
	Sep	112.8	0.14	112.94	635		
	Oct	59.11	0.2	59.31	665		
	Nov	0	0.01	0.01	665		
	Dec	194.67	0.02	194.69	762		
004	Jan	135.3	0.04	135.34	811		
	Feb	70.44	0.16	70.6	846		
	Mar	84.04	0.17	84.21	889		
	Apr	66.43	0.17	66.6	922		
	May	123.79	0.19	123.98	940		
	Jun	134.84	0.16	135	1005		
	Jul	155.65	0.12	155.77	1083		
	Aug	170.1	0.11	170.21	1168		
	Sep	183.31	0.08	183.39	1257		
	Oct	194.54	0.09	194.63	1328		
	Nov	44.04	0.08	44.12	1338		
	Dec	128.77	0.03	128.8	1402		
2005		115.66	0.02	115.68	1415		
	Feb	150.79	0.01	150.8	1489		
	Mar	29.15	0.01	29.16	1462		
	Apr May	265.29 12.7	0	265.29	1594		
	May Jun		0.21	12.91	1506		
	Jul Jul	34.93 101.54	0.18	35 11	1433		
	Aug	276.69	0.18 0.09	101.72	1391		
	Nug Sep	103.71	0.09	276.78 103.85	1424		
	Oct	105.71	0.14	97.0	1419		
	Nov	-		29.7	1438 1453		
	Dec			- 438.4 ··· ···			
2006		-	-	270.2	1642		
	Feb			14.2	1074		

TABLE 2-3
ACTUAL NO, EMISSIONS FOR THE EXISTING HOPKINS UNIT 2
BASED ON CEMS DATA

	_	NO, Em	
Year 	Month	Tons/month (TPM) TOTAL	Tons/year (TPY) Average 24 months Consecutive
Maximu	m	131	843
	Mar	0.00	NA
	Apr	22.43	NA
	May	91.98	NA NA
	Jun Jul	83.45 99.49	NA NA
	Aug	131.33	NA NA
	Sep	70.79	NA
	Oct	0.93	NA
	Nov	0.00	NA
	Dec	7.62	NA
200	2 Jan	36.00	NA
	Feb	0.00	NA NA
	Mar	11.55 99.18	NA NA
	Apr May	71.81	NA NA
	Jun	56.04	NA NA
	Jul	73.79	NA
	Aug	75.77	NA
	Sep	60.50	NA
	Oct	39.19	NA
	Nov	45.23	NA NA
200	Dec 3 Jan	30.12 52.94	NA NA
200	Feb	3.40	582
	Mar	52.18	608
	Apr	3.72	599
	May	76.00	591
	Jun	96.32	597
	Jul	88.72	592
	Aug	99.95 79.38	576 580
	Sep Oct	72.05	616
	Nov	1.31	. 616
	Dec	81.19	653
200	)4 Jan	60.74	666
	Feb	60.16	696
	Mar	79.11	729
	Apr May	78.72 124.15	719 745
	Jun	124.15 101.11	768
	Jul	79.76	77 <b>I</b>
	Aug	79.86	773
	Sep	85.54	785
	Oct	95.74	814
	Nov	24.06	803
200	Dec	44.57	810
200	)5 Jan Feb	48.36 47.05	808 830
	reo Mar	47.05 10.67	830 80 <del>9</del>
	Apr	72.16	843
	May	44.70	828
	Jun	46 56	803
	Jul	81.39	799
	Aug	114.19	806
	Sep	46.85	790
	Oct Nov	2.07 0.61	755 755
	Dec Dec	14.10	= 155 721 — —
200	16 Jan	1.32	691
	Feb	0.67	662

TABLE 2-4
STACK, OPERATING, AND EMISSION DATA FOR THE PROPOSED HOPKINS UNIT 2 REPOWERING PROJECT
FOR NATURAL GAS-FIRING FOR BASELOAD COMBINED CYCLE OPERATIONS

		Natural Gas-Firing <sup>a</sup>						
			CT Only	CT with Duct Burner on Gas				
Parameter	Units	25 °F	59 °F	95 °F	25 °F	59 °F	95 °F	
Combustion Turbine Performance			<del>-</del>					
Net power output (MW)	MW	187.8	174.4	160.3	187.8	174.4	160.3	
Net heat rate	Btu/kWh, LHV	9,110	9,270	9,495	9,110	9,270	9,495	
	Btu/kWh, HHV	10,112	10,290	10,539	10,112	10,290	10,539	
Heat Input	MMBtu/hr, LHV	1,711	1,617	1,522	1,711	1,617	1,522	
	MMBtu/hr, HHV	1,899	1,795	1,689	1,899	1,795	1,689	
Relative Humidity	%	87	78	50	87	78	50	
Fuel heating value	Btu/lb, LHV	20,714	20,714	20,714	20,714	20,714	20,714	
	Btu/lb, HHV	22,993	22,993	22,993	22,993	22,993	22,993	
Duct Burner								
Reat Input	MMBtu/hr, LHV	0.0	0.0	0.0	765	712	663	
	MMBtu/hr, HHV	0.0	0.0	0.0	689	641	597	
CT/HRSG Stack Data								
Height	ft	150	150	150	150	150	150	
Diameter	ft	18	18	18	18	18	18	
100 Percent Load								
Temperature (°F)	" <b>F</b>	203	202	201	189	188	190	
Velocity (ft/sec)	fl/sec	70.9	67.0	63.2	70.4	66.5	63.0	
Maximum Hourly Emissions								
SO <sub>2</sub>	lb/hr	10.47	9.90	9.32	14.7	13.8	13.0	
PM/PM <sub>10</sub>	lb/hr	Н.1	11.0	10.9	21.1	20.3	19.6	
NO <sub>x</sub>	lb/hr	34.3	32.4	30.5	47.8	45.0	42.2	
	ppmvd @ 15% O <sub>3</sub>	5	5	5	5	5	5	
CO	lb/hr	41.7	39.1	36.2	96.8	90.3	83.9	
	ppmvd	12.0	12.0	12.0	28.6	28.5	28.6	
	ppmvd @ 15% $O_2$	0.01	9.9	9.7	16.8	16.7	16.5	
VOC (as methane)	tb/hr	7.52	7.12	6.72	16.70	15.66	14.67	
	ppinvw	3.50	3.50	3.50	8.64	8.66	8.76	
	ppmvd @ 15% O <sub>2</sub>	3.15	3.16	3.16	5.67	5.71	5.80	
Lead	lb/hr	NA	NA	NA	- NA	NA	NA	
Sulfuric Acid Mist	lb/hr	1.05	0.99	0.93	1.89	1.77	1.66	

Refer to Appendix A for detailed information on basis of pollutant emission rates and operating data. Includes simple cycle operation with exhaust gases routed to the HRSG and SCR system.

Source: GE, 2006.

TABLE 2-5
STACK, OPERATING, AND EMISSION DATA FOR THE PROPOSED HOPKINS UNIT 2 REPOWERING PROJECT
FOR DISTILLATE OIL-FIRING FOR BASELOAD COMBINED CYCLE OPERATIONS WITH NATURAL GAS DUCT FIRING

		Distillate Oil-Firing *						
		CT Only			CT with Duct Burner on 6		r on Gas	
Parameter	Units	25 °F	59 °F	95 °F	25 °F	59 °F	95 °F	
Combustion Turbine Performance					,			
Power output (MW)	MW	198.9	187.9	172.4	198.9	187.9	172.4	
Heat rate	Btu/kWh, LHV	9,860	9,935	10,090	9,860	9,935	10,090	
real tusc	Btu/kWh, HII/V	10,452	10,531	10,695	10,452	10,531	10,695	
Heat Input	MMBtu/hr, LHV	1,961	1,867	1,740				
rical input	· · · · · · · · · · · · · · · · · · ·		1,979		1,961	1,867	1,740	
Delegan Francisco	MMBtu/hr, HHV	2,079		1,844	2,079	1,979	1,844	
Relative Humidity	%	87	78	50	87	78	50	
Fuel heating value	Btu/lb, LHIV	18,300	18,300	18,300	18,300	18,300	18,300	
·	Biwlb, HHV	19,398	19,398	19,398	19,398	19,398	19,398	
Duct Burner								
Heat Input	MMBtu/hr, LHV	0.0	0.0	0.0	765	712	663	
	MMBtu/hr, HHV	0.0	0.0	0.0	689	641	597	
CT/HRSG Stack Data								
Height	ft	150	150	150	150	150	150	
Diameter	ñ	18	18	18	18	18	18	
100 Percent Load								
Temperature (oF)	°F	248	248	247	206	204		
• • •	*					204	201	
Velocity (fl/sec)	ft/sec	79.5	75.1	70.3	75.8	71.4	66.6	
Maximum Hourly Emissions								
SO <sub>2</sub>	lb/hr	107	102	95	111	106	99	
PM/PM <sub>10</sub>	lb/hr	38.7	37.6	36.2	48.7	47.0	44.9	
NOx	lb/hr	81.4	77.5	72.2	108.4	102.6	95.6	
	ppmvd @ 15% O2	10.0	10.0	10.0	10.0	10.0	10.0	
co ·	lb/hr	87.8	82.2	76.1	142.9	133.4	123.8	
	ppmvd	25.0	25.0	25.0	41.9	41.8	41.9	
	ppmvd @ 15% O2	17.7	17.4	17.3	21.4	21.2	21.1	
VOC (as methane)	lb/hr	7,89	7.46	6.99	17.1	16.0	14.9	
,	ppmvw	3.5	3.5	3.5	7.6	7.5	7.5	
	ppmvd @ 15% O2	2.8	2.8	2.8	5.2	5.2	5.3	
Lead	lb/hr	0.029	0.028	0.026	0.029	0.028	0.026	
Sulfuric Acid Mist	lb/hr	21.4	20.4	19.0	22.3	21.2	19.7	

<sup>&</sup>lt;sup>a</sup> Refer to Air Construction Permit Application (Appendix 10.1.5) for detailed information on basis of pollutant emission rates and operating data. Includes simple cycle operation with exhaust gases routed to the HRSG and SCR system.

Source: GE, 2006

TABLE 2-6
STACK, OPERATING, AND EMISSION DATA FOR THE PROPOSED HOPKINS UNIT 2 REPOWERING PROJECT
FOR NATURAL GAS-FIRING FOR BASELOAD SIMPLE CYCLE OPERATIONS

		Natural Gas-Firing <sup>a</sup>				
		CT Only				
Parameter	Units	25 °F	59 °F	95 °F		
Combustion Turbing Performance						
Net power output (MW)	MW	187.8	174.4	160.3		
Net heat rate	Btu/kWh, LHV	9,110	9,270	9,495		
	Btu/kWh, HHV	10,112	10,290	10,539		
Heat Input	MMBtu/hr, LHV	1,711	1,617	1,522		
	MMBtu/hr, HHV	1,899	1,795	1,689		
Relative Humidity	%	87	78	50		
Fuel heating value	Btu/lb, LHV	20,714	20,714	20,714		
-	Btu/lb, HHV	22,993	22,993	22,993		
	,	,-	,			
CT/Bypass Stack Data						
Height	ft	150	150	150		
Diameter	ft	18	18	18		
100 Percent Load						
Temperature (°F)	۴	1,081	1,114	1,144		
Velocity (fl/sec)	ft/sec	164.9	159.4	153.3		
• • •			133.1	199.9		
Maximum Hourly Emissions						
SO <sub>2</sub>	lb/hr	10.5	9.90	9.32		
				y. <b>32</b>		
PM/PM <sub>10</sub>	lb/hr	9.0	9.0	9.0		
	•		2.0	7.0		
NO <sub>x</sub>	lb/hr	61.8	58.4	55.0		
	ppmvd @ 15% O2	9.0	9.0	9.0		
·	77	7. <b>*</b>	7.0	7.0		
CO	lb/hr	41.7	39.1	36.2		
	ppmvd	12.0	12.0	12.0		
	ppmvd @ 15% O2	10.0	9.9	9.7		
	•••	***		7.1		
VOC (as methane)	1b/hr	7.52	7.12	6.72		
-	ppmvw	3.50	3.50	3.50		
	ppmvd @ 15% O2	3.15	3.16	3.16		
	🔾		*	5.10		
Lead	lb/hr	NA	NA	NA		
				****		
Sulfuric Acid Mist	lb/hr	1.05	0.99	0.93		

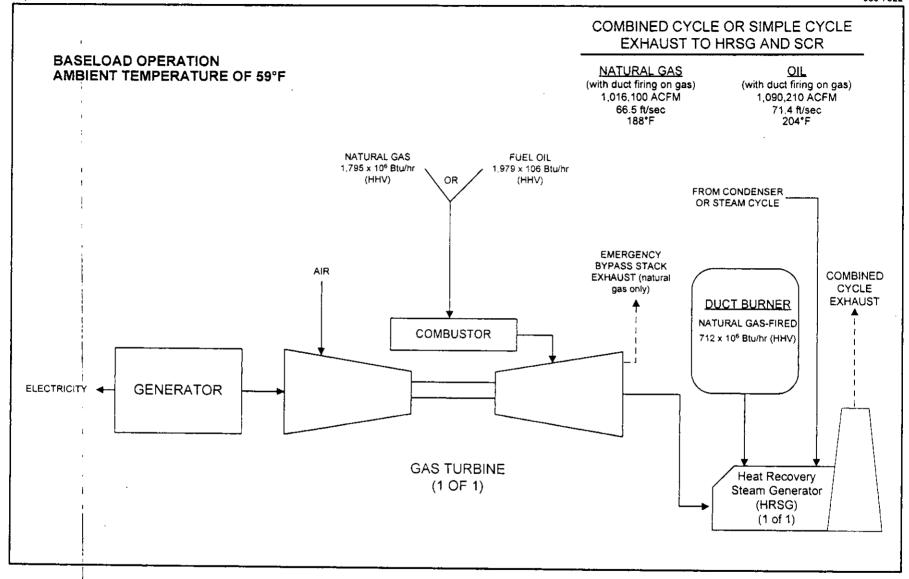
Refer to Appendix A for detailed information on basis of pollutant emission rates and operating data.
 Source: GE, 2006.

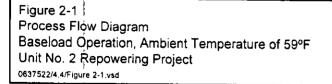
TABLE 2-7
SUMMARY OF MAXIMUM POTENTIAL ANNUAL EMISSIONS
FOR THE PROPOSED HOPKINS UNIT 2 REPOWERING PROJECT

	Maximum Potential Annual Emissions (TPY)  for CT and Duct Burner Operating Scenarios "						
Pollutant	A	В	C	D	E		
SO <sub>2</sub>	43	51	211.7	211.7	43.4		
PM	48	65	111.8	111.8	43,4 39.4		
PM <sub>10</sub>	48	65	111.8	111.8	. 39.4		
NO <sub>x</sub>	142	165	244	266	256		
СО	171	265	340	340	171		
VOC (as methane)	31.2	46.8	47,4	47.4	31.2		
Sulfuric Acid Mist	4.3	5.8	39.7	39.7	4.3		
Lead	0.00E+00	0.00E+00	4.85E-02	4.85E-02	0.00E+00		
Mercury	0.00E+00	0.00E+00	4.16E-03	4.16E-03	0.00E+00		

<sup>&</sup>lt;sup>a</sup> Based on the following hours of operation for each operating scenario:

	A	В	С	D.	E
Combined Cycle Operation					
CT, natural gas-firing	8,760	5,110	1,610	5,110	0
CT and duct burner, natural gas-firing	0	3,650	3,650	150	0
CT, fuel oil-firing	0	. 0	3,500	0	0
CT, fuel oil-firing; duct burner, natural gas-firing	0	0	0	3,500	0
CT, natural gas-firing	0	0	0	0	8,760





Process Flow Legend
Solid/Liquid 
Gas 
----



# 3.0 AIR QUALITY REVIEW REQUIREMENTS AND APPLICABILITY

The following discussion pertains to the federal, State, and local air regulatory requirements and their applicability to the Hopkins Unit 2 Repowering Project. These requirements must be satisfied before the proposed facility can begin operation.

# 3.1 National and State Aags

The existing applicable national and State of Florida local AAQS are presented in Table 3-1. Primary national AAQS were promulgated to protect the public health with an adequate margin of safety, and secondary national AAQS were promulgated to protect the public welfare from any known or anticipated adverse effects associated with the presence of pollutants in the ambient air. Areas of the country in compliance with AAQS are designated as attainment areas. New sources to be located in or near these areas may be subject to more stringent air permitting requirements.

# 3.2 New Source Review Requirements

# 3.2.1 General Requirements

Under federal and State of Florida PSD review requirements, all major new or modified sources of air pollutants regulated under the Clean Air Act (CAA) must be reviewed, and a pre-construction permit issued. Florida's State Implementation Plan (SIP), which contains PSD regulations, has been approved by EPA; therefore, PSD approval authority has been granted to FDEP.

A "major facility" is defined as any one of 28 named source categories that have the potential to emit 100 TPY or more or any other stationary facility that has the potential to emit 250 TPY or more of any pollutant regulated under CAA. "Potential to emit" means the capability, at maximum design capacity, to emit a pollutant after the application of control equipment.

PSD review is used to determine whether significant air quality deterioration will result from the new or modified facility. The State of Florida's PSD regulations are found in Rule 62-212.400, F.A.C. Major new facilities are required to undergo the following analysis related to PSD for each pollutant emitted in significant amounts (see Table 3-2):

- 1. Control technology review,
- 2. Source impact analysis,
- 3. Air quality analysis (monitoring),
- 4. Source information, and
- 5. Additional impact analyses.

In addition to these analyses, a new facility also must be reviewed with respect to GEP stack height regulations.

For new minor sources or minor modification made at a major source, the new source review requirements under the PSD regulations do not apply. Instead, an air construction permit must be obtained under the general preconstruction review requirements in Rule 62-212.300, F.A.C., and for units added at a certified site for which conditions of certification are issued under the Power Plant Siting Act.

EPA has promulgated regulations providing that certain increases above an air quality baseline concentration level of SO<sub>2</sub>, PM<sub>10</sub>, and NO<sub>2</sub> concentrations that would constitute significant deterioration. The EPA class designations and allowable PSD increments are presented in Table 3-1. The State of Florida has adopted the EPA class designations and allowable PSD increments for SO<sub>2</sub>, PM<sub>10</sub>, and NO<sub>2</sub>.

Because this Project will be a minor modification at a major source, the new source review requirements under the PSD regulations do not apply. As a result, the Project will not be required to undergo PSD review. The Project is still obligated to comply with FDEP regulations in submitting an air construction permit application.

# 3.2.2 Nonattainment Rules

FDEP has nonattainment provisions (Rule 62-212.500, F.A.C.) that apply to all major new sources facilities located in a nonattainment area. In addition, for major facilities that are located in an attainment or unclassifiable area, the nonattainment review procedures apply if the source or modification is located within the area of influence of a nonattainment area. The Hopkins Plant is located in Leon County, which is classified as an attainment or unclassifiable area for all criteria pollutants. Therefore, nonattainment new source review requirements are not applicable.

### 3.3 Emission Standards

# 3.3.1 New Source Performance Standards

The NSPS are a set of national emission standards that apply to specific categories of new sources. As stated in the 1977 CAA Amendments, these standards "shall reflect the degree of emission limitation and the percentage reduction achievable through application of the best technological system of continuous emission reduction the Administrator determines has been adequately demonstrated."

The Hopkins Unit 2 Repowering Project will be subject to one or more NSPS. The following sections describe NSPS potentially applicable to the project.

#### Combustion Turbine

The existing applicable federal New Source Performance Standards (NSPS) for the combustion turbine are those promulgated by EPA for stationary gas turbines. These NSPS (40 CFR Part 60, Subpart GG) establish emission-limiting standards for NO<sub>x</sub> and SO<sub>2</sub>. The applicable NSPS are:

- NO<sub>x</sub> 75 ppmvd corrected to 15-percent O<sub>2</sub> and heat rate plus adjustment to fuel-bound nitrogen, and
- SO<sub>2</sub> no more than 0.8-percent sulfur in the fuel.

However, on February 18, 2005, EPA proposed new NSPS for Stationary Combustion Turbines that will commence construction after February 18, 2005. These NSPS, Subpart KKKK, eventually will replace Subpart GG and Da for combustion turbines in combined cycle mode with duct burners. When finalized, the Subpart KKKK requirements will supersede the Subpart GG requirements and apply to units with a gross capacity of greater than 1 MW. The proposed Subpart KKKK requirements that would apply to the Project when finalized by EPA are applicable to combustion turbines greater than 30 MW. The NOx emissions are limited to 0.39 lb/MW-hr for gas-firing and 1.2 lb/MW-hr for light oil firing. Based on a typical simple cycle CT efficiency, these emission rates are approximately equivalent to 10 ppmvd corrected to 15-percent O<sub>2</sub> when firing natural gas and 30 ppmvd corrected to 15-percent O<sub>2</sub> when firing light oil. For SO<sub>2</sub> emissions, the proposed Subpart KKKK requirements limit emissions to 0.58 lb/MW-hr or a fuel sulfur content of 0.05 percent.

There are no emission limits in Subpart KKKK for particulate matter.

#### **Duct Burner**

The applicable federal NSPS for the duct burner are those promulgated by EPA on February 27, 2006 under 40 CFR Part 60, Subpart Da, for electric utility steam generating units capable of combusting more than 250 MMBtu/hr of fossil fuel for which construction is commenced after September 18, 1978. EPA finalized new NSPS for these units that establish emission-limiting standards for PM, NO<sub>x</sub> and SO<sub>2</sub> (PM- 0.015 lb/MMBtu; NO<sub>x</sub>- 1.0 lb/MW-hr; SO<sub>2</sub>- 1.4 lb/MW-hr; regardless of the type of fuel burned). However, HRSG and duct burners subject to the proposed NSPS, Subpart KKKK, would be exempt from the requirements of NSPS, Subpart Da.

# 3.3.2 National Emission Standards for Hazardous Air Pollutants

As discussed in Section 2.3, EPA has promulgated MACT standards for combustion turbines. The MACT standard limits formaldehyde emissions to 91 ppbvd corrected to 15-percent O<sub>2</sub>, which is equivalent to about 220 lb/10<sup>12</sup> Btu when firing natural gas and about 240 lb/10<sup>12</sup> Btu when firing light oil (see Appendix A). The MACT standard could potentially apply to the Project, if during any calendar year oil use exceeds an aggregate of 1,000 hours for all turbines on the site.

# 3.3.3 Florida Rules

The FDEP has adopted the EPA NSPS by reference in Rule 62-204.800(8): Subsection (b)39 for stationary gas turbines and Subsection (b)2 for the duct burners. Therefore, the facility is required to meet the same emissions, performance testing, monitoring, reporting, and record keeping as those described in Subsection 3.3.1. FDEP periodically updates the NSPS that are adopted by reference. FDEP has authority for implementing NSPS requirements in Florida.

### 3.3.4 Florida Air Permitting Requirements

The FDEP regulations require any new source to obtain an air permit prior to construction. Minor modifications to major sources must comply with NSPS, National Emission Standards for Hazardous Air Pollutants (NESHAP), Permit to Construct, and Permit to Operate. The requirements for construction permits and approvals are contained in Rules 62-4.030, 62-4.050, 62-4.210, and 62-210.300(1), F.A.C. Specific emission standards are set forth in Chapter 62-296, F.A.C.

### 3.4 Source Applicability

# 3.4.1 Area Classification - · ·

The Project is located in Leon County, which has been designated by EPA and FDEP as an attainment area (includes unclassifiable) for all criteria pollutants. Leon County and surrounding

counties are designated as PSD Class II areas for SO<sub>2</sub>, PM<sub>10</sub>, and NO<sub>2</sub>. The site is located approximately 28 kilometers (km) from the PSD Class I area of the Bradwell Bay National Wilderness Area (NWA) and 38 km from the closest part of the PSD Class I area of the St. Marks NWA.

# 3.4.2 New Source Review

# Pollutant Applicability

The existing Hopkins Generating Station is considered to be a major facility because the emissions of several regulated pollutants are estimated to exceed 100 TPY, and the emissions units are one of the 28 listed major source categories under the PSD rules.

The City of Tallahassee proposes to repower the existing 238-MW Unit No. 2 with the addition of one nominal 188-MW combined-cycle unit and the permanent shut down of the fossil fuel steam generator for Unit 2. The emissions of each unit have been previously described. A summary of the maximum potential annual emissions for the repowered Unit 2 with the emission reductions due to the shutdown of the existing Unit 2 boiler is presented in Table 3-3.

The PSD definition of a net emission increase consists of two additive components as follows:

- Any increase in actual emissions from a particular physical change or change in method of operation at a stationary source; and
- Any other increase and decreases in actual emissions at the source that are contemporaneous with the particular change and are otherwise creditable.

The first component narrowly includes only the emissions increases associated with a particular change at the source (the proposed CT emission). The second component more broadly includes all contemporaneous, source-wide (occurring anywhere at the entire source), creditable emission increases and decreases. For the Project, the shutdown of Unit No. 2 represents creditable emission decreases.

As shown in Table 3-3, potential annual emissions from the Hopkins Unit 2 Repowering Project, together with the emissions reductions due to the shutdown of the existing Unit 2 boiler, will not trigger PSD review for any regulated pollutant.

The maximum potential annual emissions were based the following operational scenarios at a turbine inlet temperature of 59 °F:

- CT operation when firing natural gas in combined cycle or simple cycle mode with exhaust gases routed through the HRSG and SCR system for 8,760 hours per year operation of the CT at full load for all pollutants except NO<sub>x</sub>. For NO<sub>x</sub>, the maximum annual emissions were based on the CT operation in simple cycle mode with exhaust gases routed through the emergency bypass stack for 8,760 hours per year operation of the CT at full load at full load. Only natural gas will be fired in this mode.
- Maximum duct firing with natural gas of 2,598,800 MMBtu/yr (HHV), which is equivalent to 3,650 hours/year operation at the maximum hourly duct firing rate.
- Maximum distillate oil-firing in the CT of 6,926,500 MMBtu/yr (HHV), which is equivalent to 3,500 hours of the CT at full load.

A summary of the maximum short-term emission proposed for the repowered unit is presented in Table 3-4.

Therefore, under PSD regulations, the Project is classified as a minor modification at a major source. As a result, the new source review requirements under the PSD regulations do not apply and the Project will not be required to undergo PSD review. Instead, the Project will be required to be reviewed under the general preconstruction review requirements in Rule 62-212.300, F.A.C., and subject to a final order issued pursuant to the PPSA.

#### Emission Standards

The applicable NSPS for the CTs is 40 CFR Part 60, Subpart GG, and the applicable NSPS for the duct burner is 40 CFR Part 60, Subpart Da. These NSPS are being replaced by Subpart KKKK.

For this Project, the NO<sub>x</sub> emissions from the CT will be less than 0.2 lb/MW-hr for gas-firing and 0.42 lb/MW-hr for light oil firing for the combined cycle and simple cycle operations when the exhaust gases are routed to the HRSG and SCR system. For simple cycle operation when the exhaust gases are routed to the bypass stack, the NOx emissions from combustion turbine will be approximately 0.3 lb/MW-hr for gas-firing. For SO<sub>2</sub>, the Project's emissions will be limited to a fuel sulfur content of 0.05 percent.

The NESHAPs Subpart YYYY may potentially apply to the Project. Information available from the EPA's emission database indicate that the Project will meet the proposed MACT of 91 ppbvd corrected to 15-percent O<sub>2</sub> for formaldehyde.

As previously discussed, the applicable federal NSPS for the duct burner are those promulgated by EPA on February 27, 2006, under 40 CFR Part 60, Subpart Da, which establish emission-limiting standards for PM, NO<sub>x</sub>, and SO<sub>2</sub>. EPA finalized new NSPS for these units that establish emission-limiting standards for PM, NO<sub>x</sub>, and SO<sub>2</sub>. However, HRSG and duct burners subject to the proposed NSPS, Subpart KKKK, such as the duct burner proposed for this Project would be exempt from the requirements of NSPS, Subpart Da. The emission limits proposed for the Project will be well less than the limits in Subpart Da.

# **Excess Emissions**

The start-up and shutdown and fuel changes in combined cycle operation will require an excess emission allowance greater than 2 hours provided under the FDEP rules. During cold start-up, the operating load of the CTs is limited by the amount of steam that can be accepted by the steam turbine requiring low-load operation for longer than 2 hours and resulting in excess emissions during these periods. Major tuning sessions of the DLN combustors will also result in conditions where excess emissions may occur. An excess emission allowance is requested for this Project similar to the allowance authorized by the FDEP for the City's Purdom Repowering Project. The combined cycle unit associated with this facility has a similar steam turbine that receives steam during start-up. The proposed condition follows:

Excess emissions resulting from startup, shutdown, malfunction, or fuel switching shall be permitted providing best operational practices to minimize emissions are adhered to and the duration of excess emissions shall be minimized but in no case exceed the following in any 24-hour period: a total of six hours during any day including a cold startup; a total of four hours during any day that includes a hot startup; and a total of two hours during days not including a hot or cold startup. A cold startup is startup after the combined cycle unit has been down for more than 48 hours. A hot startup is startup after the combined cycle unit has been down for 48 hours or less.

In addition, excess emissions resulting from a major DLN/water injection tuning session without SCR operation shall be permitted provided the tuning session is performed in accordance with the manufacturer's specifications and in no case shall exceed 72 hours in any calendar year. A "major tuning session" would occur after a combustor change-out, a major repair to a combustor, or other similar circumstances. Prior to performing any major tuning session, the permittee shall provide the Compliance Authority with an advance notice that details the activity and proposed tuning schedule. The notice may be made by telephone, facsimile transmittal, or electronic mail.

# 3.4.3 Other Clean Air Act Requirements

The 1990 CAA Amendments established a program to reduce potential precursors of acidic deposition. The Acid Rain Program was delineated in Title IV of the CAA Amendments and required EPA to develop the program. EPA's final regulations were promulgated on January 11, 1993, and included permit provisions (40 CFR Part 72), allowance system (Part 73), continuous emission monitoring (Part 75), excess emission procedures (Part 77), and appeal procedures (Part 78).

EPA's Acid Rain Program applies to all existing and new utility units except those serving a generator less than 25 MW, existing simple cycle CTs, and certain non-utility facilities; units that fall under the program are referred to as affected units. The EPA regulations are applicable to the Project for the purposes for obtaining a permit and allowances, as well as emission monitoring. New units are required to obtain permits under the program by submitting a complete application 24 months before the date on which the unit commences operation (e.g., first fire). (Rule 62-210.370). The City has submitted the Acid Rain Program application for this project.

The permit would require the units to hold SO<sub>2</sub> emission allowances. An allowance is a market-based financial instrument that is equivalent to 1 ton of SO<sub>2</sub> emissions. Allowances can be sold, purchased, or traded.

CEM for SO<sub>2</sub> and NO<sub>x</sub> is required for gas-fired and oil-fired affected units. When an SO<sub>2</sub> CEM is selected to monitor SO<sub>2</sub> mass emissions, a flow monitor is also required. Alternately, SO<sub>2</sub> emissions may be\_determined\_using procedures\_established in Appendix D, 40 CFR Part-75 (flow-proportional—oil sampling or manual daily oil sampling). CO<sub>2</sub> emissions must also be determined either through a CEM (e.g., as a diluent for NO<sub>x</sub> monitoring) or calculation. Alternate procedures, test methods, and

quality assurance/quality control (QA/QC) procedures for CEM are specified (Part 75, Appendices A through I). The acid rain CEM requirements including QA/QC procedures are, in general, more stringent than those specified in the NSPS for Subpart GG. New units are required to meet the requirements by the later of January 1, 1995, or not later than 90 days after the unit commences commercial operation. The City will install a NOx CEMS and utilize the alternative procedures for SO<sub>2</sub> and CO<sub>2</sub> in accordance with the applicable Title IV appendixes.



TABLE 3-1

NATIONAL AND STATE AAOS, ALLOWABLE PSD INCREMENTS, AND SIGNIFICANT IMPACT LEVELS

		A	AQS (μg/m³) <sup>a</sup>			crements /m³)*	PSD Class II
Pollutant	Averaging Time	Primary Standard	Secondary Standard	Florida	Class I	Class II	Significant Impact Levels (μg/m³) b
Particulate Matter	Annual Arithmetic Mean	50	50	50	. 4	17	1
(PM 10)	24-Hour Maximum	150	150	150	8	30	5
Sulfur Dioxide	Annual Arithmetic Mean	80	NA	60	2	20	1
	24-Hour Maximum	365	NA	260	5	91	5
1	3-Hour Maximum	NA	1,300	1,300	25	512	25
Carbon Monoxide	8-Hour Maximum	10,000	10,000	10,000	NA	NA	500
	1-Hour Maximum	40,000	40,000	40,000	NA	NA	2,000
Nitrogen Dioxide	Annual Arithmetic Mean	100	100	100	2.5	25	I
Ozone <sup>c</sup>	1-Hour Maximum	235	235	235	NA	NA	NA
Lead	Calendar Quarter Arithmetic Mean	1.5	1.5	1.5	NA	NA	NA

Note: Particulate matter  $(PM_{10})$  = particulate matter with aerodynamic diameter less than or equal to 10 micrometers. NA = Not applicable, i.e., no standard exists.

Sources:

Federal Register, Vol. 43, No. 118, June 19, 1978. 40 CFR 50; 40 CFR 52.21.

Chapter 62-204, F.A.C.

Short-term maximum concentrations are not to be exceeded more than once per year except for the PM<sub>10</sub> and ozone AAQS. The 24-hour PM<sub>10</sub> AAQS is attained when the expected number of days per year with a 24-hour concentration above 150 μ/m³ is equal to or less than 1. For modeling purposes, compliance is based on the sixth highest 24-hour concentration over a 5-year period. For ozone, the daily maximum 1-hour concentration cannot be exceeded an average of more than one per year.

Maximum concentrations are not to be exceeded.

On July 18, 1997, EPA promulgated revised AAQS for particulate matter and ozone. For particulate matter, PM<sub>2.5</sub> standards were introduced with a 24-hour standard of 65 g/m³ (3-year average of 98th percentile) and an annual standard of 15 g/m³ (3-year average at community monitors). The ozone standard was modified to be 0.08 ppm; achieved when 3-year average of 99th percentile is 0.08 ppm 157 μ/m³ or less. FDEP has not yet adopted these standards.

TABLE 3-2
PSD SIGNIFICANT EMISSION RATES

Pollutant	Regulated Under	Significant Emission Rate (TPY)
Sulfur Dioxide	NAAQS, NSPS	40
Particulate Matter [PM(TSP)]	NSPS	25
Particulate Matter (PM <sub>10</sub> )	NAAQS	15
Nitrogen Dioxide	NAAQS, NSPS	40
Carbon Monoxide	NAAQS, NSPS	100
Volatile Organic	·	
Compounds (Ozone)	NAAQS, NSPS	40
Lead	NAAQS	0.6
Sulfuric Acid Mist	NSPS	7
Total Fluorides	NSPS	3
Total Reduced Sulfur	NSPS	10
Reduced Sulfur Compounds	NSPS	10
Hydrogen Sulfide	NSPS	10
Mercury	NESHAP	0.1

NAAQS = National Ambient Air Quality Standards.

NSPS = New Source Performance Standards.

NESHAP = National Emission Standards for Hazardous Air Pollutants.

Sources: 40 CFR 52.21; Rule 62-212.400.

# TABLE 3-3 SUMMARY OF MAXIMUM POTENTIAL ANNUAL EMISSIONS FOR THE PROPOSED HOPKINS UNIT 2 REPOWERING PROJECT COMPARED TO THE PSD SIGNIFCANT EMISSION RATES

				Annu	al Emissions (T	(PY)			
Pollutant	M	Maximum Potential Annual Emissions (TPY)  for CT and DB Operating Scenarios <sup>a</sup>					Emission Changes- Proposed Project with Existing	PSD Significant Emission Rate	PSD Review
	A	В	C	D	E	from Existing with Existing Unit 2 b Unit 2 Shutdown	(tons/year)	Required?	
SO <sub>2</sub>	43.4	50.5	211.7	211.7	43.4	1642.0		***	
PM	48.2	65.2	111.8	111.8	39.4	136,3	-1,430	40	No
PM <sub>10</sub>	48.2	65.2	111.8	111.8	39.4	97.5	-25	25	No
NO,	142.0	164.9	243.7	265.7	255.6	843,3	14	15	No
CO	171.1	264.6	340.1	340.1	171.1	د.ده 241.1	-578	40	No
VOC (as methane)	31.2	46.8	47.4	47.4	31.2	19.7	99	001	No
Sulfuric Acid Mist	4,3	5.8	39.7	39.7	4.3	73.0	28	40	No
ead	0.000	0.000	0.05	0.05	0.00	0,019	•33 0	7	No
Mercury ·	0.0000	0.0000	0.00	0.00	0.00	0.0014	0	0.6 · 0.1	No No

<sup>\*</sup> Based on the following hours of operation for each operating scenario:

1	A	В	С	D	r
Combined Cycle Operation					
CT, natural gas-firing	8,760	5,110	1,610	5,110	0
CT and duct burner, natural gas-firing	0	3,650	3,650	150	0
CT, fuel oil-firing	0	0	3,500	0	ō
CT, fuel oil-firing; duct burner, natural gas-firing CT, fuel oil-firing; duct burner, natural gas-firing	0	0	0	3,500	0
Simple Cycle Operation	0	0	0	0	8,760

Based on maximum annual average PM, PM10, CO, VOC, lead, and mercury emissions based on AOR data for the 24-month consecutive period from 2001 to 2005. For SO<sub>2</sub> and NO<sub>3</sub>, based on the maximum annual average emissions from monthly CEM data from March 2001 to February 2006.

TABLE 3-4
SUMMARY OF MAXIMUM SHORT-TERM EMISSIONS
FOR THE PROPOSED HOPKINS UNIT 2 REPOWERING PROJECT

		CT Natural	Gas-Firing	<u>C</u> Γ Distilla	ite Oil-Firing
Pollutant		Emission Rate	Basis	Emission Rate	Basis
Combined Cyc	le Operation				
		No Duct Firing		No Duct Firing	
SO <sub>2</sub>		9.9 lb/hr	2 gr S/100 scf	102.0 lb/hr	0.05% S
PM/PM <sub>10</sub>	СТ	9.0 lb/hr	filterable	37.6 lb/hr	filterable
PM/PM <sub>10</sub>	CT/SCR	11.0 lb/hr	filterable	37.6 lb/hr	filterable
NO <sub>x</sub>	CT/SCR	32.4 lb/hr	5 ppmvd@15%O2	77.5 Jb/hr	10 ppmvd@15%O2
co		39.1 lb/hr	9.9 ppmvd@15%O2	82.2 lb/hr	17.4 ppmvd@15%O2
VOC		7.1 lb/hr	3.16 ppmvd@15%O2	7.5 lb/hr	2.77 ppmvd@15%O2
		Duct Firing with Gas *		Duct Firing with Gas	s *
SO <sub>2</sub>		13.8 lb/hr	2 gr S/100 scf	105.9 ib/hr	2 gr S/100 scf (DB)
PM/PM <sub>10</sub>	CT/SCR	20.3 lb/hr	filterable	47.0 lb/hr	filterable
NO <sub>x</sub>	CT/SCR	45.0 lb/hr	5 ppmvd@15%O2	102.6 lb/hr	10 ppmvd@15%O2
co		90.3 lb/hr	16.7 ppmvd@15%O2	133.4 lb/hr	21.2 ppmvd@15%O2
VOC		15.7 lb/hr	5.7 ppmvd@15%O2	16.0 lb/hr	5.2 ppmvd@15%O2
Simple Cycle (	Operation				
SO <sub>2</sub>		9.9 lb/hr	2 gr S/100 scf	NA	
PM/PM <sub>10</sub>		9.0 lb/hr	filterable	NA	•
NO <sub>z</sub>		58.4 lb/hr	9 ppmvd@15%O2	NA	
CO		39.1 lb/hr	9.9 ppmvd@15%O2	NA	
VOC		7.1 lb/hr	3.2 ppmvd@15%O2	NA	

Note: Based on 59 °F ambient inlet air temperature. NA= not applicable

<sup>\*</sup> Basis of duct burner emissions :

Pollutant	Natural Gas-Firing	Oil-Firing		
PM <sub>10</sub>	0.0120 lb/MMBtu	0.0150 lb/MMBtu		
NO <sub>x</sub>	0.10 lb/MMBtu	0.15 lb/MMBtu		
co	0.072 lb/MMBtu	0.10 lb/MMBtu		
VOC	0.012 lb/MMRtu	0.012 lb/MMBni		

## APPENDIX A

EXPECTED PERFORMANCE AND EMISSIONS INFORMATION FOR THE COMBUSTION TURBINE AND DUCT BURNER

TABLE A-SUM-1
SUMMARY OF MAXIMUM SHORT-TERM EMISSIONS FOR THE HOPKINS 2 REPOWERING PROJECT

	_		Maximi	im Hourly E	missions (lb/hr) <sup>a. b</sup>	
Pollutant	_		Combined C	yele (CC)		Simple Cycle (SC)
	CT Fuel: Load:	NG 100%	NG 100% w/DB on NG	FO 100%	FO 100% w/DB on NG	NG 100%
Combustion Turbine						
SO <sub>2</sub>		9.90	13.8	102.0	105.9	9.90
PM		11.0	20.3	37.6	47.0	9.00
PM <sub>10</sub>		11.0	20.3	37.6	47.0	9.00
NO.		32.4	45.0	77.5	102.6	58.4
CO		39.1	90.3	82.2	133.4	39.1
VOC (as methane)		7.12	15.7	7.5	16.0	7.12
Sulfuric Acid Mist		0.99	1.77	20.4	21.2	0.99
Lead		0.00	0.00	0.028	0.028	0.00
Mercury		0.00	0.00	0.0024	0 0024	0.00
HAPs		0.78	1,09	2.45	2.45	0.78
Combustion Turbines:	2					
SO <sub>2</sub>		19.8	27.6	204 0	211.9	19.8
PM		22.0	40.7	75.2	93.9	18.0
PM <sub>10</sub>		22.0	40.7	75.2	93.9	18.0
NO <sub>x</sub>		64.8	89.9	154.9	205.1	117
со		78.1	181	164	266.9	78.1
VOC (as methane)		14 24	31.3	14.9	32.0	14.24
Sulfuric Acid Mist		1.98	3.55	40.80	42.4	1.98
Lead		0.00	0.00	0.055	0.055	0.00
Mercury		0.00	0.00	0.0047	0.0047	0.00
HAPs		1.56	2.17	4.91	4,9	1.56

Based on 59 °F ambient inlet air temperature.
 Source: GE, 2005 - CT Performance Data;
 Golder, 2005

TABLE A-SUM-2
SUMMARY OF MAXIMUM ANNUAL EMISSIONS FOR THE HOPKINS 2 REPOWERING PROJECT

Operating Scenario	Н	•	ing- Maximu based on hou	m Emissions (* irs for	TPY)		Net Emis		imum Futur ed on hours		Actual)	
	Α	В	С	D	E		Α	В	С	D	E	
CC/ CT-NG	8,760	5,110	1,610	5,110	0		8,760	5,110	1,610	5,110	0	
CC/ CT & DB- NG	0.00	<b>SP49</b>	2000	e-15025			0	3,650	3,650	150	0.	
CC/CT -FO	J. 40 - 2	<b>全日李</b>	1.00	3.00	2.50		0	0	3,500	0	0	PSD
	134054	S 40 50		10 to 10 to 10	An 30 33.5	Actual c	0	0	0	0	0	Significa
CC/ CT -FO; DB -NG	5,55,75	100	S. A. Beer			Emissions-	0	0	0	3,500	0	Emissio
			•			2-yr Average						Rate
SC/ NG			<b>经</b>		\$2.00 M	(TPY)	0	0	0	0	8,760	(TPY
TOTAL	8,760	8,760	8,760	8,760	B,760		8,760	8,760	8,760	8,760	8,760	
Combustion Turbine												
SO <sub>2</sub>	43.4	50.5	211.7	211.7	43.4	1.642.0	-1.599	-1,591	-1,430	-1,430	-1,599	40
PM	48,2	65.2	111.8	111.8	39.4	136.3	-88	-71	-25	-25	-97	25
PM <sub>10</sub>	48.2	65.2	111.8	111.8	39.4	97.5	-49	-32	14	14	-58	15
NO.	142.0	164.9	243.7	265.7	255.6	843.3	-701	-678	-600	-578	-588	40
CO	171.1	264.6	340.1	340.1	171.1	241.1	-701	23	99	99	-70	100
VOC (as methane)	31.2	46.8	47.4	47.4	31.2	19.7	11	27	28	28	11	40
Sulfuric Acid Mist	4.3	5.8	39.7	39.7	4.3	73.0	-68.7	-67.3	-33.3	-33.3	-68.7	7
Lead	0.00	0.00	0.05	0.05	0.00	0.02	-0.019	-0.019	0.030	. 0.030	-0.019	0.6
Mercury	0.000	0.000	0.004	0.004	0.000	0.0014	-0.001	-0.001	0.003	0.003	-0.001	0.1
HAPs	3.4	4.0	6.9	6.4	3,4					2.202		
Combustion Turbines:	2			•				• •				
SO <sub>2</sub>	87	101	423	423	87	1,642.0	-1,555	-1.541	-1,219	-1.219	-1.555	40
PM	96	130	223.6	224	79	136.3	-40	-6	87	87	-57	25
PM <sub>10</sub>	96	130	223.6	224	79	97.5	-i	33	126	126	-19	15
NO,	284	330	487	531	511	843.3	-559	-514	-356	-312	-332	40
co	342	529	680	680	342	241.1	101	288	439	439	101	100
VOC (as methane)	62.4	93.5	94.7	94.7	62.4	19.7	43	74	75	75	43	40
Sulfuric Acid Mist	8.7	11.5	79.5	79.5	8.7	73.0	-64.4	-61.5	6.5	6.5	64.4	7
Lead	0.000	0.000	0.097	0.097	0.000	0.02	-0.019	-0.019	0.08	0.08	-0.02	0.6
Mercury	0,000	0.000	0.008	0.008	0.000	0.0014	-0.001	-0.001	0.007	0.007	-0.001	0.1
HAPs	6.83	7.95	13.81	12.7	6.8							

<sup>&</sup>lt;sup>b</sup> Basis of Emissions for Hopkins 2 Repowering:

	Natural gas	Fuel oil		
SO2	2 gr S/100 scf	0.050%	S	<del></del>
PM	filterable		filterable	(includes ammonium sulfate from SCR for CC operation)
PM10	filterable		filterable	(includes ammonium sulfate from SCR for CC operation)
NOx	5 ppmvd (5	10	ppmvd (10	w/DB) CC operation (corrected to 15% oxygen)
NOx	9 ppmvd	NA		SC operation (corrected to 15% oxygen)
CO	12 ppmvd (29	25	ppinvd (50	w/DB)
VOC	3.5 ppmvw (8.7	3.5	ppmvw (7.9	w/DB) (assumes 50% UHC)

Actual emissions based on CEMS for SO<sub>2</sub> and NO<sub>4</sub>; AP-42 factors for other pollutants.
 CEMS data used from March 2001 to February 2006. AOR data used 2001 to 2005.
 Emission factors based on latest factors from AP-42 and used for all years (AOR emissions adjusted accordingly). PM/PM10 factors based on filterable PM.

 ${\bf TABLE~A-1} \\ {\bf DESIGN~INFORMATION~AND~STACK~PARAMETERS~FOR~THE~HOPKINS~UNIT~2~REPOWERING~PROJECT~} \\ {\bf GE~FRAME~7FA,~DRY~LOW~NO_x~COMBUSTOR,~NATURAL~GAS,~BASE~LOAD,~WITH~NATURAL~GAS~DUCT~FIRING~} \\ {\bf CASTAGLAR} \\$ 

				CT Only			CT with Duct Burner (Natural Gas)			
_			lalet Temperatur			e Inlet Temperatu				
Parameter			2659 <b>P</b> 3 . 13 Pc		P 25 TF W/DB	59 TF w/DB 44				
Combustion Turbine Performance										
Power output (MW)	р	187.8	174.40	160.3	187.8	174.4	160.3			
Heat rate (Btu/kWh, LHV)	p	9,110	9,270	9,495	9,110	9,270	9,495			
(Btu/kWh, HHV)	•	10,112	10,290	10,539	10,112	10,290	10,539			
Heat Input (MMBtu/hr, LHV)	р	1,710.9	1,616.7	1,522	1,711	1,616.7	1,522			
(MMBtu/hr, HHV)		1,899	1,795	1,689	1,899	1,795	1,689			
Evaporative Cooler	P	Off	On	On	Off	On	On			
Relative Humidity (%)	р	87	78	50	87	78	50			
Natural gas										
Fuel heating value (Btu/lb, LHV)	р	20,714	20,714	20,714	20,714	20,714	20,714			
(Bm/lb, HHV)		22,993	22,993	22,993	22,993	22,993	22,993			
(HHV/LHV)		1.110	1.110	1.110	1.110	1.110	1,110			
Duct Burner (DB)										
Heat input (MMBtu/hr, HHV)		0	0	0	765	712	663			
(MMBtu/hr, LHV)		0	0	0	688.8	641.1	596.9			
CT/DB Exhaust Flow							•			
Mass Flow (lb/hr)- with no margin		3,826,000	3,607,000	3,382,000	e 3,856,721.2	3,635,594	3,408,622			
- provided	P	3,826,000	3,607,000	3,382,000						
Temperature (°F)	р	1,081	1,114	i,144	1,081	1,114	1,144			
Moisture (% Vol.)	р	7.54	8.55	10.28	c 10.26	11.21	12 88			
Oxygen (% Vol.)	P	12.77	12.57	12.22	c · 9.76	9.61	9.30			
Molecular Weight	c	2 <b>8.4</b> 9 2 <b>8.4</b> 9	28.38 28.37	28.19 28.18	c 28.31	28.20	28.02			
Fuel Usage	Р	20.47	26.37	20.10						
Natural Gas										
Fuel usage CT (lb/hr) = Heat Input (MMBh	⊿hr) x 1,000,00	0 Btu/MMBtu (Fuel Heat	Content, Btu/lb (LF	HV))						
Heat input (MMBtu/hr, LHV)		1,711	1,617	1,522	1,711	1,617	1,522			
Heat content (Btu/lb, LHV)		20,714	20,714	20,714	20,714	20,714	20,714			
Fuel usage (lb/hr)- calculated	c	82,596	78,049	73,477	82,596	78,049	73,477			
		1,036								
Heat content (Btu/cf, LHV)- assumed		933	933	933	933	933	933			
Fuel density (lb/ft')		0.0451	0.0451	0.0451	0.0451	0.0451	0.0451			
Fuel usage (cf/hr)- calculated		1,832,961	1,732,040	1,630,584	1,832,961	1,732,040	1 (10 (8)			
Fuel Usage - Duct Burner Only							1,630,584			
							1,030,384			
Fuel usage (lb/hr)- calculated		0	0	0	c 33,253	30,950	28,816			
		0	0	0 0	c 33,253 737,941	30,950 686,838				
Fuel usage (lb/hr)- calculated Fuel usage (cf/hr)- calculated  Bypass Stack and Flow Conditions		0	0	0	737,941	686,838	28,816			
Fuel usage (lb/hr)- calculated Fuel usage (cf/hr)- calculated Bypass Stack and Flow Conditions Stack Height (ft)		0	0	0 150	737,941 150	686,838 150	28,816			
Fuel usage (lb/hr)- calculated Fuel usage (cf/hr)- calculated Bypass Stack and Flow Conditions		0	0	0	737,941	686,838	28,816 639,485			
Fuel usage (Ib/hr)- calculated Fuel usage (cf/hr)- calculated  Bypass Stack and Flow Conditions  Stack Height (ft)  Diameter (ft)  Velocity (ft/sec) = Volume flow (acfin) / [i	{(diameter)² /4)	0 150 18 x 3.14159] / 60 sec/min	0 150 18	0 150 18	737,941 150 18	686,838 150 18	28,816 639,485 150 18			
Fuel usage (lb/hr)- calculated Fuel usage (cf/hr)- calculated  Bypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)	{(díameter)² /4)	0 150 18	0	0 150	737,941 150	686,838 150	28,816 639,485			
Fuel usage (lb/hr)- calculated Fuel usage (cf/hr)- calculated  Bypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfin) / [i	((diameter)² /4)	0 150 18 x 3.14159] / 60 sec/min	0 150 18	0 150 18	737,941 150 18	686,838 150 18	28,816 639,485 150 18			
Fuel usage (lb/hr)- calculated Fuel usage (cf/hr)- calculated  Bypass Stack and Flow Conditions  Stack Height (ft)  Diameter (ft)  Velocity (ft/sec) = Volume flow (acfin) / [th/hr)	{(diameter)* /4}	0 150 18 x 3.14159] / 60 sec/min 3,826,000 1,081 28,49	0 150 18 3,607,000	0 150 18 3,382,000	737,941 150 18 NA	686,838 150 18	28,816 639,485 150 18			
Fuel usage (lb/hr)- calculated Fuel usage (cf/hr)- calculated  Bypass Stack and Flow Conditions  Stack Height (ft)  Diameter (ft)  Velocity (ft/sec) = Volume flow (acfm) / [i Mass flow (lb/hr)  Stack Temperature (°F)	((diameter) <sup>†</sup> /4)	0 150 18 x 3.14159] / 60 sec/min 3.826,000 1,081	0 150 18 3,607,000 1,114	0 150 18 3,382,000 1,144	737,941 150 18 NA NA	686,838 150 18 NA NA	28,816 639,485 150 18 NA			
Fuel usage (lb/hr)- calculated Fuel usage (cf/hr)- calculated  Bypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfm) / [i Mass flow (lb/hr) Stack Temperature (°F) Molecular weight	{(diameter)* /4}	0 150 18 x 3.14159] / 60 sec/min 3,826,000 1,081 28,49	0 150 18 3,607,000 1,114 28.38	150 18 3,382,000 1,144 28.19 2,341,021 18	737,941 150 18 NA NA NA	686,838 150 18  NA NA NA	28,816 639,485 150 18 NA NA			
Fuel usage (lb/hr)- calculated Fuel usage (cf/hr)- calculated  Bypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfm) / [the Mass flow (lb/hr) Stack Temperature (*F) Molecular weight Volume flow (acfm)	((diameter)* /4)	0 150 18 x 3.14159] / 60 sec/min 3,826,000 1,081 28,49 2,517,808	3,607,000 1,114 28,38 2,433,691	0 150 18 3,382,000 1,144 28.19 2,341,021	737,941 150 18 NA NA NA NA	686,838 150 18 NA NA NA NA	28,816 639,485 150 18 NA NA NA			
Fuel usage (lb/hr)- calculated Fuel usage (cf/hr)- calculated  Bypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfm) / [i Mass flow (lb/hr) Stack Temperature (*F) Molecular weight Volume flow (acfm) Diameter (ft) Velocity (ft/sec)- calculated	((diameter)¹/4)	0 150 18 x 3.14159] / 60 sec/min 3,826,000 1,081 28,49 2,517,808 18	3,607,000 1,114 28.38 2,433,691 18	0 150 18 3,382,000 1,144 28.19 2,341,021 18	737,941 150 18 NA NA NA NA	686,838 150 18 NA NA NA NA	28,816 639,485 150 18 NA NA NA			
Fuel usage (lb/hr)- calculated Fuel usage (cf/hr)- calculated  Bypass Stack and Flow Conditions  Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfin) / [it Mass flow (lb/hr)  Stack Temperature (°F) Molecular weight Volume flow (acfin) Diameter (ft)	((diameter)†/4)	0 150 18 x 3.14159] / 60 sec/min 3,826,000 1,081 28,49 2,517,808 18	3,607,000 1,114 28.38 2,433,691 18	0 150 18 3,382,000 1,144 28.19 2,341,021 18	737,941 150 18 NA NA NA NA	686,838 150 18 NA NA NA NA	28,816 639,485 150 18 NA NA NA			
Fuel usage (lb/hr)- calculated Fuel usage (cf/hr)- calculated  Bypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfm) / [i Mass flow (lb/hr) Stack Temperature (*F) Molecular weight Volume flow (acfm) Diameter (ft) Velocity (ft/sec)- calculated  HRSG Stack and Flow Conditions	((diameter) <sup>†</sup> /4)	0 150 18 x 3.14159] / 60 sec/min 3,826,000 1,081 28,49 2,517,808 18 164,9	3,607,000 1,114 28.38 2,433,691 18 159.4	0 150 18 3,382,000 1,144 28.19 2,341,021 18 153.3	737,941 150 18 NA NA NA NA NA	686,838 150 18 NA NA NA NA NA	28,816 639,485 150 18 NA NA NA NA			
Fuel usage (Ib/hr)- calculated Fuel usage (cf/hr)- calculated Bypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfm) / [it Mass flow (Ib/hr) Stack Temperature (°F) Molecular weight Volume flow (acfm) Diameter (ft) Velocity (ft/sec) - calculated  HRSG Stack and Flow Conditions Stack Height (ft)	((diameter)² /4)	0 150 18 x 3.14159] / 60 sec/min 3,826,000 1,081 28,49 2,517,808 18 164.9	0 150 18 3,607,000 1,114 28,38 2,433,691 18 159,4	150 18 3,382,000 1,144 28.19 2,341,021 18 153.3	737,941 150 18 NA NA NA NA NA NA	686,838 150 18	28,816 639,485 150 18 NA NA NA NA NA			
Fuel usage (Ib/hr)- calculated Fuel usage (cf/hr)- calculated Bypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfm) / [it Mass flow (Ib/hr) Stack Temperature (*F) Molecular weight Volume flow (acfm) Diameter (ft) Velocity (ft/sec)- calculated  HRSG Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Mass flow (Ib/hr)	((diameter)* /4)	0 150 18 x 3.14159] / 60 sec/min 3,826,000 1,081 28.49 2,517,808 18 164.9	3,607,000 1,114 28.38 2,433,691 18 159.4 150 18	150 18 3,382,000 1,144 28.19 2,341,021 18 153.3	737,941 150 18  NA NA NA NA NA 150 18 3,856,721	686,838 150 18 NA NA NA NA NA 150 18	28,816 639,485 150 18 NA NA NA NA NA 150 18			
Fuel usage (Ib/hr)- calculated Fuel usage (cf/hr)- calculated Bypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfin) / [it Mass flow (Ib/hr) Stack Temperature (*F) Molecular weight Volume flow (acfin) Diameter (ft) Velocity (ft/sec)- calculated  HRSG Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Mass flow (Ib/hr) Stack Temperature (*F)	((diameter)¹ /4)	0 150 18 x 3.14159] / 60 sec/min 3,826,000 1,081 28,49 2,517,808 18 164.9 150 18	150 18 3,607,000 1,114 28,38 2,433,691 18 159,4 150 18	150 18 3,382,000 1,144 28.19 2,341,021 18 153.3	737,941  150 18  NA NA NA NA NA NA 150 18  3,856,721 189.0	150 18 18 NA NA NA NA NA NA NA NA NA NA NA NA NA	28,816 639,485 150 18 NA NA NA NA NA 150 18 3,408,622			
Fuel usage (lb/hr)- calculated Fuel usage (cf/hr)- calculated Bypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfm) / ft Mass flow (lb/hr) Stack Temperature (°F) Molecular weight Volume flow (acfm) Diameter (ft) Velocity (ft/sec) - calculated  HRSG Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Mass flow (lb/hr) Stack Temperature (°F) Molecular weight	((diameter) <sup>†</sup> /4)	0 150 18 x 3.14159] / 60 sec/min 3.826,000 1,081 28.49 2,517,808 18 164.9 150 18 3,826,000 203.0 28.49	150 18 3,607,000 1,114 28,38 2,433,691 18 159,4 150 18 3,607,000 202,0 28,38	150 18 3,382,000 1,144 28.19 2,341,021 18 153.3	737,941  150 18  NA NA NA NA NA NA 150 18  3,856,721 189.0 28.31	086,838 150 18 NA NA NA NA NA 150 18 3.635,594 188.0 28.20	28,816 639,485 150 18 NA NA NA NA NA NA 150 18 3,408,622 190 28.02			
Fuel usage (lb/hr)- calculated Fuel usage (cf/hr)- calculated Bypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfin) / [i Mass flow (lb/hr) Stack Temperature (*F) Molecular weight Volume flow (acfin) Diameter (ft) Velocity (ft/sec)- calculated  HRSG Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Mass flow (lb/hr) Stack Temperature (*F)	((diameter) <sup>2</sup> /4)	0 150 18 x 3.14159] / 60 sec/min 3,826,000 1,081 28,49 2,517,808 18 164.9 150 18	150 18 3,607,000 1,114 28,38 2,433,691 18 159,4 150 18	150 18 3,382,000 1,144 28.19 2,341,021 18 153.3	737,941  150 18  NA NA NA NA NA NA 150 18  3,856,721 189.0	150 18 18 NA NA NA NA NA NA NA NA NA NA NA NA NA	28,816 639,485 150 18 NA NA NA NA NA 150 18 3,408,622			

Note: Universal gas constant = 1,545 ft-lb(force)/oR; atmospheric pressure = 2,116.8 lb(force)/ft2; 14.7 lb/ft3.

Source: GE, 2006 - CT Performance Data; Golder, 2006 - DB Catculations.

TABLE A-2
MAXIMUM EMISSIONS FOR CRITERIA POLLUTANTS FOR THE HOPKINS UNIT 2 REPOWERING PROJECT
GE FRAME 7FA, DRY LOW NOX COMBUSTOR, NATURAL GAS, BASE LOAD, WITH NATURAL GAS DUCT FIRING

	Tu-ki-a	CT Only Inlet Temperate		vith Duct Burne • Inlet Temperat		
Parameter	4 FF 25 °F 3.5 4 5			25,°F w/DB &	e Inlet Temperat	95.°F w/DB
·	real distriction			Pikne K		<b>地位现</b>
Particulate from CT, DB, and SCR						
Total PM10 = PM10 (front half) + PM10 ((NH4)2SO4) from SCR or	nly					
a PM <sub>10</sub> (front half) (lb hr)						
CT- provided	9.0	9.0	9.0	9.0	9.0	9
DB (lb/hr) - calculated	0.0	0.0	0.0	9.2	8.5	8
Total CT/DB emission rate (lb/hr)	90	9.0	9.0	18.2	17.5	1.
b. PM <sub>10</sub> ((NH <sub>4</sub> ) <sub>2</sub> SO <sub>4</sub> ) from SCR only = Sulfur trioxide from conv	version of SO <sub>2</sub> converts to amm	onium sulfate (=	PM₁e)			
Particulate from conversion of SO <sub>2</sub> = SO <sub>2</sub> emissions (lb/hr) x						
conversion of SO,	to (NH4)2SO4 x lb (NH4)2SO4	lb SO <sub>3</sub>				
SO <sub>7</sub> emission rate (lb/hr)- calculated	10.5	9.9	9.3	14,7	13.8	1.3
Conversion (%) from SO <sub>2</sub> to SO <sub>3</sub>	9.8	9.8	9.8	9.8	9.8	
MW SO <sub>3</sub> / SO <sub>2</sub> (80/64)	1.3	1.3	1.3	1,3	1.3	
Conversion (%) from SO <sub>3</sub> to (NH <sub>4</sub> ) <sub>7</sub> (SO <sub>4</sub> )	100	100	100	100	100	ŀ
MW (NH <sub>4</sub> ) <sub>2</sub> SO <sub>4</sub> /SO <sub>5</sub> (132/80)	1.7	1.7	1.7	. 1.7	1.7	
SCR Particulate (fb/hr)- calculated	2.12	2.00	1.88	2.97	2.79	2.
, , , , , , , , , , , , , , , , , , ,						-
CT emission rate (lb/hr) {a + b} assumes SCR	11.1	11.0	10.9	11.1	11.0	10
HRSG stack emission rate (lb/hr) [a + b]	11.1	11.0	10.9	21.1	20.3	19
(fb.mmBtu, HHV)	0 0059	0.0061	0 0064	0 0079	0 008 \$	0.00
Sulfur Dioxide						
SO <sub>2</sub> (lb/hr)= Natural gas (scf/hr) v sulfur content(gr/100 scf) v 1 il	b/7000 gr x (lb SO <sub>2</sub> /lb S) /100					
Fuel use (cf/hr)	1,832,961	1,732,040	1,630,584	2,570,901	2,418,878	2,270,0
Sulfur content (grains/ 100 cf)	2	2	2	2	2	
1b SO <sub>2</sub> /lb S (64/32)	2	2	2	2	2	
CT emission rate (lb hr)	10.5	9.9	9.3	10.5	9.9	ę
HRSG stack emission rate (lb hr)	10.5	9,9	9.3	14.7	13.8	1
(lb/MW)	0.056	0.057	0.058			
Nitropen Oxides						
Nitrogen Oxides  NOx (BrOr) = NOx (commv4@ 15% Q.) x [[20.9 x (L-Moisture (%	(2/1001 - Oxwen, des(%)) x 21	16.8 lb/6 <sup>2</sup> x Volu	ne flow (acfm) x			
NOx (fb/hr) = NOx (ppmvd@ 15% O <sub>2</sub> ) x ([20.9 x (1-Moisture (%						
NOx (fb/hr) = NOx (ppmvd@ 15% O <sub>1</sub> ) x ([20.9 x (1-Moisture (% 46 (mole. wgt NOx) x 60 min/hr/[1545 x (CT te	mp (°F) + 460) x (20.9-15) x 1.	000,000 (adj. for	ppm)]	14.5	14.4	14
NOx (fb/hr) = NOx (ppmvd@ 15% O <sub>2</sub> ) x ([20.9 x (1-Moisture (% 46 (mole. wgt NOx) x 60 min/hr / [1545 x (CT te CT/DB, ppmvd @15% O <sub>2</sub>	mp (°F) + 460) x (20.9-15) x 1. 9	000,000 (adj. for 9	ppm)] 9	14.5 10.26	14.4 31.21	
NOx (fb/hr) = NOx (ppmvd@ 15% O <sub>2</sub> ) x ({20.9 x (1-Moisture (%) 46 (mole. wgt NOx) x 60 min/hr / [1545 x (CT tel CT/DB, ppmvd @15% O <sub>2</sub> Moisture (%)	mp (°F) + 460) x (20.9-15) x 1. 9 7.54	000,000 (adj. for 9 8.55	ppm)] 9 10.28	10.26	11.21	12.
NOx (fb/hr) = NOx (ppmvd@ 15% O <sub>2</sub> ) x ([20.9 x (1-Moisture (% 46 (mole. wgt NOx) x 60 min/hr / [1545 x (CT te CT/DB, ppmvd @15% O <sub>2</sub> Moisture (%) Oxygen (%)	mp (°F) + 460) x (20.9-15) x 1, 9 7.54 . 12.77	000,000 (adj. for 9 8.55 12.57	ppm)] 9	10.26 9.76	11.21 961	12. 9.
NOx (fb/hr) = NOx (ppmvd@ 15% O <sub>2</sub> ) x ({20.9 x (1-Moisture (%) 46 (mole. wgt NOx) x 60 min/hr / [1545 x (CT tel CT/DB, ppmvd @15% O <sub>2</sub> Moisture (%)	mp (°F) + 460) x (20.9-15) x 1. 9 7.54	000,000 (adj. for 9 8.55	ppm)] 9 10.28 12.22	10.26	11.21	12. 9. 2,373,6
NOx (fb/hr) = NOx (ppmvd@ 15% O <sub>2</sub> ) x ([20.9 x (1-Moisture (% 46 (mole. wgt NOx) x 60 min/hr / [1545 x (CT tet CT/DB, ppmvd @15% O <sub>2</sub> Moisture (%) Oxygen (%) Turbine Flow (acfm) Turbine Exhaust Temperature (°F)	mp (°F) + 460) x (20.9-15) x 1, 9 7.54 . 12.77 2,517,808 1,081	000,000 (adj. for 9 8.55 12.57 2,433,691 1,114	ppm)] 9 10.28 12.22 2,341,021 1,144	10.26 9.76 2,553,753 1,081	11.21 9 61 2,468.107 1,114	12. 9, 2,373,6 , 1,1
NOx (fb/hr) = NOx (ppmvd@ 15% O <sub>2</sub> ) x ([20.9 x (1-Moisture (% 46 (mole. wgt NOx) x 60 min/hr / [1545 x (CT tel CT/DB, ppmvd @15% O <sub>2</sub> Moisture (%) Oxygen (%) Turbine Flow (acfin)	mp (°F) + 460) x (20.9-15) x 1.7 9 7.54 12.77 2,517,808	000,000 (adj. for 9 8.55 12.57 2,433,691	ppm)] 9 10.28 12.22 2,341,021	10.26 9.76 2.553,753 1,081	11.21 9 61 2,468.107 1,114	12. 9. 2,373,6 , 1,1
NOx (fb/hr) = NOx (ppmvd@ 15% O <sub>2</sub> ) x ([20.9 x (1-Moisture (% 46 (mole. wgt NOx) x 60 min/hr / [1545 x (CT tec CT/DB, ppmvd @15% O <sub>2</sub> Moisture (%) Oxygen (%) Turbine Flow (acfin) Turbine Exhaust Temperature (°F)  CT emission rate (lb/hr)	mp (°F) + 460) x (20.9-15) x 1.7 9 7.54 . 12.77 2,517,808 1,081	000,000 (adj. for 9 8.55 12.57 2,433,691 1,114 58.4	ppm)] 9 10.28 12.22 2,341,021 1,144 55.0	10.26 9.76 2,553,753 1,081	9 61 2,468.107 1,114 58.4 NA	12. 9, 2,373,6 1,1 55
NOx (Br/hr) = NOx (ppmvd@ 15% O <sub>2</sub> ) x ([20.9 x (1-Moisture (% 46 (mole. wgt NOx) x 60 min/hr / [1545 x (CT tet CT/DB, ppmvd @15% O <sub>2</sub> Moisture (%) Oxygen (%) Turbine Flow (acfin) Turbine Exhaust Temperature (°F)  CT emission rate (Ib/hr) (Ib/MW) HRSG emission rate (Ib/hr)	mp (°F) + 460) x (20.9-15) x 1.7 9 7.54 . 12.77 2,517.808 1.081 61.8 0.3	000,000 (adj. for 9 8.55 12.57 2,433,691 1,114 58.4 0.3	ppm)] 9 10.28 12.22 2,341,021 1,144 55.0 0.3 55.0	10.26 9.76 2,553,753 1,081 61.8 NA 138.2	11.21 9 61 2.468.107 1.114 58.4 NA 129.5	12. 9. 2,373,6 , 1,1 55 N
NOx (fb/hr) = NOx (ppmvd@ 15% O <sub>2</sub> ) x ([20.9 x (1-Moisture (% 46 (mole. wgt NOx) x 60 min/hr / [1545 x (CT tec. CT/DB, ppmvd @15% O <sub>2</sub> Moisture (%) Oxygen (%) Turbine Flow (acfm) Turbine Exhaust Temperature (*F)  CT emission rate (fb/hr) (fb/MW) HRSG emission rate (fb/hr) HRSG stack emission rate (fb/hr) HRSG Stack emission rate (fb/hr)	mp (°F) + 460) x (20.9-15) x 1.7 9 7.54 12.77 2,517,808 1,081 61.8 0.3 61.8 5.0 34.3	000,000 (adj. for 9  8.55 12.57 2.433,691 1,114 58.4 0.3 58.4 5.0 32.4	ppm)]  9 10.28 12.22 2,341,021 1,144  55.0 0.3 55.0 5 0 30.5	10.26 9.76 2,553,753 1,081 61.8 NA	9 61 2,468.107 1,114 58.4 NA	12. 9. 2,373,6 1,1 55 N 121
NOx (fb/hr) = NOx (ppmvd@ 15% O <sub>2</sub> ) x ([20.9 x (1-Moisture (% 46 (mole. wgt NOx) x 60 min/hr / [1545 x (CT tet CT/DB, ppmvd @15% O <sub>2</sub> Moisture (%) Oxygen (%) Turbine Flow (acfin) Turbine Exhaust Temperature (°F)  CT emission rate (fb/hr) (fb/MW)  HRSG emission rate (fb/hr)  HRSG stack emission rate (fb/hr) (fb/MW)	mp (°F) + 460) x (20.9-15) x 1.7 9 7.54 . 12.77 2.517.808 1.081 61.8 0.3 61.8 5.0	000,000 (adj. for 9 8.55 12.57 2,433,69) 1,114 58.4 0.3 58.4 5.0	ppm)]  9 10.28 12.22 2.341,021 1,144  55.0 0.3 55.0 5 0	10.26 9.76 2,553,753 1,081 61.8 NA 138.2 5.0	11.21 9 61 2.468.107 1.114 58.4 NA 129.5 5.0	144 12. 9. 2.373,6 1,1: 55 N 121 5
NOx (fb/hr) = NOx (ppmvd@ 15% O <sub>2</sub> ) x ([20.9 x (1-Moisture (% 46 (mole. wgt NOx) x 60 min/hr / [1545 x (CT tec CT/DB, ppmvd @15% O <sub>2</sub> Moisture (%) Oxygen (%) Oxygen (%) Turbine Flow (acfm) Turbine Exhaust Temperature (°F)  CT emission rate (lb/hr) (lb/MW)  HRSG emission rate (lb/hr) HRSG stack emission rate (lb/hr) (lb/MW)  Carbon Monoxids	mp (°F) + 460) x (20.9-15) x 1, 9 7.54 12.77 2,517,808 1,081 61.8 0.3 61.8 5.0 34.3 0.18	000,000 (adj. for 9  8.55 12.57 2.433,691 1,114 58.4 0.3 58.4 5.0 32.4	ppm)]  9 10.28 12.22 2,341,021 1,144  55.0 0.3 55.0 5 0 30.5	10.26 9.76 2,553,753 1,081 61.8 NA 138.2 5.0	11.21 9 61 2.468.107 1.114 58.4 NA 129.5 5.0	12. 9. 2,373,6 1,1 55 N 121
NOx (fb/hr) = NOx (ppmvd@ 15% O <sub>2</sub> ) x ([20.9 x (1-Moisture (% 46 (mole. wgt NOx) x 60 min/hr / [1545 x (CT tec CT/DB, ppmvd @15% O <sub>2</sub> Moisture (%) Oxygen (%) Oxygen (%) Turbine Flow (acfin) Turbine Exhaust Temperature (°F)  CT emission rate (lb/hr)	mp (°F) + 460) x (20.9-15) x 1, 9 7.54 12.77 2,517,808 1,081 61.8 0.3 61.8 5.0 34.3 0.18	000,000 (adj. for 9 8.55 12.57 2.433,691 1.114 58.4 0.3 58.4 5.0 32.4 0.19	ppm)]  9 10.28 12.22 2,341,021 1,144  55.0 0.3 55.0 5 0 30.5	10.26 9.76 2,553,753 1,081 61.8 NA 138.2 5.0	11.21 9 61 2.468.107 1.114 58.4 NA 129.5 5.0	12. 9. 2,373,6 1,1 55 N 121
NOx (Br/hr) = NOx (ppmvd@ 15% O <sub>2</sub> ) x ([20.9 x (1-Moisture (% 46 (mole. wgt NOx) x 60 min/hr / [1545 x (CT tec. CT/DB, ppmvd @ 15% O <sub>2</sub> Moisture (%)  Turbine Flow (acfin)  Turbine Exhaust Temperature (°F)  CT emission rate (Ib/hr)  (Ib/MW)  HRSG emission rate (Ib/hr)  HRSG stack emission rate, ppmvd @ 15% O <sub>2</sub> HRSG Stack emission rate (Ib/hr)  (Ib/MW)  Carbon Monoxide  CO (Ib/hr) = CO(ppm) x [1 - Moisture(%)/100] x 2116.8 Ib/f <sup>2</sup> x \ 28 (mole. wgt CO) x 60 min/hr / [1545 x (CT temp	mp (°F) + 460) x (20.9-15) x 1.7 9 7.54 12.77 2,517.808 1.081 61.8 0.3 61.8 5.0 34.3 0.18  Volume flow (acfm) x 0.(°F) + 460°F) x 1,000,000 (adj	000,000 (adj. for 9 8.55 12.57 2.433,691 1,114 58.4 0.3 58.4 5.0 32.4 0.19	ppm)] 9 10.28 12.22 2.341,021 1,144 55.0 0.3 55.0 5 0 30.5 0.19	10.26 9.76 2.553.753 1.081 61.8 NA 138.2 5.0 47.8	11.21 9 61 2.468.107 1.114 58.4 NA 129.5 5.0 45 0	12. 9. 2,373,6 1,1 52 N 121 53
NOx (fb/hr) = NOx (ppmvd@ 15% O <sub>2</sub> ) x ([20.9 x (1-Moisture (% 46 (mole. wgt NOx) x 60 min/hr / [1545 x (CT tec. CT/DB, ppmvd @ 15% O <sub>2</sub> Moisture (%) Oxygen (%) Turbine Flow (acfm) Turbine Flow (acfm) Turbine Exhaust Temperature (°F)  CT emission rate (lb/hr) (lb/MW) HRSG emission rate (lb/hr) HRSG stack emission rate (lb/hr) (lb/MW)  Carbon Monoxide CO (fb/hr) = CO(ppm) x [1 - Moisture(%)/100] x 2116.8 lb/ft² x N 28 (mole. wgt CO) x 60 min/hr / [1545 x (CT temp Basis, ppmvd]	mp (°F) + 460) x (20.9-15) x 1, 9 7.54 12.77 2,517,808 1,081 61.8 0.3 61.8 5.0 34.3 0.18	000,000 (adj. for 9 8.55 12.57 2.433,691 1,114 58.4 0.3 58.4 5.0 32.4 0.19	ppm)]  9 10.28 12.22 2.341,021 1,144 55.0 0.3 55.0 5 0 30.5 0.19	10.26 9.76 2.553.753 1.081 61.8 NA 138.2 5.0 47.8	11.21 9 61 2.468.107 1,114 58.4 NA 129.5 5.0 45 0	12. 9. 2,373,6 , 1,1 55 N 121 5
NOx (fb/hr) = NOx (ppmvd@ 15% O <sub>2</sub> ) x ([20.9 x (1-Moisture (% 46 (mole. wgt NOx) x 60 min/hr / [1545 x (CT tec. CT/DB, ppmvd @15% O <sub>2</sub> Moisture (%) Oxygen (%) Oxygen (%) Oxygen (%)  CT emission rate (ib/hr) (ib/MW)  HRSG emission rate (ib/hr) HRSG stack emission rate (ib/hr) (ib/MW)  Carbon Monoxids  CO (ib/hr) = CO(ppm) x [1 - Moisture(%)/100] x 2116.8 lb/ft² x N 28 (mole. wgt CO) x 60 min/hr / [1545 x (CT temp Basis, ppmvd @ 15% O2 - calculated	mp (°F) + 460) x (20.9-15) x 1.7 9 7.54 12.77 2,517.808 1.081 61.8 0.3 61.8 5.0 34.3 0.18  Volume flow (acfin) x 9.(°F) + 460°F) x 1,000,000 (adj 9.99	000,000 (adj. for 9 8.55 12.57 2,433,691 1,114 58.4 0.3 58.4 5.0 32.4 0.19	ppm)] 9 10.28 12.22 2.341,021 1,144 55.0 0.3 55.0 5 0 30.5 0.19	10.26 9.76 2.553.753 1,081 61.8 NA 138.2 5.0 47.8	11.21 9 61 2.468.107 1.114 58.4 NA 129.5 5.0 45 0	12. 9. 2,373,6 , 1,1 55 121 5 42
NOx (fb/hr) = NOx (ppmvd@ 15% O <sub>2</sub> ) x ([20.9 x (1-Moisture (% 46 (mole. wgt NOx) x 60 min/hr / [1545 x (CT tec. CT/DB, ppmvd @ 15% O <sub>2</sub> Moisture (%) Oxygen (%) Oxygen (%) Turbine Flow (acfm) Turbine Exhaust Temperature (*F)  CT emission rate (fb/hr) (fb/MW) HRSG emission rate (fb/hr) HRSG stack emission rate (fb/hr) (fb/MW)  Carbon Monoxide CO (fb/hr) = CO(ppm) x [1 - Moisture(%)/100] x 2116.8 lb/ft <sup>2</sup> x V 28 (mole. wgt CO) x 60 min/hr / [1545 x (CT temp Basis, ppmvd @ 15% O2 - calculated Moisture (%)	mp (°F) + 460) x (20.9-15) x 1, 9 7.54 12.77 2,517,808 1,081 61.8 0.3 61.8 5.0 34.3 0.18  Volume flow (acfin) x 0.(°F) + 460°F) x 1,000,000 (adj 12 9.99 7.54	000,000 (adj. for 9 8.55 12.57 2.433,691 1.114 58.4 0.3 58.4 5.0 32.4 0.19 . for ppm)] 12 9.90 8.55	ppm)] 9 10.28 12.22 2,341,021 1,144 55.0 0.3 55.0 5 0 30.5 0.19	10.26 9.76 2.553.753 1.081 61.8 NA 138.2 5.0 47.8 28.6 16.8 10.26	11.21 9 61 2,468.107 1,114 58.4 NA 129.5 5.0 45 0	12. 9, 2,373,6 1,1 52 N 121 2 42
NOx (fb/hr) = NOx (ppmvd@ 15% O <sub>2</sub> ) x ([20.9 x (1-Moisture (% 46 (mole. wgt NOx) x 60 min/hr / [1545 x (CT tec. CT/DB, ppmvd @15% O <sub>2</sub> Moisture (%) Oxygen (%) Oxygen (%) Oxygen (%)  CT emission rate (ib/hr) (ib/MW)  HRSG emission rate (ib/hr) HRSG stack emission rate (ib/hr) (ib/MW)  Carbon Monoxids  CO (ib/hr) = CO(ppm) x [1 - Moisture(%)/100] x 2116.8 lb/ft² x N 28 (mole. wgt CO) x 60 min/hr / [1545 x (CT temp Basis, ppmvd @ 15% O2 - calculated	mp (°F) + 460) x (20.9-15) x 1.2 9 7.54 12.77 2,517.808 1,081 61.8 0.3 61.8 5.0 34.3 0.18  Volume flow (acfm) x 0.(°F) + 460°F) x 1,000,000 (adj 12 9.99 7.54 12.77	000,000 (adj. for 9 8.55 12.57 2.433,691 1,114 58.4 0.3 58.4 5.0 32.4 0.19 12 9.90 8.55 12.57	ppm)]  9 10.28 12.22 2.341,021 1,144  55.0 0.3 55.0 5 0 30.5 0.19	10.26 9.76 2.553.753 1.081 61.8 NA 138.2 5.0 47.8 28.6 16.8 10.26 9.76	11.21 9 61 2.468.107 1,114 58.4 NA 129.5 5.0 45 0	12. 9. 2,373,6 1,1 55 N 121 42 42 28 166 12. 9.
NOx (Br/hr) = NOx (ppmvd@ 15% O <sub>2</sub> ) x ([20.9 x (1-Moisture (% 46 (mole. wgt NOx) x 60 min/hr / [1545 x (CT tec. CT/DB, ppmvd @ 15% O <sub>2</sub> Moisture (%)  Moisture (%)  Turbine Flow (acfm)  Turbine Exhaust Temperature (°F)  CT emission rate (Ib/hr)  (Ib/MW)  HRSG emission rate (Ib/hr)  HRSG stack emission rate, ppmvd @ 15% O <sub>2</sub> HRSG Stack emission rate (Ib/hr)  (Ib/MW)  Carbon Monoxids  CO (Ib/hr) = CO(ppm) x [1 - Moisture(%)/100] x 2116.8 Ib/ft <sup>2</sup> x \ 28 (mole. wgt CO) x 60 min/hr / [1545 x (CT temp Basis, ppmvd @ 15% O <sub>2</sub> - calculated Moisture (%)  Oxygen (%)	mp (°F) + 460) x (20.9-15) x 1, 9 7.54 12.77 2,517,808 1,081 61.8 0.3 61.8 5.0 34.3 0.18  Volume flow (acfin) x 0.(°F) + 460°F) x 1,000,000 (adj 12 9.99 7.54	000,000 (adj. for 9 8.55 12.57 2.433,691 1.114 58.4 0.3 58.4 5.0 32.4 0.19 . for ppm)] 12 9.90 8.55	ppm)] 9 10.28 12.22 2,341,021 1,144 55.0 0.3 55.0 5 0 30.5 0.19	10.26 9.76 2.553.753 1.081 61.8 NA 138.2 5.0 47.8 28.6 16.8 10.26	11.21 9 61 2,468.107 1,114 58.4 NA 129.5 5.0 45 0	12. 9, 2,373,6 1,1 5: N 121 4: 4:
NOx (fb/hr) = NOx (ppmvd@ 15% O <sub>2</sub> ) x ([20.9 x (1-Moisture (% 46 (mole, wgt NOx) x 60 min/hr / [1545 x (CT tec. CT/DB, ppmvd @ 15% O <sub>2</sub> Moisture (%) Oxygen (%) Turbine Flow (acfm) Turbine Exhaust Temperature (°F)  CT emission rate (fb/hr) (fb/MW) HRSG emission rate (fb/hr) HRSG stack emission rate (fb/hr) (fb/MW)  Carbon Monoxide CO (fb/hr) = CO(ppm) x [1 - Moisture(%)/100] x 2116.8 fb/f² x \( 28 \) (mole, wgt CO) x 60 min/hr / [1545 x (CT temp Basis, ppmvd @ 15% O2 - calculated Moisture (%) Oxygen (%) Turbine Flow (acfm)	mp (°F) + 460) x (20.9-15) x 1.7 9 7.54 12.77 2,517.808 1,081 61.8 0.3 61.8 5.0 34.3 0.18  Volume flow (acfin) x 1.(°F) + 460°F) x 1,000,000 (adj 2.9.99 7.54 12.77 2,517.808	000,000 (adj. for 9 8.55 12.57 2.433,691 1,114 58.4 0.3 58.4 5.0 32.4 0.19 12 9.90 8.55 12.57 2.433,691	ppm)]  9 10.28 12.22 2.341,021 1,144  55.0 0.3 55.0 5 0 30.5 0.19  12 9.73 10.28 12.22 2.341,021	10.26 9.76 2.553.753 1.081 61.8 NA 138.2 5.0 47.8 28.6 16.8 30.26 9.76 2.553.753	11.21 9 61 2.468.107 1,114 58.4 NA 129.5 5.0 45 0	12. 9. 2.373,6 1,1 5: N 12: 4: 4: 4: 28 16: 12. 9.

TABLE A-2

MAXIMUM EMISSIONS FOR CRITERIA POLLUTANTS FOR THE HOPKINS UNIT 2 REPOWERING PROJECT
GE FRAME 7FA, DRY LOW NOX COMBUSTOR, NATURAL GAS, BASE LOAD, WITH NATURAL GAS DUCT FIRING

	Turkin	CT Only Inlet Temperate	CT with Duct Burner Turbine Inlet Temperature			
Parameter	25°T		95 97	25 °F w/DB	59 'F W/DB	
Volatile Organic Compounds	. 1, 1, 2, 3			4 100		70.4
VOCs (fb/hr) = VOC(ppmvd) x [1-Moisture(%)/100] x 2116 8 1	L/A <sup>2</sup> - Val					
16 (mole. wgt as methane) x 60 min/hr / [1545 x (CT ter		i 60				
To those. We as members to the market (1543 x (C) to	up.( r) + 400 r) x 1,000,000 (ac	g. roi ppmjj				
Basis, ppmvw	3.50	3.50	3.50	8.6	8.7	٤
Basis, ppmvd @ 15% O2 - calculated	3.15	3.16	3.16	5.67	5.71	5.
Moisture (%)	7.54	8.55	10 28	10 26	11.21	12.
Oxygen (%) wet	12.77	12.57	12.22	9.76	9.61	9.
Oxygen (%) dry						
Turbine Flow (actim)	2,517,808	2,433,691	2,341,021	2,553,753	2,468,107	2,373,6
Turbine Exhaust Temperature (°F)	180,1	1,114	1,144	180.1	1,114	1,1
CT emission rate (lb/hr)	7.52	7.12	6.72	7.52	7.12	6.
HRSG stack Emission rate (fb/hr)	7.52	7.12	6.72	16.70	15.66	14.
Sulfuric Acid Mist						
Sulfuric Acid Must (lb/hr)= SO <sub>2</sub> emission (lb/hr) x Conversion to	H <sub>2</sub> SO <sub>4</sub> (% by weight)/100					
CT SO <sub>2</sub> emission rate (lb/br) - provided	10.5	9.9	9.3	10.5	9.9	,
CT Conversion to H2SO4 (% by weight) - provided	10	10	10	10	10	
DB SO <sub>2</sub> emission rate (lb/hr) - provided	0	0	0	4	4	
DB Conversion to H <sub>2</sub> SO <sub>4</sub> (%) - provided	20	20	20	20	20	
CT emission rate (lb/hr)	1.05	0 99	0.93	1 05	0 99	0.
HRSG stack Emission rate (lb/hr)	1.05	0.99	0 93	1 89	1.77	- 1
Lead						
Lead (fb/hr) = NA						
Emission Rate Basis	NA	NA	NA	NA	NA	١
CT emission rate (lb/hr)	NA	NA	NA	NA	NA	r
HRSG stack Emission rate (lb/hr)	NA	NA	NA	NA	NA	N

Source: GE, 2006 - CT Performance Data; Golder, 2006 - DB Calculations.

TABLE A-3 DESIGN INFORMATION AND STACK PARAMETERS FOR THE HOPKINS UNIT 2 REPOWERING PROJECT GE FRAME 7FA, DRY LOW NO $_{\rm X}$  COMBUSTOR, NATURAL GAS, 75% LOAD

Combustion Turbine Performance Power output (MW) Heat rate (Btu/kWh, LHV)	140.9 9.840 10,923 1,387 1,539 87 20,714 22,993 1.110  3,019,000 3,019,000 1,136 7.66 12.64 28.48  Heat Content, Btu/ 1,387 20,714	130.8 10,080 11,189 1,319 1,464 78 20,714 22,993 1.110 2,905,000 2,905,000 1,161 8.45 12.57 28.39	95 °F  120 10,4 11,5: 1,2: 1,3: 20,7! 22,95 1.11  2,798,00 2,798,00 1,18 9,7 12,4 28,2
Power output (MW) Heat rate (Btu/kWh, LHV) (Btu/kWh, HHV) Heat Input (MMBtu/hr, LHV) (MMBtu/hr, LHV) (MMBtu/hr, HHV) Relative Humidity (%) Fuel heating value (Btu/lb, LHV) (Btu/lb, HHV) (HHV/LHV)  CT Exhaust Flow Mass Flow (lb/hr)- with no margin - provided  Temperature (°F) Moisture (% Vol.) Oxygen (% Vol.) Molecular Weight  Fuel Usage Fuel usage (lb/hr) = Heat Input (MMBtu/hr) x 1,000,000 Btu/MMBtu (Fuel input (MMBtu/hr, LHV) Heat content (Btu/lb, LHV) Fuel usage (lb/hr)- calculated  Heat content (Btu/cf, LHV)- assumed Fuel density (lb/h²) Fuel usage (cf/hr)- calculated  Bypass Stack and Flow Conditions Stack Height (fi) Diameter (fi)  Velocity (ft/sec) = Volume flow (acfm) / [((diameter)² /4) x 3.14159] / 60 sec	9,840 10,923 1,387 1,539 87 20,714 22,993 1,110 3,019,000 3,019,000 1,136 7.66 12,64 28,48 Heat Content, Btu/	10,080 11,189 1,319 1,464 78 20,714 22,993 1,110 2,905,000 2,905,000 1,161 8,45 12.57 28.39	10,4 11,5: 1,2: 1,3: 20,7: 22,9: 1.11 2,798,00 2,798,00 1,18: 9.7
Heat rate (Btu/kWh, LHV) (Btu/kWh, HHV) Heat Input (MMBtu/hr, LHV) (MMBtu/hr, LHV) (Relative Humidity (%) Fuel heating value (Btu/lb, LHV) (Btu/lb, HHV) (HHV/LHV)  CT Exhaust Flow Mass Flow (lb/hr)- with no margin - provided  Temperature (*F) Moisture (*Vol.) Oxygen (*Vol.) Molecular Weight  Fuel Usage Fuel usage (lb/hr) = Heat Input (MMBtu/hr) x 1,000,000 Btu/MMBtu (Fuel Beat Input (Btu/lb, LHV) Fuel usage (lb/hr)- calculated  Heat content (Btu/cf, LHV)- assumed Fuel density (lb/ft³) Fuel usage (cf/hr)- calculated  Bypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfm) / {((diameter)² /4) x 3.14159} / 60 sec	9,840 10,923 1,387 1,539 87 20,714 22,993 1,110 3,019,000 3,019,000 1,136 7.66 12,64 28,48 Heat Content, Btu/	10,080 11,189 1,319 1,464 78 20,714 22,993 1,110 2,905,000 2,905,000 1,161 8,45 12.57 28.39	10,4 11,5: 1,2: 1,3: 20,7: 22,9: 1.11 2,798,00 2,798,00 1,18: 9.7
(Btu/kWh, HHV)  Heat Input (MMBtu/hr, LHV) (MMBtu/hr, LHV) (Belative Humidity (%)  Fuel heating value (Btu/lb, LHV) (Btu/lb, HHV) (HHV/LHV)  CT Exhaust Flow Mass Flow (Ib/hr)- with no margin - provided  Temperature (*F) Moisture (% Vol.) Oxygen (% Vol.) Molecular Weight  Fuel Usage Fuel usage (Ib/hr) = Heat Input (MMBtu/hr) x 1,000,000 Btu/MMBtu (Fuel Belta input (MMBtu/hr, LHV) Heat content (Btu/b, LHV) Fuel usage (Ib/hr)- calculated  Heat content (Btu/cf, LHV)- assumed Fuel density (Ib/ft³) Fuel usage (cf/hr)- calculated  Bypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfm) / {((diameter)² /4) x 3.14159] / 60 sec	10,923 1,387 1,539 87 20,714 22,993 1.110 3,019,000 3,019,000 1,136 7.66 12.64 28.48	11,189 1,319 1,464 78 20,714 22,993 1,110 2,905,000 2,905,000 1,161 8,45 12.57 28.39	10,4 11,5: 1,2: 1,3: 20,7: 22,9: 1.11 2,798,00 2,798,00 1,18: 9.7
Heat Input (MMBtu/hr, LHV) (MMBtu/hr, HHV) Relative Humidity (%) Fuel heating value (Btu/lb, LHV) (Btu/lb, HHV) (HHV/LHV)  CT Exhaust Flow Mass Flow (lb/hr)- with no margin - provided  Temperature (°F) Moisture (% Vol.) Oxygen (% Vol.) Molecular Weight  Fuel Usage Fuel usage (lb/hr) = Heat Input (MMBtu/hr) x 1,000,000 Btu/MMBtu (Fuel Bette input (MMBtu/hr, LHV) Heat content (Btu/lb, LHV) Fuel usage (lb/hr)- calculated  Heat content (Btu/cf, LHV)- assumed Fuel density (lb/ft³) Fuel density (lb/ft³) Fuel usage (cf/hr)- calculated  Bypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfm) / {((diameter)² /4) x 3.14159] / 60 sec	1,387 1,539 87 20,714 22,993 1.110 3,019,000 3,019,000 1,136 7.66 12.64 28.48	11,189 1,319 1,464 78 20,714 22,993 1,110 2,905,000 2,905,000 1,161 8,45 12.57 28.39	11,5: 1,2: 1,3: 20,7: 22,9: 1.11 2,798,00 2,798,00 1,18: 9.7:
(MMBtu/hr, HHV)  Relative Humidity (%)  Fuel heating value (Btu/lb, LHV)	1,387 1,539 87 20,714 22,993 1.110 3,019,000 3,019,000 1,136 7.66 12.64 28.48	1,319 1,464 78 20,714 22,993 1,110  2,905,000 2,905,000 1,161 8,45 12,57 28,39	1,2: 1,3: 20,7 22,99 1.1: 2,798,00 2,798,00 1,18: 9.7
Relative Humidity (%)  Fuel heating value (Btu/lb, LHV)	1,539 87 20,714 22,993 1.110 3,019,000 3,019,000 1,136 7.66 12.64 28.48 Heat Content, Btu/ 1,387	1,464 78 20,714 22,993 1,110 2,905,000 2,905,000 1,161 8,45 12.57 28.39	2,798,00 2,798,00 1,18 2,798,00 1,18 9,5
Fuel heating value (Btu/lb, LHV) (Btu/lb, HHV) (HHV/LHV)  CT Exhaust Flow Mass Flow (lb/hr)- with no margin - provided  Temperature (°F) Moisture (% Vol.) Oxygen (% Vol.) Molecular Weight  Fuel Usage Fuel usage (lb/hr) = Heat Input (MMBtu/hr) x 1,000,000 Btu/lMMBtu (Fuel Beat input (MMBtu/hr, LHV) Heat content (Btu/lb, LHV) Fuel usage (lb/hr)- calculated  Heat content (Btu/cf, LHV)- assumed Fuel density (lb/ft³) Fuel usage (cf/hr)- calculated  3ypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfm) / {((diameter)²/4) x 3.14159] / 60 sec	87 20,714 22,993 1.110 3,019,000 3,019,000 1,136 7.66 12.64 28.48 Heat Content, Btu/ 1,387	78 20,714 22,993 1.110  2,905,000 2,905,000 1,161 8.45 12.57 28.39	20,7 22,9 1.1 2,798,00 2,798,00 1,18 9.0
(Btu/lb, HHV) (HHV/LHV)  CT Exhaust Flow Mass Flow (lb/hr)- with no margin - provided  Temperature (°F) Moisture (% Vol.) Oxygen (% Vol.) Molecular Weight  Fuel Usage Fuel usage (lb/hr) = Heat Input (MMBtu/hr) x 1,000,000 Btu/lMMBtu (Fuel Bette Heat input (MMBtu/hr, LHV) Heat content (Btu/lb, LHV) Fuel usage (lb/hr)- calculated  Heat content (Btu/cf, LHV)- assumed Fuel density (lb/ft³) Fuel usage (cf/hr)- calculated  3ypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfm) / {((diameter)²/4) x 3.14159} / 60 sec	20,714 22,993 1.110 3,019,000 3,019,000 1,136 7.66 12.64 28.48 Heat Content, Btu/ 1,387	20,714 22,993 1.110 2,905,000 2,905,000 1,161 8.45 12.57 28.39	20,7 22,9 1.1 2,798,00 2,798,00 1,11 9.
(Btu/lb, HHV) (HHV/LHV)  CT Exhaust Flow Mass Flow (lb/hr)- with no margin - provided  Temperature (°F) Moisture (% Vol.) Oxygen (% Vol.) Molecular Weight  Fuel Usage Fuel usage (lb/hr) = Heat Input (MMBtu/hr) x 1,000,000 Btu/lMMBtu (Fuel Bette Heat input (MMBtu/hr, LHV) Heat content (Btu/lb, LHV) Fuel usage (lb/hr)- calculated  Heat content (Btu/cf, LHV)- assumed Fuel density (lb/ft³) Fuel usage (cf/hr)- calculated  Bypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfm) / {((diameter)² /4) x 3.14159} / 60 sec	22,993 1.110 3,019,000 3,019,000 1,136 7.66 12.64 28.48 Heat Content, Btu/ 1,387	22,993 1.110 2,905,000 2,905,000 1,161 8.45 12.57 28.39	22,9 1.1 2,798,00 2,798,00 1,10 9.0 12.0
CT Exhaust Flow  Mass Flow (lb/hr)- with no margin - provided  Temperature (°F) Moisture (% Vol.) Oxygen (% Vol.) Oxygen (% Vol.) Molecular Weight  Fuel Usage Fuel usage (lb/hr) = Heat Input (MMBtu/hr) x 1,000,000 Btu/MMBtu (Fuel Bett Input (MMBtu/hr, LHV) Heat input (MMBtu/hr, LHV) Fuel usage (lb/hr)- calculated  Heat content (Btu/cf, LHV)- assumed Fuel density (lb/ft³) Fuel usage (cf/hr)- calculated  Bypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfm) / {((diameter)² /4) x 3.14159} / 60 sec	3,019,000 3,019,000 1,136 7.66 12.64 28.48 Heat Content, Btu/ 1,387	2,905,000 2,905,000 1,161 8.45 12.57 28.39	2,798,00 2,798,00 1,18 9.0
Mass Flow (lb/hr)- with no margin - provided  Temperature (°F) Moisture (% Vol.) Oxygen (% Vol.) Molecular Weight  Fuel Usage Fuel usage (lb/hr) = Heat Input (MMBtu/hr) x 1,000,000 Btu/MMBtu (Fuel B Heat input (MMBtu/hr, LHV) Heat content (Btu/lb, LHV) Fuel usage (lb/hr)- calculated  Heat content (Btu/cf, LHV)- assumed Fuel density (lb/ft³) Fuel usage (cf/hr)- calculated  Bypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfm) / {((diameter)²/4) x 3.14159} / 60 sec	3,019,000 1,136 7.66 12.64 28.48 Heat Content, Btu/ 1,387	2,905,000 1,161 8.45 12.57 28.39	2,798,00 1,18 9.5 12.4
- provided  Temperature (°F) Moisture (% Vol.) Oxygen (% Vol.) Molecular Weight  Fuel Usage Fuel usage (lb/hr) = Heat Input (MMBtu/hr) x 1,000,000 Btu/MMBtu (Fuel Beat Input (MMBtu/hr, LHV) Heat content (Btu/lb, LHV) Fuel usage (lb/hr)- calculated  Heat content (Btu/cf, LHV)- assumed Fuel density (lb/ft³) Fuel usage (cf/hr)- calculated  Bypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfm) / {((diameter)²/4) x 3.14159} / 60 sec	3,019,000 1,136 7.66 12.64 28.48 Heat Content, Btu/ 1,387	2,905,000 1,161 8.45 12.57 28.39	2,798,00 1,18 9.1 12.4
Temperature (°F) Moisture (% Vol.) Oxygen (% Vol.) Molecular Weight  Eucl Usage Fucl usage (lb/hr) = Heat Input (MMBtu/hr) x 1,000,000 Btu/MMBtu (Fuel if Heat input (MMBtu/hr, LHV) Heat content (Btu/lb, LHV) Fuel usage (lb/hr)- calculated  Heat content (Btu/cf, LHV)- assumed Fuel density (lb/ft³) Fuel usage (cf/hr)- calculated  Bypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfm) / {((diameter)²/4) x 3.14159} / 60 sec	1,136 7.66 12.64 28.48 Heat Content, Btu/ 1,387	2,905,000 1,161 8.45 12.57 28.39	2,798,00 1,18 9.5 12.4
Moisture (% Vol.) Oxygen (% Vol.) Molecular Weight  Fuel Usage Fuel usage (lb/hr) = Heat Input (MMBtu/hr) x 1,000,000 Btu/IMMBtu (Fuel is Heat input (MMBtu/hr, LHV) Heat content (Btu/lb, LHV) Fuel usage (lb/hr)- calculated  Heat content (Btu/cf, LHV)- assumed Fuel density (lb/ft³) Fuel usage (cf/hr)- calculated  Bypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfm) / {((diameter)²/4) x 3.14159} / 60 sec	1,136 7.66 12.64 28.48 Heat Content, Btu/ 1,387	1,161 8.45 12.57 28.39	1,18 9.1 12.4
Oxygen (% Vol.) Molecular Weight  Fuel Usage Fuel usage (lb/hr) = Heat Input (MMBtu/hr) x 1,000,000 Btu/MMBtu (Fuel it Heat input (MMBtu/hr, LHV) Heat content (Btu/b, LHV) Fuel usage (lb/hr)- calculated  Heat content (Btu/cf, LHV)- assumed Fuel density (lb/ft³) Fuel usage (cf/hr)- calculated  Bypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfm) / {((diameter)²/4) x 3.14159} / 60 sec	7.66 12.64 28.48 Heat Content, Btu/ 1,387	8.45 12.57 28.39	9.1 12.4
Molecular Weight  Fuel Usage Fuel usage (lb/hr) = Heat Input (MMBtu/hr) x 1,000,000 Btu/MMBtu (Fuel if Heat input (MMBtu/hr, LHV) Heat content (Btu/b, LHV) Fuel usage (lb/hr)- calculated  Heat content (Btu/cf, LHV)- assumed Fuel density (lb/ft <sup>3</sup> ) Fuel usage (cf/hr)- calculated  Bypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfm) / {((diameter) <sup>1</sup> /4) x 3.14159} / 60 sec	28.48 Heat Content, Btu/ 1,387	12.57 28.39	12.4
Fuel Usage Fuel usage (lb/hr) = Heat Input (MMBtu/hr) x 1,000,000 Btu/MMBtu (Fuel is Heat input (MMBtu/hr, LHV) Heat content (Btu/lb, LHV) Fuel usage (lb/hr)- calculated  Heat content (Btu/cf, LHV)- assumed Fuel density (lb/ft³) Fuel usage (cf/hr)- calculated  Bypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfm) / [((diameter)² /4) x 3.14159] / 60 sec	28.48 Heat Content, Btu/ 1,387	28.39	
Fuel usage (lb/hr) = Heat Input (MMBtu/hr) x 1,000,000 Btu/MMBtu (Fuel if Heat input (MMBtu/hr, LHV) Heat content (Btu/lb, LHV) Fuel usage (lb/hr)- calculated  Heat content (Btu/cf, LHV)- assumed Fuel density (lb/ft³) Fuel usage (cf/hr)- calculated  Bypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfm) / {((diameter)²/4) x 3.14159} / 60 sec	1,387	ዜ (f ዘ <b>V</b> ))	
Fuel density (lb/ft³) Fuel usage (cf/hr)- calculated  Bypass Stack and Flow Conditions  Stack Height (ft)  Diameter (ft)  Velocity (ft/sec) = Volume flow (acfm) / {((diameter)²/4) x 3.14159] / 60 sec	66,935	1,319 20,714 63,653	1,2: 20,7 60,4:
Fuel density (lb/ft³) Fuel usage (cf/hr)- calculated  Bypass Stack and Flow Conditions  Stack Height (ft)  Diameter (ft)  Velocity (ft/sec) = Volume flow (acfm) / {((diameter)²/4) x 3.14159] / 60 sec	933	022	
Fuel usage (cf/hr)- calculated  Bypass Stack and Flow Conditions  Stack Height (ft)  Diameter (ft)  Velocity (ft/sec) = Volume flow (acfm) / {((diameter)^1/4) x 3.14159} / 60 sec		933	93
Stack Height (ft) Diameter (ft) Velocity (ft/sec) = Volume flow (acfm) / $\{((diameter)^2/4) \times 3.14159\} / 60 \text{ sec}$	0 0450 1,485,951	0.0450 1,413,074	0.045 1,342,12
Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfm) / {((diameter) <sup>1</sup> /4) x 3.14159} / 60 sec			
Diameter (ft)  Velocity (ft/sec) = Volume flow (acfm) / $\{((diameter)^2/4) \times 3.14159\} / 60 \text{ sec}$	150	150	1.5
· · · · · · · · · · · · · · · · · · ·	18	18	15 1
· · · · · · · · · · · · · · · · · · ·	/min		
Mass flow (lb/hr)	3,019,000	2,905,000	2,798,00
Stack Temperature (°F)	1,136	1,161	
Molecular weight	28.48	28.39	1,18
Volume flow (acfm)	2,058,166	2,017,660	28.2
Diameter (ft)	18	2,017,000	1,983,74
Velocity (ft/sec)- calculated	134.8	132.1	1 129.
HRSG Stack and Flow Conditions			
Stack Height (ft)	150	150	15
Diameter (ft)	18	18	13
Mass flow (lb/hr)	3,019,000	2,905,000	2,798,00
Stack Temperature (°F)	187	188	
Molecular weight	28.48		19
Volume flow (acfm)	28.48 834,099	28.39	28.2
Diameter (ft)	18	806,317 18	783,13.
Velocity (ft/sec)- calculated	54.6	52.8	1) 51.1

Note: Universal gas constant = 1,545 ft-lb(force)/°R; atmospheric pressure = 2,116.8 lb(force)/ft<sup>2</sup>; 14.7 lb/ft<sup>3</sup>

TABLE A-4 MAXIMUM EMISSIONS FOR CRITERIA POLLUTANTS FOR THE HOPKINS UNIT 2 REPOWERING PROJECT GE FRAME 7FA, DRY LOW NO\_x COMBUSTOR, NATURAL GAS, 75% LOAD

	25 °F	95 °F	
Parameter	25 ° F	59 °F	75 °F
Particulate from CT and SCR			
Total $PM_{10} = PM_{10}$ (front half) + $PM_{10}$ ((NH <sub>4</sub> ) <sub>2</sub> SO <sub>4</sub> ) from SCR only			
a. PM <sub>10</sub> (front half) (lb/hr)			
CI- provided	9.0	9.0	9.0
b. PM <sub>10</sub> ((NH <sub>4</sub> ) <sub>2</sub> SO <sub>4</sub> ) from SCR only = Sulfur trioxide from conversion	on of SO <sub>2</sub> converts to amme	onium sulfate (= PM <sub>1</sub>	n)
Particulate from conversion of $SO_2 = SO_2$ emissions (lb/hr) x con	iversion of SO <sub>2</sub> to SO <sub>2</sub> x lb	SO <sub>2</sub> /lb SO <sub>2</sub> x	<i>.</i>
	$H_4)_2SO_4 \times lb (NH_4)_2SO_4/lt$		
SO <sub>2</sub> emission rate (lb/hr)- calculated	8.5	8.1	7.7
Conversion (%) from SO <sub>2</sub> to SO <sub>3</sub>	9.8	9.8	9.8
MW SO <sub>2</sub> / SO <sub>2</sub> (80/64)	1.3	1.3	1.3
Conversion (%) from SO <sub>1</sub> to (NH <sub>4</sub> ) <sub>2</sub> (SO <sub>4</sub> )	100		
* * * **		100	100
MW (NH <sub>4</sub> ) <sub>2</sub> SO <sub>4</sub> /SO <sub>3</sub> (132/80)	1.7	1.7	1.7
SCR Particulate (lb/hr)- calculated	1.72	1.63	1.55
CT emission rate (lb/hr) [a]	9.0	9.0	9.0
HRSG stack emission rate (lb/hr) [a + b]	10.7	10.6	10.6
(lb/mmBtu, HHV)	0.0070	0.0073	0.0076
Sulfur Diexide			
SO <sub>2</sub> (lb/hr)= Natural gas (scf/hr) x sulfur content(gr/100 scf) x 1 lb/704	00 gr x (lb SO <sub>2</sub> /lb S) /100		
Fuel use (ct/hr)	1,485,951	1,413,074	1,342,125
Sulfur content (grains/ 100 cf)	2	2	2
lb SO <sub>2</sub> /lb S (64/32)	2	2	2
CT emission rate (lb/hr)	8.5	8.1	7.7
HRSG Stack emission rate (lb/hr)	8.5	8.1	7.7
Nitrogen Oxides			
NOx (lb/hr) = NOx (ppmvd@ 15% $O_2$ ) x {[20.9 x (1-Moisture (%)/100]	0] - Oxygen, dry(%)} x 211	6.8 lb/fl <sup>2</sup> x Volume f	low (acfm) x
46 (mole. wgt NOx) x 60 min/hr / [1545 x (CT temp.(*	'F) + 460) x (20.9-15) x 1.0	IVV.UVV TAGI. 10F DDM	)}
46 (mole, wgt NOx) x 60 min/hr / [1545 x (CT temp.(CT / DB, ppmvd @15% O <sub>2</sub>	°F) + 460) x (20.9-15) x 1,0	оо,ооо (аај. 16г ррт 9	-
			9.0
CT / DB, ppmvd @15% O <sub>2</sub>	9	9	9.0 9.74
CT / DB, ppmvd @15% O <sub>2</sub> Moisture (%)	9 7.66	9 8.45	9.0
CT / DB, ppmvd @15% O <sub>2</sub> Moisture (%) Oxygen (%)	9 7.66 12.64	9 8.45 12.57	9.0 9.74 12.43
CT / DB, ppmvd @15% O <sub>2</sub> Moisture (%) Oxygen (%) Turbine Flow (acfm)	9 7.66 12.64 2,058,166	9 8.45 12.57 2,017,660	9.0 9.74 12.43 1,983,749
CT / DB, ppmvd @15% O <sub>2</sub> Moisture (%) Oxygen (%) Turbine Flow (acfm) Turbine Exhaust Temperature (°F) CT Emission rate (lb/hr)	9 7.66 12.64 2,058,166 1,136 49.5	9 8.45 12.57 2,017,660 1,161 47.1	9.0 9.74 12.43 1,983,749 1,186
CT / DB, ppmvd @15% O <sub>2</sub> Moisture (%) Oxygen (%) Turbine Flow (acfm) Turbine Exhaust Temperature (°F)	9 7.66 12.64 2,058,166 1,136	9 8.45 12.57 2,017,660 1,161	9.0 9.74 12.43 1,983,749 1,186
CT / DB, ppmvd @15% O <sub>2</sub> Moisture (%) Oxygen (%) Turbine Flow (acfm) Turbine Exhaust Temperature (°F) CT Emission rate (lb/hr) HRSG Stack emission rate, ppmvd @ 15% O <sub>2</sub>	9 7.66 12.64 2,058,166 1,136 49.5	9 8.45 12.57 2,017,660 1,161 47.1	9.0 9.74 12.43 1,983,749 1,186 44.7
CT / DB, ppmvd @15% O <sub>2</sub> Moisture (%) Oxygen (%) Turbine Flow (acfm) Turbine Exhaust Temperature (°F)  CT Emission rate (lb/hr)  HRSG Stack emission rate, ppmvd @ 15% O <sub>2</sub> HRSG Stack emission rate (lb/hr)  Carbon Monoxide CO (lb/hr) = CO(ppm) x [1 - Moisture(%)/100] x 2116.8 lb/ft <sup>2</sup> x Volur	9 7.66 12.64 2,058,166 1,136 49.5 5 27.5	9 8.45 12.57 2,017,660 1,161 47.1 5 26.2	9.0 9.74 12.43 1,983,749 1,186 44.7
CT / DB, ppmvd @15% O <sub>2</sub> Moisture (%) Oxygen (%) Turbine Flow (acfm) Turbine Exhaust Temperature (°F)  CT Emission rate (lb/hr)  HRSG Stack emission rate, ppmvd @ 15% O <sub>2</sub> HRSG Stack emission rate (lb/hr)  Carbon Monoxide  CO (lb/hr) = CO(ppm) x [1 - Moisture(%)/100] x 2116.8 lb/ft <sup>2</sup> x Volum 28 (mole. wgt CO) x 60 min/hr / [1545 x (CT temp.(°F)	9 7.66 12.64 2,058,166 1,136 49.5 5 27.5  ne flow (acfin) x + 460°F) x 1,000,000 (adj.	9 8.45 12.57 2,017,660 1,161 47.1 5 26.2	9.0 9.74 12.43 1,983,749 1,186 44.7 5.0 24.9
CT / DB, ppmvd @15% O <sub>2</sub> Moisture (%) Oxygen (%) Turbine Flow (acfm) Turbine Exhaust Temperature (°F)  CT Emission rate (lb/hr)  HRSG Stack emission rate, ppmvd @ 15% O <sub>2</sub> HRSG Stack emission rate (lb/hr)  Carbon Monoxide  CO (lb/hr) = CO(ppm) x [1 - Moisture(%)/100] x 2116.8 lb/ft <sup>2</sup> x Volum  28 (mole. wgt CO) x 60 min/hr / [1545 x (CT temp.(°F))  Basis, ppmvd	9 7.66 12.64 2,058,166 1,136 49.5 5 27.5  ne flow (acfm) x + 460°F) x 1,000,000 (adj.	9 8.45 12.57 2,017,660 1,161 47.1 5 26.2 for ppm)]	9.0 9.74 12.43 1,983,749 1,186 44.7 5.0 24.9
CT / DB, ppmvd @15% O <sub>2</sub> Moisture (%) Oxygen (%) Turbine Flow (acfm) Turbine Exhaust Temperature (°F)  CT Emission rate (lb/hr)  HRSG Stack emission rate, ppmvd @ 15% O <sub>2</sub> HRSG Stack emission rate (lb/hr)  Carbon Monoxide  CO (lb/hr) = CO(ppm) x [1 - Moisture(%)/100] x 2116.8 lb/ft <sup>2</sup> x Volum  28 (mole. wgt CO) x 60 min/hr / [1545 x (CT temp.(°F)  Basis, ppmvd Moisture (%)	9 7.66 12.64 2,058,166 1,136 49.5 5 27.5  ne flow (acfin) x + 460°F) x 1,000,000 (adj. 12 7.66	9 8.45 12.57 2,017,660 1,161 47.1 5 26.2 for ppm)]	9.0 9.74 12.43 1,983,749 1,186 44.7 5.0 24.9
CT / DB, ppmvd @15% O <sub>2</sub> Moisture (%) Oxygen (%) Turbine Flow (acfm) Turbine Exhaust Temperature (°F)  CT Emission rate (lb/hr)  HRSG Stack emission rate, ppmvd @ 15% O <sub>2</sub> HRSG Stack emission rate (lb/hr)  Carbon Monoxide  CO (lb/hr) = CO(ppm) x [1 - Moisture(%)/100] x 2116.8 lb/ft <sup>2</sup> x Volum  28 (mole. wgt CO) x 60 min/hr / [1545 x (CT temp.(°F) Basis, ppmvd Moisture (%) Turbine Flow (acfm)	9 7.66 12.64 2,058,166 1,136 49.5 5 27.5  ne flow (acfin) x + 460°F) x 1,000,000 (adj. 12 7.66 2,058,166	9 8.45 12.57 2,017,660 1,161 47.1 5 26.2 for ppm)]	9.0 9.74 12.43 1,983,749 1,186 44.7 5.0 24.9
CT / DB, ppmvd @15% O <sub>2</sub> Moisture (%) Oxygen (%) Turbine Flow (acfm) Turbine Exhaust Temperature (°F)  CT Emission rate (lb/hr)  HRSG Stack emission rate, ppmvd @ 15% O <sub>2</sub> HRSG Stack emission rate (lb/hr)  Carbon Monoxide  CO (lb/hr) = CO(ppm) x [1 - Moisture(%)/100] x 2116.8 lb/ft <sup>2</sup> x Volum  28 (mole. wgt CO) x 60 min/hr / [1545 x (CT temp.(°F)  Basis, ppmvd Moisture (%) Turbine Flow (acfm) Turbine Exhaust Temperature (°F)	9 7.66 12.64 2,058,166 1,136 49.5 5 27.5 the flow (acfin) x + 460°F) x 1,000,000 (adj. 12 7.66 2,058,166 1,136	9 8.45 12.57 2,017,660 1,161 47.1 5 26.2 for ppm)] 12 8.45 2,017,660 1,161	9.0 9.74 12.43 1,983,749 1,186 44.7 5.0 24.9 12 9.74 1,983,749 1,186
CT / DB, ppmvd @15% O <sub>2</sub> Moisture (%) Oxygen (%) Turbine Flow (acfm) Turbine Exhaust Temperature (°F)  CT Emission rate (lb/hr)  HRSG Stack emission rate, ppmvd @ 15% O <sub>2</sub> HRSG Stack emission rate (lb/hr)  Carbon Monoxide CO (lb/hr) = CO(ppm) x [1 - Moisture(%)/100] x 2116.8 lb/ft <sup>2</sup> x Volum 28 (mole. wgt CO) x 60 min/hr / [1545 x (CT temp.(°F) Basis, ppmvd Moisture (%) Turbine Flow (acfm) Turbine Exhaust Temperature (°F)	9 7.66 12.64 2,058,166 1,136 49.5 5 27.5  ne flow (acfin) x + 460°F) x 1,000,000 (adj. 12 7.66 2,058,166	9 8.45 12.57 2,017,660 1,161 47.1 5 26.2 for ppm)]	9.0 9.74 12.43 1,983,749 1,186 44.7 5.0 24.9
CT / DB, ppmvd @15% O <sub>2</sub> Moisture (%) Oxygen (%) Turbine Flow (acfm) Turbine Exhaust Temperature (°F)  CT Emission rate (lb/hr)  HRSG Stack emission rate, ppmvd @ 15% O <sub>2</sub> HRSG Stack emission rate (lb/hr)  Carbon Monoxide  CO (lb/hr) = CO(ppm) x [1 - Moisture(%)/100] x 2116.8 lb/ft <sup>2</sup> x Volum  28 (mole. wgt CO) x 60 min/hr / [1545 x (CT temp.(°F) Basis, ppmvd Moisture (%) Turbine Flow (acfm)	9 7.66 12.64 2,058,166 1,136 49.5 5 27.5 the flow (acfin) x + 460°F) x 1,000,000 (adj. 12 7.66 2,058,166 1,136	9 8.45 12.57 2,017,660 1,161 47.1 5 26.2 for ppm)] 12 8.45 2,017,660 1,161	9.0 9.74 12.43 1,983,749 1,186 44.7 5.0 24.9 12 9.74 1,983,749 1,186

TABLE A-4 MAXIMUM EMISSIONS FOR CRITERIA POLLUTANTS FOR THE HOPKINS UNIT 2 REPOWERING PROJECT GE FRAME 7FA, DRY LOW NO $_{\rm X}$  COMBUSTOR, NATURAL GAS, 75% LOAD

	Turbine Inlet Temperature			
Parameter	25 °F	59 °F	95 °F	
Volatile Organic Compounds		· · · · · · · · · · · · · · · · · · ·		
VOCs (lb/hr) = VOC(ppmvd) x [1-Moisture(%)/100] x 2116.8	lb/ft² x Volume flow (acfm) x			
16 (mole, wgt as methane) x 60 min/hr / [1545 x (CT te		idi, for ppin)]		
Basis, ppmvw	3.50	3.5	3.50	
Moisture (%)	7.66	8.45	9.7	
Turbine Flow (acfm)	2,058,166	2,017,660	1,983,749	
Turbine Exhaust Temperature (°F)	1,136	1,161	1,180	
HRSG Exhaust Temperature (°F)	186.8	186.8	186.3	
CT Emission rate (lb/hr)	5.94	5.73	5.5	
HRSG Stack emission rate (lb/hr)	5.94	5.73	5.53	
Sulfuric Acid Mist				
Sulfuric Acid Mist (lb/hr)= SO <sub>2</sub> emission (lb/hr) x Conversion t	o H <sub>2</sub> SO <sub>4</sub> (% by weight)/100			
CT SO <sub>2</sub> emission rate (lb/hr) - provided	8.5	8.1	7.7	
CT Conversion to H <sub>2</sub> SO <sub>4</sub> (% by weight) - provided	10	10	10	
DB SO <sub>2</sub> emission rate (lb/hr) - provided	0	0	(	
DB Conversion to H <sub>2</sub> SO <sub>4</sub> (%) - provided	20	20	20	
CT Emission rate (lb/hr)	0.85	0.81	0.77	
HRSG Stack emission rate (lb/hr)	0.85	0.81	0.77	
<u>Lead</u>				
Lead (lb/hr) = NA				
Emission Rate Basis	NA	NA	NA	
CT Emission rate (lb/hr)	NA	NA	NA NA	
HRSG Stack emission rate (lb/hr)	NA	NA	NA NA	

 $TABLE~a-5\\ DESIGN INFORMATION~AND~STACK~PARAMETERS~FOR~THE~HOPKINS~UNIT~2~REPOWERING~PROJECT~GE~FRAME~7FA, DRY~LOW~NO_X~COMBUSTOR, NATURAL~GAS, 60%~LOAD$ 

	Turbine lulet Temperature				
Parameter	25 °F	59 °F	95 °F		
Combustion Turbine Performance		-			
Power output (MW)	112.7	104.6	96		
Heat rate (Btu/kWh, LHV)	10,880	11,160	11,46		
(Btu/kWh, HHV)	12,077	12,387	12,72		
Heat Input (MMBtw/hr, LHV)	1,226	1,167	1,10		
(MMBtw/hr, HHV)	1,361	1,296	1,22		
Relative Humidity (%)	87	78	:		
Fuel heating value (Btu/lb, LHV)	20,714	20,714	20,7		
(Btu/lb, HHV)	22,993	22,993	22,99		
(HHV/LHV)	1.110	1.110	LE		
CT Exhaust Flow					
Mass Flow (lb/hr)- with no margin	2,707,000	2,608,000	2,523,00		
- provided	2,707,000	2,608,000	2,523,00		
Temperature (°F)	1,167	1,190	1,20		
Moisture (% Vol.)	7.52	8.32	9.5		
Oxygen (% Vol.)	12.80	12.73	12.0		
Molecular Weight	28.49	28.40	28,2		
Fuel Usage					
Fuel usage (lb/hr) = Heat Input (MMBtu/hr) x 1,000,000 Btu/	MMBtu (Fuel Heat Content, Btu	/lb (LHV))			
Heat input (MMBtu/hr, LHV)	1,226	1,167	1,10		
Heat content (Btu/lb, LHV)	20,714	20,714	20,7		
Fuel usage (lb/hr)- calculated	59,197	56,353	53,22		
Heat content (Btu/cf, LHV)- assumed	933	933	93		
Fuel density (lb/ft <sup>3</sup> )	0.0450	0.0450	0.045		
Fuel usage (cf/hr)- calculated	1,314,153	1,251,028	1,181,58		
Bypass Stack and Flow Conditions					
Stack Height (ft)	150	150	15		
Diameter (ft)	18	81	ı		
Velocity (ft/sec) = Volume flow (acfin) / $\{((diameter)^2/4) \times 3.$	.14159] / 60 sec/min				
Mass flow (lb/hr)	2,707,000	2,608,000	2,523,00		
Stack Temperature (°F)	1,167	1,190	1.20		
Molecular weight	28.49	28.40	28.2		
Volume flow (acfm)	1,880,545	1,843,332	1,803,43		
Diameter (ft)	18	81	1		
Velocity (fl/sec)- calculated	123.2	120.7	118.		
BRSG Stack and Flow Conditions					
Stack Height (ft)	150	150	15		
Diameter (ft)	18	18	ı		
Mass flow (lb/hr)	2,707,000	2,608,900	2,523,00		
Stack Temperature (°F)	175	178	18		
Molecular weight	28.49	28.40	28.2		
Volume flow (acfm)	734,303	712,196	697,68		
Diameter (ft)	18	18	1		
Diameter (1t)					

Note: Universal gas constant = 1,545 ft-lb(force)/°R; atmospheric pressure = 2,116.8 lb(force)/ft<sup>2</sup>; 14.7 lb/ft<sup>3</sup>.

TABLE A-6 MAXIMUM EMISSIONS FOR CRITERIA POLLUTANTS FOR THE HOPKINS UNIT 2 REPOWERING PROJECT GE FRAME 7FA, DRY LOW NO\_x COMBUSTOR, NATURAL GAS, 60% LOAD

	Turbine Inlet Temperature				
Parameter	25 °F	59 °F	95 °F		
Particulate from CTand SCR					
Total $PM_{10} = PM_{10}$ (front half) + $PM_{10}$ ((NH <sub>4</sub> ) <sub>2</sub> SO <sub>4</sub> ) from SCR of	only				
a. PM <sub>10</sub> (front half) (lb/hr)	-				
CT- provided	9.0	9.0	9.0		
b. PM <sub>10</sub> ((NH <sub>4</sub> ) <sub>2</sub> SO <sub>4</sub> ) from SCR only = Sulfur trioxide from cor			10)		
Particulate from conversion of $SO_2 = SO_2$ emissions (lb/hr)					
	to $(NH_4)_2SO_4 \times lb (NH_4)_2SO_4$	lb SO <sub>3</sub>			
SO <sub>2</sub> emission rate (lb/hr)- calculated	7.5	7.1	6.8		
Conversion (%) from SO <sub>2</sub> to SO <sub>3</sub>	9.8	9.8	9.8		
MW SO <sub>3</sub> / SO <sub>2</sub> (80/64)	1.3	- 1.3	1.3		
Conversion (%) from SO <sub>3</sub> to (NH <sub>4</sub> ) <sub>2</sub> (SO <sub>4</sub> )	100	100	100		
MW (NH <sub>4</sub> ) <sub>2</sub> SO <sub>4</sub> / SO <sub>3</sub> (132/80)	1.7	1.7	1.3		
SCR Particulate (lb/hr)- calculated	1.52	1.44	- 1.36		
CT emission rate (lb/hr) [a]	9.0	9.0	9.0		
HRSG stack emission rate (lb/hr) [a + b]	10.5	10.4	10.4		
(lb/mmBtu, HHV)	0.0077	0.0081	0.0085		
Sulfur Dioxide					
SO <sub>2</sub> (lb/hr)= Natural gas (scf/hr) x sulfur content(gr/100 scf) x 1	lb/7000 gr x (lb SO <sub>2</sub> /lb S)/100	)			
Fuel use (cf/hr)	1,314,153	1,251,028	1,181,580		
Sulfur content (grains/ 100 cf)	2	2	2,101,500		
lb SO <sub>2</sub> /lb S (64/32)	2	2	2		
CT emission rate (lb/hr)	7.5	7.1	6.8		
HRSG Stack emission rate (lb/hr)	7.5	7.1	6.8		
Nitrogen Oxides					
NOx (lb/hr) = NOx (ppmvd@ 15% O <sub>2</sub> ) x {[20.9 x (1-Moisture (5 46 (mole. wgt NOx) x 60 min/hr / [1545 x (CT te					
CT / DB, ppmvd @15% O <sub>2</sub>	9	9	9		
Moisture (%)	7.52	8.32	9.54		
Oxygen (%)	12.80	12.73	12.66		
Turbine Flow (acfm)	1,880,545	1,843,332	1,803,432		
Turbine Exhaust Temperature (°F)	1,167	1,190	1,200		
CT Emission rate (lb/hr)	43.5	41,4	39.1		
HRSG Stack emission rate, ppmvd @ 15% O <sub>2</sub>	5	5	5		
HRSG Stack emission rate (lb/hr)	24.2	23.0	21.7		

TABLE~A-6 MAXIMUM EMISSIONS FOR CRITERIA POLLUTANTS FOR THE HOPKINS UNIT 2 REPOWERING PROJECT GE FRAME 7FA, DRY LOW NO\_X COMBUSTOR, NATURAL GAS, 60% LOAD

	Turbine Inlet Temperature				
Parameter	25 °F	59 °F	95 °F		
Carbon Monoxide					
$CO (fb/hr) = CO(ppm) \times [1 - Moisture(%)/100] \times 2116.8 lb/ft^2 x$	Volume flow (acfm) x				
28 (mole. wgt CO) x 60 min/hr / [1545 x (CT tem		di. for nom)]			
Basis, ppmvd	12	12	12		
Moisture (%)	7.52	8.32	9.54		
Turbine Flow (acfm)	1,880,545	1,843,332	1,803,432		
Turbine Exhaust Temperature (°F)	1,167	1,190	1,200		
HRSG Exhaust Temperature (°F)	175	178	182		
CT Emission rate (lb/hr)	29.5	28.3	27.1		
HRSG Stack emission rate (lb/hr)	29.5	28.3	27.1		
Volatile Organic Compounds					
VOCs (lb/hr) = VOC(ppmvd) x [1-Moisture(%)/100] x 2116.8 lt	/ft <sup>2</sup> x Volume flow (acfm) x				
16 (mole, wgt as methane) x 60 min/hr / [1545 x (CT terr	p.(°F) + 460°F) x 1,000,000 (a	di. for ppm)]			
Basis, ppmvw	3.50	3.5	3.50		
Moisture (%)	7.52	8.32	9.54		
Turbine Flow (acfm)	1,880,545	1,843,332	1,803,432		
Turbine Exhaust Temperature (°F)	1,167	1,190	1,200		
HRSG Exhaust Temperature (°F)	175	175	175		
CT Emission rate (lb/hr)	5.32	5.14	5.00		
HRSG Stack emission rate (lb/hr)	5.32	5.14	5.00		
Sulfuric Acid Mist					
Sulfuric Acid Mist (lb/hr)= SO <sub>2</sub> emission (lb/hr) x Conversion to	H <sub>2</sub> SO <sub>4</sub> (% by weight)/100				
CT SO <sub>2</sub> emission rate (lb/hr) - provided	7.5	7.1	6.8		
CT Conversion to H <sub>2</sub> SO <sub>4</sub> (% by weight) - provided	10	10	10		
DB SO <sub>2</sub> emission rate (lb/hr) - provided	0	0	0		
DB Conversion to H <sub>2</sub> SO <sub>4</sub> (%) - provided	20	20	20		
CT Emission rate (lb/hr)	0.75	0.71	0.68		
HRSG Stack emission rate (lb/hr)	0.75	0.71	0.68		
<u>Lead</u>					
Lead (lb/hr) = NA					
Emission Rate Basis	NA	NA	NA		
CT Emission rate (lb/hr)	NA	NA	NA		
HRSG Stack emission rate (lb/hr)	NA	NA	NA		

 $TABLE\ a-7 \\ DESIGN INFORMATION AND STACK PARAMETERS FOR THE HOPKINS UNIT 2 REPOWERING PROJECT \\ GE FRAME 7FA, DRY LOW NO_X COMBUSTOR, DISTILLATE OIL, BASE LOAD, WITH NATURAL GAS DUCT FIRING$ 

		Turbin	CT Only e Inlet Temperature			ct Burner (Natural ( e Inlet Temperature	
Parameter	4	215 P ( 70 P)	1 (59 7)	27.7	15 °V, w/DB	59 °T w/DB	95 °F w/DB
Combustion Turbine Performance							
Power output (MW)	р	198.9	187.9	172.4	198.9	187.9	172.4
Heat rate (Btu/kWh, LHV)	P	9,860	9,935	10,090	9,860	9,935	
(Btu/kWh, HHV)	ν	10,452	10,531	10,695			10,094
Heat Imput (MMBts/lw, LHV)	_	1,961.2	1,866.8		10,452	10,531	10,69:
(MMBtu/hr, HHV)	P	2,079	1,979	1,739.5	1,961.2	1,866.8	1,739.3
Evaporative Cooler		2,079 Off		1,844	2,079	1,979	1,84
Relative Humidity (%)	_	87	On 78	On	Off	On	Or
	р	0/	/8	50	37 Q	78.0	50.0
Fuel oil		10.200					
Fuel heating value (Btu/lb, LHV)	p	18,300	18,300	18,300	18,300	18,300	18,300
(Bru/Ib, HHV)		19,398	19,398	19,398	19,398	19,398	. 19,391
(HHV/LHV)		1.060	1.060	1.060	1.060	1.060	1 060
Fuel heating value (Btu/Ib, LHV)		NA	NA	NA	18,300	18,300	18,300
(Btu/bb, HHV)		NA.	NA	NA	19,398	19,398	19,398
(HHV/LHV)		' NA	NA	NA.	1.11	1.11	E. E.
Duct Burner (DB)							
Heat input (MMBtu/hr, HHV)		0	0	0	764.6	711.6	662.6
(MMBtu/lsr, LHV)		0	ō	ō	688.8	641.1	596.9
					*****	*****	370
T Exhaust Flow							
Mass Flow (lb/hr)- with no margin		3,995,000	3,764,000	3,512,000	4,025,724	3,792,596	3,538,625
- provided	P	3,995,000	3,764,000	3,512,000	4,025,724	2,772,374	2,30,02.
Temperature (°F)		1,059	1,096		1.040	1.004	
	p			1,130	1,059	1,096	1,130
Moisture (% Vol.)	P	10.95	11.82	12.96	13.50	14.32	15.4
Oxygen (% Vol.)	₽	11 20	10.97	10.77	8.35	8.16	7.9
Molecular Weight	c	28.36	28.26	28.13	28.19	28.10	27.9
	р	28.35	28.26	28.13			
uel Usage							
Fuel oil							
Fuel usage CT (lb/hr) = Heat Input (MMBtu/hr) x	1,000,000 Btu/MMBt	ı (Fuel Heat Content, F	Btu/To(LHV))				
Heat input (MMBtu/hr, LHV)		1,961	1,867	1,740	NA	NA.	NA
Heat content (Btu/lb, LHV)		18,300	18,300	18,300	NA	NA	NA
Fuel usage (lb/hr)- calculated	c	107,169	102,011	95,055	NA.	NA.	NA
Vatural gas							
Fuel usage DB (fb/hr) = Heat Input (MMBtu/hr) x	1,000,000 Bts/MMBi	u (Fuel Heat Content, I	Bru/lb (LHV))				
Heat input (MMBtu/hr, LHV)		NA	NA.	NA	688.8	641.1	- 596 5
Heat content (Btu/lb, LHV)		NA	NA	NA	20,714	20,714	20,714
Fuel usage (lb/hr)- calculated		NA	NA.	NA.	33,253	30,950	
		,,,,	1473	""	33,233		
Heat content (Btu/cf, LHV)- assumed						30,330	28,816
		1.14	Na	314	011		28,816
		NA	NA	NA	933	933	
Fuel density (lb/ft <sup>3</sup> )		NA	NA	NA NA	933 0 0451		93
Fuel density (lb/ft <sup>3</sup> )						933	931 0.0451
Fuel density (lb/ft <sup>3</sup> )		NA	NA	NA	0 0451	933 0.0451	931 0.0451
Fuel density (fb/ft <sup>3</sup> ) Fuel usage (cf/hr)- calculated		NA	NA	NA	0 0451	933 0.0451	931 0.0451
Fuel density (fb/ft <sup>1</sup> ) Fuel usage (c0/tr)- calculated <u>Appass Stack and Flow Conditions</u>		NA	NA	NA NA	0 0451 737,941	933 0.0451 686,838	933 0.0451 639,483
Fuel density (lb/ft <sup>3</sup> ) Fuel usage (cb/tr) - calculated  bypass Stack and Flow Conditions Stack Height (ft)		NA NA	NA NA	NA	0 0451 737,941 150	933 0.0451 686,838	933 0.0451 639,485
Fuel density (lb/ft <sup>3</sup> ) Fuel usage (cb/tr) - calculated  bypass Stack and Flow Conditions Stack Height (ft)		NA NA 150	NA NA	NA NA 150	0 0451 737,941	933 0.0451 686,838	933 0.0451 639,485
Fuel density (lb/ft <sup>3</sup> ) Fuel usage (cb/tr)- calculated  bypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)	reri <sup>y</sup> /4) x 3.141591/ <i>6</i> 4	NA NA 150 18	NA NA	NA NA 150	0 0451 737,941 150	933 0.0451 686,838	931 0.0451 639,485
Fuel density (fb/ft <sup>1</sup> ) Fuel usage (cf/fr)- calculated bypass Stack and Flow Conditions Stack Height (ft) Diameter (ft) Velocity (fl/sec) = Volume flow (acfin) / [[(diamet	er)²/4) x 3.14159]/6	NA NA 150 18	NA NA 150 18	NA NA 150 18	0 0451 737,941 150 18	933 0.0451 686,838 150 18	933 0.0451 639,485 150
Fuel density (fb/ft <sup>1</sup> ) Fuel usage (cf/fr)- calculated  bypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (fb/sec) = Volume flow (acfin) / [((diameted Mass flow (fb/fr))]	ier)* /4) x 3,14159] / 6/	NA NA 150 18 0 sec/min 3,995,000	NA NA 150 18 3,764,000	NA NA 150 18 3,512,000	0 0451 737,941 150 18	933 0.0451 686.838 150 18	931 0.0451 639,485 150 18
Fuel density (B/ft <sup>3</sup> ) Fuel usage (cf/tr)- calculated bypass Stack and Flow Conditions Stack Height (ft) Diameter (ft) Velocity (B/sec) = Volume flow (acfin) / [((diamet Mass flow (B/ftr) Stack Temperature ( <sup>3</sup> F)	eer}' /4) x 3.14 [59] / 6/	NA NA 150 18 9 sec/min 3,995,000 1,059	NA NA 130 18 3,764,000 1,096	NA NA 150 18 3,512,000 1,130	0 0451 737,941 L50 18 NA NA	933 0.0451 686.838 150 1B NA	93: 0,045: 639,48: 150: 111: NA: NA:
Fuel density (B/ft <sup>3</sup> ) Fuel usage (cf/tr)- calculated  httpass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfin) / [((diamet Mass flow (b/fr)  Stack Temperature (*F)  Molecular weight	ier) <sup>, 7</sup> (4) x 3.14   59] / 6 <sup>(</sup>	NA NA 150 18 9 sec/min 3,995,000 1,059 28.36	NA NA 150 18 3,764,000 1,096 28,26	NA NA 150 18 3,512,000 1,130 28.13	0 0451 737,941 150 18 NA NA	933 0.0451 686.838 150 18 NA NA	93. 0.0451 639,481 150 111 NA NA
Fuel density (lb/ft <sup>3</sup> ) Fuel usage (cf/tr)- calculated  Expass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfin) / [((diamet Mass flow (fb/tr) Stack Temperature (*F) Molecular weight Volume flow (acfin)	юг) <sup>, 7</sup> 4) х 3.14159] / 6 <sup>,</sup>	NA NA 150 18 0 sec/min 3,995,000 1,059 28,36 2,603,400	NA NA 150 18 3,764,000 1,096 28,26 2,520,733	NA NA 150 18 3,512,000 1,130 28,13 2,414,634	0 0451 737,941 L50 18 NA NA	933 0.0451 686.838 150 1B NA	93: 0.0451 639,485 150 18 NA NA
Fuel density (lb/ft <sup>3</sup> ) Fuel usage (cb/hr)- calculated  Expass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfin) / [((diamet Mass flow (lb/hr) Stack Temperature (*F) Molecular weight Volume flow (acfin) Diameter (ft)	eer}' /4) x 3.14 [59] / 6/	NA NA 150 18 9 sec/min 3,995,000 1,059 28.36 2,603,400 18	NA NA 150 18 3,764,000 1,996 28.26 2,520,733 18	NA NA 150 18 3,512,000 1,130 28,13 2,414,634	0 0451 737,941 150 18 NA NA	933 0.0451 686.838 150 18 NA NA	933 0:0451 639,485 150 18 NA NA NA
Fuel density (lb/ft <sup>3</sup> ) Fuel usage (cb/tr)- calculated  bypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfin) / [((diamet Mass flow (fb/tr) Stack Temperature (*F) Molecular weight Volume flow (acfin)	ler}* /4) x 3.14159] / 6/	NA NA 150 18 0 sec/min 3,995,000 1,059 28,36 2,603,400	NA NA 150 18 3,764,000 1,096 28,26 2,520,733	NA NA 150 18 3,512,000 1,130 28,13 2,414,634	0 0451 737,941 150 18 NA NA NA	933 0.0451 686.838 150 18 NA NA	933 0.0451 639,485 150 18 NA NA NA
Fuel density (fb/ft <sup>3</sup> ) Fuel usage (cf/fr)- calculated hypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfin) / [((diamet Mass flow (fb/fr) Stack Temperature (*F) Molecular weight Volume flow (acfin) Diameter (ft) Velocity (ft/sec)- calculated	ier)* /4) x 3.J4159] / 6/	NA NA 150 18 9 sec/min 3,995,000 1,059 28.36 2,603,400 18	NA NA 150 18 3,764,000 1,996 28.26 2,520,733 18	NA NA 150 18 3,512,000 1,130 28,13 2,414,634	0 0451 737,941 150 18 NA NA NA NA	933 0.0451 686.838 150 18 NA NA NA	933 0.0451 639,485 150 18 NA NA NA
Fuel density (lb/ft <sup>3</sup> ) Fuel usage (cb/tr)- calculated  hypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfin) / [((diamet Mass flow (fb/tr) Mass flow (fb/tr) Stack Temperature (*F) Molecular weight Volume flow (acfin) Diameter (ft) Velocity (ft/sec)- calculated	eer}' /4) x 3.14 [59] / 6/	NA NA 150 18 9 sec/min 3,995,000 1,059 28.36 2,603,400 18	NA NA 150 18 3,764,000 1,996 28.26 2,520,733 18	NA NA 150 18 3,512,000 1,130 28,13 2,414,634	0 0451 737,941 150 18 NA NA NA NA	933 0.0451 686.838 150 18 NA NA NA	933 0.0451 639,485 150 18 NA NA NA
Fuel density (lb/ft <sup>3</sup> ) Fuel usage (cb/tr)- calculated  dypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfin) / [((diameter Mass flow (fb/fr) Stack Temperature (*F) Molecular weight Volume flow (acfin) Diameter (ft) Velocity (ft/sec)- calculated  IRSG Stack and Flow Conditions	er)* /4) x 3.14 59] / 6/	NA NA 150 18 9 sec/min 3,995,000 1,059 28.36 2,603,400 18	NA NA 150 18 3,764,000 1,996 28.26 2,520,733 18	NA NA 150 18 3,512,000 1,130 28.13 2,414,634 18 158.1	0 0451 737,941 150 18 NA NA NA NA NA	933 0.0451 686.838 150 1B NA NA NA NA	933 0.0451 639,485 150 18 NA NA NA NA
Fuel density (lb/ft <sup>3</sup> ) Fuel usage (cb/tr) - calculated  bypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfin) / [((diameter Mass flow (lb/tr) Stack Temperature (*F) Molecular weight Volume flow (acfin) Diameter (ft) Velocity (ft/sec) - calculated  IRSG Stack and Flow Conditions Stack Height (ft)	ren') <sup>,</sup> /4) x 3.14159] / 6/	NA NA 150 18 0 sec/min 3,995,000 1,059 28.36 2,603,400 18 170.5	NA NA 150 18 3,764,000 1,996 28,26 2,520,733 18 165,1	NA NA 150 18 3,512,000 1,130 28,13 2,414,634	0 0451 737,941 L50 18 NA NA NA NA NA NA	933 0.0451 686.838 150 1B NA NA NA NA	933 0.0451 639,485 150 18 NA NA NA NA
Fuel density (B/R <sup>3</sup> ) Fuel usage (cPhr)- calculated bypass Stack and Flow Conditions Stack Height (R) Diameter (R) Velocity (R/sec) = Volume flow (acfin) / [((diamet Mass flow (b/hr) Stack Temperature (*F) Molecular weighs Volume flow (acfin) Diameter (R) Velocity (R/sec)- calculated IRSG Stack and Flow Conditions Stack Height (R)	er)* /4) x 3.14159] / 6/	NA NA 150 18 9 sec/min 3,995,000 1,059 28.36 2,603,400 18 170.5	NA NA 150 18 3,764,000 1,096 28,26 2,520,733 18 165,1	NA NA L50 18 3,512,000 1,130 28.13 2,414,634 18 158.1	0 0451 737,941 150 18 NA NA NA NA NA	933 0.0451 686.838 150 1B NA NA NA NA	933 0.0451 639,485 150 18 NA NA NA NA
Fuel density (B/R <sup>3</sup> ) Fuel usage (cPhr)- calculated bypass Stack and Flow Conditions Stack Height (R) Diameter (R) Velocity (R/sec) = Volume flow (acfin) / [((diamet Mass flow (b/hr) Stack Temperature (*F) Molecular weighs Volume flow (acfin) Diameter (R) Velocity (R/sec)- calculated IRSG Stack and Flow Conditions Stack Height (R)	ier) <sup>y</sup> /4) х 3.14159] / 64	NA NA 150 18 9 sec/min 3,995,000 1,059 28.36 2,603,400 18 170.5	NA NA 150 18 3,764,000 1,096 28,26 2,520,733 18 165,1	3,512,000 1,130 2,414,634 18 158.1	0 0451 737,941 150 18 NA NA NA NA NA NA NA	933 0.0451 686.838 150 1B NA NA NA NA NA	93: 0.045  639,48: 150 18 NA NA NA NA NA
Fuel density (fb/ft <sup>3</sup> ) Fuel usage (cf/fr)- calculated bypass Stack and Flow Conditions Stack Height (ft) Diameter (ft) Velocity (fb/sec) = Volume flow (acfin) / [((diamet Mass flow (fb/fr) Stack Temperature (*F) Molecular weight Volume flow (acfin) Diameter (ft) Velocity (fb/sec)- calculated IRSG Stack and Flow Conditions Stack Height (ft) Diameter (ft) Mass flow (fb/fr)	ren'?' /4) x 3.14159] / 6/	NA NA 150 18 9 sec/min 3,995,000 1,059 28.36 2,603,400 18 170.5	NA NA 150 18 3,764,000 1.996 28.26 2,520,733 165.1 150 18	3,512,000 18 3,512,000 1,130 28.13 2,414,634 158.1	0 0451 737,941 150 18 NA NA NA NA NA NA 150 18	933 0.0451 686.838 150 18 NA NA NA NA NA 150 18	931 0.0451 639,485 150 18 NA NA NA NA NA 150 18
Fuel density (B/R <sup>3</sup> ) Fuel usage (cPhr)- calculated bypass Stack and Flow Conditions Stack Height (R) Diameter (R)  Velocity (R/sec) = Volume flow (acfin) / [((diamet Mass flow (b/hr) Stack Temperature (*F) Molecular weight Volume flow (acfin) Diameter (R) Usec)- calculated  IRSG Stack and Flow Conditions Stack Height (R) Diameter (R)  Mass flow (B/hr) Stack Temperature (*F)	ice; <sup>у</sup> /4) х 3.14 (59] / 6/	NA NA  150 18  9 sec/min 3,995,000 1,059 28.36 2,603,400 18 170.5 150 18 3,995,000 248.0	3,764,000 1,096 28,26 2,520,733 18 165.1 150 18	3,512,000 1,130 28.13 2,414,634 18 158.1 150 18 3,512,000 247 0	0 0451 737,941  150 18  NA NA NA NA NA NA 150 18  4,025,724 206	933 0.0451 686.838 150 18 NA NA NA NA NA 150 18	931 0.0451 639,485 150 18 NA NA NA NA NA 150 18 3,538,625 201
Fuel density (lb/ft <sup>3</sup> ) Fuel usage (cb/tr)- calculated  hypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfin) / [((diamet Mass flow (ft/tr) Stack Temperature (*F) Molecular weight Volume flow (acfin) Diameter (ft) Velocity (ft/sec)- calculated  HRSG Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Mass flow (lb/tr)  Stack Temperature (*F) Molecular weight	ier)* /4) x 3.14159] / 64	NA NA  150 18  0 sec/min 3,995,000 1,059 28.36 2,603,400 18 170.5  150 18 3,995,000 248.0 248.0 28.36	3,764,000 1,096 28,26 2,520,733 18 165,1 150 18	3,512,000 1,130 28.13 2,414,634 18 158.1 150 18 3,512,000 247 0 28.13	0 0451 737,941  150 18  NA NA NA NA NA NA 150 18  4,025,724 206 28 19	933 0.0451 686.838 150 18 NA NA NA NA NA 150 18 3.792,596 204 28.10	931 0.0451 639,485 150 18 NA NA NA NA NA 150 18 3,538,625 201 27,97
Fuel density (lb/ft <sup>3</sup> ) Fuel usage (cb/tr)- calculated  dypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfin) / [((diameter Mass flow (lb/ftr) Stack Temperature (*fr) Molecular weight Volume flow (acfin) Diameter (ft) Velocity (ft/sec)- calculated  IRSG Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Mass flow (lb/ftr) Stack Temperature (*fr) Molecular weight Volume flow (acfin)	rer)* /4) x 3.14159] / 6/	NA NA 150 18 9 sec/min 3,995,000 1,059 28,36 2,603,400 18 170.5 150 18 3,995,000 248,0 28,36 1,213,435	NA NA 150 18 3,764,000 1.096 28.26 2,520,733 18 165.1 150 18 3,764,000 248.0 28.26 1,146,966	3,512,000 18 3,512,000 1,130 28.13 2,414,634 158.1 150 18 3,512,000 247.0 28.13 1,073,677	0 0451 737,941  150 18  NA NA NA NA NA NA 150 18  4,025,724 206	933 0.0451 686.838 150 18 NA NA NA NA NA 150 18	931 0.0451 639,485 150 18 NA NA NA NA NA 150 18 3,538,625 201 27,97
Fuel density (lb/ft <sup>1</sup> ) Fuel usage (cf/hr)- calculated  Bypass Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Velocity (ft/sec) = Volume flow (acfin) / [((diameter Mass flow (ft/hr) Stack Temperature (*F) Molecular weight Volume flow (acfin) Diameter (ft) Velocity (ft/sec)- calculated  dtRSG Stack and Flow Conditions Stack Height (ft) Diameter (ft)  Mass flow (ft/hr) Stack Temperature (*F) Molecular weight	ler)* /4) x 3.14159] / 6/	NA NA  150 18  0 sec/min 3,995,000 1,059 28.36 2,603,400 18 170.5  150 18 3,995,000 248.0 248.0 28.36	3,764,000 1,096 28,26 2,520,733 18 165,1 150 18	3,512,000 1,130 28.13 2,414,634 18 158.1 150 18 3,512,000 247 0 28.13	0 0451 737,941  150 18  NA NA NA NA NA NA 150 18  4,025,724 206 28 19	933 0.0451 686.838 150 18 NA NA NA NA NA 150 18 3.792,596 204 28.10	933 0.0451 639,485 150 18 NA NA NA NA

Note: Universal gas constant = 1,545 ft-lb(force)/°R; atmospheric pressure = 2,116.8 lb(force)/ft<sup>2</sup>; 14.7 lb/ft<sup>3</sup>.

TABLE~a.\$ MAXIMUM EMISSIONS FOR CRITERIA POLLUTANTS HOPKINS UNIT 2 REPOWERING PROJECT GE FRAME 7FA, DRY LOW NO\_X COMBUSTOR, DISTILLATE OIL, BASE LOAD, WITH NATURAL GAS DUCT FIRING

	2 2 2 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3	CT Only Inlet Temperate	生理为是		et Burner (Natu Lafet Temperat	
arameter	2617 25 <b>27</b> 20 25 2	59 °P	95 °F	25 °F w/DB		95 °F w/DB
	# 1 (	**************************************	racte (bilding region)	10 1000 0 223,000	Parameter State of the Nation	ALIENT AND
articulate from CT and SCR	con .					
Total $PM_{10} = PM_{10}$ (front half) + $PM_{10}$ ((NH <sub>4</sub> ) <sub>2</sub> SO <sub>4</sub> ) from	SCR only					
a. PM <sub>10</sub> (front half) (lb/hr)	12.0	17.6	170			
CT- provided  DR (It/In) and add to the	17.0 0.0	17.0 0.0	17.0 0.0	17,0 9,2	17.0 8.5	17.0
DB (lb/hr) - calculated Total CT/DB emission rate (lb/hr)	17.0	17.0	17.0	26.2	25.5	8.6 25.6
b. PM <sub>10</sub> ((NH <sub>4</sub> ) <sub>2</sub> SO <sub>4</sub> ) from SCR only = Sulfur trioxide for	om conversion of SO <sub>3</sub> conver	ts to ammonium :	sulfate (= PM	)		
Particulate from conversion of SO <sub>2</sub> = SO <sub>2</sub> emissions	(lb/hr) x conversion of SO <sub>2</sub> to	sO3 x 16 SO4/16		,		
	of SO <sub>3</sub> to (NH <sub>4</sub> ) <sub>2</sub> SO <sub>4</sub> x lb (NI	472 - 3	05.1		1060	
SO <sub>2</sub> emission rate (lb/hr)- calculated	107.2	102.0	95.1	111.4	105.9	98.
Conversion (%) from SO <sub>2</sub> to SO <sub>3</sub>	9.8	9.8	9.8	9.8	9.8	9.:
MW SO <sub>3</sub> / SO <sub>2</sub> (80/64)	1.3	1.3	1.3	1.3	1.3	I.
Conversion (%) from SO <sub>3</sub> to (NH <sub>4</sub> ) <sub>2</sub> (SO <sub>4</sub> )	100	100	100	100	100	100
MW (NH <sub>4</sub> ) <sub>2</sub> SO <sub>4</sub> / SO <sub>3</sub> (132/80)	1.7	1.7	1.7	1.7	1.7	1.7
SCR Particulate (lb/ltr)- calculated	21.66	20.62	19.21	22.51	21.41	19.9
CT emission rate (lb/hr) [a + b] assumes SCR	38.7	37.6	36.2	38.7	37.6	36.
HRSG stack emission rate (lb/hr) [a + b]	38.7	37.6	36.2	48.7	47.0	44.9
(lb/mmBtu, HHV)	0.0186	0.0190	0.0196	0.0171	0.0175	0.017
ulfur Dioxide						
CT/SO <sub>2</sub> (lb/hr)= Fuel oil (lb/hr) x sulfur content(% weigh						
Fuel oil Sulfur Content	0.0500%	0.0500%	0.0500%	0.0500%	0.0500%	0.0500%
Fuel oil use (lb/hr)	107,169	102.011	95,055	NA	102,011	95,05
lb SO2 / lb S (64/32)	2	2	2	2	2	:
DB/SO <sub>2</sub> (lb/hr)= Natural gas (scf/hr) x sulfur content(gr/f		•				
Fuel use (cf/hr)	NA NA	NA	NA	737,941	686,838	639,48
Sulfur content (grains/ 100 cf)	NA	NA	NA	2	2	2
CT emission rate (lb/hr)	107.2	102.0	95.1	107.2	102.0	95.
HRSG stack emission rate (lb/hr)	107.2	102 0	95.1	111.4	105.9	98.
(lb/MW)	0.54	0.54	0.55			
litrogen Oxides			-2			
NOx (lb/hr) = NOx (ppmvd@ $15\% O_2$ ) x {[20.9 x {1-Moi} 46 (mole, wgt NOx) x 60 min/hr / [1545 v						
CT/DB, ppmvd @15% O <sub>1</sub>	42	42	42	38.6	38.7	38.7
Moisture (%)	10.95	11.82	12.96	13.50	14.32	15.43
Oxygen (%)	11.20	10.97	10.77	8.35	8.16	7.98
- VB-11 117/			2,414,634	2,639,095	2,554,769	
Turbine Flow (acfm)	2,603,400	2,520,733				2,446,776
	2,603,400 1,059	1,096	1,130	1,059	1,096	
Turbine Exhaust Temperature (°F)					1,096 396.5	1,130
Turbine Exhaust Temperature (°F)	1,059	1,096	1,130	1,059		1,130 369.0
Turbine Exhaust Temperature (°F)  CT emission rate (lb/hr)  (lb/MW)	1,059 341.9	1,096 325.3	1,130 303.4	1,059 418.4	396.5	1,130 369.6 NA
Turbine Exhaust Temperature (°F) CT emission rate (lb/hr) (lb/MW) HRSG stack emission rate, ppmvd @ 15% O <sub>2</sub>	1,059 341.9 1.7	1,096 325.3 1.7	1,130 303,4 1.8	1,059 418.4 NA 10	396.5 NA 10	1,130 369.6 NA 10
Turbine Exhaust Temperature (°F)  CT emission rate (ib/hr)  (lb/MW)  HRSG stack emission rate, ppmvd @ 15% O <sub>2</sub>	1,059 341.9 1.7 10	1,096 325.3 1.7 10	1,130 303.4 1.8 10	1,059 418.4 NA	396.5 NA	1,130 369.6 NA 10
Turbine Exhaust Temperature (°F)  CT emission rate (lb/hr) (lb/MW)  HRSG stack emission rate, ppmvd @ 15% O <sub>2</sub> HRSG stack emission rate (lb/hr) (lb/MW)	1,059 341.9 1.7 10 81.4 0.41	1,096 325.3 1.7 10 77.5 0.41	1,130 303.4 1.8 10 72.2	1,059 418.4 NA 10	396.5 NA 10	1,130 369.6 NA 10
Turbine Exhaust Temperature (°F)  CT emission rate (lb/hr) (lb/MW)  HRSG stack emission rate, ppmvd @ 15% O <sub>2</sub> HRSG stack emission rate (lb/hr) (lb/MW)  Carbon Monoxide  CO (lb/hr) = CO(ppm) x [1 - Moisture(%)/100] x 2116.8	1,059 341.9 1.7 10 81.4 0.41	1,096 325.3 1.7 10 77.5 0.41	1,130 303,4 1.8 10 72,2 0,42	1,059 418.4 NA 10	396.5 NA 10	1,130 369.6 NA 10
Turbine Exhaust Temperature (°F)  CT emission rate (ib/hr)	1,059  341.9  1.7  10  81.4  0.41  1b/R <sup>2</sup> x Volume flow (acfin) x  T temp.(°F) + 460°F) x 1,000	1,096 325.3 1.7 10 77.5 0.41	1,130 303,4 1.8 10 72,2 0,42	1,059 418.4 NA 10	396.5 NA 10	1,130 369.6 NA 10 95.6
HRSG stack emission rate, ppmvd @ 15% O <sub>2</sub> HRSG stack emission rate (lb/hr) (lb/MW)  Carbon Monoxide CO (lb/hr) = CO(ppm) x [1 - Moisture(%)/100] x 2116.8	1,059  341.9  1.7  10  81.4  0.41  (b/R <sup>2</sup> x Volume flow (acfm) x  T temp.(°F) + 460°F) x 1,000	1,096 325.3 1.7 10 77.5 0.41	1,130 303.4 1.8 10 72.2 0.42	1,059 418.4 NA 10 108.4	396.5 NA 10 102.6	1,130 369.6 NA 10 95.6
Turbine Exhaust Temperature (°F)  CT emission rate (lb/hr) (lb/MW)  HRSG stack emission rate, ppmvd @ 15% O <sub>2</sub> HRSG stack emission rate (lb/hr) (lb/MW)  Carbon Monoxids  CO (lb/hr) = CO(ppm) x [1 - Moisture(%)/100] x 2116.8  28 (mole. wgt CO) x 60 mir/hr / [1545 x (6)  Basis, ppmvd  Basis, ppmvd @ 15% O <sub>2</sub> Moisture (%)	1,059  341.9  1.7  10  81.4  0.41  1b/R <sup>2</sup> x Volume flow (acfin) x  T temp.(°F) + 460°F) x 1,000	1,096 325.3 1.7 10 77.5 0.41	1,130 303.4 1.8 10 72.2 0.42	1,059 418.4 NA 10 108.4	396.5 NA 10 102.6	1,130 369.6 NA 10 95.6 41.9
Turbine Exhaust Temperature (°F)  CT emission rate (lb/hr) (lb/MW)  HRSG stack emission rate, ppmvd @ 15% O <sub>2</sub> HRSG stack emission rate (lb/hr) (lb/MW)  Carbon Monoxide  CO (lb/hr) = CO(ppm) x [1 - Moisture(%)/100] x 2116.8 28 (mole. wgt CO) x 60 min/hr / [1545 x (6)  Basis, ppmvd @ 15% O <sub>2</sub>	1,059  341.9 1.7 10 81.4 0.41  1b/ft² x Volume flow (acfin) x T temp.(°F) + 460°F) x 1,000 25 17.72	1,096 325.3 1.7 10 77.5 0.41 0,000 (adj. for ppp	1,130 303.4 1.8 10 72.2 0.42 m)}	1,059 418.4 NA 10 108.4 41.9 21.44	396.5 NA 10 102.6 41.8 21.18	1,130 369.6 NA 10 95.6 41.9 21.14
Turbine Exhaust Temperature (°F)  CT emission rate (lb/hr) (lb/MW)  HRSG stack emission rate, ppmvd @ 15% O <sub>2</sub> HRSG stack emission rate (lb/hr) (lb/MW)  Carbon Monoxids  CO (lb/hr) = CO(ppm) x [1 - Moisture(%)/100] x 2116.8  28 (mole. wgt CO) x 60 mir/hr / [1545 x (6)  Basis, ppmvd  Basis, ppmvd @ 15% O <sub>2</sub> Moisture (%)	1,059  341.9  1.7  10  81.4  0.41  1b/ft <sup>2</sup> x Volume flow (acfin) x  T temp.(°F) + 460°F) x 1,00  25  17.72  10.95	1,096 325.3 1.7 10 77.5 0.41 0,000 (adj. for pp) 25 17.44 11.82	(a) 1,130 303.4 1.8 10 72.2 0.42 (m)}	1,059 418.4 NA 10 108.4 41.9 21.44 13.74	396.5 NA 10 102.6 41.8 21.18 14.55	2,446,776 1,130 369.6 NA 10 95.6 41.9 21.14 15.62 7.76 2,446,776
Turbine Exhaust Temperature (°F)  CT emission rate (ib/hr)	1,059  341.9  1.7  10  81.4  0.41  (b/ft <sup>2</sup> x Volume flow (acfm) x  T temp.(°F) + 460°F) x 1,000  25  17.72 10.95 11.20	1,096 325.3 1.7 10 77.5 0.41 0,000 (adj. for pp: 25 17.44 11.82 10.97	(a) 1,130 303.4 1.8 10 72.2 0.42 (b) 12.96 10.77	1,059 418.4 NA 10 108.4 41.9 21.44 13.74 8.07	396.5 NA 10 102.6 41.8 21.18 14.55 7.90	1,130 369.6 NA 10 95.6 41.5 21.14 15.62 7.76 2,446,776
Turbine Exhaust Temperature (°F)  CT emission rate (lb/hr) (lb/MW)  HRSG stack emission rate, ppmvd @ 15% O <sub>2</sub> HRSG stack emission rate (lb/hr) (lb/MW)  Carbon Monoxide  CO (lb/hr) = CO(ppm) x [1 - Moisture(%)/100] x 2116.8 28 (mole. wgt CO) x 60 min/hr / [1545 x (6)  Basis, ppmvd  Basis, ppmvd @ 15% O <sub>2</sub> Moisture (%)  Oxygen (%)	1,059  341.9  1.7  10  81.4  0.41  1b/ft <sup>2</sup> x Volume flow (acfin) x  25  17.72  10.95  11.20  2,603,400	1,096 325.3 1.7 10 77.5 0.41 0,000 (adj. for ppi 25 17.44 11.82 10.97 2,520,733	(1,130) 303.4 1.8 10 72.2 0.42 (m)] 25 17.30 12.96 10.77 2,414,634	1,059 418.4 NA 10 108.4  41.9 21.44 13.74 8.07 2,639,095	396.5 NA 10 102.6 41.8 21.18 14.55 7.90 2,554,769	1,130 369.6 NA 10 95.6 41.9 21.14 15.62 7.76

TABLE A-8 MAXIMUM EMISSIONS FOR CRITERIA POLLUTANTS HOPKINS UNIT 2 REPOWERING PROJECT GE FRAME 7FA, DRY LOW NO $_{\rm X}$  COMBUSTOR, DISTILLATE OIL, BASE LOAD, WITH NATURAL GAS DUCT FIRING

		CT Only			ct Burner (Natur	
Parameter	25°P	Inlet Temperat		25 F w/DB		
Volatile Organic Compounds						
VOCs (lb/hr) = VOC(ppmvd) x 2116.8 lb/ft <sup>2</sup> x Volume	e flow (acfin) x					
16 (mole, wgt as methane) x 60 min/hr / [1545	x (CT temp.(°F) + 460°F) x 1,00	00,000 (adj. for p	pm)]			
Basis, ppmvw	3.50	3.50	3.50	7.6	7.5	7.5
Basis, ppmvd	3.93	3 97	4.02	8.8	8.8	8.9
Basis, ppmvd @ 15% O <sub>2</sub>	2.79	2.77	2.78	5.2	5.2	5.3
Moisture (%)	10.95	11.82	12.96	13.74	14.55	15.62
Oxygen (%)	11.20	10.97	10.77	8.07	7.90	7.76
Oxygen (%-dry)	12.58	12.44	12.37	9.36	9.25	9.20
Turbine Flow (acfm)	2,603,400	2,520,733	2,414,634	2,639,095	2,554,769	2,446,776
Turbine Exhaust Temperature (°F)	1,059	1,096	1,130	1,059	1,096	1,130
CT emission rate (lb/hr)	7.89	7,46	6.99	7.89	7.46	6.99
HRSG Stack emission rate (lb/hr)	7.89	7.46	6.99	17.1	16.0	14.9
Sulfuric Acid Mist		4400				
Sulfuric Acid Mist (Ib/hr) = SO <sub>2</sub> emission (Ib/hr) x Cor		102.0	95.1	***	105.9	98.7
CT SO <sub>2</sub> emission rate (lb/hr) - provided	107.2			111.4		
CT Conversion to H <sub>2</sub> SO <sub>4</sub> (% by weight)	20	20	20	20	20	20
DB SO <sub>2</sub> emission rate (lb/hr) - provided	0	0	0	0.0	0.0	0.0
DB Conversion to H <sub>2</sub> SO <sub>4</sub> (%) - provided	20	20	20	20	20	20
CT emission rate (lb/hr)	21,4	20.4	19.0	21.4	20.4	19.0
HRSG Stack emission rate (lb/hr)	21.4	20.4	19.0	22,3	21.2	19.7
.cad.						
Lead (lb/hr) = Basis (lb/1012 Btu) x Heat Input (MMB	tw/hr) / 1,000,000 MMBtw/10 <sup>12</sup> E	Stu				
Emission Rate Basis (lb/10 <sup>12</sup> Btu)	14	14	14	14	14	14
CT emission rate (fb/hr)	0.0291	0.0277	0.0258	0.0291	0.0277	0.0258
HRSG stack Emission rate (lb/hr)	0.0291	0.0277	0.0258	0.0291	0.0277	0.0258

TABLE A-9 DESIGN INFORMATION AND STACK PARAMETERS FOR THE HOPKINS UNIT 2 REPOWERING PROJECT GE FRAME 7FA, DRY LOW NO\_x COMBUSTOR, DISTILLATE OIL, 75% LOAD

	Turbine Inlet Temperature			
Parameter	25 °F	59 °F	95 °F	
Combustion Turbine Performance				
Power output (MW)	149.2	140.9	129.	
Heat rate (Btu/kWh, LHV)	10,580	10,740	10,94	
(Btu/kWh, HHV)	11,215	11,385	11,59	
Heat Input (MMBtu/hr, LHV)	1,579	1,513	1,41	
(MMBtu/hr, HHV)	1,673	1,604	1,49	
Relative Humidity (%)	87	78	5	
Fuel heating value (Btu/lb, LHV)	18,300	18,300	18,30	
(Btu/lb, HHV)	19,398	19,398	19,39	
(HHV/LHV)	1.060	1.060	1.06	
CT Exhaust Flow				
Mass Flow (lb/hr)- with no margin	3,085,000	2,993,000	2,848,00	
- provided	3,085,000	2,993,000	2,848,00	
Temperature (°F)	1,136	1,159	1,18-	
Moisture (% Vol.)	10.91	11.46	12.2	
Oxygen (% Vol.)	10.96	10.96	10.9	
Molecular Weight	28.38	28.31	28,2	
Fuel Usage				
Fuel usage (lb/hr) = Heat Input (MMBtu/hr) x 1,000,000	D Btu/MMBtu (Fuel Heat Content, Btu/	lb (LHV))		
Heat input (MMBtu/hr, LHV)	1,579	1,513	1,41	
Heat content (Btu/lb, LHV)	18,300	18,300	18,300	
Fuel usage (lb/hr)- calculated	86,257	82,694	77,29	
HRSG Stack and Flow Conditions				
Stack Height (ft)	150	150	150	
Diameter (ft)	18	18	18	
Velocity (fl/sec) = Volume flow (acfin) / [((diameter)* /4	x 3.14159] / 60 sec/min			
Mass flow (lb/hr)	3,085,000	2,993,000	2,848,000	
Stack Temperature (oF)	233	233	232	
Molecular weight	28.38	28.31	28.21	
Volume flow (acfm)	916,430	891,229	849,841	
Diameter (fl)	18	18	18	
Velocity (ft/sec)- calculated	60.0	58.4	55.7	

Note: Universal gas constant = 1,545 ft-lb(force)/6R; atmospheric pressure = 2,116.8 lb(force)/ft<sup>2</sup>; 14.7 lb/ft<sup>3</sup>.

 $TABLE~a\cdot 10$  MAXIMUM EMISSIONS FOR CRITERIA POLLUTANTS FOR THE HOPKINS UNIT 2 REPOWERING PROJECT GE FRAME 7FA, DRY LOW NO\_x COMBUSTOR, DISTILLATE OIL, 75% LOAD

	Turbi	ne Inlet Temperature	
Parameter	25 °F	59 °F	95 °F
Particulate from CT and SCR		<u> </u>	
Total PM <sub>10</sub> = PM <sub>10</sub> (front half) + PM <sub>10</sub> ((NH <sub>4</sub> ) <sub>2</sub> SO <sub>4</sub> ) from SCR only			
a. PM <sub>10</sub> (front half) (lb/hr)			
CT- provided	17.0	17.0	17
b. PM <sub>10</sub> ((NH <sub>4</sub> ) <sub>2</sub> SO <sub>4</sub> ) from SCR only = Sulfur trioxide from convers	sion of SO <sub>2</sub> converts to ammoni	um sulfate (= PM <sub>10</sub> )	
Particulate from conversion of $SO_2 = SO_2$ emissions (lb/hr) x co	onversion of SO <sub>2</sub> to SO <sub>3</sub> x lb SC	)₁/lb SO₂ x	
	NH <sub>4</sub> ) <sub>2</sub> SO <sub>4</sub> x lb (NH <sub>4</sub> ) <sub>2</sub> SO <sub>2</sub> / lb S	-	
SO <sub>2</sub> emission rate (lb/lur)- calculated	86 3	82.7	71
Conversion (%) from SO <sub>2</sub> to SO <sub>3</sub>	9.8	9.8	5
MW SO√ SO <sub>2</sub> (80/64)	1.3	1.3	1
Conversion (%) from SO <sub>4</sub> to (NH <sub>4</sub> ) <sub>2</sub> (SO <sub>4</sub> )	100	100	1
MW (NH <sub>4</sub> ) <sub>2</sub> SO <sub>4</sub> / SO <sub>3</sub> (132/80)	1.7	1.7	1
SCR Particulate (lb/hr)- calculated	17.43	16.71	15.
CT emission rate (lb/hr) [a]	17.0	17.0	17
HRSG stack emission rate (lb/hr) [a + b]	34.4	33.7	33
(Ib/mmBtu, HHV)	0.0206	0.0210	0.02
ulfur Dioxide			
SO2 (lb/hr)= Fuel oil (lb/hr) v sulfur content(% weight) v (lb SO2 /lb	S) /100		
Fuel oil Sulfur Content	0.050%	0.050%	0.050
Fuel oil use (lb/hr)	86,257	82,694	77,2
lb SO2 / lb S (64/32)	2	2	,
CT emission rate (lb/hr)	86.3	82.7	77
HRSO Stack emission rate (lb/hr)	86.3	82.7	77
Sprogen Oxides			
NOx (lb/hr) = NOx (ppinvd $@$ 15% O <sub>2</sub> ) x ([20.9 x (1-Moisture (%)/]			(acfm) x
46 (mole, wgt NOx) x 60 min/hr / [1545 x (CT temp.	(°F) + 460) x (20.9-15) x t,000	,000 (adj. for ppm)}	
CT/DB, ppmvd @ 15% O <sub>2</sub>	42	42	
Moisture (%)	10.91	11.46	12.3
Oxygen (%)	10,96	10.96	10.9
Turbine Flow (acfin)	2,110,565	2,082,106	2,018,98
Turbine Exhaust Temperature (°F)	1,136	1,159	1,11
CT Emission rate (lb/hr)	272.7	261.2	244
•	10	10	10
HRSG Stack emission rate, ppinvd @ 15% O2		62.2	58
HRSG Stack emission rate, ppinvd @ 15% O <sub>2</sub> HRSG Stack emission rate (lb/hr)	64.9		50
HRSG Stack emission rate (lb/hr)  Carbon Monoxide			
HRSG Stack emission rate (lb/hr)  Carbon Monoxide  CO (lb/hr) = CO(ppin) x [1 - Moisture(%)/100] x 2116.8 lb/ft <sup>2</sup> x Voli	ume flow (acfm) x	ppm)ļ	
HRSG Stack emission rate (lb/hr) Carbon Monoxide	ume flow (acfm) x	r ppm)  25	
HRSG Stack emission rate (lb/hr)  Carbon Monoxide  CO (lb/hr) = CO(ppin) x [1 - Moisture(%)/100] x 2116.8 lb/ft <sup>2</sup> x Voli 28 (mole, wgt CO) x 60 min/hr / [1545 x (CT temp.(°f Basis, ppmvd Moisture (%)	ume flow (acfm) x 7) + 460°F) x 1,000,000 (adj. fo		2
HRSG Stack emission rate (lb/hr)  Carbon Monoxide  CO (lb/hr) = CO(ppm) x [1 - Moisture(%)/100] x 2116.8 lb/ft <sup>2</sup> x Vol.  28 (mole. wgt CO) x 60 min/hr / [1545 x (CT temp.(°f Basis, ppmvd Moisture (%)  Turbine Flow (acfm)	ume flow (acfm) x F) + 460°F) x 1,000,000 (adj. for 25	25	2 12.2 2,018,98
HRSG Stack emission rate (lb/hr)  Carbon Monoxide  CO (lb/hr) = CO(ppm) x [1 - Moisture(%/100] x 2116.8 lb/ft <sup>2</sup> x Vol. 28 (mole, wgt CO) x 60 min/hr / [1545 x (CT temp.(°f Basis, ppmvd Moisture (%) Turbine Flow (acfm) Turbine Exhaust Temperature (°F)	ume flow (acfm) x F) + 460°F) x 1,000,000 (adj. for 25 10.91	25 11 46	2 12.2 2,018,98
HRSG Stack emission rate (lb/hr)  Carbon Monoxide  CO (lb/hr) = CO(ppm) x [1 - Moisture(%)/100] x 2116.8 lb/ft <sup>2</sup> x Vol.  28 (mole. wgt CO) x 60 min/hr / [1545 x (CT temp.(°f Basis, ppmvd Moisture (%)  Turbine Flow (acfm)	name flow (acfm) x F) + 460°F) x 1,000,000 (adj. for 25 10.91 2,110,565	25 11 46 2,082,106	2 12.2 2,018,98 t,18
HRSG Stack emission rate (lb/hr)  Carbon Monoxide  CO (lb/hr) = CO(ppm) x [1 - Moisture(%/100] x 2116.8 lb/ft <sup>2</sup> x Vol. 28 (mole, wgt CO) x 60 min/hr / [1545 x (CT temp.(°f Basis, ppmvd Moisture (%) Turbine Flow (acfm) Turbine Exhaust Temperature (°F)	nume flow (acfm) x F) + 460°F) x 1,000,000 (adj. fo 25 10.91 2,110,565 1,136	25 11 46 2,082,106 1,159	2 12.2

 $TABLE\ A-10$  MAXIMUM EMISSIONS FOR CRITERIA POLLUTANTS FOR THE HOPKINS UNIT 2 REPOWERING PROJECT GE FRAME 7FA, DRY LOW NO<sub>X</sub> COMBUSTOR, DISTILLATE OIL, 75% LOAD

	Turbii	ne Inlet Temperature	
Parameter	25 °F	59 °F	95 °F
Volatile Organic Compounds			
VOCs (ib/hr) = VOC(ppmvd) x 2116.8 ib/ft <sup>2</sup> x Volume flow (acfir	n) x		
16 (mole, wgt as methane) x 60 min/hr / (1545 x (CT temp	.(°F) + 460°F) x 1,000,000 (adj. f	or ppin)]	
Basis, ppmvw	3.5	3.5	3.
Moisture (%)	10.91	11.46	12,2
Turbine Flow (acfm)	10.96	10.96	10.90
Turbine Exhaust Temperature (°F)	2,110,565	2,082,106	2,018,98
HRSG Exhaust Temperature (°F)	1,136	1,159	1,18
CT Emission rate (lb/hr)	6.09	5.92	5.6
HRSG Stack emission rate (lb/hr)	6.09	5.92	5.6
Sulfuric Acid Mist			
Sulfuric Acid Mist (lb/hr)= SO2 emission (lb/hr) x Conversion to I	I <sub>2</sub> SO <sub>4</sub> (% by weight)/100		
CT SO <sub>2</sub> emission rate (lb/hr) - provided	86.3	82,7	77.3
CT Conversion to H2SO4 (% by weight) - provided	20	20	20
DB SO <sub>2</sub> emission rate (lb/hr) - provided	0	0	(
DB Conversion to H <sub>2</sub> SO <sub>4</sub> (%) - provided	20	20	20
CT Emission rate (lb/hr)	17.25	16.54	15.46
HRSG Stack emission rate (lb/hr)	17.25	16.54	15.46
Lead			
Lead (lb/hr) = Basis (lb/1012 Btu) x Heat Input (MMBtu/hr) / 1,000	0,000 MMBtu/10 <sup>12</sup> Btu		
Emission Rate Basis (lb/1012 Btu)	14	14	14
CT Emission rate (lb/hr)	0.0221	0.0212	0.0198
HRSG Stack emission rate (lb/hr)	0.0221	0.0212	0.0198

Note: ppinvd= parts per million, volume dry; O2= oxygen.

TABLE A-11 DESIGN INFORMATION AND STACK PARAMETERS FOR THE HOPKINS UNIT 2 REPOWERING PROJECT GE FRAME 7FA, DRY LOW NO $_{\rm X}$  COMBUSTOR, DISTILLATE OIL, 60% LOAD

	Turbine falet Temperature			
Parameter	25 °F	59 °F	95 °F	
Combustion Turbine Performance		· · · · ·		
Power output (MW)	119.4	1 t 2.7	103.	
Heat rate (Btu/kWh, LHV)	11,570	11,750	12,01	
(Btu/kWh, HHV)	12,265	12,455	12,73	
Heat Input (MMBtu/hr, LHV)	1,382	1,324	1,24	
(MMBtu/hr, HHV)	1,464	1,404	1,31	
Relative Humidity (%)	87	78	. 5	
Fuel heating value (Btu/lb, LHV)	18,300	18,300	18,30	
(Btw/lb, HHV)	19,398	19,398	19,39	
(HHV/LHV)	1.060	1.060	1.06	
CT Exhaust Flow				
Mass Flow (lb/hr)- with no margin	2,743,000	2,667,000	2,579,00	
- provided	2,743,000	2,667,000	2,579,00	
Temperature (°F)	1,167	1,188	1,20	
Moisture (% Vol.)	10.42	10.96	11.6	
Oxygen (% Vol.)	11.23	11.23	11.3	
Molecular Weight	28.42	28.35	28.2	
Fuel Usage				
Fuel usage (lb/hr) = Heat Input (MMBtu/hr) x 1,000,000	) Btu/MMBtu (Fuel Heat Content, Btu/II	(LHV))		
Heat input (MMBtu/hr, LHV)	1,382	1,324	1,24	
Heat content (Btu/lb, LHV)	18,300	18,300	18,30	
Fuel usage (lb/hr)- calculated	75,492	72,361	67,92	
HRSG Stack and Flow Conditions				
Stack Height (ft)	150	150	150	
Diameter (fl)	18	18	1:	
Velocity (fl/sec) = Volume flow (acfm) / {((diameter) <sup>2</sup> /4	3) x 3.14159] / 60 sec/min			
Mass flow (lb/hr)	2,743,000	2,667,000	2,579,000	
Stack Temperature (oF)	223	223	22.	
Molecular weight	28.42	28.35	28.2	
Volume flow (acfin)	802,010	781,670	757,25	
Diameter (ft)	18	18	11	
Velocity (fl/sec)- calculated	52.5	51.2	49.6	

Note: Universal gas constant = 1,545 fl-lb(force)/°R; atmospheric pressure = 2,116.8 lb(force)/fl<sup>2</sup>; 14.7 lb/fl<sup>3</sup>.

TABLE~A-12 MAXIMUM EMISSIONS FOR CRITERIA POLLUTANTS FOR THE HOPKINS UNIT 2 REPOWERING PROJECT GE FRAME 7FA, DRY LOW NO\_x COMBUSTOR, DISTILLATE OIL, 60% LOAD

		e lalet Temperature	ture	
Parameter	25 °F	59 °F	95 °F	
Particulate from CTand SCR				
Total PM10 = PM10 (front half) + PM10 ((NH4)2SO4) from SCR or	ily			
a. PM <sub>10</sub> (front half) (lb/hr)				
CT- provided	17.0	17.0	17.0	
b. PM <sub>10</sub> ((NH <sub>4</sub> ) <sub>2</sub> SO <sub>4</sub> ) from SCR only = Sulfur thoxade from con-	version of SO <sub>2</sub> converts to armino	nium sulfate (= PM <sub>in</sub> )	•	
Particulate from conversion of $SO_2 = SO_2$ emissions (lb/hr):	<u>-</u>	. ,,,,		
conversion of SO <sub>1</sub>	to (NH <sub>4</sub> ) <sub>2</sub> SO <sub>4</sub> x lb (NH <sub>4</sub> ) <sub>2</sub> SO <sub>4</sub> lb	SO <sub>3</sub>		
SO <sub>2</sub> emission rate (lb/hr)- calculated	75.5	72.4	67.9	
Conversion (%) from SO <sub>2</sub> to SO <sub>3</sub>	9.8	9.8	9.1	
MW SO <sub>3</sub> / SO <sub>2</sub> (80/64)	1.3	1.3	1.3	
Conversion (%) from SO <sub>1</sub> to (NH <sub>4</sub> ) <sub>7</sub> (SO <sub>4</sub> )	100	100	10	
MW (NH <sub>4</sub> ) <sub>2</sub> SO <sub>4</sub> SO <sub>3</sub> (132/80)	1.7	1.7	1.3	
SCR Particulate (lb/hr)- calculated	15.26	14.63	13.73	
CT emission rate (lb/hr) [a]	17.0	17.0	17.0	
HRSG stack emission rate (lb/hr) [a + b]	32.3	31 6	30.	
(lb/mmBtu, HHV)	0.0220	0.0225	0.023	
Sulfur Dioxide				
SO <sub>2</sub> (lb/hr)= Fuel oil (lb/hr) x sulfur content(% weight) x (lb SO <sub>2</sub>	/lb S) /100			
Fuel oil Sulfur Content	0.050%	0.050%	0.050%	
Fuel oil use (lb/hr)	75,492	72,361	67,92	
Ib SO2 / Ib S (64/32)	, , , ,	7	01,72	
CT emission rate (lb/hr)	75.5	72.4	67.9	
HRSG Stack emission rate (lb/hr)	75.5	72.4	67.5	
Nitrogen Oxides				
NOx (lb/hr) = NOx (ppmvd@ 15% O <sub>2</sub> ) x {{20.9 x (1-Moisture (%	1/100] - Oxygen drof*(1) × 211)	5.8 lb/ft <sup>2</sup> x Volume flo	w (acfm) ×	
46 (mole, wgt NOx) x 60 min/hr / [1545 x (CT tel				
CT/DB, ppmvd @15% O <sub>3</sub>	мр.( г) + 400) х (20 9-13) х 1 <sub>1</sub> 0 <sub>1</sub> 42	u,vov (auj. 101 ppm)j 42	42	
Moisture (%)	10.42	10.96		
Moisture (%) Oxygen (%)	10.42	11.23	11.63	
Turbine Flow (acfm)	1,910,499		11.33	
Turbine Exhaust Temperature (°F)		080,888,1 881,1	1,843,173	
Twome Exhaust Temperature ( F)	1,167	1,105	1,200	
CT Emission rate (lb/hr)	236.8	227.3	213.4	
	01	10	10.0	
HRSG Stack emission rate, ppmvd @ 15% O2	10	54.1	50.8	
HRSG Stack emission rate, ppmvd @ 15% O <sub>2</sub> HRSG Stack emission rate (lb/hr)	56.4	34.1	30.0	
0		34.1	50.6	
HRSG Stack emission rate (lb/hr)  Carbon Monoxide  CO (lb/hr) = CO(ppm) x [1 - Moisture(%)/100] x 2116.8 lb/ft² x 1	56.4 Volume flow (acfm) x		30.8	
HRSG Stack emission rate (lb/hr)  Carbon Monoxide  CO (lb/hr) = CO(ppm) x [1 - Moisture(%)/100] x 2116.8 lb/ft <sup>2</sup> x \dagger 28 (mole, wgt CO) x 60 min/hr / [1545 x (CT temp	56.4 Volume flow (acfm) x .(°F) + 460°F) x 1,000,000 (adj.	for ppm)]		
HRSG Stack emission rate (lb/hr)  Carbon Monoxide  CO (lb/hr) = CO(ppm) x [1 - Moisture(%)/100] x 2116.8 lb/ft <sup>2</sup> x 1  28 (mole. wgt CO) x 60 min/hr / [1545 x (CT temp Basis, ppmvd	56.4 Volume flow (acfm) x .(°F) + 460°F) x 1,000,000 (adj. 25	for ppm)] 25	25	
HRSG Stack emission rate (lb/hr)  Carbon Monoxide  CO (lb/hr) = CO(ppm) x [1 - Moisture(%)/100] x 2116.8 lb/ft <sup>2</sup> x 7  28 (mole. wgt CO) x 60 min/hr / [1545 x (CT temp Basis, ppmvd Moisture (%)	56.4 Volume flow (acfm) x L(°F) + 460°F) x 1,000,000 (adj. 25 10.42	for ppm)] 25 10 96	25 11.63	
HRSG Stack emission rate (lb/hr)  Carbon Monoxide  CO (lb/hr) = CO(ppm) x [1 - Moisture(%)/100] x 2116.8 lb/ft <sup>2</sup> x 1 28 (mole. wgt CO) x 60 min/hr / [1545 x (CT temp Basis, ppm/vd Moisture (%)  Turbine Flow (acfin)	56.4 Volume flow (acfm) x .(°F) + 460°F) x 1,000,000 (adj. 25 10.42 1,910,499	for ppm)] 25 10 96 1,886,080	25 11.63 1,843,173	
HRSG Stack emission rate (lb/hr)  Carbon Monoxide  CO (lb/hr) = CO(ppm) x [1 - Moisture(%4)/100] x 2116.8 lb/ft <sup>2</sup> x v  28 (mole, wgt CO) x 60 min/hr / [1545 x (CT temp Basis, ppmvd Moisture (%4) Turbine Flow (acfin) Turbine Exhaust Temperature (°F)	56.4 Volume flow (acfin) x .(°F) + 460°F) x 1,000,000 (adj. 25 10.42 1,910,499 1,167	for ppm)] 25 10 96 1,886,080 1,188	25 11.63 1,843,173 1,200	
HRSG Stack emission rate (lb/hr)  Carbon Monoxide  CO (lb/hr) = CO(ppm) x [1 - Moisture(%)/100] x 2116.8 lb/ft <sup>2</sup> x 1 28 (mole. wgt CO) x 60 min/hr / [1545 x (CT temp Basis, ppm/vd Moisture (%)  Turbine Flow (acfin)	56.4 Volume flow (acfm) x .(°F) + 460°F) x 1,000,000 (adj. 25 10.42 1,910,499	for ppm)] 25 10 96 1,886,080	25 11.63 1,843,173	
HRSG Stack emission rate (lb/hr)  Carbon Monoxide  CO (lb/hr) = CO(ppm) x [1 - Moisture(%4)/100] x 2116.8 lb/ft <sup>2</sup> x v  28 (mole, wgt CO) x 60 min/hr / [1545 x (CT temp Basis, ppmvd Moisture (%4) Turbine Flow (acfin) Turbine Exhaust Temperature (°F)	56.4 Volume flow (acfin) x .(°F) + 460°F) x 1,000,000 (adj. 25 10.42 1,910,499 1,167	for ppm)] 25 10 96 1,886,080 1,188	25 11.63 1,843,173 1,200	

 $TABLE\ A-12$  MAXIMUM EMISSIONS FOR CRITERIA POLLUTANTS FOR THE HOPKINS UNIT 2 REPOWERING PROJECT GE FRAME 7FA, DRY LOW NO\_X COMBUSTOR, DISTILLATE OIL, 60% LOAD

	Turbine Inlet Temperature			
Parameter	25 °F	59 °F	95 °F	
Volatile Organic Compounds				
VOCs ( $\frac{1}{2}$ / $\frac{1}{2}$ VOC(ppmvd) x 2116.8 $\frac{1}{2}$ Volume flow (act	fm) x			
16 (mole, wgt as methane) x 60 min/hr / [1545 x (CT tem	p.(°F) + 460°F) x 1,000,000 (ad)	. for ppm)]		
Basis, ppmvw	3.5	3.5	3.5	
Moisture (%)	10,42	10.96	11.63	
Turbine Flow (acfm)	11.23	11.23	11.33	
Turbine Exhaust Temperature (°F)	1,910,499	1,886,080	1,843,173	
HRSG Exhaust Temperature (°F)	1,167	1,188	1,200	
CT Emission rate (lb/hr)	5.41	5.27	5.11	
HRSG Stack emission rate (lb/hr)	5.41	5.27	5.11	
Sulfurie Acid Mist				
Sulfuric Acid Mist (lb/hr)= SO2 emission (lb/hr) x Conversion to	H <sub>2</sub> SO <sub>4</sub> (% by weight)/100			
CT SO <sub>2</sub> emission rate (lb/hr) - provided	75.5	72.4	67.9	
CT Conversion to H2SO4 (% by weight) - provided	20	20	20	
DB SO <sub>2</sub> emission rate (lb/hr) - provided	0	0	0	
DB Conversion to H <sub>2</sub> SO <sub>4</sub> (%) - provided	20	20	20	
CT Emission rate (lb/hr)	15.10	14.47	13.58	
HRSG Stack emission rate (lb/hr)	15.10	14.47	13.58	
Lead				
Lead (ib/hr) = Basis (lb/ $10^{12}$ Btu) x Heat input (MMBtu/hr) / 1,00	00,000 MMBtu/10 <sup>12</sup> Btu			
Emission Rate Basis (lb/10 <sup>12</sup> Btu)	14	14	14	
CT Emission rate (lb/lu)	0.0193	0.0185	0 0174	
HRSG Stack emission rate (lb/hr)	0.0193	0.0185	0.0174	

Note: ppinvd= parts per million, volume dry; O2= oxygen.

TABLE A-13
DUCT BURNER EMISSIONS: FULL DUCT FIRING

	Emission Rate		Heat Inpu	<u>it (MMBru/l</u>	br) (HHV)	Emission Rate (lb/hr)		
Pollutant	(lb/MMBtu)	AP-42	25 °F	59 °F	95 °F	25 °F	59 °F	95 °F
Natural Gas-Firing								
PM-10	0.012		765	712	663	9.2	8.5	8.0
NO.	0.10		765	712	663	76.5	71.2	66.3
co	0.072		765	712	663	55.0	51.2	47.7
VOC	0.012		765	712	663	9.2	8.5	8.0

Natural gas:	<u>iring</u> AP-42 (199)	3)	
PM-10	i.9 lb/10 <sup>6</sup> scf		0.0018 lb/MMBtu
NOx	190 lb/10 <sup>6</sup> scf	h	0.183 lb/MMBnu
co	84 lb/10 <sup>6</sup> scf	b .	0.081 1b/MMBtu
VOC	5.5 lb/10 <sup>6</sup> scf	•	0.0053 fb/MMBtu

1036 Btu/scf

Heat content

Table 1.4-2. Emission Factors for Criteria Pollutants and Greenhouse Gases from Natural Gas Combustion, Uncontrolled Post-NSPS

Table 1.4-1. Emission Factors for Nitrogen Oxides (NOx) and Carbon Monoxide (CO) from Natural Gas Combustion

TABLE A-14

REGULATED AND HAZARDOUS AIR POLLUTANT EMISSION FACTORS AND EMISSIONS
FOR HOPKINS UNIT 2 REPOWERING PROJECT, NATURAL GAS-FIRING ONLY

Parameter	Emission Rate (I	Natural Gas Maximum Annu	
	for Operating C	Emissions (TPY)	
Ambient Temperature (*F):	59 °F	59 °F w/DB	59 °F
HIR (MMBtu/hr):	1,795	2,506	CT/HRSG
HAPs (Section 112(b) of Clean Air Act)			
1,3-Butadiene	7.72E-04	1.08E-03	4.18E-03
Acetaldehyde	7.18E-02	1.00E-01	3.89E-01
Acrolein	1.15E-02	1.60E-02	6.23E-02
Benzene	2.15E-02	3.01E-02	1.17E-01
Ethylbenzene	5.74E-02	8.02E-02	3.11E-01
ormadehyde	3.85E-01	5.34E-01	2.08E+00
Vaphthalene	2.33E-03	3.26E-03	1.27E-02
olycyclic Aromatic Hydrocarbons (PAH)	3.95E-03	5.51E-03	2.14E-02
Propylene Oxide	5.20E-02	7.27E-02	2.82E-01
Toluene	5.92E-02	8.27E-02	3.21E-01
Sylene	1.15E-01	1.60E-01	6.23E-01
Antimony	0.00E+00	0.00E+00	0.00E+00
Arsenic	0.00E+00	0.00E+00	0.00E+00
Beryllium	0.00E+00	0.00E+00	0.00E+00
Cadmium	0.00E+00	0.00E+00	0.00E+00
Chromium	0.00E+00	0 00E+00	0.00E+00
æad	0.00E+00	0.00E+00	0.00E+00
Manganese	0.00E+00	0.00E+00	0.00E+00
Mercury	0.00E+00	0.00E+00	0.00E+00
Nickel	0.00E+00	0.00E+00	0.00E+00
Selenium	0.00E+00	0.00E+00	0.00E+00
-IAPs (Total)	0.780	1.086	4.22

Emission Factors	Value Reference
1,3-Butadiene (	(a) 0.43 lb/10 <sup>12</sup> Btu; AP-42, Table 3.1-3. EPA 2000
Acetaldehyde	40 lb/10 <sup>12</sup> Btu; AP-42, Table 3.1-3. EPA 2000
Acrolein	6.4 lb/10 <sup>12</sup> Btu; AP-42, Table 3.1-3. EPA 2000
Benzene	12 lb/10 <sup>12</sup> Btu; AP-42,Table 3.1-3, EPA 2000
Ethylbenzene	32 lb/10 <sup>12</sup> Btu; AP-42, Table 3.1-3. EPA 2000
Formadehyde	0.091 ppmvd @15% O2 (see Table 15a)
Naphthalene	1.3 lb/10 <sup>12</sup> Btu; AP-42, Table 3.1-3. EPA 2000
Polycyclic Aromatic Hydrocarbons (PAH)	2.2 lb/1012 Btu; AP-42, Table 3.1-3. EPA 2000
Propylene Oxide (	(a) 29 lb/10 <sup>12</sup> Btu; AP-42, Table 3.1-3, EPA 2000
Toluene	33 lb/10 <sup>12</sup> Btu; AP-42, Table 3.1-3. EPA 2000. Database
Xylene	64 lb/10 <sup>12</sup> Btu; AP-42, Table 3.1-3. EPA 2000
Antimony	0.00E+00
Arsenic	0.00E+00
Beryllium	0.00E+00
Cadmium	0.00E+00
Chromium	0.00E+00
Lead	0.00E+00
Manganese	0.00E+00
Mercury	0.00E+00
Nickel	0.00E+00
Selenium	0.00E+00

Annual emissions based on ambient temperature of 59 °F firing natural gas for following hours:

(a) Based on 1/2 the detection limit; expected emissions are lower.

<sup>3,500</sup> hours, NG w/o duct firing 5,260 hours, NG w/ duct firing

Assumed to be representative of Polycyclic Organic Matter (POM) emissions, a regulated HAP.

TABLE A-15 MAXIMUM FORMALDEHYDE EMISSIONS FOR THE HOPKINS UNIT 2 REPOWERING PROJECT GE FRAME 7FA, DRY LOW NO\_X COMBUSTOR, NATURAL GAS, BASE LOAD

Parameter		CT Only  Turbine Inlet Temperature			
	25 °F	59 °F	25 °F w/DB	59 °F w/DB	
Formaldehyde (CH <sub>2</sub> O) MW =	30				
$CH_2O (lb/hr) = CH_2O (ppmvd@ 15\% O2) x {[20.9]}$	(1-Moisture (%)/100] - Oxygen, dry(%)} >	: 2116.8 lb/ft2 x Volum	e flow (acfm) x		
	$1545 \times (CT \text{ temp.}(^{\circ}F) + 460) \times (20.9-15) \times$				
CT, ppmvd @15% O <sub>2</sub>	0.091	0.091	0.091	0.091	
Moisture (%)	7.54	8.55	10.26	11.21	
Oxygen (%)	12.77	12.57	9.76	9.61	
Turbine Flow (acfm)	1,083,262	1,023,573	1,075,526	1,016,095	
Turbine Exhaust Temperature (°F)	203	202	189	188	
CT Emission rate (lb/hr)	0.407	0.385	0.567	0.534	
CT Emission rate (lb/10 <sup>12</sup> Btu) (HHV)	214.5	214,4	213.0	200.4	

TABLE A-16

REGULATED AND HAZARDOUS AIR POLLUTANT EMISSION FACTORS AND EMISSIONS FOR THE HOPKINS UNIT 2 REPOWERING PROJECT

NATURAL GAS-FIRING AND DISTILLATE OIL-FIRING

Parameter	Emission Rate (lb/hr) Firing Distillate Fuel Oil *	Maximum Annual Emissions (TPY)		
Ambient Temperature (°F):	Base Load 59 °F	Distillate Fuel Oil	Natural Gas 4	Natural Gas and
•	•	1		
HIR (MMBiu/br):	1,979	CT/HRSG	CT/HRSG	Fuel Oil *
HAPs (Section 112(b) of Clean Air Act)				
L3-Butadiene	3.17E-02	3.17E-02	4.18E-03	3.45E-02
Acetaldehyde	0 00E+00	0 00E+00	3.89E-01	2.64E-01
Acrol <del>cin</del>	0.00E+00	0 00E+00	6.23E-02	4 22E-02
Benzene	1.09E-01	1.09E-01	1.17E-01	1,88E-01
Shylbenzene	0.00E+00	0.00E+00	3.11E-01	2.11E-01
formadehyde	4.60E-01	4.60E-01	2.08E+00	1.86E+00
Naphthalene	6 93E-02	6.93E-02	1.27E-02	7.78E-02
Polycyclic Aromatic Hydrocarbons (PAH)	7.92E-02	7.92E-02	2.14E-02	9.37E-02
Propylene Oxide	0 00E+00	0 00E+00	2.82E-01	1.91E-01
Coluene Coluene	0.00E+00	0.00E+00	3.21E-01	2.18E-01
Kylene	0.00E+00	0.00E+00	6.23E-01	4.22E-01
Antimony	0.00E+00	0 00E+00	0.00E+00	0.00E+00
Arsenic	2.18E-02	2.18E-02	0 00E+00	2.18E-02
Beryllium	6.13E-04	6.13E-04	0.00E+00	6.13E-04
Cadmium	9,50E-03	9 50E-03	0.00E+00	9.50E-03
Chromium	2.18E-02	2.18E-02	0.00E+00	2.18E-02
.ead	2.77E-02	2 77E-02	00+300	2.77E-02
Manganese	1.56E+00	1.56E+00	0.00E+00	1.56E+00
Mercury	2.37E-03	2.37E-03	0 00E+00	2.37E-03
Nickel	9.10E-03	9.10E-03	0 00E+00	9.10E-03
Selenium	4.95E-02	4.95E-02	0 00E+00	4.95E-02
-lAPs (Total)	2.45	1.64	4.2	5.3

<sup>\*</sup> Emissions based on the following emission factors and conversion factors for firing distillate fuel oil.

Emission Factors	Valu Reference
Sulfuric acid mist	5 %; Conversion of SO <sub>2</sub> to SO <sub>3</sub> in gas turbine
1.3-Butadiene	(a) 16 fb/10 <sup>12</sup> Btu; AP-42, Table 3.1-4. EPA 2000
Acetaldehyde	00
Acrolein	0.0
Benzene	55 lb/1012 Btu; AP-42, Table 3 1-4. EPA 2000
Ethylbenzene	0 0
Formadehyde	### ppmvd @15% O <sub>2</sub> (see Table 16a)
Naphthalene	35 lb/10 <sup>12</sup> Bru; AP-42, Table 3.1-4. EPA 2000
Polycyclic Aromatic Hydrocarbons (PAH)	40 lb/10 <sup>12</sup> Btu, AP-42, Table 3.1-4, EPA 2000
Propylene Oxide	0.0
Toluene	0 0
Xylene	0 0
Antimony	0 0
Arsenic	(a) 11 lb/10 <sup>12</sup> Btu; AP-42,Table 3.1-5, EPA 2000
Beryllium	(a) 0.3 Rb/10 <sup>12</sup> Bru; AP-42, Table 3.1-5. EPA 2000
Cadmium	4.8 fb/10 <sup>12</sup> Btu; AP-42,Table 3.1-5. EPA 2000
Chromsum	11 fb/10 <sup>12</sup> Btu; AP-42, Table 3.1-5. EPA 2000
Lead	14 lb/10 <sup>12</sup> Btu; AP-42,Table 3.1-5, EPA 2000
Manganese	790 lb/t0 <sup>12</sup> Bru, AP-42,Table 3.1-5. EPA 2000
Mercury	1.2 lb/10 <sup>12</sup> Btu; AP-42,Table 3.1-5. EPA 2000
Nickel	(a) 4 6 lb/1612 Btu; AP-42, Table 3.1-5. EPA 2000
Selenium	(a) 25 lb/10 <sup>12</sup> Bru; AP-42, Table 3 1-5. EPA 2000

<sup>(</sup>a) Based on 1/2 the detection limit; expected emissions are lower.

3,500 hours, FO w/o duct firing

3,500 hours, NG w/o duct firing 5,260 hours, NG w/ duct firing

0 hours, NG w/o duct firing 5,260 hours, NG w/ duct firing

<sup>&</sup>lt;sup>b</sup> Annual emissions based on ambient temperature of 59 °F and firing fixel oil at base load for :

<sup>&</sup>lt;sup>e</sup> Assumed to be representative of Polycyclic Organic Matter (POM) emissions, a regulated HAP.

<sup>&</sup>lt;sup>d</sup> Annual emissions based on maximum emissions presented for natural gas-firing

<sup>\*</sup> Maximum total annual emissions based on maximum oil-firing and natural gas firing

TABLE A-17 MAXIMUM FORMALDEHYDE EMISSIONS FOR THE HOPKINS UNIT 2 REPOWERING PROJECT GE FRAME 7FA, DRY LOW NO $_{\rm X}$  COMBUSTOR, DISTILLATE OIL, BASE LOAD

	CT Only			
	Turbine Inlet Temperature			
Parameter	25 °F	59 °F		
F. HILL (CHO) MAY	70			
Formaldehyde (CH <sub>2</sub> O) MW =	30			
$CH_2O$ (lb/hr) = $CH_2O$ (ppmvd@ 15% O2) x {[20.9 x (1-Moistur	re (%)/100] - Oxygen, dry(%)} x 2116.8 lb/ft2 x Volume flow	v (acfm) x		
30 (mole. wgt CH2O) x 60 min/hr / [1545 x (CT	T temp.(°F) + 460) x (20.9-15) x 1,000,000 (adj. for ppm)]			
CT, ppmvd @15% O <sub>2</sub>	0.091	0.091		
Moisture (%)	10.95	11.82		
Oxygen (%)	11.20	10.97		
Exhaust Flow (acfm)	1,213,435	1,146,966		
Exhaust Temperature (°F)	248	248		
CT Emission rate (lb/hr)	0.483	0.460		
CT Emission rate (lb/10 <sup>12</sup> Btu) (HHV)	232.4	232.3		