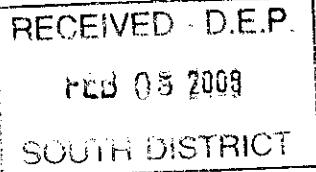




February 4, 2009

Ajaya Satyal
Environmental Administrator
Florida Department of Environmental Protection - South District
2295 Victoria Avenue
P.O. Box 2549
Fort Myers, Florida 33902-2549

**RE: E-Stone USA Corporation
Title V Air Operating Permit Application
EPSAP Application No.: 2165-1**



Dear Mr. Satyal:

Enclosed are the professional engineer signature document and the attachments for the above referenced facility. The application was submitted on February 3, 2009 via EPSAP.

If you have any questions, please call me at (407) 298-2282 or e-mail me at sara@grovescientific.com.

Respectfully,
GROVE SCIENTIFIC & ENGINEERING COMPANY

A handwritten signature in black ink that reads "Sara Greivell".

Sara Greivell
Environmental Scientist

cc: Jim Gorsuch - Trend USA Ltd.
Polly Mandrell- E-Stone USA Corporation

E-Stone oper Sub to FDEP 09 / 330700 / 020409

Electronic Permit Submittal and Processing System (EPSAP) Professional Engineer Signature Document

"This document is signed and sealed to secure the data in this permit application and any attached files that were submitted electronically as described in Florida Department of Business and Professional Regulation, Board of Professional Engineers, Procedures for Signing and Sealing Electronically Transmitted Plan, Specifications, Reports or other Documents, Rule 61G15-23.003., F.A.C.."

EPSAP Application Number: 2165-1

Facility Identification Number: 0550049

Facility Owner/Company Name: E-STONE USA CORPORATION

Purpose of Application:

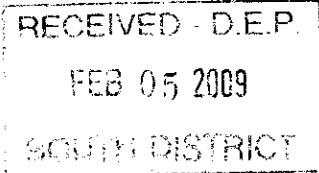
Initial Title V air operation permit.

Signature File Created: 2/3/2009 4:15:05 PM

| File Description | Authentication Code |
|--|--|
| Submitted Application Data | 6746B2F67470000A2CFBC09214E336E62B7AEC3F |
| This Application Has No Uploaded Facility Documents. | |
| This Application Has No Uploaded Emissions Unit Documents. | |
| Final Signature File | 3425D3AA888FE14DF754694BB026931A85BE42F2 |

Professional Engineer (PE): JAMES SHOW License No: 34361

(sign and affix PE seal below)




James T. Show
PE Signature

2/3/09
Date

Attachment A
Supplemental Information

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Supplemental Information

E-Stone USA Corporation

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Introduction:

E-Stone USA Corporation, located at 420 Haywood Taylor Blvd. in Sebring, FL, is applying for their 5-year operating permit. Under the construction permit number 0550049-003-AC, E-Stone has completed construction and stack testing for Polymerizing Line 1. Polymerizing Line 2 is not complete and will not be completed until product demands require it. E-Stone is requesting to leave this current construction permit open until construction on Line 2 is completed and stack testing is done. At that time E-Stone will apply for a permit modification to close out the open construction permit and incorporate Polymerizing Line 2 into the operating permit.

Process for Making Cultured Marble:

First, the granite rock and various aggregates are dried, then crushed and then screened. Next, the crushed aggregates are mixed with polyester resin inside a total enclosure. Depending on the product, various additives are mixed with the granite and resin mixture.

Inside the polymerizing stations, the mixture is poured into the open mold to form a slab. Then, the slab gets a thin layer of limestone on the bottom in order to strengthen the finished product. The entire polymerizing station is in a Permanent Total Enclosure (PTE). The PTE is equipped with a dust collection system to control the PM emissions from the limestone. The RTO controls a portion of the VOC and HAP emissions from the pouring stations and polymerizing oven. The oven operates on electricity; therefore, the oven has no fuel emissions. The RTO and rotary dryer operate on natural gas. The RTO has a manufacturer's guarantee of 98% destruction efficiency and tested at 99.04% in the December 2008 stack test.

After the mixture has set and cooled, it goes to one of two polishing lines. Polishing Line 1 uses a wet grinder to smooth the rough edges and polish the surface. If further touch-up is required then the slab goes to Polishing Line 2 that consists of an epoxy touch-up station, an oven and two dryers.

A process flow diagram is included in Attachment E.

Emission Calculations:

All of the materials listed on the attached spreadsheet are used inside the enclosure and are ultimately vented to two locations; the RTO and dust collector (DC3). The stack test results provided a measurement breakdown for the percentage of emissions vented to each location; 44.6% of the emissions are uncontrolled; vented to the dust collector;

55.4% of the emissions are vented to the RTO, which has a measured destruction efficiency of 99.04%. These emission data were then used to calculate the potential emissions, see Attachment H.

The emission factor for the resin was established in the stack test. The emission rate for styrene was 35.36 lbs of organic HAP (styrene) per ton of resin used.

The projected usage of each raw material other than resin was multiplied by the amount of organic HAP it contained, then multiplied by the 44.6% uncontrolled and 55.4% vented to the RTO with a 99.04% destruction efficiency.

The potential emissions before controls are included in Attachment I. Since the emissions are facility-wide and we do not have an actual measured emission rate for Polymerizing Line 2, the potential emissions before controls are calculated using the equation from Table 1 to 40 CFR Part 63 Subpart WWWW. It is expected that the emissions rate will be very closed to that of Line 1 however, we used the conservative calculated emission factor to calculate the potential emissions before controls until Line 2 is complete and tested.

A copy of the 2008 record keeping is included in Attachment G which shows the actual emissions.

List of Applicable Requirements:

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- This facility is subject to:
- 40 CFR Part 63, Subpart WWWW
 - 62-210.300(1) Air Construction Permits
 - 62-210.300(6) Emission Unit Reclassification
 - 62-210.350 Public Notice and Comment
 - 62-210.350(1) Public Notice of Proposed Agency Action
 - 62-210.350(3) Additional Public Notice Requirements for Source Subject to Operation Permits for Title V Source
 - 62-210.370(3) Annual Operating Report for Air Pollution Emitting Facility
 - 62-210.400 Emission Estimates
 - 62-210.650 Circumvention
 - 62-210.700 Excess Emissions
 - 62-213.205 Annual Emissions Fee
 - 62-213.400 Permits and Permit Revision Required
 - 62-213.900(1) Major Air Pollution Source Annual Emissions Fee Form
 - 62-296.320(4)(c) Unconfined Emissions of Particulate Matter
 - 62-296.320(2) Objectionable Odor Prohibited
 - 62-297.310 General Test Requirements
 - 62-297.330 Applicable Test Requirements
 - 62-297.340 Frequency of Compliance Tests
 - 62-297.345 Stack Sampling Provided by the Owner of an Emissions Unit

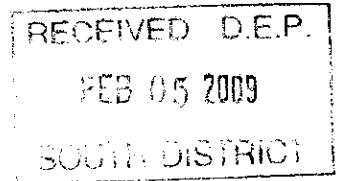
62-297.570 Test Report

Exempt Emissions Units:

Exempt emission unit include compressors and emergency generators. Attachment D contains the list of insignificant activities at this facility.

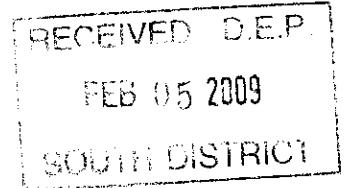
Requested Changes to Operating Permit:

Page 10 of 19, Specific Condition B.2 in the current construction permit states the Gas Exhaust Temperature shall be 70-100 ° F. This condition should not be included in the operating permit, is incorrect and has no bearing on the emissions.

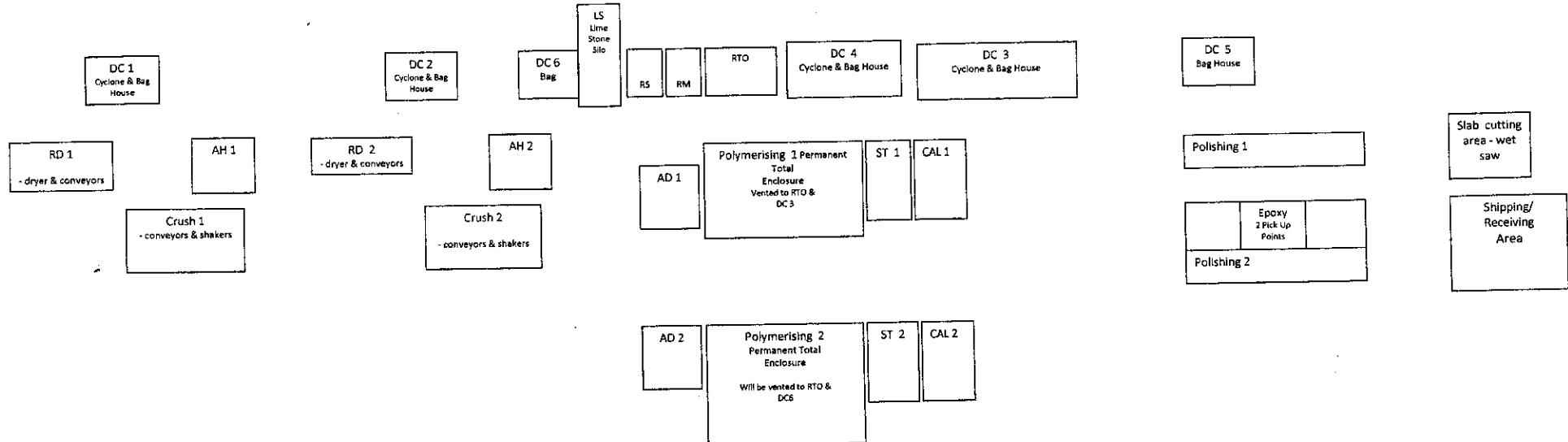


Attachment B

Plot Plan



E-Stone USA Corporation
Process Layout
Revised 1-23-08



| Process Equipment List | | | |
|--------------------------|-----------------------|--------------------------|-----------------------|
| Equipment Identification | Equipment Description | Equipment Identification | Equipment Description |
| AH1 | Aggregate Hopper #1 | AD 1 | Aggregate Dosing 1 |
| RD1 | Rotary Dryer #1 | Polymerising 1 | Polymerising 1 |
| Crush 1 | Mill #1 | | |
| AH2 | Aggregate Hopper #2 | CAL 1 | Calibrator 1 |
| RD2 | Rotary Dryer #2 | Polymerising 1 | Polymerising 1 |
| Crush 2 | Mill #2 | | |
| AD2 | Aggregate Dosing #1 | | |
| Polymerising 2 | Polymerising 2 | Polymerising 2 | Polymerising 2 |
| ST 2 | Slab Take Off Area | Polishing 2 | Polishing 2 |
| CAL 2 | Calibrator 2 | Polishing 2 | Polishing 2 |
| LS | Limestone Silo | Epoxy | Epoxy Touch Up |
| ST 1 | Slab Take Off Area | RS | Resin Storage |
| | | RM | Resin Mix Tanks |

| Control Device List | | |
|--------------------------|-------------------------------|--|
| Equipment Identification | Equipment Description | Controls Emissions From |
| DC1 | Cyclone & baghouse | Mill #1 |
| DC2 | Cyclone & baghouse | Mill #2 |
| DC6 | Baghouse | Polymerising 2 |
| RTO | Regenerative Thermal Oxidizer | Polymerising 1 |
| DC4 | Cyclone & baghouse | ST 2 & CAL 2 |
| DC3 | Cyclone & baghouse | LS, ST 1, AD 1, CAL 1, Polymerizing Line 1 |
| DC5 | Baghouse | Epoxy & Polishing Line 2 |

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Attachment C
Compliance Report

| |
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January 14, 2009



Mr. Ajaya Satyal
District Air Program Administrator
FDEP - South District
2295 Victoria Avenue, Suite 364
Fort Myers, Florida 33902-2549

**RE: E-Stone USA Corporation
FDEP Permit No 0550049-003-AC
Test Report Transmittal**

Dear Mr Satyal,

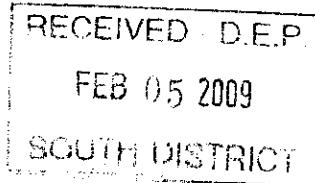
Grove Scientific & Engineering Company has completed the compliance test report for E-Stone. Attached is a paper copy for your files. An electronic version has been also emailed to you.

If you have any questions regarding this test report, please call me at 407-298-2282 or email bruno@grovescientific.com.

Sincerely
Grove Scientific & Engineering Company


Bruno Ferraro, CEP, QEP
President

cc: James Gorsuch, CFO
Polly Mandrell, E-Stone



**EMISSION TEST REPORT
FOR A CULTURED GRANITE MANUFACTURING PROCESS -
LINE NO. 1**

**40 CFR PART 63 SUBPART WWWWW
NATIONAL EMISSION STANDARDS FOR HAZARDOUS AIR
POLLUTANTS: REINFORCED PLASTICS COMPOSITES
PRODUCTION**

Prepared for

**E-Stone USA Corporation
420 Haywood Taylor Boulevard
Sebring, Florida 33870**

Prepared by

**Grove Scientific & Engineering Company
6140 Edgewater Drive, Suite F
Orlando, Florida 32810
(407) 298-2282
www.grovescientific.com**

December 2008

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FEB 05 2009

SOUTH DISTRICT

Project Number 330700

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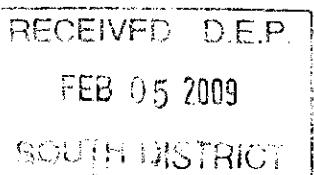


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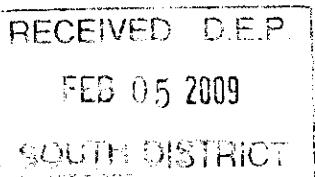


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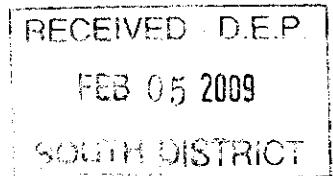
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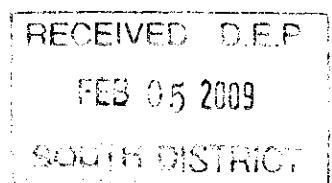


Report Certification

This test was conducted under my supervision and in accordance with the approved test protocol submitted to the Florida Department of Environmental Protection. All data submitted are true and correct and meet the requirements of the permit and test methods.

Bruno A. Ferraro, CEP, QEP

Date



SECTION 1.0

INTRODUCTION

1.1 Background

E-Stone USA, located at 420 Haywood Taylor Boulevard, Sebring, Florida 33870, is authorized by FDEP construction permit 0550049-003-AC to construct a cultured granite reinforced plastics manufacturing facility with a permanent total enclosure around the polymerization line(s). This test addresses production line number 1 and its associated dust collector and regenerative thermal oxidizer. The following emission units were tested and are included in this report:

| E.U. No. | Emission Unit Description |
|----------|--|
| 001 | Non-metallic mineral processing line no. 1 |
| 002 | Non-metallic mineral processing line no. 2 |
| 003 | Polymerization line 1 |
| 005 | Regenerative thermal oxidizer (RTO) |
| 007 | Polishing line no. 2 |

Polymerization line number 2 has not completed construction and has been placed on hold until production demands increase.

1.2 Test Protocol

Two locations will be monitored for VOC emissions; the outlet of the RTO and the outlet of the baghouse using EPA Methods 1-4, 9 and 25A. Preliminary test conducted in December 2006 indicated a styrene concentration of less than 25 ppm

as styrene from the RTO outlet (2.74 ppm) and the baghouse outlet (14.02 ppm). This makes EPA Method 25A the preferred test method for determining styrene emissions. Also, since styrene is the only volatile organic compound (VOC) and organic hazardous air pollutant (HAP) in the resin used at E-Stone a response factor for styrene will be developed for each analyzer used during this test. We will also test the inlet of the RTO so that we can determine VOC destruction efficiency of the RTO.

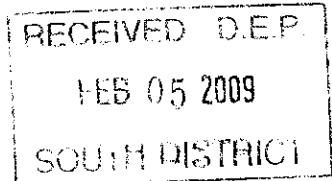
1.2.1 40 CFR Part 63 Subpart SS Requirements

Air permit 0550049-002-AC and Subpart WWWW NESHAP references Subpart SS as required for testing the VOC control device. Subpart SS defines the RTO as an “incinerator”, therefore §63.988, §63.997, §63.998(a)(2) and §63.999(a)(2) apply. Each of the regulations that pertain to this test protocol are addressed below:

§63.988(c) requires a temperature monitoring device be installed in the combustion zone of the RTO. The RTO is equipped with a continuous temperature recorder as per §63.988(c)(1) and will be monitored during the compliance test per §63.998(b) and (c). During the compliance test, the minimum RTO operating temperature will be established as well as the continuous combustion chamber temperature recorded.

1.2.2 §63.997 Performance test and compliance assessment requirements for control devices

(c)(i) requires the test be performed within 180 days of start up. Since E-Stone has elected to not complete construction on Line 2 at this time, E-Stone is preparing for testing of Line 1 only by preparing and submitting this test protocol. Once the test protocol has been approved and all relevant details agreed to, the test will be scheduled with the FDEP South District Office.



(d)(1) requires sampling ports be installed adequate for test methods applicable to the source. Sampling ports have been installed and meet USEPA Method 1.

(d)(1)(i) require the air pollution control systems to be constructed such that volumetric flow rates and pollutant emission rates can be accurately determined by applicable test methods and procedures. Sampling ports have been installed and meet USEPA Method 1.

(d)(1)(ii) requires ducts and stacks free of cyclonic flow during performance test. Sampling ports have been installed and meet USEPA Method 1. Preliminary testing indicates the stacks are free of cyclonic flow.

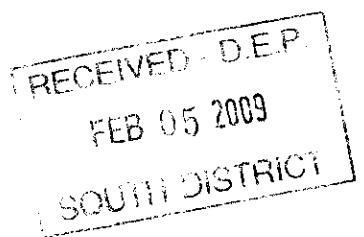
(2) requires safe sampling platform(s); (3) requires safe access to sampling platform(s); (4) requires utilities for sampling and sampling equipment. The RTO and dust collector has safe testing platform(s), OSHA compliant caged ladders and utilities for conducting a safe compliance test.

(e) (1) requires the performance test on a continuous unit operation be tested at the maximum rate. The maximum production rate for Line 1 is 13 slabs/hour and will be the target production rate during the test ($\pm 10\%$).

(v) requires a minimum test run of at least 1 hour and three separate runs conducted. The arithmetic mean of the three runs shall apply.

(e)(2)(i) through (iv) apply and reference test methods and reporting procedures as follows:

(i) requires the use of USEPA Method 1 for the selection of sampling sites. Each of the sample locations has been installed in accordance with Method 1.



(i)(A)(1) requires the inlet of the RTO to be tested and located downstream of the process but before the control device. E-Stone meets this requirement

(ii) requires volumetric flowrate to be determined by USEPA Methods 2, 2A, 2C, 2D, 2F or 2G as appropriate and E-Stone will comply with this requirement.

(iii) requires the use of USEPA Method 18 or 25A as applicable to measure the total organic compound concentration. Since styrene is the only expected VOC and HAP at concentrations less than 50 ppm, we selected USEPA Method 25A as the appropriate test method. We will also determine the styrene response factor for each analyzer so that the data can be reported in pounds per hour "as styrene".

(iii)(A) requires a minimum sampling time of 1 hour per test run.

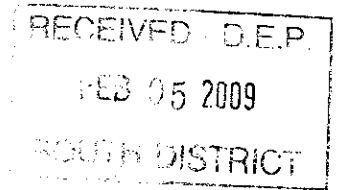
(iii)(B) dictates how the pollutant concentration will be calculated and the test report will comply with this requirement.

(iii)(C) requires the final organic concentration be corrected to 3% oxygen if combustion air is used to combust the emissions.

(iii)(D) In this application the total organic regulated material is equal to the TOC and are proposing to measure all of the TOC and report it as styrene therefore we elect to test using the more accurate test method 25A (see item (iii)(E) below).

(iii)(E) TOC concentration will be measured in accordance with USEPA Method 25A using a response factor for styrene. All TOC will be reported in pounds/hr "as styrene".

(iv) Percent reduction calculation: Subpart WWWW does not require a specific



destruction efficiency or VOC reduction requirement. However, as part of this test, we will measure both inlet and outlet mass emissions and will calculate an overall VOC destruction efficiency and include this in the test report.

(iv)(A) requires a minimum sampling time of 1 hour per run.

(iv)(B) provides the method to calculate the mass rate of TOC or total organic regulated material. As stated above, the TOC will be reported as styrene using the instrument response factor established as part of this test. Since styrene is the only VOC and the only organic HAP used in the resin all of the TOC will be styrene and will be calculated in accordance with this section.

(iv)(C) Percent reduction, though not required in Subpart WWWW for sources under 100 TPY of organic HAP, will be determined and calculated in accordance with this section.

(iv)(D) does not apply as the vent stream is not introduced with the combustion air.

(iv)(E) applies only to transfer racks, therefore, does not apply.

(iv)(F) see item (iii)(D) and (iii)(E) above.

(iv)(G) see item (iv)(H) below

(iv)(H)(1) and (2) specify the use of Method 25A in lieu of Method 25 when the expected concentrations are below 50 ppm as TNMO. During previous engineering tests, we measured the outlet of the RTO at 2.74 ppm as styrene and the dust collect at 22.53 ppm as styrene. The inlet to the RTO was measured at 208.71 ppm as styrene with a high control efficiency measured on the RTO (98.54%), therefore per

section (iv)(H)(2) the inlet can be measured using Method 25A.

(iv)(I) does not apply since the inlet gas does not contain formaldehyde.

1.2.3 §63.998 Recordkeeping Requirements

(a)(2) Non-flare control device performance test records requires the owner record and maintain performance test records and make them available upon request.

(a)(2)(ii)(A) requires the owner record and maintain performance test records and make them available upon request.

(a)(2)(ii)(B)(1) requires the RTO combustion chamber temperature to be recorded during the test. The RTO is equipped with a thermal couple and data logger that continuously records this parameter.

(2) and (3) do not apply.

(a)(2)(ii)(B)(4) E-Stone is not required to determine the reduction efficiency of the RTO, only the mass emission rate from both the RTO and the dust collector. However, as previously stated, we will determine reduction efficiency in accordance with the subpart and use it for ongoing record keeping.

(5) and (6) do not apply.

(a)(2)(ii)(C) and (D) do not apply

(a)(3)and (4) do not apply.

| | |
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| GAS/11 DISTRICT | |

§63.998(b)(1) requires continuous records of the measurement device, in this case, the RTO combustion chamber temperature. Records will be collected and maintained in accordance with (b)(1)(iii) from the continuous recording device.

(b)(2)(i) through (iii) excludes temperature data from startup, shutdown and malfunctions from the data averages.

(b)(3)(b)(ii) addresses daily average temperatures when all recorded temperatures are within the acceptable range established during the compliance test. In this case, the RTO maintains a very steady temperature at or above the minimum set point except during startup, shutdown and malfunction.

(b)(5) we are not requesting an alternate recordkeeping procedure.

(b)(6)(i) addresses excursions of the RTO temperature values and applies to long-term recordkeeping, not specific to this test protocol.

(b)(6)(ii) addresses additional recordkeeping requirements for the continuous temperature monitor of the RTO and are not specific to the actual compliance test.

§63.998(c)(1)(i) the continuous temperature recorder will be calibrated prior to the test and a record of the calibration procedure and results retained. Also, (c)(1)(ii)(A) through (H) are specific to the calibration procedure and records that will be maintained on the continuous temperature monitoring system and not specific to the test protocol. These procedures will be followed and the records submitted with the test report.

(c)(2)(ii) addresses the RTO temperature records in (b)(3)(i) above and will be maintained. Additionally, (c)(2)(iii) requires E-Stone to maintain up-to-date records

of the continuous temperature monitoring system.

(c)(3) does not apply to E-Stone.

§63.998(d)(1) does not apply to this test protocol.

(2) through (5) does not apply to this test protocol.

1.2.4 §63.999 Notification and Other Reports

(a)(1)(i) requires E-Stone to give as least 30 days notice before conducting the compliance test. Following approval of the test protocol, E-Stone will schedule the test with FDEP and provide at least 30 day notice as required or select a date mutually agreeable to both E-Stone and FDEP.

(ii) requires E-Stone to submit the compliance test report within 60 days of completion of the test.

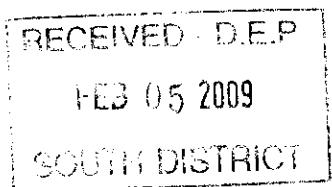
(iii) pertains to a waiver of the compliance test which E-Stone is not requesting.

(iv) does not apply

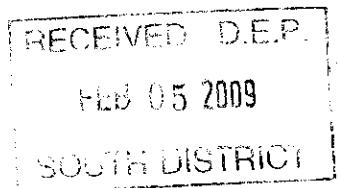
(a)(2)(i) through (iii) E-Stone will submit a complete copy of the test report with all required components and records as required by this sub-section.

1.2.5 Summary

The following summarizes the proposed test protocol for polymerization line 1.



1. Demonstrate that the enclosure on polymerization line 1 meets the requirements of EPA Method 204 procedure T for 100% capture.
2. Sample the inlet and outlet of the RTO to determine overall VOC destruction efficiency and the outlet of the Zanetti dust collector using EPA methods 1-4, 9 (on outlets only) and 25A for three one-hour test runs. Visible emissions will be conducted for 1 hour only.
3. Determine the response factor of each flame ionization analyzer to styrene, the only VOC and HAP; measure total organic compounds of the RTO and Zanetti exhaust stacks using 25A and report the results in lbs/hr "as styrene". The combined results will equal the mass emission rate of styrene.
4. Establish the minimum RTO combustion chamber operating temperature using the continuous temperature recorder in accordance with 40 CFR part 63 Subpart SS including calibration determinations and records as required by the subpart.
5. Establish and record the minimum airflow rates through the RTO and the Zanetti dust collector using the magnahelic and record this data.
6. Establish and record the differential pressure on the enclosure's differential pressure gauge as required by Specific Condition B.4 and report this data.
7. Prepare a test report that complies with the reporting requirements of subpart SS and submit this report within 60 days of completing the compliance test.



SECTION 2.0

VISIBLE EMISSIONS TESTS E.U. 001, 002, 003 and 007

2.1 Description E.U. 001 and 002

Emission Units 001 and 002 are the non-metallic mineral processing lines 1 and 2 respectfully. Each line is essentially identical and are equipped with gas-fired rotary dryers, conveyors, hoppers, shakers and a crusher. Each line is equipped with a cyclone and baghouse to control particulate emissions. During the visible emission test process throughput was measured using the internal weigh hoppers; fuel was measured using the in-line fuel meters with a meter correction factor applied.

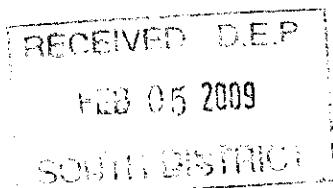
2.1.2 Test Data E.U. 001 and 002

Table 2-1 presents the fuel consumption and process rate measured during the emission test.

Table 2-1: Summary of Fuel Consumption Rate and Process Rate of Rotary Dryers 1 and 2

| E.U No | Description | Fuel CF/hr | Process rate TPH |
|--------|-------------|------------|------------------|
| 001 | Line 1 | 620 | 2.77 |
| 002 | Line 2 | 610 | 3.58 |

Visible emissions were 0% opacity. Field data sheets for E.U. 001 and 002 and visible emissions results are included in Attachment A along with the observer's certification.



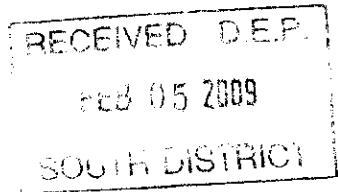
2.2 Emission Unit 003 Dust Collector

Emission Unit 003 includes the Zanetti cyclone and baghouse (DC3) used to control particulate emissions from polymerization line-1 enclosure. A visible emission test on the outlet of this dust collector was conducted during run 3 of the stack test. Visible emissions were 0% opacity. Field data sheets for DC3 are included in Attachment A along with the observer's certification documentation.

Specific Condition B.3 of the permit and 40 CFR part 63 Subpart SS requires the use of a magnehelic pressure gauge to be installed in the outlet stack of DC3 and to establish operating parameters during the initial performance test that demonstrates compliance with the standards. This gauge was installed and read during the test to establish this baseline. The field data sheets are included in Attachment B and summarized below in Table 2-2. The magnehelics read in both inches of w.c. (in.w.c.)and feet per min (fpm) and both were recorded during each of the 3 runs and did not fluctuate.

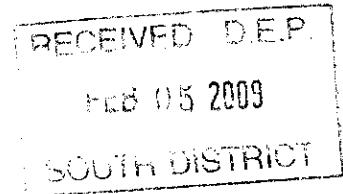
Table 2-2: Summary of Parametric Data DC3

| Run Number | 1 | 2 | 3 |
|---------------------|------|------|------|
| Pressure (in. w.c.) | +0.4 | +0.4 | +0.4 |
| Airspeed (fpm) | 2400 | 2400 | 2400 |



2.3 Emissions Unit 007 Dust Collector

Emission Unit 007 includes a Zanetti baghouse. During the test, the line was actively polishing a slab. Visible emissions were 0% opacity. Field data sheets are included in Attachment A along with the observer's certification documentation.



SECTION 3.0

POLYMERIZATION LINE 1 E.U. 003

3.1 Description

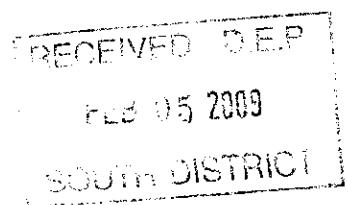
Emission Unit 003 is polymerization line 1. Associated with this polymerization line is the Zanetti dust collector described in Section 2 of this report, the regenerative thermal oxidizer (EU 005), the enclosure around the process and the associated mixing and storage tanks. The enclosure is a permanent total enclosure (PTE) and must meet the requirements of 40 CFR part 52 EPA Method 204 - Procedure T. This was verified prior to this test and the results discussed below. During this stack test, the enclosures was tested again to verify the PTE parameters. The test data for the PTE verification is included in Attachment C.

3.2 Permanent Total Enclosure (PTE) Criteria

Procedure T establishes the criteria for verifying a permanent total enclosure (PTE). The principle behind the procedure is presented below and quoted form the USEPA method .

An enclosure is evaluated against a set of criteria. If the criteria are met and if all the exhaust gases are ducted to a control device, the volatile organic compounds capture efficiency (CE) is assumed to be 100% and CE need not be measured. However, if part of the exhaust gas stream is not ducted to a control device, CE must be determined.

A summary of the design criteria follows:



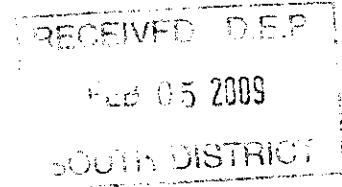
1. Any natural draft opening (NDO) shall be at least 4 equivalent opening diameters from each VOC emitting point unless otherwise specified by the Administrator.
2. The total area of all NDOs shall not exceed 5% of the surface area of the enclosure's four walls, floor, and ceiling.
3. The average facial velocity of air through all NDOs shall be at least 200 feet per minute. The direction of air through the NDOs shall be into the enclosure.
4. All access doors and windows whose areas are not included in item 2 and are not included in the calculation in item 3 shall be closed during routine operation of the process.
5. All VOC emissions must be captured and contained for discharge through a control device.

3.2.1 Results of Procedure T

There are two (2) natural draft openings in polymerization line 1 enclosure; the dosing conveyor entrance and the slab discharge exit. The results of Procedure T are included in Table 3-1 below.

Emissions from the enclosure are vented to two control devices. One is the regenerative thermal oxidizer which controls VOC and HAP. The second is a cyclone-baghouse dust collector that control particulate matter from the process and is not a VOC control device.

The enclosure for polymerization line 1 meets all of the criteria of a PTE in accordance with Procedure T, when the RTO vacuum set point is 0.6 inches w.c or greater. During the stack test data were collected of airflow into the enclosure using a digital manometer, air current smoke tubes and the differential pressure



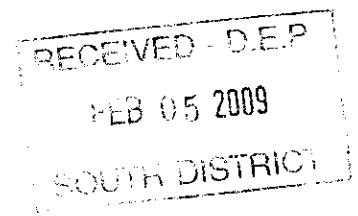
gauges located in the upper and lower portions of the enclosure. All airflows were greater than -200 fpm through the NDO's. The lower differential pressure gauge (no. 1) read -0.005 inches w.c., the upper (no. 2) read -0.02 to -0.04. These data sheets are included in Attachment C and summarized in Table 3-2.

Table 3-1: Results of Procedure-T on Polymerization Line 1

| Criteria | Dosing Conveyor Entrance NDO | Slab Discharge Exit NDO |
|--|--|--|
| Criteria 1: NDO > 4 Equivalent Diameters (> 4 = Pass) | > 30 diameters (pass) | > 7 diameters (pass) |
| Criteria 2: Total Area of NDOs Not More Than 5% of Surface Area (<= 5% = Pass) | < 0.28 % (pass) | < 0.28 % (pass) |
| Criterion 3a: Average Facial Velocity At Least 200 Feet Per Minute (>= 200 fpm = Pass) | - 285 fpm (pass) at -0.6 in. W.C. RTO set point | - 225 fpm (pass) at -0.6 in. W.C. RTO set point |
| Criterion 3b: Direction of Air Shall Be Into Enclosure (Results of Smoke Test) | Inward airflow verified | Inward airflow verified |
| Criterion 4: Access Doors / Windows To Be Closed When Not In Use Status During Operation | all doors and access areas closed during operation | all doors and access areas closed during operation |
| Criterion 5 VOC Emissions To Routed to Control Device | RTO and Dust Collector | RTO and Dust Collector |

Table 3-2: Summary of Enclosure Air Pressure Data with RTO Vacuum Set
Point is Set At -0.6 inches water column (in w.c.)

| Run No | 1 | 2 | 3 |
|-------------------------------------|--------|--------|--------|
| Magnehelic 1 (in w.c.) | -0.005 | -0.005 | -0.005 |
| Magnehelic 2 (in w.c.) | -.002 | -0.035 | -0.04 |
| NDO Inlet (fpm) | -365 | -355 | -319 |
| NDO Outlet (fpm) | -204 | -214 | -220 |
| Air Current Tubes Direction of flow | inward | inward | inward |



SECTION 4.0

REGENERATIVE THERMAL OXIDIZER (E.U.005)

4.1 Description

The VOC/organic HAP control device is a Crawford Industrial Group Regenerative Thermal Oxidizer (RTO) equipped with a variable frequency drive motor. The RTO is computer controlled and can be programmed to operate at different vacuums. The RTO vacuum controls the negative pressure inside the polymerization line enclosure. The PTE demonstrated compliance during this test with the RTO vacuum set point at -0.6 in.w.c. and placed all NDO's under a negative flow greater than 200 fpm.

4.2 Parametric Monitoring

During the compliance test, several parameters were monitored as required by either a permit condition or by Subpart SS as presented in Section 1.2 of this report. Each of those parameters are presented below and the field data sheet and the RTO temperature chart are included in Attachment D.

4.2.1 Fuel consumption

Fuel consumption was determined by reading the in-line gas meter dedicated to the RTO. The data are presented in Table 4-1.

Table 4-1: RTO Fuel Consumption Data

| Start Time | Stop Time | Start Reading | Stop Reading | Total Fuel Consumption | |
|------------|-----------|---------------|--------------|------------------------|-----------|
| 0920 hrs | 1505 hrs | 181500 cf | 184400 cf | 2900 cf | 504 cf/hr |

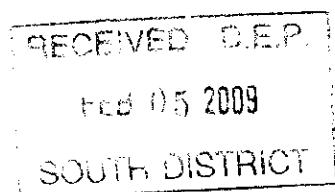
4.2.2 RTO Parametric Data

The RTO parametric data are presented below in Table 4-2

Table 4-2: RTO Parametric Data

| Run Number | 1 | 2 | 3 |
|--------------------------------------|-------|-------|-------|
| Inlet Magnehelic Pressure (in.w.c.) | 0.175 | 0.175 | 0.175 |
| Inlet Magnehelic Flowrate (fpm) | 1800 | 1800 | 1800 |
| Outlet Magnehelic pressure (in.w.c.) | 0.25 | 0.25 | 0.25 |
| Outlet Magnehelic Flowrate (FPM) | 2000 | 2000 | 2000 |
| Stack Temperature (deg F) | 235 | 235 | 235 |
| Combustion Chamber Temp (deg F) | 1577 | 1577 | 1577 |
| Inlet vacuum set point (in.w.c.) | -0.6 | -0.6 | -0.6 |

All parameters remain constant through out all three runs.



SECTION 5.0

PRODUCTION DATA AND MASS ORGANIC HAP EMISSION RESULTS

5.1 Production Monitoring System

The robotic manufacturing process at E-Stone is computer controlled and monitored. The operator can select any time sequence and obtain real-time raw material consumption rate and production rate. The computer generated report and the AOC Resins MSDS are included in Attachment E.

The report includes the time between 09:12:25 hours to 15:04:52 hours for a total of 292 minutes during which 78 slabs were produced. This equates to 16 slabs/hr of production. A total of 1674.901 lbs of AOC polyester resin was used in 292 minutes or 344.158 lbs/hr. The resin is a 50/50 mixture of two AOC resins; A520-PKC-00 which is 35% styrene and A520-PKE-00 which is 35% styrene. A small amount of styrene is added to the batch as a diluent for the micro-additive Tinuvin. A summary of the raw material usage is presented below in Table 5-1.

Table 5-1: Summary of Raw Material Usage

| Raw Material | Total Pounds used in 78 Slabs | Usage Rate (lbs/hr) |
|--------------------------|-------------------------------|---------------------|
| Limestone Rock (backing) | 5850.000 | 1202.055 |
| Decorative Aggregate | 9069.984 | 1863.695 |
| Catalyst (Norox 90 cc) | 16.741 | 3.440 |
| Styrene | 4.68 | 0.96 |
| Polyester Resin | 1674.901 | 344.158 |

5.2 Emission Summary

The stack test report is included in its entirety in Attachment F. Three locations were tested for styrene using EPA Method 25A applying a measured response factor to styrene, the only organic HAP. The three locations tested were the inlet and outlet of the RTO and the dust collector outlet (DC3). The mass emissions are based on the combined emission rate of the RTO outlet and the DC3 outlet. The inlet of the RTO was measured to determine overall RTO destruction efficiency for in-house purposes only. The results of the destruction efficiency are summarized below in Table 5-2.

Table 5-2: Summary of RTO Destruction Efficiency

| Run No. | RTO Inlet (lbs/hr as styrene) | RTO Outlet (lbs/hr as styrene) | Destruction Efficiency (%) |
|---------|-------------------------------|--------------------------------|----------------------------|
| 1 | 7.48 | 0.06 | 99.17 |
| 2 | 7.74 | 0.06 | 99.21 |
| 3 | 7.22 | 0.09 | 98.76 |
| Average | 7.48 | 0.07 | 99.04 |

The results of the mass styrene (HAP) emissions are presented below in Table 5-3.

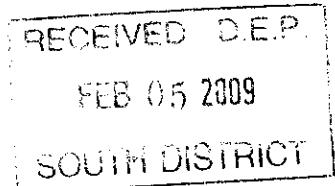


Table 5-3: Summary of Mass Styrene (HAP) Emissions

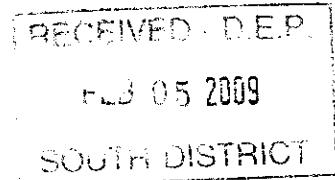
| Run No. | RTO Outlet (lbs/hr as styrene) | DC3 Outlet (lbs/hr as styrene) | Total Organic HAP Mass Emission Rate (lbs/hr as styrene) |
|---------|-----------------------------------|-----------------------------------|---|
| 1 | 0.06 | 5.39 | 5.45 |
| 2 | 0.06 | 6.60 | 6.66 |
| 3 | 0.09 | 6.12 | 6.21 |
| Average | 0.07 | 6.03 | 6.10 |

5.3 Compliance with HAP Emission Limit

In accordance with Specific Condition B.12 of the referenced construction permit, this open molding - non-CR/HS polymerization process is required to meet the organic HAP emission limit referenced in 40 Part 63 Subpart WWWWW Table 3, item 2, of 88 pounds of organic HAP per ton of resin. As presented in Table 5-1, the hourly resin usage during the test was 344.158 lbs plus 0.96 lbs of additional styrene or 0.1725 tons/hr. Styrene is the only organic HAP in this product.

The emission limit is calculated as follows:

$$(6.10 \text{ lbs organic HAP}) / (0.1725 \text{ tons of resin}) = 35.36 \text{ lbs organic HAP/ton of resin.}$$



ATTACHMENT A

**E.U 001, 002 AND 007 FIELD DATA SHEETS, VISIBLE
EMISSION RESULTS AND CERTIFICATION**

RECEIVED D.E.P.
FEB 05 2009
SOUTH DISTRICT



E-Stone Rotary Drier Process Data Sheet

Test Date 12-11-08

GSE Employee Name Sara Grinell

Drier Number 1 EU001

Time Start (fuel) 09:56

Time Start (aggregate) 10:00

Fuel Meter Reading at Start 0247

Time End (fuel) 11:25

Time end (aggregate) 11:22 (crushed granite into drier)

Fuel Meter Reading at End 0254

Total Time in Minutes (fuel) = 65 minutes (aggregate) = 22 minutes

Total Fuel Used 881 CF or 620 CF/h

Total Quantity of Aggregate Processed 7566 lbs

Method of Determining Process Rate put dried material into empty bin at weigh at end

Comments METER reading correction factor = 1.27 X 100

VISIBLE EMISSIONS OBSERVATION FORM

| | | |
|-------------------|----|-----|
| COMPLIANCE STATUS | | |
| YES | NO | UNK |

| Source/Process Information | | Observation Readings | | | | | | | | | | | | |
|---|---|--------------------------------|---|------------|------------|------|------------|--|--|--|--|--|--|--|
| Facility Name | Source Name | Permit No. | EPA Method | Start Time | Stop Time | | | | | | | | | |
| 1. Stone USA Corporation | Rotary Dryer #1 | DEP0049-003-A | 9 | 10:08 | 10:38 | | | | | | | | | |
| Location Address | 420 Thawood Taylor Blvd, Sebring Rd | 1 | 0 0 0 0 | Sec. | 0 15 30 45 | Min. | 0 15 30 45 | | | | | | | |
| Contact | Bob Hyres | 2 | 0 0 0 0 | Sec. | 0 15 30 45 | Min. | 0 15 30 45 | | | | | | | |
| Process/Production Rate | aggregate drying | 3 | 0 0 0 0 | Sec. | 0 15 30 45 | Min. | 0 15 30 45 | | | | | | | |
| Control Equipment | cyclone dust collector, dc | 4 | 0 0 0 0 | Sec. | 0 15 30 45 | Min. | 0 15 30 45 | | | | | | | |
| Fuel Type/Rate | natural gas 2.77/hr | 5 | 0 0 0 0 | Sec. | 0 15 30 45 | Min. | 0 15 30 45 | | | | | | | |
| Describe Emission Point | round metal stack | 6 | 0 0 0 0 | Sec. | 0 15 30 45 | Min. | 0 15 30 45 | | | | | | | |
| Height Above Ground Level | ~30 ft | 7 | 0 0 0 0 | Sec. | 0 15 30 45 | Min. | 0 15 30 45 | | | | | | | |
| | | 8 | 0 0 0 0 | Sec. | 0 15 30 45 | Min. | 0 15 30 45 | | | | | | | |
| Emissions Description | | | | | | | | | | | | | | |
| Describe Emissions | Start none visible End same | 9 | 0 0 0 0 | Sec. | 0 15 30 45 | Min. | 0 15 30 45 | | | | | | | |
| Plume Color | N/A | 10 | 0 0 0 0 | Sec. | 0 15 30 45 | Min. | 0 15 30 45 | | | | | | | |
| Water Droplets Present | If yes, is plume Attached [] N/A Detached [] | 11 | 0 0 0 0 | Sec. | 0 15 30 45 | Min. | 0 15 30 45 | | | | | | | |
| | | 12 | 0 0 0 0 | Sec. | 0 15 30 45 | Min. | 0 15 30 45 | | | | | | | |
| Meteorological Information | | | | | | | | | | | | | | |
| Background Start SKY End same | Background Color Start blue/white End white | 13 | 0 0 0 0 | Sec. | 0 15 30 45 | Min. | 0 15 30 45 | | | | | | | |
| Sky Conditions % Cloud Cover Start 0% End 35% | Ambient Temp Start 70°F End 77°F | 14 | 0 0 0 0 | Sec. | 0 15 30 45 | Min. | 0 15 30 45 | | | | | | | |
| Wind Speed Start 1 mph End same | Wind Direction Start SE End SE | 15 | 0 0 0 0 | Sec. | 0 15 30 45 | Min. | 0 15 30 45 | | | | | | | |
| Observation Data, Site Diagram | | | | | | | | | | | | | | |
| Stack with Plume | | 16 | 0 0 0 0 | Sec. | 0 15 30 45 | Min. | 0 15 30 45 | | | | | | | |
| Sun | | 17 | 0 0 0 0 | Sec. | 0 15 30 45 | Min. | 0 15 30 45 | | | | | | | |
| Wind | | 18 | 0 0 0 0 | Sec. | 0 15 30 45 | Min. | 0 15 30 45 | | | | | | | |
| | | 19 | 0 0 0 0 | Sec. | 0 15 30 45 | Min. | 0 15 30 45 | | | | | | | |
| | | 20 | 0 0 0 0 | Sec. | 0 15 30 45 | Min. | 0 15 30 45 | | | | | | | |
| | | 21 | 0 0 0 0 | Sec. | 0 15 30 45 | Min. | 0 15 30 45 | | | | | | | |
| | | 22 | 0 0 0 0 | Sec. | 0 15 30 45 | Min. | 0 15 30 45 | | | | | | | |
| | | 23 | 0 0 0 0 | Sec. | 0 15 30 45 | Min. | 0 15 30 45 | | | | | | | |
| | | 24 | 0 0 0 0 | Sec. | 0 15 30 45 | Min. | 0 15 30 45 | | | | | | | |
| | | 25 | 0 0 0 0 | Sec. | 0 15 30 45 | Min. | 0 15 30 45 | | | | | | | |
| | | 26 | 0 0 0 0 | Sec. | 0 15 30 45 | Min. | 0 15 30 45 | | | | | | | |
| | | 27 | 0 0 0 0 | Sec. | 0 15 30 45 | Min. | 0 15 30 45 | | | | | | | |
| | | 28 | 0 0 0 0 | Sec. | 0 15 30 45 | Min. | 0 15 30 45 | | | | | | | |
| | | 29 | 0 0 0 0 | Sec. | 0 15 30 45 | Min. | 0 15 30 45 | | | | | | | |
| | | 30 | 0 0 0 0 | Sec. | 0 15 30 45 | Min. | 0 15 30 45 | | | | | | | |
| Compliance Information | | Certification Data, Signatures | | | | | | | | | | | | |
| Range of Opacity Readings | Min 0 | Max 0 | Observer's Name: <u>Jara Greivell</u> | | | | | | | | | | | |
| Average of Highest 24 Consecutive Readings | 0 | 0 | Observer's Signature: <u>Jara Greivell</u> Date: <u>12-9-08</u> | | | | | | | | | | | |
| Short Term Average Data | 3 minutes | Actual Average 0 | Organization: <u>Grove Scientific & Engineering Co.</u> | | | | | | | | | | | |
| Averaging Period | | | Certified By: <u>Aeromet Engineering</u> Date: <u>4/10/08</u> | | | | | | | | | | | |
| Comments | I have received a copy of these observations Signature: _____ Date: _____ | | | | | | | | | | | | | |
| APLS Number: | | | | | | | | | | | | | | |

No objectional odors detected



E-Stone Rotary Drier Process Data Sheet

Test Date 12-4-08

GSE Employee Name Sara Gravelle

Drier Number 2 EU002

Time Start (fuel) 10:43

Start time (aggregate) 10:47

Fuel Meter Reading at Start 0165

Time End (fuel) 11:58

Time end (aggregate) 11:47

Fuel Meter Reading at End 0171

Total Time in Minutes fuel = 75 minutes (aggregate = 60 minutes)

Total Fuel Used 762 CF 610 CF/hr

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FEB 05 2009

Total Quantity of Aggregate Processed 7150 lbs

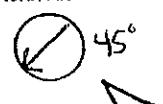
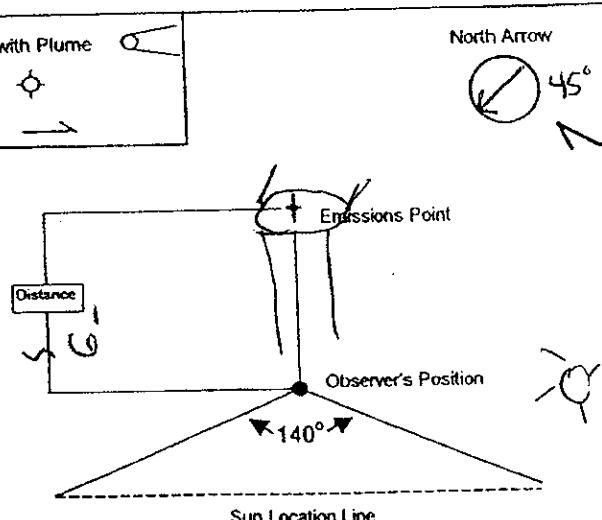
SOUTH DISTRICT

Method of Determining Process Rate put dried material into
empty bin & weigh at end

Comments meter reading correction factor = 1.27 x 100
kg/ft³

VISIBLE EMISSIONS OBSERVATION FORM

| | | |
|-------------------|----|-----|
| COMPLIANCE STATUS | | |
| YES | NO | UNK |

| Source/Process Information | | Observation Readings | | | | | | | | | | | |
|---|---|------------------------------------|---|----------------------------|---------------------------|--------------|----|-------------------|-------------|----|--|--|--|
| Facility Name P. Stone USA Corporation | Source Name Rotary Dryer #2 | Permit No. 0550049-03 AC | Observation Method EPA Method 9 | Start Time 10:42 | Stop Time 11:22 | | | | | | | | |
| Location Address 400 Maywood Taylor Blvd, Sebring | Sec. Min. | 0 | 15 | 30 | 45 | Sec. Min. | 0 | 15 | 30 | 45 | | | |
| Contact Bob Hykes | Phone No. (803) 455-1273 | 1 | 0 | 0 | 0 | 0 | 31 | | | | | | |
| Process Production Rate Rubber Tire Drying | Control Equipment Conveyer Belts | 2 | 0 | 0 | 0 | 0 | 32 | | | | | | |
| Fuel Type/Rate natural gas | Material Type/Rate 3.58 ton/hr | 3 | 0 | 0 | 0 | 0 | 33 | | | | | | |
| Permitted Rate 5 tons/hr | Description Emission Point Plant Metal Stack | 4 | 0 | 0 | 0 | 0 | 34 | | | | | | |
| Height Above Ground Level ~25 ft | Height Relative to Observer ~0 ft | 5 | 0 | 0 | 0 | 0 | 35 | | | | | | |
| Emissions Description | | 6 | 0 | 0 | 0 | 0 | 36 | | | | | | |
| Describe Emissions None visible | Start Same | 7 | 0 | 0 | 0 | 0 | 37 | | | | | | |
| Plume Color N/A | End Same | 8 | 0 | 0 | 0 | 0 | 38 | | | | | | |
| Water Droplets Present No | Plume Type N/A | 9 | 0 | 0 | 0 | 0 | 39 | | | | | | |
| Yes <input type="checkbox"/> | If yes, is plume Attached | 10 | 0 | 0 | 0 | 0 | 40 | | | | | | |
| No <input checked="" type="checkbox"/> | Attached <input type="checkbox"/> | 11 | 0 | 0 | 0 | 0 | 41 | | | | | | |
| Meteorological Information | | 12 | 0 | 0 | 0 | 0 | 42 | | | | | | |
| Background Start light yellow End same | Background Color Start green End same | 13 | 0 | 0 | 0 | 0 | 43 | | | | | | |
| Sky Condition/CLOUD COVER Start 35% End 40% | Ambient Temp Start 77°F End same | 14 | 0 | 0 | 0 | 0 | 44 | | | | | | |
| Wind Speed Start 5-10 mph End same | Wind Direction Start SE End same | 15 | 0 | 0 | 0 | 0 | 45 | | | | | | |
| Observation Data, Site Diagram | | 16 | 0 | 0 | 0 | 0 | 46 | | | | | | |
| Stack with Plume | North Arrow | 17 | 0 | 0 | 0 | 0 | 47 | | | | | | |
| Sun |  | 18 | 0 | 0 | 0 | 0 | 48 | | | | | | |
| Wind | 19 | 0 | 0 | 0 | 0 | 0 | 49 | | | | | | |
|  | 20 | 0 | 0 | 0 | 0 | 0 | 50 | | | | | | |
| Distance | 21 | 0 | 0 | 0 | 0 | 0 | 51 | | | | | | |
| 22 | 0 | 0 | 0 | 0 | 0 | 0 | 52 | RECEIVED - D.E.P. | | | | | |
| | 23 | 0 | 0 | 0 | 0 | 0 | 53 | | HEB 05 2009 | | | | |
| | 24 | 0 | 0 | 0 | 0 | 0 | 54 | | | | | | |
| | 25 | 0 | 0 | 0 | 0 | 0 | 55 | SOUTH DISTRICT | | | | | |
| | 26 | 0 | 0 | 0 | 0 | 0 | 56 | | | | | | |
| | 27 | 0 | 0 | 0 | 0 | 0 | 57 | | | | | | |
| | 28 | 0 | 0 | 0 | 0 | 0 | 58 | | | | | | |
| | 29 | 0 | 0 | 0 | 0 | 0 | 59 | | | | | | |
| | 30 | 0 | 0 | 0 | 0 | 0 | 60 | | | | | | |
| Compliance Information | | Certification Data, Signatures | | | | | | | | | | | |
| Range of Opacity Readings Min 8 Max 0 | Observer's Name Sara Blewett | | | | | | | | | | | | |
| Average of Highest 24 Consecutive Readings 8 | Observer's Signature Sara Blewett Date 12-9-08 | | | | | | | | | | | | |
| Short Term Average Data Averaging Period 3 minutes | Organization Grove Scientific + Engineering | | | | | | | | | | | | |
| Comments * WE done on lift no objectional odors detected! | Certified By AEROMET Engineering Date 8-08 | | | | | | | | | | | | |
| | I have received a copy of these observations Signature _____ Date _____ | | | | | | | | | | | | |
| | APIS Number _____ | | | | | | | | | | | | |

VISIBLE EMISSIONS OBSERVATION FORM

| | | |
|-------------------|----|-----|
| COMPLIANCE STATUS | | |
| YES | NO | UNK |

| Source/Process Information | | | Observation Readings | | | | | | | | | | | | | | | |
|--|--|--|------------------------------------|---|----|----|----------------------------|---------------------------|---|----|----|----|---|---|---|---|----|--------------------------|
| Facility Name <i>E-Stone USA Corporation</i> | Source Name <i>Polishing Line 2</i> | Permit No. <i>0550049-003-A</i> | Observation <i>EPA Method 9</i> | | | | Start Time <i>11:38</i> | Stop Time <i>12:08</i> | | | | | | | | | | |
| Location Address <i>420 Maywood Taylor Blvd, Sebring</i> | Contact <i>Bob Hypes</i> | Phone No. <i>863-655-1273</i> | Sec. Min. | 0 | 15 | 30 | 45 | Sec. Min. | 0 | 15 | 30 | 45 | | | | | | |
| Process/Production Rate <i>Polishing Slabs</i> | Control Equipment <i>Dust Collector</i> | Operating Mode <i>Normal</i> | 1 | 0 | 0 | 0 | 0 | 31 | | | | | | | | | | |
| Fuel Type/Rate <i>Natural Gas</i> | Material Type/Rate <i>Polish Slabs</i> | Permitted Rate <i>N/A</i> | 2 | 0 | 0 | 0 | 0 | 32 | | | | | | | | | | |
| Describe Emission Point <i>round metal stack on top of dust collector</i> | Height Above Ground Level <i>~35 FT</i> | Height Relative to Observer <i>~15 FT</i> | 3 | 0 | 0 | 0 | 0 | 33 | | | | | | | | | | |
| | | | 4 | 0 | 0 | 0 | 0 | 34 | | | | | | | | | | |
| | | | 5 | 0 | 0 | 0 | 0 | 35 | | | | | | | | | | |
| | | | 6 | 0 | 0 | 0 | 0 | 36 | | | | | | | | | | |
| | | | 7 | 0 | 0 | 0 | 0 | 37 | | | | | | | | | | |
| | | | 8 | 0 | 0 | 0 | 0 | 38 | | | | | | | | | | |
| | | | 9 | 0 | 0 | 0 | 0 | 39 | | | | | | | | | | |
| | | | 10 | 0 | 0 | 0 | 0 | 40 | | | | | | | | | | |
| | | | 11 | 0 | 0 | 0 | 0 | 41 | | | | | | | | | | |
| | | | 12 | 0 | 0 | 0 | 0 | 42 | | | | | | | | | | |
| Background <i>Start: SETTLING TANKS End: same</i> | Background Color <i>tan</i> | Background Color <i>tan</i> | 13 | 0 | 0 | 0 | 0 | 43 | | | | | | | | | | |
| Sky Condition/CLOUD COVER <i>Start: 40% End: 40%</i> | Ambient Temp <i>78°F</i> | End Same | 14 | 0 | 0 | 0 | 0 | 44 | | | | | | | | | | |
| Wind Speed <i>Start: 5 mph End: 5-10 mph</i> | Wind Direction <i>SE</i> | Wind Direction <i>SE</i> | 15 | 0 | 0 | 0 | 0 | 45 | | | | | | | | | | |
| Distance <i>50</i> | Observer's Position <i>140°</i> | Observer's Position <i>140°</i> | 16 | 0 | 0 | 0 | 0 | 46 | | | | | | | | | | |
| Stack with Plume | North Arrow | | | | | | | | | | | 17 | 0 | 0 | 0 | 0 | 47 | |
| Sun | | | | | | | | | | | | 18 | 0 | 0 | 0 | 0 | 48 | |
| Wind | | | | | | | | | | | | 19 | 0 | 0 | 0 | 0 | 49 | |
| | | | | | | | | | | | | 20 | 0 | 0 | 0 | 0 | 50 | |
| | | | | | | | | | | | | 21 | 0 | 0 | 0 | 0 | 51 | |
| | | | | | | | | | | | | 22 | 0 | 0 | 0 | 0 | 52 | |
| | | | | | | | | | | | | 23 | 0 | 0 | 0 | 0 | 53 | RECEIVED - B.E.P. |
| | | | | | | | | | | | | 24 | 0 | 0 | 0 | 0 | 54 | FEB 05 2009 |
| | | | | | | | | | | | | 25 | 0 | 0 | 0 | 0 | 55 | SOUTH DISTRICT |
| | | | | | | | | | | | | 26 | 0 | 0 | 0 | 0 | 56 | |
| | | | | | | | | | | | | 27 | 0 | 0 | 0 | 0 | 57 | |
| | | | | | | | | | | | | 28 | 0 | 0 | 0 | 0 | 58 | |
| | | | | | | | | | | | | 29 | 0 | 0 | 0 | 0 | 59 | |
| | | | | | | | | | | | | 30 | 0 | 0 | 0 | 0 | 60 | |
| Compliance Information | | | Certification Data, Signatures | | | | | | | | | | | | | | | |
| Range of Opacity Readings Min. 0 Max. 0 | Observer's Name <i>Sara Greivell</i> | | | | | | | | | | | | | | | | | |
| Average of Highest 24 Consecutive Readings 0 | Observer's Signature <i>Sara Greivell</i> Date 12-9-08 | | | | | | | | | | | | | | | | | |
| Short Term Average Data Averaging Period 3 minutes Actual Average 0 | Organization <i>Grove Scientific & Engineering</i> | | | | | | | | | | | | | | | | | |
| Comments <i>No objectional odors detected VE done on lower roof</i> | Certified By <i>Aeromet Eng</i> Date 8/08 | | | | | | | | | | | | | | | | | |
| | I have received a copy of these observations. Signature _____ Date _____ | | | | | | | | | | | | | | | | | |
| | APLS Number _____ | | | | | | | | | | | | | | | | | |



AeroMet
Engineering, Inc.
Solutions for a Changing Environment

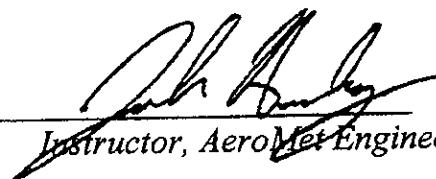
RECEIVED : D.E.P.
FEB 05 2009
SOUTHERN DISTRICT

Certification of Visible Opacity Reading

Sara Greivell

*qualified to conduct EPA Method 9 Tests for visible opacity in accordance with the
methods established for such qualification in 40 CFR Part 60 Appendix A
on August 7, 2008*

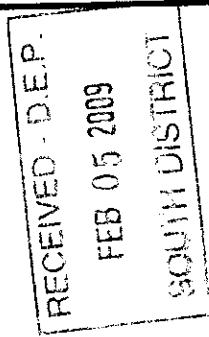
Date: 8/7/08

Signature: 
Instructor, AeroMet Engineering

Certificate expires: 02/07/09



AeroMet
Engineering, Inc.
Solutions for a Changing Environment



Certification of Visible Opacity Reading

Bruno A. Ferraro

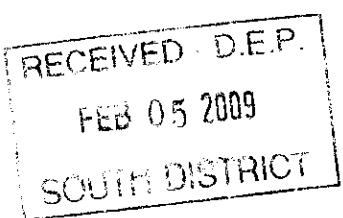
*qualified to conduct EPA Method 9 Tests for visible opacity in accordance with the
methods established for such qualification in 40 CFR Part 60 Appendix A
on August 7, 2008*

Date: 8/7/08

Signature: 
Instructor, AeroMet Engineering

Certificate expires: 02/07/09

ATTACHMENT B
DUST COLLECTOR 3 (E.U. 003) FIELD DATA SHEET





E-Stone Line 1 Dust Collector Test Data Sheet

Test Date 12-9-08

GSE Employee Name John A. Kins

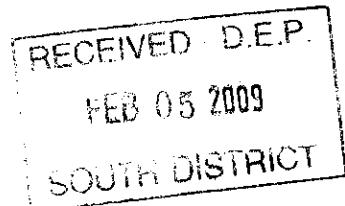
Dust Collector ID: Line 1 Zennoff E4003

Time 1020, 1145, 1300

Run Number 1, 2 & 3

Exhaust Stack Magnahelic Airflow Reading 0.4"WC 2400 FPM

Comments: *Magnahelic checked all 3 runs - no change in pressure*

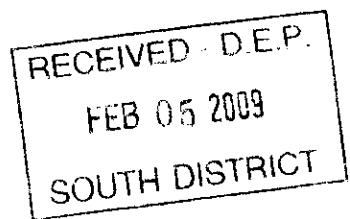


VISIBLE EMISSIONS OBSERVATION FORM

COMPLIANCE STATUS
YES NO UNK

| Source/Process Information | | Observation Readings | | | | | | | | | | | | | | |
|--|---|--------------------------------|---|--|----------|------|---|----|----|----|------|------|----------------|----------|--------|----|
| | | Observation | Start Time | Stop Time | | | | | | | | | | | | |
| Facility Name | E-5ton | Wk/Mnd 9 | 1210 | 1240 | Sec. | Min. | 0 | 15 | 30 | 45 | Sec. | Min. | 0 | 15 | 30 | 45 |
| Source Name | Poly Line / dust Collector DC 3 | Permit No | 0550046-003-AC | | | | | | | | | | | | | |
| Location Address | 420 Haywood Taylor Blvd, Sebring FL 33870 | Phone No | (863) 655-1273 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 31 | | | | | |
| Contact | Brian Hayes | | | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 32 | | | | | |
| Process/Production Rate | Produce Granite Slabs 13/hr (see production report) | | | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 33 | | | | | |
| Control Equipment | Zennith Dust Collector DC 3 | Operating Mode | -0.4" w.c. | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 34 | | | | | |
| Fuel Type/Rate | n/a | Material Type/Rate | see Prod. Report | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 35 | | | | | |
| Describe Emission Point | Silver Colored shaped Stock | Permitted Rate | n/a | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 36 | | | | | |
| Height Above Ground Level | 135 FT | Height Relative to Observer | ~2 FT | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 37 | | | | | |
| Emissions Description | | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 38 | | | | | |
| Describe Emissions | Start NONE visible | End NONE visible | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 39 | | | | | |
| Plume Color | colorless | Plume Type | NONE visible | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 40 | | | | | |
| Water Droplets Present | <input checked="" type="checkbox"/> Yes <input type="checkbox"/> No | If yes, is plume | Attached <input type="checkbox"/> n/a Detached <input type="checkbox"/> | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 41 | | | | | |
| Meteorological Information | | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 42 | | | | | |
| Background | Start Bldg | Background Color | Start Blue | End Bldg | End Blue | 13 | 0 | 0 | 0 | 0 | 0 | 43 | | | | |
| Sky Conditions/% Cloud Cover | Start Partly 50% End Partly 50% | Ambient Temp | Start 77°F | End 77°F | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 44 | | | | |
| Wind Speed | Start 10-15 End 10-15 | Wind Direction | Start SE | End SE | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 45 | | | | |
| Observation Data, Site Diagram | | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 46 | | | | |
| Stack with Plume | | North Arrow | | 17 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 47 | | | | |
| Sun | | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 48 | | | | |
| Wind | | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 49 | | | | |
| | | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 50 | | | | |
| Observer's Position | ridge | 21 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 51 | | | | |
| Distance | 50' | 22 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 52 | | | | |
| Sun Location Line | | 23 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 53 | | | | |
| 140° | | 24 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 54 | | | | |
| | | 25 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 55 | | RECEIVED | D.E.P. | |
| 26 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 56 | | FEB 05 2009 | | | |
| 27 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 57 | | SOUTH DISTRICT | | | |
| 28 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 58 | | | | | |
| 29 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 59 | | | | | |
| 30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 60 | | | | | |
| Compliance Information | | Certification Data, Signatures | | | | | | | | | | | | | | |
| Range of Opacity Readings | Min: 0 | Max: 0 | Observer's Name: Bruno Ferrara | | | | | | | | | | | | | |
| Average of Highest 24 Consecutive Readings | 0 | | Observer's Signature: | | | | | | | | | | | | | |
| Short Term Average Data | 3 | minutes | Actual Average: 0 | Organization: Grove Scientific & Engineering | | | | | | | | | | | | |
| Averaging Period | 3 minutes | | x | Certified By: Acmetech | | | | | | | | | | | | |
| Comments | No odors | | | I have received a copy of these observations. Signature: | | | | | | | | | | | | |
| APIS Number: | | | | | | | | | | | | | | | | |
| EUCD3 | | | | | | | | | | | | | | | | |

ATTACHMENT C
PTE TEST DATA SHEETS VERIFYING COMPLIANCE
WITH PROCEDURE-T



EPA Method 204 Procedure-T
PTE Certification Data Sheet



Each of the compliance and performance criteria have been tested and the data presented below. Calculations and notes are presented on the back of this worksheet.

Facility Name: E-Stone

Facility Address: 420 Howard Taylor Blvd, Sebring, FL

Production Line Number and Type: Polymerization Line 1

Area of natural Draft Opening(s) (NDO): 16.9''x 6'' or 4.1' x 0.5' = 2.04 ft²

NDO Location and Description: Slab discharge / enclosure exit

EPA Method 204 Procedure-T referenced in 40 CFR Chapter I, Part 52 Appendix B requires that the following criteria be met.

1) Any NDO shall be at least 4 equivalent opening diameters from each VOC emitting point.

Equivalent opening diameters = 2.47 ft

4 equivalent diameters = 11.97 ft

Distance to VOC emitting point = > 20'

2) The total area of all NDO's shall not exceed 5% of the surface area of the enclosure.

Surface area of enclosure = 44 ft² > 263.6 ft²

Surface area of all NDO's = 2.47 ft²

% of area of enclosure = > 2.8% of first floor of building (no fence area)

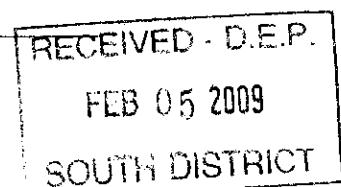
3) The facial velocity of the air into the NDO shall be greater than 200 fpm.

Measured velocity through NDO = 220 - 280 fpm

4) All lids and covers must be in place during operation.

Verified and dry-ice test passed by: yes

PTE Certified by: Bruno A. Ferraro 10/30/08
Bruno A. Ferraro, CEP, QEP





EPA Method 204 Procedure-T
PTE Certification Data Sheet

Each of the compliance and performance criteria have been tested and the data presented below. Calculations and notes are presented on the back of this worksheet.

Facility Name: F-Stone

Facility Address: 420 Maywood Taylor Blvd, Sebring FL

Production Line Number and Type: Line 1 (Furnace) / NDO on ceiling

Area of natural Draft Opening(s) (NDO): (2" x 3") + (2" x 3") + (2" x 3") + (2" x 3") = 24" Sq. inches
0.12 sq ft

NDO Location and Description: During Corrugated Extrusion

EPA Method 204 Procedure-T referenced in 40 CFR Chapter I, Part 52 Appendix B requires that the following criteria be met.

1) Any NDO shall be at least 4 equivalent opening diameters from each VOC emitting point.

Equivalent opening diameters = 0.34 ft

4 equivalent diameters = 1.36

Distance to VOC emitting point = >1.2 ft

2) The total area of all NDO's shall not exceed 5% of the surface area of the enclosure.

Surface area of enclosure = 24 ft x 24 ft = 576 ft² (just floor & ceiling)

Surface area of all NDO's = 7.4 ft²

% of area of enclosure = 0.13% of just floor & ceiling

3) The facial velocity of the air into the NDO shall be greater than 200 fpm.

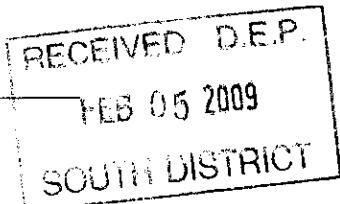
Measured velocity through NDO = -285 fpm in/sec

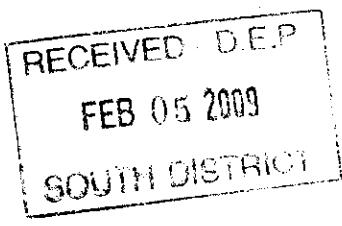
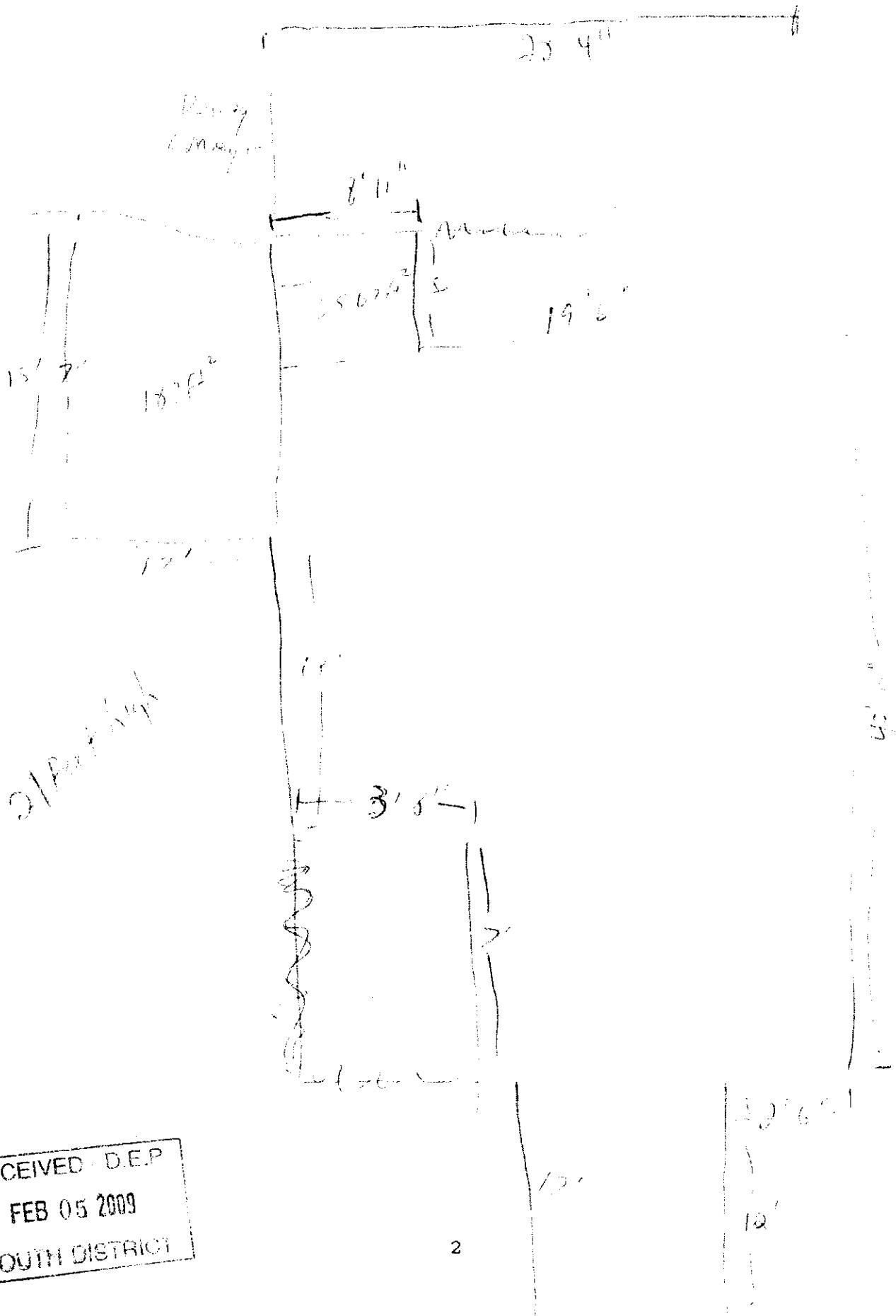
4) All lids and covers must be in place during operation.

Verified and dry-ice test passed by: Yes

PTE Certified by: Bruno A. Ferraro 12/30/08

Bruno A. Ferraro, CEP, QEP







E-Stone Enclosure Line 1 Test Data Sheet

Test Date 12-9-08

GSE Employee Name Steve A. Kins

Time Start 1015 Run 1

Time End 1115

Total Time in Minutes 60 min Run 1

Magnahelic 1 Reading -0.005" w.c.

Magnahelic 2 Reading -0.02" w.c.

NDO airspeed at conveyor inlet (fpm) -365 & -0.6" w.c set point

NDO airspeed at slab outlet (fpm) -204 & -0.6" w.c. set point

1-hour NDO Airflow Check Using Smoke Tubes

| Time (minutes) | Inlet NDO | Outlet NDO |
|----------------|-----------|------------|
| 0 | Neg | Neg |
| 10 | Neg | Neg |
| 20 | Neg | Neg |
| 30 | Neg | Neg |
| 40 | Neg | Neg |
| 50 | Neg | Neg |
| 60 | Neg | Neg |

Comments: _____

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E-Stone Enclosure Line 1 Test Data Sheet

Test Date 12-9-08

GSE Employee Name Bruce A. Gunn

Time Start 1155

Time End 1255

Total Time in Minutes 60

Magnahelic 1 Reading 0.005

Magnahelic 2 Reading 0.035

NDO airspeed at conveyor inlet (fpm) -355 c -0.6" w.c. set point

NDO airspeed at slab outlet (fpm) -214 c -0.6" w.c. set point

1-hour NDO Airflow Check Using Smoke Tubes

| Time (minutes) | Inlet NDO | Outlet NDO |
|----------------|-----------|------------|
| 0 | NEG | NEG |
| 10 | NEG | NEG |
| 20 | NEG | NEG |
| 30 | NEG | NEG |
| 40 | NEG | NEG |
| 50 | NEG | NEG |
| 60 | NEG | NEG |

Comments: _____

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E-Stone Enclosure Line 1 Test Data Sheet

Test Date 12-9-03

GSE Employee Name Brian A. Jones

Time Start 1405

Time End 1505

Total Time in Minutes 60

Magnahelic 1 Reading -0.005

Magnahelic 2 Reading -0.04

NDO airspeed at conveyor inlet (fpm) -319 @ -0.6" w.c. set point

NDO airspeed at slab outlet (fpm) -220 @ 0.6" w.c. set point

1-hour NDO Airflow Check Using Smoke Tubes

| Time (minutes) | Inlet NDO | Outlet NDO |
|----------------|-----------|------------|
| 0 | NEG | NEG |
| 10 | NEG | NEG |
| 20 | NEG | NEG |
| 30 | NEG | NEG |
| 40 | NEG | NEG |
| 50 | NEG | NEG |
| 60 | NEG | NEG |

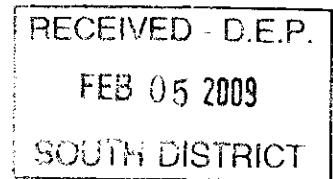
Comments: _____

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ATTACHMENT D
RTO FIELD DATA SHEETS AND RTO TEMPERATURE
CHART





E-Stone RTO Parametric Data Sheet

Test Date 12-9-08

GSE Employee Name Bruce A. Kuehn

Control Device Crawford Industrial Group RTO 7000

Time Start 0908 (computer time) start dosing,
0914 clock time

Fuel Meter Reading at Start 181500 CF @ 0920 hrs

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Time End 1503 computer time point
1505 clock time

SOUTH DISTRICT

Fuel Meter Reading at End 184400 CF @ 1505

Total Time in Minutes 240 + 51 = 291 min

Total Fuel Used 2900 CF in 345 min or 504 CF/hr

| Run 1 | Run 2 | Run 3 |
|-------|-------|-------|
| ✓ | ✓ | |
| | ✓ | ✓ |

Inlet Duct Airflow Rate Magnahelic Reading 0.125" w.c 1800 fpm

Exhaust Stack Airflow Rate Magnahelic Reading 0.25" w.c & 2000 fpm

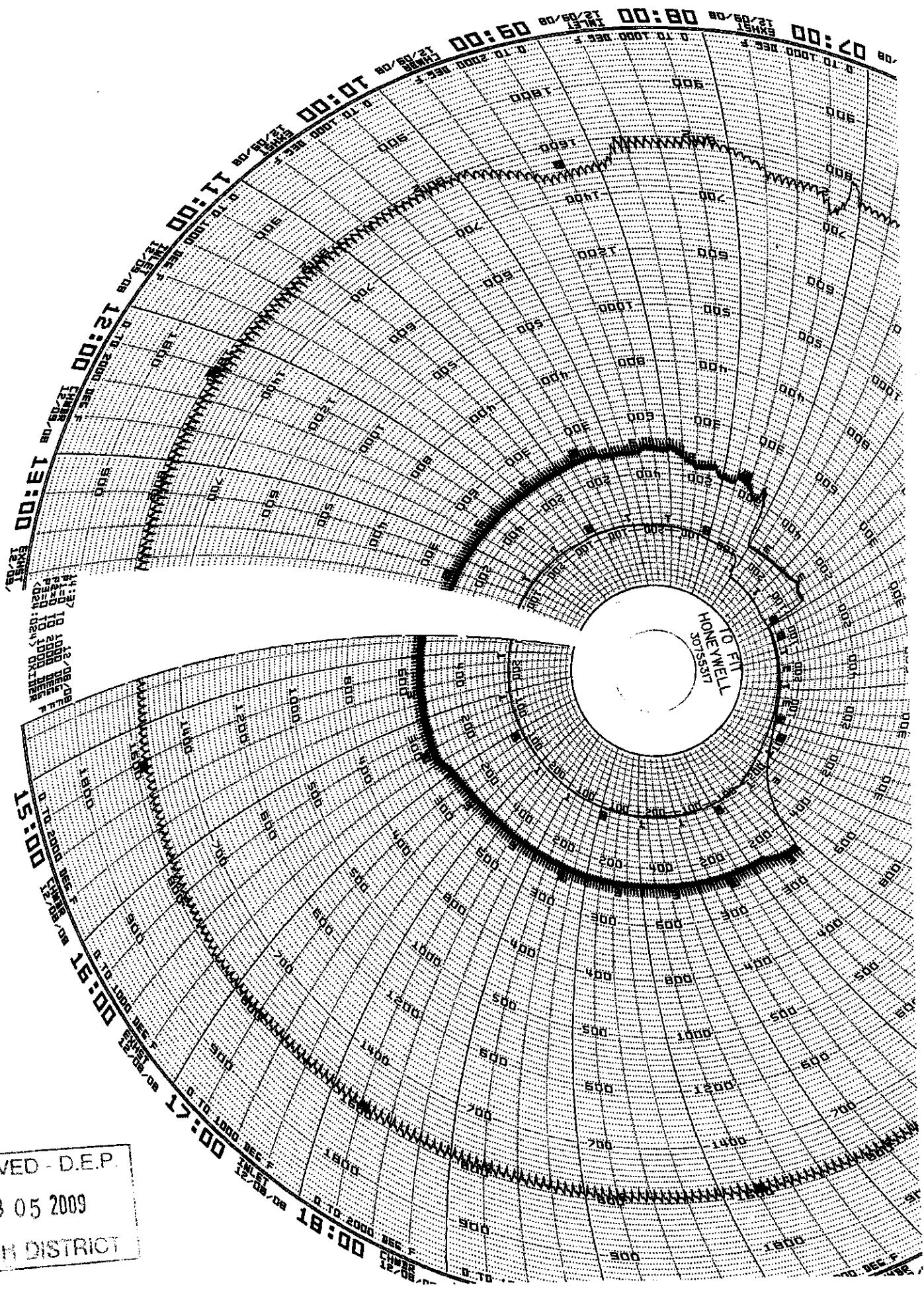
Vacuum Set-point -0.6" w.c. At 13 min

Combustion Chamber Temperature 1577°F

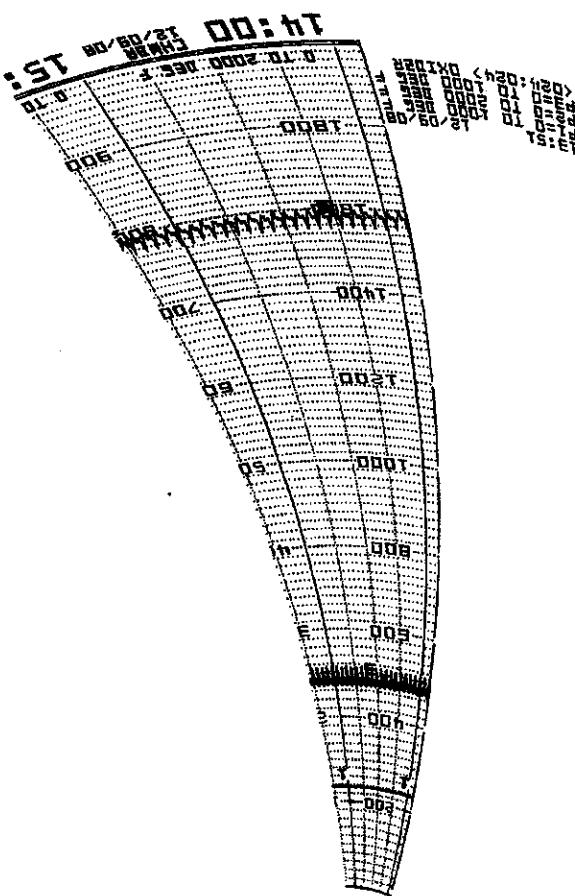
Comments Product ID 635 Tropico - 13-14 slabs/hr production rate

resin

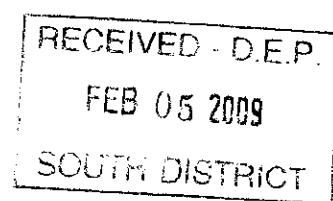
Test start 10:15 Run 1 - vacuum set point remains at -0.6" w.c.
Inlet & outlet duct flows remained constant during all runs



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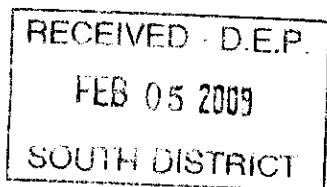
30TS5327
HONEYWELL
TO FIT



ATTACHMENT E

COMPUTER GENERATED PRODUCTION REPORT

AND MSDS FOR 2 AOC POLYESTER RESINS



| | | | | | | | | |
|--------------------------------|------------|------------------------------------|-------------|-------------------------------|---------------|---------------|-------------------------|---------------|
| MP 370 151 - Report New | WKS635204 | Print Screen | Main Screen | Recipe Production Code: US635 | Desc: Tropico | Date: ES81635 | Store & Clear Total | Stored Report |
| Raw Material Report: | | | | | | | | |
| Star Time: 2008-12-09 09:12:10 | | | | | | | | |
| Code: US635 | | Order: ES81635 | | | | | | |
| Name: Tropico | | | | | | | E-Stone USA Corporation | |
| Notes: revised 10/15/07 | | | | | | | Total Slabs: 1 | |
| Bin/Slot | | | | | | | | |
| A111 | ID G019485 | Desc Baltic Brown 48/5 | | Total Weight | 11.596 | lb | 5.260 | kg |
| A112 | ID G019484 | Desc Baltic Brown 48/4 | | Total Weight | 33.598 | lb | 15.240 | kg |
| A113 | ID G019483 | Desc Baltic Brown 48/3 | | Total Weight | 9.877 | lb | 4.480 | kg |
| A114 | ID G019470 | Desc Baltic Brown 47 | | Total Weight | 22.421 | lb | 10.170 | kg |
| A115 | ID G019460 | Desc Baltic Brown 46 | | Total Weight | 9.546 | lb | 4.330 | kg |
| A116 | ID G019450 | Desc Baltic Brown 45 | | Total Weight | 7.275 | lb | 3.300 | kg |
| A117 | ID G012 | Desc Quartz GS20 | | Total Weight | 5.666 | lb | 2.570 | kg |
| A118 | ID G009 | Desc GS40 | | Total Weight | 3.968 | lb | 1.800 | kg |
| A119 | ID RM0009 | Desc Silcosil 125 | | Total Weight | 12.610 | lb | 5.720 | kg |
| A120 | ID | Desc | | Total Weight | 0.000 | lb | 0.000 | kg |
| A121 | ID | Desc | | Total Weight | 0.000 | lb | 0.000 | kg |
| A122 | ID | Desc | | Total Weight | 0.000 | lb | 0.000 | kg |
| A123 | ID | Desc | | Total Weight | 0.000 | lb | 0.000 | kg |
| A101-104 | ID RNTR | Desc Polyester Resin 50/50 Nuetral | | Total Weight | 21.667 | lb | 9.828 | kg |
| M1609 | ID RM0012 | Desc Norox 90cc | | Total Weight | 0.222 | lb | 0.101 | kg |

Print Screen 09:11:42 10 CALIBRATING NOT READY 05 2008-12-09 09:12:25

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FEB 05 2009

SOUTH DISTRICT



Raw Material Report:

[Store & Clear Total](#)

[Stored Report](#)

Star Time: 2008-12-09 09:12:10

Code: US635 Order: ES81635

Name: Tropico

Notes: revised 10/15/07

**E-Stone USA
Corporation**

Total Slabs: 78

Bin/Slot

| | | | | | | | |
|----------|------------|------------------------------------|--------------|----------|----|----------|----|
| A111 | ID G019485 | Desc Baltic Brown 48/5 | Total Weight | 922.413 | lb | 418.400 | kg |
| A112 | ID G019484 | Desc Baltic Brown 48/4 | Total Weight | 2634.390 | lb | 1194.940 | kg |
| A113 | ID G019483 | Desc Baltic Brown 48/3 | Total Weight | 749.703 | lb | 340.060 | kg |
| A114 | ID G019470 | Desc Baltic Brown 47 | Total Weight | 1713.497 | lb | 777.230 | kg |
| A115 | ID G019460 | Desc Baltic Brown 46 | Total Weight | 726.687 | lb | 329.620 | kg |
| A116 | ID G019450 | Desc Baltic Brown 45 | Total Weight | 578.977 | lb | 262.620 | kg |
| A117 | ID G012 | Desc Quartz GS20 | Total Weight | 434.420 | lb | 197.050 | kg |
| A118 | ID G009 | Desc GS40 | Total Weight | 305.494 | lb | 138.570 | kg |
| A119 | ID RM0009 | Desc Silcosil 125 | Total Weight | 1004.403 | lb | 455.590 | kg |
| A120 | ID | Desc | Total Weight | 0.000 | lb | 0.000 | kg |
| A121 | ID | Desc | Total Weight | 0.000 | lb | 0.000 | kg |
| A122 | ID | Desc | Total Weight | 0.000 | lb | 0.000 | kg |
| A123 | ID | Desc | Total Weight | 0.000 | lb | 0.000 | kg |
| A101-104 | ID RNTR | Desc Polyester Resin 50/50 Nuetral | Total Weight | 1674.901 | lb | 759.723 | kg |
| M1609 | ID RM0012 | Desc Norox 90cc | Total Weight | 16.741 | lb | 7.594 | kg |

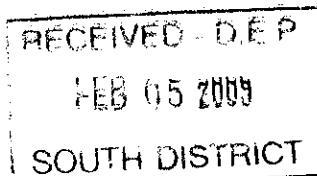
Print Screen

15:04:45

M1001 - WARNING INVERTER MOTOR M1001 - UNLOAD SLABS TROLLEY

US

2008-12-09 15:04:52



[Main Screen](#)

[Dosing Home Page](#)

Recipe: Dosing Formula

| Archives | Code: | Name: | Display Mode | |
|----------|------------|------------------------------------|--------------|-----------|
| Bln/Slot | | Notes: | | |
| A111 | ID G019485 | Desc Baltic Brown 48/5 | 12.000 lb | 5.443 kg |
| A112 | ID G019484 | Desc Baltic Brown 48/4 | 33.640 lb | 15.259 kg |
| A113 | ID G019483 | Desc Baltic Brown 48/3 | 9.080 lb | 4.119 kg |
| A114 | ID G019470 | Desc Baltic Brown 47 | 21.890 lb | 9.929 kg |
| A115 | ID G019460 | Desc Baltic Brown 46 | 9.680 lb | 4.391 kg |
| A116 | ID G019450 | Desc Baltic Brown 45 | 7.320 lb | 3.320 kg |
| A117 | ID G012 | Desc Quartz GS20 | 5.500 lb | 2.495 kg |
| A118 | ID G009 | Desc GS40 | 4.000 lb | 1.814 kg |
| A119 | ID RM0009 | Desc Silcosil 125 | 13.000 lb | 5.897 kg |
| A120 | ID | Desc | 0.000 lb | 0.000 kg |
| A121 | ID | Desc | 0.000 lb | 0.000 kg |
| A122 | ID | Desc | 0.000 lb | 0.000 kg |
| A123 | ID | Desc | 0.000 lb | 0.000 kg |
| A101-104 | ID RNTR | Desc Polyester Resin 50/50 Nuetral | 21.500 lb | 9.752 kg |
| M1609 | ID RM0012 | Desc Norox 90cc | 0.200 lb | 0.091 kg |

[Read Data From PLC](#)
[Write Data To PLC](#)

Print Screen

09:11:42 10

CALIBRATING NOT READY

05

G

2008-12-09 09:15:31

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FEB 05 2009

SOUTH DISTRICT



E-Stone Polymerization Line Process Data Sheet

Test Date 12-9-08

GSE Employee Name Bryan A. Furr

Polymerization Line Number 1

Time Start 0900 Computer Time

Time End 1504 Computer Time

Total Time in Minutes 292 min

Total Quantity of Slabs Produced 78 Slabs in 292 min = 16 Slab/hr

Method of Determining Process Rate Automated data collection system

Comments see production report generated by E-stone process computer
resin 50% - PKE AOC Resin and 50% PLE AOC Resin

| |
|-------------------|
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Resin Preparation Verification Sheet

Date 12/18/08
 Job # S136-08
 Silo # 103
 Slab Color 635
 Resin Blend Ratio / Code 55/50 RNTR

| | Catalyzed Qty (Lbs) | Un-Catalyzed Qty (Lbs) |
|--------------------------|------------------------|---------------------------|
| Existing Qty PKE | | |
| Existing Qty PKC | | |
| Resin Blend Ratio / Code | | |

| | Qty (Lbs) | Qty (CC) | Manual Calculation (Lbs) |
|--------------------------|---------------|------------|-----------------------------|
| Added Qty PKE (PLC) | <u>1245.2</u> | | <u>1276</u> |
| Added Qty PKC (PLC) | <u>1250.3</u> | | <u>1275</u> |
| Added Qty of Tinuvin | <u>9.0</u> | | |
| Added Qty of Styrene | <u>7.0</u> | | <u>2551</u> |
| Added Qty of Silquest | <u>7.2</u> | | |
| Added Qty of Coatosil | | <u>195</u> | |
| Added Qty of NL 51P | | <u>177</u> | <u>2596</u> |
| Added Qty of Pigment (1) | | | |
| Added Qty of Pigment (2) | | | |
| Added Qty of Pigment (3) | | | |

| | Checklist | Check @ completion |
|---------------------|--|--------------------|
| Pumping Resin | Verify Upper valve for selected silo open | / |
| | Verify that the bottom valve & downstream valve for selected silo are closed | / |
| Silo Identification | Verify that the upper valve is closed after charging material | / |
| | Verify that the silo is properly identified in PLC (ex. RNTR, R620) | / |
| | Verify that the silo is properly identified with label | / |
| | Verify that the cycle settings for silo is in Automatic @ PLC | / |

Prepared by
 Approved by

Mason Johnson
215-117

| |
|-----------------|
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| FEB 05 2009 |
| SOUTH DISTRICT |

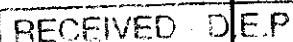


Material Safety Data Sheet

MSDS no. 12666V1

| WHMIS (Canada) | NFPA (USA) | HMIS (USA) | Protective clothing |
|----------------|---------------------|--|---------------------|
| | Specific hazard | Health hazards Fire hazard Reactivity Personal protection | |

Section I. Chemical Product and Company Identification

| | | | |
|---|---|------------------|---|
| Trade name | A520-PKC-00 | Product type | Polyester Resin Solution |
| CAS # | Not applicable. | Synonym | None. |
| Chemical name | Not applicable. | Chemical formula | Not applicable.  FEB 05 2003 |
| Chemical family | Aromatic. | | |
| Material uses | Used in the manufacture of thermoset plastic parts. | | |
| TSCA | All ingredients are listed or compliant with TSCA. | | SOUTH DISTRICT |
| DSL | All ingredients are listed or compliant with the NSNR. | | |
| <u>Manufacturer</u> | <u>In case of emergency</u> | | |
| AOC, LLC 950 Highway 57 East Collierville, TN U.S.A. 38017 Phone Number: (901) 854-2800 8am-5pm (CST) Mon-Fri | CHEMTRAC (US): 24 hours/7 days (800) 424-9300 CANUTEC (Canada): 24 hours/7 days (613) 996-6666 | | |

Section II. Information on Hazardous Ingredients

| Name | CAS # | % by weight |
|------------|----------|-------------|
| 1) Styrene | 100-42-5 | 35.0 |

Section III. Hazards Identification.

| | |
|----------------------------------|--|
| Potential acute health effects | Inhalation of spray mist or liquid vapors may cause upper respiratory irritation and possible central nervous system effects including headaches, nausea, vomiting, dizziness, drowsiness, loss of coordination, impaired judgement and general weakness. Severe eye irritant which may result in redness, burning, tearing and blurred vision. Skin irritant which may result in burning sensation. Ingestion may result in mouth, throat and gastrointestinal irritation, nausea, vomiting and diarrhea. |
| Potential chronic health effects | CARCINOGENIC EFFECTS: <u>Styrene:</u> Classified A4 (not classifiable for human or animal) by ACGIH. Classified 2B (possible for human) by IARC. An increased incidence of lung tumors was observed in mice from a recent inhalation study. The relevance of this finding is uncertain since data from other long-term animal studies and from epidemiology studies of workers exposed to styrene do not provide a basis to conclude that styrene is carcinogenic. Lung effects have been observed in mouse studies following repeated exposure. MUTAGENIC EFFECTS Not available. TERATOGENIC EFFECTS |
| Effective Date: 05/17/2006 | Supersedes Date: Not applicable. |
| | Page: 1 |

Section VI. Accidental Release Measures

| | |
|-------------|---|
| Small Spill | Absorb with an inert material and place in an appropriate waste disposal container. |
| Large Spill | Stop leak if without risk. Eliminate all ignition sources. Contain with an inert material, recover as much as possible and place the remainder in an appropriate waste disposal container. Warn unauthorized personnel to move away. Prevent entry into sewers or confined areas. |

Section VII. Handling and Storage

| | |
|-------------|--|
| Precautions | <p>WARNING! Use only in well-ventilated areas. Store away from direct sunlight. Avoid inhalation and contact with eyes, skin, and clothing. Wear appropriate personal protective equipment for your task. Ground and bond all containers when transferring the material. Empty containers may retain product and product vapor. Do not expose to heat, flame, sparks or other ignition sources such as cutting, welding, drilling, grinding or static electricity. Do not pressurize. Provide adequate safety showers and eyewashes in the area of use.</p> <p>Note: If product contains metal compounds (Section II), avoid dust from dried product or grinding of articles made from this material.</p> |
| Storage | Keep away from heat. Keep away from sources of ignition. Keep container tightly closed. Keep in a cool, well-ventilated place. Containers should be grounded. |

Section VIII. Exposure Controls/Personal Protection

| | | |
|--|--|---|
| Exposure limits | 1) Styrene | OSHA PEL (United States). TWA: 100 ppm TWA: 426 mg/m ³ ACGIH TLV (United States). TWA: 20 ppm TWA: 85 mg/m ³ |
| Engineering controls | Provide exhaust ventilation or other engineering controls to keep the airborne concentrations of vapors below their respective occupational exposure limits. Provide adequate safety showers and eyewashes in the area of use. | |
| Personal protection | Personal protective equipment may vary depending on the job being performed. Eye/Face: Wear eye protection such as safety glasses with side shields, splash goggles or face shield with safety glasses. Skin: Avoid skin contact. Impervious gloves should be worn. Other items may include long sleeves, lab coats, or impervious jackets. Respiratory: Determine if airborne concentrations are below the recommended exposure limits in accordance your company's PPE program and regulatory requirements. If they are not, select a NIOSH-approved respirator that provides adequate protection from the concentration levels encountered. Air-purifying respirators are generally adequate for organic vapors. Use positive pressure, supplied-air respirators if there is potential for an uncontrolled release, if exposure levels are unknown, or under circumstances where air-purifying respirators may not provide adequate protection. Reference OSHA 29 CFR 1910.134 | |
| RECEIVED - D.E.P. FEB 05 2009 SOUTH DISTRICT | Personal protection in case of a large spill | Chemical resistant gloves, full protective suit, and boots. Respiratory protection in accordance with OSHA regulation 29 CFR 1910.134. A self-contained breathing apparatus should be used to avoid inhalation of the product vapors. |

Section IX. Physical and Chemical Properties

| | | | |
|--------------------------|---------------------------------|------------------------|------------------------|
| Physical state | Liquid. | Odor | Aromatic. |
| Color | Yellow. | pH (1% soln/water) | Not applicable. |
| Molecular weight (g/mol) | 1000 to 15000 | Boiling point | 293°F (145°C) Styrene |
| melting point | Not available. | Specific gravity | 1.1 (Water = 1) |
| Vapor pressure | 4.5 mm Hg @ 68°F (20°C) Styrene | Vapor density | 3.59 Styrene (Air = 1) |
| Odor threshold | 0.14 ppm Styrene | Water/oil dist. coeff. | Not available. |

Section XIV. Transport Information

| | | | |
|----------------------------------|--|--------|---|
| TDG - Shipping description | Resin Solution; 3; UN1866; III. | Labels |  |
| IATA/IMDG - Shipping description | IATA: UN1866; Resin Solution; 3; III; Pkg. Inst.: Passenger - 309; Cargo - 310 IMDG: UN1866; Resin Solution; 3; III; FP=31°C; EmS No.: F-E, S-E | | |
| Additional information | US regulations require the reporting of spills when the amount exceeds the Reportable Quantity (RQ) for specific components of this material. See CERCLA in Section 15, Regulatory Information, for the Reportable Quantities. | | |

Section XV. Other Regulatory Information

| | |
|-------------------|---|
| Other regulations | <p>This section does not reference all applicable regulatory compliance lists.</p> <p>OSHA: Hazardous by definition of Hazard Communication Standard (29 CFR 1910.1200).</p> <p>Proposition 65 Warning: This product contains a chemical(s) known to the State of California to cause cancer, birth defects and/or reproductive harm.</p> <p>SARA 302 component(s): None.</p> <p>SARA 313 component(s): Styrene.</p> <p>CERCLA RQ(s):</p> <p>Styrene-1000 lbs. (453.6 kg)</p> |
|-------------------|---|

Section XVI. Other Information

| | |
|------------|--|
| References | <ul style="list-style-type: none"> -Transportation of Dangerous Goods Act - "Regulations respecting the handling, offering for transport and transporting of dangerous goods." Extract from the Canada Gazette Part II -Canada Gazette Part II, Hazardous Products Act "Ingredient Disclosure List". -Manufacturer's Material Safety Data Sheet. -29 CFR 1910.1000, Z - Tables -ACGIH 2000 TLVs for Chemical Substances and Physical Agents -Registry of Toxic Effects of Chemical Substances (RTECS) -California Code of Regulation Proposition 65 |
|------------|--|

| | | |
|-------------|--|----|
| Prepared by | AOC, LLC - Corporate Regulatory Affairs. | FL |
|-------------|--|----|

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The information contained in this data sheet is furnished in good faith and without warranty, representation, or inducement or license of any kind, except that it is accurate to the best of AOC, LLC's knowledge, or was obtained from sources believed by AOC, LLC to be reliable. The accuracy, adequacy or completeness of health and safety precautions set forth herein cannot be guaranteed, and the buyer is solely responsible for ensuring that the product is used, handled, stored, and disposed of safely and in compliance with applicable federal, state or provincial, and local laws. AOC, LLC disclaims liability for any loss, damage or personal injury that arises from, or is in any way related to, use of the information contained in this data sheet.

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World Leader in Resin Technology

Material Safety Data Sheet

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FEB 05 2009

SOUTH DISTRICT

MSDS no. 12795V3

| WHMIS (Canada) | NFPA (USA) Fire | HMIS (USA) | Protective clothing |
|---|---|--|---|
|  |  |  |  |
| B-2 D-2A D-2B | Health Reactivity Specific hazard | Flammability Personal protection | |

Section 1. Chemical product and company identification

| | | |
|-----------------|---|---|
| Trade name | A520-PKE-00 | |
| Product type | Polyester Resin Solution | |
| Chemical family | Aromatic. | |
| Material uses | Used in the manufacture of thermoset plastic parts. | |
| Manufacturer | AOC, LLC 950 Highway 57 East Collierville, TN U.S.A. 38017 Website: www.aoc-resins.com Phone Number: (901) 854-2800 8am-5pm (Central Time) Mon-Fri | In case of emergency CHEMTREC (US): 24 hours/7 days (800) 424-9300 CANUTEC (Canada): 24 hours/7 days (613) 996-6666 |

Section 2. Hazards identification

| | |
|----------------------------------|--|
| OSHA status | This material is considered hazardous by the OSHA Hazard Communication Standard (29 CFR 1910.1200). |
| Routes of entry | Eye contact, Skin contact, Inhalation, Ingestion |
| Potential acute health effects | Eyes: Severe eye irritant which may result in redness, burning, tearing and blurred vision. Skin: Skin irritant which may result in burning sensation. Repeated or prolonged skin contact may cause dermatitis. Ingestion: Ingestion may result in mouth, throat and gastrointestinal irritation, nausea, vomiting and diarrhea. Inhalation: Inhalation of spray mist or liquid vapors may cause upper respiratory irritation and possible central nervous system effects including headaches, nausea, vomiting, dizziness, drowsiness, loss of coordination, impaired judgement and general weakness. |
| Potential chronic health effects | CARCINOGENIC EFFECTS: <u>Styrene</u> : Classified A4 (not classifiable for human or animal) by ACGIH. Classified 2B (possible for human) by IARC. An increased incidence of lung tumors was observed in mice from a recent inhalation study. The relevance of this finding is uncertain since data from other long-term animal studies and from epidemiology studies of workers exposed to styrene do not provide a basis to conclude that styrene is carcinogenic to humans. Lung effects have been observed in mouse studies following repeated exposure. MUTAGENIC or TERATOGENIC EFFECTS: No known effect according to our database. |

Section 3. Composition/information on ingredients

| Name | CAS # | % by weight |
|------------|----------|-------------|
| 1) Styrene | 100-42-5 | 35.0 |

Section 4. First aid measures

| | |
|--------------|---|
| Eye contact | Flush with a continuous flow of water for at least 15 minutes, occasionally lifting the upper and lower eyelids. Use of buffered baby shampoo will aid in removal. Seek medical attention. |
| Skin contact | Gently and thoroughly wash the contaminated skin with running water and non-abrasive soap. If irritation persists, seek medical attention. |
| Inhalation | Move the victim to a safe area as soon as possible. Allow the victim to rest in a well-ventilated area. If breathing is difficult, give oxygen. If the victim is not breathing, perform mouth-to-mouth resuscitation. Seek immediate medical attention. |
| Ingestion | Do not induce vomiting. Seek immediate medical attention. |

Section 5. Fire fighting measures

| | |
|--------------------------------------|---|
| The product is: | Flammable liquid, Class IC. |
| Auto-ignition temperature | 914°F (490°C) Styrene |
| Flash point | 87.6°F (31°C) Styrene |
| Flammable limits | Lower: 0.9% Upper: 6.8% (Styrene) |
| Products of combustion | May produce carbon monoxide, carbon dioxide, and irritating or toxic vapors, gases or particulate. |
| Fire hazard | Flammable in the presence of open flames, sparks, or heat. |
| Explosion hazard | Can react with oxidizing materials. Explosive in the form of vapor when exposed to heat or flame. Material may polymerize when container is exposed to heat (fire) and polymerization will increase pressure in a closed container which may cause the container to rupture violently. |
| Fire-fighting media and instructions | SMALL FIRE: Use carbon dioxide, foam, dry chemical or water fog to extinguish. LARGE FIRE: Evacuate surrounding areas. Use carbon dioxide, foam, dry chemical or water fog to extinguish. Wear self-contained breathing apparatus (SCBA) and full fire-fighting protective clothing. Cool containing vessels with water spray in order to prevent pressure build-up, autoignition or explosion. Prevent run off to sewers or other water ways. |

Section 6. Accidental release measures

| | |
|-------------|---|
| Small spill | Absorb with an inert material and place in an appropriate waste disposal container. |
| Large spill | Stop leak if without risk. Eliminate all ignition sources. Contain with an inert material, recover as much as possible and place the remainder in an appropriate waste disposal container. Warn unauthorized personnel to move away. Prevent entry into sewers or confined areas. |

Section 7. Handling and storage

| | |
|----------|---|
| Handling | WARNING! Use only in well-ventilated areas. Store away from direct sunlight. Avoid inhalation and contact with eyes, skin, and clothing. Wear appropriate personal protective equipment for your task. Ground and bond all containers when transferring the material. Empty containers may retain product and product vapor. Do not expose to heat, flame, sparks or other ignition sources such as cutting, welding, drilling, grinding or static electricity. Do not pressurize. Provide adequate safety showers and eyewashes in the area of use. Note: If product contains metal compounds (Section II), avoid dust from dried product or grinding of articles made from this material. |
| Storage | Keep away from heat. Keep away from sources of ignition. Keep container tightly closed. Keep in a cool, well-ventilated place. Containers should be grounded. |

Section 8. Exposure controls/personal protection

| | | |
|--|---------|--|
| Exposure limits | Styrene | OSHA PEL (United States). TWA: 100 ppm TWA: 426 mg/m ³ ACGIH TLV (United States). TWA: 20 ppm TWA: 85 mg/m ³ |
| Engineering controls | | Provide exhaust ventilation or other engineering controls to keep the airborne concentrations of vapors below their respective occupational exposure limits. Provide adequate safety showers and eyewashes in the area of use. |
| Personal protection | | Personal protective equipment may vary depending on the job being performed. Eye/Face: Wear eye protection such as safety glasses with side shields, splash goggles or face shield with safety glasses. Skin: Avoid skin contact. Impervious gloves should be worn. Other items may include long sleeves, lab coats, or impervious jackets. Respiratory: Determine if airborne concentrations are below the recommended exposure limits in accordance your company's PPE program and regulatory requirements. If they are not, select a NIOSH-approved respirator that provides adequate protection from the concentration levels encountered. Air-purifying respirators are generally adequate for organic vapors. Use positive pressure, supplied-air respirators if there is potential for an uncontrolled release, if exposure levels are unknown, or under circumstances where air-purifying respirators may not provide adequate protection. Reference OSHA 29 CFR 1910.134 |
| Personal protection in case of a large spill | | Chemical resistant gloves, full protective suit, and boots. Respiratory protection in accordance with OSHA regulation 29 CFR 1910.134. A self-contained breathing apparatus should be used to avoid inhalation of the product vapors. |

Section 9. Physical and chemical properties

| | |
|---------------------------|---------------------------------|
| Physical state | Liquid. |
| Color | Yellow. |
| Odor | Aromatic. |
| Molecular weight (g/mol) | 1000 to 15000 |
| Boiling point | 293°F (145°C) Styrene |
| Melting point | Not available. |
| pH (1% soln/water) | Not applicable. |
| Vapor pressure | 4.5 mm Hg @ 68°F (20°C) Styrene |
| Vapor density | 3.59 Styrene (Air = 1) |
| Specific gravity | 1.1 (Water = 1) |
| Water/oil dist. coeff. | Not available. |
| Evaporation rate | Not available. |
| Odor threshold | 0.14 ppm Styrene |
| Solubility in water | Slight. |
| Dispersibility properties | Not dispersed in water. |

Section 10. Stability and reactivity

| | |
|---|--|
| Stability | This product is normally stable, but can become unstable at elevated temperatures and undergo polymerization, which could produce heat and fumes resulting in over-pressurization and rupture in a closed container. |
| Instability temperature | >170°F (77°C) |
| Conditions of instability | Heat. |
| Incompatibility with various substances | Polymerizes in the presence of organic peroxides, oxidizing materials, or heat. |
| Corrosivity | Our database contains no additional remark on the corrosivity of this product |

Section 11. Toxicological information

| Toxicity to animals | Name | Result | Species | Dose | Exposure |
|--|---|---------------------------------------|------------|--------------------------|--------------|
| | Styrene | LD50 Oral LC50 Inhalation Vapor | Rat Rat | 2650 mg/kg 5634.2 ppm | - 4 hours |
| Special remarks on toxicity to animals | Lung effects have been observed in mouse studies following repeated exposure. | | | | |
| Special remarks on chronic effects on humans | No additional remark. | | | | |
| Special remarks on other toxic effects on humans | No additional remark. | | | | |

Section 12. Ecological information

| | |
|-------------|--|
| Ecotoxicity | Toxic to aquatic organisms. Should not be released to sewage system or other bodies of water at concentrations above limits established in regulations or permits. |
|-------------|--|

Section 13. Disposal considerations

| | |
|----------------|--|
| Waste disposal | Recycle to process, if possible. Consult your local or regional authorities. Ignitable characteristic. |
|----------------|--|

Section 14. Transport information

| | | |
|------------------------|--|--------|
| DOT | UN1866; Resin Solution; 3; III. | Labels |
| TDG | UN1866; Resin Solution; 3; III. | |
| IATA/IMDG | IATA: UN1866; Resin Solution; 3; III; Pkg. Inst: Passenger - 309; Cargo - 310 IMDG: UN1866; Resin Solution; 3; III; FP=31°C; EmS No.: F-E, S-E | |
| Additional information | US regulations require the reporting of spills when the amount exceeds the Reportable Quantity (RQ) for specific components of this material. See CERCLA in Section 15, Regulatory Information, for the Reportable Quantities. | |

Section 15. Regulatory information

| | |
|-------------------|---|
| Other regulations | This section does not reference all applicable regulatory compliance lists. TSCA: All ingredients are listed or compliant with TSCA. DSL: All ingredients are listed or compliant with the NSNR. Proposition 65 Warning: This product contains a chemical(s) known to the State of California to cause cancer, birth defects and/or reproductive harm. SARA 302 component(s): None. SARA 313 component(s): Styrene. CERCLA(RQ): Styrene - 1000 lbs. (453.6 kg) |
|-------------------|---|

Section 16. Other information

Prepared by AOC, LLC - Corporate Regulatory Affairs. FL

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The information contained in this data sheet is furnished in good faith and without warranty, representation, or inducement or license of any kind, except that it is accurate to the best of AOC, LLC's knowledge, or was obtained from sources believed by AOC, LLC to be reliable. The accuracy, adequacy or completeness of health and safety precautions set forth herein cannot be guaranteed, and the buyer is solely responsible for ensuring that the product is used, handled, stored, and disposed of safely and in compliance with applicable federal, state or provincial, and local laws. AOC, LLC disclaims liability for any loss, damage or personal injury that arises from, or is in any way related to, use of the information contained in this data sheet.

ATTACHMENT F

STACK TEST REPORT BY ANALYTICAL TESTING

CONSULTANTS

STYRENE DESTRUCTION EFFICIENCY TESTING
ON A REGENERATIVE THERMAL OXIDIZERS (RTO)
AND STYRENE EMISSIONS FROM A BAGHOUSE



E-Stone USA
Corporation

**420 Haywood Taylor Boulevard
Sebring, Florida 33870**

(863) 655-1273 Plant Telephone Number

(863) 655-1309 Plant Facsimile Number

Test Date-December 9, 2008



Providing Quality Air Testing and Consulting Services Since 1981.

ATC Project Number P-8192

Testing Conducted for:

Mr. Bruno Ferraro, C.E.P., Q.E.P.
Grove Scientific and Engineering
Orlando, Florida

ANALYTICAL TESTING CONSULTANTS, INC.

301 Brookdale Street
Kannapolis, N. C. 28083
(704) 932-3193 phone
(704) 932-0570 facsimile
(800) 733-3193 toll-free

corp@atc-net.net e-mail
www.atc-net.net Web site

Distribution:
Mr. Bruno Ferraro
(One copy)

Issue Date:
January 8, 2009



Accreditation limited to LELAP Scope



Certificate #04044 Expiration Date 6/30/09

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INTRODUCTION

This report presents the results of styrene destruction/removal efficiency (DRE) testing performed on a Regenerative Thermal Oxidizer (RTO) at E-Stone USA in Sebring, Florida. Styrene emissions were also continuously monitored on a baghouse exhaust.

The purpose of this test was to determine styrene inlet mass loading and mass emission rate of the RTO and also calculate destruction/removal efficiencies from the acquired data as required in the facility permit no. 0550049-001-AC.

ANALYTICAL TESTING CONSULTANTS, INC. of Kannapolis, North Carolina conducted the testing and associated measurements. Members of the ATC test team were Bill Kissel, Flavel Smith, James Roberts and Kent Childers.

CERTIFICATION OF RESULTS

"I certify under penalty of law that I believe the information provided in this document is true, accurate and complete. I am aware that there are significant civil and criminal penalties, including the possibility of fine or imprisonment or both, for submitting false, inaccurate or incomplete information."

W. Keith Poole 1/7/09
Signature/Date

W. Keith Poole

Technical Director
Test Report Preparation

Bill Kissel 1/7/09
Signature/Date

William G. "Bill" Kissel

President
On-site Supervisor/Report Review

Results Summary of Gaseous Emissions Testing

| | |
|-----------|--------------------------|
| Client: | E-Stone/Grove Scientific |
| Location: | Sebring, Florida |
| Date: | 12/09/08 |

| <u>General Stack Parameters</u> | <u>Run #1</u> | <u>Run #2</u> | <u>Run #3</u> | <u>Average</u> |
|---|---------------|---------------|---------------|----------------|
| <i>Run Times-</i> | | | | |
| Start | 10:15 AM | 11:55 AM | 2:05 PM | |
| End | 11:15 AM | 12:55 PM | 3:05 PM | |
| <u>RTO Inlet</u> | | | | |
| Stack Velocity, feet per second | 31.62 | 33.15 | 31.73 | 32.17 |
| Actual Volumetric Air Flow Rate, cubic feet per minute | 3,541 | 3,712 | 3,554 | 3,602 |
| Stack moisture, percent | 2.96 | 2.41 | 2.72 | 2.70 |
| Stack temperature, degrees F | 104.44 | 111.50 | 112.31 | 109.4 |
| Standard Volumetric Air Flow Rate, cubic feet per minute | 3,222 | 3,354 | 3,196 | 3,257 |
| <u>RTO Exhaust</u> | | | | |
| Stack Velocity, feet per second | 39.97 | 40.98 | 42.46 | 41.14 |
| Actual Volumetric Air Flow Rate, cubic feet per minute | 6,622 | 6,789 | 7,034 | 6,815 |
| Stack moisture, percent | 1.68 | 1.38 | 2.93 | 2.00 |
| Stack temperature, degrees F | 238.94 | 218.13 | 224.44 | 227.2 |
| Standard Volumetric Air Flow Rate, cubic feet per minute | 4,939 | 5,235 | 5,290 | 5,155 |
| Oxygen Concentration, percent (corrected per 7e-5b) | 20.41 | 20.70 | 20.37 | 20.49 |
| Carbon Dioxide concentration, percent (corrected per 7e-5b) | 0.04 | 0.08 | 0.16 | 0.09 |
| <u>Baghouse Exhaust</u> | | | | |
| Stack Velocity, feet per second | 47.75 | 46.77 | 45.52 | 46.68 |
| Actual Volumetric Air Flow Rate, cubic feet per minute | 16,506 | 16,166 | 15,733 | 16,135 |
| Stack moisture, percent | 2.61 | 2.44 | 2.61 | 2.55 |
| Stack temperature, degrees F | 88.63 | 88.94 | 94.44 | 90.7 |
| Standard Volumetric Air Flow Rate, cubic feet per minute | 15,538 | 15,236 | 14,655 | 15,143 |

Results Summary of Gaseous Emissions Testing

| | |
|-----------|--------------------------|
| Client: | E-Stone/Grove Scientific |
| Location: | Sebring, Florida |
| Date: | 12/9/2008 |

| <u>Measured Gaseous Pollutants</u> | <u>Run #1</u> | <u>Run #2</u> | <u>Run #3</u> | <u>Average</u> |
|---|---------------|---------------|---------------|----------------|
| <u>Volatile Organic Compounds</u> | | | | |
| RTO Inlet | | | | |
| VOC, ppm as calibration gas v/v dry basis | 436.46 | 434.17 | 424.79 | 431.81 |
| VOC, ppm as styrene, v/v dry basis | 142.90 | 142.15 | 139.08 | 141.38 |
| VOC, lbs/hr as styrene | 7.48 | 7.74 | 7.22 | 7.48 |
| VOC, lbs/hr as carbon | 2.63 | 2.73 | 2.67 | 2.68 |
| Baghouse Exhaust | | | | |
| VOC, ppm as calibration gas v/v dry basis | 67.27 | 84.03 | 80.99 | 77.43 |
| VOC, ppm as styrene, v/v dry basis | 21.35 | 26.67 | 25.71 | 24.58 |
| VOC, lbs/hr as styrene | 5.39 | 6.60 | 6.12 | 6.03 |
| VOC, lbs/hr as carbon | 1.96 | 2.40 | 2.22 | 2.19 |
| Annual Potential Uncontrolled VOC emissions (as carbon-8,760 hour basis)-includes RTO inlet and Baghouse Exhaust | | | | 21.34 |
| RTO Exhaust | | | | |
| VOC, ppm as calibration gas v/v dry basis | 3.60 | 3.39 | 5.23 | 4.07 |
| VOC, ppm as styrene, v/v dry basis | 1.19 | 1.12 | 1.73 | 1.35 |
| VOC, lbs/hr as styrene | 0.06 | 0.06 | 0.09 | 0.07 |
| VOC, lbs/hr as carbon | 0.03 | 0.03 | 0.05 | 0.04 |
| Annual Potential Controlled VOC emissions (as carbon-8,760 hour basis)-includes RTO Exhaust and Baghouse Exhaust | | | | 9.77 |

Removal Efficiency Calculations

| | Inlet, lbs/hr Styrene | Outlet, lbs/hr Styrene | DRE, % |
|--------|--------------------------|---------------------------|--------|
| Run #1 | 7.48 | 0.06 | 99.17% |
| Run #2 | 7.74 | 0.06 | 99.21% |
| Run #3 | 7.22 | 0.09 | 98.76% |
| | | Average | 99.04% |

22.44
 21
 - 22.23

RESULTS, CONCLUSIONS AND COMMENTS

Results from the destruction efficiency testing are presented in the preceding test summaries. Additional information can be reviewed in the Calculations and Appendix sections of this report.

RTO Inlet

Mean velocity measurements on the eighteen (18) inch round diameter inlet stack were 32.16 feet per second (ft/s). This yielded a mean actual volumetric flow rate of 3,602 cubic feet per minute (acfm). A resultant mean standard flow rate of 3,257 scfm was utilized for calculation of inlet loading.

US EPA method 25a continuous emission monitoring results indicated a mean VOC concentration of 431.8 parts per million as propane (the calibration gas) dry basis. Upon conversion to styrene utilizing the generated response factor, a mean concentration of 141.38 ppm as styrene was calculated. This yields a styrene loading rate on the inlet to the RTO at 7.48 lbs/hr (2.68 lbs/hr as carbon).

RTO Outlet

Mean velocity measurements on the twenty-two point five (22.5) inch diameter round outlet stack were 41.14 feet per second (ft/s). This yielded a mean actual volumetric flow rate of 6,815 cubic feet per minute (acfm). A resultant mean standard flow rate of 5,155 scfm was utilized for calculation of VOC emissions.

US EPA method 25a continuous emission monitoring results indicated a mean VOC concentration of 4.1 parts per million as propane (the calibration gas) dry basis. This is the equivalent of 1.35 ppm as styrene which yields an RTO mass emission rate of 0.07 lbs-styrene/hr (0.04 lbs-carbon/hr).

The destruction/removal efficiency, based on these results, is 99.04%.

Baghouse Exhaust

Mean velocity measurements on the thirty-two point five (22.5) inch diameter round baghouse outlet stack were 46.68 feet per second (ft/s). This yielded a mean actual volumetric flow rate of 16,135 cubic feet per minute (acfm). A resultant mean standard flow rate of 15,143 scfm was utilized for calculation of VOC emissions.

US EPA method 25a continuous emission monitoring results indicated a mean VOC concentration of 77.4 parts per million as propane (the calibration gas) dry basis. This is the equivalent of 24.6 ppm as styrene which yields a baghouse mass emission rate of 6.0 lbs-styrene/hr (2.19 lbs-carbon/hr).

SAMPLING AND ANALYTICAL PROCEDURES

Volatile organic compound emissions testing were performed according to procedures developed by the U. S. Environmental Protection Agency (US EPA) and referred to as Method 25a.

Sampling port locations and number of test points to be used were determined according to US EPA Method 1. Gas sampling and analysis for oxygen content were performed in accordance with US EPA Method 3a on the RTO exhaust. A dry, molecular weight of 29.0 was assigned to the RTO inlet stack gas and baghouse exhaust.

Flows were performed according to US EPA method 2 on all ducts and moistures by US EPA method 4, reference method on the RTO exhaust. Moisture was calculated for the RTO inlet and baghouse exhaust ducts by determining wet bulb/dry bulb temperatures. This data was collected for each Method 25a run. Prior to each moisture run, the sampling trains were leak-checked according to optional procedures outlined in method four. The inlet to the first impinger was plugged and a vacuum of 15" was pulled. Each train had a preliminary leak-check of less than 0.02 cfm. After reconnecting the probe, the runs were started. Prior to each traverse, the pitot tubes were also successfully leak-checked according to established procedures in US EPA method 2.

US EPA method 25a was conducted utilizing dual heated flame ionization detectors. US EPA method 205 (40CFR51, appendix M) was utilized in conjunction with an Environics 2020 gas dilution system, high purity nitrogen, and protocol gases of 20.9% and 10.50% oxygen, balance nitrogen to verify the dilution system prior to full step-down calibrations of the FIDs. Method 205 stipulates that the analyzer of choice (ATC utilizes a Servomex 1400B) must be successfully calibrated according to the appropriate reference method (3a). Once the Servomex was successfully calibrated, the gas in the 20.9% cylinder was diluted with nitrogen utilizing the Environics to post dilution levels of 2.5% and 10.0%. These dilutions were injected into the Servomex in triplicate and responses recorded on a DILUTION SYSTEM VERIFICATION form. Following this demonstration of the accuracy of the dilution system, the heated FIDs were calibrated by diluting a US EPA protocol mixture of 10,110 ppm propane in air with nitrogen to inlet levels of 1000, 500, and 250 parts per million with a span value of 1100 parts per million. The outlet analyzer was calibrated to a span value of 110 ppm with a high range of 100, mid range of 50, and low range of 25 parts per million. The baghouse analyzer was calibrated to a span value of 330 ppm with a high range of 300 ppm, a mid-range of 150 ppm and a low range of 75 ppm. All pre- and post-test calibration errors may be viewed on ATC form 18 and also as reflected on the raw test data.

Three one-hour instrumental sampling runs were conducted on the inlet and exhaust of each RTO. Immediately following each sampling period, zero and mid-level gases were introduced to the appropriate analyzer and responses recorded. Post-test calibrations included the intermediate level most closely matching the measured concentrations (in addition to zero gas). All calibrations were within specification.

SAMPLING AND ANALYTICAL PROCEDURES (continued)

Styrene Response Factors

Styrene response factors were generated for each analyzer by introducing a concentration of 49.2 ppm styrene and determining the response. Results were as below:

| Response Factor Summary | | | | | | |
|-------------------------|---------------------|---------------------|---------------------|---------------------|--------------------|---------|
| | VOC 1 11/10/2008 | VOC 1 11/11/2008 | VOC 2 11/10/2008 | VOC 2 11/11/2008 | VOC 3 12/9/2008 | Average |
| PPM C3 | 147.912 | 149.436 | 160.413 | 149.963 | 150.256 | 151.596 |
| Styrene Conc. | 49.2 | 49.2 | 49.2 | 49.2 | 49.2 | 49.2 |
| ppm C3/C8H8 | 3.006 | 3.037 | 3.260 | 3.048 | 3.054 | 3.08122 |
| ppm C8H8/C3 | 0.3326 | 0.3292 | 0.3067 | 0.3281 | 0.3274 | 0.32482 |
| | VOC 1 RF | 0.3309 | | | | |
| | VOC 2 RF | 0.3174 | | | | |
| | VOC 3 RF | 0.3274 | | | | |

The above response factors were utilized in converting the instrument responses to a styrene basis.

Project Sampling Issues

Testing was completed according to the test plan submitted and approved. No deviations were necessary to accomplish sampling.

QA/QC Procedures

The following QA/QC steps were taken in preparing this report and reviewing the accompanying data.

- 1) All raw field data computer entry was re-checked for errors against the field data sheets,
- 2) All field data sheets were checked for completeness, accuracy, legibility, specifications, reasonableness and signatures.
- 3) All CEM raw data was reviewed, all calibration data was verified against

SAMPLING AND ANALYTICAL PROCEDURES

(continued)

calibration records and raw data compared to entries on ATC Form 18s.

- 4) Post-test calibrations were performed on all manual sampling equipment to method specifications and were within acceptable ranges.
- 5) All pre-and post-test on-site CEM calibrations were within method specifications. Oxygen and carbon dioxide measurements were adjusted for drift per equation 7e-5b of method 7e.
- 6) The assembled report was proof-read by the QA/QC officer prior to submittal to the client.

REFERENCES

1. CODE OF FEDERAL REGULATIONS, Title 40, Part 60, Appendix A, July 1, 2008.

CALCULATIONS

Air Flow Calculations

Supporting Measurements

VOC Data

Sample Calculations

Nomenclature

Calculation Formulae

FLOW CALCULATIONS

CLIENT: E-Stone/Grove Scientific
LOCATION: Sebring, FL

| Run # | 1-In | 2-In | 3-In | 1-Bag | 2-Bag | 3-Bag |
|------------------------|----------|-----------|----------|----------|----------|----------|
| SOURCE | | RTO Inlet | | | | |
| DATE | 12/09/08 | 12/09/08 | 12/09/08 | 12/09/08 | 12/09/08 | 12/09/08 |
| Avg DH (in H2O) | 0 | 0 | 0 | 0 | 0 | 0 |
| P ATM (in HG) | 30.05 | 30.05 | 30.05 | 30.05 | 30.05 | 30.05 |
| PM (in HG) | 30.05 | 30.05 | 30.05 | 30.05 | 30.05 | 30.05 |
| PS (Gauge) | -1.10 | -1.20 | -1.10 | -0.25 | -0.24 | -0.25 |
| PS (in HG) | 29.97 | 29.96 | 29.97 | 30.03 | 30.03 | 30.03 |
| %M | 2.956 | 2.412 | 2.724 | 2.607 | 2.441 | 2.607 |
| MD | 0.970 | 0.976 | 0.973 | 0.974 | 0.976 | 0.974 |
| MWD | 29.0 | 29.0 | 29.0 | 29.0 | 29.0 | 29.0 |
| M | 28.675 | 28.735 | 28.700 | 28.713 | 28.731 | 28.713 |
| tS (deg F) | 104.4375 | 111.5 | 112.3125 | 88.625 | 88.9375 | 94.4375 |
| TS (deg R) | 564.1075 | 571.17 | 571.9825 | 548.295 | 548.6075 | 554.1075 |
| SUM SQRT DP | 8.6953 | 9.0679 | 8.6696 | 13.3442 | 13.0703 | 12.6525 |
| N DP | 16 | 16 | 16 | 16 | 16 | 16 |
| Avg SQRT DP | 0.5435 | 0.5667 | 0.5419 | 0.8340 | 0.8169 | 0.7908 |
| CP | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 | 0.84 |
| VS (ft/sec) | 31.62 | 33.15 | 31.73 | 47.75 | 46.77 | 45.52 |
| DS (in) | 18.5 | 18.5 | 18.5 | 32.5 | 32.5 | 32.5 |
| AS (ft2) | 1.867 | 1.867 | 1.867 | 5.761 | 5.761 | 5.761 |
| QS, ACFM | 3,541 | 3,712 | 3,554 | 16,506 | 16,166 | 15,733 |
| Q STD (ft3/min) | 3,320 | 3,437 | 3,286 | 15,954 | 15,617 | 15,048 |
| Q STD DRY, SCFM | 3,222 | 3,354 | 3,196 | 15,538 | 15,236 | 14,655 |

Volumetric Airflow Rate and Stack Moisture Determination

LOCATION: E-Stone/Grove
SOURCE: RTO Exhaust

| | DATA | Run #1 | Run #2 | Run #3 | AVERAGE |
|---|-------------|---------------|---------------|---------------|----------------|
| Test Date | 12/09/08 | 12/09/08 | 12/09/08 | | |
| Run Time (min) | 60.00 | 60.00 | 60.00 | | |
| Average orifice reading (inches H₂O) | 2.00 | 2.00 | 2.00 | | |
| Barometric pressure (inches Hg) | 30.05 | 30.05 | 30.05 | | |
| Absolute meter pressure (inches Hg) | 30.20 | 30.20 | 30.20 | | |
| Stack static pressure (inches H₂O) | -0.26 | -0.22 | -0.22 | | |
| Absolute stack pressure (inches H₂O) | 30.03 | 30.03 | 30.03 | | |
| Meter temperature (F) | 66.42 | 78.08 | 83.62 | | |
| Meter temperature (R) | 526.09 | 537.75 | 543.29 | | |
| Dry gas meter sample volume (ft³) | 48.24 | 49.50 | 49.68 | | |
| Standard sample volume (ft³) | 47.00 | 47.19 | 46.88 | | |
| Volume of liquid collected (ml) | 17.00 | 14.00 | 30.00 | | |
| Water vapor volume, std (ft³) | 0.80 | 0.66 | 1.41 | | |
| Total standard sample volume (ft³) | 47.81 | 47.85 | 48.29 | | |
| Percent moisture | 1.68 | 1.38 | 2.93 | | 1.99 |
| % Moisture @ 100% saturation¹ | 100.00 | 100.00 | 100.00 | | |
| Mole fraction of the dry gas | 0.983 | 0.986 | 0.971 | | |
| Molecular weight of the dry gas | 28.82 | 28.84 | 28.84 | | |
| Molecular weight of the wet gas | 28.64 | 28.69 | 28.52 | | |
| Stack temperature (F) | 238.94 | 218.13 | 224.44 | | 227.17 |
| Stack temperature (Rankine) | 698.61 | 677.80 | 684.11 | | 686.84 |
| Sum of the square roots of delta Ps | 9.88 | 10.29 | 10.59 | | |
| Number of data points | 16.00 | 16.00 | 16.00 | | |
| Average square root of delta P | 0.62 | 0.64 | 0.66 | | |
| Pitot tube coefficient | 0.84 | 0.84 | 0.84 | | |
| Stack velocity (ft/s) | 39.97 | 40.98 | 42.46 | | 41.14 |
| Diameter of the stack (inches) | 22.50 | 22.50 | 22.50 | | |
| Area of the stack (ft²) | 2.76 | 2.76 | 2.76 | | |
| Actual stack volumetric flow rate (ft³/min) | 6,622 | 6,789 | 7,034 | | 6,815 |
| Stack volumetric flow, standard wet (ft³/min) | 5,024 | 5,309 | 5,450 | | 5,261 |
| Stack volumetric flow, standard dry (ft³/min) | 4,939 | 5,235 | 5,290 | | 5,155 |
| %Carbon Dioxide | 0.04 | 0.08 | 0.16 | | 0.09 |
| % Oxygen | 20.41 | 20.70 | 20.37 | | 20.49 |
| % Carbon Monoxide | 0.00 | 0.00 | 0.00 | | |
| % Nitrogen | 79.55 | 79.22 | 79.47 | | |

¹ The % Moisture at 100% saturation is the theoretical amount of moisture the stack gas can hold at the measured stack temperature. If the measured moisture is greater than the calculated level, the mole fraction will be calculated using the saturation level.

Individual Velocity Head Readings
RTO Inlet

| Point No. | Run # | 1-in | |
|-----------|--------|---------|-----|
| | dP | sqrt dP | Ts |
| A1 | 0.290 | 0.5385 | 108 |
| A2 | 0.340 | 0.5831 | 107 |
| A3 | 0.380 | 0.6164 | 107 |
| A4 | 0.370 | 0.6083 | 107 |
| A5 | 0.330 | 0.5745 | 107 |
| A6 | 0.300 | 0.5477 | 105 |
| A7 | 0.310 | 0.5568 | 104 |
| A8 | 0.280 | 0.5292 | 100 |
| | | | |
| B1 | 0.260 | 0.5099 | 104 |
| B2 | 0.320 | 0.5657 | 105 |
| B3 | 0.310 | 0.5568 | 105 |
| B4 | 0.250 | 0.5000 | 106 |
| B5 | 0.280 | 0.5292 | 105 |
| B6 | 0.240 | 0.4899 | 101 |
| B7 | 0.230 | 0.4796 | 100 |
| B8 | 0.260 | 0.5099 | 100 |
| | | | |
| | 8.6953 | 104.4 | |

| Point No. | Run # | 2-in | |
|-----------|--------|---------|-----|
| | dP | sqrt dP | Ts |
| A1 | 0.340 | 0.5831 | 111 |
| A2 | 0.350 | 0.5916 | 112 |
| A3 | 0.340 | 0.5831 | 111 |
| A4 | 0.330 | 0.5745 | 113 |
| A5 | 0.300 | 0.5477 | 113 |
| A6 | 0.290 | 0.5385 | 113 |
| A7 | 0.340 | 0.5831 | 108 |
| A8 | 0.320 | 0.5657 | 108 |
| | | | |
| B1 | 0.290 | 0.5385 | 111 |
| B2 | 0.400 | 0.6325 | 112 |
| B3 | 0.380 | 0.6164 | 112 |
| B4 | 0.340 | 0.5831 | 112 |
| B5 | 0.350 | 0.5916 | 112 |
| B6 | 0.290 | 0.5385 | 112 |
| B7 | 0.250 | 0.5000 | 112 |
| B8 | 0.250 | 0.5000 | 112 |
| | | | |
| | 9.0679 | 111.5 | |

| Point No. | Run # | 3-in | |
|-----------|--------|---------|-----|
| | dP | sqrt dP | Ts |
| A1 | 0.340 | 0.5831 | 113 |
| A2 | 0.350 | 0.5916 | 113 |
| A3 | 0.330 | 0.5745 | 113 |
| A4 | 0.320 | 0.5657 | 113 |
| A5 | 0.300 | 0.5477 | 113 |
| A6 | 0.280 | 0.5292 | 113 |
| A7 | 0.270 | 0.5196 | 113 |
| A8 | 0.260 | 0.5099 | 113 |
| | | | |
| B1 | 0.310 | 0.5568 | 111 |
| B2 | 0.340 | 0.5831 | 111 |
| B3 | 0.330 | 0.5745 | 112 |
| B4 | 0.330 | 0.5745 | 112 |
| B5 | 0.240 | 0.4899 | 112 |
| B6 | 0.240 | 0.4899 | 112 |
| B7 | 0.240 | 0.4899 | 113 |
| B8 | 0.240 | 0.4899 | 110 |
| | | | |
| | 8.6696 | 112.3 | |

Individual Velocity Head Readings
Baghouse Exhaust

| Point No. | Run # | 1-Bag | |
|-----------|-------|---------|----|
| | dP | sqrt dP | Ts |
| A1 | 0.530 | 0.7280 | 88 |
| A2 | 0.690 | 0.8307 | 89 |
| A3 | 0.830 | 0.9110 | 89 |
| A4 | 0.900 | 0.9487 | 89 |
| A5 | 0.890 | 0.9434 | 89 |
| A6 | 0.870 | 0.9327 | 89 |
| A7 | 0.890 | 0.9434 | 89 |
| A8 | 0.870 | 0.9327 | 89 |
| | | | |
| B1 | 0.550 | 0.7416 | 88 |
| B2 | 0.580 | 0.7616 | 88 |
| B3 | 0.590 | 0.7681 | 88 |
| B4 | 0.580 | 0.7616 | 88 |
| B5 | 0.570 | 0.7550 | 88 |
| B6 | 0.580 | 0.7616 | 89 |
| B7 | 0.620 | 0.7874 | 89 |
| B8 | 0.700 | 0.8367 | 89 |
| 13.3442 | | 88.6 | |

| Point No. | Run # | 2-Bag | |
|-----------|-------|---------|----|
| | dP | sqrt dP | Ts |
| A1 | 0.440 | 0.6633 | 89 |
| A2 | 0.510 | 0.7141 | 88 |
| A3 | 0.530 | 0.7280 | 89 |
| A4 | 0.560 | 0.7483 | 89 |
| A5 | 0.720 | 0.8485 | 89 |
| A6 | 0.770 | 0.8775 | 89 |
| A7 | 0.780 | 0.8832 | 89 |
| A8 | 0.800 | 0.8944 | 89 |
| | | | |
| B1 | 0.460 | 0.6782 | 89 |
| B2 | 0.550 | 0.7416 | 89 |
| B3 | 0.760 | 0.8718 | 89 |
| B4 | 0.800 | 0.8944 | 89 |
| B5 | 0.800 | 0.8944 | 90 |
| B6 | 0.790 | 0.8888 | 90 |
| B7 | 0.760 | 0.8718 | 88 |
| B8 | 0.760 | 0.8718 | 88 |
| 13.0703 | | 88.9 | |

| Point No. | Run # | 3-Bag | |
|-----------|-------|---------|----|
| | dP | sqrt dP | Ts |
| A1 | 0.46 | 0.6782 | 95 |
| A2 | 0.55 | 0.7416 | 95 |
| A3 | 0.57 | 0.7550 | 95 |
| A4 | 0.59 | 0.7681 | 94 |
| A5 | 0.64 | 0.8000 | 94 |
| A6 | 0.65 | 0.8062 | 94 |
| A7 | 0.65 | 0.8062 | 94 |
| A8 | 0.65 | 0.8062 | 94 |
| | | | |
| B1 | 0.5 | 0.7071 | 94 |
| B2 | 0.57 | 0.7550 | 94 |
| B3 | 0.6 | 0.7746 | 94 |
| B4 | 0.71 | 0.8426 | 94 |
| B5 | 0.74 | 0.8602 | 95 |
| B6 | 0.71 | 0.8426 | 94 |
| B7 | 0.72 | 0.8485 | 95 |
| B8 | 0.74 | 0.8602 | 96 |
| 12.6525 | | 94.4 | |

ISOKINETIC DATA AND CALCULATIONS

DATE 12/09/08
SOURCE RTO Exhaust

Run #1

| POINT # | T_m | T_s | d_p | SQRT DP |
|----------------|----------------------|----------------------|----------------------|----------------|
| A1 | 59 | 217 | 0.10 | 0.316 |
| A2 | 61 | 218 | 0.38 | 0.616 |
| A3 | 63 | 222 | 0.52 | 0.721 |
| A4 | 63 | 226 | 0.54 | 0.735 |
| A5 | 64 | 229 | 0.46 | 0.678 |
| A6 | 66 | 238 | 0.41 | 0.640 |
| A7 | 68 | 240 | 0.35 | 0.592 |
| A8 | 68 | 236 | 0.12 | 0.346 |
| A9 | 70 | | | |
| A10 | 70 | | | |
| A11 | 72 | | | |
| A12 | 73 | | | |
| B1 | | 236 | 0.47 | 0.686 |
| B2 | | 239 | 0.50 | 0.707 |
| B3 | | 250 | 0.50 | 0.707 |
| B4 | | 259 | 0.51 | 0.714 |
| B5 | | 263 | 0.47 | 0.686 |
| B6 | | 271 | 0.39 | 0.624 |
| B7 | | 250 | 0.33 | 0.574 |
| B8 | | 229 | 0.29 | 0.539 |
| B9 | | | | |
| B10 | | | | |
| B11 | | | | |
| B12 | | | | |

66.42 238.94 9.882

| | | |
|---------------------------|--------------|--------------|
| Vm(ft³) | Initial | 401.37 |
| | Final | 449.61 |
| | Total | 48.24 |

| | |
|---|-------|
| Station Pressure, inches Hg | 30.05 |
| Delta H for run, inches H₂O | 2.00 |
| Stack Static Pressure, inches H₂O | -0.26 |
| Module Calibration Coefficient | 0.962 |
| Pitot Tube Coefficient | 0.84 |
| Stack Diameter, inches | 22.5 |
| Percent Oxygen | 20.41 |
| Percent Carbon Dioxide | 0.04 |
| Percent Carbon Monoxide | 0 |
| Percent Nitrogen | 79.55 |

ISOKINETIC DATA AND CALCULATIONS

DATE 12/09/08
SOURCE RTO Exhaust

Run #2

| POINT # | T _m | T _s | d _p | SQRT DP |
|---------|----------------|----------------|----------------|---------|
| A1 | 75 | 241 | 0.54 | 0.735 |
| A2 | 75 | 225 | 0.53 | 0.728 |
| A3 | 76 | 220 | 0.51 | 0.714 |
| A4 | 76 | 220 | 0.49 | 0.700 |
| A5 | 77 | 221 | 0.46 | 0.678 |
| A6 | 78 | 227 | 0.37 | 0.608 |
| A7 | 78 | 226 | 0.35 | 0.592 |
| A8 | 79 | 220 | 0.32 | 0.566 |
| A9 | 80 | 227 | | |
| A10 | 80 | 212 | | |
| A11 | 81 | 209 | | |
| A12 | 82 | 209 | | |
| B1 | | 210 | 0.42 | 0.648 |
| B2 | | 211 | 0.44 | 0.663 |
| B3 | | 212 | 0.45 | 0.671 |
| B4 | | 200 | 0.44 | 0.663 |
| B5 | | | 0.40 | 0.632 |
| B6 | | | 0.35 | 0.592 |
| B7 | | | 0.32 | 0.566 |
| B8 | | | 0.29 | 0.539 |
| B9 | | | | |
| B10 | | | | |
| B11 | | | | |
| B12 | | | | |

78.08 218.13 10.295

| | | |
|--------------------------------------|--------------|--------------|
| V_m(ft³) | Initial | 450.14 |
| | Final | 499.64 |
| | Total | 49.50 |

| | |
|---|-------|
| Station Pressure, inches Hg | 30.05 |
| Delta H for run, inches H₂O | 2 |
| Stack Static Pressure, inches H₂O | -0.22 |
| Module Calibration Coefficient | 0.962 |
| Pitot Tube Coefficient | 0.84 |
| Stack Diameter, inches | 22.5 |
| Percent Oxygen | 20.7 |
| Percent Carbon Dioxide | 0.08 |
| Percent Carbon Monoxide | 0 |
| Percent Nitrogen | 79.22 |

ISOKINETIC DATA AND CALCULATIONS

DATE 12/09/08
SOURCE RTO Exhaust

Run #3

| POINT # | T_m | T_s | d_p | SQRT DP |
|----------------|----------------------|----------------------|----------------------|----------------|
| A1 | 82 | 260 | 0.62 | 0.787 |
| A2 | 81 | 227 | 0.53 | 0.728 |
| A3 | 81 | 218 | 0.52 | 0.721 |
| A4 | 82 | 215 | 0.50 | 0.707 |
| A5 | 83 | 215 | 0.46 | 0.678 |
| A6 | 83 | 215 | 0.40 | 0.632 |
| A7 | 84 | 215 | 0.33 | 0.574 |
| A8 | 84 | 211 | 0.29 | 0.539 |
| A9 | 85 | | | |
| A10 | 85 | | | |
| A11 | 85 | | | |
| A12 | 86 | | | |
| B1 | 86 | 235 | 0.35 | 0.592 |
| B2 | | 225 | 0.41 | 0.640 |
| B3 | | 226 | 0.44 | 0.663 |
| B4 | | 225 | 0.45 | 0.671 |
| B5 | | 221 | 0.45 | 0.671 |
| B6 | | 223 | 0.44 | 0.663 |
| B7 | | 227 | 0.44 | 0.663 |
| B8 | | 233 | 0.43 | 0.656 |
| B9 | | | | |
| B10 | | | | |
| B11 | | | | |
| B12 | | | | |

83.62 224.44 10.587

| | | |
|--------------------------------------|--------------|--------------|
| V_m(ft³) | Initial | 499.78 |
| | Final | 549.46 |
| | Total | 49.68 |

| | |
|---|-------|
| Station Pressure, inches Hg | 30.05 |
| Delta H for run, inches H₂O | 2 |
| Stack Static Pressure, inches H₂O | -0.22 |
| Module Calibration Coefficient | 0.962 |
| Pitot Tube Coefficient | 0.84 |
| Stack Diameter, inches | 22.5 |
| Percent Oxygen | 20.37 |
| Percent Carbon Dioxide | 0.16 |
| Percent Carbon Monoxide | 0 |
| Percent Nitrogen | 79.47 |

Modified Carrier Equation for Prediction of Stack Moisture with a Wet Bulb Thermometer

Client: E-Stone/Grove Scientific
City, State: Sebring, FL

| Run # | Pbar, in. Hg | Ps, gauge-in. H2O | Ps, in. Hg | Tdry, deg. F | Tw, deg. F | %Moisture |
|-------|--------------|-------------------|------------|--------------|------------|-----------|
| 1-In | 30.05 | -1.10 | 29.97 | 86.0 | 78.0 | 2.956 |
| 2-In | 30.05 | -1.20 | 29.96 | 98.0 | 77.0 | 2.412 |
| 3-In | 30.05 | -1.10 | 29.97 | 97.0 | 79.0 | 2.724 |
| 1-Bag | 30.05 | -0.25 | 30.03 | 88.0 | 76.0 | 2.607 |
| 2-Bag | 30.05 | -0.24 | 30.03 | 89.0 | 75.0 | 2.441 |
| 3-Bag | 30.05 | -0.25 | 30.03 | 88.0 | 76.0 | 2.607 |

$$\%Water = \left(\frac{100}{P_s} \right) \left[10 \left(6.6912 - \left[\frac{3144}{T_w + 390.86} \right] \right) \right] - (0.0011)(P_s)(T_s - T_w) \left[1 + \frac{T_w - 32}{1571} \right]$$

Where:

Ps=

stack pressure (absolute), inches of mercury

Ts=

stack temperature, degrees F

Tw=

stack wet bulb temperature, degrees F

MOISTURE DATA

RTO Exhaust

12/9/2008

Run #1

| | 1st Imp. | 2nd Imp. | 3rd Imp. | 4th Imp. | TOTALS |
|-----------|----------|----------|----------|----------|--------|
| BEGINNING | 100 | 100 | 0 | 300.0 | |
| ENDING | 110 | 102 | 0 | 305.0 | |
| NET | 10 | 2 | 0 | 5.0 | 17.0 |

Run #2

| | 1st Imp. | 2nd Imp. | 3rd Imp. | 4th Imp. | TOTALS |
|-----------|----------|----------|----------|----------|--------|
| BEGINNING | 100 | 100 | 0 | 300.0 | |
| ENDING | 104 | 100 | 0 | 310.0 | |
| NET | 4 | 0 | 0 | 10.0 | 14 |

Run #3

| | 1st Imp. | 2nd Imp. | 3rd Imp. | 4th Imp. | TOTALS |
|-----------|----------|----------|----------|----------|--------|
| BEGINNING | 100 | 100 | 0 | 300.0 | |
| ENDING | 110 | 105 | 0 | 315.0 | |
| NET | 10 | 5 | 0 | 15.0 | 30 |

VOC Mass Rates and Destruction/Removal Efficiency

E-VOC = MG/M3 * Q STD DRY * 3.75E-06
 WHERE
 E-VOC = VOC EMISSION RATE, LBS/HR AS CARBON
 Q std dry = FLOW RATE DRY SCFM
 MG/M3 = CONCENTRATION OF VOC AS CARBON
 3.75E-06 = 0.0022 LBS/GR*1G/1000MG * 60 MIN/HR * M3/35.31 FT3

| | | | | | |
|-----------|---------------------------------------|--|--|--|--|
| CLIENT: | E-Stone/Grove Scientific | | | | |
| LOCATION: | Sebring, Florida | | | | |
| DATE: | 12/9/2008 | | | | |
| SOURCE: | RTO Inlet/Outlet and Baghouse Exhaust | | | | |

Run One

| | Unit Concentration | | Mass Rate, lbs/hr | | |
|------------|--|--|------------------------------|------------|-----------|
| | ppmv _w as C ₆ H ₆ | ppmv _d as C ₆ H ₆ | ppmv _d as Styrene | as styrene | as carbon |
| RTO Inlet | 423.56 | 436.46 | 142.90 | 7.48 | 2.63 |
| RTO Outlet | 3.54 | 3.60 | 1.19 | 0.06 | 0.03 |
| Baghouse | 65.52 | 67.27 | 21.35 | 5.39 | 1.96 |

Run Two

| | Unit Concentration | | Mass Rate, lbs/hr | | |
|------------|--|--|------------------------------|------------|-----------|
| | ppmv _w as C ₆ H ₆ | ppmv _d as C ₆ H ₆ | ppmv _d as Styrene | as styrene | as carbon |
| RTO Inlet | 423.70 | 434.17 | 142.15 | 7.74 | 2.73 |
| RTO Outlet | 3.35 | 3.39 | 1.12 | 0.06 | 0.03 |
| Baghouse | 81.98 | 84.03 | 26.67 | 6.60 | 2.40 |

Run Three

| | Unit Concentration | | Mass Rate, lbs/hr | | |
|------------|--|--|------------------------------|------------|-----------|
| | ppmv _w as C ₆ H ₆ | ppmv _d as C ₆ H ₆ | ppmv _d as Styrene | as styrene | as carbon |
| RTO Inlet | 413.22 | 424.79 | 139.08 | 7.22 | 2.67 |
| RTO Outlet | 5.08 | 5.23 | 1.73 | 0.09 | 0.05 |
| Baghouse | 78.88 | 80.99 | 25.71 | 6.12 | 2.22 |

Removal Efficiency Calculations

| | Inlet, lbs/hr styrene | Outlet, lbs/hr styrene | DRE, % |
|---------|-----------------------|------------------------|--------|
| Run #1 | 7.48 | 0.06 | 99.17% |
| Run #2 | 7.74 | 0.06 | 99.21% |
| Run #3 | 7.22 | 0.09 | 98.76% |
| Average | | | 99.04% |

Sample Calculations

1) Calculation of average VOC concentration as propane wet

= mean logged reading as propane wet for the one hour run.
Run #1 RTO Inlet 423.56

2) Convert ppmv C₃H₈ wet to dry by dividing the concentration by the mole fraction of the dry gas.

| | MD | ppmv dry as C ₃ H ₈ |
|------------------|-------|---|
| Run #1 RTO Inlet | 0.970 | 436.46 |

3) Convert to ppmvd as styrene by multiplying by the response factor for the inlet FID.

| | RF (ppm C ₈ H ₈ /ppm C ₃ H ₈) | ppmv dry as styrene |
|------------------|--|---------------------|
| Run #1 RTO Inlet | 0.3274 | 142.90 |

4) Convert ppmv to mg/m³ at STP

(Equation F-1 in EPA Course 450-Source Sampling for Particulate Pollutants")

$$\frac{mg}{dscm} = \frac{10^3 mg}{g} \times \frac{ppm \times MW \left(\frac{g}{g - mole} \right)}{22.414 \frac{liters}{g - mole} \times 10^3 \frac{M^3}{liter} \times \left(\frac{293.15^\circ K}{273.15^\circ K} \right) \times 10^6 ppm}$$

= ppmvd as styrene x MW Styrene (104.088) x 0.0416

| | mg/dscm |
|------------------|---------|
| Run #1 RTO Inlet | 618.75 |

5) Calculate mass rate of styrene.

$$lbs/hr = \frac{mg}{dscm} \times \frac{ft^3}{min} \times 3.75e^{-06}$$

| | Mass Rate, lbs/hr as styrene |
|------------------|------------------------------|
| Run #1 RTO Inlet | 7.48 |

$$3.75e-06 = \frac{0.0022 lbs}{g} \times \frac{g}{1000 mg} \times \frac{60 min}{hr} \times \frac{m^3}{35.31 ft^3}$$

Oxygen/Carbon Dioxide Concentration Measurements

| | |
|-----------|--------------------------|
| Client: | E-Stone/Grove Scientific |
| Location: | Sebring, Florida |
| Source: | RTO Exhaust |
| Date: | 12/9/08 |

Run One

| Time | Oxygen unit concentrations in percent | Carbon Dioxide | Comments |
|--|---|----------------|----------|
| Uncorrected Average for Run #1 | 20.40 | 0.07 | |
| Data corrected for Pre-/Post- Calibrations | 20.41 | 0.04 | |

Run Two

| Time | Oxygen unit concentrations in percent | Carbon Dioxide | Comments |
|--|---|----------------|----------|
| Uncorrected Average for Run #2 | 20.70 | 0.11 | |
| Data corrected for Pre-/Post- Calibrations | 20.70 | 0.08 | |

Run Three

| Time | Oxygen unit concentrations in percent | Carbon Dioxide | Comments |
|--|---|----------------|----------|
| Uncorrected Average for Run #3 | 20.35 | 0.19 | |
| Data corrected for Pre-/Post- Calibrations | 20.37 | 0.16 | |

System Calibration Error Data

| | | | |
|--------|--------------------------|--|--|
| Client | E-Stone/Grove Scientific | | |
|--------|--------------------------|--|--|

| | | | |
|----------|------------------|--|--|
| Location | Sebring, Florida | | |
|----------|------------------|--|--|

Oxygen

| | | | |
|------------------------|--------------------------------|--------------------------|---------|
| Analyzer Model No. | Servomex 1400B | US EPA Method | 3A |
| Gas Conc./Dilution Gas | 20.9% Oxygen in N ₂ | Protocol Expiration Date | 8/20/11 |
| Cylinder Number | CC166921 | Technician | Smith |

Initial Calibration

| | Range | Dilution | Response | Error | %Error |
|----------|-------|----------|----------|-------|--------|
| | % | % | % | % | % |
| Zero/Low | 0 | 0.02 | 0.02 | 0.02 | 0.10% |
| Mid | 10 | 10.01 | 10.01 | 0.01 | 0.05% |
| High | 20.9 | 20.87 | 20.87 | 0.03 | 0.14% |

| | Actual Value | | System Response | | System Bias % | | Calibration Drift % | |
|-------|--------------|----------|-----------------|----------|---------------|----------|---------------------|----------|
| Time | Zero | Midscale | Zero | Midscale | Zero | Midscale | Zero | Midscale |
| 7:02 | 0.00 | 20.90 | 0.02 | 20.88 | 0.10% | 0.10% | | |
| 11:16 | 0.00 | 20.90 | 0.02 | 20.90 | 0.10% | 0.00% | 0.00% | 0.10% |
| 12:56 | 0.00 | 20.90 | 0.02 | 20.90 | 0.10% | 0.00% | 0.00% | 0.00% |
| 15:06 | 0.00 | 20.90 | 0.02 | 20.87 | 0.10% | 0.14% | 0.00% | 0.14% |

Carbon Dioxide

| | | | |
|------------------------|--|--------------------------|---------|
| Analyzer Model No. | Servomex 1400B | US EPA Method | 3A |
| Gas Conc./Dilution Gas | 20.99% CO ₂ in N ₂ | Protocol Expiration Date | 2/12/11 |
| Cylinder Number | CC100081 | Technician | Smith |

Initial Calibration

| | Range | Dilution | Response | Error | %Error |
|----------|-------|----------|----------|-------|--------|
| | % | % | % | % | % |
| Zero/Low | 0 | 0.03 | 0.03 | 0.03 | 0.14% |
| Mid | 10 | 9.96 | 9.96 | 0.04 | 0.19% |
| High | 20.99 | 20.96 | 20.96 | 0.03 | 0.14% |

| | Actual Value | | System Response | | System Bias % | | Calibration Drift % | |
|-------|--------------|----------|-----------------|----------|---------------|----------|---------------------|----------|
| Time | Zero | Midscale | Zero | Midscale | Zero | Midscale | Zero | Midscale |
| 7:02 | 0.00 | 10.00 | 0.03 | 9.99 | 0.14% | 0.05% | | |
| 11:16 | 0.00 | 10.00 | 0.03 | 10.02 | 0.14% | 0.10% | 0.00% | 0.14% |
| 12:56 | 0.00 | 10.00 | 0.03 | 10.02 | 0.14% | 0.10% | 0.00% | 0.00% |
| 15:06 | 0.00 | 10.00 | 0.03 | 10.02 | 0.14% | 0.10% | 0.00% | 0.00% |

NOMENCLATURE

| | |
|----------------------------|---|
| A_N | (square inches), cross sectional area of nozzle |
| A_S | (square feet), cross sectional area of stack |
| C_P | Pitot tube calibration coefficient, dimensionless |
| % EA | Percent excess air |
| F | (scfd/MMBtu), F factor |
| D_H | (inches of water) average orifice meter reading |
| HI | (MMBtu/hr), heat input rate |
| % I | Percent isokineticity |
| M | (lb/lb mole), molecular weight of wet gas |
| % M | Percent moisture |
| MD | Mole fraction of dry gas |
| MWD | (lb/lb mole) molecular weight of dry gas |
| N DP | Number of sampling data points |
| P_{ATM} | (in Hg), local atmospheric pressure |
| P_M | (in Hg), absolute pressure in dry gas meter |
| P_s | (in Hg), absolute stack pressure |
| P_{s Gauge} | (inches of water), measured static stack pressure gauge |
| P_{STD} | (29.92 in Hg), standard pressure |
| PMRC | (lb/hr), pollutant mass rate based on concentration |
| PMRU | (lb/mmBtu), specific emission rate |

NOMENCLATURE (continued)

| | |
|---|---|
| D_P | (inches of water), velocity pressure |
| Q_s | (ft ³ /min.), actual stack volume flow rate |
| Q_{STD} | (ft ³ /min.), stack volume flow rate at standard conditions |
| Time(min) | duration of test |
| T_M | (°R), average dry gas meter temperature |
| T_s | (°R), average stack temperature |
| T_{STD} | (528 °R), standard temperature |
| VLQ | (ml), liquid volume |
| V_M | (ft ³), sample volume measured by dry gas meter |
| V_{MSTD}(ft³) | Sample volume at standard conditions |
| V_s | (ft/sec), stack velocity |
| VV_{STD} | (ft ³), volume of water vapor collected, corrected to standard conditions |
| WT | (grams), total weight of particulate collected |

CALCULATION FORMULAE

1. Absolute pressure at the dry gas meter, P_m

$$P_m = P_{bar} \pm \left(\frac{dH}{13.6} \right)$$

2. Absolute stack pressure, P_s

$$P_s = P_{bar} \pm \left(\frac{P_g}{13.6} \right)$$

3. Sample volume at standard conditions, $V_{m(std)}$

$$\begin{aligned} V_{m(std)} &= K_1 \times V_m \times Y \times \left(\frac{P_{bar} + \frac{\Delta h}{13.6}}{T_m} \right) \\ &= Y \times (V_m \times 528 \times P_m) / (T_m \times 29.92) \\ K_1 &= \frac{528^o R}{29.92 \text{ inHg}} \end{aligned}$$

4. Volume of water collected, corrected to standard conditions, $V_{v(std)}$

$$\begin{aligned} V_{v(std)} &= V_{v(std)_w} + V_{v(std)_g} \\ V_{v(std)_w} &= 0.04706 \frac{ft^3}{ml} \times \frac{29.92 \text{ inHg}}{528^o R} \times ml \\ V_{v(std)_g} &= 0.04715 \frac{ft^3}{ml} \times \frac{29.92 \text{ inHg}}{528^o R} \times ml \end{aligned}$$

5. Total sample volume at standard conditions, V_{std}

$$V_{std} = V_{m(std)} + V_{v(std)}$$

6. Percent moisture in stack gas, %M

$$\%M = \frac{V_{v(std)}}{V_{(std)}} \times 100$$

7. Mole Fraction of the dry gas, MD

$$MD = \frac{(100 - \%M)}{100}$$

CALCULATION FORMULAE (continued)

8. Molecular weight of the Dry Gas, MWD

$$MWD = 0.440(\%CO_2) + 0.320(\%O_2) + 0.280(\%N_2 + \%CO)$$

9. Molecular weight of stack gas, wet basis, g/g-mole (lb/lb-mole), M

$$M = MWD \times MD + 18(1 - MD)$$

10. Stack velocity, V_s

$$V_s = K_p \times C_p \sqrt{\Delta p_{avg}} \times \sqrt{\frac{T_{s(abs)}}{P_s \times M}}$$

11. Average stack gas dry volumetric flow rate, Q_{std} dry

$$Q_{s(dry)} = 17.647 \times 60 \times MD \times V_s \times A \times \left(\frac{P_s}{T_s} \right)$$

12. Pollutant mass rate, concentration basis, lbs/hr

$$PMRC = \frac{0.1323lb-min}{gram-hr} \times grams \times Q_{std} \div V_{std}$$

13. Percent Isokineticity

$$I = \frac{100T_s [K_3V_{lc} + (V_m Y / T_m)(P_{bar} + \Delta h / 13.6)]}{60 \times \theta \times V_s \times P_s \times A_n}$$

14. % Excess Air

$$\%EA = \left(\frac{(\%O_2 - 0.5\%CO)}{(0.264 \times \%N_2) - \%O_2 + 0.5 \times \%CO} \right) \times 100$$

15. Dry Gas Meter Check

$$Y_c = \frac{10}{V_m} \left| 0.0319 \frac{T_m}{P_{bar}} \right|^{1/2}$$

CALCULATION FORMULAE (continued)

16. Heat Input Rate, mmBtu/hr

$$HI = \frac{60 \text{ min/hr} \times \text{dscf/min}}{\text{dscf/mmBtu}} \times \frac{20.9 - \%O_2}{20.9}$$

17. Specific emission rate, lbs/mmBtu

$$PMRU = \frac{PMRC}{HI}$$

18. Modified Carrier Equation for Prediction of Stack Moisture with a Wet Bulb Thermometer

$$\%M = \left(\frac{100}{P_s} \right) \left[10^{\left(6.6911 \left[\frac{3144}{T_w + 390.86} \right] \right)} - (0.000367)(P_s)(T_d - T_w) \left[1 + \frac{T_w - 32}{1571} \right] \right]$$

19. Correction of Gas Concentrations for Calibration Error, Equation 6c-1

$$C_{gas} = \left(\bar{C} - C_o \right) \frac{C_{ma}}{C_m - C_o}$$

20. VOC Emission Rate as {compound specified by molecular weight}

$$\frac{lbsC_1}{hr} = \frac{ppmvd \times M \left(\frac{g}{g-mole} \right)}{22.414 \frac{liters}{g-mole} \times 10^3 \frac{m^3}{liter} \times \frac{293.15^\circ K}{273.15^\circ K}} \times \frac{1}{1 \times 10^6 ppm} \times \frac{10^3 mg}{g} \times Q_{stdry} \times 3.75e^{-06}$$

$$\text{where } 3.75e^{-06} = \frac{0.0022lbs}{g} \times \frac{g}{1000mg} \times \frac{60 \text{ min}}{\text{hour}} \times \frac{m^3}{35.315 ft^3}$$

APPENDIX

ATC Raw Data from Data Logger
Field Data Sheets
Calibration Data
LELAP Accreditation

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | | | RTO Outlet | | | Baghouse | | Calibration Comments | Error % |
|-----------|----------|--------|------|--|--|--|--|---|--|----------|--|-------------------------|--|
| | | % | % | VOC 3 ppm C ₂ H ₆ | VOC 1 ppm C ₂ H ₆ | VOC 2 ppm C ₂ H ₆ | RTO ppm C ₂ H ₆ | Baghouse ppm C ₂ H ₆ | | | | | |
| 12/8/2008 | 11:49:50 | 21.538 | 0.03 | 3.516 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:50:00 | 21.568 | 0.03 | 3.59 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:50:10 | 21.568 | 0.03 | 3.59 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:50:20 | 21.553 | 0.03 | 3.59 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:50:30 | 21.568 | 0.03 | 3.37 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:50:40 | 21.553 | 0.03 | 3.297 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:50:50 | 21.568 | 0.03 | 3.37 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:51:00 | 22.726 | 0.03 | 3.297 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:51:10 | 23.549 | 0.03 | 3.37 | 0 | 0.078 | | | | | | | |
| 12/8/2008 | 11:51:20 | 24.447 | 0.03 | 3.37 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:51:30 | 25.773 | 0.03 | 3.297 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:51:40 | 25.544 | 0.03 | 3.297 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:51:50 | 21.02 | 0.03 | 3.443 | 0.073 | 0.078 | | | | | | | Method 265 |
| 12/8/2008 | 11:52:00 | 20.929 | 0.03 | 3.37 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:52:10 | 20.959 | 0.03 | 3.516 | 0.073 | 0.078 | | | | | | | 0.28% |
| 12/8/2008 | 11:52:20 | 21.37 | 0.03 | 3.37 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:52:30 | 21.127 | 0.03 | 3.223 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:52:40 | 21.035 | 0.03 | 3.223 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:52:50 | 21.02 | 0.03 | 3.15 | 0 | 0.078 | | | | | | | |
| 12/8/2008 | 11:53:00 | 21.02 | 0.03 | 3.223 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:53:10 | 24.067 | 0.03 | 3.15 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:53:20 | 23.884 | 0.03 | 3.297 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:53:30 | 17.959 | 0.03 | 3.297 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:53:40 | 14.501 | 0.03 | 3.37 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:53:50 | 12.841 | 0.03 | 3.37 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:54:00 | 12.018 | 0.03 | 3.223 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:54:10 | 11.622 | 0.03 | 3.15 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:54:20 | 11.424 | 0.03 | 3.15 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:54:30 | 11.317 | 0.03 | 3.297 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:54:40 | 11.272 | 0.03 | 3.37 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:54:50 | 11.241 | 0.03 | 3.15 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:55:00 | 11.089 | 0.03 | 3.15 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:55:10 | 10.571 | 0.03 | 3.297 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:55:20 | 10.48 | 0.03 | 3.297 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:55:30 | 10.48 | 0.03 | 3.15 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:55:40 | 10.48 | 0.03 | 3.15 | 0.073 | 0.078 | | | | | | | 0.10% |
| 12/8/2008 | 11:55:50 | 10.48 | 0.03 | 3.15 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:56:00 | 9.362 | 0.03 | 3.223 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:56:10 | 9.962 | 0.03 | 3.297 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:56:20 | 7.342 | 0.03 | 3.297 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:56:30 | 2.94 | 0.03 | 3.223 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:56:40 | 0.685 | 0.03 | 3.15 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:56:50 | 0.015 | 0.03 | 3.15 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:57:00 | 0.015 | 0.03 | 3.15 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:57:10 | 0.015 | 0.03 | 3.15 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:57:20 | 0.015 | 0.03 | 3.223 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:57:30 | 0.015 | 0.03 | 3.223 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:57:40 | 0.015 | 0.03 | 3.297 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:57:50 | 0.015 | 0.03 | 3.297 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:58:00 | 0.015 | 0.03 | 3.297 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:58:10 | 0.015 | 0.03 | 3.37 | 0.073 | 0.078 | | | | | | | 0.07% |
| 12/8/2008 | 11:58:20 | 0.015 | 0.03 | 3.37 | 0 | 0.078 | | | | | | | |
| 12/8/2008 | 11:58:30 | 0.015 | 0.03 | 3.37 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:58:40 | 0.046 | 0.03 | 3.37 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:58:50 | 0.442 | 0.03 | 3.37 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:59:00 | 0.67 | 0.03 | 3.37 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:59:10 | 0.792 | 0.03 | 3.297 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:59:20 | 0.853 | 0.03 | 3.297 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:59:30 | 2.574 | 0.03 | 3.223 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:59:40 | 2.559 | 0.03 | 3.223 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 11:59:50 | 2.544 | 0.03 | 3.223 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 12:00:00 | 2.483 | 0.03 | 3.15 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 12:00:10 | 2.529 | 0.03 | 3.15 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 12:00:20 | 2.483 | 0.03 | 3.297 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 12:00:30 | 2.483 | 0.03 | 3.37 | 0.073 | 0.078 | | | | | | | Trial #1-1 st Dil'n (diff. from avg.) |
| 12/8/2008 | 12:00:40 | 2.483 | 0.03 | 3.37 | 0.073 | 0.078 | | | | | | | 0.015 |
| 12/8/2008 | 12:00:50 | 2.346 | 0.03 | 3.37 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 12:01:00 | 1.158 | 0.03 | 3.37 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 12:01:10 | 0.533 | 0.03 | 3.223 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 12:01:20 | 0.777 | 0.03 | 3.297 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 12:01:30 | 1.598 | 0.03 | 3.37 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 12:01:40 | 2.026 | 0.03 | 3.37 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 12:01:50 | 2.239 | 0.03 | 3.37 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 12:02:00 | 2.361 | 0.03 | 3.297 | 0.073 | 0.078 | | | | | | | |
| 12/8/2008 | 12:02:10 | 2.407 | 0.03 | 3.223 | 0.073 | 0.078 | | | | | | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|----------|--------|------|-----------------------------------|-----------------------------------|-----------------------------------|--|------------|
| | | % | % | ppm C ₂ H ₆ | ppm C ₂ H ₆ | ppm C ₂ H ₆ | | |
| 12/8/2008 | 12:02:20 | 2.437 | 0.03 | 3.15 | 0 | 0.076 | | |
| 12/8/2008 | 12:02:30 | 2.407 | 0.03 | 3.15 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:02:40 | 2.62 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:02:50 | 2.544 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:03:00 | 2.498 | 0.03 | 3.223 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:03:10 | 2.513 | 0.03 | 3.223 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:03:20 | 2.513 | 0.03 | 3.297 | 0.073 | 0.076 | Trial #2-1 st Dil'n (diff. from avg.) | 0.015 |
| 12/8/2008 | 12:03:30 | 2.498 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:03:40 | 2.193 | 0.03 | 3.297 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:03:50 | 1.081 | 0.03 | 3.223 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:04:00 | 1.447 | 0.03 | 3.223 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:04:10 | 1.965 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:04:20 | 2.224 | 0.03 | 3.297 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:04:30 | 2.376 | 0.03 | 3.15 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:04:40 | 2.437 | 0.03 | 3.223 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:04:50 | 2.468 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:05:00 | 2.483 | 0.03 | 3.223 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:05:10 | 2.483 | 0.03 | 3.15 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:05:20 | 2.498 | 0.03 | 3.297 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:05:30 | 2.483 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:05:40 | 2.498 | 0.03 | 3.223 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:05:50 | 2.498 | 0.03 | 3.15 | 0.073 | 0.076 | Trial #3-1 st Dil'n (diff. from avg.) | 0.000 |
| 12/8/2008 | 12:06:00 | 1.889 | 0.03 | 3.223 | 0.073 | 0.076 | Avg of 3 trials-1 st dil'n | 2.498 |
| 12/8/2008 | 12:06:10 | 1.158 | 0.03 | 3.223 | 0.073 | 0.076 | Precision of 2.5% split | 0.60% |
| 12/8/2008 | 12:06:20 | 2.041 | 0.03 | 3.297 | 0.073 | 0.076 | Accuracy of 2.5% split | 0.08% |
| 12/8/2008 | 12:06:30 | 6.397 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:06:40 | 8.286 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:06:50 | 9.261 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:07:00 | 9.748 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:07:10 | 10.007 | 0.03 | 3.297 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:07:20 | 10.007 | 0.03 | 3.297 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:07:30 | 10.023 | 0.03 | 3.223 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:07:40 | 9.977 | 0.03 | 3.223 | 0.073 | 0.076 | Trial #1-2 nd Dil'n (diff. from avg.) | 0.010 |
| 12/8/2008 | 12:07:50 | 10.007 | 0.03 | 3.15 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:08:00 | 10.099 | 0.03 | 3.223 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:08:10 | 10.068 | 0.03 | 3.297 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:08:20 | 8.53 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:08:30 | 5.103 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:08:40 | 3.869 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:08:50 | 7.205 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:09:00 | 8.621 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:09:10 | 9.337 | 0.03 | 3.516 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:09:20 | 9.688 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:09:30 | 9.87 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:09:40 | 10.007 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:09:50 | 9.962 | 0.03 | 3.223 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:10:00 | 9.992 | 0.03 | 3.223 | 0.073 | 0.076 | Trial #2-2 nd Dil'n (diff. from avg.) | 0.005 |
| 12/8/2008 | 12:10:10 | 10.007 | 0.03 | 3.297 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:10:20 | 9.992 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:10:30 | 10.114 | 0.03 | 3.223 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:10:40 | 10.023 | 0.03 | 3.223 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:10:50 | 6.367 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:11:00 | 3.61 | 0.03 | 3.223 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:11:10 | 3.854 | 0.03 | 3.223 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:11:20 | 7.022 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:11:30 | 8.499 | 0.03 | 3.223 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:11:40 | 9.246 | 0.03 | 3.15 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:11:50 | 9.827 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:12:00 | 9.84 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:12:10 | 9.916 | 0.03 | 3.223 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:12:20 | 9.977 | 0.03 | 3.223 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:12:30 | 9.992 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:12:40 | 10.023 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:12:50 | 10.023 | 0.03 | 3.223 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:13:00 | 9.962 | 0.03 | 3.223 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:13:10 | 10.084 | 0.03 | 3.223 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:13:20 | 9.992 | 0.03 | 3.297 | 0.073 | 0.076 | Trial #3-2 nd Dil'n (diff. from avg.) | 0.005 |
| 12/8/2008 | 12:13:30 | 8.301 | 0.03 | 3.37 | 0.073 | 0.076 | Avg. of 3 trials-2 nd dil'n | 9.987 |
| 12/8/2008 | 12:13:40 | 3.823 | 0.03 | 3.37 | 0.073 | 0.076 | Precision of 10.0% split | 0.10% |
| 12/8/2008 | 12:13:50 | 1.934 | 0.03 | 3.223 | 0.073 | 0.076 | Accuracy of 10.0% split | 0.13% |
| 12/8/2008 | 12:14:00 | 3.382 | 0.03 | 3.223 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:14:10 | 7.525 | 0.03 | 3.223 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:14:20 | 9.535 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:14:30 | 10.566 | 0.03 | 3.297 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:14:40 | 11.074 | 0.03 | 3.297 | 0.073 | 0.076 | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|----------|--------|------|-----------------------------------|-----------------------------------|-----------------------------------|-------------------------|------------|
| | | % | % | ppm C ₂ H ₆ | ppm C ₂ H ₆ | ppm C ₂ H ₆ | | |
| 12/8/2008 | 12:14:50 | 10.525 | 0.03 | 3.297 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:15:00 | 10.586 | 0.03 | 3.297 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:15:10 | 10.48 | 0.03 | 3.287 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:15:20 | 10.525 | 0.03 | 3.297 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:15:30 | 10.48 | 0.03 | 3.297 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:15:40 | 10.495 | 0.03 | 3.297 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:15:50 | 9.429 | 0.03 | 3.297 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:16:00 | 9.261 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:16:10 | 4.768 | 0.03 | 3.297 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:16:20 | 1.905 | 0.03 | 3.297 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:16:30 | 3.412 | 0.03 | 3.297 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:16:40 | 6.839 | 0.03 | 3.297 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:16:50 | 8.56 | 0.03 | 3.297 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:17:00 | 9.459 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:17:10 | 9.916 | 0.03 | 3.297 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:17:20 | 10.129 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:17:30 | 10.236 | 0.03 | 3.297 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:17:40 | 10.297 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:17:50 | 10.327 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:18:00 | 10.343 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:18:10 | 10.358 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:18:20 | 10.343 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:18:30 | 10.48 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:18:40 | 10.495 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:18:50 | 10.495 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:19:00 | 10.51 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:19:10 | 9.794 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:19:20 | 9.383 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:19:30 | 6.9 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:19:40 | 2.65 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:19:50 | 0.503 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:20:00 | 0.015 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:20:10 | 0.015 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:20:20 | 4.539 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:20:30 | 7.448 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:20:40 | 8.956 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:20:50 | 9.733 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:21:00 | 10.114 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:21:10 | 10.297 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:21:20 | 10.403 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:21:30 | 10.449 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:21:40 | 10.464 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:21:50 | 10.48 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:22:00 | 10.48 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:22:10 | 10.495 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:22:20 | 10.495 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:22:30 | 10.51 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:22:40 | 10.495 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:22:50 | 10.495 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:23:00 | 7.555 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:23:10 | 7.555 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:23:20 | 7.555 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:23:30 | 7.555 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:23:40 | 7.555 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:23:50 | 7.555 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:24:00 | 7.54 | 0.03 | 3.516 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:24:10 | 7.54 | 0.03 | 3.516 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:24:20 | 7.54 | 0.03 | 3.516 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:24:30 | 7.54 | 0.03 | 3.516 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:24:40 | 7.54 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:24:50 | 7.54 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:25:00 | 7.525 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:25:10 | 7.525 | 0.03 | 3.516 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:25:20 | 7.525 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:25:30 | 7.54 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:25:40 | 7.525 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:25:50 | 7.509 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:26:00 | 7.525 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:26:10 | 7.525 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:26:20 | 7.525 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:26:30 | 7.509 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:26:40 | 7.525 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:26:50 | 7.525 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:27:00 | 7.525 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:27:10 | 7.494 | 0.03 | 3.37 | 0.073 | 0.076 | | |

Mid-level audit-Trial #1 (10.50%) 0.000
Avg of 3 Mid-level audit injections 10.493
Precision of Mid-level audit 0.00%
Accuracy of Mid-level audit 0.14%

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 % | CO2 % | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|----------|---------|----------|--|--|--|-------------------------|------------|
| | | | | VOC 3 ppm C ₂ H ₆ | VOC 1 ppm C ₂ H ₆ | VOC 2 ppm C ₂ H ₆ | | |
| 12/8/2008 | 12:27:20 | 7.509 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:27:30 | 7.509 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:27:40 | 7.509 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:27:50 | 7.509 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:28:00 | 7.509 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:28:10 | 7.494 | 0.03 | 3.297 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:28:20 | 7.509 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:28:30 | 7.494 | 0.03 | 3.297 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:28:40 | 7.494 | 0.03 | 3.297 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:28:50 | 7.494 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:29:00 | 7.494 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:29:10 | 7.494 | 0.03 | 3.297 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:29:20 | 7.494 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:29:30 | 7.494 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:29:40 | 7.494 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:29:50 | 7.494 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:30:00 | 7.494 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:30:10 | 7.494 | 0.03 | 3.297 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:30:20 | 7.494 | 0.03 | 3.297 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:30:30 | 7.494 | 0.03 | 3.297 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:30:40 | 7.494 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:30:50 | 7.479 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:31:00 | 7.494 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:31:10 | 7.494 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:31:20 | 7.494 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:31:30 | 7.494 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:31:40 | 7.479 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:31:50 | 7.479 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:32:00 | 7.479 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:32:10 | 7.479 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:32:20 | 7.479 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:32:30 | 7.479 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:32:40 | 7.479 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:32:50 | 7.479 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:33:00 | 7.479 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:33:10 | 7.479 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:33:20 | 7.464 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:33:30 | 7.464 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:33:40 | 7.479 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:33:50 | 7.479 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:34:00 | 7.479 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:34:10 | 7.479 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:34:20 | 7.479 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:34:30 | 7.464 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:34:40 | 7.479 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:34:50 | 7.479 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:35:00 | 7.464 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:35:10 | 7.464 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:35:20 | 7.464 | 0.03 | 3.516 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:35:30 | 7.479 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:35:40 | 7.464 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:35:50 | 7.464 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:36:00 | 7.448 | 0.03 | 3.37 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:36:10 | 7.479 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:36:20 | 7.479 | 0.03 | 3.443 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:36:30 | 7.464 | 0.03 | 2.711 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:36:40 | 7.464 | 0.03 | 2.784 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:36:50 | 7.464 | 0.03 | 2.711 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:37:00 | 7.464 | 0.03 | 1.026 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:37:10 | 7.464 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:37:20 | 7.464 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:37:30 | 7.464 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:37:40 | 7.448 | 0.03 | 0.147 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:37:50 | 7.448 | 0.03 | 0.147 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:38:00 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:38:10 | 7.464 | 0.03 | 0.147 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:38:20 | 7.464 | 0.03 | 0.806 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:38:30 | 7.464 | 0.03 | 0.879 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:38:40 | 7.464 | 0.03 | 0.879 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:38:50 | 7.464 | 0.03 | 0.513 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:39:00 | 7.448 | 0.03 | 0.293 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:39:10 | 7.448 | 0.03 | 0.22 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:39:20 | 7.448 | 0.03 | 0.293 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:39:30 | 7.464 | 0.03 | 0.44 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:39:40 | 7.464 | 0.03 | 0.513 | 0.073 | 0.076 | | |

VOC zero gas = 0.02%

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|----------|-------|------|--|--|--|-------------------|-------------------------|------------|
| | | % | % | VOC 3 ppm C ₂ H ₆ | VOC 1 ppm C ₂ H ₆ | VOC 2 ppm C ₂ H ₆ | | | |
| 12/8/2008 | 12:39:50 | 7.464 | 0.03 | 0.733 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:40:00 | 7.448 | 0.03 | 0.952 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:40:10 | 7.448 | 0.03 | 0.952 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:40:20 | 7.448 | 0.03 | 0.806 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:40:30 | 7.464 | 0.03 | 0.806 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:40:40 | 7.464 | 0.03 | 0.879 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:40:50 | 7.448 | 0.03 | 0.879 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:41:00 | 7.464 | 0.03 | 0.879 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:41:10 | 7.464 | 0.03 | 1.026 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:41:20 | 7.448 | 0.03 | 1.099 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:41:30 | 7.448 | 0.03 | 1.026 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:41:40 | 7.448 | 0.03 | 1.026 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:41:50 | 7.448 | 0.03 | 0.806 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:42:00 | 7.448 | 0.03 | 2.418 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:42:10 | 7.433 | 0.03 | 0.22 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:42:20 | 7.448 | 0.03 | 0.879 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:42:30 | 7.448 | 0.03 | 0.879 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:42:40 | 7.448 | 0.03 | 0.659 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:42:50 | 7.448 | 0.03 | 59.56 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:43:00 | 7.433 | 0.03 | 107.253 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:43:10 | 7.448 | 0.03 | 123.15 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:43:20 | 7.448 | 0.03 | 133.187 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:43:30 | 7.433 | 0.03 | 143.516 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:43:40 | 7.448 | 0.03 | 151.138 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:43:50 | 7.433 | 0.03 | 157.07 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:44:00 | 7.433 | 0.03 | 161.392 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:44:10 | 7.448 | 0.03 | 165.128 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:44:20 | 7.448 | 0.03 | 167.546 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:44:30 | 7.433 | 0.03 | 170.696 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:44:40 | 7.433 | 0.03 | 171.355 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:44:50 | 7.433 | 0.03 | 172.821 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:45:00 | 7.448 | 0.03 | 173.7 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:45:10 | 7.433 | 0.03 | 175.018 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:45:20 | 7.433 | 0.03 | 175.604 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:45:30 | 7.448 | 0.03 | 175.878 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:45:40 | 7.448 | 0.03 | 176.85 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:45:50 | 7.448 | 0.03 | 177.656 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:46:00 | 7.433 | 0.03 | 177.729 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:46:10 | 7.448 | 0.03 | 178.681 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:46:20 | 7.433 | 0.03 | 178.681 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:46:30 | 7.433 | 0.03 | 178.681 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:46:40 | 7.418 | 0.03 | 178.828 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:46:50 | 7.433 | 0.03 | 178.388 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:47:00 | 7.433 | 0.03 | 178.096 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:47:10 | 7.418 | 0.03 | 179.56 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:47:20 | 7.433 | 0.03 | 179.048 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:47:30 | 7.433 | 0.03 | 179.287 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:47:40 | 7.418 | 0.03 | 179.194 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:47:50 | 7.418 | 0.03 | 179.194 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:48:00 | 7.418 | 0.03 | 179.56 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:48:10 | 7.418 | 0.03 | 180.073 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:48:20 | 7.433 | 0.03 | 179.707 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:48:30 | 7.418 | 0.03 | 179.707 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:48:40 | 7.433 | 0.03 | 200.44 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:48:50 | 7.433 | 0.03 | 252.308 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:49:00 | 7.418 | 0.03 | 295.165 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:49:10 | 7.418 | 0.03 | 296.777 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:49:20 | 7.418 | 0.03 | 296.703 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:49:30 | 7.418 | 0.03 | 297.656 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:49:40 | 7.433 | 0.03 | 297.875 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:49:50 | 7.433 | 0.03 | 297.802 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:50:00 | 7.418 | 0.03 | 297.363 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:50:10 | 7.418 | 0.03 | 168.425 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:50:20 | 7.418 | 0.03 | 150.11 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:50:30 | 7.418 | 0.03 | 149.963 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:50:40 | 7.418 | 0.03 | 149.597 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:50:50 | 7.418 | 0.03 | 148.304 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:51:00 | 7.433 | 0.03 | 149.524 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:51:10 | 7.433 | 0.03 | 130.403 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:51:20 | 7.418 | 0.03 | 76.264 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:51:30 | 7.418 | 0.03 | 75.678 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:51:40 | 7.418 | 0.03 | 75.678 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:51:50 | 7.418 | 0.03 | 75.531 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:52:00 | 7.418 | 0.03 | 76.631 | 0.073 | 0.076 | | | |
| 12/8/2008 | 12:52:10 | 7.418 | 0.03 | 75.385 | 0.073 | 0.076 | VOC low range gas | 0.71% | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|----------|-------|------|-----------------------------------|-----------------------------------|-----------------------------------|-------------------------|------------|
| | | % | % | ppm C ₆ H ₆ | ppm C ₆ H ₆ | ppm C ₆ H ₆ | | |
| 12/8/2008 | 12:52:20 | 7.418 | 0.03 | 75.824 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:52:30 | 7.418 | 0.03 | 75.458 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:52:40 | 7.418 | 0.03 | 75.458 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:52:50 | 7.418 | 0.03 | 75.824 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:53:00 | 7.418 | 0.03 | 75.531 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:53:10 | 7.418 | 0.03 | 5.201 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:53:20 | 7.403 | 0.03 | 1.245 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:53:30 | 7.418 | 0.03 | 1.245 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:53:40 | 7.418 | 0.03 | 11.502 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:53:50 | 7.433 | 0.03 | 188.813 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:54:00 | 7.418 | 0.03 | 170.256 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:54:10 | 7.418 | 0.03 | 187.473 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:54:20 | 7.418 | 0.03 | 180.879 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:54:30 | 7.418 | 0.03 | 149.817 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:54:40 | 7.418 | 0.03 | 150.037 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:54:50 | 7.418 | 0.03 | 150.33 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:55:00 | 7.418 | 0.03 | 150.11 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:55:10 | 7.418 | 0.03 | 150.256 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:55:20 | 7.418 | 0.03 | 150.696 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:55:30 | 7.418 | 0.03 | 150.769 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:55:40 | 7.418 | 0.03 | 150.842 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:55:50 | 7.403 | 0.03 | 151.136 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:56:00 | 7.433 | 0.03 | 145.934 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:56:10 | 7.433 | 0.03 | 145.495 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:56:20 | 7.433 | 0.03 | 145.495 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:56:30 | 7.433 | 0.03 | 145.588 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:56:40 | 7.433 | 0.03 | 145.588 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:56:50 | 7.433 | 0.03 | 142.051 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:57:00 | 7.418 | 0.03 | 5.201 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:57:10 | 7.433 | 0.03 | 1.538 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:57:20 | 7.433 | 0.03 | 1.172 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:57:30 | 7.433 | 0.03 | 1.099 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:57:40 | 7.418 | 0.03 | 40.733 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:57:50 | 7.433 | 0.03 | 14.359 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:58:00 | 7.433 | 0.03 | 10.037 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:58:10 | 7.433 | 0.03 | 7.985 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:58:20 | 7.418 | 0.03 | 6.74 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:58:30 | 7.433 | 0.03 | 5.788 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:58:40 | 7.433 | 0.03 | 5.128 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:58:50 | 7.418 | 0.03 | 4.815 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:59:00 | 7.433 | 0.03 | 4.176 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:59:10 | 7.418 | 0.03 | 3.81 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:59:20 | 7.418 | 0.03 | 3.516 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:59:30 | 7.433 | 0.03 | 3.223 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:59:40 | 7.433 | 0.03 | 3.004 | 0.073 | 0.076 | | |
| 12/8/2008 | 12:59:50 | 7.418 | 0.03 | 2.857 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:00:00 | 7.433 | 0.03 | 2.637 | 0.073 | 0 | | |
| 12/8/2008 | 13:00:10 | 7.448 | 0.03 | 2.418 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:00:20 | 7.433 | 0.03 | 1.485 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:00:30 | 7.433 | 0.03 | 1.245 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:00:40 | 7.448 | 0.03 | 1.099 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:00:50 | 7.433 | 0.03 | 1.028 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:01:00 | 7.433 | 0.03 | 0.852 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:01:10 | 7.418 | 0.03 | 0.879 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:01:20 | 7.418 | 0.03 | 0.513 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:01:30 | 7.433 | 0.03 | 0.659 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:01:40 | 7.418 | 0.03 | 0.586 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:01:50 | 7.433 | 0.03 | 0.586 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:02:00 | 7.433 | 0.03 | 0.44 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:02:10 | 7.433 | 0.03 | 0.368 | 0 | 0.076 | | |
| 12/8/2008 | 13:02:20 | 7.433 | 0.03 | 0.368 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:02:30 | 7.433 | 0.03 | 0.22 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:02:40 | 7.433 | 0.03 | 0.22 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:02:50 | 7.433 | 0.03 | 81.612 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:03:00 | 7.433 | 0.03 | 135.018 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:03:10 | 7.433 | 0.03 | 140.813 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:03:20 | 7.433 | 0.03 | 141.026 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:03:30 | 7.418 | 0.03 | 141.685 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:03:40 | 7.433 | 0.03 | 142.491 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:03:50 | 7.433 | 0.03 | 146.886 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:04:00 | 7.418 | 0.03 | 150.476 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:04:10 | 7.433 | 0.03 | 150.989 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:04:20 | 7.418 | 0.03 | 150.037 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:04:30 | 7.418 | 0.03 | 148.791 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:04:40 | 7.418 | 0.03 | 148.205 | 0.073 | 0.076 | | |

Mid range calibration drift check 0.01%

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | D2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|----------|-------|------|-----------------------------------|-----------------------------------|-----------------------------------|-------------------------|------------|
| | | % | % | ppm C ₂ H ₆ | ppm C ₂ H ₆ | ppm C ₂ H ₆ | | |
| 12/8/2008 | 13:04:50 | 7.418 | 0.03 | 150.037 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:05:00 | 7.418 | 0.03 | 52.674 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:05:10 | 7.418 | 0.03 | 0.808 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:05:20 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:05:30 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:05:40 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:05:50 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:06:00 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:06:10 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:06:20 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:06:30 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:06:40 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:06:50 | 7.448 | 0.03 | 0.073 | 0 | 0.076 | | |
| 12/8/2008 | 13:07:00 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:07:10 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:07:20 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:07:30 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:07:40 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:07:50 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:08:00 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:08:10 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:08:20 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:08:30 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:08:40 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:08:50 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:09:00 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:09:10 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:09:20 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:09:30 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:09:40 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:09:50 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:10:00 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:10:10 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:10:20 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:10:30 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:10:40 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:10:50 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:11:00 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:11:10 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:11:20 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:11:30 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:11:40 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:11:50 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:12:00 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:12:10 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:12:20 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:12:30 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:12:40 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:12:50 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:13:00 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:13:10 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:13:20 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:13:30 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:13:40 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:13:50 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:14:00 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:14:10 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:14:20 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:14:30 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:14:40 | 7.433 | 0.03 | 38.022 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:14:50 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:15:00 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:15:10 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:15:20 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:15:30 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:15:40 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:15:50 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:16:00 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:16:10 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:16:20 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:16:30 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:16:40 | 7.433 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:16:50 | 7.448 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:17:00 | 8.469 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:17:10 | 8.484 | 0.03 | 0.073 | 0.073 | 0.076 | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|----------|--------|--------|--|--|--|-------------------------|------------|
| | | % | % | VOC 3 ppm C ₆ H ₆ | VOC 1 ppm C ₆ H ₆ | VOC 2 ppm C ₆ H ₆ | | |
| 12/8/2008 | 13:17:20 | 10.51 | 0.396 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:17:30 | 13.846 | 0.122 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:17:40 | 15.476 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:17:50 | 13.846 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:18:00 | 9.596 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:18:10 | 5.697 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:18:20 | 2.772 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:18:30 | 0.914 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:18:40 | 0.015 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:18:50 | 0.015 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:18:00 | 0.015 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:19:10 | 0.015 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:19:20 | 0.015 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:19:30 | 0.015 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:19:40 | 0.015 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:19:50 | 0.015 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:20:00 | 0.015 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:20:10 | 0.015 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:20:20 | 0.015 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:20:30 | 0.015 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:20:40 | 0.015 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:20:50 | 0.015 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:21:00 | 0.015 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:21:10 | 1.569 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:21:20 | 3.976 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:21:30 | 5.636 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:21:40 | 6.763 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:21:50 | 7.388 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:22:00 | 7.788 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:22:10 | 8.027 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:22:20 | 8.134 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:22:30 | 8.241 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:22:40 | 8.241 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:22:50 | 8.301 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:23:00 | 8.637 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:23:10 | 9.794 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:23:20 | 9.886 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:23:30 | 9.946 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:23:40 | 9.977 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:23:50 | 9.992 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:24:00 | 10.007 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:24:10 | 10.023 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:24:20 | 10.038 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:24:30 | 10.038 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:24:40 | 10.007 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:24:50 | 8.439 | 0.274 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:25:00 | 8.301 | 1.005 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:25:10 | 8.286 | 1.036 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:25:20 | 8.271 | 1.127 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:25:30 | 8.256 | 1.219 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:25:40 | 8.241 | 1.31 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:25:50 | 9.535 | 2.407 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:26:00 | 8.301 | 0.091 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:26:10 | 3.29 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:26:20 | 0.564 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:26:30 | 0.015 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:26:40 | 0.015 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:26:50 | 0.015 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:27:00 | 0.015 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:27:10 | 0.015 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:27:20 | 0.015 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:27:30 | 0.015 | 11.485 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:27:40 | 0.015 | 23.031 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:27:50 | 0.015 | 21.325 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:28:00 | 0.015 | 21.203 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:28:10 | 0.015 | 21.051 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:28:20 | 0.015 | 21.081 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:28:30 | 0.015 | 20.99 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:28:40 | 0.015 | 21.112 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:28:50 | 0.015 | 21.081 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:29:00 | 0.015 | 21.081 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:29:10 | 0.015 | 10.937 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:29:20 | 0.015 | 10.358 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:29:30 | 0.015 | 10.266 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:29:40 | 0.015 | 9.87 | 0.073 | 0.073 | 0.076 | | |

Oxygen zero system bias check 1.43%

Oxygen full range system bias check 2.20%

CO2 zero calibration 0.14%

CO2 high range calibration 0.00%

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 % | CO2 % | RTO Inlet ppm C ₂ H ₆ | RTO Outlet ppm C ₂ H ₆ | Baghouse ppm C ₂ H ₆ | Calibration Comments | Error % |
|-----------|----------|---------|----------|--|---|---|---------------------------------|------------|
| | | | | VOC 3 | VOC 1 | VOC 2 | | |
| 12/8/2008 | 13:29:50 | 0.015 | 9.962 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:30:00 | 0.015 | 10.114 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:30:10 | 0.015 | 10.114 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:30:20 | 0.015 | 10.114 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:30:30 | 0.015 | 10.114 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:30:40 | 0.015 | 10.114 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:30:50 | 0.015 | 10.145 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:31:00 | 0.015 | 10.114 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:31:10 | 0.015 | 9.931 | 0.073 | 0 | 0.076 | | |
| 12/8/2008 | 13:31:20 | 0.015 | 6.793 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:31:30 | 0.122 | 7.588 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:31:40 | 2.011 | 5.057 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:31:50 | 5.133 | 3.869 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:32:00 | 4.752 | 1.676 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:32:10 | 2.666 | 0.84 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:32:20 | 0.746 | 0.183 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:32:30 | 0.015 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:32:40 | 0.015 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:32:50 | 0.015 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:33:00 | 0.015 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:33:10 | 0.015 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:33:20 | 0.015 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:33:30 | 0.015 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:33:40 | 0.015 | 1.158 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:33:50 | 0.015 | 5.575 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:34:00 | 0.015 | 7.921 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:34:10 | 0.015 | 9.017 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:34:20 | 0.015 | 8.444 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:34:30 | 0.015 | 9.857 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:34:40 | 0.015 | 8.778 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:34:50 | 0.015 | 9.84 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:35:00 | 0.015 | 9.901 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:35:10 | 0.015 | 9.931 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:35:20 | 0.015 | 9.962 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:35:30 | 0.015 | 9.982 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:35:40 | 0.015 | 10.205 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:35:50 | 0.015 | 10.114 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:36:00 | 0.015 | 10.175 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:36:10 | 0.015 | 10.145 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:36:20 | 0.015 | 10.145 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:36:30 | 0.015 | 10.023 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:36:40 | 0.015 | 10.023 | 0.073 | 0.073 | 0.076 | CO2 mid range system bias check | 0.00% |
| 12/8/2008 | 13:36:50 | 0.015 | 10.023 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:37:00 | 0.015 | 10.023 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:37:10 | 0.015 | 8.682 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:37:20 | 1.645 | 4.328 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:37:30 | 8.408 | 1.493 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:37:40 | 14.044 | 0.579 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:37:50 | 17.689 | 0.152 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:38:00 | 19.832 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:38:10 | 21.005 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:38:20 | 21.827 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:38:30 | 22.223 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:38:40 | 22.492 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:38:50 | 22.589 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:39:00 | 22.665 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:39:10 | 22.711 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:39:20 | 22.772 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:39:30 | 22.711 | 0.03 | 0 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:39:40 | 22.698 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:39:50 | 22.711 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:40:00 | 22.711 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:40:10 | 22.698 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:40:20 | 22.728 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:40:30 | 22.757 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:40:40 | 22.85 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:40:50 | 22.85 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:41:00 | 22.62 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:41:10 | 22.62 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:41:20 | 22.559 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:41:30 | 22.604 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:41:40 | 22.665 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:41:50 | 22.665 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:42:00 | 22.665 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:42:10 | 22.65 | 0.03 | 0.073 | 0.073 | 0.076 | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|----------|--------|-------|-----------------------------------|-----------------------------------|-----------------------------------|----------------------------------|------------|
| | | % | % | ppm C ₂ H ₆ | ppm C ₂ H ₆ | ppm C ₂ H ₆ | | |
| 12/8/2008 | 13:42:20 | 22.543 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:42:30 | 22.589 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:42:40 | 22.589 | 0.03 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:42:50 | 22.406 | 0.061 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:43:00 | 22.223 | 0.122 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:43:10 | 21.995 | 0.152 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:43:20 | 22.056 | 0.122 | 0.073 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:43:30 | 21.904 | 0.152 | 0.073 | 0.073 | 0.006 | | |
| 12/8/2008 | 13:43:40 | 21.934 | 0.152 | 2.198 | 0.073 | 2.952 | | |
| 12/8/2008 | 13:43:50 | 21.797 | 0.152 | 17.216 | 0.073 | 6.208 | | |
| 12/8/2008 | 13:44:00 | 21.797 | 0.152 | 28.571 | 0.073 | 11.658 | | |
| 12/8/2008 | 13:44:10 | 21.767 | 0.152 | 20.368 | 0.073 | 19.077 | | |
| 12/8/2008 | 13:44:20 | 21.827 | 0.152 | 6.447 | 0.073 | 24.982 | | |
| 12/8/2008 | 13:44:30 | 21.762 | 0.152 | 5.128 | 0.073 | 30.584 | | |
| 12/8/2008 | 13:44:40 | 21.797 | 0.183 | 4.762 | 0.073 | 40.652 | | |
| 12/8/2008 | 13:44:50 | 21.827 | 0.183 | 4.396 | 0.073 | 36.791 | | |
| 12/8/2008 | 13:45:00 | 21.858 | 0.152 | 4.176 | 0.073 | 22.105 | | |
| 12/8/2008 | 13:45:10 | 21.812 | 0.152 | 4.615 | 0.073 | 20.515 | | |
| 12/8/2008 | 13:45:20 | 21.843 | 0.183 | 4.689 | 0.073 | 19.304 | | |
| 12/8/2008 | 13:45:30 | 21.782 | 0.183 | 4.396 | 0.073 | 19.001 | | |
| 12/8/2008 | 13:45:40 | 21.782 | 0.183 | 4.103 | 0.073 | 18.396 | | |
| 12/8/2008 | 13:45:50 | 21.782 | 0.183 | 3.956 | 0.073 | 18.168 | | |
| 12/8/2008 | 13:46:00 | 21.782 | 0.152 | 5.275 | 0.073 | 18.396 | | |
| 12/8/2008 | 13:46:10 | 21.736 | 0.152 | 4.396 | 0.073 | 18.85 | | |
| 12/8/2008 | 13:46:20 | 21.751 | 0.183 | 4.103 | 0.073 | 18.623 | | |
| 12/8/2008 | 13:46:30 | 21.751 | 0.183 | 4.029 | 0.073 | 18.017 | | |
| 12/8/2008 | 13:46:40 | 21.751 | 0.122 | 4.176 | 0.073 | 17.639 | | |
| 12/8/2008 | 13:46:50 | 21.706 | 0.152 | 4.982 | 0.073 | 17.336 | | |
| 12/8/2008 | 13:47:00 | 21.787 | 0.183 | 3.663 | 0.073 | 18.623 | | |
| 12/8/2008 | 13:47:10 | 21.767 | 0.183 | 3.81 | 0.073 | 19.153 | | |
| 12/8/2008 | 13:47:20 | 21.721 | 0.152 | 4.469 | 0.073 | 19.985 | | |
| 12/8/2008 | 13:47:30 | 21.721 | 0.152 | 4.469 | 0.073 | 19.834 | | |
| 12/8/2008 | 13:47:40 | 21.721 | 0.183 | 3.663 | 0.073 | 21.878 | | |
| 12/8/2008 | 13:47:50 | 21.675 | 0.152 | 4.322 | 0.073 | 6.435 | | |
| 12/8/2008 | 13:48:00 | 21.736 | 0.183 | 5.275 | 0.073 | 0.454 | | |
| 12/8/2008 | 13:48:10 | 21.675 | 0.183 | 4.689 | 0.073 | 6.51 | | |
| 12/8/2008 | 13:48:20 | 21.66 | 0.152 | 5.056 | 0.073 | 19.38 | | |
| 12/8/2008 | 13:48:30 | 21.66 | 0.152 | 4.542 | 0.073 | 22.559 | | |
| 12/8/2008 | 13:48:40 | 21.736 | 0.183 | 3.37 | 0.073 | 4.239 | | |
| 12/8/2008 | 13:48:50 | 21.629 | 0.152 | 4.322 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:49:00 | 21.051 | 0.152 | 4.616 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:49:10 | 20.898 | 0.183 | 3.736 | 0.073 | 0.076 | | |
| 12/8/2008 | 13:49:20 | 20.868 | 0.183 | 3.443 | 0.073 | 17.941 | | |
| 12/8/2008 | 13:49:30 | 20.822 | 0.152 | 3.883 | 0.073 | 22.862 | | |
| 12/8/2008 | 13:49:40 | 20.837 | 0.183 | 3.956 | 0.073 | 23.695 | | |
| 12/8/2008 | 13:49:50 | 20.868 | 0.183 | 3.736 | 0.073 | 27.556 | | |
| | | 4.029 | 0.073 | 29.751 | | | Stratification Check Point No. 1 | |
| | | 3.956 | 0.073 | 28.237 | | | Average O2 = | 20.650 |
| | | 4.469 | 0.073 | 27.707 | | | Average CO2 = | 0.170 |
| | | 4.176 | 0.073 | 32.779 | | | | |
| | | 3.59 | 0.073 | 27.707 | | | Deviation from mean, O2 = | 0.24% |
| | | 4.029 | 0.073 | 31.189 | | | Deviation from mean, CO2 = | 3.69% |
| | | 3.956 | 0.073 | 30.129 | | | | |
| | | 4.103 | 0.073 | 28.818 | | | | |
| | | 3.956 | 0.073 | 31.416 | | | | |
| | | 4.249 | 0.073 | 31.871 | | | | |
| | | 3.883 | 0.073 | 31.719 | | | | |
| | | 3.663 | 0.073 | 31.189 | | | | |
| | | 3.883 | 0.073 | 28.767 | | | | |
| | | 4.542 | 0.073 | 29.448 | | | | |
| | | 4.615 | 0.073 | 27.404 | | | | |
| | | 4.982 | 0.073 | 28.464 | | | | |
| | | 5.128 | 0.073 | 26.042 | | | | |
| | | 4.615 | 0.073 | 28.313 | | | | |
| | | 4.249 | 0.073 | 27.556 | | | | |
| | | 4.103 | 0.073 | 29.448 | | | | |
| | | 4.029 | 0.073 | 27.253 | | | | |
| | | 3.883 | 0.073 | 25.512 | | | | |
| | | 3.738 | 0.073 | 25.512 | | | | |
| | | 4.029 | 0.073 | 26.042 | | | | |
| | | 4.322 | 0.073 | 25.057 | | | | |
| | | 4.322 | 0.073 | 26.42 | | | Stratification Check Point No. 2 | |
| | | 4.322 | 0.073 | 30.129 | | | Average O2 = | 20.600 |
| | | 4.396 | 0.073 | 30.129 | | | Average CO2 = | 0.150 |
| | | 4.469 | 0.073 | 30.659 | | | | |
| | | 4.322 | 0.073 | 27.707 | | | Deviation from mean, O2 = | 0.06% |
| | | | | | | | Deviation from mean, CO2 = | 1.05% |
| | | | | | | | | |
| | | | | | | | Stratification Check Point No. 3 | |
| | | | | | | | Average O2 = | 20.949 |
| | | | | | | | Average CO2 = | 0.189 |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|----------|--------|--------|--|--|--|---------------------------------|------------|
| | | % | % | VOC 3 ppm C ₄ H ₈ | VOC 1 ppm C ₄ H ₈ | VOC 2 ppm C ₄ H ₈ | | |
| 12/8/2008 | 13:56:10 | 20.944 | 0.152 | 4.908 | 0.073 | 29.145 | Deviation from mean, O2 = | 0.24% |
| 12/8/2008 | 13:56:20 | 20.853 | 0.152 | 4.029 | 0.073 | 25.436 | Deviation from mean, CO2 = | 1.95% |
| 12/8/2008 | 13:56:30 | 20.853 | 0.183 | 4.322 | 0.073 | 22.559 | | |
| 12/8/2008 | 13:56:40 | 20.883 | 0.152 | 4.396 | 0.073 | 21.424 | Overall Average, O2 = | 20.800 |
| 12/8/2008 | 13:56:50 | 20.898 | 0.183 | 4.103 | 0.073 | 20.591 | Overall Average, CO2 = | 0.177 |
| 12/8/2008 | 13:57:00 | 20.853 | 0.183 | 1.319 | 0.073 | 19.304 | | |
| 12/8/2008 | 13:57:10 | 20.837 | 0.183 | 1.245 | 0.073 | 19.38 | | |
| 12/8/2008 | 13:57:20 | 20.822 | 0.183 | 1.382 | 0.073 | 19.226 | Greatest Deviation | |
| 12/8/2008 | 13:57:30 | 20.822 | 0.183 | 1.538 | 0.073 | 19.807 | O2 = 0.24% | |
| 12/8/2008 | 13:57:40 | 20.853 | 0.183 | 1.758 | 0.073 | 18.698 | CO2 = 3.89% | |
| 12/8/2008 | 13:57:50 | 20.868 | 0.183 | 1.665 | 0.073 | 116.264 | | |
| 12/8/2008 | 13:58:00 | 20.853 | 0.183 | 1.685 | 0.073 | 114.652 | | |
| 12/8/2008 | 13:58:10 | 20.837 | 0.183 | 1.685 | 0.073 | 135.238 | | |
| 12/8/2008 | 13:58:20 | 20.853 | 0.183 | 1.685 | 0.073 | 17.79 | Largest CO2 difference is | 0.010 |
| 12/8/2008 | 13:58:30 | 20.883 | 0.152 | 1.685 | 0.073 | 167.892 | Single point sampling okay. | |
| 12/8/2008 | 13:58:40 | 20.853 | 0.183 | 1.685 | 0.073 | 15.519 | | |
| 12/8/2008 | 13:58:50 | 20.868 | 0.183 | 1.685 | 0.073 | 229.231 | | |
| 12/8/2008 | 13:59:00 | 20.853 | 0.183 | 1.685 | 0.073 | 16.595 | | |
| 12/8/2008 | 13:59:10 | 20.853 | 0.213 | 1.685 | 0.073 | 231.282 | | |
| 12/8/2008 | 13:59:20 | 20.853 | 0.183 | 1.685 | 0.073 | 191.722 | | |
| 12/8/2008 | 13:59:30 | 20.883 | 0.152 | 1.685 | 0.073 | 14.081 | | |
| 12/8/2008 | 13:59:40 | 20.868 | 0.183 | 1.685 | 0.073 | 234.139 | | |
| 12/8/2008 | 13:59:50 | 20.853 | 0.183 | 1.685 | 0.073 | 15.519 | | |
| 12/8/2008 | 14:00:00 | 20.822 | 0.183 | 1.685 | 0.073 | 235.092 | | |
| 12/8/2008 | 14:00:10 | 20.837 | 0.183 | 1.685 | 0.073 | 13.336 | | |
| 12/8/2008 | 14:00:20 | 20.853 | 0.183 | 1.685 | 0.073 | 236.41 | | |
| 12/8/2008 | 14:00:30 | 20.807 | 0.183 | 1.685 | 0.073 | 15.695 | | |
| 12/8/2008 | 14:00:40 | 20.853 | 0.183 | 1.685 | 0.073 | 236.264 | | |
| 12/8/2008 | 14:00:50 | 20.822 | 0.183 | 1.685 | 0.073 | 14.005 | | |
| 12/8/2008 | 14:01:00 | 20.807 | 0.152 | 1.685 | 0.073 | 236.996 | | |
| 12/8/2008 | 14:01:10 | 20.853 | 0.183 | 1.685 | 0.073 | 12.587 | | |
| 12/8/2008 | 14:01:20 | 20.837 | 0.183 | 1.685 | 0.073 | 237.289 | | |
| 12/8/2008 | 14:01:30 | 20.853 | 0.183 | 1.685 | 0.073 | 14.686 | | |
| 12/8/2008 | 14:01:40 | 20.807 | 0.183 | 1.685 | 0.073 | 238.315 | | |
| 12/8/2008 | 14:01:50 | 20.853 | 0.183 | 1.685 | 0.073 | 20.212 | | |
| 12/8/2008 | 14:02:00 | 20.883 | 0.183 | 1.685 | 0.073 | 13.396 | | |
| 12/8/2008 | 14:02:10 | 20.807 | 0.183 | 1.685 | 0.073 | 238.315 | | |
| 12/8/2008 | 14:02:20 | 20.853 | 0.183 | 1.685 | 0.073 | 15.973 | | |
| 12/8/2008 | 14:02:30 | 20.822 | 0.183 | 1.685 | 0.073 | 238.388 | | |
| 12/8/2008 | 14:02:40 | 20.807 | 0.152 | 1.685 | 0.073 | 13.096 | | |
| 12/8/2008 | 14:02:50 | 20.853 | 0.183 | 1.685 | 0.073 | 238.315 | | |
| 12/8/2008 | 14:03:00 | 20.822 | 0.731 | 1.685 | 0.073 | 12.567 | | |
| 12/8/2008 | 14:03:10 | 18.446 | 3.656 | 1.685 | 0.073 | 10.825 | | |
| 12/8/2008 | 14:03:20 | 12.81 | 6.854 | 1.685 | 0.073 | 11.961 | | |
| 12/8/2008 | 14:03:30 | 7.357 | 8.499 | 1.685 | 0.073 | 11.431 | | |
| 12/8/2008 | 14:03:40 | 3.595 | 9.231 | 1.685 | 0.073 | 11.734 | | |
| 12/8/2008 | 14:03:50 | 1.31 | 9.535 | 1.685 | 0.073 | 13.399 | | |
| 12/8/2008 | 14:04:00 | 0.015 | 9.718 | 1.685 | 0.073 | 13.324 | | |
| 12/8/2008 | 14:04:10 | 0.015 | 9.809 | 1.685 | 0.073 | 11.128 | | |
| 12/8/2008 | 14:04:20 | 0.015 | 9.87 | 1.685 | 0.073 | 13.626 | | |
| 12/8/2008 | 14:04:30 | 0.015 | 9.931 | 1.685 | 0.073 | 13.096 | | |
| 12/8/2008 | 14:04:40 | 0.015 | 10.053 | 1.685 | 0.073 | 13.248 | Post-test mid range drift check | 0.14% |
| 12/8/2008 | 14:04:50 | 0.015 | 10.084 | 1.685 | 0.073 | 13.248 | Post-test zero drift check | 0.06% |
| 12/8/2008 | 14:05:00 | 0.015 | 9.931 | 1.685 | 0.073 | 12.794 | | |
| 12/8/2008 | 14:05:10 | 0.015 | 9.627 | 1.685 | 0.073 | 13.778 | | |
| 12/8/2008 | 14:05:20 | 0.015 | 7.068 | 1.685 | 0.073 | 14.535 | | |
| 12/8/2008 | 14:05:30 | 3.991 | 3.503 | 1.685 | 0.073 | 19.985 | | |
| 12/8/2008 | 14:05:40 | 9.982 | 1.371 | 1.685 | 0.073 | 18.85 | | |
| 12/8/2008 | 14:05:50 | 14.638 | 0.579 | 1.685 | 0.073 | 18.093 | | |
| 12/8/2008 | 14:06:00 | 17.578 | 0.213 | 1.685 | 0.073 | 22.181 | | |
| 12/8/2008 | 14:06:10 | 19.268 | 0.091 | 1.685 | 0.073 | 23.241 | | |
| 12/8/2008 | 14:06:20 | 20.228 | 0.03 | 1.685 | 0.073 | 15.67 | | |
| 12/8/2008 | 14:06:30 | 20.716 | 0.03 | 1.685 | 0.073 | 14.913 | | |
| 12/8/2008 | 14:06:40 | 20.974 | 0.03 | 1.685 | 0.073 | 12.784 | | |
| 12/8/2008 | 14:06:50 | 21.112 | 0.03 | 1.685 | 0.073 | 11.355 | | |
| 12/8/2008 | 14:07:00 | 21.157 | 0.03 | 1.685 | 0.073 | 11.734 | | |
| 12/8/2008 | 14:07:10 | 20.853 | 0.03 | 1.685 | 0.073 | 11.204 | | |
| 12/8/2008 | 14:07:20 | 20.776 | 0.03 | 1.685 | 0.073 | 10.901 | | |
| 12/8/2008 | 14:07:30 | 20.866 | 0.03 | 1.685 | 0.073 | 11.204 | | |
| 12/8/2008 | 14:07:40 | 20.883 | 0.03 | 1.685 | 0.073 | 15.14 | | |
| 12/8/2008 | 14:07:50 | 20.898 | 0.03 | 1.685 | 0.073 | 14.383 | Post-test zero drift check | 0.00% |
| 12/8/2008 | 14:08:00 | 20.914 | 0.03 | 1.685 | 0.073 | 13.324 | | |
| 12/8/2008 | 14:08:10 | 20.929 | 0.03 | 1.685 | 0.073 | 13.929 | | |
| 12/8/2008 | 14:08:20 | 20.853 | 0.03 | 1.685 | 0.073 | 14.762 | | |
| 12/8/2008 | 14:08:30 | 20.883 | 0.03 | 1.685 | 0.073 | 12.339 | | |
| 12/8/2008 | 14:08:40 | 20.894 | 0.03 | 1.685 | 0.073 | 15.897 | | |
| 12/8/2008 | 14:08:50 | 20.837 | 0.122 | 1.685 | 0.073 | 16.427 | Post-test mid range drift check | 0.22% |
| 12/8/2008 | 14:09:00 | 20.865 | 0.244 | 1.685 | 0.073 | 15.973 | | |
| 12/8/2008 | 14:09:10 | 20.533 | 0.305 | 1.685 | 0.073 | 15.443 | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Boothouse | Calibration Comments | Error % |
|---------------------------------------|----------|--------|-------|-----------------------------------|-----------------------------------|-----------------------------------|-------------------------|------------|
| | | % | % | ppm C ₂ H ₆ | ppm C ₂ H ₆ | ppm C ₂ H ₆ | | |
| 12/8/2008 | 14:07:20 | 20.426 | 0.335 | 1.099 | 125.861 | 12.945 | | |
| 12/8/2008 | 14:07:30 | 20.385 | 0.335 | 1.685 | 230.696 | 14.535 | | |
| 12/8/2008 | 14:07:40 | 20.304 | 0.335 | 1.099 | 196.484 | 10.977 | | |
| 12/8/2008 | 14:07:50 | 20.319 | 0.335 | 0.879 | 200.806 | 13.096 | | |
| 12/8/2008 | 14:08:00 | 20.304 | 0.335 | 1.245 | 219.56 | 16.579 | | |
| 12/8/2008 | 14:08:10 | 20.289 | 0.335 | 1.319 | 232.088 | 16.579 | | |
| 12/8/2008 | 14:08:20 | 20.289 | 0.335 | 1.099 | 237.856 | 13.778 | | |
| 12/8/2008 | 14:08:30 | 20.335 | 0.335 | 0.879 | 240.806 | 12.339 | | |
| 12/8/2008 | 14:08:40 | 20.335 | 0.335 | 0.952 | 242.418 | 9.614 | | |
| 12/8/2008 | 14:08:50 | 20.304 | 0.335 | 1.392 | 244.542 | 9.841 | | |
| 12/8/2008 | 14:09:00 | 20.304 | 0.335 | 1.685 | 246.96 | 11.204 | | |
| 12/8/2008 | 14:09:10 | 20.304 | 0.366 | 0.952 | 248.205 | 11.053 | | |
| 12/8/2008 | 14:09:20 | 20.304 | 0.366 | 0.733 | 249.158 | 11.734 | | |
| 12/8/2008 | 14:09:30 | 20.304 | 0.366 | 0.806 | 251.355 | 10.674 | | |
| Test Day Calibrations and Data | | | | | | | | |
| 12/9/2008 | 6:46:14 | 18.324 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:46:24 | 18.309 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:46:34 | 18.324 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:46:44 | 18.309 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:46:54 | 18.324 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:47:04 | 18.644 | 0.305 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:47:14 | 20.336 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:47:24 | 20.914 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:47:34 | 20 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:47:44 | 18.813 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:47:54 | 18.309 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:48:04 | 18.233 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:48:14 | 18.233 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:48:24 | 18.949 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:48:34 | 21.584 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:48:44 | 21.706 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:48:54 | 21.401 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:49:04 | 20.868 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:49:14 | 20.883 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:49:24 | 20.914 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:49:34 | 20.868 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:49:44 | 20.868 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:49:54 | 20.868 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:50:04 | 20.015 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:50:14 | 20.182 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:50:24 | 14.272 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:50:34 | 11.272 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:50:44 | 10.068 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:50:54 | 9.55 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:51:04 | 9.352 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:51:14 | 9.246 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:51:24 | 9.474 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:51:34 | 9.886 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:51:44 | 9.886 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:51:54 | 9.931 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:52:04 | 9.916 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:52:14 | 0.015 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:52:24 | 8.439 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:52:34 | 8.408 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:52:44 | 0.015 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:52:54 | 8.454 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:53:04 | 8.468 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:53:14 | 8.469 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:53:24 | 8.484 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:53:34 | 8.499 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:53:44 | 8.637 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:53:54 | 9.733 | 0.03 | 0.244 | 0.024 | 3.256 | | |
| 12/9/2008 | 6:54:04 | 7.707 | 0.03 | 0.244 | 0.024 | 0.757 | | |
| 12/9/2008 | 6:54:14 | 9.124 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:54:24 | 9.52 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:54:34 | 9.672 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:54:44 | 9.748 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:54:54 | 9.794 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:55:04 | 9.962 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:55:14 | 9.946 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:55:24 | 9.962 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:55:34 | 9.962 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:55:44 | 10.007 | 0.03 | 0.244 | 0.024 | 0.303 | | |
| 12/9/2008 | 6:55:54 | 10.007 | 0.03 | 0.244 | 0.024 | 0.379 | | |
| 12/9/2008 | 6:56:04 | 8.911 | 0.03 | 0.244 | 0.024 | 0.076 | | |

Hi range calibration gas 0.15%

Zero gas 0.14%

Mid Range gas 0.03%

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|---------|--------|--------|-----------------------------------|-----------------------------------|-----------------------------------|----------------------|---------|
| | | % | % | ppm C ₂ H ₆ | ppm C ₂ H ₆ | ppm C ₂ H ₆ | | |
| 12/9/2008 | 6:56:14 | 9.764 | 0.487 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:56:24 | 7.266 | 20.228 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:56:34 | 2.072 | 20.898 | 1.221 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:56:44 | 0.015 | 20.959 | 3.419 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:56:54 | 0.015 | 21.02 | 5.128 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:57:04 | 0.015 | 21.02 | 3.663 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:57:14 | 0.015 | 21.051 | 0.244 | 0.024 | 0.606 | | |
| 12/9/2008 | 6:57:24 | 0.015 | 20.959 | 0.244 | 0.024 | 0.681 | | |
| 12/9/2008 | 6:57:34 | 0.015 | 20.959 | 0.244 | 0.024 | 0.681 | | |
| 12/9/2008 | 6:57:44 | 0.015 | 20.959 | 0.244 | 0.024 | 0.379 | | |
| 12/9/2008 | 6:57:54 | 0.015 | 14.349 | 0.244 | 0.024 | 0.379 | | |
| 12/9/2008 | 6:58:04 | 0.015 | 10.449 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:58:14 | 0.015 | 10.145 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:58:24 | 0.015 | 9.779 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:58:34 | 0.015 | 9.605 | 1.221 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:58:44 | 0.015 | 9.139 | 2.93 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:58:54 | 0.015 | 8.987 | 1.954 | 0.024 | 0.076 | | |
| 12/9/2008 | 6:59:04 | 0.015 | 8.895 | 1.954 | 0.024 | 0.379 | | |
| 12/9/2008 | 6:59:14 | 0.015 | 8.621 | 1.709 | 0.024 | 0.454 | | |
| 12/9/2008 | 6:59:24 | 0.015 | 8.408 | 1.485 | 0.024 | 0.53 | | |
| 12/9/2008 | 6:59:34 | 0.015 | 8.804 | 0.733 | 0.024 | 0.454 | | |
| 12/9/2008 | 6:59:44 | 0.015 | 9.413 | 0.733 | 0.024 | 0.379 | | |
| 12/9/2008 | 6:59:54 | 0.015 | 9.322 | 2.198 | 0.024 | 0.303 | | |
| 12/9/2008 | 7:00:04 | 0.015 | 9.231 | 3.175 | 0.024 | 0.303 | | |
| 12/9/2008 | 7:00:14 | 0.015 | 9.078 | 5.128 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:00:24 | 0.015 | 9.383 | 3.663 | 0.024 | 0.303 | | |
| 12/9/2008 | 7:00:34 | 0.015 | 9.931 | 0.244 | 0.024 | 0.908 | | |
| 12/9/2008 | 7:00:44 | 0.015 | 9.901 | 0.244 | 0.024 | 1.06 | | |
| 12/9/2008 | 7:00:54 | 0.015 | 10.053 | 0.244 | 0.024 | 0.984 | | |
| 12/9/2008 | 7:01:04 | 0.015 | 9.992 | 0.244 | 0.024 | 1.136 | | |
| 12/9/2008 | 7:01:14 | 0.015 | 9.962 | 0.244 | 0.024 | 0.757 | | |
| 12/9/2008 | 7:01:24 | 0.015 | 9.962 | 0.244 | 0.024 | 0.757 | | |
| 12/9/2008 | 7:01:34 | 0.015 | 10.053 | 0.244 | 0.024 | 0.833 | | |
| 12/9/2008 | 7:01:44 | 0.015 | 9.992 | 0.244 | 0.024 | 0.908 | | |
| 12/9/2008 | 7:01:54 | 0.015 | 9.962 | 0.244 | 0.024 | 1.211 | | |
| 12/9/2008 | 7:02:04 | 0.015 | 9.901 | 0.244 | 0.024 | 1.211 | | |
| 12/9/2008 | 7:02:14 | 0.015 | 8.931 | 2.198 | 0.024 | 0.681 | | |
| 12/9/2008 | 7:02:24 | 0.015 | 9.779 | 3.419 | 0.024 | 0.151 | | |
| 12/9/2008 | 7:02:34 | 0.015 | 0.426 | 0.244 | 0.024 | 0.53 | | |
| 12/9/2008 | 7:02:44 | 3.503 | 0.03 | 0.244 | 0.024 | 0.908 | | |
| 12/9/2008 | 7:02:54 | 9.535 | 0.03 | 0.244 | 0.024 | 1.287 | | |
| 12/9/2008 | 7:03:04 | 13.221 | 0.03 | 0.244 | 0.024 | 1.287 | | |
| 12/9/2008 | 7:03:14 | 17.593 | 0.03 | 3.175 | 0.024 | 0.379 | | |
| 12/9/2008 | 7:03:24 | 20.045 | 0.03 | 0.733 | 0.024 | 0.53 | | |
| 12/9/2008 | 7:03:34 | 20.548 | 0.457 | 0.244 | 0.024 | 1.136 | | |
| 12/9/2008 | 7:03:44 | 20.457 | 0.426 | 0.244 | 0.024 | 1.211 | | |
| 12/9/2008 | 7:03:54 | 20.67 | 0.274 | 1.221 | 0.024 | 0.984 | | |
| 12/9/2008 | 7:04:04 | 20.898 | 0.03 | 2.442 | 0.024 | 0.379 | | |
| 12/9/2008 | 7:04:14 | 20.959 | 0.03 | 0.244 | 0.024 | 0.681 | | |
| 12/9/2008 | 7:04:24 | 21.188 | 0.03 | 0.244 | 0.024 | 1.06 | | |
| 12/9/2008 | 7:04:34 | 21.294 | 0.03 | 0.244 | 0.024 | 1.514 | | |
| 12/9/2008 | 7:04:44 | 20.807 | 0.03 | 0.244 | 0.024 | 1.363 | | |
| 12/9/2008 | 7:04:54 | 20.837 | 0.03 | 0.244 | 0.024 | 1.211 | | |
| 12/9/2008 | 7:05:04 | 20.929 | 0.03 | 0.244 | 0.024 | 1.136 | | |
| 12/9/2008 | 7:05:14 | 20.944 | 0.03 | 0.244 | 0.024 | 1.136 | | |
| 12/9/2008 | 7:05:24 | 20.99 | 0.03 | 0.244 | 0.024 | 1.267 | | |
| 12/9/2008 | 7:05:34 | 20.883 | 0.03 | 0.244 | 0.024 | 1.363 | | |
| 12/9/2008 | 7:05:44 | 20.868 | 0.03 | 0.244 | 0.024 | 1.363 | | |
| 12/9/2008 | 7:05:54 | 20.883 | 0.03 | 0.244 | 0.024 | 1.136 | | |
| 12/9/2008 | 7:06:04 | 20.837 | 0.03 | 0.244 | 0.024 | 0.833 | | |
| 12/9/2008 | 7:06:14 | 20.822 | 0.03 | 3.863 | 0.024 | 0.454 | | |
| 12/9/2008 | 7:06:24 | 20.853 | 0.03 | 0.244 | 0.024 | 1.211 | | |
| 12/9/2008 | 7:06:34 | 20.898 | 0.03 | 0.244 | 0.024 | 1.438 | | |
| 12/9/2008 | 7:06:44 | 20.824 | 1.188 | 0.244 | 0.024 | 1.211 | | |
| 12/9/2008 | 7:06:54 | 17.273 | 5.544 | 0.244 | 0.024 | 0.908 | | |
| 12/9/2008 | 7:07:04 | 11.18 | 8.347 | 0.244 | 0.024 | 0.833 | | |
| 12/9/2008 | 7:07:14 | 5.94 | 9.779 | 3.863 | 0.024 | 0.379 | | |
| 12/9/2008 | 7:07:24 | 2.805 | 10.48 | 0.244 | 0.024 | 1.363 | | |
| 12/9/2008 | 7:07:34 | 0.731 | 10.358 | 0.244 | 0.024 | 1.514 | | |
| 12/9/2008 | 7:07:44 | 0.015 | 10.205 | 0.244 | 0.024 | 1.363 | | |
| 12/9/2008 | 7:07:54 | 0.015 | 10.084 | 0.244 | 0.024 | 0.908 | | |
| 12/9/2008 | 7:08:04 | 0.015 | 10.053 | 0.244 | 0.024 | 0.908 | | |
| 12/9/2008 | 7:08:14 | 0.015 | 9.992 | 1.465 | 0.024 | 0.606 | | |
| 12/9/2008 | 7:08:24 | 0.015 | 9.992 | 3.419 | 0.024 | 0.606 | | |
| 12/9/2008 | 7:08:34 | 0.015 | 9.992 | 2.198 | 0.024 | 0.681 | | |

Hi range system bias check 0.07%
Zero system bias check 0.00%

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 % | CO2 % | RTO Inlet | | | RTO Outlet | | | Baghouse | | | Calibration Comments | Error % |
|-----------|---------|---------|----------|--|--|--|--|---|---|----------|--|--|-------------------------|------------|
| | | | | VOC 3 ppm C ₂ H ₆ | VOC 1 ppm C ₂ H ₆ | VOC 2 ppm C ₂ H ₆ | RTO Inlet ppm C ₂ H ₆ | RTO Outlet ppm C ₂ H ₆ | Baghouse ppm C ₂ H ₆ | | | | | |
| 12/9/2008 | 7:08:44 | 0.015 | 9.992 | 1.709 | 0.024 | 0.757 | | | | | | | | |
| 12/9/2008 | 7:08:54 | 0.015 | 9.992 | 0.977 | 0.024 | 1.211 | | | | | | | | |
| 12/9/2008 | 7:09:04 | 0.015 | 9.992 | 0.244 | 0.024 | 1.438 | | | | | | | | |
| 12/9/2008 | 7:09:14 | 0.015 | 9.992 | 0.244 | 0.024 | 1.59 | | | | | | | | |
| 12/9/2008 | 7:09:24 | 0.015 | 9.992 | 0.244 | 0.024 | 1.59 | | | | | | | | |
| 12/9/2008 | 7:09:34 | 0.015 | 9.995 | 0.244 | 0.024 | 1.59 | | | | | | | | |
| 12/9/2008 | 7:09:44 | 2.254 | 4.448 | 0.244 | 0.024 | 1.59 | | | | | | | | |
| 12/9/2008 | 7:09:54 | 8.317 | 1.98 | 0.244 | 0.024 | 1.665 | | | | | | | | |
| 12/9/2008 | 7:10:04 | 13.374 | 0.883 | 0.244 | 0.024 | 1.665 | | | | | | | | |
| 12/9/2008 | 7:10:14 | 16.709 | 0.366 | 0.244 | 0.024 | 1.287 | | | | | | | | |
| 12/9/2008 | 7:10:24 | 18.69 | 0.122 | 0.244 | 0.024 | 1.514 | | | | | | | | |
| 12/9/2008 | 7:10:34 | 19.756 | 0.03 | 0.244 | 0.024 | 1.287 | | | | | | | | |
| 12/9/2008 | 7:10:44 | 20.35 | 0.03 | 0.244 | 0.024 | 1.136 | | | | | | | | |
| 12/9/2008 | 7:10:54 | 20.609 | 0.03 | 0.244 | 0.024 | 1.136 | | | | | | | | |
| 12/9/2008 | 7:11:04 | 20.781 | 0.03 | 0.244 | 0.024 | 1.665 | | | | | | | | |
| 12/9/2008 | 7:11:14 | 20.868 | 0.03 | 0.244 | 61.905 | 2.271 | | | | | | | | |
| 12/9/2008 | 7:11:24 | 20.898 | 0.03 | 0.244 | 86.349 | 2.725 | | | | | | | | |
| 12/9/2008 | 7:11:34 | 20.914 | 0.03 | 0.244 | 64.2 | 3.558 | | | | | | | | |
| 12/9/2008 | 7:11:44 | 20.929 | 0.03 | 0.244 | 80.073 | 4.466 | | | | | | | | |
| 12/9/2008 | 7:11:54 | 20.944 | 0.03 | 0.244 | 58.828 | 4.391 | | | | | | | | |
| 12/9/2008 | 7:12:04 | 20.959 | 0.03 | 0.244 | 61.05 | 4.239 | | | | | | | | |
| 12/9/2008 | 7:12:14 | 20.944 | 0.061 | 0.733 | 78.974 | 3.937 | | | | | | | | |
| 12/9/2008 | 7:12:24 | 20.959 | 0.03 | 0.244 | 93.7 | 3.937 | | | | | | | | |
| 12/9/2008 | 7:12:34 | 20.959 | 0.03 | 0.244 | 99.096 | 4.088 | | | | | | | | |
| 12/9/2008 | 7:12:44 | 20.959 | 0.03 | 0.244 | 98.928 | 4.088 | | | | | | | | |
| 12/9/2008 | 7:12:54 | 20.959 | 0.03 | 0.244 | 98.706 | 3.785 | | | | | | | | |
| 12/9/2008 | 7:13:04 | 20.959 | 0.03 | 0.488 | 98.584 | 3.634 | | | | | | | | |
| 12/9/2008 | 7:13:14 | 20.959 | 0.03 | 0.977 | 98.437 | 3.709 | | | | | | | | |
| 12/9/2008 | 7:13:24 | 20.959 | 0.03 | 1.221 | 98.755 | 3.634 | | | | | | | | |
| 12/9/2008 | 7:13:34 | 20.974 | 0.03 | 0.733 | 99.023 | 3.709 | | | | | | | | |
| 12/9/2008 | 7:13:44 | 20.959 | 0.03 | 3.883 | 53.773 | 3.558 | | | | | | | | |
| 12/9/2008 | 7:13:54 | 20.944 | 0.03 | 0.244 | 44.688 | 3.709 | | | | | | | | |
| 12/9/2008 | 7:14:04 | 20.944 | 0.03 | 0.244 | 44.713 | 3.634 | | | | | | | | |
| 12/9/2008 | 7:14:14 | 20.929 | 0.03 | 0.977 | 44.688 | 3.634 | | | | | | | | |
| 12/9/2008 | 7:14:24 | 21.035 | 0.03 | 0.977 | 44.811 | 3.558 | | | | | | | | |
| 12/9/2008 | 7:14:34 | 21.035 | 0.03 | 0.977 | 44.908 | 3.558 | | | | | | | | |
| 12/9/2008 | 7:14:44 | 21.035 | 0.03 | 0.244 | 45.006 | 3.634 | | | | | | | | |
| 12/9/2008 | 7:14:54 | 21.02 | 0.03 | 0.488 | 45.055 | 3.558 | | | | | | | | |
| 12/9/2008 | 7:15:04 | 21.02 | 0.03 | 0.733 | 45.006 | 3.568 | | | | | | | | |
| 12/9/2008 | 7:15:14 | 21.02 | 0.03 | 0.244 | 45.177 | 3.634 | | | | | | | | |
| 12/9/2008 | 7:15:24 | 21.005 | 0.03 | 2.442 | 44.982 | 3.482 | | | | | | | | |
| 12/9/2008 | 7:15:34 | 21.02 | 0.03 | 4.64 | 45.128 | 3.255 | | | | | | | | |
| 12/9/2008 | 7:15:44 | 21.005 | 0.03 | 0.977 | 44.702 | 3.558 | | | | | | | | |
| 12/9/2008 | 7:15:54 | 21.005 | 0.03 | 1.221 | 48.23 | 3.558 | | | | | | | | |
| 12/9/2008 | 7:16:04 | 21.005 | 0.03 | 2.442 | 50.085 | 3.255 | | | | | | | | |
| 12/9/2008 | 7:16:14 | 21.035 | 0.03 | 1.709 | 50.183 | 3.407 | | | | | | | | |
| 12/9/2008 | 7:16:24 | 21.035 | 0.03 | 1.954 | 50.281 | 3.709 | | | | | | | | |
| 12/9/2008 | 7:16:34 | 21.02 | 0.03 | 0.977 | 50.501 | 3.709 | | | | | | | | |
| 12/9/2008 | 7:16:44 | 21.02 | 0.03 | 0.244 | 50.476 | 3.861 | | | | | | | | |
| 12/9/2008 | 7:16:54 | 21.02 | 0.03 | 0.244 | 50.823 | 3.861 | | | | | | | | |
| 12/9/2008 | 7:17:04 | 21.005 | 0.03 | 0.244 | 50.769 | 3.937 | | | | | | | | |
| 12/9/2008 | 7:17:14 | 21.02 | 0.03 | 0 | 38.777 | 3.407 | | | | | | | | |
| 12/9/2008 | 7:17:24 | 21.051 | 0.03 | 0.244 | 21.319 | 3.709 | | | | | | | | |
| 12/9/2008 | 7:17:34 | 21.035 | 0.03 | 0.244 | 0.024 | 3.558 | | | | | | | | |
| 12/9/2008 | 7:17:44 | 17.837 | 0.03 | 0.244 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 7:17:54 | 17.684 | 0.03 | 0.244 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 7:18:04 | 17.684 | 0.03 | 0.244 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 7:18:14 | 21.005 | 0.03 | 2.188 | 8.107 | 3.634 | | | | | | | | |
| 12/9/2008 | 7:18:24 | 21.035 | 0.03 | 0.244 | 9.695 | 3.861 | | | | | | | | |
| 12/9/2008 | 7:18:34 | 21.035 | 0.03 | 0.244 | 9.719 | 3.861 | | | | | | | | |
| 12/9/2008 | 7:18:44 | 21.035 | 0.03 | 0.244 | 9.988 | 3.709 | | | | | | | | |
| 12/9/2008 | 7:18:54 | 21.02 | 0.03 | 2.442 | 10.061 | 3.331 | | | | | | | | |
| 12/9/2008 | 7:19:04 | 21.02 | 0.03 | 0.244 | 10.281 | 3.407 | | | | | | | | |
| 12/9/2008 | 7:19:14 | 21.005 | 0.03 | 0.244 | 10.379 | 3.709 | | | | | | | | |
| 12/9/2008 | 7:19:24 | 21.035 | 0.03 | 0.244 | 10.379 | 3.709 | | | | | | | | |
| 12/9/2008 | 7:19:34 | 21.051 | 0.03 | 0.244 | 10.698 | 3.558 | | | | | | | | |
| 12/9/2008 | 7:19:44 | 21.02 | 0.03 | 0.244 | 10.549 | 3.407 | | | | | | | | |
| 12/9/2008 | 7:19:54 | 21.02 | 0.03 | 0.244 | 31.551 | 3.179 | | | | | | | | |
| 12/9/2008 | 7:20:04 | 21.035 | 0.03 | 0.244 | 31.6 | 2.877 | | | | | | | | |
| 12/9/2008 | 7:20:14 | 21.02 | 0.03 | 0.244 | 31.795 | 3.179 | | | | | | | | |
| 12/9/2008 | 7:20:24 | 21.02 | 0.03 | 0.488 | 32.332 | 3.179 | | | | | | | | |
| 12/9/2008 | 7:20:34 | 21.005 | 0.03 | 0.733 | 31.038 | 3.331 | | | | | | | | |
| 12/9/2008 | 7:20:44 | 21.02 | 0.03 | 0.244 | 28.963 | 3.331 | | | | | | | | |
| 12/9/2008 | 7:20:54 | 21.005 | 0.03 | 0.733 | 33.431 | 3.407 | | | | | | | | |
| 12/9/2008 | 7:21:04 | 21.005 | 0.03 | 1.465 | 37.485 | 3.407 | | | | | | | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|---------|--------|------|-----------------------------------|-----------------------------------|-----------------------------------|-------------------------|------------|
| | | % | % | ppm C ₂ H ₆ | ppm C ₂ H ₆ | ppm C ₂ H ₆ | | |
| 12/9/2008 | 7:21:14 | 21.005 | 0.03 | 0.733 | 42.491 | 3.407 | | |
| 12/9/2008 | 7:21:24 | 21.02 | 0.03 | 0.733 | 47.326 | 3.255 | | |
| 12/9/2008 | 7:21:34 | 21.005 | 0.03 | 0.244 | 49.868 | 3.482 | | |
| 12/9/2008 | 7:21:44 | 21.02 | 0.03 | 3.663 | 50.72 | 3.028 | | |
| 12/9/2008 | 7:21:54 | 21.02 | 0.03 | 2.686 | 51.331 | 3.028 | | |
| 12/9/2008 | 7:22:04 | 21.005 | 0.03 | 0.733 | 51.917 | 3.407 | | |
| 12/9/2008 | 7:22:14 | 21.02 | 0.03 | 0.244 | 50.085 | 3.482 | | |
| 12/9/2008 | 7:22:24 | 21.005 | 0.03 | 0.244 | 22.125 | 3.407 | | |
| 12/9/2008 | 7:22:34 | 20.974 | 0.03 | 0.244 | 18.486 | 3.331 | | |
| 12/9/2008 | 7:22:44 | 20.974 | 0.03 | 0.244 | 18.808 | 3.104 | | |
| 12/9/2008 | 7:22:54 | 20.99 | 0.03 | 0.244 | 18.632 | 3.255 | | |
| 12/9/2008 | 7:23:04 | 20.99 | 0.03 | 0.244 | 18.535 | 3.255 | | |
| 12/9/2008 | 7:23:14 | 21.005 | 0.03 | 0.244 | 18.852 | 3.179 | | |
| 12/9/2008 | 7:23:24 | 21.005 | 0.03 | 0.244 | 22.882 | 3.255 | | |
| 12/9/2008 | 7:23:34 | 21.005 | 0.03 | 0.244 | 25.275 | 3.255 | | |
| 12/9/2008 | 7:23:44 | 20.974 | 0.03 | 0.244 | 25.592 | 3.104 | | |
| 12/9/2008 | 7:23:54 | 20.99 | 0.03 | 0.244 | 24.908 | 3.265 | | |
| 12/9/2008 | 7:24:04 | 21.005 | 0.03 | 0.244 | 24.908 | 3.104 | | |
| 12/9/2008 | 7:24:14 | 21.005 | 0.03 | 0.244 | 25.006 | 3.255 | | |
| 12/9/2008 | 7:24:24 | 20.99 | 0.03 | 0.244 | 24.689 | 3.255 | | |
| 12/9/2008 | 7:24:34 | 20.974 | 0.03 | 0.244 | 25.055 | 3.028 | | |
| 12/9/2008 | 7:24:44 | 21.005 | 0.03 | 0.244 | 27.912 | 3.104 | | |
| 12/9/2008 | 7:24:54 | 21.005 | 0.03 | 0.244 | 45.006 | 3.104 | | |
| 12/9/2008 | 7:25:04 | 21.005 | 0.03 | 0.244 | 46.52 | 3.104 | | |
| 12/9/2008 | 7:25:14 | 21.02 | 0.03 | 0.244 | 47.106 | 3.179 | | |
| 12/9/2008 | 7:25:24 | 20.99 | 0.03 | 0.244 | 46.838 | 3.179 | | |
| 12/9/2008 | 7:25:34 | 21.005 | 0.03 | 0.733 | 44.103 | 3.179 | | |
| 12/9/2008 | 7:25:44 | 21.02 | 0.03 | 2.686 | 34.896 | 3.104 | | |
| 12/9/2008 | 7:25:54 | 21.005 | 0.03 | 2.93 | 28.816 | 3.179 | | |
| 12/9/2008 | 7:26:04 | 21.005 | 0.03 | 5.128 | 28.303 | 2.952 | | |
| 12/9/2008 | 7:26:14 | 21.005 | 0.03 | 4.64 | 28.205 | 2.725 | | |
| 12/9/2008 | 7:26:24 | 21.005 | 0.03 | 4.64 | 25.91 | 2.801 | | |
| 12/9/2008 | 7:26:34 | 21.005 | 0.03 | 2.198 | 24.737 | 3.331 | | |
| 12/9/2008 | 7:26:44 | 20.99 | 0.03 | 0.244 | 25.031 | 3.407 | | |
| 12/9/2008 | 7:26:54 | 20.99 | 0.03 | 0.244 | 25.275 | 3.331 | | |
| 12/9/2008 | 7:27:04 | 21.035 | 0.03 | 0.244 | 25.69 | 3.255 | | |
| 12/9/2008 | 7:27:14 | 21.035 | 0.03 | 0.244 | 26.129 | 3.634 | | |
| 12/9/2008 | 7:27:24 | 20.7 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:27:34 | 20.38 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:27:44 | 20.35 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:27:54 | 20.335 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:28:04 | 20.319 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:28:14 | 20.304 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:28:24 | 20.304 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:28:34 | 20.731 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:28:44 | 20.929 | 0.03 | 0.244 | 0.024 | 1.514 | | |
| 12/9/2008 | 7:28:54 | 20.822 | 0.03 | 0.244 | 0.024 | 0.53 | | |
| 12/9/2008 | 7:29:04 | 20.746 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:29:14 | 20.716 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:29:24 | 20.685 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:29:34 | 20.685 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:29:44 | 20.655 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:29:54 | 20.639 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:30:04 | 20.639 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:30:14 | 20.624 | 0.03 | 0.244 | 0.024 | 8.403 | | |
| 12/9/2008 | 7:30:24 | 20.609 | 0.03 | 0.244 | 0.024 | 193.495 | | |
| 12/9/2008 | 7:30:34 | 20.639 | 0.03 | 0.244 | 0.024 | 238.991 | | |
| 12/9/2008 | 7:30:44 | 20.639 | 0.03 | 0.244 | 0.024 | 258.252 | | |
| 12/9/2008 | 7:30:54 | 20.624 | 0.03 | 0.244 | 0.024 | 262.081 | | |
| 12/9/2008 | 7:31:04 | 20.609 | 0.03 | 0.244 | 0.024 | 265.467 | | |
| 12/9/2008 | 7:31:14 | 20.594 | 0.03 | 0.244 | 0.024 | 267.758 | | |
| 12/9/2008 | 7:31:24 | 20.609 | 0.03 | 0.244 | 0.024 | 269.499 | | |
| 12/9/2008 | 7:31:34 | 20.563 | 0.03 | 0.244 | 0.024 | 273.133 | | |
| 12/9/2008 | 7:31:44 | 20.594 | 0.03 | 0.244 | 0.024 | 293.8 | | |
| 12/9/2008 | 7:31:54 | 20.578 | 0.03 | 0.244 | 0.024 | 300.537 | | |
| 12/9/2008 | 7:32:04 | 20.609 | 0.03 | 0.244 | 0.024 | 299.175 | | |
| 12/9/2008 | 7:32:14 | 20.624 | 0.03 | 0.244 | 0.024 | 298.948 | | |
| 12/9/2008 | 7:32:24 | 20.594 | 0.03 | 0.244 | 0.024 | 299.856 | | |
| 12/9/2008 | 7:32:34 | 20.609 | 0.03 | 0.244 | 0.024 | 300.764 | | |
| 12/9/2008 | 7:32:44 | 20.624 | 0.03 | 0.244 | 0.024 | 298.115 | | |
| 12/9/2008 | 7:32:54 | 20.609 | 0.03 | 0.244 | 0.024 | 298.645 | | |
| 12/9/2008 | 7:33:04 | 20.594 | 0.03 | 0.244 | 0.024 | 299.25 | | |
| 12/9/2008 | 7:33:14 | 20.578 | 0.03 | 0.244 | 0.024 | 300.159 | | |
| 12/9/2008 | 7:33:24 | 20.578 | 0.03 | 0.244 | 0.024 | 300.84 | | |
| 12/9/2008 | 7:33:34 | 20.578 | 0.03 | 0.244 | 0.024 | 301.976 | | |

High range calibration gas 0.28%

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 % | CO2 % | RTO Inlet | | RTO Outlet | | Calibration Comments | Error % |
|-----------|---------|--------|-------|---|---|---|---|----------------------|---------|
| | | | | VOC 3 ppm C ₂ H ₆ | VOC 1 ppm C ₂ H ₆ | VOC 2 ppm C ₂ H ₆ | VOC 3 ppm C ₂ H ₆ | | |
| 12/9/2008 | 7:33:44 | 20.594 | 0.03 | 0.244 | 0.024 | 301.9 | | | |
| 12/9/2008 | 7:33:54 | 20.809 | 0.03 | 0.244 | 0.024 | 302.127 | | | |
| 12/9/2008 | 7:34:04 | 20.578 | 0.03 | 0.244 | 0.024 | 302.278 | | | |
| 12/9/2008 | 7:34:14 | 20.809 | 0.03 | 0.244 | 0.024 | 302.43 | | | |
| 12/9/2008 | 7:34:24 | 20.594 | 0.03 | 0.244 | 0.024 | 303.035 | | | |
| 12/9/2008 | 7:34:34 | 20.594 | 0.03 | 0 | 0.024 | 303.111 | | | |
| 12/9/2008 | 7:34:44 | 20.578 | 0.03 | 0.244 | 0.024 | 303.956 | | | |
| 12/9/2008 | 7:34:54 | 20.563 | 0.03 | 0.244 | 0.024 | 157.008 | | | |
| 12/9/2008 | 7:35:04 | 20.594 | 0.03 | 0.244 | 0.024 | 154.357 | | | |
| 12/9/2008 | 7:35:14 | 20.594 | 0.03 | 0.244 | 0.024 | 153.524 | | | |
| 12/9/2008 | 7:35:24 | 20.809 | 0.03 | 0.244 | 0.024 | 153.372 | | | |
| 12/9/2008 | 7:35:34 | 20.578 | 0.03 | 0.244 | 0.024 | 152.994 | | | |
| 12/9/2008 | 7:35:44 | 20.578 | 0.03 | 0.244 | 0.024 | 151.934 | | | |
| 12/9/2008 | 7:35:54 | 20.578 | 0.03 | 0.244 | 0.024 | 151.48 | | | |
| 12/9/2008 | 7:36:04 | 20.594 | 0.03 | 0.244 | 0.024 | 151.831 | | | |
| 12/9/2008 | 7:36:14 | 20.578 | 0.03 | 0.244 | 0.024 | 151.253 | | | |
| 12/9/2008 | 7:36:24 | 20.578 | 0.03 | 0.244 | 0.024 | 151.253 | | | |
| 12/9/2008 | 7:36:34 | 20.578 | 0.03 | 0.244 | 0.024 | 151.101 | | | |
| 12/9/2008 | 7:36:44 | 20.594 | 0.03 | 0.244 | 0.024 | 151.253 | | | |
| 12/9/2008 | 7:36:54 | 20.563 | 0.03 | 0.244 | 0.024 | 150.799 | | | |
| 12/9/2008 | 7:37:04 | 20.548 | 0.03 | 0.244 | 0.024 | 150.723 | Mid range calibration gas | 0.48% | |
| 12/9/2008 | 7:37:14 | 20.594 | 0.03 | 0.244 | 0.024 | 151.328 | | | |
| 12/9/2008 | 7:37:24 | 20.809 | 0.03 | 0.244 | 0.024 | 151.556 | | | |
| 12/9/2008 | 7:37:34 | 20.809 | 0.03 | 0.244 | 0.024 | 151.177 | | | |
| 12/9/2008 | 7:37:44 | 20.809 | 0.03 | 0.244 | 0.024 | 128.271 | | | |
| 12/9/2008 | 7:37:54 | 20.624 | 0.03 | 0.244 | 0.024 | 78.854 | | | |
| 12/9/2008 | 7:38:04 | 20.578 | 0.03 | 0.244 | 0.024 | 78.383 | | | |
| 12/9/2008 | 7:38:14 | 20.578 | 0.03 | 0.244 | 0.024 | 75.778 | | | |
| 12/9/2008 | 7:38:24 | 20.594 | 0.03 | 0.244 | 0.024 | 75.929 | | | |
| 12/9/2008 | 7:38:34 | 20.624 | 0.03 | 0.244 | 0.024 | 75.702 | | | |
| 12/9/2008 | 7:38:44 | 20.624 | 0.03 | 0.244 | 0.024 | 74.945 | | | |
| 12/9/2008 | 7:38:54 | 20.578 | 0.03 | 0.244 | 0.024 | 74.642 | | | |
| 12/9/2008 | 7:39:04 | 20.578 | 0.03 | 0.244 | 0.024 | 74.869 | | | |
| 12/9/2008 | 7:39:14 | 20.563 | 0.03 | 0.244 | 0.024 | 74.567 | | | |
| 12/9/2008 | 7:39:24 | 20.578 | 0.03 | 0.244 | 0.024 | 75.096 | | | |
| 12/9/2008 | 7:39:34 | 20.809 | 0.03 | 0.244 | 0.024 | 75.096 | Low range calibration gas | 0.13% | |
| 12/9/2008 | 7:39:44 | 20.839 | 0.03 | 0.244 | 0.024 | 74.718 | | | |
| 12/9/2008 | 7:39:54 | 20.809 | 0.03 | 0.244 | 0.024 | 74.339 | | | |
| 12/9/2008 | 7:40:04 | 20.594 | 0.03 | 0.244 | 0.024 | 74.188 | | | |
| 12/9/2008 | 7:40:14 | 20.563 | 0.03 | 0.244 | 0.024 | 74.339 | | | |
| 12/9/2008 | 7:40:24 | 20.578 | 0.03 | 0.244 | 0.024 | 74.112 | | | |
| 12/9/2008 | 7:40:34 | 20.578 | 0.03 | 0.244 | 0.024 | 62.151 | | | |
| 12/9/2008 | 7:40:44 | 20.563 | 0.03 | 0.244 | 0.024 | 1.665 | | | |
| 12/9/2008 | 7:40:54 | 20.563 | 0.03 | 0.244 | 0.024 | 0.076 | | | |
| 12/9/2008 | 7:41:04 | 20.578 | 0.03 | 0.244 | 0.024 | 0.076 | | | |
| 12/9/2008 | 7:41:14 | 20.578 | 0.03 | 0.244 | 0.024 | 0.076 | | | |
| 12/9/2008 | 7:41:24 | 20.594 | 0.03 | 0.244 | 0.024 | 0.076 | | | |
| 12/9/2008 | 7:41:34 | 20.594 | 0.03 | 0.244 | 0.024 | 0.076 | | | |
| 12/9/2008 | 7:41:44 | 20.809 | 0.03 | 0.244 | 0.024 | 0.076 | | | |
| 12/9/2008 | 7:41:54 | 20.809 | 0.03 | 0.244 | 0.024 | 0.076 | Zero gas | 0.02% | |
| 12/9/2008 | 7:42:04 | 20.594 | 0.03 | 0.244 | 0.024 | 0.076 | | | |
| 12/9/2008 | 7:42:14 | 20.809 | 0.03 | 0.244 | 0.024 | 0.076 | | | |
| 12/9/2008 | 7:42:24 | 20.594 | 0.03 | 0.244 | 0.024 | 0.076 | | | |
| 12/9/2008 | 7:42:34 | 20.594 | 0.03 | 897.436 | 0.024 | 0.076 | | | |
| 12/9/2008 | 7:42:44 | 20.624 | 0.03 | 921.367 | 0.024 | 0.076 | | | |
| 12/9/2008 | 7:42:54 | 20.594 | 0.03 | 925.519 | 0.024 | 0.076 | | | |
| 12/9/2008 | 7:43:04 | 20.809 | 0.03 | 928.205 | 0.024 | 0.076 | | | |
| 12/9/2008 | 7:43:14 | 20.578 | 0.03 | 933.088 | 0.024 | 0.076 | | | |
| 12/9/2008 | 7:43:24 | 20.563 | 0.03 | 934.554 | 0.024 | 0.076 | | | |
| 12/9/2008 | 7:43:34 | 20.578 | 0.03 | 937.728 | 0.024 | 0.076 | | | |
| 12/9/2008 | 7:43:44 | 20.563 | 0.03 | 938.708 | 0.024 | 0.076 | | | |
| 12/9/2008 | 7:43:54 | 20.563 | 0.03 | 938.95 | 0.024 | 0.076 | | | |
| 12/9/2008 | 7:44:04 | 20.563 | 0.03 | 938.462 | 0.024 | 0.076 | | | |
| 12/9/2008 | 7:44:14 | 20.563 | 0.03 | 938.462 | 0.024 | 0.076 | | | |
| 12/9/2008 | 7:44:24 | 20.578 | 0.03 | 940.659 | 0.024 | 0.076 | | | |
| 12/9/2008 | 7:44:34 | 20.563 | 0.03 | 941.638 | 0.024 | 0.076 | | | |
| 12/9/2008 | 7:44:44 | 20.578 | 0.03 | 940.904 | 0.024 | 0.076 | | | |
| 12/9/2008 | 7:44:54 | 20.578 | 0.03 | 999.756 | 0.024 | 0.076 | | | |
| 12/9/2008 | 7:45:04 | 20.594 | 0.03 | 999.756 | 0.024 | 0.076 | | | |
| 12/9/2008 | 7:45:14 | 20.609 | 0.03 | 979.976 | 0.024 | 0.076 | | | |
| 12/9/2008 | 7:45:24 | 20.578 | 0.03 | 999.512 | 0.024 | 0.076 | | | |
| 12/9/2008 | 7:45:34 | 20.809 | 0.03 | 999.756 | 0.024 | 0.076 | | | |
| 12/9/2008 | 7:45:44 | 20.594 | 0.03 | 999.756 | 0.024 | 0.076 | | | |
| 12/9/2008 | 7:45:54 | 20.594 | 0.03 | 999.756 | 0.024 | 0.076 | | | |
| 12/9/2008 | 7:46:04 | 20.578 | 0.03 | 999.756 | 0.024 | 0.076 | High range calibration gas | 0.02% | |
| 12/9/2008 | 7:46:14 | 20.578 | 0.03 | 999.756 | 0.024 | 0.076 | | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|---------|--------|------|--|--|--|-------------------------|------------|
| | | % | % | VOC 3 ppm C ₄ H ₈ | VOC 1 ppm C ₄ H ₈ | VOC 2 ppm C ₄ H ₈ | | |
| 12/9/2008 | 7:46:14 | 20.578 | 0.03 | 570.696 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:46:24 | 20.563 | 0.03 | 508.913 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:46:34 | 20.548 | 0.03 | 508.181 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:46:44 | 20.578 | 0.03 | 502.808 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:46:54 | 20.578 | 0.03 | 498.168 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:47:04 | 20.578 | 0.03 | 501.098 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:47:14 | 20.548 | 0.03 | 503.297 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:47:24 | 20.578 | 0.03 | 501.343 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:47:34 | 20.578 | 0.03 | 499.145 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:47:44 | 20.578 | 0.03 | 497.192 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:47:54 | 20.548 | 0.03 | 500.368 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:48:04 | 20.548 | 0.03 | 504.029 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:48:14 | 20.548 | 0.03 | 503.297 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:48:24 | 20.578 | 0.03 | 502.32 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:48:34 | 20.563 | 0.03 | 500.122 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:48:44 | 20.563 | 0.03 | 498.901 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:48:54 | 20.578 | 0.03 | 492.552 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:49:04 | 20.594 | 0.03 | 492.552 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:49:14 | 20.609 | 0.03 | 494.017 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:49:24 | 20.624 | 0.03 | 498.168 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:49:34 | 20.608 | 0.03 | 496.948 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:49:44 | 20.594 | 0.03 | 497.68 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:49:54 | 20.578 | 0.03 | 499.634 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:50:04 | 20.563 | 0.03 | 499.878 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:50:14 | 20.578 | 0.03 | 354.335 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:50:24 | 20.563 | 0.03 | 249.328 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:50:34 | 20.563 | 0.03 | 246.107 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:50:44 | 20.578 | 0.03 | 248.352 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:50:54 | 20.578 | 0.03 | 248.352 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:51:04 | 20.594 | 0.03 | 246.642 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:51:14 | 20.578 | 0.03 | 247.375 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:51:24 | 20.578 | 0.03 | 245.685 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:51:34 | 20.578 | 0.03 | 245.685 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:51:44 | 20.594 | 0.03 | 243.468 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:51:54 | 20.594 | 0.03 | 241.026 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:52:04 | 20.609 | 0.03 | 105.983 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:52:14 | 20.609 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:52:24 | 20.609 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:52:34 | 20.594 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:52:44 | 20.578 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:52:54 | 20.563 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:53:04 | 20.563 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:53:14 | 20.594 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:53:24 | 20.609 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:53:34 | 20.609 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:53:44 | 20.624 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:53:54 | 20.639 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:54:04 | 20.624 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:54:14 | 20.609 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:54:24 | 20.624 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:54:34 | 20.624 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:54:44 | 20.639 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:54:54 | 20.639 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:55:04 | 20.624 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:55:14 | 20.578 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:55:24 | 20.578 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:55:34 | 20.639 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:55:44 | 20.639 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:55:54 | 20.655 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:56:04 | 20.609 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:56:14 | 20.594 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:56:24 | 20.578 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:56:34 | 20.594 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:56:44 | 20.594 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:56:54 | 20.578 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:57:04 | 20.578 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:57:14 | 20.594 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 7:57:24 | 20.609 | 0.03 | 0.244 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:15:56 | 19.969 | 0.03 | 521.795 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:16:06 | 20.015 | 0.03 | 519.744 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:16:16 | 20.03 | 0.03 | 520 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:16:26 | 20.061 | 0.03 | 497.438 | 0 | 0.076 | | |
| 12/9/2008 | 8:16:36 | 19.969 | 0.03 | 498.718 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:16:46 | 20.396 | 0.03 | 520.256 | 0.024 | 3.104 | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 % | CO2 % | RTO Inlet | | | RTO Outlet | | | Baghouse | | | Calibration Comments | Error % |
|-----------|---------|---------|----------|--|--|--|--|--|--|--|--|--|-------------------------|------------|
| | | | | VOC 3 ppm C ₂ H ₆ | VOC 1 ppm C ₂ H ₆ | VOC 2 ppm C ₂ H ₆ | VOC 3 ppm C ₂ H ₆ | VOC 1 ppm C ₂ H ₆ | VOC 2 ppm C ₂ H ₆ | VOC 3 ppm C ₂ H ₆ | VOC 1 ppm C ₂ H ₆ | VOC 2 ppm C ₂ H ₆ | | |
| 12/9/2008 | 8:16:56 | 19.969 | 0.03 | 499.231 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:17:08 | 19.893 | 0.03 | 42.821 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:17:16 | 19.878 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:17:26 | 19.839 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:17:36 | 20.03 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:17:46 | 20.03 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:17:56 | 20 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:18:06 | 19.954 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:18:16 | 19.893 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:18:26 | 20.304 | 0.03 | 2.051 | 0.024 | 2.65 | | | | | | | | |
| 12/9/2008 | 8:18:36 | 19.832 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:18:46 | 19.756 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:18:56 | 19.786 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:19:06 | 19.908 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:19:16 | 20.03 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:19:26 | 20.076 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:19:36 | 20.091 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:19:46 | 20.045 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:19:56 | 19.984 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:20:06 | 20.396 | 0.03 | 5.841 | 0.024 | 2.725 | | | | | | | | |
| 12/9/2008 | 8:20:16 | 19.923 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:20:26 | 19.893 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:20:36 | 19.878 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:20:46 | 19.939 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:20:56 | 20.015 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:21:06 | 20.061 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:21:16 | 20.03 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:21:26 | 19.954 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:21:36 | 19.893 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:21:46 | 20.319 | 0.03 | 7.436 | 0.024 | 2.12 | | | | | | | | |
| 12/9/2008 | 8:21:56 | 19.847 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:22:06 | 19.817 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:22:16 | 19.878 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:22:26 | 20.03 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:22:36 | 20.091 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:22:46 | 20.121 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:22:56 | 20.091 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:23:06 | 20.045 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:23:16 | 20 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:23:26 | 20.411 | 0.03 | 0.769 | 0.024 | 3.255 | | | | | | | | |
| 12/9/2008 | 8:23:36 | 19.969 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:23:46 | 19.878 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:23:56 | 19.847 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:24:06 | 19.939 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:24:16 | 20.091 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:24:26 | 20.091 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:24:36 | 20.03 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:24:46 | 19.984 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:24:56 | 19.969 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:25:06 | 20.319 | 0.03 | 0.256 | 0.024 | 2.422 | | | | | | | | |
| 12/9/2008 | 8:25:16 | 19.883 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:25:26 | 19.908 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:25:36 | 19.939 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:25:46 | 19.954 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:25:56 | 20 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:26:06 | 20.076 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:26:16 | 20.106 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:26:26 | 20.045 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:26:36 | 19.969 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:26:46 | 20.38 | 0.061 | 11.026 | 0.024 | 2.877 | | | | | | | | |
| 12/9/2008 | 8:26:56 | 19.893 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:27:06 | 19.863 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:27:16 | 19.878 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:27:26 | 19.954 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:27:36 | 20.045 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:27:46 | 20.091 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:27:56 | 20.03 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:28:06 | 19.839 | 0.03 | 0.256 | 0.024 | 0 | | | | | | | | |
| 12/9/2008 | 8:28:16 | 19.954 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:28:26 | 20.304 | 0.091 | 11.026 | 0.024 | 2.422 | | | | | | | | |
| 12/9/2008 | 8:28:36 | 19.832 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:28:46 | 19.802 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:28:56 | 19.786 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:29:06 | 19.878 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |
| 12/9/2008 | 8:29:16 | 20 | 0.03 | 0.256 | 0.024 | 0.076 | | | | | | | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|---------|--------|-------|-----------------------------------|-----------------------------------|-----------------------------------|-------------------------|------------|
| | | % | % | ppm C ₂ H ₆ | ppm C ₂ H ₆ | ppm C ₂ H ₆ | | |
| 12/9/2008 | 8:29:26 | 20.091 | 0.03 | 0.256 | 0.024 | 0 | | |
| 12/9/2008 | 8:29:36 | 20.091 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:29:46 | 20.03 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:29:56 | 19.984 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:30:06 | 20.411 | 0.091 | 0.513 | 0.024 | 3.937 | | |
| 12/9/2008 | 8:30:16 | 19.969 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:30:26 | 19.939 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:30:36 | 19.984 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:30:46 | 20.015 | 0.03 | 0.256 | 0 | 0.076 | | |
| 12/9/2008 | 8:30:56 | 20.076 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:31:06 | 20.091 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:31:16 | 20.061 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:31:26 | 20 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:31:36 | 19.939 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:31:46 | 20.304 | 0.091 | 0.256 | 0.024 | 3.785 | | |
| 12/9/2008 | 8:31:56 | 19.878 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:32:06 | 19.786 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:32:16 | 19.802 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:32:26 | 19.939 | 0.03 | 0.256 | 0 | 0.076 | | |
| 12/9/2008 | 8:32:36 | 20.137 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:32:46 | 20.167 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:32:56 | 20.091 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:33:06 | 20.045 | 0.03 | 0.266 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:33:16 | 20.03 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:33:26 | 20.365 | 0.091 | 0.256 | 0.024 | 3.785 | | |
| 12/9/2008 | 8:33:36 | 19.923 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:33:46 | 19.832 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:33:56 | 19.847 | 0.03 | 0.256 | 0 | 0.076 | | |
| 12/9/2008 | 8:34:06 | 19.984 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:34:16 | 20.137 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:34:26 | 20.198 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:34:36 | 20.152 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:34:46 | 20.061 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:34:56 | 20.03 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:35:06 | 20.365 | 0.091 | 0.256 | 0.024 | 3.482 | | |
| 12/9/2008 | 8:35:16 | 19.923 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:35:26 | 19.878 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:35:36 | 19.863 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:35:46 | 19.923 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:35:56 | 20 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:36:06 | 20.076 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:36:16 | 20.045 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:36:26 | 19.989 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:36:36 | 19.989 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:36:46 | 20.365 | 0.061 | 4.359 | 0.024 | 2.877 | | |
| 12/9/2008 | 8:36:56 | 19.969 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:37:06 | 19.969 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:37:16 | 20 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:37:26 | 20.061 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:37:36 | 20.152 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:37:46 | 20.137 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:37:56 | 20.121 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:38:06 | 20.045 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:38:16 | 19.954 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:38:26 | 20.304 | 0.122 | 0.256 | 0.024 | 3.255 | | |
| 12/9/2008 | 8:38:36 | 19.863 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:38:46 | 19.847 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:38:56 | 19.847 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:39:06 | 19.863 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:39:16 | 19.908 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:39:26 | 20 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:39:36 | 20.061 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:39:46 | 20.045 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:39:56 | 20 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:40:06 | 20.335 | 0.061 | 0.256 | 0.024 | 3.104 | | |
| 12/9/2008 | 8:40:16 | 19.854 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:40:26 | 19.832 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:40:36 | 19.832 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:40:46 | 20.03 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:40:56 | 20.152 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:41:06 | 20.076 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:41:16 | 20.106 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:41:26 | 20 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:41:36 | 19.954 | 0.03 | 2.051 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:41:46 | 19.954 | 0.03 | 0.256 | 0.024 | 0.227 | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|---------|--------|-------|-----------------------------------|-----------------------------------|-----------------------------------|-------------------------|------------|
| | | % | % | ppm C ₂ H ₆ | ppm C ₂ H ₆ | ppm C ₂ H ₆ | | |
| 12/9/2008 | 8:41:56 | 20.243 | 0.091 | 0.256 | 0.024 | 3.331 | | |
| 12/9/2008 | 8:42:06 | 19.908 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:42:16 | 19.878 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:42:26 | 19.854 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:42:36 | 19.984 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:42:46 | 20.106 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:42:56 | 20.198 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:43:06 | 20.061 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:43:16 | 20 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:43:26 | 19.884 | 0.03 | 0.256 | 0.024 | 0.379 | | |
| 12/9/2008 | 8:43:36 | 20 | 0.03 | 0.256 | 0.024 | 0.379 | | |
| 12/9/2008 | 8:43:46 | 19.854 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:43:56 | 19.923 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:44:06 | 20.015 | 0.03 | 1.026 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:44:16 | 20.152 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:44:26 | 20.228 | 0.03 | 0.256 | 0.024 | 0.151 | | |
| 12/9/2008 | 8:44:36 | 20.167 | 0.03 | 0.256 | 0.024 | 0.151 | | |
| 12/9/2008 | 8:44:46 | 20.076 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:44:56 | 20.03 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:45:06 | 20 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:45:16 | 20.152 | 0.03 | 0.256 | 0.024 | 1.893 | | |
| 12/9/2008 | 8:45:26 | 19.939 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:45:36 | 19.923 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:45:46 | 19.908 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:45:56 | 19.893 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:46:06 | 19.863 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:46:16 | 19.863 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:46:26 | 19.878 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:46:36 | 19.908 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:46:46 | 19.954 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:46:56 | 20.045 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:47:06 | 20 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:47:16 | 20 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:47:26 | 19.969 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:47:36 | 20 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:47:46 | 19.984 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:47:56 | 19.969 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:48:06 | 19.939 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:48:16 | 19.939 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:48:26 | 19.939 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:48:36 | 19.984 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:48:46 | 19.969 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:48:56 | 19.984 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:49:06 | 19.984 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:49:16 | 19.969 | 0.03 | 0.256 | 0 | 0.024 | | 0.076 |
| 12/9/2008 | 8:49:26 | 19.954 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:49:36 | 19.923 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:49:46 | 19.923 | 0.03 | 1.282 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:49:56 | 19.923 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:50:06 | 19.969 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:50:16 | 20.045 | 0.03 | 0.256 | 0.024 | 0.681 | | |
| 12/9/2008 | 8:50:26 | 20.015 | 0.03 | 0.256 | 0.024 | 0.227 | | |
| 12/9/2008 | 8:50:36 | 20.015 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:50:46 | 19.854 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:50:56 | 19.939 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:51:06 | 19.939 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:51:16 | 19.939 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:51:26 | 20 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:51:36 | 20.015 | 0.03 | 0.256 | 0.024 | 0.53 | | |
| 12/9/2008 | 8:51:46 | 20.045 | 0.03 | 0.256 | 0.024 | 0.227 | | |
| 12/9/2008 | 8:51:56 | 20.076 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:52:06 | 19.954 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:52:16 | 19.923 | 0.03 | 1.026 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:52:26 | 19.954 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:52:36 | 19.984 | 0.03 | 0.256 | 0.024 | 0.227 | | |
| 12/9/2008 | 8:52:46 | 20.015 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:52:56 | 20.015 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:53:06 | 19.969 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:53:16 | 19.923 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:53:26 | 19.923 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:53:36 | 19.984 | 0.03 | 1.282 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:53:46 | 19.939 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:53:56 | 19.908 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:54:06 | 19.908 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:54:16 | 19.908 | 0.03 | 0.256 | 0.024 | 0.076 | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|---------|--------|------|--|--|--|-------------------------|------------|
| | | % | % | VOC 3 ppm C ₂ H ₆ | VOC 1 ppm C ₂ H ₆ | VOC 2 ppm C ₂ H ₆ | | |
| 12/9/2008 | 8:54:26 | 19.908 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:54:36 | 19.923 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:54:46 | 19.954 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:54:56 | 19.984 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:55:06 | 19.969 | 0.03 | 0.256 | 0.024 | 0.454 | | |
| 12/9/2008 | 8:55:16 | 20.03 | 0.03 | 0.256 | 0.024 | 1.136 | | |
| 12/9/2008 | 8:55:26 | 19.939 | 0.03 | 0.256 | 0.024 | 0.303 | | |
| 12/9/2008 | 8:55:36 | 19.893 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:55:46 | 19.893 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:55:56 | 19.923 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:56:06 | 19.954 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:56:16 | 19.954 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:56:26 | 19.939 | 0.03 | 0.256 | 0.024 | 0.454 | | |
| 12/9/2008 | 8:56:36 | 19.878 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:56:46 | 19.878 | 0.03 | 1.026 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:56:56 | 19.969 | 0.03 | 2.051 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:57:06 | 19.923 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:57:16 | 19.923 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:57:26 | 19.939 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:57:36 | 19.893 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:57:46 | 19.923 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:57:56 | 19.923 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:58:06 | 19.923 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:58:16 | 19.908 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:58:26 | 19.939 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:58:36 | 20 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:58:46 | 19.939 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:58:56 | 19.923 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:59:06 | 19.923 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:59:16 | 19.939 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:59:26 | 19.969 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:59:36 | 19.969 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 8:59:46 | 19.969 | 0.03 | 0.256 | 0.024 | 0.227 | | |
| 12/9/2008 | 8:59:56 | 19.969 | 0.03 | 0.256 | 0.024 | 0.908 | | |
| 12/9/2008 | 9:00:06 | 19.923 | 0.03 | 0.256 | 0.024 | 0.681 | | |
| 12/9/2008 | 9:00:16 | 19.954 | 0.03 | 0.256 | 0.024 | 0.53 | | |
| 12/9/2008 | 9:00:26 | 19.908 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 9:00:36 | 19.984 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 9:00:46 | 19.969 | 0.03 | 0.256 | 0.024 | 1.06 | | |
| 12/9/2008 | 9:00:56 | 19.908 | 0.03 | 0.256 | 0.024 | 0.379 | | |
| 12/9/2008 | 9:01:06 | 19.908 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 9:01:16 | 19.984 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 9:01:26 | 19.969 | 0.03 | 0.256 | 0.024 | 0.53 | | |
| 12/9/2008 | 9:01:36 | 19.954 | 0.03 | 0.256 | 0.024 | 0.908 | | |
| 12/9/2008 | 9:01:46 | 19.908 | 0.03 | 0.256 | 0.024 | 0.227 | | |
| 12/9/2008 | 9:01:56 | 19.969 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 9:02:06 | 19.984 | 0.03 | 0.256 | 0.024 | 0.53 | | |
| 12/9/2008 | 9:02:16 | 19.969 | 0.03 | 0.256 | 0.024 | 0.908 | | |
| 12/9/2008 | 9:02:26 | 19.893 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 9:02:36 | 19.939 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 9:02:46 | 19.954 | 0.03 | 0.256 | 0.024 | 0.833 | | |
| 12/9/2008 | 9:02:56 | 19.878 | 0.03 | 1.538 | 0.024 | 0.076 | | |
| 12/9/2008 | 9:03:06 | 19.969 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 9:03:16 | 19.939 | 0.03 | 0.256 | 0.024 | 0.757 | | |
| 12/9/2008 | 9:03:26 | 19.893 | 0.03 | 1.282 | 0.024 | 0.076 | | |
| 12/9/2008 | 9:03:36 | 20.03 | 0.03 | 0.256 | 0.024 | 1.136 | | |
| 12/9/2008 | 9:03:46 | 19.984 | 0.03 | 0.256 | 0.024 | 1.136 | | |
| 12/9/2008 | 9:03:56 | 19.908 | 0.03 | 2.308 | 0.024 | 0.076 | | |
| 12/9/2008 | 9:04:06 | 19.984 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 9:04:16 | 19.984 | 0.03 | 0.256 | 0.024 | 1.06 | | |
| 12/9/2008 | 9:04:26 | 19.908 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 9:04:36 | 19.954 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 9:04:46 | 19.984 | 0.03 | 0.256 | 0.024 | 0.908 | | |
| 12/9/2008 | 9:04:56 | 19.939 | 0.03 | 0.256 | 0.024 | 0.908 | | |
| 12/9/2008 | 9:05:06 | 19.923 | 0.03 | 0.789 | 0.024 | 0.076 | | |
| 12/9/2008 | 9:05:16 | 20.03 | 0.03 | 0.256 | 0.024 | 1.287 | | |
| 12/9/2008 | 9:05:26 | 20 | 0.03 | 0.256 | 0.024 | 1.136 | | |
| 12/9/2008 | 9:05:36 | 19.923 | 0.03 | 0.256 | 0.024 | 0.833 | | |
| 12/9/2008 | 9:05:46 | 19.908 | 0.03 | 2.584 | 0.024 | 0.076 | | |
| 12/9/2008 | 9:05:56 | 19.939 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 9:06:06 | 19.923 | 0.03 | 0.789 | 0.024 | 0.076 | | |
| 12/9/2008 | 9:06:16 | 20 | 0.03 | 0.256 | 0.024 | 0.303 | | |
| 12/9/2008 | 9:06:26 | 19.984 | 0.03 | 0.256 | 0.024 | 0.606 | | |
| 12/9/2008 | 9:06:36 | 20 | 0.03 | 0.256 | 0.024 | 0.833 | | |
| 12/9/2008 | 9:06:46 | 20 | 0.03 | 0.256 | 0.024 | 0.757 | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|---------|--------|------|-----------------------------------|-----------------------------------|-----------------------------------|-------------------------|------------|
| | | % | % | ppm C ₂ H ₆ | ppm C ₂ H ₆ | ppm C ₂ H ₆ | | |
| 12/9/2008 | 9:06:56 | 20.045 | 0.03 | 0.256 | 0.024 | 1.211 | | |
| 12/9/2008 | 9:07:06 | 20.015 | 0.03 | 0.256 | 0.024 | 0.757 | | |
| 12/9/2008 | 9:07:16 | 20 | 0.03 | 0.256 | 0.024 | 0.757 | | |
| 12/9/2008 | 9:07:26 | 20 | 0.03 | 0.256 | 0.024 | 0.681 | | |
| 12/9/2008 | 9:07:36 | 20 | 0.03 | 0.256 | 0.024 | 0.379 | | |
| 12/9/2008 | 9:07:46 | 19.984 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 9:07:56 | 19.989 | 0.03 | 0 | 0.024 | 0.076 | | |
| 12/9/2008 | 9:08:06 | 19.989 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 9:08:16 | 19.954 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 9:08:26 | 19.954 | 0.03 | 0.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 9:08:36 | 20 | 0.03 | 6.154 | 0.024 | 0.076 | | |
| 12/9/2008 | 9:08:46 | 19.989 | 0.03 | 1.026 | 0.024 | 0.076 | | |
| 12/9/2008 | 9:08:56 | 19.939 | 0.03 | 0.256 | 0.024 | 0.908 | | |
| 12/9/2008 | 9:09:06 | 19.954 | 0.03 | 0.256 | 0.024 | 1.287 | | |
| 12/9/2008 | 9:09:16 | 19.984 | 0.03 | 0.256 | 0.024 | 1.438 | | |
| 12/9/2008 | 9:09:26 | 19.984 | 0.03 | 0.256 | 0.024 | 1.685 | | |
| 12/9/2008 | 9:09:36 | 19.984 | 0.03 | 0.256 | 0.024 | 1.59 | | |
| 12/9/2008 | 9:09:46 | 20 | 0.03 | 0.256 | 0.024 | 1.514 | | |
| 12/9/2008 | 9:09:56 | 20 | 0.03 | 0.256 | 0.024 | 1.438 | | |
| 12/9/2008 | 9:10:06 | 20.015 | 0.03 | 0.256 | 0.024 | 1.438 | | |
| 12/9/2008 | 9:10:16 | 20.061 | 0.03 | 0.256 | 0.024 | 1.685 | | |
| 12/9/2008 | 9:10:26 | 20.03 | 0.03 | 0.256 | 0.024 | 1.06 | | |
| 12/9/2008 | 9:10:36 | 19.984 | 0.03 | 0.256 | 0.024 | 0.303 | | |
| 12/9/2008 | 9:10:46 | 19.954 | 0.03 | 0.256 | 0.024 | 0.151 | | |
| 12/9/2008 | 9:10:56 | 19.939 | 0.03 | 0.513 | 0.024 | 0.227 | | |
| 12/9/2008 | 9:11:06 | 19.939 | 0.03 | 3.59 | 0.024 | 0.303 | | |
| 12/9/2008 | 9:11:16 | 19.954 | 0.03 | 5.841 | 0.024 | 0.076 | | |
| 12/9/2008 | 9:11:26 | 19.954 | 0.03 | 4.359 | 0.024 | 0.151 | | |
| 12/9/2008 | 9:11:36 | 19.969 | 0.03 | 2.564 | 0.024 | 0.227 | | |
| 12/9/2008 | 9:11:46 | 19.984 | 0.03 | 0.256 | 0.024 | 0.454 | | |
| 12/9/2008 | 9:11:56 | 20.045 | 0.03 | 0.256 | 0.024 | 1.136 | | |
| 12/9/2008 | 9:12:06 | 20.045 | 0.03 | 0.256 | 0.024 | 2.12 | | |
| 12/9/2008 | 9:12:16 | 20.061 | 0.03 | 0.256 | 0.024 | 5.072 | | |
| 12/9/2008 | 9:12:26 | 20.03 | 0.03 | 0.256 | 0.024 | 6.208 | | |
| 12/9/2008 | 9:12:36 | 20.03 | 0.03 | 0.256 | 0.024 | 5.763 | | |
| 12/9/2008 | 9:12:46 | 20.03 | 0.03 | 0 | 0.024 | 5.753 | | |
| 12/9/2008 | 9:12:56 | 20.015 | 0.03 | 0.256 | 0.024 | 4.996 | | |
| 12/9/2008 | 9:13:06 | 20.03 | 0.03 | 0.256 | 0.024 | 4.315 | | |
| 12/9/2008 | 9:13:16 | 20.061 | 0.03 | 0.256 | 0.024 | 3.709 | | |
| 12/9/2008 | 9:13:26 | 20.045 | 0.03 | 0.256 | 0.024 | 3.634 | | |
| 12/9/2008 | 9:13:36 | 20.091 | 0.03 | 0.256 | 0.024 | 4.391 | | |
| 12/9/2008 | 9:13:46 | 20.03 | 0.03 | 0.256 | 0.024 | 4.088 | | |
| 12/9/2008 | 9:13:56 | 20.045 | 0.03 | 0.256 | 0.024 | 4.391 | | |
| 12/9/2008 | 9:14:06 | 20.03 | 0.03 | 0.256 | 0.024 | 4.694 | | |
| 12/9/2008 | 9:14:16 | 19.984 | 0.03 | 0.256 | 0.024 | 4.542 | | |
| 12/9/2008 | 9:14:26 | 19.969 | 0.03 | 0.256 | 0.024 | 4.391 | | |
| 12/9/2008 | 9:14:36 | 19.984 | 0.03 | 0.256 | 0.024 | 5.299 | | |
| 12/9/2008 | 9:14:46 | 20 | 0.03 | 1.282 | 0.024 | 14.156 | | |
| 12/9/2008 | 9:14:56 | 20 | 0.03 | 0.769 | 0.024 | 18.093 | | |
| 12/9/2008 | 9:15:06 | 20.045 | 0.03 | 0.256 | 0.024 | 19.834 | | |
| 12/9/2008 | 9:15:16 | 20.137 | 0.03 | 0.256 | 0.024 | 21.954 | | |
| 12/9/2008 | 9:15:26 | 20.091 | 0.03 | 0.256 | 0.024 | 22.786 | | |
| 12/9/2008 | 9:15:36 | 20 | 0.03 | 0.256 | 0.024 | 22.256 | | |
| 12/9/2008 | 9:15:46 | 19.893 | 0.03 | 10.256 | 0.024 | 20.867 | | |
| 12/9/2008 | 9:15:56 | 19.954 | 0.03 | 8.974 | 0.024 | 19.304 | | |
| 12/9/2008 | 9:16:06 | 20.03 | 0.03 | 0.256 | 0.024 | 20.667 | | |
| 12/9/2008 | 9:16:16 | 20.076 | 0.03 | 0.256 | 0.024 | 23.468 | | |
| 12/9/2008 | 9:16:26 | 19.984 | 0.03 | 0.256 | 0.024 | 24.225 | | |
| 12/9/2008 | 9:16:36 | 19.923 | 0.03 | 5.641 | 0.024 | 24.376 | | |
| 12/9/2008 | 9:16:46 | 19.839 | 0.03 | 15.385 | 0.024 | 22.711 | | |
| 12/9/2008 | 9:16:56 | 20.045 | 0.03 | 15.897 | 0.024 | 23.089 | | |
| 12/9/2008 | 9:17:06 | 20.03 | 0.03 | 3.333 | 0.024 | 21.861 | | |
| 12/9/2008 | 9:17:16 | 20.061 | 0.03 | 0.256 | 0.024 | 21.424 | | |
| 12/9/2008 | 9:17:26 | 20.091 | 0.03 | 0.256 | 0.024 | 22.256 | | |
| 12/9/2008 | 9:17:36 | 20.091 | 0.03 | 0.256 | 0.024 | 22.256 | | |
| 12/9/2008 | 9:17:46 | 20.091 | 0.03 | 0.256 | 0.024 | 24.225 | | |
| 12/9/2008 | 9:17:56 | 20.061 | 0.03 | 0.256 | 0.024 | 16.73 | | |
| 12/9/2008 | 9:18:06 | 20.03 | 0.03 | 0.256 | 0.024 | 9.993 | | |
| 12/9/2008 | 9:18:16 | 20 | 0.03 | 1.282 | 0.024 | 7.267 | | |
| 12/9/2008 | 9:18:26 | 19.954 | 0.03 | 13.077 | 0.024 | 4.996 | | |
| 12/9/2008 | 9:18:36 | 20.061 | 0.03 | 21.538 | 0.024 | 3.937 | | |
| 12/9/2008 | 9:18:46 | 20.015 | 0.03 | 19.231 | 0.024 | 2.271 | | |
| 12/9/2008 | 9:18:56 | 20 | 0.03 | 18.718 | 0.024 | 1.665 | | |
| 12/9/2008 | 9:19:06 | 19.969 | 0.03 | 21.538 | 0.024 | 1.438 | | |
| 12/9/2008 | 9:19:16 | 19.954 | 0.03 | 25.897 | 0.024 | 1.211 | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|---------|--------|-------|-----------------------------------|-----------------------------------|-----------------------------------|-------------------------|------------|
| | | % | % | ppm C ₂ H ₆ | ppm C ₂ H ₆ | ppm C ₂ H ₆ | | |
| 12/9/2008 | 9:19:26 | 19.939 | 0.03 | 35.385 | 0.024 | 0.908 | | |
| 12/9/2008 | 9:19:36 | 19.908 | 0.03 | 42.821 | 0.024 | 1.363 | | |
| 12/9/2008 | 9:19:46 | 19.923 | 0.03 | 39.744 | 0.024 | 2.801 | | |
| 12/9/2008 | 9:19:56 | 20 | 0.03 | 31.795 | 0.024 | 3.861 | | |
| 12/9/2008 | 9:20:06 | 20.078 | 0.03 | 35.126 | 0.024 | 4.486 | | |
| 12/9/2008 | 9:20:16 | 20.274 | 0.152 | 60.513 | 0.024 | 6.208 | | |
| 12/9/2008 | 9:20:26 | 20.167 | 0.122 | 136.41 | 0.024 | 3.558 | | |
| 12/9/2008 | 9:20:36 | 20.015 | 0.03 | 128.482 | 0.024 | 2.801 | | |
| 12/9/2008 | 9:20:46 | 20 | 0.03 | 71.026 | 0.024 | 4.542 | | |
| 12/9/2008 | 9:20:56 | 20.045 | 0.03 | 26.887 | 0.024 | 5.375 | | |
| 12/9/2008 | 9:21:06 | 20.03 | 0.03 | 78.205 | 0.024 | 3.861 | | |
| 12/9/2008 | 9:21:16 | 19.939 | 0.03 | 95.841 | 0.024 | 11.28 | | |
| 12/9/2008 | 9:21:26 | 19.893 | 0.03 | 91.282 | 0.024 | 27.783 | | |
| 12/9/2008 | 9:21:36 | 19.984 | 0.03 | 41.026 | 0.024 | 31.946 | | |
| 12/9/2008 | 9:21:46 | 20.061 | 0.03 | 30.769 | 0.024 | 30.811 | | |
| 12/9/2008 | 9:21:56 | 20.259 | 0.183 | 90.769 | 0.317 | 31.189 | | |
| 12/9/2008 | 9:22:06 | 20.106 | 0.122 | 105.841 | 0 | 28.767 | | |
| 12/9/2008 | 9:22:16 | 19.969 | 0.061 | 108.482 | 0.024 | 18.396 | | |
| 12/9/2008 | 9:22:26 | 19.969 | 0.03 | 94.359 | 0.024 | 16.048 | | |
| 12/9/2008 | 9:22:36 | 20.045 | 0.03 | 77.179 | 0.024 | 15.443 | | |
| 12/9/2008 | 9:22:46 | 20.061 | 0.061 | 99.487 | 0.024 | 13.551 | | |
| 12/9/2008 | 9:22:56 | 19.969 | 0.03 | 102.308 | 0.024 | 12.188 | | |
| 12/9/2008 | 9:23:06 | 19.939 | 0.03 | 101.538 | 0.024 | 10.977 | | |
| 12/9/2008 | 9:23:16 | 19.863 | 0.03 | 121.538 | 0.024 | 10.598 | | |
| 12/9/2008 | 9:23:26 | 19.923 | 0.061 | 133.59 | 0.024 | 11.507 | | |
| 12/9/2008 | 9:23:36 | 20.152 | 0.244 | 138.974 | 5.128 | 14.005 | | |
| 12/9/2008 | 9:23:46 | 20.152 | 0.244 | 137.179 | 0.024 | 13.853 | | |
| 12/9/2008 | 9:23:56 | 20.106 | 0.183 | 129.744 | 0.024 | 13.551 | | |
| 12/9/2008 | 9:24:06 | 20.045 | 0.122 | 121.026 | 0.024 | 14.838 | | |
| 12/9/2008 | 9:24:16 | 20 | 0.091 | 118.718 | 0.024 | 16.049 | | |
| 12/9/2008 | 9:24:26 | 19.984 | 0.091 | 103.848 | 0.024 | 17.866 | | |
| 12/9/2008 | 9:24:36 | 19.989 | 0.091 | 105.385 | 0.024 | 17.714 | | |
| 12/9/2008 | 9:24:46 | 19.969 | 0.091 | 106.41 | 0.024 | 16.73 | | |
| 12/9/2008 | 9:24:56 | 19.969 | 0.061 | 121.795 | 0.024 | 15.897 | | |
| 12/9/2008 | 9:25:06 | 19.984 | 0.091 | 178.41 | 0.024 | 16.352 | | |
| 12/9/2008 | 9:25:16 | 20.152 | 0.244 | 141.538 | 14.408 | 17.941 | | |
| 12/9/2008 | 9:25:26 | 20.167 | 0.244 | 113.333 | 0.024 | 17.487 | | |
| 12/9/2008 | 9:25:36 | 20.076 | 0.183 | 99.744 | 0.024 | 18.774 | | |
| 12/9/2008 | 9:25:46 | 20.03 | 0.152 | 91.538 | 0.024 | 30.054 | | |
| 12/9/2008 | 9:25:56 | 19.984 | 0.122 | 88.154 | 0.024 | 40.652 | | |
| 12/9/2008 | 9:26:06 | 19.939 | 0.091 | 83.846 | 0.024 | 41.409 | | |
| 12/9/2008 | 9:26:16 | 19.908 | 0.061 | 85.385 | 0.024 | 40.274 | | |
| 12/9/2008 | 9:26:26 | 19.908 | 0.061 | 87.179 | 0.024 | 37.548 | | |
| 12/9/2008 | 9:26:36 | 19.893 | 0.03 | 108.205 | 0.024 | 36.11 | | |
| 12/9/2008 | 9:26:46 | 19.954 | 0.091 | 125.897 | 0.024 | 24.452 | | |
| 12/9/2008 | 9:26:56 | 20.152 | 0.244 | 187.692 | 8.962 | 20.061 | | |
| 12/9/2008 | 9:27:06 | 20.152 | 0.244 | 187.179 | 0.024 | 18.774 | | |
| 12/9/2008 | 9:27:16 | 20.091 | 0.213 | 155.897 | 0.024 | 18.093 | | |
| 12/9/2008 | 9:27:26 | 20 | 0.152 | 138.205 | 0.024 | 15.897 | | |
| 12/9/2008 | 9:27:36 | 19.954 | 0.122 | 130.256 | 0.024 | 15.368 | | |
| 12/9/2008 | 9:27:46 | 19.969 | 0.091 | 138.744 | 0.024 | 14.838 | | |
| 12/9/2008 | 9:27:56 | 19.969 | 0.091 | 144.872 | 0.024 | 14.913 | | |
| 12/9/2008 | 9:28:06 | 20 | 0.091 | 126.923 | 0.024 | 15.973 | | |
| 12/9/2008 | 9:28:16 | 20 | 0.091 | 115.128 | 0.024 | 16.503 | | |
| 12/9/2008 | 9:28:26 | 20.03 | 0.091 | 127.436 | 0.024 | 17.336 | | |
| 12/9/2008 | 9:28:36 | 20.182 | 0.213 | 131.538 | 11.282 | 19.683 | | |
| 12/9/2008 | 9:28:46 | 20.213 | 0.213 | 188.154 | 0.024 | 22.258 | | |
| 12/9/2008 | 9:28:56 | 20.152 | 0.183 | 187.436 | 0.024 | 23.998 | | |
| 12/9/2008 | 9:29:06 | 20.091 | 0.152 | 170.513 | 0.024 | 25.209 | | |
| 12/9/2008 | 9:29:16 | 20.045 | 0.122 | 189.487 | 0.024 | 25.663 | | |
| 12/9/2008 | 9:29:26 | 20.045 | 0.152 | 206.923 | 0.024 | 24.579 | | |
| 12/9/2008 | 9:29:36 | 20 | 0.122 | 185.841 | 0.024 | 23.77 | | |
| 12/9/2008 | 9:29:46 | 19.923 | 0.122 | 190.513 | 0.024 | 23.316 | | |
| 12/9/2008 | 9:29:56 | 19.878 | 0.091 | 178.41 | 0.024 | 24.225 | | |
| 12/9/2008 | 9:30:06 | 19.939 | 0.183 | 190 | 0.024 | 24.073 | | |
| 12/9/2008 | 9:30:16 | 20.152 | 0.244 | 176.41 | 9.695 | 33.99 | | |
| 12/9/2008 | 9:30:26 | 20.188 | 0.213 | 144.359 | 0.024 | 49.131 | | |
| 12/9/2008 | 9:30:36 | 20.167 | 0.213 | 128.974 | 0.024 | 52.991 | | |
| 12/9/2008 | 9:30:46 | 20.061 | 0.183 | 146.923 | 0.024 | 49.282 | | |
| 12/9/2008 | 9:30:56 | 19.984 | 0.152 | 198.867 | 0.024 | 45.497 | | |
| 12/9/2008 | 9:31:06 | 20 | 0.03 | 220 | 0.024 | 41.788 | | |
| 12/9/2008 | 9:31:16 | 20.045 | 0.03 | 214.872 | 0.024 | 30.054 | | |
| 12/9/2008 | 9:31:26 | 20.078 | 0.03 | 207.179 | 0.024 | 26.289 | | |
| 12/9/2008 | 9:31:36 | 20.045 | 0.03 | 198.205 | 0.024 | 25.814 | | |
| 12/9/2008 | 9:31:46 | 20.091 | 0.03 | 178.205 | 0.024 | 25.057 | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|---------|--------|-------|-----------------------------------|-----------------------------------|-----------------------------------|-------------------------|------------|
| | | % | % | ppm C ₂ H ₆ | ppm C ₂ H ₆ | ppm C ₂ H ₆ | | |
| 12/9/2008 | 9:31:56 | 20.198 | 0.03 | 164.872 | 16.581 | 25.436 | | |
| 12/9/2008 | 9:32:06 | 20.198 | 0.081 | 173.59 | 0.024 | 24.527 | | |
| 12/9/2008 | 9:32:16 | 20.182 | 0.03 | 199.744 | 0.024 | 23.922 | | |
| 12/9/2008 | 9:32:26 | 20.152 | 0.03 | 182.051 | 0.024 | 22.938 | | |
| 12/9/2008 | 9:32:36 | 20.106 | 0.03 | 191.282 | 0.024 | 22.029 | | |
| 12/9/2008 | 9:32:46 | 20.045 | 0.03 | 208.974 | 0.024 | 21.499 | | |
| 12/9/2008 | 9:32:56 | 19.984 | 0.03 | 233.846 | 0.024 | 21.802 | | |
| 12/9/2008 | 9:33:06 | 19.923 | 0.03 | 247.692 | 0.024 | 24.603 | | |
| 12/9/2008 | 9:33:16 | 19.893 | 0.03 | 257.436 | 0.024 | 27.026 | | |
| 12/9/2008 | 9:33:26 | 20.045 | 0.061 | 249.231 | 0.024 | 31.416 | | |
| 12/9/2008 | 9:33:36 | 20.152 | 0.061 | 225.128 | 21.245 | 34.066 | | |
| 12/9/2008 | 9:33:46 | 20.182 | 0.091 | 273.846 | 0.073 | 32.476 | | |
| 12/9/2008 | 9:33:56 | 20.137 | 0.122 | 285.385 | 0.024 | 29.372 | | |
| 12/9/2008 | 9:34:06 | 20.03 | 0.091 | 286.154 | 0 | 28.891 | | |
| 12/9/2008 | 9:34:16 | 20 | 0.061 | 227.179 | 0.024 | 30.811 | | |
| 12/9/2008 | 9:34:26 | 20.03 | 0.03 | 190 | 0.024 | 32.552 | | |
| 12/9/2008 | 9:34:36 | 20.091 | 0.03 | 190.256 | 0.024 | 35.958 | | |
| 12/9/2008 | 9:34:46 | 19.984 | 0.03 | 207.949 | 0.024 | 49.131 | | |
| 12/9/2008 | 9:34:56 | 19.908 | 0.03 | 215.385 | 0.024 | 53.521 | | |
| 12/9/2008 | 9:35:06 | 19.984 | 0.03 | 194.615 | 0.024 | 55.414 | | |
| 12/9/2008 | 9:35:16 | 20.152 | 0.03 | 184.103 | 15.58 | 55.338 | | |
| 12/9/2008 | 9:35:26 | 20.198 | 0.061 | 201.026 | 0.024 | 54.733 | | |
| 12/9/2008 | 9:35:36 | 20.167 | 0.061 | 266.154 | 0.024 | 40.652 | | |
| 12/9/2008 | 9:35:46 | 20.091 | 0.061 | 274.615 | 0.024 | 32.779 | | |
| 12/9/2008 | 9:35:56 | 19.984 | 0.03 | 282.564 | 0.024 | 29.221 | | |
| 12/9/2008 | 9:36:06 | 19.839 | 0.03 | 267.949 | 0.024 | 29.221 | | |
| 12/9/2008 | 9:36:16 | 19.923 | 0.03 | 242.051 | 0.024 | 29.978 | | |
| 12/9/2008 | 9:36:26 | 19.854 | 0.03 | 222.308 | 0.024 | 29.448 | | |
| 12/9/2008 | 9:36:36 | 19.984 | 0.03 | 224.359 | 0.024 | 29.448 | | |
| 12/9/2008 | 9:36:46 | 20.121 | 0.03 | 228.718 | 0.024 | 29.524 | | |
| 12/9/2008 | 9:36:56 | 20.182 | 0.03 | 217.178 | 20.147 | 29.751 | | |
| 12/9/2008 | 9:37:06 | 20.182 | 0.03 | 233.846 | 0.317 | 29.978 | | |
| 12/9/2008 | 9:37:16 | 20.182 | 0.03 | 229.744 | 0.024 | 30.886 | | |
| 12/9/2008 | 9:37:26 | 20.182 | 0.03 | 250 | 0.024 | 33.006 | | |
| 12/9/2008 | 9:37:36 | 20.152 | 0.03 | 266.154 | 0.024 | 33.687 | | |
| 12/9/2008 | 9:37:46 | 20.137 | 0.03 | 268.974 | 0.024 | 34.974 | | |
| 12/9/2008 | 9:37:56 | 20.106 | 0.03 | 246.667 | 0.024 | 36.261 | | |
| 12/9/2008 | 9:38:06 | 20.091 | 0.03 | 300.256 | 0.024 | 36.034 | | |
| 12/9/2008 | 9:38:16 | 20.091 | 0.03 | 294.359 | 0.024 | 34.066 | | |
| 12/9/2008 | 9:38:26 | 20.091 | 0.03 | 256.667 | 0.024 | 34.823 | | |
| 12/9/2008 | 9:38:36 | 20.137 | 0.061 | 234.872 | 23.248 | 37.245 | | |
| 12/9/2008 | 9:38:46 | 20.152 | 0.091 | 220.256 | 0.024 | 37.927 | | |
| 12/9/2008 | 9:38:56 | 20.152 | 0.091 | 221.538 | 0.024 | 41.333 | | |
| 12/9/2008 | 9:39:06 | 20.121 | 0.061 | 205.128 | 0.024 | 56.825 | | |
| 12/9/2008 | 9:39:16 | 20.091 | 0.03 | 199.487 | 0.024 | 61.167 | | |
| 12/9/2008 | 9:39:26 | 20.091 | 0.03 | 197.436 | 0.024 | 60.41 | | |
| 12/9/2008 | 9:39:36 | 20.061 | 0.03 | 210.513 | 0.024 | 58.366 | | |
| 12/9/2008 | 9:39:46 | 20.015 | 0.03 | 226.41 | 0.024 | 58.063 | | |
| 12/9/2008 | 9:39:56 | 19.984 | 0.03 | 256.923 | 0.024 | 45.497 | | |
| 12/9/2008 | 9:40:06 | 20.076 | 0.091 | 263.846 | 0.024 | 38.305 | | |
| 12/9/2008 | 9:40:16 | 20.091 | 0.091 | 263.846 | 20.781 | 36.11 | | |
| 12/9/2008 | 9:40:26 | 20.106 | 0.091 | 269.744 | 0.513 | 34.747 | | |
| 12/9/2008 | 9:40:36 | 20.121 | 0.122 | 264.615 | 0.024 | 33.763 | | |
| 12/9/2008 | 9:40:46 | 20.106 | 0.091 | 253.077 | 0.024 | 33.233 | | |
| 12/9/2008 | 9:40:56 | 20.106 | 0.061 | 245.128 | 0.024 | 33.385 | | |
| 12/9/2008 | 9:41:06 | 20.106 | 0.03 | 234.615 | 0.024 | 32.249 | | |
| 12/9/2008 | 9:41:16 | 20.106 | 0.03 | 248.974 | 0.024 | 31.568 | | |
| 12/9/2008 | 9:41:26 | 20.081 | 0.03 | 271.538 | 0.024 | 30.811 | | |
| 12/9/2008 | 9:41:36 | 20.076 | 0.03 | 279.487 | 0.024 | 31.169 | | |
| 12/9/2008 | 9:41:46 | 20.076 | 0.091 | 297.692 | 0.024 | 33.46 | | |
| 12/9/2008 | 9:41:56 | 20.106 | 0.091 | 328.205 | 25.812 | 34.672 | | |
| 12/9/2008 | 9:42:06 | 20.137 | 0.122 | 346.923 | 0.024 | 35.201 | | |
| 12/9/2008 | 9:42:16 | 20.106 | 0.152 | 323.59 | 0.024 | 36.943 | | |
| 12/9/2008 | 9:42:26 | 20.045 | 0.122 | 360.256 | 0.024 | 35.429 | | |
| 12/9/2008 | 9:42:36 | 20 | 0.091 | 375.641 | 0.024 | 33.783 | | |
| 12/9/2008 | 9:42:46 | 19.954 | 0.091 | 332.308 | 0.024 | 35.201 | | |
| 12/9/2008 | 9:42:56 | 19.939 | 0.081 | 312.051 | 0.024 | 38.84 | | |
| 12/9/2008 | 9:43:06 | 19.923 | 0.03 | 281.026 | 0.024 | 37.851 | | |
| 12/9/2008 | 9:43:16 | 19.939 | 0.03 | 270.513 | 0.024 | 42.08 | | |
| 12/9/2008 | 9:43:26 | 20.091 | 0.091 | 265.385 | 0.024 | 58.972 | | |
| 12/9/2008 | 9:43:36 | 20.106 | 0.091 | 240.769 | 20.391 | 64.725 | | |
| 12/9/2008 | 9:43:46 | 20.152 | 0.091 | 223.333 | 0.757 | 65.179 | | |
| 12/9/2008 | 9:43:56 | 20.167 | 0.061 | 247.179 | 0.024 | 62.681 | | |
| 12/9/2008 | 9:44:06 | 20.182 | 0.091 | 264.103 | 0.024 | 63.363 | | |
| 12/9/2008 | 9:44:16 | 20.152 | 0.061 | 303.333 | 0.024 | 51.25 | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|---------|--------|-------|-----------------------------------|-----------------------------------|-----------------------------------|-------------------------|------------|
| | | % | % | ppm C ₆ H ₆ | ppm C ₆ H ₆ | ppm C ₆ H ₆ | | |
| 12/9/2008 | 9:44:26 | 20.045 | 0.061 | 316.667 | 0.024 | 40.425 | | |
| 12/9/2008 | 9:44:36 | 19.954 | 0.03 | 333.333 | 0.024 | 36.943 | | |
| 12/9/2008 | 9:44:46 | 19.939 | 0.03 | 319.744 | 0.024 | 36.337 | | |
| 12/9/2008 | 9:44:56 | 19.969 | 0.03 | 293.077 | 0.024 | 36.261 | | |
| 12/9/2008 | 9:45:06 | 20.045 | 0.03 | 272.821 | 0.024 | 37.321 | | |
| 12/9/2008 | 9:45:16 | 20.137 | 0.03 | 293.077 | 27.766 | 38.457 | | |
| 12/9/2008 | 9:45:26 | 20.182 | 0.03 | 281.282 | 0.024 | 37.775 | | |
| 12/9/2008 | 9:45:36 | 20.152 | 0.122 | 277.179 | 0.024 | 37.7 | | |
| 12/9/2008 | 9:45:46 | 20.121 | 0.213 | 286.154 | 0.024 | 37.245 | | |
| 12/9/2008 | 9:45:56 | 20.076 | 0.244 | 280.256 | 0.024 | 37.094 | | |
| 12/9/2008 | 9:46:06 | 20.03 | 0.213 | 301.538 | 0.024 | 38.457 | | |
| 12/9/2008 | 9:46:16 | 19.969 | 0.213 | 326.667 | 0.024 | 40.349 | | |
| 12/9/2008 | 9:46:26 | 19.939 | 0.213 | 357.949 | 0.024 | 41.106 | | |
| 12/9/2008 | 9:46:36 | 19.908 | 0.213 | 348.205 | 0.024 | 39.971 | | |
| 12/9/2008 | 9:46:46 | 20.03 | 0.335 | 425.897 | 0.024 | 39.819 | | |
| 12/9/2008 | 9:46:56 | 20.061 | 0.305 | 406.923 | 35.092 | 38.684 | | |
| 12/9/2008 | 9:47:06 | 20.121 | 0.305 | 382.308 | 3.887 | 39.744 | | |
| 12/9/2008 | 9:47:16 | 20.121 | 0.274 | 323.59 | 0.024 | 42.545 | | |
| 12/9/2008 | 9:47:26 | 20.121 | 0.244 | 282.051 | 0.024 | 45.27 | | |
| 12/9/2008 | 9:47:36 | 20.106 | 0.244 | 271.538 | 0.024 | 47.465 | | |
| 12/9/2008 | 9:47:46 | 20.03 | 0.244 | 282.308 | 0.024 | 61.897 | | |
| 12/9/2008 | 9:47:56 | 19.969 | 0.244 | 297.662 | 0.024 | 67.526 | | |
| 12/9/2008 | 9:48:06 | 19.969 | 0.213 | 293.333 | 0.024 | 68.164 | | |
| 12/9/2008 | 9:48:16 | 19.954 | 0.213 | 313.59 | 0.024 | 63.363 | | |
| 12/9/2008 | 9:48:26 | 20 | 0.274 | 331.282 | 0 | 64.195 | | |
| 12/9/2008 | 9:48:36 | 20.061 | 0.305 | 337.438 | 25.201 | 55.841 | | |
| 12/9/2008 | 9:48:46 | 20.108 | 0.305 | 338.41 | 0.024 | 47.087 | | |
| 12/9/2008 | 9:48:56 | 20.137 | 0.274 | 311.795 | 0.024 | 44.818 | | |
| 12/9/2008 | 9:49:06 | 20.137 | 0.244 | 301.282 | 0.024 | 42.545 | | |
| 12/9/2008 | 9:49:16 | 20.091 | 0.244 | 295.385 | 0.024 | 41.409 | | |
| 12/9/2008 | 9:49:26 | 20.081 | 0.244 | 307.949 | 0.024 | 39.214 | | |
| 12/9/2008 | 9:49:36 | 20.03 | 0.244 | 344.872 | 0.024 | 36.943 | | |
| 12/9/2008 | 9:49:46 | 19.984 | 0.244 | 345.385 | 0.024 | 34.596 | | |
| 12/9/2008 | 9:49:56 | 19.908 | 0.244 | 344.103 | 0.024 | 34.596 | | |
| 12/9/2008 | 9:50:06 | 20.015 | 0.335 | 335.641 | 0.024 | 37.17 | | |
| 12/9/2008 | 9:50:16 | 20.03 | 0.305 | 331.538 | 25.201 | 39.138 | | |
| 12/9/2008 | 9:50:26 | 20.091 | 0.244 | 320.769 | 1.978 | 42.469 | | |
| 12/9/2008 | 9:50:36 | 20.121 | 0.244 | 325.897 | 0.024 | 44.059 | | |
| 12/9/2008 | 9:50:46 | 20.121 | 0.274 | 351.028 | 0.024 | 43.832 | | |
| 12/9/2008 | 9:50:56 | 20.091 | 0.274 | 352.584 | 0.024 | 44.21 | | |
| 12/9/2008 | 9:51:06 | 20.03 | 0.274 | 394.615 | 0.024 | 44.059 | | |
| 12/9/2008 | 9:51:16 | 19.969 | 0.274 | 392.564 | 0.024 | 41.031 | | |
| 12/9/2008 | 9:51:26 | 19.923 | 0.244 | 390.513 | 0.024 | 40.349 | | |
| 12/9/2008 | 9:51:36 | 19.923 | 0.274 | 355.385 | 0.024 | 42.168 | | |
| 12/9/2008 | 9:51:46 | 19.923 | 0.274 | 350.256 | 0.024 | 44.967 | | |
| 12/9/2008 | 9:51:56 | 20.076 | 0.213 | 344.872 | 29.817 | 47.011 | | |
| 12/9/2008 | 9:52:06 | 20.213 | 0.213 | 330.266 | 0.024 | 62 | | |
| 12/9/2008 | 9:52:16 | 20.243 | 0.183 | 323.846 | 0.024 | 69.343 | | |
| 12/9/2008 | 9:52:26 | 20.274 | 0.122 | 318.462 | 0.024 | 69.192 | | |
| 12/9/2008 | 9:52:36 | 20.35 | 0.03 | 334.872 | 0.024 | 65.407 | | |
| 12/9/2008 | 9:52:46 | 20.398 | 0.03 | 349.744 | 0.024 | 65.937 | | |
| 12/9/2008 | 9:52:56 | 20.441 | 0.03 | 379.487 | 0.024 | 55.868 | | |
| 12/9/2008 | 9:53:06 | 20.457 | 0.03 | 381.538 | 0.024 | 47.087 | | |
| 12/9/2008 | 9:53:16 | 20.472 | 0.03 | 371.282 | 0.024 | 44.816 | | |
| 12/9/2008 | 9:53:26 | 20.578 | 0.03 | 337.438 | 0.024 | 44.891 | | |
| 12/9/2008 | 9:53:36 | 20.624 | 0.03 | 295.641 | 29.035 | 44.891 | | |
| 12/9/2008 | 9:53:46 | 20.624 | 0.061 | 291.026 | 3.077 | 43.68 | | |
| 12/9/2008 | 9:53:56 | 20.548 | 0.061 | 349.231 | 0.024 | 42.015 | | |
| 12/9/2008 | 9:54:06 | 20.487 | 0.03 | 384.872 | 0.024 | 39.744 | | |
| 12/9/2008 | 9:54:16 | 20.472 | 0.03 | 364.615 | 0.024 | 40.274 | | |
| 12/9/2008 | 9:54:26 | 20.517 | 0.03 | 348.974 | 0.024 | 42.166 | | |
| 12/9/2008 | 9:54:36 | 20.609 | 0.03 | 332.564 | 0.024 | 43.074 | | |
| 12/9/2008 | 9:54:46 | 20.639 | 0.03 | 388.974 | 0.024 | 43.68 | | |
| 12/9/2008 | 9:54:56 | 20.502 | 0.03 | 403.333 | 0.024 | 44.21 | | |
| 12/9/2008 | 9:55:06 | 20.306 | 0.03 | 433.846 | 0.024 | 45.724 | | |
| 12/9/2008 | 9:55:16 | 20.35 | 0.03 | 378.487 | 32.772 | 48.071 | | |
| 12/9/2008 | 9:55:26 | 20.319 | 0.03 | 428.205 | 0.073 | 48.222 | | |
| 12/9/2008 | 9:55:36 | 20.335 | 0.03 | 402.821 | 0.024 | 47.011 | | |
| 12/9/2008 | 9:55:46 | 20.396 | 0.03 | 390.258 | 0.024 | 46.254 | | |
| 12/9/2008 | 9:55:56 | 20.441 | 0.03 | 358.718 | 0.024 | 48.374 | | |
| 12/9/2008 | 9:56:06 | 20.472 | 0.03 | 363.846 | 0.024 | 49.206 | | |
| 12/9/2008 | 9:56:16 | 20.487 | 0.03 | 379.231 | 0.024 | 50.493 | | |
| 12/9/2008 | 9:56:26 | 20.502 | 0.03 | 355.128 | 0.024 | 64.877 | | |
| 12/9/2008 | 9:56:36 | 20.517 | 0.03 | 351.538 | 0.024 | 73.053 | | |
| 12/9/2008 | 9:56:46 | 20.594 | 0.03 | 351.026 | 0.024 | 75.096 | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|----------|--------|-------|--|--|--|-------------------------|------------|
| | | % | % | VOC 3 ppm C ₂ H ₆ | VOC 1 ppm C ₂ H ₆ | VOC 2 ppm C ₂ H ₆ | | |
| 12/9/2008 | 9:56:56 | 20.533 | 0.03 | 353.077 | 22.002 | 71.89 | | |
| 12/9/2008 | 9:57:06 | 20.457 | 0.03 | 332.051 | 1.172 | 72.447 | | |
| 12/9/2008 | 9:57:16 | 20.426 | 0.03 | 342.564 | 0.024 | 63.06 | | |
| 12/9/2008 | 9:57:26 | 20.502 | 0.03 | 356.154 | 0.024 | 52.386 | | |
| 12/9/2008 | 9:57:36 | 20.578 | 0.03 | 335.897 | 0.024 | 48.979 | | |
| 12/9/2008 | 9:57:46 | 20.624 | 0.03 | 328.154 | 0.024 | 47.541 | | |
| 12/9/2008 | 9:57:56 | 20.639 | 0.03 | 298.205 | 0.024 | 46.784 | | |
| 12/9/2008 | 9:58:06 | 20.609 | 0.03 | 302.821 | 0.024 | 45.951 | | |
| 12/9/2008 | 9:58:16 | 20.472 | 0.03 | 334.359 | 0.024 | 45.346 | | |
| 12/9/2008 | 9:58:26 | 20.38 | 0.03 | 354.872 | 0.024 | 44.513 | | |
| 12/9/2008 | 9:58:36 | 20.319 | 0.03 | 364.359 | 25.788 | 43.832 | | |
| 12/9/2008 | 9:58:46 | 20.304 | 0.03 | 372.051 | 0.024 | 42.923 | | |
| 12/9/2008 | 9:58:56 | 20.259 | 0.03 | 386.41 | 0.024 | 43.15 | | |
| 12/9/2008 | 9:59:06 | 20.335 | 0.03 | 388.923 | 0.024 | 43.907 | | |
| 12/9/2008 | 9:59:16 | 20.457 | 0.03 | 399.744 | 0.024 | 44.589 | | |
| 12/9/2008 | 9:59:26 | 20.533 | 0.03 | 390.513 | 0.024 | 46.405 | | |
| 12/9/2008 | 9:59:36 | 20.594 | 0.03 | 365.385 | 0.024 | 46.374 | | |
| 12/9/2008 | 9:59:46 | 20.639 | 0.03 | 408.205 | 0.024 | 48.374 | | |
| 12/9/2008 | 9:59:56 | 20.578 | 0.03 | 387.438 | 0.024 | 46.178 | | |
| 12/9/2008 | 10:00:06 | 20.533 | 0.03 | 383.59 | 0.024 | 46.86 | | |
| 12/9/2008 | 10:00:16 | 20.457 | 0.03 | 363.333 | 26.227 | 46.784 | | |
| 12/9/2008 | 10:00:26 | 20.396 | 0.03 | 352.821 | 1.636 | 48.222 | | |
| 12/9/2008 | 10:00:36 | 20.411 | 0.03 | 365.385 | 0.024 | 49.282 | | |
| 12/9/2008 | 10:00:46 | 20.441 | 0.03 | 356.41 | 0.024 | 62.606 | | |
| 12/9/2008 | 10:00:56 | 20.563 | 0.03 | 342.821 | 0.024 | 72.068 | | |
| 12/9/2008 | 10:01:06 | 20.639 | 0.03 | 319.744 | 0.024 | 73.981 | | |
| 12/9/2008 | 10:01:16 | 20.855 | 0.03 | 300 | 0.024 | 72.598 | | |
| 12/9/2008 | 10:01:26 | 20.609 | 0.03 | 309.231 | 0.024 | 72.75 | | |
| 12/9/2008 | 10:01:36 | 20.426 | 0.03 | 357.692 | 0.024 | 64.347 | | |
| 12/9/2008 | 10:01:46 | 20.385 | 0.03 | 387.692 | 0.024 | 51.175 | | |
| 12/9/2008 | 10:01:56 | 20.365 | 0.03 | 372.308 | 24.591 | 46.935 | | |
| 12/9/2008 | 10:02:06 | 20.396 | 0.03 | 315.897 | 0.024 | 47.919 | | |
| 12/9/2008 | 10:02:16 | 20.319 | 0.03 | 318.718 | 0.024 | 46.481 | | |
| 12/9/2008 | 10:02:26 | 20.335 | 0.03 | 346.667 | 0.024 | 43.074 | | |
| 12/9/2008 | 10:02:36 | 20.517 | 0.03 | 347.179 | 0.024 | 44.74 | | |
| 12/9/2008 | 10:02:46 | 20.548 | 0.03 | 346.667 | 0.024 | 46.254 | | |
| 12/9/2008 | 10:02:56 | 20.487 | 0.03 | 390.513 | 0.024 | 41.863 | | |
| 12/9/2008 | 10:03:06 | 20.655 | 0.03 | 342.821 | 0.024 | 44.286 | | |
| 12/9/2008 | 10:03:16 | 20.517 | 0.03 | 376.41 | 0.024 | 44.361 | | |
| 12/9/2008 | 10:03:26 | 20.563 | 0.03 | 388.205 | 0.024 | 45.194 | | |
| 12/9/2008 | 10:03:36 | 20.472 | 0.03 | 343.846 | 29.084 | 49.055 | | |
| 12/9/2008 | 10:03:46 | 20.319 | 0.03 | 402.051 | 2.54 | 47.768 | | |
| 12/9/2008 | 10:03:56 | 20.396 | 0.03 | 374.815 | 0.024 | 48.828 | | |
| 12/9/2008 | 10:04:06 | 20.487 | 0.03 | 374.872 | 0.024 | 50.872 | | |
| 12/9/2008 | 10:04:16 | 20.487 | 0.03 | 411.795 | 0.024 | 48.828 | | |
| 12/9/2008 | 10:04:26 | 20.578 | 0.03 | 413.59 | 0.024 | 46.784 | | |
| 12/9/2008 | 10:04:36 | 20.655 | 0.03 | 333.59 | 0.024 | 50.72 | | |
| 12/9/2008 | 10:04:46 | 20.533 | 0.03 | 382.308 | 0.024 | 49.661 | | |
| 12/9/2008 | 10:04:56 | 20.548 | 0.03 | 365.385 | 0.024 | 50.798 | | |
| 12/9/2008 | 10:05:06 | 20.472 | 0.03 | 319.231 | 0.024 | 66.845 | | |
| 12/9/2008 | 10:05:16 | 20.319 | 0.03 | 363.848 | 22.882 | 75.248 | | |
| 12/9/2008 | 10:05:26 | 20.319 | 0.03 | 359.231 | 0.024 | 76.308 | | |
| 12/9/2008 | 10:05:36 | 20.35 | 0.03 | 320 | 0.024 | 76.156 | | |
| 12/9/2008 | 10:05:46 | 20.365 | 0.03 | 346.154 | 0.024 | 75.778 | | |
| 12/9/2008 | 10:05:56 | 20.411 | 0.03 | 396.923 | 0.024 | 65.255 | | |
| 12/9/2008 | 10:06:06 | 20.578 | 0.03 | 384.615 | 0.024 | 54.733 | | |
| 12/9/2008 | 10:06:16 | 20.624 | 0.03 | 331.795 | 0.024 | 52.234 | | |
| 12/9/2008 | 10:06:26 | 20.639 | 0.03 | 330.256 | 0.024 | 50.569 | | |
| 12/9/2008 | 10:06:36 | 20.548 | 0.03 | 337.179 | 0.024 | 46.708 | | |
| 12/9/2008 | 10:06:46 | 20.517 | 0.03 | 355.385 | 0.024 | 45.194 | | |
| 12/9/2008 | 10:06:56 | 20.411 | 0.061 | 390.256 | 20.811 | 43.302 | | |
| 12/9/2008 | 10:07:06 | 20.319 | 0.03 | 402.821 | 0.488 | 42.545 | | |
| 12/9/2008 | 10:07:16 | 20.35 | 0.03 | 387.949 | 0.024 | 42.847 | | |
| 12/9/2008 | 10:07:26 | 20.441 | 0.03 | 383.333 | 0.024 | 43.453 | | |
| 12/9/2008 | 10:07:36 | 20.517 | 0.03 | 390.513 | 0.024 | 44.286 | | |
| 12/9/2008 | 10:07:46 | 20.563 | 0.03 | 423.333 | 0.024 | 46.254 | | |
| 12/9/2008 | 10:07:56 | 20.594 | 0.03 | 408.462 | 0.024 | 47.238 | | |
| 12/9/2008 | 10:08:06 | 20.548 | 0.03 | 405.897 | 0.024 | 47.011 | | |
| 12/9/2008 | 10:08:16 | 20.396 | 0.03 | 394.359 | 0.024 | 50.115 | | |
| 12/9/2008 | 10:08:26 | 20.319 | 0.03 | 430.513 | 0.024 | 52.083 | | |
| 12/9/2008 | 10:08:36 | 20.228 | 0.03 | 419.487 | 23.419 | 50.115 | | |
| 12/9/2008 | 10:08:46 | 20.213 | 0.03 | 399.231 | 0.024 | 48.374 | | |
| 12/9/2008 | 10:08:56 | 20.259 | 0.03 | 338.205 | 0.024 | 50.72 | | |
| 12/9/2008 | 10:09:06 | 20.396 | 0.03 | 321.538 | 0.024 | 52.613 | | |
| 12/9/2008 | 10:09:16 | 20.502 | 0.03 | 345.641 | 0.024 | 53.143 | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | CO ₂ % | RTO Inlet | | | Calibration Comments | Error % |
|-----------|----------|----------------------|--|--|--|-------------------------|------------|
| | | | VOC 3 ppm C ₂ H ₆ | VOC 1 ppm C ₂ H ₆ | VOC 2 ppm C ₂ H ₆ | | |
| 12/9/2008 | 10:09:26 | 20.517 | 0.03 372.051 | 0.024 | 63.893 | | |
| 12/9/2008 | 10:09:36 | 20.517 | 0.03 385.841 | 0.024 | 78.005 | | |
| 12/9/2008 | 10:09:46 | 20.578 | 0.03 309.231 | 0.024 | 78.427 | | |
| 12/9/2008 | 10:09:56 | 20.563 | 0.03 304.103 | 0.024 | 76.308 | | |
| 12/9/2008 | 10:10:06 | 20.517 | 0.03 316.154 | 0.024 | 75.929 | | |
| 12/9/2008 | 10:10:16 | 20.411 | 0.03 341.282 | 22.051 | 70.554 | | |
| 12/9/2008 | 10:10:26 | 20.35 | 0.03 362.564 | 1.465 | 56.247 | | |
| 12/9/2008 | 10:10:36 | 20.35 | 0.03 362.051 | 0.024 | 52.007 | | |
| 12/9/2008 | 10:10:46 | 20.411 | 0.03 367.179 | 0.024 | 50.342 | | |
| 12/9/2008 | 10:10:56 | 20.487 | 0.03 342.051 | 0.024 | 48.071 | | |
| 12/9/2008 | 10:11:06 | 20.517 | 0.03 352.308 | 0.024 | 45.8 | | |
| 12/9/2008 | 10:11:16 | 20.563 | 0.03 383.333 | 0.024 | 44.513 | | |
| 12/9/2008 | 10:11:26 | 20.517 | 0.03 408.874 | 0.024 | 43.15 | | |
| 12/9/2008 | 10:11:36 | 20.457 | 0.03 358.462 | 0.024 | 44.134 | | |
| 12/9/2008 | 10:11:46 | 20.411 | 0.081 367.179 | 0.024 | 45.118 | | |
| 12/9/2008 | 10:11:56 | 20.319 | 0.03 352.051 | 21.636 | 45.875 | | |
| 12/9/2008 | 10:12:06 | 20.289 | 0.03 385.385 | 0.024 | 48.828 | | |
| 12/9/2008 | 10:12:16 | 20.289 | 0.03 364.359 | 0.024 | 49.055 | | |
| 12/9/2008 | 10:12:26 | 20.38 | 0.03 369.487 | 0.024 | 50.589 | | |
| 12/9/2008 | 10:12:36 | 20.502 | 0.03 350.789 | 0.024 | 53.37 | | |
| 12/9/2008 | 10:12:46 | 20.563 | 0.03 385.841 | 0.024 | 54.505 | | |
| 12/9/2008 | 10:12:56 | 20.594 | 0.03 381.282 | 0.024 | 52.891 | | |
| 12/9/2008 | 10:13:06 | 20.809 | 0.03 380.789 | 0.024 | 50.342 | | |
| 12/9/2008 | 10:13:16 | 20.563 | 0.03 338.718 | 0.024 | 51.023 | | |
| 12/9/2008 | 10:13:26 | 20.487 | 0.03 332.308 | 0.024 | 52.991 | | |
| 12/9/2008 | 10:13:36 | 20.411 | 0.03 350.513 | 21.88 | 55.035 | | |
| 12/9/2008 | 10:13:46 | 20.365 | 0.03 335.887 | 2.173 | 67.148 | | |
| 12/9/2008 | 10:13:56 | 20.365 | 0.03 335.887 | 0.024 | 78.957 | | |
| 12/9/2008 | 10:14:06 | 20.441 | 0.03 313.846 | 0.024 | 79.714 | | |
| 12/9/2008 | 10:14:16 | 20.533 | 0.03 318.974 | 0.024 | 77.746 | | |
| 12/9/2008 | 10:14:26 | 20.624 | 0.03 339.487 | 0.024 | 76.459 | | |
| 12/9/2008 | 10:14:36 | 20.609 | 0.03 358.205 | 0.024 | 71.614 | | |
| 12/9/2008 | 10:14:46 | 20.517 | 0.03 389.487 | 0.024 | 56.02 | | |
| 12/9/2008 | 10:14:56 | 20.38 | 0.03 379.487 | 0.024 | 51.856 | | |
| 12/9/2008 | 10:15:06 | 20.319 | 0.081 393.846 | 0.024 | 49.358 | | |
| 12/9/2008 | 10:15:16 | 20.259 | 0.061 384.815 | 20.588 | 47.768 | | |
| 12/9/2008 | 10:15:26 | 20.259 | 0.091 337.692 | 0.024 | 45.951 | | |
| 12/9/2008 | 10:15:36 | 20.274 | 0.03 352.308 | 0.024 | 46.405 | | |
| 12/9/2008 | 10:15:46 | 20.396 | 0.03 363.59 | 0.024 | 46.103 | | |
| 12/9/2008 | 10:15:56 | 20.502 | 0.03 360.256 | 0.024 | 45.194 | | |
| 12/9/2008 | 10:16:06 | 20.578 | 0.03 357.692 | 0.024 | 44.589 | | |
| 12/9/2008 | 10:16:16 | 20.639 | 0.03 358.867 | 0.024 | 45.118 | | |
| 12/9/2008 | 10:16:26 | 20.67 | 0.03 363.846 | 0.024 | 47.087 | | |
| 12/9/2008 | 10:16:36 | 20.594 | 0.03 378.462 | 0.024 | 48.374 | | |
| 12/9/2008 | 10:16:46 | 20.517 | 0.03 383.333 | 0.781 | 51.099 | | |
| 12/9/2008 | 10:16:56 | 20.411 | 0.03 380.256 | 23.37 | 56.701 | | |
| 12/9/2008 | 10:17:06 | 20.335 | 0.03 391.795 | 1.929 | 57.155 | | |
| 12/9/2008 | 10:17:16 | 20.365 | 0.03 402.821 | 0.024 | 54.505 | | |
| 12/9/2008 | 10:17:26 | 20.457 | 0.03 384.872 | 0.024 | 51.175 | | |
| 12/9/2008 | 10:17:36 | 20.517 | 0.03 374.103 | 0.024 | 51.856 | | |
| 12/9/2008 | 10:17:46 | 20.594 | 0.03 373.59 | 0.024 | 52.991 | | |
| 12/9/2008 | 10:17:56 | 20.609 | 0.061 381.282 | 0.024 | 53.824 | | |
| 12/9/2008 | 10:18:06 | 20.548 | 0.122 396.154 | 0.024 | 63.438 | | |
| 12/9/2008 | 10:18:16 | 20.426 | 0.183 370 | 0.024 | 78.049 | | |
| 12/9/2008 | 10:18:26 | 20.35 | 0.244 357.692 | 0.024 | 80.471 | | |
| 12/9/2008 | 10:18:36 | 20.289 | 0.213 352.821 | 18.706 | 78.427 | | |
| 12/9/2008 | 10:18:46 | 20.274 | 0.244 374.103 | 0.024 | 77.595 | | |
| 12/9/2008 | 10:18:56 | 20.274 | 0.152 389.744 | 0.024 | 76.811 | | |
| 12/9/2008 | 10:19:06 | 20.35 | 0.061 381.282 | 0.024 | 61.773 | | |
| 12/9/2008 | 10:19:16 | 20.487 | 0.03 368.974 | 0.024 | 57.155 | | |
| 12/9/2008 | 10:19:26 | 20.594 | 0.03 355.128 | 0.024 | 54.43 | | |
| 12/9/2008 | 10:19:36 | 20.639 | 0.03 333.846 | 0.024 | 53.143 | | |
| 12/9/2008 | 10:19:46 | 20.594 | 0.03 335.128 | 0.024 | 51.402 | | |
| 12/9/2008 | 10:19:56 | 20.441 | 0.122 376.154 | 0.024 | 49.206 | | |
| 12/9/2008 | 10:20:06 | 20.396 | 0.213 413.077 | 0.024 | 48.904 | | |
| 12/9/2008 | 10:20:16 | 20.35 | 0.213 374.103 | 23.832 | 50.039 | | |
| 12/9/2008 | 10:20:26 | 20.335 | 0.183 342.308 | 2.344 | 50.418 | | |
| 12/9/2008 | 10:20:36 | 20.319 | 0.122 347.692 | 0.024 | 50.418 | | |
| 12/9/2008 | 10:20:46 | 20.35 | 0.061 386.823 | 0.024 | 51.553 | | |
| 12/9/2008 | 10:20:56 | 20.457 | 0.03 401.282 | 0.024 | 53.219 | | |
| 12/9/2008 | 10:21:06 | 20.502 | 0.03 389.487 | 0.024 | 54.051 | | |
| 12/9/2008 | 10:21:16 | 20.517 | 0.091 421.282 | 0.024 | 54.808 | | |
| 12/9/2008 | 10:21:26 | 20.502 | 0.152 396.41 | 0.024 | 56.852 | | |
| 12/9/2008 | 10:21:36 | 20.426 | 0.183 407.692 | 0.024 | 57.079 | | |
| 12/9/2008 | 10:21:46 | 20.365 | 0.213 385.841 | 0.024 | 55.111 | | |

Start Run #1

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error: % |
|-----------|----------|--------|-------|-----------------------------------|-----------------------------------|-----------------------------------|-------------------------|-------------|
| | | % | % | ppm C ₂ H ₆ | ppm C ₂ H ₆ | ppm C ₂ H ₆ | | |
| 12/9/2008 | 10:21:56 | 20.274 | 0.213 | 372.051 | 23.98 | 58.322 | | |
| 12/9/2008 | 10:22:06 | 20.274 | 0.213 | 343.846 | 0.293 | 57.382 | | |
| 12/9/2008 | 10:22:16 | 20.289 | 0.122 | 356.41 | 0.024 | 58.139 | | |
| 12/9/2008 | 10:22:26 | 20.38 | 0.03 | 365.897 | 0.024 | 63.665 | | |
| 12/9/2008 | 10:22:36 | 20.487 | 0.03 | 358.744 | 0.024 | 79.033 | | |
| 12/9/2008 | 10:22:46 | 20.578 | 0.03 | 356.154 | 0.024 | 81.001 | | |
| 12/9/2008 | 10:22:56 | 20.563 | 0.03 | 372.564 | 0.024 | 78.033 | | |
| 12/9/2008 | 10:23:06 | 20.533 | 0.061 | 379.231 | 0.024 | 77.595 | | |
| 12/9/2008 | 10:23:16 | 20.472 | 0.122 | 375.641 | 0.024 | 77.822 | | |
| 12/9/2008 | 10:23:26 | 20.426 | 0.183 | 385.128 | 0.024 | 65.179 | | |
| 12/9/2008 | 10:23:36 | 20.35 | 0.183 | 374.359 | 27.619 | 56.171 | | |
| 12/9/2008 | 10:23:46 | 20.319 | 0.183 | 364.815 | 3.101 | 53.37 | | |
| 12/9/2008 | 10:23:56 | 20.35 | 0.091 | 357.949 | 0.024 | 50.039 | | |
| 12/9/2008 | 10:24:06 | 20.428 | 0.03 | 332.308 | 0.024 | 49.131 | | |
| 12/9/2008 | 10:24:16 | 20.517 | 0.061 | 384.103 | 0.024 | 49.206 | | |
| 12/9/2008 | 10:24:26 | 20.578 | 0.03 | 393.846 | 0.024 | 49.812 | | |
| 12/9/2008 | 10:24:36 | 20.578 | 0.03 | 395.897 | 0.024 | 49.812 | | |
| 12/9/2008 | 10:24:46 | 20.487 | 0.03 | 397.692 | 0.024 | 49.055 | | |
| 12/9/2008 | 10:24:56 | 20.35 | 0.03 | 412.051 | 0.024 | 48.374 | | |
| 12/9/2008 | 10:25:06 | 20.289 | 0.091 | 412.308 | 0.024 | 49.433 | | |
| 12/9/2008 | 10:25:16 | 20.213 | 0.091 | 419.231 | 24.762 | 51.705 | | |
| 12/9/2008 | 10:25:26 | 20.198 | 0.091 | 422.564 | 0.024 | 52.537 | | |
| 12/9/2008 | 10:25:36 | 20.213 | 0.03 | 434.872 | 0.024 | 53.521 | | |
| 12/9/2008 | 10:25:46 | 20.304 | 0.03 | 411.795 | 0.024 | 54.203 | | |
| 12/9/2008 | 10:25:56 | 20.38 | 0.03 | 459.744 | 0.024 | 53.824 | | |
| 12/9/2008 | 10:26:06 | 20.472 | 0.03 | 446.41 | 0.024 | 53.143 | | |
| 12/9/2008 | 10:26:16 | 20.533 | 0.03 | 437.436 | 0.024 | 53.748 | | |
| 12/9/2008 | 10:26:26 | 20.548 | 0.03 | 396.923 | 0.024 | 55.338 | | |
| 12/9/2008 | 10:26:36 | 20.502 | 0.03 | 378.718 | 0.024 | 57.382 | | |
| 12/9/2008 | 10:26:46 | 20.441 | 0.03 | 378.867 | 0.024 | 60.259 | | |
| 12/9/2008 | 10:26:56 | 20.35 | 0.061 | 358.974 | 26.642 | 76.989 | | |
| 12/9/2008 | 10:27:06 | 20.274 | 0.03 | 381.795 | 2.882 | 84.786 | | |
| 12/9/2008 | 10:27:16 | 20.304 | 0.03 | 345.128 | 0.024 | 84.105 | | |
| 12/9/2008 | 10:27:26 | 20.426 | 0.03 | 358.462 | 0.024 | 80.926 | | |
| 12/9/2008 | 10:27:36 | 20.517 | 0.03 | 360.256 | 0.024 | 81.91 | | |
| 12/9/2008 | 10:27:46 | 20.609 | 0.03 | 383.333 | 0.024 | 72.75 | | |
| 12/9/2008 | 10:27:56 | 20.624 | 0.03 | 378.974 | 0.024 | 61.548 | | |
| 12/9/2008 | 10:28:06 | 20.548 | 0.03 | 373.846 | 0.024 | 57.004 | | |
| 12/9/2008 | 10:28:16 | 20.411 | 0.03 | 377.179 | 0.024 | 53.143 | | |
| 12/9/2008 | 10:28:26 | 20.319 | 0.03 | 346.923 | 0.024 | 52.007 | | |
| 12/9/2008 | 10:28:36 | 20.243 | 0.03 | 353.333 | 23.101 | 51.099 | | |
| 12/9/2008 | 10:28:46 | 20.198 | 0.03 | 383.58 | 0.024 | 51.25 | | |
| 12/9/2008 | 10:28:56 | 20.198 | 0.03 | 400.513 | 0.024 | 50.569 | | |
| 12/9/2008 | 10:29:06 | 20.304 | 0.03 | 408.974 | 0.024 | 51.326 | | |
| 12/9/2008 | 10:29:16 | 20.396 | 0.03 | 422.308 | 0.024 | 50.19 | | |
| 12/9/2008 | 10:29:26 | 20.487 | 0.03 | 431.026 | 0 | 50.115 | | |
| 12/9/2008 | 10:29:36 | 20.548 | 0.03 | 425.128 | 0.024 | 50.947 | | |
| 12/9/2008 | 10:29:46 | 20.594 | 0.03 | 432.564 | 0.024 | 52.689 | | |
| 12/9/2008 | 10:29:56 | 20.548 | 0.03 | 428.41 | 0.024 | 56.852 | | |
| 12/9/2008 | 10:30:06 | 20.457 | 0.03 | 406.154 | 0.024 | 60.335 | | |
| 12/9/2008 | 10:30:16 | 20.35 | 0.061 | 428.41 | 31.722 | 60.637 | | |
| 12/9/2008 | 10:30:26 | 20.289 | 0.03 | 403.333 | 4.2 | 58.063 | | |
| 12/9/2008 | 10:30:36 | 20.304 | 0.03 | 392.564 | 0.024 | 56.322 | | |
| 12/9/2008 | 10:30:46 | 20.396 | 0.03 | 382.821 | 0.024 | 57.306 | | |
| 12/9/2008 | 10:30:56 | 20.517 | 0.03 | 378.154 | 0.024 | 57.988 | | |
| 12/9/2008 | 10:31:06 | 20.594 | 0.03 | 380.513 | 0.024 | 62.606 | | |
| 12/9/2008 | 10:31:16 | 20.609 | 0.03 | 377.949 | 0.024 | 79.714 | | |
| 12/9/2008 | 10:31:26 | 20.583 | 0.03 | 351.538 | 0.024 | 85.619 | | |
| 12/9/2008 | 10:31:36 | 20.441 | 0.03 | 342.051 | 0.024 | 86.755 | | |
| 12/9/2008 | 10:31:46 | 20.335 | 0.061 | 384.359 | 0.024 | 82.894 | | |
| 12/9/2008 | 10:31:56 | 20.289 | 0.081 | 379.487 | 25.128 | 82.212 | | |
| 12/9/2008 | 10:32:06 | 20.259 | 0.081 | 387.179 | 0.049 | 68.965 | | |
| 12/9/2008 | 10:32:16 | 20.274 | 0.03 | 398.718 | 0.024 | 58.745 | | |
| 12/9/2008 | 10:32:26 | 20.385 | 0.03 | 408.154 | 0.024 | 55.641 | | |
| 12/9/2008 | 10:32:36 | 20.487 | 0.03 | 390.513 | 0.024 | 54.657 | | |
| 12/9/2008 | 10:32:46 | 20.563 | 0.03 | 354.103 | 0.024 | 53.9 | | |
| 12/9/2008 | 10:32:56 | 20.624 | 0.03 | 363.077 | 0.024 | 53.748 | | |
| 12/9/2008 | 10:33:06 | 20.624 | 0.03 | 399.231 | 0.024 | 54.733 | | |
| 12/9/2008 | 10:33:16 | 20.533 | 0.03 | 380.789 | 0.024 | 55.111 | | |
| 12/9/2008 | 10:33:26 | 20.441 | 0.03 | 376.667 | 0.024 | 54.884 | | |
| 12/9/2008 | 10:33:36 | 20.335 | 0.03 | 404.359 | 27.228 | 54.278 | | |
| 12/9/2008 | 10:33:46 | 20.259 | 0.03 | 392.308 | 3.585 | 55.338 | | |
| 12/9/2008 | 10:33:56 | 20.274 | 0.03 | 408.41 | 0.024 | 57.458 | | |
| 12/9/2008 | 10:34:06 | 20.335 | 0.03 | 432.051 | 0.024 | 57.836 | | |
| 12/9/2008 | 10:34:16 | 20.441 | 0.03 | 432.308 | 0.024 | 60.259 | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|----------|--------|-------|-----------------------------------|-----------------------------------|-----------------------------------|-------------------------|------------|
| | | % | % | ppm C ₂ H ₆ | ppm C ₂ H ₆ | ppm C ₂ H ₆ | | |
| 12/9/2008 | 10:34:26 | 20.517 | 0.03 | 427.692 | 0.024 | 61.016 | | |
| 12/9/2008 | 10:34:36 | 20.533 | 0.03 | 447.436 | 0.024 | 60.335 | | |
| 12/9/2008 | 10:34:46 | 20.472 | 0.03 | 430.513 | 0.024 | 59.198 | | |
| 12/9/2008 | 10:34:56 | 20.385 | 0.061 | 422.564 | 0.024 | 58.972 | | |
| 12/9/2008 | 10:35:06 | 20.289 | 0.091 | 398.974 | 0.024 | 59.578 | | |
| 12/9/2008 | 10:35:16 | 20.228 | 0.091 | 389.231 | 24.713 | 62 | | |
| 12/9/2008 | 10:35:26 | 20.243 | 0.061 | 387.692 | 0.708 | 64.347 | | |
| 12/9/2008 | 10:35:36 | 20.274 | 0.03 | 380.513 | 0.024 | 80.244 | | |
| 12/9/2008 | 10:35:46 | 20.35 | 0.03 | 375.385 | 0.024 | 85.241 | | |
| 12/9/2008 | 10:35:56 | 20.472 | 0.03 | 388.462 | 0.024 | 83.651 | | |
| 12/9/2008 | 10:36:06 | 20.487 | 0.03 | 417.692 | 0.024 | 81.38 | | |
| 12/9/2008 | 10:36:16 | 20.533 | 0.03 | 417.949 | 0.024 | 82.137 | | |
| 12/9/2008 | 10:36:26 | 20.533 | 0.03 | 438.205 | 0.024 | 71.463 | | |
| 12/9/2008 | 10:36:36 | 20.441 | 0.03 | 429.744 | 0.024 | 80.884 | | |
| 12/9/2008 | 10:36:46 | 20.365 | 0.091 | 408.205 | 0.024 | 57.306 | | |
| 12/9/2008 | 10:36:56 | 20.274 | 0.091 | 412.564 | 28.059 | 54.808 | | |
| 12/9/2008 | 10:37:06 | 20.213 | 0.091 | 383.846 | 3.126 | 53.597 | | |
| 12/9/2008 | 10:37:16 | 20.228 | 0.03 | 382.564 | 0.024 | 52.84 | | |
| 12/9/2008 | 10:37:26 | 20.335 | 0.03 | 394.872 | 0.024 | 54.203 | | |
| 12/9/2008 | 10:37:36 | 20.457 | 0.03 | 388.974 | 0.024 | 56.474 | | |
| 12/9/2008 | 10:37:46 | 20.548 | 0.03 | 407.892 | 0.024 | 58.474 | | |
| 12/9/2008 | 10:37:56 | 20.548 | 0.03 | 412.051 | 0.024 | 54.96 | | |
| 12/9/2008 | 10:38:06 | 20.457 | 0.03 | 437.179 | 0.024 | 54.96 | | |
| 12/9/2008 | 10:38:16 | 20.319 | 0.091 | 463.846 | 0.024 | 58.322 | | |
| 12/9/2008 | 10:38:26 | 20.304 | 0.091 | 437.692 | 0.024 | 60.032 | | |
| 12/9/2008 | 10:38:36 | 20.259 | 0.061 | 410 | 29.133 | 63.885 | | |
| 12/9/2008 | 10:38:46 | 20.213 | 0.091 | 397.692 | 1.343 | 86.164 | | |
| 12/9/2008 | 10:38:56 | 20.182 | 0.03 | 468.462 | 0.024 | 63.893 | | |
| 12/9/2008 | 10:39:06 | 20.304 | 0.03 | 445.641 | 0.024 | 60.259 | | |
| 12/9/2008 | 10:39:16 | 20.472 | 0.03 | 404.359 | 0.024 | 81.243 | | |
| 12/9/2008 | 10:39:26 | 20.502 | 0.03 | 385.128 | 0.024 | 81.548 | | |
| 12/9/2008 | 10:39:36 | 20.533 | 0.03 | 419.487 | 0.024 | 59.653 | | |
| 12/9/2008 | 10:39:46 | 20.639 | 0.03 | 409.487 | 0.024 | 64.877 | | |
| 12/9/2008 | 10:39:56 | 20.548 | 0.03 | 371.538 | 0.024 | 82.969 | | |
| 12/9/2008 | 10:40:06 | 20.38 | 0.091 | 417.179 | 0.024 | 87.436 | | |
| 12/9/2008 | 10:40:16 | 20.319 | 0.061 | 405.128 | 28.449 | 87.436 | | |
| 12/9/2008 | 10:40:26 | 20.319 | 0.03 | 389.487 | 4.127 | 86.073 | | |
| 12/9/2008 | 10:40:36 | 20.304 | 0.03 | 380.513 | 0.024 | 87.436 | | |
| 12/9/2008 | 10:40:46 | 20.335 | 0.03 | 421.795 | 0.024 | 73.607 | | |
| 12/9/2008 | 10:40:56 | 20.411 | 0.03 | 452.564 | 0.024 | 62.227 | | |
| 12/9/2008 | 10:41:06 | 20.502 | 0.03 | 451.538 | 0.024 | 57.988 | | |
| 12/9/2008 | 10:41:16 | 20.533 | 0.03 | 447.436 | 0.024 | 55.263 | | |
| 12/9/2008 | 10:41:26 | 20.472 | 0.061 | 417.692 | 0.024 | 54.203 | | |
| 12/9/2008 | 10:41:36 | 20.35 | 0.091 | 415.897 | 0.024 | 53.446 | | |
| 12/9/2008 | 10:41:46 | 20.259 | 0.122 | 437.179 | 0.024 | 53.978 | | |
| 12/9/2008 | 10:41:56 | 20.167 | 0.122 | 453.333 | 30.354 | 55.414 | | |
| 12/9/2008 | 10:42:06 | 20.182 | 0.091 | 433.333 | 1.368 | 56.701 | | |
| 12/9/2008 | 10:42:16 | 20.228 | 0.03 | 418.974 | 0.024 | 57.231 | | |
| 12/9/2008 | 10:42:26 | 20.38 | 0.03 | 427.949 | 0.024 | 57.079 | | |
| 12/9/2008 | 10:42:36 | 20.441 | 0.03 | 475.897 | 0.024 | 56.322 | | |
| 12/9/2008 | 10:42:46 | 20.472 | 0.03 | 474.359 | 0.024 | 57.685 | | |
| 12/9/2008 | 10:42:56 | 20.563 | 0.03 | 451.538 | 0.024 | 62.681 | | |
| 12/9/2008 | 10:43:06 | 20.624 | 0.03 | 417.436 | 0.024 | 65.104 | | |
| 12/9/2008 | 10:43:16 | 20.548 | 0.03 | 477.949 | 0.024 | 63.893 | | |
| 12/9/2008 | 10:43:26 | 20.38 | 0.122 | 486.718 | 0.024 | 59.805 | | |
| 12/9/2008 | 10:43:36 | 20.259 | 0.061 | 456.923 | 35.751 | 61.167 | | |
| 12/9/2008 | 10:43:46 | 20.243 | 0.061 | 388.667 | 6.422 | 63.136 | | |
| 12/9/2008 | 10:43:56 | 20.289 | 0.061 | 405.641 | 0.781 | 62.833 | | |
| 12/9/2008 | 10:44:06 | 20.35 | 0.091 | 453.333 | 0.024 | 64.801 | | |
| 12/9/2008 | 10:44:16 | 20.411 | 0.061 | 419.487 | 0.024 | 63.424 | | |
| 12/9/2008 | 10:44:26 | 20.578 | 0.03 | 385.385 | 0.024 | 90.313 | | |
| 12/9/2008 | 10:44:36 | 20.609 | 0.091 | 389.487 | 0.024 | 90.313 | | |
| 12/9/2008 | 10:44:46 | 20.487 | 0.213 | 430.769 | 0.024 | 85.846 | | |
| 12/9/2008 | 10:44:56 | 20.35 | 0.244 | 421.282 | 0.024 | 86.982 | | |
| 12/9/2008 | 10:45:06 | 20.319 | 0.213 | 409.231 | 0.024 | 74.567 | | |
| 12/9/2008 | 10:45:16 | 20.259 | 0.213 | 418.205 | 33.675 | 64.952 | | |
| 12/9/2008 | 10:45:26 | 20.228 | 0.244 | 425.841 | 2.32 | 60.032 | | |
| 12/9/2008 | 10:45:36 | 20.198 | 0.213 | 442.051 | 0.024 | 56.171 | | |
| 12/9/2008 | 10:45:46 | 20.289 | 0.122 | 417.179 | 0.024 | 55.187 | | |
| 12/9/2008 | 10:45:56 | 20.38 | 0.061 | 392.821 | 0.024 | 54.808 | | |
| 12/9/2008 | 10:46:06 | 20.517 | 0.03 | 392.308 | 0.024 | 57.231 | | |
| 12/9/2008 | 10:46:16 | 20.609 | 0.03 | 397.949 | 0.024 | 58.366 | | |
| 12/9/2008 | 10:46:26 | 20.609 | 0.061 | 413.077 | 0.024 | 57.534 | | |
| 12/9/2008 | 10:46:36 | 20.517 | 0.183 | 438.974 | 0.024 | 57.231 | | |
| 12/9/2008 | 10:46:46 | 20.335 | 0.244 | 472.584 | 0.024 | 58.291 | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|----------|--------|-------|-----------------------------------|-----------------------------------|-----------------------------------|-------------------------|------------|
| | | % | % | ppm C ₂ H ₆ | ppm C ₂ H ₆ | ppm C ₂ H ₆ | | |
| 12/9/2008 | 10:46:56 | 20.259 | 0.244 | 482.821 | 36.068 | 60.486 | | |
| 12/9/2008 | 10:47:06 | 20.213 | 0.244 | 459.497 | 6.203 | 62.833 | | |
| 12/9/2008 | 10:47:16 | 20.213 | 0.183 | 468.923 | 0.806 | 65.104 | | |
| 12/9/2008 | 10:47:26 | 20.304 | 0.091 | 434.615 | 0.024 | 67.148 | | |
| 12/9/2008 | 10:47:36 | 20.441 | 0.061 | 448.205 | 0.024 | 67.223 | | |
| 12/9/2008 | 10:47:46 | 20.517 | 0.03 | 435.641 | 0.024 | 65.482 | | |
| 12/9/2008 | 10:47:56 | 20.578 | 0.061 | 432.821 | 0.024 | 64.044 | | |
| 12/9/2008 | 10:48:06 | 20.517 | 0.152 | 408.974 | 0.024 | 64.65 | | |
| 12/9/2008 | 10:48:16 | 20.396 | 0.213 | 420.769 | 0.024 | 66.088 | | |
| 12/9/2008 | 10:48:26 | 20.289 | 0.244 | 438.718 | 0.024 | 69.118 | | |
| 12/9/2008 | 10:48:36 | 20.228 | 0.274 | 440 | 33.529 | 65.77 | | |
| 12/9/2008 | 10:48:46 | 20.152 | 0.274 | 433.846 | 2.32 | 91.07 | | |
| 12/9/2008 | 10:48:56 | 20.152 | 0.213 | 419.744 | 0.024 | 91.372 | | |
| 12/9/2008 | 10:49:06 | 20.259 | 0.122 | 438.205 | 0.024 | 68.404 | | |
| 12/9/2008 | 10:49:16 | 20.411 | 0.03 | 430.769 | 0.024 | 90.54 | | |
| 12/9/2008 | 10:49:26 | 20.517 | 0.03 | 424.359 | 0.024 | 78.125 | | |
| 12/9/2008 | 10:49:36 | 20.809 | 0.03 | 430 | 0.024 | 66.694 | | |
| 12/9/2008 | 10:49:46 | 20.639 | 0.03 | 433.333 | 0.024 | 61.319 | | |
| 12/9/2008 | 10:49:56 | 20.533 | 0.03 | 441.538 | 0.024 | 57.988 | | |
| 12/9/2008 | 10:50:06 | 20.411 | 0.061 | 411.282 | 0.024 | 57.382 | | |
| 12/9/2008 | 10:50:16 | 20.335 | 0.061 | 427.692 | 28.523 | 57.079 | | |
| 12/9/2008 | 10:50:26 | 20.304 | 0.061 | 475.128 | 4.518 | 58.896 | | |
| 12/9/2008 | 10:50:36 | 20.304 | 0.03 | 452.051 | 0.024 | 59.653 | | |
| 12/9/2008 | 10:50:46 | 20.396 | 0.03 | 450.256 | 0.024 | 60.713 | | |
| 12/9/2008 | 10:50:56 | 20.487 | 0.03 | 452.051 | 0.024 | 60.864 | | |
| 12/9/2008 | 10:51:06 | 20.578 | 0.03 | 448.205 | 0.024 | 62.53 | | |
| 12/9/2008 | 10:51:16 | 20.578 | 0.03 | 434.872 | 0.024 | 64.044 | | |
| 12/9/2008 | 10:51:26 | 20.472 | 0.03 | 436.887 | 0.024 | 64.852 | | |
| 12/9/2008 | 10:51:36 | 20.335 | 0.091 | 440.513 | 0.024 | 65.785 | | |
| 12/9/2008 | 10:51:46 | 20.198 | 0.122 | 483.077 | 0.024 | 69.495 | | |
| 12/9/2008 | 10:51:56 | 20.198 | 0.122 | 506.154 | 38.284 | 67.829 | | |
| 12/9/2008 | 10:52:06 | 20.243 | 0.091 | 477.692 | 3.468 | 65.785 | | |
| 12/9/2008 | 10:52:16 | 20.228 | 0.03 | 430.231 | 0.488 | 64.952 | | |
| 12/9/2008 | 10:52:26 | 20.259 | 0.03 | 424.359 | 0.024 | 64.347 | | |
| 12/9/2008 | 10:52:36 | 20.335 | 0.03 | 471.538 | 0.024 | 64.422 | | |
| 12/9/2008 | 10:52:46 | 20.457 | 0.03 | 482.821 | 0.024 | 68.359 | | |
| 12/9/2008 | 10:52:56 | 20.563 | 0.03 | 445.897 | 0.024 | 86.603 | | |
| 12/9/2008 | 10:53:06 | 20.609 | 0.03 | 427.179 | 0.024 | 91.875 | | |
| 12/9/2008 | 10:53:16 | 20.578 | 0.03 | 418.205 | 0.024 | 91.07 | | |
| 12/9/2008 | 10:53:26 | 20.457 | 0.061 | 447.949 | 0.024 | 88.647 | | |
| 12/9/2008 | 10:53:36 | 20.335 | 0.091 | 457.436 | 38.117 | 88.117 | | |
| 12/9/2008 | 10:53:46 | 20.259 | 0.091 | 484.615 | 5.885 | 73.431 | | |
| 12/9/2008 | 10:53:56 | 20.243 | 0.03 | 502.308 | 0.659 | 85.558 | | |
| 12/9/2008 | 10:54:06 | 20.335 | 0.03 | 507.692 | 0.024 | 81.773 | | |
| 12/9/2008 | 10:54:16 | 20.426 | 0.03 | 485.385 | 0.024 | 60.183 | | |
| 12/9/2008 | 10:54:26 | 20.487 | 0.03 | 468.154 | 0.024 | 57.912 | | |
| 12/9/2008 | 10:54:36 | 20.517 | 0.03 | 482.308 | 0.024 | 58.063 | | |
| 12/9/2008 | 10:54:46 | 20.457 | 0.03 | 472.821 | 0.024 | 59.578 | | |
| 12/9/2008 | 10:54:56 | 20.365 | 0.091 | 478.718 | 0.024 | 60.259 | | |
| 12/9/2008 | 10:55:06 | 20.274 | 0.091 | 476.41 | 0.024 | 60.562 | | |
| 12/9/2008 | 10:55:16 | 20.213 | 0.091 | 491.282 | 37.118 | 59.956 | | |
| 12/9/2008 | 10:55:26 | 20.198 | 0.091 | 468.41 | 3.59 | 60.107 | | |
| 12/9/2008 | 10:55:36 | 20.182 | 0.061 | 464.103 | 0.073 | 62.454 | | |
| 12/9/2008 | 10:55:46 | 20.228 | 0.03 | 473.333 | 0.024 | 64.85 | | |
| 12/9/2008 | 10:55:56 | 20.35 | 0.03 | 465.128 | 0.024 | 68.845 | | |
| 12/9/2008 | 10:56:06 | 20.457 | 0.03 | 455.641 | 0.024 | 69.343 | | |
| 12/9/2008 | 10:56:16 | 20.548 | 0.03 | 468.974 | 0.024 | 69.419 | | |
| 12/9/2008 | 10:56:26 | 20.594 | 0.03 | 452.308 | 0.024 | 67.375 | | |
| 12/9/2008 | 10:56:36 | 20.548 | 0.03 | 454.103 | 0.024 | 66.315 | | |
| 12/9/2008 | 10:56:46 | 20.441 | 0.03 | 416.41 | 0.024 | 68.845 | | |
| 12/9/2008 | 10:56:56 | 20.335 | 0.061 | 447.949 | 35.531 | 67.526 | | |
| 12/9/2008 | 10:57:06 | 20.228 | 0.091 | 475.385 | 5.763 | 71.236 | | |
| 12/9/2008 | 10:57:16 | 20.198 | 0.03 | 491.538 | 0.586 | 87.436 | | |
| 12/9/2008 | 10:57:26 | 20.289 | 0.03 | 463.846 | 0.024 | 93.843 | | |
| 12/9/2008 | 10:57:36 | 20.396 | 0.03 | 425.385 | 0.024 | 93.871 | | |
| 12/9/2008 | 10:57:46 | 20.533 | 0.03 | 434.615 | 0.024 | 91.978 | | |
| 12/9/2008 | 10:57:56 | 20.594 | 0.03 | 421.538 | 0.024 | 93.114 | | |
| 12/9/2008 | 10:58:06 | 20.548 | 0.03 | 473.846 | 0.024 | 79.26 | | |
| 12/9/2008 | 10:58:16 | 20.35 | 0.091 | 504.615 | 0.024 | 67.451 | | |
| 12/9/2008 | 10:58:26 | 20.259 | 0.122 | 480.266 | 0.024 | 63.817 | | |
| 12/9/2008 | 10:58:36 | 20.228 | 0.061 | 437.949 | 38.584 | 62.151 | | |
| 12/9/2008 | 10:58:46 | 20.243 | 0.091 | 411.026 | 3.614 | 59.956 | | |
| 12/9/2008 | 10:58:56 | 20.182 | 0.061 | 458.205 | 0.024 | 58.215 | | |
| 12/9/2008 | 10:59:06 | 20.274 | 0.03 | 464.103 | 0.024 | 62.454 | | |
| 12/9/2008 | 10:59:16 | 20.457 | 0.03 | 437.949 | 0.024 | 63.498 | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Data | Time | O2 % | CO2 % | RTO Inlet | | | Calibration Comments | Error % |
|-----------|----------|---------|----------|--|--|--|-------------------------|------------|
| | | | | VOC 3 ppm C ₂ H ₆ | VOC 1 ppm C ₂ H ₆ | VOC 2 ppm C ₂ H ₆ | | |
| 12/9/2008 | 10:59:26 | 20.517 | 0.03 | 476.923 | 0.024 | 61.016 | | |
| 12/9/2008 | 10:59:36 | 20.517 | 0.03 | 492.308 | 0.024 | 60.032 | | |
| 12/9/2008 | 10:59:46 | 20.563 | 0.03 | 473.077 | 0.024 | 62.908 | | |
| 12/9/2008 | 10:59:56 | 20.548 | 0.03 | 458.205 | 0.024 | 65.709 | | |
| 12/9/2008 | 11:00:06 | 20.441 | 0.03 | 489.744 | 0.024 | 65.179 | | |
| 12/9/2008 | 11:00:16 | 20.274 | 0.091 | 503.333 | 39.927 | 64.725 | | |
| 12/9/2008 | 11:00:26 | 20.213 | 0.122 | 500 | 6.227 | 69.495 | | |
| 12/9/2008 | 11:00:36 | 20.213 | 0.03 | 488.974 | 1.294 | 72.75 | | |
| 12/9/2008 | 11:00:46 | 20.35 | 0.03 | 448.718 | 0.024 | 69.04 | | |
| 12/9/2008 | 11:00:56 | 20.472 | 0.03 | 474.103 | 0.024 | 67.526 | | |
| 12/9/2008 | 11:01:06 | 20.563 | 0.03 | 480 | 0.024 | 68.586 | | |
| 12/9/2008 | 11:01:16 | 20.594 | 0.03 | 484.103 | 0.024 | 68.889 | | |
| 12/9/2008 | 11:01:26 | 20.502 | 0.03 | 465.128 | 0.024 | 71.084 | | |
| 12/9/2008 | 11:01:36 | 20.38 | 0.091 | 461.282 | 0.024 | 88.906 | | |
| 12/9/2008 | 11:01:46 | 20.304 | 0.091 | 486.923 | 0.024 | 91.751 | | |
| 12/9/2008 | 11:01:56 | 20.259 | 0.091 | 441.028 | 40.098 | 91.372 | | |
| 12/9/2008 | 11:02:06 | 20.228 | 0.061 | 494.103 | 3.956 | 89.404 | | |
| 12/9/2008 | 11:02:16 | 20.228 | 0.03 | 471.026 | 0.342 | 84.559 | | |
| 12/9/2008 | 11:02:26 | 20.304 | 0.03 | 431.538 | 0.024 | 83.575 | | |
| 12/9/2008 | 11:02:36 | 20.396 | 0.03 | 407.692 | 0.024 | 82.061 | | |
| 12/9/2008 | 11:02:46 | 20.472 | 0.03 | 403.59 | 0.024 | 79.639 | | |
| 12/9/2008 | 11:02:56 | 20.533 | 0.03 | 412.564 | 0.024 | 78.654 | | |
| 12/9/2008 | 11:03:06 | 20.548 | 0.03 | 419.231 | 0.024 | 80.32 | | |
| 12/9/2008 | 11:03:16 | 20.487 | 0.03 | 417.692 | 0.024 | 81.834 | | |
| 12/9/2008 | 11:03:26 | 20.35 | 0.061 | 425.897 | 0.024 | 81.531 | | |
| 12/9/2008 | 11:03:36 | 20.274 | 0.091 | 443.333 | 31.966 | 83.424 | | |
| 12/9/2008 | 11:03:46 | 20.259 | 0.091 | 425.128 | 4.835 | 85.241 | | |
| 12/9/2008 | 11:03:56 | 20.289 | 0.03 | 403.59 | 0.586 | 72.447 | | |
| 12/9/2008 | 11:04:06 | 20.38 | 0.03 | 408.462 | 0.024 | 66.012 | | |
| 12/9/2008 | 11:04:16 | 20.426 | 0.03 | 425.897 | 0.024 | 62 | | |
| 12/9/2008 | 11:04:26 | 20.487 | 0.03 | 459.231 | 0.024 | 56.549 | | |
| 12/9/2008 | 11:04:36 | 20.548 | 0.03 | 419.744 | 0.024 | 56.396 | | |
| 12/9/2008 | 11:04:46 | 20.533 | 0.03 | 394.872 | 0.024 | 56.701 | | |
| 12/9/2008 | 11:04:56 | 20.411 | 0.03 | 406.923 | 0.024 | 58.215 | | |
| 12/9/2008 | 11:05:06 | 20.335 | 0.061 | 394.103 | 0.024 | 60.259 | | |
| 12/9/2008 | 11:05:16 | 20.274 | 0.03 | 400.258 | 36.972 | 59.502 | | |
| 12/9/2008 | 11:05:26 | 20.213 | 0.061 | 418.718 | 3.189 | 58.139 | | |
| 12/9/2008 | 11:05:36 | 20.167 | 0.091 | 448.462 | 0.024 | 57.155 | | |
| 12/9/2008 | 11:05:46 | 20.198 | 0.03 | 482.821 | 0.024 | 57.231 | | |
| 12/9/2008 | 11:05:56 | 20.335 | 0.03 | 507.949 | 0.024 | 59.199 | | |
| 12/9/2008 | 11:06:06 | 20.457 | 0.061 | 478.205 | 0.024 | 61.167 | | |
| 12/9/2008 | 11:06:16 | 20.548 | 0.061 | 474.872 | 0.024 | 63.363 | | |
| 12/9/2008 | 11:06:26 | 20.563 | 0.122 | 516.887 | 0.024 | 62.984 | | |
| 12/9/2008 | 11:06:36 | 20.472 | 0.213 | 500 | 0.024 | 61.394 | | |
| 12/9/2008 | 11:06:46 | 20.319 | 0.274 | 511.538 | 0.024 | 60.713 | | |
| 12/9/2008 | 11:06:56 | 20.213 | 0.274 | 453.59 | 39.78 | 63.06 | | |
| 12/9/2008 | 11:07:06 | 20.196 | 0.244 | 419.231 | 6.74 | 66.012 | | |
| 12/9/2008 | 11:07:16 | 20.243 | 0.152 | 409.231 | 1.465 | 69.57 | | |
| 12/9/2008 | 11:07:26 | 20.365 | 0.03 | 425.841 | 0.024 | 85.77 | | |
| 12/9/2008 | 11:07:36 | 20.472 | 0.03 | 401.282 | 0.024 | 93.114 | | |
| 12/9/2008 | 11:07:46 | 20.548 | 0.03 | 397.692 | 0.024 | 92.886 | | |
| 12/9/2008 | 11:07:56 | 20.594 | 0.061 | 410.513 | 0.024 | 90.388 | | |
| 12/9/2008 | 11:08:06 | 20.533 | 0.152 | 415.385 | 0.024 | 90.787 | | |
| 12/9/2008 | 11:08:16 | 20.411 | 0.183 | 432.308 | 0.024 | 82.137 | | |
| 12/9/2008 | 11:08:26 | 20.304 | 0.213 | 433.848 | 0.024 | 69.287 | | |
| 12/9/2008 | 11:08:36 | 20.228 | 0.244 | 428.41 | 39.878 | 63.741 | | |
| 12/9/2008 | 11:08:46 | 20.182 | 0.244 | 409.231 | 3.59 | 60.032 | | |
| 12/9/2008 | 11:08:56 | 20.167 | 0.183 | 401.538 | 0.024 | 58.139 | | |
| 12/9/2008 | 11:09:06 | 20.243 | 0.122 | 410.513 | 0.024 | 58.745 | | |
| 12/9/2008 | 11:09:16 | 20.385 | 0.091 | 481.795 | 0.024 | 60.259 | | |
| 12/9/2008 | 11:09:26 | 20.441 | 0.061 | 492.564 | 0.024 | 59.805 | | |
| 12/9/2008 | 11:09:36 | 20.517 | 0.061 | 488.462 | 0.024 | 59.88 | | |
| 12/9/2008 | 11:09:46 | 20.578 | 0.091 | 450.513 | 0.024 | 59.805 | | |
| 12/9/2008 | 11:09:56 | 20.533 | 0.152 | 438.462 | 0.024 | 61.924 | | |
| 12/9/2008 | 11:10:06 | 20.426 | 0.213 | 437.692 | 0.024 | 68.088 | | |
| 12/9/2008 | 11:10:16 | 20.335 | 0.183 | 459.231 | 43.492 | 67.148 | | |
| 12/9/2008 | 11:10:26 | 20.228 | 0.213 | 455.897 | 7.766 | 67.905 | | |
| 12/9/2008 | 11:10:36 | 20.243 | 0.152 | 477.179 | 1.441 | 70.706 | | |
| 12/9/2008 | 11:10:46 | 20.269 | 0.091 | 473.846 | 0.024 | 72.22 | | |
| 12/9/2008 | 11:10:56 | 20.38 | 0.091 | 481.795 | 0.024 | 69.267 | | |
| 12/9/2008 | 11:11:06 | 20.441 | 0.03 | 526.41 | 0.024 | 65.482 | | |
| 12/9/2008 | 11:11:16 | 20.487 | 0.03 | 503.333 | 0.024 | 65.104 | | |
| 12/9/2008 | 11:11:26 | 20.441 | 0.03 | 488.205 | 0.024 | 66.996 | | |
| 12/9/2008 | 11:11:36 | 20.335 | 0.091 | 489.231 | 0.024 | 70.024 | | |
| 12/9/2008 | 11:11:46 | 20.259 | 0.122 | 481.028 | 0.024 | 85.998 | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|----------|--------|--------|--|--|--|-------------------------|------------|
| | | % | % | VOC 3 ppm C ₂ H ₆ | VOC 1 ppm C ₂ H ₆ | VOC 2 ppm C ₂ H ₆ | | |
| 12/9/2008 | 11:11:56 | 20.182 | 0.122 | 486.154 | 39.756 | 92.054 | | |
| 12/9/2008 | 11:12:06 | 20.182 | 0.122 | 500.769 | 2.686 | 91.07 | | |
| 12/9/2008 | 11:12:16 | 20.152 | 0.061 | 496.154 | 0.024 | 88.847 | | |
| 12/9/2008 | 11:12:26 | 20.274 | 0.03 | 482.564 | 0.024 | 84.408 | | |
| 12/9/2008 | 11:12:36 | 20.396 | 0.03 | 455.128 | 0.024 | 82.867 | | |
| 12/9/2008 | 11:12:46 | 20.502 | 0.03 | 455.385 | 0.024 | 82.212 | | |
| 12/9/2008 | 11:12:56 | 20.578 | 0.03 | 424.359 | 0.024 | 79.109 | | |
| 12/9/2008 | 11:13:06 | 20.809 | 0.03 | 424.872 | 0.024 | 76.535 | | |
| 12/9/2008 | 11:13:16 | 20.533 | 0.03 | 436.867 | 0.024 | 77.443 | | |
| 12/9/2008 | 11:13:26 | 20.396 | 0.061 | 448.462 | 0.024 | 75.778 | | |
| 12/9/2008 | 11:13:36 | 20.274 | 0.091 | 450.769 | 39.243 | 74.842 | | |
| 12/9/2008 | 11:13:46 | 20.198 | 0.091 | 454.359 | 5.934 | 73.507 | | |
| 12/9/2008 | 11:13:56 | 20.213 | 0.03 | 484.369 | 0.073 | 71.89 | | |
| 12/9/2008 | 11:14:06 | 20.304 | 0.03 | 479.231 | 0.024 | 70.403 | | |
| 12/9/2008 | 11:14:16 | 20.396 | 0.03 | 464.815 | 0.024 | 69.192 | | |
| 12/9/2008 | 11:14:26 | 20.472 | 0.03 | 450.266 | 0.024 | 68.056 | | |
| 12/9/2008 | 11:14:36 | 20.517 | 0.03 | 445.128 | 0.024 | 68.283 | | |
| 12/9/2008 | 11:14:46 | 20.441 | 0.03 | 432.564 | 0.024 | 68.51 | | |
| 12/9/2008 | 11:14:56 | 20.35 | 0.091 | 428.923 | 0.024 | 67.802 | | |
| 12/9/2008 | 11:15:06 | 20.243 | 0.091 | 408.462 | 0.024 | 64.498 | | |
| 12/9/2008 | 11:15:16 | 20.198 | 0.091 | 391.026 | 33.993 | 63.136 | | |
| 12/9/2008 | 11:15:26 | 20.182 | 0.091 | 376.667 | 2.54 | 62.908 | | |
| 12/9/2008 | 11:15:36 | 20.187 | 0.03 | 365.385 | 0.024 | 63.06 | | |
| 12/9/2008 | 11:15:46 | 20.259 | 0.03 | 367.436 | 0.024 | 63.06 | | |
| 12/9/2008 | 11:15:56 | 20.38 | 0.03 | 364.103 | 0.024 | 62.757 | | |
| 12/9/2008 | 11:16:06 | 20.487 | 0.03 | 350.789 | 0.024 | 63.287 | | |
| 12/9/2008 | 11:16:16 | 20.594 | 0.03 | 346.923 | 0.024 | 66.391 | | |
| 12/9/2008 | 11:16:26 | 20.578 | 0.03 | 332.308 | 0.024 | 66.315 | | |
| 12/9/2008 | 11:16:36 | 20.502 | 0.03 | 331.538 | 0.024 | 65.179 | | |
| 12/9/2008 | 11:16:46 | 20.152 | 0.792 | 321.282 | 0.024 | 64.12 | | |
| 12/9/2008 | 11:16:56 | 17.288 | 4.082 | 320.513 | 26.867 | 63.211 | | |
| 12/9/2008 | 11:17:06 | 11.729 | 6.885 | 315.385 | 3.785 | 62.681 | | |
| 12/9/2008 | 11:17:16 | 6.656 | 8.286 | 316.923 | 0.024 | 62.303 | | |
| 12/9/2008 | 11:17:26 | 3.188 | 8.956 | 318.205 | 0.024 | 61.167 | | |
| 12/9/2008 | 11:17:36 | 1.158 | 9.2 | 316.667 | 0.024 | 60.637 | | |
| 12/9/2008 | 11:17:46 | 0.061 | 9.413 | 318.462 | 0.024 | 59.426 | | |
| 12/9/2008 | 11:17:56 | 0.015 | 9.535 | 328.974 | 0.024 | 59.048 | | |
| 12/9/2008 | 11:18:06 | 0.015 | 9.596 | 319.744 | 0.024 | 59.426 | | |
| 12/9/2008 | 11:18:16 | 0.015 | 9.657 | 311.282 | 0.024 | 58.869 | | |
| 12/9/2008 | 11:18:26 | 0.015 | 9.87 | 313.59 | 0.024 | 57.685 | | |
| 12/9/2008 | 11:18:36 | 0.015 | 9.87 | 307.949 | 22.344 | 56.928 | | |
| 12/9/2008 | 11:18:46 | 0.015 | 9.892 | 309.744 | 0.855 | 57.534 | | |
| 12/9/2008 | 11:18:56 | 0.015 | 10.023 | 308.41 | 0.024 | 56.625 | | |
| 12/9/2008 | 11:19:06 | 0.015 | 10.023 | 320.256 | 0.024 | 55.565 | | |
| 12/9/2008 | 11:19:16 | 0.015 | 10.053 | 337.436 | 0.024 | 54.278 | | |
| 12/9/2008 | 11:19:26 | 0.015 | 10.084 | 337.179 | 0.024 | 53.294 | | |
| 12/9/2008 | 11:19:36 | 0.015 | 10.084 | 310.513 | 0.024 | 54.733 | | |
| 12/9/2008 | 11:19:46 | 0.015 | 8.499 | 308.462 | 0.024 | 54.98 | | |
| 12/9/2008 | 11:19:56 | 1.203 | 6.062 | 307.692 | 0.024 | 54.884 | | |
| 12/9/2008 | 11:20:06 | 6.895 | 3.107 | 306.154 | 0.024 | 54.733 | | |
| 12/9/2008 | 11:20:16 | 10.815 | 1.188 | 275.385 | 19.121 | 54.505 | | |
| 12/9/2008 | 11:20:26 | 14.812 | 0.366 | 274.872 | 2.222 | 53.446 | | |
| 12/9/2008 | 11:20:36 | 17.623 | 0.03 | 271.282 | 0.024 | 53.446 | | |
| 12/9/2008 | 11:20:46 | 19.192 | 0.03 | 286.867 | 0.024 | 53.143 | | |
| 12/9/2008 | 11:20:56 | 20.03 | 0.03 | 262.051 | 0.024 | 52.007 | | |
| 12/9/2008 | 11:21:06 | 20.457 | 0.03 | 257.949 | 0.024 | 52.007 | | |
| 12/9/2008 | 11:21:16 | 20.67 | 0.03 | 257.692 | 0.024 | 50.72 | | |
| 12/9/2008 | 11:21:26 | 20.761 | 0.03 | 255.128 | 0.024 | 51.326 | | |
| 12/9/2008 | 11:21:36 | 20.807 | 0.03 | 251.026 | 0.024 | 51.705 | | |
| 12/9/2008 | 11:21:46 | 20.853 | 0.03 | 254.815 | 0.024 | 50.796 | | |
| 12/9/2008 | 11:21:56 | 20.837 | 0.03 | 251.795 | 16.996 | 50.796 | | |
| 12/9/2008 | 11:22:06 | 20.853 | 0.03 | 245.385 | 0.024 | 50.115 | | |
| 12/9/2008 | 11:22:16 | 20.868 | 0.03 | 248.205 | 0.024 | 48.828 | | |
| 12/9/2008 | 11:22:26 | 20.863 | 0.03 | 228.462 | 0.024 | 48.904 | | |
| 12/9/2008 | 11:22:36 | 20.868 | 0.03 | 225.128 | 0.024 | 48.147 | | |
| 12/9/2008 | 11:22:46 | 20.898 | 0.03 | 208.205 | 0.024 | 49.509 | | |
| 12/9/2008 | 11:22:56 | 20.898 | 0.03 | 215.897 | 0.024 | 48.298 | | |
| 12/9/2008 | 11:23:06 | 20.898 | 0.03 | 207.436 | 0.024 | 48.222 | | |
| 12/9/2008 | 11:23:16 | 20.898 | 0.03 | 212.308 | 0.415 | 48.071 | | |
| 12/9/2008 | 11:23:26 | 20.914 | 0.03 | 213.333 | 0.024 | 47.011 | | |
| 12/9/2008 | 11:23:36 | 20.822 | 0.03 | 221.026 | 7.863 | 47.465 | | |
| 12/9/2008 | 11:23:46 | 20.855 | 0.03 | 238.462 | 33.553 | 47.087 | | |
| 12/9/2008 | 11:23:56 | 20.517 | 0.03 | 245.128 | 39.902 | 45.724 | | |
| 12/9/2008 | 11:24:06 | 20.472 | 0.03 | 253.077 | 42.491 | 46.027 | | |
| 12/9/2008 | 11:24:16 | 20.517 | 0.03 | 253.333 | 42.857 | 45.8 | | |

Mid range drift check 0.15%

Zero drift check 0.00%

Hi range drift check 0.07%

Zero drift check 0.00%

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Sughouse | Calibration Comments | Error % |
|-----------|----------|--------|-------|--|--|--|-------------------------|------------|
| | | % | % | VOC 3 ppm C ₂ H ₆ | VOC 1 ppm C ₂ H ₆ | VOC 2 ppm C ₂ H ₆ | | |
| 12/9/2008 | 11:24:26 | 20.563 | 0.03 | 250.769 | 42.906 | 45.724 | | |
| 12/9/2008 | 11:24:36 | 20.517 | 0.03 | 259.744 | 39.438 | 45.648 | | |
| 12/9/2008 | 11:24:46 | 20.411 | 0.03 | 242.564 | 35.702 | 49.282 | | |
| 12/9/2008 | 11:24:56 | 20.319 | 0.081 | 221.538 | 31.282 | 56.095 | | |
| 12/9/2008 | 11:25:06 | 20.259 | 0.03 | 191.282 | 27.819 | 60.259 | | |
| 12/9/2008 | 11:25:16 | 20.243 | 0.03 | 200.513 | 24.298 | 65.937 | | |
| 12/9/2008 | 11:25:26 | 20.289 | 0.081 | 215.128 | 22.468 | 66.694 | | |
| 12/9/2008 | 11:25:36 | 20.182 | 0.091 | 257.949 | 22.857 | 48.762 | | |
| 12/9/2008 | 11:25:46 | 20.213 | 0.03 | 259.744 | 23.907 | 42.545 | | |
| 12/9/2008 | 11:25:56 | 20.319 | 0.03 | 226.923 | 25.739 | 43.15 | | |
| 12/9/2008 | 11:26:06 | 20.472 | 0.03 | 209.744 | 27.155 | 41.636 | | |
| 12/9/2008 | 11:26:16 | 20.583 | 0.03 | 221.538 | 25.588 | 40.046 | | |
| 12/9/2008 | 11:26:26 | 20.457 | 0.03 | 241.282 | 24.469 | 37.473 | | |
| 12/9/2008 | 11:26:36 | 20.38 | 0.03 | 227.436 | 25.788 | 40.122 | | |
| 12/9/2008 | 11:26:46 | 20.319 | 0.03 | 210.513 | 25.714 | 41.56 | | |
| 12/9/2008 | 11:26:56 | 20.259 | 0.081 | 233.077 | 26.545 | 39.516 | | |
| 12/9/2008 | 11:27:06 | 20.213 | 0.244 | 259.231 | 27.008 | 39.138 | | |
| 12/9/2008 | 11:27:16 | 20.213 | 0.152 | 248.462 | 25.448 | 40.576 | | |
| 12/9/2008 | 11:27:26 | 20.35 | 0.03 | 233.077 | 26.935 | 41.883 | | |
| 12/9/2008 | 11:27:36 | 20.472 | 0.03 | 250 | 27.131 | 43.302 | | |
| 12/9/2008 | 11:27:46 | 20.583 | 0.03 | 256.867 | 27.814 | 44.134 | | |
| 12/9/2008 | 11:27:56 | 20.548 | 0.091 | 272.051 | 5.568 | 45.648 | | |
| 12/9/2008 | 11:28:06 | 20.441 | 0.183 | 282.051 | 0.024 | 46.935 | | |
| 12/9/2008 | 11:28:16 | 20.335 | 0.213 | 296.923 | 0.024 | 45.951 | | |
| 12/9/2008 | 11:28:26 | 20.259 | 0.244 | 317.436 | 0.024 | 44.569 | | |
| 12/9/2008 | 11:28:36 | 20.213 | 0.213 | 310.513 | 0.024 | 44.437 | | |
| 12/9/2008 | 11:28:46 | 20.198 | 0.244 | 280.769 | 0.024 | 44.967 | | |
| 12/9/2008 | 11:28:56 | 20.182 | 0.244 | 278.205 | 0.024 | 46.178 | | |
| 12/9/2008 | 11:29:06 | 20.213 | 0.152 | 287.179 | 0.024 | 62.984 | | |
| 12/9/2008 | 11:29:16 | 20.335 | 0.061 | 270.256 | 0.024 | 75.021 | | |
| 12/9/2008 | 11:29:26 | 20.457 | 0.03 | 272.821 | 0.024 | 77.67 | | |
| 12/9/2008 | 11:29:36 | 20.533 | 0.091 | 267.436 | 0.024 | 77.973 | | |
| 12/9/2008 | 11:29:46 | 20.472 | 0.152 | 271.795 | 0.024 | 76.232 | | |
| 12/9/2008 | 11:29:56 | 20.396 | 0.183 | 274.103 | 0.024 | 76.459 | | |
| 12/9/2008 | 11:30:06 | 20.304 | 0.213 | 278.718 | 1.954 | 59.275 | | |
| 12/9/2008 | 11:30:16 | 20.259 | 0.213 | 271.282 | 18.193 | 51.099 | | |
| 12/9/2008 | 11:30:26 | 20.213 | 0.183 | 262.051 | 2.637 | 49.358 | | |
| 12/9/2008 | 11:30:36 | 20.228 | 0.091 | 255.128 | 0.024 | 48.86 | | |
| 12/9/2008 | 11:30:46 | 20.335 | 0.03 | 252.584 | 0.024 | 45.497 | | |
| 12/9/2008 | 11:30:56 | 20.457 | 0.03 | 245.385 | 0.024 | 31.038 | | |
| 12/9/2008 | 11:31:06 | 20.548 | 0.03 | 265.128 | 0.024 | 12.718 | | |
| 12/9/2008 | 11:31:16 | 20.533 | 0.091 | 286.867 | 0.024 | 8.479 | | |
| 12/9/2008 | 11:31:26 | 20.457 | 0.183 | 312.564 | 0.024 | 5.905 | | |
| 12/9/2008 | 11:31:36 | 20.319 | 0.244 | 311.538 | 0.024 | 5.602 | | |
| 12/9/2008 | 11:31:46 | 20.274 | 0.244 | 281.795 | 0.293 | 6.586 | | |
| 12/9/2008 | 11:31:56 | 20.228 | 0.183 | 300.769 | 16.264 | 5.678 | | |
| 12/9/2008 | 11:32:06 | 20.213 | 0.152 | 336.867 | 0.342 | 3.861 | | |
| 12/9/2008 | 11:32:16 | 20.167 | 0.061 | 340.513 | 0.024 | 2.574 | | |
| 12/9/2008 | 11:32:26 | 20.243 | 0.03 | 320.769 | 0.024 | 3.028 | | |
| 12/9/2008 | 11:32:36 | 20.396 | 0.03 | 301.538 | 0.024 | 4.391 | | |
| 12/9/2008 | 11:32:46 | 20.517 | 0.03 | 289.744 | 0.024 | 4.164 | | |
| 12/9/2008 | 11:32:56 | 20.578 | 0.03 | 319.744 | 0.024 | 2.877 | | |
| 12/9/2008 | 11:33:06 | 20.517 | 0.03 | 328.718 | 0.024 | 1.514 | | |
| 12/9/2008 | 11:33:16 | 20.38 | 0.091 | 317.949 | 0.024 | 1.514 | | |
| 12/9/2008 | 11:33:26 | 20.304 | 0.061 | 285.385 | 3.175 | 3.482 | | |
| 12/9/2008 | 11:33:36 | 20.243 | 0.03 | 277.436 | 17.705 | 3.028 | | |
| 12/9/2008 | 11:33:46 | 20.228 | 0.061 | 307.438 | 2.1 | 1.287 | | |
| 12/9/2008 | 11:33:56 | 20.213 | 0.03 | 313.59 | 0.024 | 0.53 | | |
| 12/9/2008 | 11:34:06 | 20.319 | 0.03 | 311.538 | 0.024 | 1.741 | | |
| 12/9/2008 | 11:34:16 | 20.441 | 0.03 | 298.205 | 0.024 | 3.028 | | |
| 12/9/2008 | 11:34:26 | 20.533 | 0.03 | 287.179 | 0.024 | 2.65 | | |
| 12/9/2008 | 11:34:36 | 20.548 | 0.03 | 315.897 | 0.024 | 1.817 | | |
| 12/9/2008 | 11:34:46 | 20.457 | 0.03 | 323.333 | 0.024 | 0.908 | | |
| 12/9/2008 | 11:34:56 | 20.335 | 0.061 | 340.513 | 0.024 | 0.379 | | |
| 12/9/2008 | 11:35:06 | 20.243 | 0.081 | 325.897 | 0.024 | 0.151 | | |
| 12/9/2008 | 11:35:16 | 20.213 | 0.091 | 308.974 | 15.558 | 0.151 | | |
| 12/9/2008 | 11:35:26 | 20.198 | 0.091 | 308.718 | 0.283 | 0.881 | | |
| 12/9/2008 | 11:35:36 | 20.213 | 0.03 | 296.867 | 0.024 | 1.893 | | |
| 12/9/2008 | 11:35:46 | 20.304 | 0.03 | 291.026 | 0.024 | 2.422 | | |
| 12/9/2008 | 11:35:56 | 20.411 | 0.03 | 342.051 | 0.024 | 0.908 | | |
| 12/9/2008 | 11:36:06 | 20.487 | 0.03 | 341.795 | 0.024 | 0.076 | | |
| 12/9/2008 | 11:36:16 | 20.578 | 0.03 | 311.795 | 0.024 | 9.69 | | |
| 12/9/2008 | 11:36:26 | 20.563 | 0.03 | 315.385 | 0.024 | 61.167 | | |
| 12/9/2008 | 11:36:36 | 20.441 | 0.061 | 329.744 | 0.024 | 66.315 | | |
| 12/9/2008 | 11:36:46 | 20.304 | 0.091 | 349.487 | 2.979 | 67.148 | | |

Post-test zero calibration drift check 0.00%

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|----------|--------|-------|-----------------------------------|-----------------------------------|-----------------------------------|---|------------|
| | | % | % | ppm C ₂ H ₆ | ppm C ₂ H ₆ | ppm C ₂ H ₆ | | |
| 12/9/2008 | 11:36:56 | 20.274 | 0.061 | 305.128 | 19.731 | 69.873 | | |
| 12/9/2008 | 11:37:06 | 20.228 | 0.03 | 266.867 | 3.468 | 71.917 | | |
| 12/9/2008 | 11:37:16 | 20.213 | 0.03 | 305.841 | 0.024 | 71.69 | | |
| 12/9/2008 | 11:37:26 | 20.304 | 0.03 | 330.256 | 0.024 | 70.176 | | |
| 12/9/2008 | 11:37:36 | 20.457 | 0.03 | 317.436 | 0.024 | 71.311 | | |
| 12/9/2008 | 11:37:46 | 20.548 | 0.03 | 283.59 | 0.024 | 74.112 | | |
| 12/9/2008 | 11:37:56 | 20.548 | 0.03 | 273.077 | 0.024 | 74.869 | Post-test third range calibration drift check | 0.07% |
| 12/9/2008 | 11:38:06 | 20.441 | 0.03 | 302.564 | 0.024 | 74.112 | | |
| 12/9/2008 | 11:38:16 | 20.365 | 0.091 | 293.59 | 0.024 | 73.734 | | |
| 12/9/2008 | 11:38:26 | 20.289 | 0.091 | 299.231 | 0.024 | 73.507 | | |
| 12/9/2008 | 11:38:36 | 20.213 | 0.061 | 297.179 | 15.36 | 73.507 | | |
| 12/9/2008 | 11:38:46 | 20.213 | 0.061 | 328.974 | 0.342 | 73.507 | | |
| 12/9/2008 | 11:38:56 | 20.198 | 0.03 | 353.077 | 0.024 | 73.355 | | |
| 12/9/2008 | 11:39:06 | 20.639 | 0.03 | 443.846 | 0.024 | 73.204 | | |
| 12/9/2008 | 11:39:16 | 20.792 | 0.03 | 518.974 | 0.024 | 73.734 | | |
| 12/9/2008 | 11:39:26 | 20.883 | 0.03 | 524.359 | 0.024 | 72.901 | | |
| 12/9/2008 | 11:39:36 | 20.959 | 0.03 | 506.923 | 0.024 | 34.899 | | |
| 12/9/2008 | 11:39:46 | 20.883 | 0.03 | 490.769 | 0.024 | 40.803 | | |
| 12/9/2008 | 11:39:56 | 20.792 | 0.03 | 476.923 | 0.024 | 45.573 | | |
| 12/9/2008 | 11:40:06 | 20.7 | 0.03 | 494.615 | 3.565 | 46.557 | | |
| 12/9/2008 | 11:40:16 | 20.624 | 0.061 | 526.41 | 17.187 | 46.481 | | |
| 12/9/2008 | 11:40:26 | 20.594 | 0.061 | 554.359 | 1.783 | 46.708 | | |
| 12/9/2008 | 11:40:36 | 20.639 | 0.03 | 545.385 | 0.024 | 48.071 | | |
| 12/9/2008 | 11:40:46 | 20.792 | 0.03 | 508.462 | 0.024 | 48.804 | | |
| 12/9/2008 | 11:40:56 | 20.914 | 0.03 | 612.308 | 0.024 | 48.601 | | |
| 12/9/2008 | 11:41:06 | 20.974 | 0.03 | 543.846 | 0.024 | 48.525 | | |
| 12/9/2008 | 11:41:16 | 20.898 | 0.03 | 557.692 | 0.024 | 50.493 | | |
| 12/9/2008 | 11:41:26 | 20.792 | 0.061 | 509.487 | 0.024 | 54.581 | | |
| 12/9/2008 | 11:41:36 | 20.731 | 0.03 | 466.154 | 0.024 | 55.263 | | |
| 12/9/2008 | 11:41:46 | 20.594 | 0.091 | 535.385 | 0.024 | 53.976 | | |
| 12/9/2008 | 11:41:56 | 20.563 | 0.091 | 535.385 | 16.284 | 55.944 | | |
| 12/9/2008 | 11:42:06 | 20.578 | 0.061 | 492.584 | 1.221 | 57.988 | | |
| 12/9/2008 | 11:42:16 | 20.594 | 0.03 | 528.718 | 0.024 | 67.299 | | |
| 12/9/2008 | 11:42:26 | 20.685 | 0.03 | 537.18 | 0.024 | 76.913 | | |
| 12/9/2008 | 11:42:36 | 20.807 | 0.03 | 492.051 | 0.024 | 81.38 | | |
| 12/9/2008 | 11:42:46 | 20.944 | 0.03 | 523.333 | 0.024 | 82.384 | | |
| 12/9/2008 | 11:42:56 | 20.929 | 0.03 | 537.436 | 0.024 | 84.786 | | |
| 12/9/2008 | 11:43:06 | 20.883 | 0.03 | 505.385 | 0.024 | 81.758 | | |
| 12/9/2008 | 11:43:16 | 20.776 | 0.03 | 497.949 | 0.024 | 87.905 | | |
| 12/9/2008 | 11:43:26 | 20.7 | 0.061 | 501.282 | 4.444 | 59.048 | | |
| 12/9/2008 | 11:43:36 | 20.624 | 0.091 | 539.487 | 17.383 | 54.051 | | |
| 12/9/2008 | 11:43:46 | 20.594 | 0.061 | 550.513 | 2.173 | 51.932 | | |
| 12/9/2008 | 11:43:56 | 20.594 | 0.03 | 553.59 | 0.024 | 51.829 | | |
| 12/9/2008 | 11:44:06 | 20.761 | 0.03 | 319.487 | 0.024 | 51.705 | | |
| 12/9/2008 | 11:44:16 | 20.868 | 0.03 | 23.077 | 0.024 | 52.159 | | |
| 12/9/2008 | 11:44:26 | 20.944 | 0.03 | 7.436 | 0.024 | 52.537 | | |
| 12/9/2008 | 11:44:36 | 20.898 | 0.03 | 0.256 | 0.024 | 53.143 | | |
| 12/9/2008 | 11:44:46 | 20.792 | 0.03 | 0.256 | 0.024 | 52.462 | | |
| 12/9/2008 | 11:44:56 | 20.7 | 0.091 | 0.256 | 0.024 | 50.947 | | |
| 12/9/2008 | 11:45:06 | 20.809 | 0.091 | 0.256 | 0.684 | 51.705 | | |
| 12/9/2008 | 11:45:16 | 20.809 | 0.061 | 0.256 | 19.318 | 53.976 | | |
| 12/9/2008 | 11:45:26 | 20.548 | 0.091 | 0.256 | 1.49 | 57.382 | | |
| 12/9/2008 | 11:45:36 | 20.548 | 0.03 | 2.308 | 0.024 | 58.215 | | |
| 12/9/2008 | 11:45:46 | 20.67 | 0.03 | 2.051 | 0.024 | 57.534 | | |
| 12/9/2008 | 11:45:56 | 20.807 | 0.03 | 1.538 | 0.024 | 57.079 | | |
| 12/9/2008 | 11:46:06 | 20.883 | 0.03 | 0.513 | 0.024 | 56.398 | | |
| 12/9/2008 | 11:46:16 | 20.929 | 0.03 | 0.256 | 0.024 | 55.792 | | |
| 12/9/2008 | 11:46:26 | 20.868 | 0.03 | 0.256 | 0.024 | 55.565 | | |
| 12/9/2008 | 11:46:36 | 20.781 | 0.03 | 0.256 | 0.024 | 70.933 | | |
| 12/9/2008 | 11:46:46 | 20.639 | 0.061 | 0.256 | 2.198 | 83.045 | | |
| 12/9/2008 | 11:46:56 | 20.594 | 0.061 | 0.256 | 18.828 | 86.679 | | |
| 12/9/2008 | 11:47:06 | 20.563 | 0.03 | 0.256 | 2.862 | 86.527 | | |
| 12/9/2008 | 11:47:16 | 20.578 | 0.03 | 0.256 | 0.024 | 88.344 | | |
| 12/9/2008 | 11:47:26 | 20.781 | 0.03 | 1.538 | 0.024 | 78.2 | | |
| 12/9/2008 | 11:47:36 | 20.883 | 0.061 | 4.359 | 0.024 | 84.952 | | |
| 12/9/2008 | 11:47:46 | 20.829 | 0.061 | 116.923 | 0.024 | 59.426 | | |
| 12/9/2008 | 11:47:56 | 20.883 | 0.152 | 330.769 | 0.024 | 57.004 | | |
| 12/9/2008 | 11:48:06 | 20.776 | 0.183 | 338.462 | 0.024 | 54.43 | | |
| 12/9/2008 | 11:48:16 | 20.885 | 0.213 | 326.923 | 0.024 | 52.84 | | |
| 12/9/2008 | 11:48:26 | 20.809 | 0.213 | 358.874 | 0.024 | 52.689 | | |
| 12/9/2008 | 11:48:36 | 20.563 | 0.213 | 392.584 | 21.221 | 54.581 | | |
| 12/9/2008 | 11:48:46 | 20.533 | 0.274 | 398.205 | 1.197 | 55.111 | | |
| 12/9/2008 | 11:48:56 | 20.563 | 0.213 | 406.154 | 0.024 | 54.278 | | |
| 12/9/2008 | 11:49:06 | 20.655 | 0.091 | 400.769 | 0.024 | 54.884 | | |
| 12/9/2008 | 11:49:16 | 20.776 | 0.061 | 407.436 | 0.024 | 56.928 | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 % | CO2 % | RTO Inlet | | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|----------|--------|-------|---|---|------------|----------|----------------------|---------|
| | | | | VOC 3 ppm C ₂ H ₆ | VOC 1 ppm C ₂ H ₆ | | | | |
| 12/9/2008 | 11:49:26 | 20.883 | 0.03 | 416.687 | 0.024 | 58.886 | | | |
| 12/9/2008 | 11:49:36 | 20.929 | 0.061 | 398.874 | 0.024 | 59.805 | | | |
| 12/9/2008 | 11:49:46 | 20.883 | 0.152 | 384.103 | 0.024 | 61.092 | | | |
| 12/9/2008 | 11:49:56 | 20.781 | 0.213 | 404.872 | 0.024 | 61.849 | | | |
| 12/9/2008 | 11:50:06 | 20.67 | 0.213 | 427.436 | 1.612 | 61.092 | | | |
| 12/9/2008 | 11:50:16 | 20.809 | 0.244 | 400.256 | 25.348 | 58.199 | | | |
| 12/9/2008 | 11:50:26 | 20.578 | 0.213 | 362.821 | 4.249 | 57.888 | | | |
| 12/9/2008 | 11:50:36 | 20.594 | 0.091 | 345.385 | 0.537 | 59.048 | | | |
| 12/9/2008 | 11:50:46 | 20.716 | 0.061 | 365.841 | 0.024 | 61.092 | | | |
| 12/9/2008 | 11:50:56 | 20.837 | 0.03 | 369.487 | 0.024 | 75.324 | | | |
| 12/9/2008 | 11:51:06 | 20.914 | 0.061 | 371.026 | 0.024 | 87.739 | | | |
| 12/9/2008 | 11:51:16 | 20.883 | 0.152 | 349.487 | 0.024 | 88.42 | | | |
| 12/9/2008 | 11:51:26 | 20.782 | 0.213 | 363.846 | 0.024 | 86.149 | | | |
| 12/9/2008 | 11:51:36 | 20.885 | 0.213 | 366.41 | 0.024 | 86.819 | | | |
| 12/9/2008 | 11:51:46 | 20.609 | 0.244 | 374.103 | 0.024 | 78.73 | | | |
| 12/9/2008 | 11:51:56 | 20.578 | 0.213 | 385.841 | 22.637 | 65.634 | | | |
| 12/9/2008 | 11:52:06 | 20.548 | 0.244 | 401.795 | 1.441 | 60.335 | | | |
| 12/9/2008 | 11:52:16 | 20.563 | 0.183 | 406.718 | 0.024 | 58.063 | | | |
| 12/9/2008 | 11:52:26 | 20.7 | 0.03 | 389.487 | 0.024 | 57.306 | | | |
| 12/9/2008 | 11:52:36 | 20.837 | 0.03 | 363.846 | 0.024 | 56.474 | | | |
| 12/9/2008 | 11:52:46 | 20.898 | 0.03 | 387.436 | 0.024 | 56.095 | | | |
| 12/9/2008 | 11:52:56 | 20.929 | 0.03 | 407.436 | 0.024 | 56.247 | | | |
| 12/9/2008 | 11:53:06 | 20.898 | 0.03 | 397.179 | 0.024 | 56.095 | | | |
| 12/9/2008 | 11:53:16 | 20.807 | 0.061 | 422.308 | 0.024 | 55.792 | | | |
| 12/9/2008 | 11:53:26 | 20.7 | 0.091 | 431.282 | 0.806 | 54.98 | | | |
| 12/9/2008 | 11:53:36 | 20.624 | 0.091 | 428.718 | 24.054 | 56.247 | | | |
| 12/9/2008 | 11:53:46 | 20.563 | 0.03 | 433.077 | 4.054 | 59.048 | | | |
| 12/9/2008 | 11:53:56 | 20.639 | 0.03 | 425.897 | 0.024 | 61.697 | | | |
| 12/9/2008 | 11:54:06 | 20.746 | 0.03 | 421.282 | 0.024 | 63.287 | | | |
| 12/9/2008 | 11:54:16 | 20.837 | 0.03 | 459.231 | 0.024 | 62.984 | | | |
| 12/9/2008 | 11:54:26 | 20.898 | 0.03 | 429.487 | 0.024 | 62.908 | | | |
| 12/9/2008 | 11:54:36 | 20.898 | 0.03 | 439.487 | 0.024 | 62.151 | | | |
| 12/9/2008 | 11:54:46 | 20.807 | 0.03 | 390.256 | 0.024 | 60.94 | | | |
| 12/9/2008 | 11:54:56 | 20.7 | 0.091 | 414.615 | 0.024 | 60.183 | | | |
| 12/9/2008 | 11:55:06 | 20.609 | 0.122 | 452.061 | 0.024 | 63.211 | | | |
| 12/9/2008 | 11:55:16 | 20.578 | 0.091 | 406.41 | 23.541 | 79.184 | | | |
| 12/9/2008 | 11:55:26 | 20.533 | 0.061 | 396.154 | 1.661 | 90.313 | | | |
| 12/9/2008 | 11:55:36 | 20.578 | 0.03 | 374.103 | 0.024 | 91.978 | | | |
| 12/9/2008 | 11:56:46 | 20.7 | 0.03 | 376.667 | 0.024 | 88.858 | | | |
| 12/9/2008 | 11:56:56 | 20.822 | 0.03 | 406.41 | 0.024 | 89.328 | | | |
| 12/9/2008 | 11:56:06 | 20.914 | 0.03 | 426.41 | 0.024 | 82.288 | | | |
| 12/9/2008 | 11:56:16 | 20.944 | 0.03 | 429.231 | 0.024 | 87.829 | | | |
| 12/9/2008 | 11:56:26 | 20.888 | 0.03 | 426.923 | 0.024 | 61.849 | | | |
| 12/9/2008 | 11:56:36 | 20.792 | 0.061 | 429.744 | 0.024 | 60.864 | | | |
| 12/9/2008 | 11:56:46 | 20.685 | 0.122 | 413.59 | 0.024 | 58.275 | | | |
| 12/9/2008 | 11:56:56 | 20.594 | 0.091 | 412.308 | 23.468 | 58.139 | | | |
| 12/9/2008 | 11:57:06 | 20.594 | 0.03 | 430.513 | 3.58 | 57.231 | | | |
| 12/9/2008 | 11:57:16 | 20.839 | 0.03 | 404.103 | 0.293 | 57.685 | | | |
| 12/9/2008 | 11:57:26 | 20.731 | 0.03 | 410.513 | 0.024 | 57.306 | | | |
| 12/9/2008 | 11:57:36 | 20.822 | 0.03 | 454.103 | 0.024 | 55.717 | | | |
| 12/9/2008 | 11:57:46 | 20.929 | 0.03 | 450.256 | 0.024 | 57.458 | | | |
| 12/9/2008 | 11:57:56 | 20.898 | 0.03 | 461.795 | 0.024 | 57.912 | | | |
| 12/9/2008 | 11:58:06 | 20.761 | 0.061 | 467.436 | 0.024 | 58.063 | | | |
| 12/9/2008 | 11:58:16 | 20.655 | 0.091 | 480.513 | 0.024 | 57.836 | | | |
| 12/9/2008 | 11:58:26 | 20.594 | 0.091 | 410.513 | 0.024 | 82.984 | | | |
| 12/9/2008 | 11:58:36 | 20.533 | 0.061 | 430 | 28.349 | 66.466 | | | |
| 12/9/2008 | 11:58:46 | 20.517 | 0.091 | 443.846 | 2.1 | 66.789 | | | |
| 12/9/2008 | 11:58:56 | 20.563 | 0.03 | 492.564 | 0.024 | 61.394 | | | |
| 12/9/2008 | 11:59:06 | 20.67 | 0.03 | 460.769 | 0.024 | 60.789 | | | |
| 12/9/2008 | 11:59:16 | 20.807 | 0.03 | 430.769 | 0.024 | 61.897 | | | |
| 12/9/2008 | 11:59:26 | 20.914 | 0.03 | 441.028 | 0.024 | 65.834 | | | |
| 12/9/2008 | 11:59:36 | 20.959 | 0.03 | 431.795 | 0.024 | 77.973 | | | |
| 12/9/2008 | 11:59:46 | 20.929 | 0.03 | 432.821 | 0.024 | 89.48 | | | |
| 12/9/2008 | 11:59:56 | 20.853 | 0.061 | 403.333 | 0.024 | 90.085 | | | |
| 12/9/2008 | 12:00:06 | 20.731 | 0.091 | 405.897 | 0.024 | 89.328 | | | |
| 12/9/2008 | 12:00:16 | 20.609 | 0.091 | 420.769 | 27.131 | 89.177 | | | |
| 12/9/2008 | 12:00:26 | 20.594 | 0.061 | 438.974 | 4.005 | 84.332 | | | |
| 12/9/2008 | 12:00:36 | 20.855 | 0.03 | 460.513 | 0.024 | 68.889 | | | |
| 12/9/2008 | 12:00:46 | 20.781 | 0.03 | 465.897 | 0.024 | 65.028 | | | |
| 12/9/2008 | 12:00:56 | 20.868 | 0.03 | 460.769 | 0.024 | 62.908 | | | |
| 12/9/2008 | 12:01:06 | 20.914 | 0.03 | 442.821 | 0.024 | 61.697 | | | |
| 12/9/2008 | 12:01:16 | 20.898 | 0.03 | 419.231 | 0.024 | 60.713 | | | |
| 12/9/2008 | 12:01:26 | 20.822 | 0.03 | 431.028 | 0.024 | 62.757 | | | |
| 12/9/2008 | 12:01:36 | 20.7 | 0.061 | 425.385 | 0.024 | 63.893 | | | |
| 12/9/2008 | 12:01:46 | 20.594 | 0.091 | 425.385 | 0.024 | 63.741 | | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|----------|--------|-------|--|--|--|-------------------------|------------|
| | | % | % | VOC 3 ppm C ₆ H ₆ | VOC 1 ppm C ₆ H ₆ | VOC 2 ppm C ₆ H ₆ | | |
| 12/9/2008 | 12:01:56 | 20.517 | 0.091 | 435.385 | 30.159 | 63.06 | | |
| 12/9/2008 | 12:02:06 | 20.502 | 0.152 | 464.103 | 1.465 | 60.183 | | |
| 12/9/2008 | 12:02:16 | 20.563 | 0.03 | 471.795 | 0.024 | 59.805 | | |
| 12/9/2008 | 12:02:26 | 20.67 | 0.03 | 451.026 | 0.024 | 62.964 | | |
| 12/9/2008 | 12:02:36 | 20.761 | 0.03 | 474.615 | 0.024 | 61.924 | | |
| 12/9/2008 | 12:02:46 | 20.837 | 0.03 | 475.128 | 0.024 | 60.486 | | |
| 12/9/2008 | 12:02:56 | 20.944 | 0.03 | 464.872 | 0.024 | 66.239 | | |
| 12/9/2008 | 12:03:06 | 20.814 | 0.03 | 462.051 | 0.024 | 78.913 | | |
| 12/9/2008 | 12:03:16 | 20.807 | 0.061 | 485.897 | 0.024 | 84.408 | | |
| 12/9/2008 | 12:03:26 | 20.685 | 0.122 | 472.308 | 0.024 | 87.057 | | |
| 12/9/2008 | 12:03:36 | 20.809 | 0.091 | 451.282 | 28.034 | 89.707 | | |
| 12/9/2008 | 12:03:46 | 20.578 | 0.183 | 424.615 | 4.371 | 92.659 | | |
| 12/9/2008 | 12:03:56 | 20.624 | 0.122 | 410.513 | 0.342 | 104.772 | | |
| 12/9/2008 | 12:04:06 | 20.7 | 0.061 | 411.026 | 0.024 | 112.493 | | |
| 12/9/2008 | 12:04:16 | 20.807 | 0.061 | 411.026 | 0.024 | 104.62 | | |
| 12/9/2008 | 12:04:26 | 20.853 | 0.091 | 436.154 | 0.024 | 100.808 | | |
| 12/9/2008 | 12:04:36 | 20.883 | 0.152 | 452.308 | 0.024 | 103.788 | | |
| 12/9/2008 | 12:04:46 | 20.746 | 0.244 | 468.718 | 0.024 | 104.82 | | |
| 12/9/2008 | 12:04:56 | 20.609 | 0.305 | 477.179 | 0.024 | 93.114 | | |
| 12/9/2008 | 12:05:06 | 20.533 | 0.305 | 470.769 | 0.024 | 87.512 | | |
| 12/9/2008 | 12:05:16 | 20.517 | 0.274 | 450.256 | 29.011 | 86.803 | | |
| 12/9/2008 | 12:05:26 | 20.487 | 0.305 | 448.462 | 1.343 | 86.149 | | |
| 12/9/2008 | 12:05:36 | 20.487 | 0.183 | 412.564 | 0.024 | 88.647 | | |
| 12/9/2008 | 12:05:46 | 20.639 | 0.091 | 410.513 | 0.024 | 84.559 | | |
| 12/9/2008 | 12:05:56 | 20.807 | 0.03 | 449.744 | 0.024 | 76.886 | | |
| 12/9/2008 | 12:06:06 | 20.883 | 0.03 | 438.974 | 0.024 | 70.933 | | |
| 12/9/2008 | 12:06:16 | 20.959 | 0.03 | 445.897 | 0.024 | 67.905 | | |
| 12/9/2008 | 12:06:26 | 20.883 | 0.091 | 445.385 | 0.024 | 85.785 | | |
| 12/9/2008 | 12:06:36 | 20.853 | 0.213 | 464.103 | 0.024 | 64.271 | | |
| 12/9/2008 | 12:06:46 | 20.716 | 0.244 | 508.462 | 0.024 | 63.211 | | |
| 12/9/2008 | 12:06:56 | 20.809 | 0.274 | 486.867 | 32.798 | 84.422 | | |
| 12/9/2008 | 12:07:06 | 20.533 | 0.244 | 486.923 | 4.567 | 84.877 | | |
| 12/9/2008 | 12:07:16 | 20.578 | 0.152 | 515.385 | 0.024 | 65.179 | | |
| 12/9/2008 | 12:07:26 | 20.716 | 0.091 | 480.769 | 0.024 | 68.889 | | |
| 12/9/2008 | 12:07:36 | 20.853 | 0.03 | 471.282 | 0.024 | 74.188 | | |
| 12/9/2008 | 12:07:46 | 20.914 | 0.03 | 440.513 | 0.024 | 82.384 | | |
| 12/9/2008 | 12:07:56 | 20.914 | 0.091 | 423.333 | 0.024 | 85.543 | | |
| 12/9/2008 | 12:08:06 | 20.853 | 0.183 | 446.923 | 0.024 | 86.149 | | |
| 12/9/2008 | 12:08:16 | 20.731 | 0.244 | 444.103 | 0.024 | 95.98 | | |
| 12/9/2008 | 12:08:26 | 20.594 | 0.274 | 443.846 | 0.024 | 102.425 | | |
| 12/9/2008 | 12:08:36 | 20.548 | 0.274 | 430.513 | 28.303 | 98.186 | | |
| 12/9/2008 | 12:08:46 | 20.517 | 0.274 | 439.744 | 0.952 | 95.687 | | |
| 12/9/2008 | 12:08:56 | 20.517 | 0.213 | 452.821 | 0.024 | 99.018 | | |
| 12/9/2008 | 12:09:06 | 20.639 | 0.03 | 472.564 | 0.024 | 98.261 | | |
| 12/9/2008 | 12:09:16 | 20.776 | 0.03 | 478.206 | 0.024 | 88.799 | | |
| 12/9/2008 | 12:09:26 | 20.853 | 0.03 | 456.41 | 0.024 | 88.225 | | |
| 12/9/2008 | 12:09:36 | 20.944 | 0.03 | 445.128 | 0.024 | 85.922 | | |
| 12/9/2008 | 12:09:46 | 20.944 | 0.03 | 419.487 | 0.024 | 84.181 | | |
| 12/9/2008 | 12:09:56 | 20.822 | 0.03 | 424.872 | 0.024 | 78.882 | | |
| 12/9/2008 | 12:10:06 | 20.7 | 0.091 | 471.795 | 0.024 | 70.327 | | |
| 12/9/2008 | 12:10:16 | 20.809 | 0.091 | 490.513 | 33.48 | 86.012 | | |
| 12/9/2008 | 12:10:26 | 20.548 | 0.091 | 480.769 | 4.933 | 84.801 | | |
| 12/9/2008 | 12:10:36 | 20.578 | 0.03 | 508.462 | 0.024 | 84.877 | | |
| 12/9/2008 | 12:10:46 | 20.87 | 0.03 | 500.266 | 0.024 | 65.285 | | |
| 12/9/2008 | 12:10:56 | 20.776 | 0.03 | 520.266 | 0.024 | 65.331 | | |
| 12/9/2008 | 12:11:06 | 20.853 | 0.03 | 497.179 | 0.024 | 65.568 | | |
| 12/9/2008 | 12:11:16 | 20.898 | 0.03 | 468.974 | 0.024 | 65.407 | | |
| 12/9/2008 | 12:11:26 | 20.782 | 0.03 | 483.848 | 0.024 | 71.69 | | |
| 12/9/2008 | 12:11:36 | 20.855 | 0.091 | 495.385 | 0.024 | 75.626 | | |
| 12/9/2008 | 12:11:46 | 20.578 | 0.122 | 499.231 | 0.024 | 78.276 | | |
| 12/9/2008 | 12:11:56 | 20.533 | 0.122 | 498.974 | 33.431 | 79.839 | | |
| 12/9/2008 | 12:12:06 | 20.457 | 0.122 | 554.872 | 1.734 | 80.698 | | |
| 12/9/2008 | 12:12:16 | 20.487 | 0.03 | 538.205 | 0.024 | 80.774 | | |
| 12/9/2008 | 12:12:26 | 20.639 | 0.03 | 468.205 | 0.024 | 81.38 | | |
| 12/9/2008 | 12:12:36 | 20.792 | 0.03 | 428.974 | 0.024 | 91.07 | | |
| 12/9/2008 | 12:12:46 | 20.883 | 0.03 | 437.179 | 0.024 | 97.731 | | |
| 12/9/2008 | 12:12:56 | 20.944 | 0.03 | 436.867 | 0.024 | 99.775 | | |
| 12/9/2008 | 12:13:06 | 20.883 | 0.03 | 449.231 | 0.024 | 108.513 | | |
| 12/9/2008 | 12:13:16 | 20.822 | 0.061 | 428.974 | 0.024 | 110.374 | | |
| 12/9/2008 | 12:13:26 | 20.655 | 0.122 | 456.154 | 0.024 | 109.541 | | |
| 12/9/2008 | 12:13:36 | 20.578 | 0.122 | 460.286 | 30.847 | 112.039 | | |
| 12/9/2008 | 12:13:46 | 20.502 | 0.091 | 476.867 | 3.932 | 99.851 | | |
| 12/9/2008 | 12:13:56 | 20.578 | 0.03 | 485.641 | 0.024 | 81.91 | | |
| 12/9/2008 | 12:14:06 | 20.716 | 0.03 | 478.974 | 0.024 | 73.885 | | |
| 12/9/2008 | 12:14:16 | 20.792 | 0.03 | 462.821 | 0.024 | 72.088 | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|----------|--------|-------|-----------------------------------|-----------------------------------|-----------------------------------|-------------------------|------------|
| | | % | % | ppm C ₂ H ₆ | ppm C ₂ H ₆ | ppm C ₂ H ₆ | | |
| 12/9/2008 | 12:14:26 | 20.853 | 0.03 | 473.333 | 0.024 | 68.662 | | |
| 12/9/2008 | 12:14:36 | 20.868 | 0.03 | 437.179 | 0.024 | 67.148 | | |
| 12/9/2008 | 12:14:46 | 20.776 | 0.061 | 458.674 | 0.024 | 66.542 | | |
| 12/9/2008 | 12:14:56 | 20.885 | 0.091 | 479.487 | 0.024 | 67.526 | | |
| 12/9/2008 | 12:15:06 | 20.578 | 0.122 | 458.718 | 0.024 | 68.208 | | |
| 12/9/2008 | 12:15:16 | 20.517 | 0.091 | 473.59 | 34.017 | 68.283 | | |
| 12/9/2008 | 12:15:26 | 20.517 | 0.091 | 500.769 | 1.661 | 68.208 | | |
| 12/9/2008 | 12:15:36 | 20.648 | 0.03 | 502.821 | 0.024 | 68.965 | | |
| 12/9/2008 | 12:15:46 | 20.7 | 0.03 | 495.385 | 0.024 | 72.825 | | |
| 12/9/2008 | 12:15:56 | 20.776 | 0.03 | 470.769 | 0.024 | 77.87 | | |
| 12/9/2008 | 12:16:06 | 20.883 | 0.03 | 492.821 | 0.024 | 81.758 | | |
| 12/9/2008 | 12:16:16 | 20.888 | 0.03 | 475.385 | 0.024 | 81.91 | | |
| 12/9/2008 | 12:16:26 | 20.944 | 0.03 | 505.385 | 0.024 | 79.336 | | |
| 12/9/2008 | 12:16:36 | 20.822 | 0.03 | 499.744 | 0.024 | 76.005 | | |
| 12/9/2008 | 12:18:46 | 20.7 | 0.091 | 479.231 | 0.024 | 73.204 | | |
| 12/9/2008 | 12:18:56 | 20.624 | 0.091 | 435.641 | 33.626 | 73.204 | | |
| 12/9/2008 | 12:17:06 | 20.548 | 0.03 | 424.359 | 5.031 | 75.021 | | |
| 12/9/2008 | 12:17:16 | 20.624 | 0.03 | 427.438 | 0.464 | 82.894 | | |
| 12/9/2008 | 12:17:26 | 20.761 | 0.03 | 408.667 | 0.024 | 103.182 | | |
| 12/9/2008 | 12:17:36 | 20.822 | 0.03 | 403.59 | 0.024 | 109.238 | | |
| 12/9/2008 | 12:17:46 | 20.868 | 0.03 | 422.564 | 0.024 | 106.286 | | |
| 12/9/2008 | 12:17:56 | 20.837 | 0.03 | 453.077 | 0.024 | 99.321 | | |
| 12/9/2008 | 12:18:06 | 20.776 | 0.061 | 453.077 | 0.024 | 98.943 | | |
| 12/9/2008 | 12:18:16 | 20.885 | 0.091 | 466.154 | 0.024 | 83.424 | | |
| 12/9/2008 | 12:18:26 | 20.578 | 0.091 | 428.718 | 0.024 | 75.172 | | |
| 12/9/2008 | 12:18:36 | 20.533 | 0.061 | 438.718 | 36.19 | 72.523 | | |
| 12/9/2008 | 12:18:46 | 20.517 | 0.061 | 436.923 | 2.418 | 70.706 | | |
| 12/9/2008 | 12:18:56 | 20.548 | 0.03 | 428.718 | 0.024 | 71.841 | | |
| 12/9/2008 | 12:19:06 | 20.639 | 0.03 | 446.41 | 0.024 | 70.252 | | |
| 12/9/2008 | 12:19:16 | 20.746 | 0.03 | 475.897 | 0.024 | 68.586 | | |
| 12/9/2008 | 12:19:26 | 20.837 | 0.03 | 452.584 | 0.024 | 70.252 | | |
| 12/9/2008 | 12:19:36 | 20.914 | 0.03 | 442.564 | 0.024 | 71.841 | | |
| 12/9/2008 | 12:19:46 | 20.883 | 0.03 | 473.333 | 0.024 | 73.28 | | |
| 12/9/2008 | 12:19:56 | 20.761 | 0.061 | 502.821 | 0.024 | 73.053 | | |
| 12/9/2008 | 12:20:06 | 20.609 | 0.122 | 518.154 | 0.024 | 76.686 | | |
| 12/9/2008 | 12:20:16 | 20.548 | 0.152 | 480 | 32.503 | 83.272 | | |
| 12/9/2008 | 12:20:26 | 20.517 | 0.061 | 482.564 | 5.275 | 86.603 | | |
| 12/9/2008 | 12:20:36 | 20.578 | 0.03 | 459.231 | 0.708 | 88.95 | | |
| 12/9/2008 | 12:20:46 | 20.685 | 0.03 | 480.769 | 0.024 | 86.042 | | |
| 12/9/2008 | 12:20:56 | 20.792 | 0.03 | 483.077 | 0.024 | 82.515 | | |
| 12/9/2008 | 12:21:06 | 20.853 | 0.03 | 480.256 | 0.024 | 80.623 | | |
| 12/9/2008 | 12:21:16 | 20.868 | 0.03 | 458.462 | 0.024 | 79.487 | | |
| 12/9/2008 | 12:21:26 | 20.761 | 0.061 | 469.744 | 0.024 | 79.563 | | |
| 12/9/2008 | 12:21:36 | 20.624 | 0.122 | 474.103 | 0.024 | 83.348 | | |
| 12/9/2008 | 12:21:46 | 20.533 | 0.152 | 474.872 | 0.024 | 102.728 | | |
| 12/9/2008 | 12:21:56 | 20.487 | 0.122 | 448.205 | 24.2 | 108.405 | | |
| 12/9/2008 | 12:22:06 | 20.472 | 0.122 | 453.846 | 0.83 | 105.453 | | |
| 12/9/2008 | 12:22:16 | 20.502 | 0.03 | 457.179 | 0.024 | 101.214 | | |
| 12/9/2008 | 12:22:26 | 20.639 | 0.03 | 453.333 | 0.024 | 100.305 | | |
| 12/9/2008 | 12:22:36 | 20.746 | 0.03 | 457.692 | 0.024 | 85.165 | | |
| 12/9/2008 | 12:22:46 | 20.822 | 0.03 | 445.897 | 0.024 | 76.081 | | |
| 12/9/2008 | 12:22:56 | 20.883 | 0.03 | 432.308 | 0.024 | 72.523 | | |
| 12/9/2008 | 12:23:06 | 20.868 | 0.03 | 429.231 | 0.024 | 69.57 | | |
| 12/9/2008 | 12:23:16 | 20.807 | 0.03 | 417.438 | 0.024 | 70.403 | | |
| 12/9/2008 | 12:23:26 | 20.685 | 0.091 | 439.231 | 0.024 | 89.495 | | |
| 12/9/2008 | 12:23:36 | 20.609 | 0.091 | 469.744 | 27.228 | 69.797 | | |
| 12/9/2008 | 12:23:46 | 20.517 | 0.091 | 494.872 | 3.321 | 70.479 | | |
| 12/9/2008 | 12:23:56 | 20.548 | 0.03 | 479.487 | 0.024 | 70.1 | | |
| 12/9/2008 | 12:24:06 | 20.656 | 0.03 | 483.333 | 0.024 | 70.176 | | |
| 12/9/2008 | 12:24:16 | 20.776 | 0.03 | 478.667 | 0.024 | 73.128 | | |
| 12/9/2008 | 12:24:26 | 20.822 | 0.03 | 506.41 | 0.024 | 78.882 | | |
| 12/9/2008 | 12:24:36 | 20.853 | 0.03 | 505.385 | 0.024 | 83.197 | | |
| 12/9/2008 | 12:24:46 | 20.716 | 0.091 | 475.641 | 0.024 | 86.073 | | |
| 12/9/2008 | 12:24:56 | 20.609 | 0.122 | 477.436 | 0.024 | 85.695 | | |
| 12/9/2008 | 12:25:06 | 20.548 | 0.091 | 498.718 | 0.024 | 83.499 | | |
| 12/9/2008 | 12:25:16 | 20.487 | 0.091 | 484.103 | 28.107 | 79.338 | | |
| 12/9/2008 | 12:26:26 | 20.472 | 0.081 | 473.846 | 2.295 | 79.411 | | |
| 12/9/2008 | 12:25:36 | 20.517 | 0.03 | 441.262 | 0.024 | 81.001 | | |
| 12/9/2008 | 12:25:46 | 20.639 | 0.03 | 445.385 | 0.024 | 80.928 | | |
| 12/9/2008 | 12:25:56 | 20.761 | 0.03 | 467.049 | 0.024 | 86.149 | | |
| 12/9/2008 | 12:26:06 | 20.837 | 0.03 | 462.308 | 0.024 | 104.015 | | |
| 12/9/2008 | 12:26:16 | 20.868 | 0.03 | 468.923 | 0.024 | 107.27 | | |
| 12/9/2008 | 12:26:26 | 20.868 | 0.03 | 454.872 | 0.024 | 105.302 | | |
| 12/9/2008 | 12:26:36 | 20.761 | 0.061 | 466.923 | 0.024 | 101.289 | | |
| 12/9/2008 | 12:26:46 | 20.639 | 0.122 | 485.385 | 0.244 | 100.078 | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error/ % |
|-----------|----------|--------|-------|--|--|--|-------------------------|-------------|
| | | % | % | VOC 3 ppm C ₆ H ₆ | VOC 1 ppm C ₆ H ₆ | VOC 2 ppm C ₆ H ₆ | | |
| 12/9/2008 | 12:26:56 | 20.548 | 0.122 | 497.692 | 26.593 | 84.105 | | |
| 12/9/2008 | 12:27:06 | 20.517 | 0.244 | 500.769 | 3.785 | 76.081 | | |
| 12/9/2008 | 12:27:16 | 20.563 | 0.152 | 480.256 | 0.024 | 74.112 | | |
| 12/9/2008 | 12:27:26 | 20.685 | 0.091 | 473.333 | 0.024 | 71.16 | | |
| 12/9/2008 | 12:27:36 | 20.776 | 0.061 | 431.026 | 0.024 | 72.523 | | |
| 12/9/2008 | 12:27:46 | 20.868 | 0.03 | 421.795 | 0.024 | 72.088 | | |
| 12/9/2008 | 12:27:56 | 20.868 | 0.091 | 452.821 | 0.024 | 73.128 | | |
| 12/9/2008 | 12:28:06 | 20.792 | 0.213 | 460.256 | 0.024 | 72.523 | | |
| 12/9/2008 | 12:28:16 | 20.639 | 0.274 | 476.923 | 0.024 | 70.83 | | |
| 12/9/2008 | 12:28:26 | 20.517 | 0.335 | 473.333 | 0.024 | 69.949 | | |
| 12/9/2008 | 12:28:36 | 20.487 | 0.305 | 478.462 | 24.982 | 73.658 | | |
| 12/9/2008 | 12:28:46 | 20.472 | 0.274 | 478.205 | 1.929 | 81.304 | | |
| 12/9/2008 | 12:28:56 | 20.517 | 0.183 | 460 | 0.024 | 87.587 | | |
| 12/9/2008 | 12:29:06 | 20.839 | 0.091 | 446.667 | 0.024 | 91.07 | | |
| 12/9/2008 | 12:29:16 | 20.746 | 0.061 | 477.692 | 0.024 | 89.858 | | |
| 12/9/2008 | 12:29:26 | 20.837 | 0.061 | 538.974 | 0.024 | 85.392 | | |
| 12/9/2008 | 12:29:36 | 20.837 | 0.091 | 544.359 | 0.024 | 79.583 | | |
| 12/9/2008 | 12:29:46 | 20.853 | 0.152 | 509.231 | 0.024 | 78.427 | | |
| 12/9/2008 | 12:29:56 | 20.776 | 0.213 | 449.744 | 0.024 | 79.888 | | |
| 12/9/2008 | 12:30:06 | 20.685 | 0.244 | 423.59 | 0.293 | 82.969 | | |
| 12/9/2008 | 12:30:16 | 20.609 | 0.244 | 435.041 | 25.421 | 91.978 | | |
| 12/9/2008 | 12:30:26 | 20.548 | 0.213 | 427.436 | 3.98 | 111.433 | | |
| 12/9/2008 | 12:30:36 | 20.594 | 0.122 | 407.692 | 0.073 | 114.462 | | |
| 12/9/2008 | 12:30:46 | 20.7 | 0.061 | 401.026 | 0.024 | 110.298 | | |
| 12/9/2008 | 12:30:56 | 20.807 | 0.03 | 416.154 | 0.024 | 105.756 | | |
| 12/9/2008 | 12:31:06 | 20.883 | 0.061 | 420.513 | 0.024 | 103.031 | | |
| 12/9/2008 | 12:31:16 | 20.853 | 0.122 | 458.923 | 0.024 | 86.225 | | |
| 12/9/2008 | 12:31:26 | 20.761 | 0.183 | 455.641 | 0.024 | 77.14 | | |
| 12/9/2008 | 12:31:36 | 20.639 | 0.274 | 454.815 | 0.024 | 74.339 | | |
| 12/9/2008 | 12:31:46 | 20.533 | 0.274 | 448.718 | 0 | 70.933 | | |
| 12/9/2008 | 12:31:56 | 20.517 | 0.244 | 419.744 | 26.081 | 72.523 | | |
| 12/9/2008 | 12:32:06 | 20.487 | 0.274 | 424.359 | 1.636 | 73.507 | | |
| 12/9/2008 | 12:32:16 | 20.533 | 0.152 | 433.077 | 0.024 | 73.658 | | |
| 12/9/2008 | 12:32:26 | 20.839 | 0.091 | 438.974 | 0.024 | 72.977 | | |
| 12/9/2008 | 12:32:36 | 20.761 | 0.03 | 444.359 | 0.024 | 72.75 | | |
| 12/9/2008 | 12:32:46 | 20.853 | 0.03 | 438.482 | 0.024 | 72.22 | | |
| 12/9/2008 | 12:32:56 | 20.898 | 0.03 | 444.615 | 0.024 | 73.431 | | |
| 12/9/2008 | 12:33:06 | 20.898 | 0.03 | 471.538 | 0.024 | 79.79 | | |
| 12/9/2008 | 12:33:16 | 20.837 | 0.03 | 468.462 | 0.024 | 86.225 | | |
| 12/9/2008 | 12:33:26 | 20.716 | 0.061 | 465.385 | 0.024 | 90.01 | | |
| 12/9/2008 | 12:33:36 | 20.624 | 0.091 | 468.974 | 29.768 | 88.723 | | |
| 12/9/2008 | 12:33:46 | 20.548 | 0.091 | 484.615 | 4.957 | 88.193 | | |
| 12/9/2008 | 12:33:56 | 20.563 | 0.03 | 501.282 | 0.024 | 81.38 | | |
| 12/9/2008 | 12:34:06 | 20.655 | 0.03 | 499.487 | 0.024 | 78.579 | | |
| 12/9/2008 | 12:34:16 | 20.761 | 0.03 | 478.718 | 0.024 | 79.109 | | |
| 12/9/2008 | 12:34:26 | 20.853 | 0.03 | 467.438 | 0.024 | 82.137 | | |
| 12/9/2008 | 12:34:36 | 20.883 | 0.03 | 460.769 | 0.024 | 89.404 | | |
| 12/9/2008 | 12:34:46 | 20.761 | 0.03 | 436.923 | 0.024 | 108.86 | | |
| 12/9/2008 | 12:34:56 | 20.639 | 0.091 | 443.077 | 0.024 | 114.689 | | |
| 12/9/2008 | 12:35:06 | 20.578 | 0.122 | 425.897 | 0.024 | 112.669 | | |
| 12/9/2008 | 12:35:16 | 20.487 | 0.122 | 468.205 | 27.179 | 108.664 | | |
| 12/9/2008 | 12:35:26 | 20.472 | 0.152 | 479.231 | 1.221 | 103.106 | | |
| 12/9/2008 | 12:35:36 | 20.472 | 0.081 | 507.692 | 0.024 | 86.962 | | |
| 12/9/2008 | 12:35:46 | 20.809 | 0.03 | 506.923 | 0.024 | 77.443 | | |
| 12/9/2008 | 12:35:56 | 20.731 | 0.03 | 446.154 | 0.024 | 75.399 | | |
| 12/9/2008 | 12:36:06 | 20.837 | 0.03 | 441.538 | 0.024 | 73.658 | | |
| 12/9/2008 | 12:36:16 | 20.898 | 0.03 | 404.872 | 0.024 | 75.551 | | |
| 12/9/2008 | 12:36:26 | 20.883 | 0.03 | 418.462 | 0.024 | 74.587 | | |
| 12/9/2008 | 12:36:36 | 20.807 | 0.061 | 479.487 | 0.024 | 73.885 | | |
| 12/9/2008 | 12:36:46 | 20.67 | 0.122 | 493.59 | 0.024 | 73.204 | | |
| 12/9/2008 | 12:36:56 | 20.578 | 0.122 | 486.205 | 29.939 | 72.598 | | |
| 12/9/2008 | 12:37:06 | 20.517 | 0.091 | 496.41 | 4.347 | 73.204 | | |
| 12/9/2008 | 12:37:16 | 20.563 | 0.03 | 518.487 | 0.024 | 75.369 | | |
| 12/9/2008 | 12:37:26 | 20.885 | 0.03 | 531.795 | 0.024 | 80.168 | | |
| 12/9/2008 | 12:37:36 | 20.776 | 0.03 | 496.923 | 0.024 | 84.786 | | |
| 12/9/2008 | 12:37:46 | 20.822 | 0.03 | 529.231 | 0.024 | 86.527 | | |
| 12/9/2008 | 12:37:56 | 20.837 | 0.03 | 498.923 | 0.024 | 85.922 | | |
| 12/9/2008 | 12:38:06 | 20.761 | 0.091 | 500.256 | 0.024 | 83.348 | | |
| 12/9/2008 | 12:38:16 | 20.839 | 0.122 | 506.41 | 0.024 | 79.563 | | |
| 12/9/2008 | 12:38:26 | 20.548 | 0.152 | 490.513 | 0.024 | 78.049 | | |
| 12/9/2008 | 12:38:36 | 20.487 | 0.122 | 455.128 | 28.449 | 78.2 | | |
| 12/9/2008 | 12:38:46 | 20.487 | 0.122 | 484.103 | 1.852 | 81.077 | | |
| 12/9/2008 | 12:38:56 | 20.517 | 0.03 | 455.385 | 0.024 | 90.313 | | |
| 12/9/2008 | 12:39:06 | 20.624 | 0.03 | 453.59 | 0.024 | 109.011 | | |
| 12/9/2008 | 12:39:16 | 20.761 | 0.03 | 431.795 | 0.024 | 113.629 | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 % | CO2 % | RTO Inlet | | | Baghouse | Calibration Comments | Error % |
|-----------|----------|--------|-------|---|---|---|----------|----------------------|---------|
| | | | | VOC 3 ppm C ₂ H ₆ | VOC 1 ppm C ₂ H ₆ | VOC 2 ppm C ₂ H ₆ | | | |
| 12/9/2008 | 12:39:26 | 20.822 | 0.03 | 429.231 | 0.024 | 111.055 | | | |
| 12/9/2008 | 12:39:36 | 20.883 | 0.03 | 445.641 | 0.024 | 106.437 | | | |
| 12/9/2008 | 12:39:46 | 20.883 | 0.03 | 445.897 | 0.024 | 103.106 | | | |
| 12/9/2008 | 12:39:56 | 20.792 | 0.03 | 473.846 | 0.024 | 86.527 | | | |
| 12/9/2008 | 12:40:06 | 20.685 | 0.091 | 481.538 | 0.024 | 79.033 | | | |
| 12/9/2008 | 12:40:16 | 20.809 | 0.081 | 464.872 | 33.138 | 76.232 | | | |
| 12/9/2008 | 12:40:26 | 20.578 | 0.081 | 441.282 | 5.665 | 73.81 | | | |
| 12/9/2008 | 12:40:36 | 20.809 | 0.03 | 417.949 | 0.879 | 75.475 | | | |
| 12/9/2008 | 12:40:46 | 20.885 | 0.03 | 449.487 | 0.024 | 74.718 | | | |
| 12/9/2008 | 12:40:56 | 20.761 | 0.03 | 486.205 | 0.024 | 73.507 | | | |
| 12/9/2008 | 12:41:06 | 20.837 | 0.03 | 484.672 | 0.024 | 72.371 | | | |
| 12/9/2008 | 12:41:16 | 20.807 | 0.03 | 487.179 | 0.024 | 71.084 | | | |
| 12/9/2008 | 12:41:26 | 20.716 | 0.091 | 498.205 | 0.024 | 71.16 | | | |
| 12/9/2008 | 12:41:36 | 20.594 | 0.305 | 495.841 | 0.024 | 73.507 | | | |
| 12/9/2008 | 12:41:46 | 20.517 | 0.335 | 501.538 | 0.024 | 78.503 | | | |
| 12/9/2008 | 12:41:56 | 20.472 | 0.335 | 510 | 33.187 | 84.408 | | | |
| 12/9/2008 | 12:42:06 | 20.457 | 0.335 | 499.231 | 2.027 | 88.647 | | | |
| 12/9/2008 | 12:42:16 | 20.472 | 0.213 | 496.667 | 0.024 | 91.978 | | | |
| 12/9/2008 | 12:42:26 | 20.594 | 0.152 | 528.41 | 0.024 | 86.906 | | | |
| 12/9/2008 | 12:42:36 | 20.716 | 0.122 | 529.231 | 0.024 | 81.153 | | | |
| 12/9/2008 | 12:42:46 | 20.776 | 0.091 | 512.308 | 0.024 | 78.654 | | | |
| 12/9/2008 | 12:42:56 | 20.853 | 0.091 | 470.256 | 0.024 | 80.093 | | | |
| 12/9/2008 | 12:43:06 | 20.868 | 0.122 | 455.897 | 0.024 | 83.272 | | | |
| 12/9/2008 | 12:43:16 | 20.822 | 0.213 | 453.333 | 0.024 | 92.886 | | | |
| 12/9/2008 | 12:43:26 | 20.716 | 0.244 | 444.359 | 0.024 | 111.206 | | | |
| 12/9/2008 | 12:43:36 | 20.809 | 0.244 | 443.077 | 30.379 | 113.25 | | | |
| 12/9/2008 | 12:43:46 | 20.578 | 0.213 | 430.256 | 4.615 | 110.298 | | | |
| 12/9/2008 | 12:43:56 | 20.809 | 0.122 | 462.308 | 0.024 | 105.302 | | | |
| 12/9/2008 | 12:44:06 | 20.7 | 0.091 | 474.615 | 0.024 | 102.274 | | | |
| 12/9/2008 | 12:44:16 | 20.792 | 0.091 | 502.308 | 0.024 | 85.488 | | | |
| 12/9/2008 | 12:44:26 | 20.837 | 0.091 | 501.795 | 0.024 | 79.184 | | | |
| 12/9/2008 | 12:44:36 | 20.822 | 0.183 | 482.308 | 0.024 | 75.096 | | | |
| 12/9/2008 | 12:44:46 | 20.7 | 0.274 | 476.154 | 0.024 | 73.128 | | | |
| 12/9/2008 | 12:44:56 | 20.578 | 0.305 | 451.026 | 0.024 | 71.941 | | | |
| 12/9/2008 | 12:45:06 | 20.517 | 0.335 | 457.179 | 0.024 | 73.885 | | | |
| 12/9/2008 | 12:45:16 | 20.517 | 0.274 | 459.487 | 31.968 | 75.248 | | | |
| 12/9/2008 | 12:45:26 | 20.502 | 0.274 | 435.128 | 2.54 | 75.096 | | | |
| 12/9/2008 | 12:45:36 | 20.502 | 0.213 | 438.205 | 0.024 | 74.112 | | | |
| 12/9/2008 | 12:45:46 | 20.609 | 0.122 | 442.821 | 0.024 | 73.507 | | | |
| 12/9/2008 | 12:45:56 | 20.731 | 0.061 | 452.821 | 0.024 | 73.204 | | | |
| 12/9/2008 | 12:46:06 | 20.807 | 0.061 | 461.795 | 0.024 | 74.264 | | | |
| 12/9/2008 | 12:46:16 | 20.853 | 0.091 | 469.231 | 0.024 | 75.826 | | | |
| 12/9/2008 | 12:46:26 | 20.868 | 0.183 | 488.718 | 0.024 | 76.913 | | | |
| 12/9/2008 | 12:46:36 | 20.746 | 0.244 | 498.41 | 0.024 | 78.427 | | | |
| 12/9/2008 | 12:46:46 | 20.855 | 0.305 | 510.256 | 0.024 | 78.882 | | | |
| 12/9/2008 | 12:46:56 | 20.533 | 0.305 | 517.18 | 33.626 | 77.897 | | | |
| 12/9/2008 | 12:47:06 | 20.517 | 0.274 | 503.077 | 4.982 | 79.033 | | | |
| 12/9/2008 | 12:47:16 | 20.563 | 0.183 | 553.846 | 0.024 | 84.659 | | | |
| 12/9/2008 | 12:47:26 | 20.716 | 0.091 | 511.538 | 0.024 | 88.95 | | | |
| 12/9/2008 | 12:47:36 | 20.761 | 0.061 | 453.077 | 0.024 | 101.365 | | | |
| 12/9/2008 | 12:47:46 | 20.837 | 0.061 | 408.41 | 0.024 | 115.219 | | | |
| 12/9/2008 | 12:47:56 | 20.853 | 0.122 | 418.718 | 0.024 | 113.477 | | | |
| 12/9/2008 | 12:48:06 | 20.761 | 0.213 | 424.815 | 0.024 | 107.421 | | | |
| 12/9/2008 | 12:48:16 | 20.639 | 0.274 | 422.564 | 0.024 | 106.437 | | | |
| 12/9/2008 | 12:48:26 | 20.548 | 0.274 | 410.513 | 0.024 | 108.88 | | | |
| 12/9/2008 | 12:48:36 | 20.502 | 0.274 | 426.41 | 30.281 | 109.314 | | | |
| 12/9/2008 | 12:48:46 | 20.502 | 0.274 | 427.948 | 2.296 | 113.096 | | | |
| 12/9/2008 | 12:48:56 | 20.472 | 0.213 | 445.385 | 0.024 | 105.756 | | | |
| 12/9/2008 | 12:49:06 | 20.563 | 0.152 | 491.026 | 0.024 | 91.372 | | | |
| 12/9/2008 | 12:49:16 | 20.7 | 0.091 | 459.487 | 0.024 | 85.392 | | | |
| 12/9/2008 | 12:49:26 | 20.807 | 0.061 | 428.462 | 0.024 | 81.228 | | | |
| 12/9/2008 | 12:49:36 | 20.868 | 0.061 | 439.231 | 0.024 | 78.838 | | | |
| 12/9/2008 | 12:49:46 | 20.883 | 0.122 | 417.179 | 0.024 | 77.822 | | | |
| 12/9/2008 | 12:49:56 | 20.761 | 0.213 | 431.282 | 0.024 | 76.383 | | | |
| 12/9/2008 | 12:50:06 | 20.639 | 0.274 | 474.815 | 0.024 | 74.491 | | | |
| 12/9/2008 | 12:50:16 | 20.533 | 0.335 | 496.867 | 32.259 | 74.567 | | | |
| 12/9/2008 | 12:50:26 | 20.457 | 0.426 | 494.359 | 4.762 | 74.415 | | | |
| 12/9/2008 | 12:50:36 | 20.563 | 0.152 | 454.359 | 0.708 | 76.838 | | | |
| 12/9/2008 | 12:50:46 | 20.685 | 0.091 | 452.821 | 0.024 | 75.399 | | | |
| 12/9/2008 | 12:50:56 | 20.746 | 0.091 | 511.538 | 0.024 | 73.81 | | | |
| 12/9/2008 | 12:51:06 | 20.822 | 0.091 | 495.385 | 0.024 | 77.746 | | | |
| 12/9/2008 | 12:51:16 | 20.837 | 0.122 | 473.846 | 0.024 | 84.559 | | | |
| 12/9/2008 | 12:51:26 | 20.776 | 0.213 | 453.59 | 0.024 | 89.101 | | | |
| 12/9/2008 | 12:51:36 | 20.824 | 0.305 | 527.849 | 0.024 | 91.751 | | | |
| 12/9/2008 | 12:51:46 | 20.502 | 0.335 | 533.077 | 0.024 | 89.253 | | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|----------|--------|--------|--|--|--|-------------------------|------------|
| | | % | % | VOC 3 ppm C ₆ H ₆ | VOC 1 ppm C ₆ H ₆ | VOC 2 ppm C ₆ H ₆ | | |
| 12/9/2008 | 12:51:56 | 20.472 | 0.305 | 498.974 | 35.653 | 87.587 | | |
| 12/9/2008 | 12:52:06 | 20.457 | 0.274 | 432.051 | 3.004 | 82.894 | | |
| 12/9/2008 | 12:52:16 | 20.517 | 0.152 | 452.308 | 0.024 | 81.001 | | |
| 12/9/2008 | 12:52:26 | 20.594 | 0.122 | 499.231 | 0.024 | 84.558 | | |
| 12/9/2008 | 12:52:36 | 20.716 | 0.122 | 486.887 | 0.024 | 104.393 | | |
| 12/9/2008 | 12:52:46 | 20.822 | 0.061 | 434.359 | 0.024 | 112.19 | | |
| 12/9/2008 | 12:52:56 | 20.883 | 0.061 | 432.051 | 0.024 | 112.872 | | |
| 12/9/2008 | 12:53:06 | 20.853 | 0.152 | 480.769 | 0.024 | 111.206 | | |
| 12/9/2008 | 12:53:16 | 20.746 | 0.244 | 483.59 | 0.024 | 108.764 | | |
| 12/9/2008 | 12:53:26 | 20.824 | 0.426 | 476.41 | 0.024 | 92.281 | | |
| 12/9/2008 | 12:53:36 | 20.578 | 0.426 | 469.231 | 37.485 | 83.045 | | |
| 12/9/2008 | 12:53:46 | 20.517 | 0.396 | 457.436 | 6.252 | 78.276 | | |
| 12/9/2008 | 12:53:56 | 20.563 | 0.305 | 480.769 | 0.488 | 74.112 | | |
| 12/9/2008 | 12:54:06 | 20.655 | 0.244 | 452.308 | 0.024 | 74.567 | | |
| 12/9/2008 | 12:54:16 | 20.761 | 0.244 | 456.887 | 0.024 | 74.339 | | |
| 12/9/2008 | 12:54:26 | 20.868 | 0.244 | 483.846 | 0.024 | 75.853 | | |
| 12/9/2008 | 12:54:36 | 20.837 | 0.305 | 484.615 | 0.024 | 76.838 | | |
| 12/9/2008 | 12:54:46 | 20.761 | 0.396 | 473.846 | 0.024 | 76.232 | | |
| 12/9/2008 | 12:54:56 | 20.809 | 0.426 | 456.841 | 0.024 | 76.459 | | |
| 12/9/2008 | 12:55:06 | 20.533 | 0.426 | 435.128 | 0.024 | 78.579 | | |
| 12/9/2008 | 12:55:16 | 20.472 | 0.426 | 476.897 | 35.238 | 84.786 | | |
| 12/9/2008 | 12:55:26 | 20.457 | 0.426 | 493.077 | 2.93 | 90.842 | | |
| 12/9/2008 | 12:55:36 | 20.457 | 0.213 | 471.026 | 0.024 | 95.158 | | |
| 12/9/2008 | 12:55:46 | 20.563 | 0.152 | 497.179 | 0.024 | 93.416 | | |
| 12/9/2008 | 12:55:56 | 20.685 | 0.122 | 532.051 | 0.024 | 90.464 | | |
| 12/9/2008 | 12:56:06 | 20.792 | 0.091 | 547.18 | 0.024 | 85.695 | | |
| 12/9/2008 | 12:56:16 | 20.868 | 0.061 | 522.308 | 0.024 | 84.029 | | |
| 12/9/2008 | 12:56:26 | 20.883 | 0.122 | 486.718 | 0.024 | 85.392 | | |
| 12/9/2008 | 12:56:36 | 20.807 | 0.183 | 456.923 | 0.024 | 87.966 | | |
| 12/9/2008 | 12:56:46 | 20.685 | 0.244 | 446.887 | 0.024 | 95.309 | | |
| 12/9/2008 | 12:56:56 | 20.624 | 0.274 | 455.385 | 34.579 | 114.613 | | |
| 12/9/2008 | 12:57:06 | 20.533 | 0.244 | 472.051 | 5.275 | 117.944 | | |
| 12/9/2008 | 12:57:16 | 20.578 | 0.213 | 458.718 | 0.464 | 114.991 | | |
| 12/9/2008 | 12:57:26 | 19.741 | 2.378 | 492.564 | 0.024 | 109.011 | | |
| 12/9/2008 | 12:57:36 | 15.141 | 6.276 | 484.359 | 0.024 | 108.33 | | |
| 12/9/2008 | 12:57:46 | 8.987 | 8.225 | 493.333 | 0.024 | 91.675 | | |
| 12/9/2008 | 12:57:56 | 4.509 | 9.292 | 494.103 | 0.024 | 82.137 | | |
| 12/9/2008 | 12:58:06 | 1.813 | 9.688 | 474.615 | 0.024 | 78.2 | | |
| 12/9/2008 | 12:58:16 | 0.305 | 9.901 | 421.538 | 0.024 | 75.702 | | |
| 12/9/2008 | 12:58:26 | 0.015 | 10.023 | 394.103 | 0.024 | 78.427 | | |
| 12/9/2008 | 12:58:36 | 0.015 | 10.084 | 383.333 | 32.161 | 78.806 | | |
| 12/9/2008 | 12:58:46 | 0.015 | 10.084 | 411.282 | 2.466 | 78.427 | | |
| 12/9/2008 | 12:58:56 | 0.015 | 9.992 | 421.538 | 0.024 | 78.427 | | |
| 12/9/2008 | 12:59:06 | 0.015 | 10.023 | 433.59 | 0.024 | 77.973 | | |
| 12/9/2008 | 12:59:16 | 0.015 | 10.023 | 444.872 | 0.024 | 78.503 | Mid range drift check | 0.00% |
| 12/9/2008 | 12:59:26 | 0.015 | 10.023 | 403.846 | 0.024 | 80.471 | Zero drift check | 0.00% |
| 12/9/2008 | 12:59:36 | 0.015 | 9.992 | 423.077 | 0.024 | 83.272 | | |
| 12/9/2008 | 12:59:46 | 0.015 | 8.073 | 423.846 | 0.024 | 87.057 | | |
| 12/9/2008 | 12:59:56 | 1.995 | 5.209 | 455.128 | 0.024 | 89.707 | | |
| 12/9/2008 | 13:00:06 | 7.464 | 2.681 | 451.795 | 0.024 | 93.038 | | |
| 12/9/2008 | 13:00:16 | 12.399 | 1.158 | 459.487 | 35.971 | 93.341 | | |
| 12/9/2008 | 13:00:26 | 15.994 | 0.487 | 417.436 | 6.74 | 87.986 | | |
| 12/9/2008 | 13:00:36 | 18.248 | 0.091 | 420.769 | 1.294 | 84.938 | | |
| 12/9/2008 | 13:00:46 | 19.588 | 0.03 | 435.897 | 0.024 | 83.802 | | |
| 12/9/2008 | 13:00:56 | 20.335 | 0.03 | 441.795 | 0.024 | 86.225 | | |
| 12/9/2008 | 13:01:06 | 20.731 | 0.03 | 431.795 | 0.024 | 93.795 | | |
| 12/9/2008 | 13:01:16 | 20.944 | 0.03 | 426.154 | 0.024 | 113.25 | | |
| 12/9/2008 | 13:01:26 | 20.883 | 0.03 | 401.026 | 0.024 | 116.808 | | |
| 12/9/2008 | 13:01:36 | 20.944 | 0.03 | 382.821 | 0.024 | 112.569 | | |
| 12/9/2008 | 13:01:46 | 20.914 | 0.03 | 384.872 | 0.024 | 109.389 | | |
| 12/9/2008 | 13:01:56 | 20.914 | 0.03 | 381.026 | 31.355 | 108.405 | | |
| 12/9/2008 | 13:02:06 | 20.888 | 0.03 | 416.41 | 2.637 | 92.735 | | |
| 12/9/2008 | 13:02:16 | 20.896 | 0.03 | 430 | 0.024 | 83.651 | | |
| 12/9/2008 | 13:02:26 | 20.868 | 0.03 | 413.58 | 0.024 | 81.228 | | |
| 12/9/2008 | 13:02:36 | 20.883 | 0.03 | 422.821 | 0.024 | 78.2 | | |
| 12/9/2008 | 13:02:46 | 20.883 | 0.03 | 385.128 | 0.024 | 78.806 | | |
| 12/9/2008 | 13:02:56 | 20.822 | 0.03 | 376.867 | 0.024 | 78.503 | | |
| 12/9/2008 | 13:03:06 | 20.748 | 0.081 | 394.359 | 5.008 | 78.125 | | |
| 12/9/2008 | 13:03:16 | 20.578 | 0.152 | 403.846 | 28.303 | 76.838 | | |
| 12/9/2008 | 13:03:26 | 20.426 | 0.244 | 408.462 | 34.872 | 76.611 | | |
| 12/9/2008 | 13:03:36 | 20.289 | 0.244 | 420.256 | 36.484 | 76.913 | | |
| 12/9/2008 | 13:03:46 | 20.243 | 0.244 | 424.615 | 36.947 | 79.184 | | |
| 12/9/2008 | 13:03:56 | 20.269 | 0.213 | 442.821 | 29.846 | 83.854 | | |
| 12/9/2008 | 13:04:06 | 20.365 | 0.152 | 437.892 | 25.69 | 88.95 | | |
| 12/9/2008 | 13:04:16 | 20.441 | 0.122 | 444.872 | 24.2 | 93.285 | | |
| | | | | | | | Hi range drift check | 0.00% |
| | | | | | | | Zero drift check | 0.00% |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|----------|--------|-------|-----------------------------------|-----------------------------------|-----------------------------------|---|------------|
| | | % | % | ppm C ₂ H ₆ | ppm C ₂ H ₆ | ppm C ₂ H ₆ | | |
| 12/9/2008 | 13:04:26 | 20.502 | 0.122 | 423.59 | 23.297 | 98.444 | | |
| 12/9/2008 | 13:04:36 | 20.533 | 0.152 | 453.333 | 24.713 | 93.265 | | |
| 12/9/2008 | 13:04:46 | 20.441 | 0.274 | 451.785 | 25.275 | 87.814 | | |
| 12/9/2008 | 13:04:56 | 20.319 | 0.305 | 443.077 | 25.397 | 84.862 | | |
| 12/9/2008 | 13:05:06 | 20.213 | 0.335 | 434.103 | 26.201 | 84.635 | Post-test low range calibration drift check | |
| 12/9/2008 | 13:05:16 | 20.152 | 0.335 | 425.128 | 25.89 | 87.89 | 0.18% | |
| 12/9/2008 | 13:05:26 | 20.137 | 0.335 | 437.949 | 39.634 | 95.385 | | |
| 12/9/2008 | 13:05:36 | 20.152 | 0.213 | 427.949 | 0.024 | 114.31 | | |
| 12/9/2008 | 13:05:46 | 20.259 | 0.152 | 417.692 | 0.024 | 118.928 | | |
| 12/9/2008 | 13:05:56 | 20.398 | 0.091 | 393.333 | 0.024 | 116.733 | | |
| 12/9/2008 | 13:06:06 | 20.487 | 0.081 | 398.718 | 0.024 | 112.115 | Post-test zero calibration drift check | |
| 12/9/2008 | 13:06:16 | 20.548 | 0.061 | 397.692 | 0.024 | 112.115 | 0.00% | |
| 12/9/2008 | 13:06:26 | 20.548 | 0.152 | 416.667 | 0.024 | 94.93 | | |
| 12/9/2008 | 13:06:36 | 20.487 | 0.244 | 438.462 | 0.024 | 85.846 | | |
| 12/9/2008 | 13:06:46 | 20.365 | 0.274 | 423.846 | 1.294 | 81.077 | | |
| 12/9/2008 | 13:06:56 | 20.259 | 0.274 | 427.179 | 28.376 | 78.854 | | |
| 12/9/2008 | 13:07:06 | 20.198 | 0.244 | 398.718 | 5.275 | 76.005 | | |
| 12/9/2008 | 13:07:16 | 20.213 | 0.152 | 396.923 | 0.977 | 76.535 | | |
| 12/9/2008 | 13:07:26 | 20.35 | 0.122 | 404.872 | 0.024 | 79.033 | | |
| 12/9/2008 | 13:07:36 | 20.441 | 0.091 | 409.744 | 0.024 | 80.623 | | |
| 12/9/2008 | 13:07:46 | 20.548 | 0.091 | 413.846 | 0.024 | 80.774 | | |
| 12/9/2008 | 13:07:56 | 20.517 | 0.183 | 439.744 | 0.024 | 80.85 | | |
| 12/9/2008 | 13:08:06 | 20.441 | 0.274 | 439.231 | 0.024 | 82.908 | | |
| 12/9/2008 | 13:08:16 | 20.304 | 0.305 | 457.949 | 0.024 | 29.978 | | |
| 12/9/2008 | 13:08:26 | 20.213 | 0.335 | 452.821 | 0.024 | 23.619 | | |
| 12/9/2008 | 13:08:36 | 20.152 | 0.335 | 446.923 | 33.431 | 20.687 | | |
| 12/9/2008 | 13:08:46 | 20.137 | 0.335 | 421.795 | 2.979 | 19.077 | | |
| 12/9/2008 | 13:08:56 | 20.167 | 0.213 | 453.59 | 0.073 | 17.866 | | |
| 12/9/2008 | 13:09:06 | 20.304 | 0.152 | 448.974 | 0.024 | 16.957 | | |
| 12/9/2008 | 13:09:16 | 20.396 | 0.091 | 439.231 | 0.024 | 16.352 | | |
| 12/9/2008 | 13:09:26 | 20.487 | 0.091 | 404.103 | 0.024 | 15.519 | | |
| 12/9/2008 | 13:09:36 | 20.533 | 0.091 | 400.513 | 0.024 | 14.838 | | |
| 12/9/2008 | 13:09:46 | 20.563 | 0.091 | 407.436 | 0.024 | 14.308 | | |
| 12/9/2008 | 13:09:56 | 20.517 | 0.213 | 415.128 | 0.024 | 14.005 | | |
| 12/9/2008 | 13:10:06 | 20.38 | 0.244 | 407.179 | 0.024 | 13.853 | | |
| 12/9/2008 | 13:10:16 | 20.289 | 0.244 | 395.128 | 28.4 | 13.702 | | |
| 12/9/2008 | 13:10:26 | 20.243 | 0.244 | 415.641 | 4.542 | 13.324 | | |
| 12/9/2008 | 13:10:36 | 20.274 | 0.183 | 407.949 | 0.928 | 13.778 | | |
| 12/9/2008 | 13:10:46 | 20.335 | 0.122 | 422.051 | 0.024 | 13.096 | | |
| 12/9/2008 | 13:10:56 | 20.457 | 0.091 | 427.436 | 0.024 | 12.889 | | |
| 12/9/2008 | 13:11:06 | 20.517 | 0.091 | 423.077 | 0.024 | 13.324 | | |
| 12/9/2008 | 13:11:16 | 20.517 | 0.152 | 412.821 | 0.024 | 12.718 | | |
| 12/9/2008 | 13:11:26 | 20.411 | 0.244 | 385.385 | 0.024 | 12.339 | | |
| 12/9/2008 | 13:11:36 | 20.304 | 0.274 | 387.949 | 0.024 | 12.399 | | |
| 12/9/2008 | 13:11:46 | 20.213 | 0.305 | 417.436 | 0.024 | 11.885 | | |
| 12/9/2008 | 13:11:56 | 20.167 | 0.335 | 443.077 | 29.451 | 11.658 | | |
| 12/9/2008 | 13:12:06 | 20.152 | 0.457 | 451.028 | 2.173 | 11.431 | | |
| 12/9/2008 | 13:12:16 | 20.152 | 0.396 | 448.974 | 0.024 | 11.28 | | |
| 12/9/2008 | 13:12:26 | 20.289 | 0.305 | 446.867 | 0.024 | 11.28 | | |
| 12/9/2008 | 13:12:36 | 20.396 | 0.274 | 458.718 | 0.024 | 11.885 | | |
| 12/9/2008 | 13:12:46 | 20.502 | 0.274 | 460.513 | 0.024 | 11.507 | | |
| 12/9/2008 | 13:12:56 | 20.533 | 0.274 | 445.897 | 0.024 | 11.886 | | |
| 12/9/2008 | 13:13:06 | 20.563 | 0.274 | 436.154 | 0.024 | 11.81 | | |
| 12/9/2008 | 13:13:16 | 20.487 | 0.306 | 463.077 | 0.024 | 11.81 | | |
| 12/9/2008 | 13:13:26 | 20.38 | 0.426 | 450.513 | 0.024 | 11.961 | | |
| 12/9/2008 | 13:13:36 | 20.259 | 0.426 | 426.41 | 33.187 | 11.81 | | |
| 12/9/2008 | 13:13:46 | 20.213 | 0.398 | 390 | 6.154 | 12.112 | | |
| 12/9/2008 | 13:13:56 | 20.243 | 0.305 | 398.718 | 1.368 | 11.355 | | |
| 12/9/2008 | 13:14:06 | 20.385 | 0.244 | 413.077 | 0.024 | 11.582 | | |
| 12/9/2008 | 13:14:16 | 20.457 | 0.213 | 406.154 | 0.024 | 11.204 | | |
| 12/9/2008 | 13:14:26 | 20.533 | 0.244 | 397.179 | 0.024 | 10.977 | | |
| 12/9/2008 | 13:14:36 | 20.533 | 0.305 | 404.872 | 0.024 | 10.75 | | |
| 12/9/2008 | 13:14:46 | 20.441 | 0.398 | 429.487 | 0.024 | 10.623 | | |
| 12/9/2008 | 13:14:56 | 20.319 | 0.457 | 422.051 | 0.024 | 10.977 | | |
| 12/9/2008 | 13:15:06 | 20.213 | 0.457 | 439.231 | 0.024 | 10.901 | | |
| 12/9/2008 | 13:15:16 | 20.152 | 0.457 | 445.128 | 32.503 | 10.523 | | |
| 12/9/2008 | 13:15:26 | 20.137 | 0.457 | 419.487 | 2.808 | 10.76 | | |
| 12/9/2008 | 13:15:36 | 20.152 | 0.368 | 437.892 | 0.024 | 10.447 | | |
| 12/9/2008 | 13:15:46 | 20.259 | 0.305 | 412.308 | 0.024 | 10.295 | | |
| 12/9/2008 | 13:15:56 | 20.411 | 0.244 | 406.923 | 0.024 | 10.447 | | |
| 12/9/2008 | 13:16:06 | 20.487 | 0.213 | 429.744 | 0.024 | 10.22 | | |
| 12/9/2008 | 13:16:16 | 20.533 | 0.213 | 401.538 | 0.024 | 11.431 | | |
| 12/9/2008 | 13:16:26 | 20.563 | 0.305 | 411.282 | 0.024 | 11.431 | | |
| 12/9/2008 | 13:16:36 | 20.472 | 0.398 | 448.462 | 0.024 | 9.917 | | |
| 12/9/2008 | 13:16:46 | 20.335 | 0.426 | 431.026 | 0.024 | 10.144 | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|----------|--------|-------|-----------------------------------|-----------------------------------|-----------------------------------|-------------------------|------------|
| | | % | % | ppm C ₆ H ₆ | ppm C ₆ H ₆ | ppm C ₆ H ₆ | | |
| 12/9/2008 | 13:16:56 | 20.250 | 0.274 | 415.128 | 31.136 | 11.658 | | |
| 12/9/2008 | 13:17:06 | 20.213 | 0.274 | 441.795 | 5.47 | 11.355 | | |
| 12/9/2008 | 13:17:16 | 20.213 | 0.213 | 460.513 | 0.611 | 9.841 | | |
| 12/9/2008 | 13:17:26 | 20.274 | 0.122 | 411.538 | 0.024 | 10.901 | | |
| 12/9/2008 | 13:17:36 | 20.428 | 0.091 | 448.41 | 0.024 | 11.807 | | |
| 12/9/2008 | 13:17:46 | 20.517 | 0.091 | 464.872 | 0.024 | 10.144 | | |
| 12/9/2008 | 13:17:56 | 20.517 | 0.152 | 454.359 | 0.024 | 10.22 | | |
| 12/9/2008 | 13:18:06 | 20.472 | 0.244 | 426.923 | 0.024 | 9.917 | | |
| 12/9/2008 | 13:18:16 | 20.35 | 0.274 | 412.821 | 0.024 | 10.144 | | |
| 12/9/2008 | 13:18:26 | 20.243 | 0.305 | 421.795 | 0.024 | 10.523 | | |
| 12/9/2008 | 13:18:36 | 20.167 | 0.274 | 417.179 | 31.648 | 10.22 | | |
| 12/9/2008 | 13:18:46 | 20.152 | 0.305 | 419.487 | 2.515 | 9.993 | | |
| 12/9/2008 | 13:18:56 | 20.152 | 0.213 | 431.538 | 0.024 | 9.69 | | |
| 12/9/2008 | 13:19:06 | 20.304 | 0.152 | 428.154 | 0.024 | 10.22 | | |
| 12/9/2008 | 13:19:16 | 20.411 | 0.091 | 409.487 | 0.024 | 11.28 | | |
| 12/9/2008 | 13:19:26 | 20.517 | 0.061 | 411.026 | 0.024 | 11.507 | | |
| 12/9/2008 | 13:19:36 | 20.533 | 0.061 | 424.103 | 0.024 | 10.75 | | |
| 12/9/2008 | 13:19:46 | 20.578 | 0.152 | 436.923 | 0.024 | 9.69 | | |
| 12/9/2008 | 13:19:56 | 20.457 | 0.244 | 432.308 | 0.024 | 9.69 | | |
| 12/9/2008 | 13:20:06 | 20.365 | 0.274 | 374.615 | 0.244 | 11.658 | | |
| 12/9/2008 | 13:20:16 | 20.274 | 0.274 | 376.154 | 28.593 | 11.204 | | |
| 12/9/2008 | 13:20:26 | 20.213 | 0.244 | 422.308 | 4.664 | 9.841 | | |
| 12/9/2008 | 13:20:36 | 20.259 | 0.183 | 444.872 | 0.537 | 9.463 | | |
| 12/9/2008 | 13:20:46 | 20.35 | 0.122 | 404.872 | 0.024 | 10.674 | | |
| 12/9/2008 | 13:20:56 | 20.457 | 0.061 | 414.615 | 0.024 | 10.068 | | |
| 12/9/2008 | 13:21:06 | 20.533 | 0.091 | 431.282 | 0.024 | 10.523 | | |
| 12/9/2008 | 13:21:16 | 20.533 | 0.183 | 438.974 | 0.024 | 10.977 | | |
| 12/9/2008 | 13:21:26 | 20.441 | 0.244 | 81.538 | 0.024 | 10.598 | | |
| 12/9/2008 | 13:21:36 | 20.319 | 0.274 | 31.538 | 0.024 | 10.295 | | |
| 12/9/2008 | 13:21:46 | 20.228 | 0.274 | 20.769 | 0.024 | 9.993 | | |
| 12/9/2008 | 13:21:56 | 20.167 | 0.274 | 22.564 | 26.984 | 10.523 | | |
| 12/9/2008 | 13:22:06 | 20.137 | 0.335 | 19.231 | 2.589 | 10.901 | | |
| 12/9/2008 | 13:22:16 | 20.152 | 0.244 | 19.231 | 0.024 | 15.368 | | |
| 12/9/2008 | 13:22:26 | 20.304 | 0.152 | 13.846 | 0.024 | 62.984 | | |
| 12/9/2008 | 13:22:36 | 20.396 | 0.122 | 12.051 | 0.024 | 74.264 | | |
| 12/9/2008 | 13:22:46 | 20.487 | 0.091 | 10.513 | 0.024 | 85.013 | | |
| 12/9/2008 | 13:22:56 | 20.533 | 0.091 | 8.154 | 0.024 | 106.589 | | |
| 12/9/2008 | 13:23:06 | 20.548 | 0.122 | 5.641 | 0.024 | 114.083 | | |
| 12/9/2008 | 13:23:16 | 20.457 | 0.183 | 6.41 | 0.024 | 115.9 | | |
| 12/9/2008 | 13:23:26 | 20.35 | 0.244 | 7.682 | 0.073 | 53.143 | | |
| 12/9/2008 | 13:23:36 | 20.259 | 0.274 | 5.385 | 27.937 | 33.082 | | |
| 12/9/2008 | 13:23:46 | 20.213 | 0.244 | 5.385 | 5.031 | 22.559 | | |
| 12/9/2008 | 13:23:56 | 20.243 | 0.152 | 8.205 | 0.904 | 18.32 | | |
| 12/9/2008 | 13:24:06 | 20.35 | 0.091 | 8.205 | 0.024 | 16.654 | | |
| 12/9/2008 | 13:24:16 | 20.457 | 0.091 | 8.923 | 0.024 | 16.579 | | |
| 12/9/2008 | 13:24:26 | 20.517 | 0.061 | 5.385 | 0.024 | 17.714 | | |
| 12/9/2008 | 13:24:36 | 20.517 | 0.122 | 6.667 | 0.024 | 18.547 | | |
| 12/9/2008 | 13:24:46 | 20.441 | 0.213 | 7.436 | 0.024 | 27.707 | | |
| 12/9/2008 | 13:24:56 | 20.335 | 0.274 | 6.154 | 0.024 | 26.042 | | |
| 12/9/2008 | 13:25:06 | 20.213 | 0.306 | 6.923 | 0.024 | 20.515 | | |
| 12/9/2008 | 13:25:16 | 20.167 | 0.274 | 6.154 | 29.597 | 21.499 | | |
| 12/9/2008 | 13:25:26 | 20.152 | 0.305 | 7.179 | 2.735 | 19.304 | | |
| 12/9/2008 | 13:25:36 | 20.152 | 0.213 | 6.923 | 0.024 | 15.67 | | |
| 12/9/2008 | 13:25:46 | 20.274 | 0.152 | 7.438 | 0.024 | 15.14 | | |
| 12/9/2008 | 13:25:56 | 20.396 | 0.091 | 7.179 | 0.024 | 13.702 | | |
| 12/9/2008 | 13:26:06 | 20.487 | 0.091 | 8.482 | 0.024 | 14.232 | | |
| 12/9/2008 | 13:26:16 | 20.533 | 0.091 | 7.949 | 0.024 | 14.989 | | |
| 12/9/2008 | 13:26:26 | 20.533 | 0.152 | 6.667 | 0.024 | 18.898 | | |
| 12/9/2008 | 13:26:36 | 20.472 | 0.244 | 6.667 | 0.024 | 20.591 | | |
| 12/9/2008 | 13:26:46 | 20.365 | 0.274 | 4.615 | 28.107 | 15.595 | | |
| 12/9/2008 | 13:26:56 | 20.274 | 0.305 | 5.128 | 21.074 | 14.061 | | |
| 12/9/2008 | 13:27:06 | 20.198 | 0.244 | 2.821 | 4.542 | 14.969 | | |
| 12/9/2008 | 13:27:16 | 20.274 | 0.183 | 1.538 | 0.855 | 19.607 | | |
| 12/9/2008 | 13:27:26 | 20.365 | 0.122 | 0.513 | 0.024 | 18.398 | | |
| 12/9/2008 | 13:27:36 | 20.472 | 0.091 | 1.026 | 0.024 | 18.503 | | |
| 12/9/2008 | 13:27:46 | 20.517 | 0.091 | 3.333 | 0.024 | 15.595 | | |
| 12/9/2008 | 13:27:56 | 20.548 | 0.122 | 3.077 | 0.024 | 27.404 | | |
| 12/9/2008 | 13:28:06 | 20.441 | 0.244 | 4.615 | 0.024 | 24.452 | | |
| 12/9/2008 | 13:28:16 | 20.335 | 0.305 | 10.256 | 0.024 | 17.714 | | |
| 12/9/2008 | 13:28:26 | 20.213 | 0.366 | 18.462 | 20.293 | 13.778 | | |
| 12/9/2008 | 13:28:36 | 20.182 | 0.305 | 3.846 | 18.755 | 13.778 | | |
| 12/9/2008 | 13:28:46 | 20.152 | 0.305 | 0.513 | 2.271 | 13.172 | | |
| 12/9/2008 | 13:28:56 | 20.182 | 0.213 | 0.256 | 0.024 | 13.248 | | |
| 12/9/2008 | 13:29:06 | 20.259 | 0.122 | 0.256 | 0.024 | 13.172 | | |
| 12/9/2008 | 13:29:16 | 20.411 | 0.091 | 0.256 | 0.024 | 12.491 | | |

Post-test zero calibration drift check 0.00%

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|----------|--------|-------|--|--|--|---|------------|
| | | % | % | VOC 3 ppm C ₂ H ₆ | VOC 1 ppm C ₂ H ₆ | VOC 2 ppm C ₂ H ₆ | | |
| 12/9/2008 | 13:29:26 | 20.517 | 0.081 | 1.026 | 0.024 | 13.172 | | |
| 12/9/2008 | 13:29:36 | 20.548 | 0.091 | 6.41 | 0.024 | 14.005 | | |
| 12/9/2008 | 13:29:46 | 20.563 | 0.122 | 7.849 | 0.024 | 13.929 | | |
| 12/9/2008 | 13:29:56 | 20.487 | 0.213 | 456.41 | 0.024 | 12.037 | | |
| 12/9/2008 | 13:30:06 | 20.365 | 0.274 | 491.026 | 33.968 | 14.005 | | |
| 12/9/2008 | 13:30:16 | 20.304 | 0.305 | 494.103 | 22.589 | 15.519 | | |
| 12/9/2008 | 13:30:26 | 20.213 | 0.274 | 503.846 | 4.298 | 12.945 | Post-test mid range calibration drift check | 0.32% |
| 12/9/2008 | 13:30:36 | 20.274 | 0.183 | 493.077 | 0.879 | 12.491 | | |
| 12/9/2008 | 13:30:46 | 20.335 | 0.122 | 495.128 | 0.024 | 12.339 | | |
| 12/9/2008 | 13:30:56 | 20.441 | 0.081 | 493.846 | 0.024 | 14.232 | | |
| 12/9/2008 | 13:31:06 | 20.517 | 0.091 | 495.897 | 0.024 | 15.218 | | |
| 12/9/2008 | 13:31:16 | 20.533 | 0.152 | 379.487 | 0.024 | 12.889 | | |
| 12/9/2008 | 13:31:26 | 20.457 | 0.244 | 449.231 | 0.024 | 11.885 | | |
| 12/9/2008 | 13:31:36 | 20.304 | 0.274 | 461.026 | 0.024 | 11.734 | | |
| 12/9/2008 | 13:31:46 | 20.228 | 0.305 | 448.205 | 20.586 | 11.734 | | |
| 12/9/2008 | 13:31:56 | 20.167 | 0.274 | 442.821 | 17.285 | 13.172 | | |
| 12/9/2008 | 13:32:06 | 20.152 | 0.305 | 456.41 | 1.734 | 12.794 | | |
| 12/9/2008 | 13:32:16 | 20.182 | 0.213 | 453.846 | 0.024 | 17.941 | | |
| 12/9/2008 | 13:32:26 | 20.304 | 0.122 | 474.872 | 0.024 | 24.803 | | |
| 12/9/2008 | 13:32:36 | 20.396 | 0.091 | 478.462 | 0.024 | 82.227 | | |
| 12/9/2008 | 13:32:46 | 20.472 | 0.061 | 481.026 | 0.024 | 18.244 | | |
| 12/9/2008 | 13:32:56 | 20.563 | 0.03 | 446.718 | 0.024 | 13.626 | | |
| 12/9/2008 | 13:33:06 | 20.548 | 0.152 | 399.744 | 0.024 | 11.734 | | |
| 12/9/2008 | 13:33:16 | 20.502 | 0.368 | 397.692 | 0.024 | 11.128 | | |
| 12/9/2008 | 13:33:26 | 20.38 | 0.457 | 448.718 | 34.798 | 10.068 | | |
| 12/9/2008 | 13:33:36 | 20.243 | 0.426 | 432.564 | 23.004 | 10.068 | | |
| 12/9/2008 | 13:33:46 | 20.198 | 0.398 | 411.538 | 4.444 | 10.674 | | |
| 12/9/2008 | 13:33:56 | 20.259 | 0.305 | 403.59 | 0.835 | 11.431 | | |
| 12/9/2008 | 13:34:06 | 20.335 | 0.244 | 389.487 | 0.024 | 11.431 | | |
| 12/9/2008 | 13:34:16 | 20.457 | 0.244 | 422.308 | 0.024 | 11.063 | | |
| 12/9/2008 | 13:34:26 | 20.533 | 0.274 | 467.179 | 0.024 | 9.841 | | |
| 12/9/2008 | 13:34:36 | 20.548 | 0.335 | 458.462 | 0.024 | 10.371 | | |
| 12/9/2008 | 13:34:46 | 20.441 | 0.398 | 486.154 | 0.024 | 10.144 | | |
| 12/9/2008 | 13:34:56 | 20.319 | 0.457 | 447.179 | 0.024 | 9.614 | | |
| 12/9/2008 | 13:35:06 | 20.213 | 0.457 | 440.789 | 22.564 | 10.295 | | |
| 12/9/2008 | 13:35:16 | 20.198 | 0.457 | 480.513 | 19.56 | 10.371 | | |
| 12/9/2008 | 13:35:26 | 20.167 | 0.457 | 447.179 | 2.222 | 10.523 | | |
| 12/9/2008 | 13:35:36 | 20.167 | 0.368 | 415.841 | 0.024 | 10.598 | | |
| 12/9/2008 | 13:35:46 | 20.274 | 0.274 | 392.308 | 0.024 | 10.598 | | |
| 12/9/2008 | 13:35:56 | 20.396 | 0.244 | 393.077 | 0.024 | 10.447 | | |
| 12/9/2008 | 13:36:06 | 20.502 | 0.183 | 390.769 | 0.024 | 11.053 | | |
| 12/9/2008 | 13:36:16 | 20.517 | 0.213 | 400.769 | 0.024 | 10.371 | | |
| 12/9/2008 | 13:36:26 | 20.563 | 0.244 | 389.744 | 0.024 | 10.674 | | |
| 12/9/2008 | 13:36:36 | 20.502 | 0.368 | 379.744 | 0.024 | 10.295 | | |
| 12/9/2008 | 13:36:46 | 20.38 | 0.398 | 394.103 | 30.696 | 10.598 | | |
| 12/9/2008 | 13:36:56 | 20.319 | 0.426 | 393.59 | 20.195 | 10.447 | | |
| 12/9/2008 | 13:37:06 | 20.182 | 0.396 | 414.103 | 3.883 | 10.447 | | |
| 12/9/2008 | 13:37:16 | 20.228 | 0.305 | 418.205 | 0.024 | 9.766 | | |
| 12/9/2008 | 13:37:26 | 20.38 | 0.244 | 406.923 | 0.024 | 10.523 | | |
| 12/9/2008 | 13:37:36 | 20.472 | 0.091 | 425.385 | 0.024 | 9.841 | | |
| 12/9/2008 | 13:37:46 | 20.517 | 0.091 | 414.615 | 0.024 | 9.387 | | |
| 12/9/2008 | 13:37:56 | 20.548 | 0.152 | 409.231 | 0.024 | 9.841 | | |
| 12/9/2008 | 13:38:06 | 20.441 | 0.244 | 418.41 | 0.024 | 9.483 | | |
| 12/9/2008 | 13:38:16 | 20.335 | 0.305 | 409.487 | 0.024 | 10.598 | | |
| 12/9/2008 | 13:38:26 | 20.259 | 0.305 | 410 | 20.635 | 11.204 | | |
| 12/9/2008 | 13:38:36 | 20.167 | 0.274 | 398.462 | 18.384 | 11.431 | | |
| 12/9/2008 | 13:38:46 | 20.182 | 0.274 | 380.513 | 2.076 | 10.826 | | |
| 12/9/2008 | 13:38:56 | 20.182 | 0.213 | 427.179 | 0 | 10.447 | | |
| 12/9/2008 | 13:39:06 | 20.274 | 0.152 | 442.821 | 0.024 | 8.781 | | |
| 12/9/2008 | 13:39:16 | 20.411 | 0.122 | 420.513 | 0.024 | 5.375 | | |
| 12/9/2008 | 13:39:26 | 20.517 | 0.081 | 416.887 | 0.024 | 4.921 | | |
| 12/9/2008 | 13:39:36 | 20.563 | 0.061 | 438.974 | 0.024 | 4.996 | | |
| 12/9/2008 | 13:39:46 | 20.563 | 0.122 | 428.718 | 0.024 | 4.769 | | |
| 12/9/2008 | 13:39:56 | 20.472 | 0.213 | 420.258 | 0.024 | 5.299 | | |
| 12/9/2008 | 13:40:06 | 20.35 | 0.274 | 402.821 | 31.38 | 0.076 | | |
| 12/9/2008 | 13:40:16 | 20.274 | 0.305 | 399.231 | 20.757 | 0.076 | | |
| 12/9/2008 | 13:40:26 | 20.228 | 0.274 | 404.103 | 3.98 | 0.076 | | |
| 12/9/2008 | 13:40:36 | 20.243 | 0.152 | 396.41 | 0.415 | 0.076 | | |
| 12/9/2008 | 13:40:46 | 20.335 | 0.091 | 384.359 | 0.024 | 0.076 | | |
| 12/9/2008 | 13:40:56 | 20.457 | 0.061 | 382.821 | 0.024 | 0.076 | | |
| 12/9/2008 | 13:41:06 | 20.563 | 0.061 | 401.538 | 0.024 | 0.076 | | |
| 12/9/2008 | 13:41:16 | 20.548 | 0.122 | 410.513 | 0.024 | 0.076 | | |
| 12/9/2008 | 13:41:26 | 20.457 | 0.213 | 432.051 | 0.024 | 0.076 | | |
| 12/9/2008 | 13:41:36 | 20.289 | 0.274 | 441.795 | 0.024 | 0.076 | | |
| 12/9/2008 | 13:41:46 | 20.213 | 0.335 | 426.923 | 20.904 | 0.076 | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Beghouse | Calibration Comments | Error % |
|-----------|----------|--------|-------|--|--|--|-------------------------|------------|
| | | % | % | VOC 3 ppm C ₂ H ₆ | VOC 1 ppm C ₂ H ₆ | VOC 2 ppm C ₂ H ₆ | | |
| 12/9/2008 | 13:41:56 | 20.152 | 0.335 | 429.487 | 17.187 | 0.076 | | |
| 12/9/2008 | 13:42:06 | 20.152 | 0.335 | 400.513 | 1.343 | 0.076 | | |
| 12/9/2008 | 13:42:16 | 20.182 | 0.213 | 393.846 | 0.024 | 0.076 | | |
| 12/9/2008 | 13:42:26 | 20.289 | 0.152 | 440 | 0.024 | 0.076 | | |
| 12/9/2008 | 13:42:36 | 20.411 | 0.122 | 440.256 | 0.024 | 0.076 | | |
| 12/9/2008 | 13:42:46 | 20.517 | 0.091 | 433.846 | 0.024 | 0.076 | | |
| 12/9/2008 | 13:42:56 | 20.578 | 0.091 | 436.667 | 0.024 | 0.454 | | |
| 12/9/2008 | 13:43:06 | 20.563 | 0.122 | 420 | 0.024 | 8.781 | | |
| 12/9/2008 | 13:43:16 | 20.487 | 0.213 | 429.487 | 0.024 | 16.806 | | |
| 12/9/2008 | 13:43:26 | 20.365 | 0.274 | 435.841 | 33.089 | 6.356 | | |
| 12/9/2008 | 13:43:36 | 20.289 | 0.274 | 436.667 | 20.684 | 23.089 | | |
| 12/9/2008 | 13:43:46 | 20.182 | 0.274 | 436.154 | 3.98 | 33.233 | | |
| 12/9/2008 | 13:43:56 | 20.259 | 0.183 | 458.462 | 0.289 | 50.493 | | |
| 12/9/2008 | 13:44:06 | 20.335 | 0.122 | 417.949 | 0.024 | 55.035 | | |
| 12/9/2008 | 13:44:16 | 20.457 | 0.061 | 393.077 | 0.024 | 61.319 | | |
| 12/9/2008 | 13:44:26 | 20.548 | 0.061 | 374.103 | 0.024 | 76.611 | | |
| 12/9/2008 | 13:44:36 | 20.533 | 0.152 | 410.769 | 0.024 | 44.286 | | |
| 12/9/2008 | 13:44:46 | 20.457 | 0.244 | 414.615 | 0.024 | 29.524 | | |
| 12/9/2008 | 13:44:56 | 20.335 | 0.274 | 402.821 | 0.024 | 22.181 | | |
| 12/9/2008 | 13:45:06 | 20.213 | 0.335 | 396.154 | 18.926 | 14.913 | | |
| 12/9/2008 | 13:45:16 | 20.167 | 0.305 | 399.487 | 15.995 | 13.248 | | |
| 12/9/2008 | 13:45:26 | 20.167 | 0.305 | 416.154 | 1.245 | 11.81 | | |
| 12/9/2008 | 13:45:36 | 20.182 | 0.213 | 432.564 | 0.024 | 10.977 | | |
| 12/9/2008 | 13:45:46 | 20.304 | 0.122 | 444.359 | 0.024 | 10.977 | | |
| 12/9/2008 | 13:45:56 | 20.411 | 0.061 | 402.051 | 0.024 | 12.112 | | |
| 12/9/2008 | 13:46:06 | 20.487 | 0.03 | 381.026 | 0.024 | 12.945 | | |
| 12/9/2008 | 13:46:16 | 20.533 | 0.081 | 403.077 | 0.024 | 12.415 | | |
| 12/9/2008 | 13:46:26 | 20.533 | 0.152 | 409.487 | 0.024 | 10.295 | | |
| 12/9/2008 | 13:46:36 | 20.472 | 0.213 | 402.564 | 0.024 | 10.22 | | |
| 12/9/2008 | 13:46:46 | 20.335 | 0.244 | 401.538 | 34.164 | 11.658 | | |
| 12/9/2008 | 13:46:56 | 20.274 | 0.244 | 390.256 | 22.369 | 12.567 | | |
| 12/9/2008 | 13:47:06 | 20.182 | 0.274 | 409.487 | 4.581 | 11.28 | | |
| 12/9/2008 | 13:47:16 | 20.228 | 0.183 | 420.513 | 0.44 | 9.917 | | |
| 12/9/2008 | 13:47:26 | 20.35 | 0.122 | 430.256 | 0.024 | 9.841 | | |
| 12/9/2008 | 13:47:36 | 20.457 | 0.091 | 484.359 | 0.024 | 9.841 | | |
| 12/9/2008 | 13:47:46 | 20.548 | 0.091 | 449.231 | 0.024 | 10.447 | | |
| 12/9/2008 | 13:47:56 | 20.517 | 0.122 | 416.667 | 0.024 | 11.355 | | |
| 12/9/2008 | 13:48:06 | 20.457 | 0.213 | 414.103 | 0.024 | 12.037 | | |
| 12/9/2008 | 13:48:16 | 20.304 | 0.274 | 425.128 | 0.024 | 12.339 | | |
| 12/9/2008 | 13:48:26 | 20.182 | 0.274 | 412.308 | 22.051 | 12.112 | | |
| 12/9/2008 | 13:48:36 | 20.182 | 0.274 | 385.128 | 19.536 | 12.264 | | |
| 12/9/2008 | 13:48:46 | 20.228 | 0.274 | 372.308 | 3.272 | 12.188 | | |
| 12/9/2008 | 13:48:56 | 20.335 | 0.152 | 375.128 | 0.733 | 11.582 | | |
| 12/9/2008 | 13:49:06 | 20.396 | 0.091 | 393.59 | 0.024 | 10.295 | | |
| 12/9/2008 | 13:49:16 | 20.563 | 0.122 | 412.564 | 0.024 | 9.538 | | |
| 12/9/2008 | 13:49:26 | 20.639 | 0.091 | 410.513 | 0.024 | 9.538 | | |
| 12/9/2008 | 13:49:36 | 20.517 | 0.091 | 403.59 | 0.024 | 10.22 | | |
| 12/9/2008 | 13:49:46 | 20.563 | 0.152 | 399.744 | 0.024 | 11.885 | | |
| 12/9/2008 | 13:49:56 | 20.457 | 0.213 | 391.026 | 0.024 | 12.188 | | |
| 12/9/2008 | 13:50:06 | 20.365 | 0.244 | 406.974 | 34.628 | 12.264 | | |
| 12/9/2008 | 13:50:16 | 20.243 | 0.244 | 392.051 | 22.54 | 12.188 | | |
| 12/9/2008 | 13:50:26 | 20.182 | 0.213 | 381.282 | 5.397 | 12.112 | | |
| 12/9/2008 | 13:50:36 | 20.228 | 0.122 | 376.667 | 1.708 | 12.188 | | |
| 12/9/2008 | 13:50:46 | 20.35 | 0.081 | 385.128 | 0.171 | 12.188 | | |
| 12/9/2008 | 13:50:56 | 20.441 | 0.081 | 367.949 | 0.024 | 12.037 | | |
| 12/9/2008 | 13:51:06 | 20.533 | 0.081 | 394.103 | 0.024 | 12.112 | | |
| 12/9/2008 | 13:51:16 | 20.533 | 0.122 | 382.308 | 0.024 | 11.885 | | |
| 12/9/2008 | 13:51:26 | 20.441 | 0.183 | 376.667 | 0.024 | 12.188 | | |
| 12/9/2008 | 13:51:36 | 20.335 | 0.244 | 398.718 | 0.024 | 12.188 | | |
| 12/9/2008 | 13:51:46 | 20.228 | 0.274 | 388.974 | 22.979 | 11.961 | | |
| 12/9/2008 | 13:51:56 | 20.182 | 0.244 | 417.849 | 19.683 | 17.26 | | |
| 12/9/2008 | 13:52:06 | 20.152 | 0.305 | 437.179 | 2.589 | 76.535 | | |
| 12/9/2008 | 13:52:16 | 20.187 | 0.213 | 450.256 | 0.024 | 85.618 | | |
| 12/9/2008 | 13:52:26 | 20.411 | 0.152 | 453.59 | 0.024 | 88.982 | | |
| 12/9/2008 | 13:52:36 | 20.533 | 0.122 | 468.205 | 0.024 | 87.284 | | |
| 12/9/2008 | 13:52:46 | 20.639 | 0.091 | 468.718 | 0.024 | 88.183 | | |
| 12/9/2008 | 13:52:56 | 20.67 | 0.122 | 438.718 | 0.024 | 87.436 | | |
| 12/9/2008 | 13:53:06 | 20.716 | 0.152 | 421.282 | 0.024 | 87.438 | | |
| 12/9/2008 | 13:53:16 | 20.655 | 0.213 | 427.436 | 0.024 | 87.89 | | |
| 12/9/2008 | 13:53:26 | 20.365 | 0.305 | 423.077 | 31.38 | 88.183 | | |
| 12/9/2008 | 13:53:36 | 20.243 | 0.305 | 427.692 | 20.659 | 83.045 | | |
| 12/9/2008 | 13:53:46 | 20.228 | 0.244 | 403.077 | 4.398 | 78.308 | | |
| 12/9/2008 | 13:53:56 | 20.259 | 0.183 | 391.282 | 0.855 | 78.081 | | |
| 12/9/2008 | 13:54:06 | 20.35 | 0.122 | 411.538 | 0.024 | 77.065 | | |
| 12/9/2008 | 13:54:16 | 20.457 | 0.091 | 401.282 | 0.024 | 78.049 | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|----------|--------|-------|-----------------------------------|-----------------------------------|-----------------------------------|-------------------------|------------|
| | | % | % | ppm C ₂ H ₆ | ppm C ₂ H ₆ | ppm C ₂ H ₆ | | |
| 12/9/2008 | 13:54:26 | 20.517 | 0.091 | 396.154 | 0.024 | 78.654 | | |
| 12/9/2008 | 13:54:36 | 20.517 | 0.305 | 405.641 | 0.024 | 78.806 | | |
| 12/9/2008 | 13:54:46 | 20.426 | 0.366 | 380.769 | 0.024 | 78.503 | | |
| 12/9/2008 | 13:54:56 | 20.304 | 0.426 | 380.256 | 0.024 | 78.049 | | |
| 12/9/2008 | 13:55:06 | 20.228 | 0.457 | 383.59 | 19.731 | 77.292 | | |
| 12/9/2008 | 13:55:16 | 20.167 | 0.457 | 403.59 | 17.118 | 77.14 | | |
| 12/9/2008 | 13:55:26 | 20.137 | 0.457 | 439.744 | 1.832 | 76.989 | | |
| 12/9/2008 | 13:55:36 | 20.152 | 0.366 | 416.923 | 0.024 | 76.913 | | |
| 12/9/2008 | 13:55:46 | 20.274 | 0.305 | 414.872 | 0.024 | 77.216 | | |
| 12/9/2008 | 13:55:56 | 20.396 | 0.244 | 401.282 | 0.024 | 79.184 | | |
| 12/9/2008 | 13:56:06 | 20.502 | 0.213 | 378.974 | 0.024 | 81.531 | | |
| 12/9/2008 | 13:56:16 | 20.548 | 0.183 | 405.128 | 0.024 | 16.73 | | |
| 12/9/2008 | 13:56:26 | 20.578 | 0.274 | 444.872 | 0.024 | 11.204 | | |
| 12/9/2008 | 13:56:36 | 20.472 | 0.396 | 450.256 | 0.024 | 10.088 | | |
| 12/9/2008 | 13:56:46 | 20.335 | 0.457 | 444.359 | 34.505 | 9.69 | | |
| 12/9/2008 | 13:56:56 | 20.243 | 0.457 | 443.59 | 24.103 | 11.128 | | |
| 12/9/2008 | 13:57:06 | 20.213 | 0.366 | 419.744 | 5.934 | 11.658 | | |
| 12/9/2008 | 13:57:16 | 20.259 | 0.274 | 398.974 | 2.027 | 11.658 | | |
| 12/9/2008 | 13:57:26 | 20.38 | 0.244 | 380.769 | 0.317 | 10.977 | | |
| 12/9/2008 | 13:57:36 | 20.472 | 0.122 | 387.949 | 0.024 | 10.371 | | |
| 12/9/2008 | 13:57:46 | 20.533 | 0.081 | 400.513 | 0.024 | 9.993 | | |
| 12/9/2008 | 13:57:56 | 20.563 | 0.152 | 424.359 | 0.024 | 9.009 | | |
| 12/9/2008 | 13:58:06 | 20.441 | 0.244 | 418.462 | 0.024 | 8.781 | | |
| 12/9/2008 | 13:58:16 | 20.319 | 0.305 | 423.333 | 0.024 | 8.63 | | |
| 12/9/2008 | 13:58:26 | 20.213 | 0.335 | 431.026 | 19.927 | 8.403 | | |
| 12/9/2008 | 13:58:36 | 20.167 | 0.305 | 435.128 | 17.729 | 8.554 | | |
| 12/9/2008 | 13:58:46 | 20.152 | 0.305 | 461.026 | 2.442 | 8.479 | | |
| 12/9/2008 | 13:58:56 | 20.167 | 0.213 | 455.128 | 0.195 | 8.403 | | |
| 12/9/2008 | 13:59:06 | 20.289 | 0.152 | 424.359 | 0.024 | 8.781 | | |
| 12/9/2008 | 13:59:16 | 20.411 | 0.081 | 397.179 | 0.024 | 10.523 | | |
| 12/9/2008 | 13:59:26 | 20.517 | 0.03 | 380.769 | 0.024 | 10.901 | | |
| 12/9/2008 | 13:59:36 | 20.563 | 0.03 | 385.897 | 0.024 | 10.295 | | |
| 12/9/2008 | 13:59:46 | 20.563 | 0.152 | 427.179 | 0.024 | 8.706 | | |
| 12/9/2008 | 13:59:56 | 20.457 | 0.244 | 428.974 | 0.024 | 8.176 | | |
| 12/9/2008 | 14:00:06 | 20.319 | 0.274 | 405.385 | 29.768 | 9.236 | | |
| 12/9/2008 | 14:00:16 | 20.259 | 0.244 | 377.692 | 20.562 | 10.75 | | |
| 12/9/2008 | 14:00:26 | 20.228 | 0.213 | 380.513 | 5.421 | 13.853 | | |
| 12/9/2008 | 14:00:36 | 20.243 | 0.152 | 421.026 | 1.294 | 51.175 | | |
| 12/9/2008 | 14:00:46 | 20.319 | 0.152 | 454.103 | 0.024 | 58.593 | | |
| 12/9/2008 | 14:00:56 | 20.441 | 0.122 | 433.59 | 0.024 | 62.984 | | |
| 12/9/2008 | 14:01:06 | 20.502 | 0.081 | 398.385 | 0.024 | 69.04 | | |
| 12/9/2008 | 14:01:16 | 20.517 | 0.152 | 422.308 | 0.024 | 78.2 | | |
| 12/9/2008 | 14:01:26 | 20.411 | 0.213 | 417.949 | 0.024 | 88.847 | | |
| 12/9/2008 | 14:01:36 | 20.304 | 0.274 | 406.667 | 0.024 | 91.875 | | |
| 12/9/2008 | 14:01:46 | 20.213 | 0.305 | 371.538 | 22.002 | 89.404 | | |
| 12/9/2008 | 14:01:56 | 20.152 | 0.274 | 378.231 | 18.926 | 84.266 | | |
| 12/9/2008 | 14:02:06 | 20.152 | 0.305 | 405.128 | 3.028 | 84.938 | | |
| 12/9/2008 | 14:02:16 | 20.152 | 0.213 | 417.179 | 0.171 | 93.114 | | |
| 12/9/2008 | 14:02:26 | 20.274 | 0.152 | 413.333 | 0.024 | 96.974 | | |
| 12/9/2008 | 14:02:36 | 20.411 | 0.061 | 370 | 0.024 | 101.365 | | |
| 12/9/2008 | 14:02:46 | 20.502 | 0.03 | 371.795 | 0.024 | 104.696 | | |
| 12/9/2008 | 14:02:56 | 20.548 | 0.061 | 389.744 | 0.024 | 105.604 | | |
| 12/9/2008 | 14:03:06 | 20.563 | 0.152 | 435.385 | 0.024 | 87.436 | | |
| 12/9/2008 | 14:03:16 | 20.457 | 0.244 | 454.103 | 0.024 | 74.718 | | |
| 12/9/2008 | 14:03:26 | 20.335 | 0.274 | 413.59 | 31.844 | 89.949 | | |
| 12/9/2008 | 14:03:36 | 20.243 | 0.244 | 384.359 | 21.636 | 69.343 | | |
| 12/9/2008 | 14:03:46 | 20.182 | 0.274 | 373.59 | 4.762 | 70.1 | | |
| 12/9/2008 | 14:03:56 | 20.243 | 0.152 | 408.974 | 0.806 | 67.829 | | |
| 12/9/2008 | 14:04:06 | 20.365 | 0.081 | 385.897 | 0.22 | 69.846 | | |
| 12/9/2008 | 14:04:16 | 20.426 | 0.122 | 430 | 0.024 | 67.299 | | |
| 12/9/2008 | 14:04:26 | 20.548 | 0.091 | 435.897 | 0.024 | 65.937 | | |
| 12/9/2008 | 14:04:36 | 20.548 | 0.122 | 401.282 | 0.024 | 67.678 | | |
| 12/9/2008 | 14:04:46 | 20.441 | 0.244 | 421.795 | 0.024 | 67.678 | | |
| 12/9/2008 | 14:04:56 | 20.304 | 0.305 | 471.026 | 0.024 | 66.921 | | |
| 12/9/2008 | 14:05:06 | 20.228 | 0.305 | 451.026 | 20.073 | 72.447 | | |
| 12/9/2008 | 14:05:16 | 20.167 | 0.274 | 412.051 | 20.073 | 83.197 | | |
| 12/9/2008 | 14:05:26 | 20.182 | 0.244 | 393.333 | 3.419 | 89.783 | | |
| 12/9/2008 | 14:05:36 | 20.182 | 0.183 | 419.487 | 0.928 | 86.83 | | |
| 12/9/2008 | 14:05:46 | 20.289 | 0.122 | 398.231 | 0.024 | 82.818 | | |
| 12/9/2008 | 14:05:56 | 20.411 | 0.091 | 387.949 | 0.024 | 76.156 | | |
| 12/9/2008 | 14:06:06 | 20.802 | 0.061 | 362.051 | 0.024 | 72.75 | | |
| 12/9/2008 | 14:06:16 | 20.548 | 0.081 | 378.205 | 0.024 | 72.977 | | |
| 12/9/2008 | 14:06:26 | 20.563 | 0.122 | 424.359 | 0.024 | 83.197 | | |
| 12/9/2008 | 14:06:36 | 20.472 | 0.244 | 421.598 | 0.024 | 98.486 | | |
| 12/9/2008 | 14:06:46 | 20.335 | 0.305 | 403.846 | 28.669 | 102.122 | | |

Start Run #3

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 % | CO2 % | RTO Inlet | | RTO Outlet | | Calibration Comments | Error % |
|-----------|----------|--------|-------|---|---|---|--|----------------------|---------|
| | | | | VOC 3 ppm C ₆ H ₆ | VOC 1 ppm C ₆ H ₆ | VOC 2 ppm C ₆ H ₆ | | | |
| 12/9/2008 | 14:06:56 | 20.259 | 0.457 | 377.949 | 19.17 | 103.636 | | | |
| 12/9/2008 | 14:07:06 | 20.213 | 0.396 | 373.59 | 4.713 | 101.441 | | | |
| 12/9/2008 | 14:07:16 | 20.274 | 0.274 | 375.897 | 1.441 | 95.082 | | | |
| 12/9/2008 | 14:07:26 | 20.365 | 0.244 | 402.564 | 0.024 | 78.049 | | | |
| 12/9/2008 | 14:07:36 | 20.457 | 0.213 | 426.154 | 0.024 | 71.463 | | | |
| 12/9/2008 | 14:07:46 | 20.517 | 0.244 | 425.385 | 0.024 | 67.878 | | | |
| 12/9/2008 | 14:07:56 | 20.517 | 0.335 | 425.641 | 0.024 | 66.542 | | | |
| 12/9/2008 | 14:08:06 | 20.411 | 0.426 | 404.872 | 0.024 | 64.801 | | | |
| 12/9/2008 | 14:08:16 | 20.304 | 0.457 | 411.538 | 0.024 | 66.164 | | | |
| 12/9/2008 | 14:08:26 | 20.228 | 0.457 | 413.077 | 20.83 | 67.148 | | | |
| 12/9/2008 | 14:08:36 | 20.167 | 0.426 | 383.59 | 19.316 | 67.451 | | | |
| 12/9/2008 | 14:08:46 | 20.152 | 0.426 | 379.487 | 3.175 | 68.283 | | | |
| 12/9/2008 | 14:08:56 | 20.182 | 0.305 | 388.974 | 0.684 | 69.343 | | | |
| 12/9/2008 | 14:08:06 | 20.304 | 0.244 | 400.513 | 0.024 | 67.829 | | | |
| 12/9/2008 | 14:09:16 | 20.426 | 0.244 | 432.051 | 0.024 | 67.602 | | | |
| 12/9/2008 | 14:09:26 | 20.502 | 0.274 | 454.872 | 0.024 | 67.223 | | | |
| 12/9/2008 | 14:09:36 | 20.533 | 0.274 | 469.487 | 0.024 | 67.905 | | | |
| 12/9/2008 | 14:09:46 | 20.533 | 0.152 | 468.462 | 0.024 | 69.192 | | | |
| 12/9/2008 | 14:09:56 | 20.426 | 0.244 | 451.795 | 0.024 | 72.295 | | | |
| 12/9/2008 | 14:10:06 | 20.335 | 0.274 | 432.051 | 32.601 | 80.623 | | | |
| 12/9/2008 | 14:10:16 | 20.228 | 0.274 | 420 | 22.979 | 91.6 | | | |
| 12/9/2008 | 14:10:26 | 20.182 | 0.213 | 382.821 | 5.91 | 94.552 | | | |
| 12/9/2008 | 14:10:36 | 20.243 | 0.091 | 371.026 | 1.758 | 90.085 | | | |
| 12/9/2008 | 14:10:46 | 20.35 | 0.061 | 379.487 | 0.22 | 94.703 | | | |
| 12/9/2008 | 14:10:56 | 20.457 | 0.061 | 390 | 0.024 | 99.548 | | | |
| 12/9/2008 | 14:11:06 | 20.533 | 0.03 | 371.538 | 0.024 | 98.186 | | | |
| 12/9/2008 | 14:11:16 | 20.548 | 0.091 | 370 | 0.024 | 99.775 | | | |
| 12/9/2008 | 14:11:26 | 20.472 | 0.213 | 371.282 | 0.024 | 101.516 | | | |
| 12/9/2008 | 14:11:36 | 20.365 | 0.274 | 396.667 | 0.024 | 104.469 | | | |
| 12/9/2008 | 14:11:46 | 20.243 | 0.305 | 420.769 | 20.171 | 93.114 | | | |
| 12/9/2008 | 14:11:56 | 20.182 | 0.305 | 453.077 | 18.608 | 83.121 | | | |
| 12/9/2008 | 14:12:06 | 20.187 | 0.274 | 446.154 | 2.344 | 74.718 | | | |
| 12/9/2008 | 14:12:16 | 20.182 | 0.213 | 414.872 | 0.073 | 89.419 | | | |
| 12/9/2008 | 14:12:26 | 20.319 | 0.152 | 403.077 | 0.024 | 70.479 | | | |
| 12/9/2008 | 14:12:36 | 20.396 | 0.091 | 371.026 | 0.024 | 72.144 | | | |
| 12/9/2008 | 14:12:46 | 20.517 | 0.03 | 359.744 | 0.024 | 71.69 | | | |
| 12/9/2008 | 14:12:56 | 20.563 | 0.061 | 392.564 | 0.024 | 71.387 | | | |
| 12/9/2008 | 14:13:06 | 20.548 | 0.122 | 398.718 | 0.024 | 69.873 | | | |
| 12/9/2008 | 14:13:16 | 20.457 | 0.213 | 397.179 | 0.024 | 68.359 | | | |
| 12/9/2008 | 14:13:26 | 20.335 | 0.274 | 423.333 | 30.256 | 68.056 | | | |
| 12/9/2008 | 14:13:36 | 20.228 | 0.305 | 440.513 | 20.781 | 67.299 | | | |
| 12/9/2008 | 14:13:46 | 20.198 | 0.274 | 434.359 | 4.444 | 66.769 | | | |
| 12/9/2008 | 14:13:56 | 20.243 | 0.183 | 440 | 0.757 | 67.802 | | | |
| 12/9/2008 | 14:14:06 | 20.35 | 0.122 | 434.103 | 0.024 | 70.63 | | | |
| 12/9/2008 | 14:14:16 | 20.441 | 0.091 | 448.718 | 0.024 | 76.005 | | | |
| 12/9/2008 | 14:14:26 | 20.533 | 0.061 | 418.718 | 0.024 | 83.424 | | | |
| 12/9/2008 | 14:14:36 | 20.548 | 0.091 | 396.667 | 0.024 | 87.209 | | | |
| 12/9/2008 | 14:14:46 | 20.472 | 0.213 | 407.436 | 0.024 | 83.878 | | | |
| 12/9/2008 | 14:14:56 | 20.335 | 0.305 | 418.974 | 0.024 | 79.411 | | | |
| 12/9/2008 | 14:15:06 | 20.228 | 0.305 | 415.128 | 19.389 | 74.415 | | | |
| 12/9/2008 | 14:15:16 | 20.182 | 0.305 | 421.538 | 17.827 | 83.272 | | | |
| 12/9/2008 | 14:15:26 | 20.152 | 0.274 | 415.385 | 2.491 | 94.325 | | | |
| 12/9/2008 | 14:15:36 | 20.167 | 0.213 | 409.744 | 0.122 | 98.11 | | | |
| 12/9/2008 | 14:15:46 | 20.269 | 0.122 | 403.333 | 0.024 | 101.518 | | | |
| 12/9/2008 | 14:15:56 | 20.426 | 0.091 | 429.487 | 0.024 | 103.333 | | | |
| 12/9/2008 | 14:16:06 | 20.502 | 0.03 | 400.256 | 0.024 | 99.321 | | | |
| 12/9/2008 | 14:16:16 | 20.548 | 0.091 | 445.385 | 0.024 | 79.79 | | | |
| 12/9/2008 | 14:16:26 | 20.517 | 0.152 | 443.333 | 0.024 | 71.387 | | | |
| 12/9/2008 | 14:16:36 | 20.441 | 0.244 | 425.385 | 0.024 | 67.602 | | | |
| 12/9/2008 | 14:16:46 | 20.319 | 0.274 | 421.638 | 29.109 | 66.542 | | | |
| 12/9/2008 | 14:16:56 | 20.243 | 0.274 | 402.564 | 20.537 | 68.056 | | | |
| 12/9/2008 | 14:17:06 | 20.182 | 0.274 | 413.333 | 4.493 | 67.451 | | | |
| 12/9/2008 | 14:17:16 | 20.259 | 0.152 | 444.359 | 0.757 | 68.435 | | | |
| 12/9/2008 | 14:17:26 | 20.35 | 0.122 | 442.061 | 0.024 | 68.965 | | | |
| 12/9/2008 | 14:17:36 | 20.457 | 0.091 | 434.359 | 0.024 | 68.132 | | | |
| 12/9/2008 | 14:17:46 | 20.502 | 0.091 | 443.846 | 0.024 | 67.148 | | | |
| 12/9/2008 | 14:17:56 | 20.517 | 0.152 | 413.846 | 0.024 | 69.57 | | | |
| 12/9/2008 | 14:18:06 | 20.426 | 0.213 | 427.949 | 0.024 | 73.734 | | | |
| 12/9/2008 | 14:18:16 | 20.335 | 0.244 | 392.564 | 0.024 | 77.897 | | | |
| 12/9/2008 | 14:18:26 | 20.228 | 0.274 | 402.051 | 20.513 | 81.531 | | | |
| 12/9/2008 | 14:18:36 | 20.167 | 0.274 | 420.769 | 19.023 | 80.774 | | | |
| 12/9/2008 | 14:18:46 | 20.152 | 0.305 | 460.769 | 2.442 | 78.654 | | | |
| 12/9/2008 | 14:18:56 | 20.167 | 0.213 | 462.564 | 0.073 | 75.475 | | | |
| 12/9/2008 | 14:19:06 | 20.289 | 0.152 | 433.59 | 0.024 | 72.598 | | | |
| 12/9/2008 | 14:19:16 | 20.411 | 0.091 | 382.308 | 0.024 | 74.112 | | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|----------|--------|-------|--|--|--|----------|-------------------------|------------|
| | | % | % | VOC 3 ppm C ₆ H ₆ | VOC 1 ppm C ₆ H ₆ | VOC 2 ppm C ₆ H ₆ | | | |
| 12/9/2008 | 14:19:26 | 20.517 | 0.03 | 367.592 | 0.024 | 75.702 | | | |
| 12/9/2008 | 14:19:36 | 20.548 | 0.061 | 408.205 | 0.024 | 86.755 | | | |
| 12/9/2008 | 14:19:46 | 20.533 | 0.152 | 413.846 | 0.024 | 99.016 | | | |
| 12/9/2008 | 14:19:56 | 20.457 | 0.244 | 395.541 | 0.024 | 103.182 | | | |
| 12/9/2008 | 14:20:06 | 20.335 | 0.244 | 372.051 | 32.967 | 102.803 | | | |
| 12/9/2008 | 14:20:16 | 20.269 | 0.274 | 393.333 | 21.783 | 98.034 | | | |
| 12/9/2008 | 14:20:26 | 20.182 | 0.274 | 422.564 | 4.906 | 90.237 | | | |
| 12/9/2008 | 14:20:36 | 20.228 | 0.152 | 442.308 | 1.49 | 76.913 | | | |
| 12/9/2008 | 14:20:46 | 20.365 | 0.091 | 401.026 | 0.391 | 72.068 | | | |
| 12/9/2008 | 14:20:56 | 20.457 | 0.061 | 393.59 | 0.024 | 68.813 | | | |
| 12/9/2008 | 14:21:06 | 20.502 | 0.091 | 420 | 0.024 | 67.299 | | | |
| 12/9/2008 | 14:21:16 | 20.502 | 0.183 | 402.308 | 0.024 | 68.088 | | | |
| 12/9/2008 | 14:21:26 | 20.441 | 0.244 | 384.103 | 0.024 | 67.98 | | | |
| 12/9/2008 | 14:21:36 | 20.319 | 0.306 | 395.385 | 0.024 | 68.662 | | | |
| 12/9/2008 | 14:21:46 | 20.213 | 0.426 | 390 | 20.928 | 68.813 | | | |
| 12/9/2008 | 14:21:56 | 20.167 | 0.426 | 397.949 | 19.609 | 68.056 | | | |
| 12/9/2008 | 14:22:06 | 20.152 | 0.426 | 432.584 | 2.857 | 68.542 | | | |
| 12/9/2008 | 14:22:16 | 20.198 | 0.335 | 451.795 | 0.22 | 65.482 | | | |
| 12/9/2008 | 14:22:26 | 20.289 | 0.305 | 456.41 | 0.024 | 66.164 | | | |
| 12/9/2008 | 14:22:36 | 20.396 | 0.274 | 450.513 | 0.024 | 71.084 | | | |
| 12/9/2008 | 14:22:46 | 20.487 | 0.244 | 463.077 | 0.024 | 77.746 | | | |
| 12/9/2008 | 14:22:56 | 20.517 | 0.244 | 446.923 | 0.024 | 81.91 | | | |
| 12/9/2008 | 14:23:06 | 20.533 | 0.305 | 473.59 | 0.024 | 82.137 | | | |
| 12/9/2008 | 14:23:16 | 20.457 | 0.306 | 465.385 | 0.024 | 79.411 | | | |
| 12/9/2008 | 14:23:26 | 20.35 | 0.457 | 437.949 | 31.038 | 76.156 | | | |
| 12/9/2008 | 14:23:36 | 20.228 | 0.428 | 414.103 | 21.123 | 73.507 | | | |
| 12/9/2008 | 14:23:46 | 20.213 | 0.396 | 404.872 | 5.275 | 74.415 | | | |
| 12/9/2008 | 14:23:56 | 20.243 | 0.305 | 417.436 | 1.612 | 88.803 | | | |
| 12/9/2008 | 14:24:06 | 20.35 | 0.244 | 396.667 | 0.147 | 99.824 | | | |
| 12/9/2008 | 14:24:16 | 20.487 | 0.061 | 379.487 | 0.024 | 101.819 | | | |
| 12/9/2008 | 14:24:26 | 20.532 | 0.091 | 378.487 | 0.024 | 104.166 | | | |
| 12/9/2008 | 14:24:36 | 20.648 | 0.122 | 412.308 | 0.024 | 103.106 | | | |
| 12/9/2008 | 14:24:46 | 20.441 | 0.244 | 400.769 | 0.024 | 95.158 | | | |
| 12/9/2008 | 14:24:56 | 20.319 | 0.274 | 440 | 0.024 | 79.184 | | | |
| 12/9/2008 | 14:25:06 | 20.228 | 0.305 | 437.949 | 20.342 | 72.523 | | | |
| 12/9/2008 | 14:25:16 | 20.182 | 0.305 | 409.744 | 19.683 | 68.737 | | | |
| 12/9/2008 | 14:25:26 | 20.137 | 0.305 | 416.41 | 2.662 | 68.862 | | | |
| 12/9/2008 | 14:25:36 | 20.182 | 0.183 | 394.103 | 0.22 | 68.586 | | | |
| 12/9/2008 | 14:25:46 | 20.289 | 0.122 | 415.128 | 0.024 | 67.678 | | | |
| 12/9/2008 | 14:25:56 | 20.411 | 0.091 | 438.482 | 0.024 | 68.283 | | | |
| 12/9/2008 | 14:26:06 | 20.617 | 0.061 | 392.308 | 0.024 | 69.04 | | | |
| 12/9/2008 | 14:26:16 | 20.548 | 0.03 | 394.872 | 0.024 | 67.072 | | | |
| 12/9/2008 | 14:26:26 | 20.578 | 0.122 | 456.41 | 0.024 | 65.407 | | | |
| 12/9/2008 | 14:26:36 | 20.472 | 0.213 | 470 | 0.024 | 69.116 | | | |
| 12/9/2008 | 14:26:46 | 20.35 | 0.274 | 434.815 | 33.162 | 75.399 | | | |
| 12/9/2008 | 14:26:56 | 20.259 | 0.244 | 410.769 | 23.785 | 78.2 | | | |
| 12/9/2008 | 14:27:06 | 20.198 | 0.213 | 411.282 | 5.81 | 78.352 | | | |
| 12/8/2008 | 14:27:16 | 20.243 | 0.152 | 446.923 | 1.392 | 79.487 | | | |
| 12/9/2008 | 14:27:26 | 20.38 | 0.091 | 436.667 | 0.562 | 79.487 | | | |
| 12/9/2008 | 14:27:36 | 20.441 | 0.061 | 420.513 | 0.024 | 73.81 | | | |
| 12/9/2008 | 14:27:46 | 20.517 | 0.091 | 440.256 | 0.024 | 70.479 | | | |
| 12/9/2008 | 14:27:56 | 20.517 | 0.182 | 407.949 | 0.024 | 73.204 | | | |
| 12/9/2008 | 14:28:06 | 20.457 | 0.213 | 387.949 | 0.024 | 78.049 | | | |
| 12/9/2008 | 14:28:16 | 20.319 | 0.244 | 381.538 | 0.024 | 80.313 | | | |
| 12/9/2008 | 14:28:26 | 20.243 | 0.274 | 390 | 18.828 | 102.046 | | | |
| 12/9/2008 | 14:28:36 | 20.167 | 0.274 | 409.231 | 18.462 | 103.182 | | | |
| 12/9/2008 | 14:28:46 | 20.152 | 0.305 | 417.692 | 2.54 | 98.84 | | | |
| 12/9/2008 | 14:28:56 | 20.198 | 0.213 | 436.154 | 0.293 | 96.066 | | | |
| 12/9/2008 | 14:29:06 | 20.304 | 0.152 | 434.872 | 0.024 | 90.313 | | | |
| 12/9/2008 | 14:29:16 | 20.441 | 0.091 | 449.231 | 0.024 | 76.308 | | | |
| 12/9/2008 | 14:29:26 | 20.502 | 0.091 | 431.282 | 0.024 | 72.447 | | | |
| 12/9/2008 | 14:29:36 | 20.548 | 0.091 | 412.821 | 0.024 | 70.1 | | | |
| 12/9/2008 | 14:29:46 | 20.583 | 0.122 | 395.128 | 0.024 | 68.965 | | | |
| 12/9/2008 | 14:29:56 | 20.502 | 0.213 | 375.128 | 0.024 | 69.949 | | | |
| 12/9/2008 | 14:30:06 | 20.35 | 0.244 | 380.268 | 28.742 | 70.83 | | | |
| 12/9/2008 | 14:30:16 | 20.289 | 0.244 | 393.59 | 22.515 | 70.857 | | | |
| 12/9/2008 | 14:30:26 | 20.228 | 0.213 | 394.103 | 5.446 | 89.722 | | | |
| 12/9/2008 | 14:30:36 | 20.243 | 0.152 | 392.821 | 1.783 | 68.435 | | | |
| 12/9/2008 | 14:30:46 | 20.335 | 0.091 | 388.41 | 0.44 | 67.98 | | | |
| 12/9/2008 | 14:30:56 | 20.441 | 0.091 | 390.256 | 0.024 | 70.933 | | | |
| 12/9/2008 | 14:31:06 | 20.502 | 0.091 | 425.385 | 0.024 | 76.156 | | | |
| 12/9/2008 | 14:31:16 | 20.487 | 0.183 | 439.487 | 0.024 | 79.563 | | | |
| 12/9/2008 | 14:31:26 | 20.398 | 0.274 | 448.205 | 0.024 | 79.184 | | | |
| 12/9/2008 | 14:31:36 | 20.274 | 0.305 | 450.513 | 0.024 | 76.838 | | | |
| 12/9/2008 | 14:31:46 | 20.228 | 0.274 | 482.051 | 21.074 | 75.324 | | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|----------|--------|-------|--|--|--|----------|-------------------------|------------|
| | | % | % | VOC 3 ppm C ₂ H ₆ | VOC 1 ppm C ₂ H ₆ | VOC 2 ppm C ₂ H ₆ | | | |
| 12/9/2008 | 14:31:56 | 20.167 | 0.244 | 443.077 | 21.245 | 74.188 | | | |
| 12/9/2008 | 14:32:06 | 20.167 | 0.274 | 395.641 | 3.932 | 75.324 | | | |
| 12/9/2008 | 14:32:16 | 20.182 | 0.213 | 379.744 | 1.319 | 75.853 | | | |
| 12/9/2008 | 14:32:26 | 20.259 | 0.152 | 412.051 | 0.024 | 78.762 | | | |
| 12/9/2008 | 14:32:36 | 20.411 | 0.091 | 431.282 | 0.024 | 87.436 | | | |
| 12/9/2008 | 14:32:46 | 20.487 | 0.091 | 419.487 | 0.024 | 99.624 | | | |
| 12/9/2008 | 14:32:56 | 20.563 | 0.091 | 401.538 | 0.024 | 102.803 | | | |
| 12/9/2008 | 14:33:06 | 20.563 | 0.122 | 391.795 | 0.024 | 102.501 | | | |
| 12/9/2008 | 14:33:16 | 20.487 | 0.213 | 408.974 | 0.024 | 100.002 | | | |
| 12/9/2008 | 14:33:26 | 20.35 | 0.274 | 416.887 | 31.697 | 93.946 | | | |
| 12/9/2008 | 14:33:36 | 20.259 | 0.274 | 425.897 | 22.637 | 78.427 | | | |
| 12/9/2008 | 14:33:46 | 20.198 | 0.244 | 419.231 | 5.91 | 71.893 | | | |
| 12/9/2008 | 14:33:56 | 20.243 | 0.152 | 391.938 | 1.654 | 70.403 | | | |
| 12/9/2008 | 14:34:06 | 20.35 | 0.091 | 382.308 | 0.659 | 70.024 | | | |
| 12/9/2008 | 14:34:16 | 20.426 | 0.091 | 374.359 | 0.024 | 71.538 | | | |
| 12/9/2008 | 14:34:26 | 20.517 | 0.091 | 412.051 | 0.024 | 69.797 | | | |
| 12/9/2008 | 14:34:36 | 20.517 | 0.183 | 444.872 | 0.024 | 69.419 | | | |
| 12/9/2008 | 14:34:46 | 20.457 | 0.244 | 432.564 | 0.024 | 68.662 | | | |
| 12/9/2008 | 14:34:56 | 20.304 | 0.244 | 398.887 | 0.024 | 68.51 | | | |
| 12/9/2008 | 14:35:06 | 20.213 | 0.274 | 389.744 | 18.437 | 69.267 | | | |
| 12/9/2008 | 14:35:16 | 20.167 | 0.274 | 392.584 | 19.663 | 71.084 | | | |
| 12/9/2008 | 14:35:26 | 20.106 | 0.305 | 455.385 | 2.857 | 72.901 | | | |
| 12/9/2008 | 14:35:36 | 20.152 | 0.213 | 453.59 | 0.317 | 76.811 | | | |
| 12/9/2008 | 14:35:46 | 20.304 | 0.122 | 455.385 | 0.024 | 79.184 | | | |
| 12/9/2008 | 14:35:56 | 20.396 | 0.183 | 431.026 | 0.024 | 78.654 | | | |
| 12/9/2008 | 14:36:06 | 20.602 | 0.213 | 436.41 | 0.024 | 78.857 | | | |
| 12/9/2008 | 14:36:16 | 20.517 | 0.213 | 425.897 | 0.024 | 77.216 | | | |
| 12/9/2008 | 14:36:26 | 20.533 | 0.274 | 437.436 | 0.024 | 74.264 | | | |
| 12/9/2008 | 14:36:36 | 20.457 | 0.398 | 421.026 | 0.024 | 71.614 | | | |
| 12/9/2008 | 14:36:46 | 20.35 | 0.426 | 411.795 | 28.449 | 72.674 | | | |
| 12/9/2008 | 14:36:56 | 20.274 | 0.426 | 403.077 | 21.538 | 84.786 | | | |
| 12/9/2008 | 14:37:06 | 20.198 | 0.368 | 371.026 | 5.495 | 98.943 | | | |
| 12/9/2008 | 14:37:16 | 20.228 | 0.274 | 362.821 | 2.1 | 102.803 | | | |
| 12/9/2008 | 14:37:26 | 20.335 | 0.244 | 358.974 | 0.708 | 103.56 | | | |
| 12/9/2008 | 14:37:36 | 20.426 | 0.213 | 399.231 | 0.024 | 99.548 | | | |
| 12/9/2008 | 14:37:46 | 20.517 | 0.244 | 428.41 | 0.024 | 90.842 | | | |
| 12/9/2008 | 14:37:56 | 20.487 | 0.335 | 459.231 | 0.024 | 75.853 | | | |
| 12/9/2008 | 14:38:06 | 20.411 | 0.398 | 418.974 | 0.024 | 70.252 | | | |
| 12/9/2008 | 14:38:16 | 20.289 | 0.428 | 388.205 | 0.024 | 69.419 | | | |
| 12/9/2008 | 14:38:26 | 20.198 | 0.457 | 385.897 | 18.51 | 68.586 | | | |
| 12/9/2008 | 14:38:36 | 20.137 | 0.274 | 392.564 | 18.291 | 68.359 | | | |
| 12/9/2008 | 14:38:46 | 20.137 | 0.305 | 411.028 | 2.515 | 67.829 | | | |
| 12/9/2008 | 14:38:56 | 20.152 | 0.183 | 402.308 | 0.855 | 69.646 | | | |
| 12/9/2008 | 14:39:06 | 20.243 | 0.091 | 389.231 | 0.293 | 70.554 | | | |
| 12/9/2008 | 14:39:16 | 20.38 | 0.091 | 385.897 | 0.024 | 69.722 | | | |
| 12/9/2008 | 14:39:26 | 20.457 | 0.122 | 439.744 | 0.024 | 68.056 | | | |
| 12/9/2008 | 14:39:36 | 20.617 | 0.091 | 461.795 | 0.024 | 68.208 | | | |
| 12/9/2008 | 14:39:46 | 20.533 | 0.152 | 457.692 | 0.024 | 73.885 | | | |
| 12/9/2008 | 14:39:56 | 20.487 | 0.213 | 408.462 | 0.024 | 80.093 | | | |
| 12/9/2008 | 14:40:06 | 20.335 | 0.213 | 406.154 | 28.894 | 83.575 | | | |
| 12/9/2008 | 14:40:16 | 20.259 | 0.213 | 406.923 | 22.637 | 84.862 | | | |
| 12/9/2008 | 14:40:26 | 20.213 | 0.213 | 420.256 | 6.056 | 83.499 | | | |
| 12/9/2008 | 14:40:36 | 20.259 | 0.122 | 399.744 | 2.344 | 80.244 | | | |
| 12/9/2008 | 14:40:46 | 20.335 | 0.091 | 390.769 | 0.781 | 76.005 | | | |
| 12/9/2008 | 14:40:56 | 20.457 | 0.061 | 368.154 | 0.073 | 74.415 | | | |
| 12/9/2008 | 14:41:06 | 20.502 | 0.061 | 375.385 | 0.024 | 75.778 | | | |
| 12/9/2008 | 14:41:16 | 20.502 | 0.122 | 382.308 | 0.024 | 87.284 | | | |
| 12/9/2008 | 14:41:26 | 20.396 | 0.213 | 382.821 | 0.024 | 103.182 | | | |
| 12/9/2008 | 14:41:36 | 20.274 | 0.244 | 369.487 | 0.024 | 107.421 | | | |
| 12/9/2008 | 14:41:46 | 20.213 | 0.274 | 369.231 | 18.974 | 107.421 | | | |
| 12/9/2008 | 14:41:56 | 20.152 | 0.213 | 383.59 | 19.341 | 102.728 | | | |
| 12/9/2008 | 14:42:06 | 20.121 | 0.244 | 393.59 | 3.492 | 96.369 | | | |
| 12/9/2008 | 14:42:16 | 20.182 | 0.183 | 435.128 | 1.074 | 79.941 | | | |
| 12/9/2008 | 14:42:26 | 20.289 | 0.122 | 451.026 | 0.024 | 71.236 | | | |
| 12/9/2008 | 14:42:36 | 20.396 | 0.091 | 438.974 | 0.024 | 67.98 | | | |
| 12/9/2008 | 14:42:46 | 20.457 | 0.091 | 435.897 | 0.024 | 66.618 | | | |
| 12/9/2008 | 14:42:56 | 20.517 | 0.091 | 402.664 | 0.024 | 68.359 | | | |
| 12/9/2008 | 14:43:06 | 20.533 | 0.122 | 394.103 | 0.024 | 70.024 | | | |
| 12/9/2008 | 14:43:16 | 20.441 | 0.213 | 394.359 | 0.024 | 70.933 | | | |
| 12/9/2008 | 14:43:26 | 20.335 | 0.213 | 390.513 | 31.136 | 70.479 | | | |
| 12/9/2008 | 14:43:36 | 20.274 | 0.213 | 391.282 | 23.518 | 69.722 | | | |
| 12/9/2008 | 14:43:46 | 20.228 | 0.213 | 405.641 | 6.252 | 69.495 | | | |
| 12/9/2008 | 14:43:56 | 20.243 | 0.122 | 400 | 2.393 | 71.766 | | | |
| 12/9/2008 | 14:44:06 | 20.335 | 0.091 | 400.258 | 0.83 | 76.308 | | | |
| 12/9/2008 | 14:44:16 | 20.457 | 0.061 | 404.359 | 0.122 | 78.411 | | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|----------|--------|-------|-----------------------------------|-----------------------------------|-----------------------------------|-------------------------|------------|
| | | % | % | ppm C ₂ H ₆ | ppm C ₂ H ₆ | ppm C ₂ H ₆ | | |
| 12/9/2008 | 14:44:26 | 20.487 | 0.061 | 398.718 | 0.024 | 82.061 | | |
| 12/9/2008 | 14:44:36 | 20.487 | 0.152 | 400.769 | 0.024 | 81.834 | | |
| 12/9/2008 | 14:44:46 | 20.385 | 0.244 | 431.282 | 0.024 | 80.396 | | |
| 12/9/2008 | 14:44:56 | 20.259 | 0.244 | 421.282 | 0.024 | 77.065 | | |
| 12/9/2008 | 14:45:06 | 20.182 | 0.274 | 407.949 | 19.463 | 72.825 | | |
| 12/9/2008 | 14:45:16 | 20.152 | 0.274 | 409.744 | 19.536 | 70.706 | | |
| 12/9/2008 | 14:45:26 | 20.121 | 0.305 | 433.077 | 2.833 | 71.841 | | |
| 12/9/2008 | 14:45:36 | 20.182 | 0.213 | 455.128 | 0.44 | 82.44 | | |
| 12/9/2008 | 14:45:46 | 20.274 | 0.152 | 428.974 | 0.024 | 96.899 | | |
| 12/9/2008 | 14:45:56 | 20.38 | 0.091 | 422.051 | 0.024 | 100.381 | | |
| 12/9/2008 | 14:46:06 | 20.457 | 0.091 | 404.872 | 0.024 | 102.046 | | |
| 12/9/2008 | 14:46:16 | 20.517 | 0.061 | 422.051 | 0.024 | 100.154 | | |
| 12/9/2008 | 14:46:26 | 20.517 | 0.122 | 436.41 | 0.024 | 96.066 | | |
| 12/9/2008 | 14:46:36 | 20.487 | 0.244 | 455.128 | 0.024 | 79.487 | | |
| 12/9/2008 | 14:46:46 | 20.335 | 0.274 | 443.848 | 29.011 | 72.447 | | |
| 12/9/2008 | 14:46:56 | 20.228 | 0.274 | 415.897 | 23.807 | 70.857 | | |
| 12/9/2008 | 14:47:06 | 20.198 | 0.213 | 392.061 | 6.252 | 70.024 | | |
| 12/9/2008 | 14:47:16 | 20.243 | 0.091 | 346.41 | 2.125 | 71.387 | | |
| 12/9/2008 | 14:47:26 | 20.38 | 0.061 | 371.795 | 0.611 | 71.463 | | |
| 12/9/2008 | 14:47:36 | 20.472 | 0.03 | 397.949 | 0.024 | 70.63 | | |
| 12/9/2008 | 14:47:46 | 20.533 | 0.03 | 388.462 | 0.024 | 69.949 | | |
| 12/9/2008 | 14:47:56 | 20.533 | 0.152 | 408.974 | 0.024 | 67.526 | | |
| 12/9/2008 | 14:48:06 | 20.426 | 0.244 | 437.949 | 0.024 | 66.542 | | |
| 12/9/2008 | 14:48:16 | 20.274 | 0.274 | 431.538 | 0.024 | 68.132 | | |
| 12/9/2008 | 14:48:26 | 20.198 | 0.305 | 450.769 | 18.193 | 73.582 | | |
| 12/9/2008 | 14:48:36 | 20.137 | 0.305 | 453.333 | 20.024 | 78.276 | | |
| 12/9/2008 | 14:48:46 | 20.121 | 0.274 | 424.872 | 3.565 | 63.121 | | |
| 12/9/2008 | 14:48:56 | 20.167 | 0.152 | 407.436 | 1.27 | 82.894 | | |
| 12/9/2008 | 14:49:06 | 20.289 | 0.091 | 428.974 | 0.317 | 79.487 | | |
| 12/9/2008 | 14:49:16 | 20.396 | 0.061 | 431.795 | 0.024 | 76.156 | | |
| 12/9/2008 | 14:49:26 | 20.502 | 0.091 | 433.59 | 0.024 | 71.69 | | |
| 12/9/2008 | 14:49:36 | 20.533 | 0.061 | 407.436 | 0.024 | 70.781 | | |
| 12/9/2008 | 14:49:46 | 20.548 | 0.122 | 418.482 | 0.024 | 72.447 | | |
| 12/9/2008 | 14:49:56 | 20.457 | 0.213 | 426.154 | 0.024 | 83.575 | | |
| 12/9/2008 | 14:50:06 | 20.35 | 0.244 | 413.077 | 28.132 | 98.564 | | |
| 12/9/2008 | 14:50:16 | 20.259 | 0.396 | 401.795 | 20.928 | 101.516 | | |
| 12/9/2008 | 14:50:26 | 20.228 | 0.396 | 391.282 | 4.347 | 101.516 | | |
| 12/9/2008 | 14:50:36 | 20.228 | 0.335 | 410.769 | 0.761 | 98.337 | | |
| 12/9/2008 | 14:50:46 | 20.335 | 0.244 | 428.482 | 0.024 | 93.568 | | |
| 12/9/2008 | 14:50:56 | 20.426 | 0.244 | 435.385 | 0.024 | 78.276 | | |
| 12/9/2008 | 14:51:06 | 20.487 | 0.244 | 418.205 | 0.024 | 71.69 | | |
| 12/9/2008 | 14:51:16 | 20.487 | 0.305 | 386.867 | 0.024 | 70.252 | | |
| 12/9/2008 | 14:51:26 | 20.365 | 0.368 | 386.923 | 0.024 | 70.252 | | |
| 12/9/2008 | 14:51:36 | 20.243 | 0.396 | 365.385 | 0.024 | 71.084 | | |
| 12/9/2008 | 14:51:46 | 20.152 | 0.426 | 370.769 | 18.144 | 69.116 | | |
| 12/9/2008 | 14:51:56 | 20.152 | 0.396 | 402.821 | 19.316 | 68.737 | | |
| 12/9/2008 | 14:52:06 | 20.152 | 0.426 | 408.482 | 3.004 | 67.98 | | |
| 12/9/2008 | 14:52:16 | 20.167 | 0.335 | 411.795 | 0.317 | 68.239 | | |
| 12/9/2008 | 14:52:26 | 20.259 | 0.274 | 426.41 | 0.024 | 65.407 | | |
| 12/9/2008 | 14:52:36 | 20.365 | 0.091 | 434.103 | 0.024 | 66.996 | | |
| 12/9/2008 | 14:52:46 | 20.441 | 0.091 | 454.359 | 0.024 | 73.204 | | |
| 12/9/2008 | 14:52:56 | 20.517 | 0.091 | 440 | 0.024 | 78.2 | | |
| 12/9/2008 | 14:53:06 | 20.517 | 0.122 | 461.282 | 0.024 | 81.38 | | |
| 12/9/2008 | 14:53:16 | 20.441 | 0.244 | 445.385 | 0.024 | 81.001 | | |
| 12/9/2008 | 14:53:26 | 20.319 | 0.274 | 461.026 | 30.794 | 81.228 | | |
| 12/9/2008 | 14:53:36 | 20.213 | 0.274 | 439.231 | 24.151 | 77.595 | | |
| 12/9/2008 | 14:53:46 | 20.182 | 0.244 | 398.974 | 6.349 | 75.096 | | |
| 12/9/2008 | 14:53:56 | 20.243 | 0.122 | 372.051 | 2.222 | 74.415 | | |
| 12/9/2008 | 14:54:06 | 20.35 | 0.061 | 362.821 | 0.635 | 75.021 | | |
| 12/9/2008 | 14:54:16 | 20.441 | 0.061 | 400.256 | 0.024 | 82.667 | | |
| 12/9/2008 | 14:54:26 | 20.487 | 0.091 | 426.154 | 0.024 | 98.64 | | |
| 12/9/2008 | 14:54:36 | 20.472 | 0.183 | 407.949 | 0.024 | 103.409 | | |
| 12/9/2008 | 14:54:46 | 20.396 | 0.213 | 362.051 | 0.024 | 107.648 | | |
| 12/9/2008 | 14:54:56 | 20.274 | 0.213 | 377.179 | 0.024 | 102.955 | | |
| 12/9/2008 | 14:55:06 | 20.213 | 0.305 | 411.282 | 16.239 | 96.823 | | |
| 12/9/2008 | 14:55:16 | 20.152 | 0.274 | 444.103 | 18.388 | 79.563 | | |
| 12/9/2008 | 14:55:26 | 20.197 | 0.274 | 429.231 | 3.248 | 72.598 | | |
| 12/9/2008 | 14:55:36 | 20.152 | 0.183 | 380.769 | 1.172 | 70.327 | | |
| 12/9/2008 | 14:55:46 | 20.274 | 0.122 | 398.205 | 0.024 | 67.072 | | |
| 12/9/2008 | 14:55:56 | 20.38 | 0.091 | 390 | 0.024 | 68.965 | | |
| 12/9/2008 | 14:56:06 | 20.472 | 0.091 | 394.103 | 0.024 | 68.813 | | |
| 12/9/2008 | 14:56:16 | 20.533 | 0.03 | 384.615 | 0.024 | 69.797 | | |
| 12/9/2008 | 14:56:26 | 20.548 | 0.091 | 390.513 | 0.024 | 68.889 | | |
| 12/9/2008 | 14:56:36 | 20.426 | 0.213 | 426.41 | 0.024 | 67.223 | | |
| 12/9/2008 | 14:56:46 | 20.304 | 0.274 | 433.59 | 28.596 | 67.223 | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|----------|--------|-------|-----------------------------------|-----------------------------------|-----------------------------------|-------------------------|------------|
| | | % | % | ppm C ₂ H ₆ | ppm C ₂ H ₆ | ppm C ₂ H ₆ | | |
| 12/9/2008 | 14:56:56 | 20.213 | 0.244 | 386.667 | 23.932 | 69.267 | | |
| 12/9/2008 | 14:57:06 | 20.182 | 0.213 | 412.564 | 5.685 | 72.523 | | |
| 12/9/2008 | 14:57:16 | 20.228 | 0.152 | 432.564 | 1.148 | 77.822 | | |
| 12/9/2008 | 14:57:26 | 20.35 | 0.091 | 438.205 | 0.024 | 82.288 | | |
| 12/9/2008 | 14:57:36 | 20.428 | 0.081 | 407.949 | 0.024 | 84.635 | | |
| 12/9/2008 | 14:57:46 | 20.517 | 0.03 | 433.077 | 0.024 | 83.121 | | |
| 12/9/2008 | 14:57:56 | 20.533 | 0.122 | 446.667 | 0.024 | 78.654 | | |
| 12/9/2008 | 14:58:06 | 20.411 | 0.244 | 451.282 | 0.024 | 73.431 | | |
| 12/9/2008 | 14:58:16 | 20.289 | 0.091 | 387.179 | 0.024 | 75.526 | | |
| 12/9/2008 | 14:58:26 | 20.182 | 0.091 | 380 | 16.752 | 74.718 | | |
| 12/9/2008 | 14:58:36 | 20.198 | 0.091 | 430.256 | 18.071 | 80.547 | | |
| 12/9/2008 | 14:58:46 | 20.198 | 0.091 | 388.718 | 3.297 | 99.775 | | |
| 12/9/2008 | 14:58:56 | 20.228 | 0.03 | 395.897 | 0.283 | 103.182 | | |
| 12/9/2008 | 14:59:06 | 20.319 | 0.03 | 392.821 | 0.024 | 103.409 | | |
| 12/9/2008 | 14:59:16 | 20.472 | 0.03 | 368.874 | 0.024 | 99.851 | | |
| 12/9/2008 | 14:59:26 | 20.578 | 0.03 | 405.841 | 0.024 | 94.022 | | |
| 12/9/2008 | 14:59:36 | 20.578 | 0.03 | 432.564 | 0.024 | 79.79 | | |
| 12/9/2008 | 14:59:46 | 20.594 | 0.03 | 403.846 | 0.024 | 71.993 | | |
| 12/9/2008 | 14:59:56 | 20.487 | 0.091 | 430.256 | 0.024 | 67.451 | | |
| 12/9/2008 | 15:00:06 | 20.335 | 0.091 | 420 | 27.326 | 67.299 | | |
| 12/9/2008 | 15:00:16 | 20.259 | 0.081 | 363.59 | 22.637 | 69.949 | | |
| 12/9/2008 | 15:00:26 | 20.228 | 0.061 | 410 | 4.664 | 68.132 | | |
| 12/9/2008 | 15:00:36 | 20.289 | 0.03 | 389.744 | 1.856 | 70.252 | | |
| 12/9/2008 | 15:00:46 | 20.426 | 0.03 | 398.718 | 0.269 | 69.495 | | |
| 12/9/2008 | 15:00:56 | 20.533 | 0.03 | 432.051 | 0.024 | 66.618 | | |
| 12/9/2008 | 15:01:06 | 20.563 | 0.03 | 442.821 | 0.024 | 66.315 | | |
| 12/9/2008 | 15:01:16 | 20.578 | 0.03 | 418.718 | 0.024 | 89.57 | | |
| 12/9/2008 | 15:01:26 | 20.487 | 0.03 | 415.897 | 0.024 | 74.339 | | |
| 12/9/2008 | 15:01:36 | 20.38 | 0.061 | 407.438 | 0.024 | 78.654 | | |
| 12/9/2008 | 15:01:46 | 20.274 | 0.091 | 382.051 | 17.265 | 82.081 | | |
| 12/9/2008 | 15:01:56 | 20.198 | 0.081 | 395.641 | 20.269 | 82.212 | | |
| 12/9/2008 | 15:02:06 | 20.228 | 0.091 | 441.026 | 3.126 | 79.714 | | |
| 12/9/2008 | 15:02:16 | 20.228 | 0.03 | 446.923 | 0.366 | 74.842 | | |
| 12/9/2008 | 15:02:26 | 20.35 | 0.03 | 441.538 | 0.024 | 71.009 | | |
| 12/9/2008 | 15:02:36 | 20.487 | 0.03 | 411.795 | 0.024 | 69.797 | | |
| 12/9/2008 | 15:02:46 | 20.563 | 0.03 | 410.769 | 0.024 | 70.403 | | |
| 12/9/2008 | 15:02:56 | 20.609 | 0.03 | 444.872 | 0.024 | 80.244 | | |
| 12/9/2008 | 15:03:06 | 20.624 | 0.03 | 427.179 | 0.024 | 96.217 | | |
| 12/9/2008 | 15:03:16 | 20.609 | 0.081 | 421.795 | 0.024 | 98.488 | | |
| 12/9/2008 | 15:03:26 | 20.35 | 0.091 | 423.59 | 24.615 | 99.7 | | |
| 12/9/2008 | 15:03:36 | 20.259 | 0.122 | 423.333 | 21.343 | 86.444 | | |
| 12/9/2008 | 15:03:46 | 20.213 | 0.081 | 428.718 | 4.591 | 83.418 | | |
| 12/9/2008 | 15:03:56 | 20.289 | 0.03 | 447.179 | 1.001 | 77.595 | | |
| 12/9/2008 | 15:04:06 | 20.38 | 0.03 | 446.923 | 0.024 | 69.116 | | |
| 12/9/2008 | 15:04:16 | 20.487 | 0.03 | 431.026 | 0.024 | 67.072 | | |
| 12/9/2008 | 15:04:26 | 20.563 | 0.03 | 423.846 | 0.024 | 66.921 | | |
| 12/9/2008 | 15:04:36 | 20.563 | 0.03 | 393.333 | 0.024 | 68.985 | | |
| 12/9/2008 | 15:04:46 | 20.457 | 0.061 | 372.564 | 0.024 | 68.985 | | |
| 12/9/2008 | 15:04:56 | 20.35 | 0.081 | 384.358 | 0.024 | 68.343 | | |
| 12/9/2008 | 15:05:06 | 20.259 | 0.081 | 381.795 | 17.314 | 68.813 | | |
| 12/9/2008 | 15:05:16 | 20.213 | 0.091 | 398.974 | 19.536 | 87.072 | | |
| 12/9/2008 | 15:05:26 | 20.182 | 0.122 | 428.974 | 2.442 | 66.315 | | |
| 12/9/2008 | 15:05:36 | 20.182 | 0.03 | 425.385 | 0.122 | 87.828 | | |
| 12/9/2008 | 15:05:46 | 20.472 | 0.03 | 446.923 | 0 | 72.144 | | |
| 12/9/2008 | 15:05:56 | 20.894 | 0.03 | 440.513 | 0.024 | 79.109 | | |
| 12/9/2008 | 15:06:06 | 20.655 | 0.03 | 407.692 | 0.024 | 84.408 | | |
| 12/9/2008 | 15:06:16 | 20.594 | 0.03 | 378.231 | 0.024 | 84.882 | | |
| 12/9/2008 | 15:06:26 | 20.594 | 0.03 | 419.231 | 0.024 | 82.742 | | |
| 12/9/2008 | 15:06:36 | 20.502 | 0.03 | 407.179 | 0.024 | 77.585 | | |
| 12/9/2008 | 15:06:46 | 20.35 | 0.061 | 395.128 | 24.347 | 74.945 | | |
| 12/9/2008 | 15:06:56 | 20.289 | 0.061 | 372.051 | 22.173 | 74.567 | | |
| 12/9/2008 | 15:07:06 | 19.817 | 1.889 | 392.821 | 5.104 | 73.582 | | |
| 12/9/2008 | 15:07:16 | 15.416 | 5.805 | 428.923 | 1.221 | 80.774 | | |
| 12/9/2008 | 15:07:26 | 9.718 | 7.494 | 406.923 | 0.024 | 97.429 | | |
| 12/9/2008 | 15:07:36 | 5.423 | 8.743 | 359.231 | 0.024 | 102.652 | | |
| 12/9/2008 | 15:07:46 | 2.488 | 9.292 | 358.718 | 0.024 | 102.803 | | |
| 12/9/2008 | 15:07:56 | 0.777 | 9.586 | 430.256 | 0.024 | 97.883 | | |
| 12/9/2008 | 15:08:06 | 0.015 | 9.718 | 421.026 | 0.024 | 94.779 | | |
| 12/9/2008 | 15:08:16 | 0.015 | 9.688 | 438.974 | 0.024 | 79.639 | | |
| 12/9/2008 | 15:08:26 | 0.015 | 9.748 | 430 | 11.206 | 71.69 | | |
| 12/9/2008 | 15:08:36 | 0.018 | 9.779 | 389.231 | 22.247 | 69.873 | | |
| 12/9/2008 | 15:08:46 | 0.015 | 9.779 | 377.949 | 3.761 | 68.737 | | |
| 12/9/2008 | 15:08:56 | 0.015 | 9.87 | 345.385 | 1.172 | 69.873 | | |
| 12/9/2008 | 15:09:06 | 0.015 | 9.992 | 346.41 | 0.22 | 69.267 | | |
| 12/9/2008 | 15:09:16 | 0.015 | 9.992 | 377.436 | 0.024 | 68.965 | | |

End Run #2

Zero drift check 0.00%

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|----------|--------|--------|-----------------------------------|-----------------------------------|-----------------------------------|-------------------------|------------|
| | | % | % | ppm C ₂ H ₆ | ppm C ₂ H ₆ | ppm C ₂ H ₆ | | |
| 12/9/2008 | 15:09:26 | 0.015 | 9.992 | 398.718 | 0.024 | 68.359 | | |
| 12/9/2008 | 15:09:36 | 0.015 | 10.023 | 398.41 | 0.024 | 66.996 | | |
| 12/9/2008 | 15:09:46 | 0.015 | 10.023 | 421.538 | 0.024 | 65.558 | | |
| 12/9/2008 | 15:09:56 | 0.015 | 9.992 | 431.282 | 0.024 | 66.694 | | |
| 12/9/2008 | 15:10:06 | 0.015 | 8.103 | 444.872 | 21.245 | 70.554 | | |
| 12/9/2008 | 15:10:16 | 2.315 | 4.417 | 448.974 | 24.444 | 74.339 | | |
| 12/9/2008 | 15:10:26 | 8.225 | 1.918 | 440.769 | 5.588 | 76.156 | | |
| 12/9/2008 | 15:10:36 | 13.13 | 0.823 | 440.513 | 1.612 | 75.324 | | |
| 12/9/2008 | 15:10:46 | 16.161 | 0.366 | 445.841 | 0.171 | 76.383 | | |
| 12/9/2008 | 15:10:56 | 16.096 | 0.091 | 436.887 | 0.024 | 73.858 | | |
| 12/9/2008 | 15:11:06 | 19.116 | 0.03 | 428.462 | 0.024 | 69.04 | | |
| 12/9/2008 | 15:11:16 | 19.802 | 0.03 | 406.385 | 0.024 | 68.662 | | |
| 12/9/2008 | 15:11:26 | 20.121 | 0.03 | 400.513 | 0.024 | 69.873 | | |
| 12/9/2008 | 15:11:36 | 20.319 | 0.03 | 418.718 | 0.024 | 78.049 | | |
| 12/9/2008 | 15:11:46 | 20.457 | 0.03 | 417.849 | 10.847 | 93.795 | | |
| 12/9/2008 | 15:11:56 | 20.548 | 0.03 | 420 | 20.293 | 98.337 | | |
| 12/9/2008 | 15:12:06 | 20.624 | 0.03 | 430.513 | 2.837 | 100.002 | | |
| 12/9/2008 | 15:12:16 | 20.67 | 0.03 | 438.205 | 0.415 | 97.126 | | |
| 12/9/2008 | 15:12:26 | 20.624 | 0.03 | 424.103 | 0.024 | 94.476 | | |
| 12/9/2008 | 15:12:36 | 20.868 | 0.03 | 414.103 | 0.024 | 79.033 | | |
| 12/9/2008 | 15:12:46 | 20.929 | 0.03 | 398.205 | 0.024 | 71.387 | | |
| 12/9/2008 | 15:12:56 | 20.974 | 0.03 | 371.026 | 0.024 | 70.327 | | |
| 12/9/2008 | 15:13:06 | 20.944 | 0.03 | 371.026 | 0.024 | 67.223 | | |
| 12/9/2008 | 15:13:16 | 20.822 | 0.03 | 370.769 | 0.024 | 68.737 | | |
| 12/9/2008 | 15:13:26 | 20.822 | 0.03 | 358.231 | 17.387 | 71.463 | | |
| 12/9/2008 | 15:13:36 | 20.868 | 0.03 | 367.436 | 21.392 | 73.507 | | |
| 12/9/2008 | 15:13:46 | 20.837 | 0.03 | 380 | 6.299 | 72.523 | | |
| 12/9/2008 | 15:13:56 | 20.761 | 0.03 | 385.641 | 1.856 | 70.327 | | |
| 12/9/2008 | 15:14:06 | 20.776 | 0.03 | 384.359 | 0.44 | 68.737 | | |
| 12/9/2008 | 15:14:16 | 20.685 | 0.03 | 376.887 | 0.024 | 69.495 | | |
| 12/9/2008 | 15:14:26 | 20.274 | 0.03 | 413.077 | 0.024 | 72.295 | | |
| 12/9/2008 | 15:14:36 | 16.161 | 0.03 | 440.513 | 0.024 | 72.901 | | |
| 12/9/2008 | 15:14:46 | 9.794 | 0.03 | 443.59 | 0.024 | 74.037 | | |
| 12/9/2008 | 15:14:56 | 5.072 | 0.03 | 437.436 | 0.024 | 74.491 | | |
| 12/9/2008 | 15:15:06 | 2.148 | 0.03 | 436.41 | 10.452 | 75.475 | | |
| 12/9/2008 | 15:15:16 | 0.487 | 0.03 | 410 | 21.245 | 74.339 | | |
| 12/9/2008 | 15:15:26 | 0.015 | 0.03 | 387.436 | 3.916 | 72.447 | | |
| 12/9/2008 | 15:15:36 | 0.015 | 0.03 | 375.641 | 1.001 | 71.69 | | |
| 12/9/2008 | 15:15:46 | 0.015 | 0.03 | 413.846 | 0.024 | 71.084 | | |
| 12/9/2008 | 15:15:56 | 0.015 | 0.03 | 430.769 | 0.024 | 77.897 | | |
| 12/9/2008 | 15:16:06 | 0.015 | 0.03 | 389.231 | 0.024 | 95.839 | | |
| 12/9/2008 | 15:16:16 | 0.015 | 0.03 | 362.821 | 0.024 | 100.305 | | |
| 12/9/2008 | 15:16:26 | 0.015 | 0.03 | 370 | 0.024 | 101.668 | | |
| 12/9/2008 | 15:16:36 | 0.015 | 0.03 | 418.462 | 0.024 | 97.807 | | |
| 12/9/2008 | 15:16:46 | 6.839 | 0.03 | 417.692 | 4.811 | 96.52 | | |
| 12/9/2008 | 15:16:56 | 15.704 | 0.03 | 390 | 27.253 | 81.683 | | |
| 12/9/2008 | 15:17:06 | 19.345 | 0.03 | 393.333 | 6.154 | 72.901 | | |
| 12/9/2008 | 15:17:16 | 21.005 | 0.03 | 412.308 | 1.685 | 68.965 | | |
| 12/9/2008 | 15:17:26 | 21.708 | 0.03 | 419.231 | 0.024 | 64.877 | | |
| 12/9/2008 | 15:17:36 | 22.102 | 0.03 | 377.692 | 0.024 | 66.164 | | |
| 12/9/2008 | 15:17:46 | 22.208 | 0.03 | 350.513 | 0.024 | 69.267 | | |
| 12/9/2008 | 15:17:56 | 22.223 | 0.03 | 383.077 | 0.024 | 28.161 | | |
| 12/9/2008 | 15:18:06 | 22.264 | 0.03 | 412.821 | 0.024 | 20.591 | | |
| 12/9/2008 | 15:18:16 | 22.3 | 0.03 | 415.385 | 0.024 | 17.033 | | |
| 12/9/2008 | 15:18:26 | 22.284 | 0.03 | 384.103 | 0.024 | 16.352 | | |
| 12/9/2008 | 15:18:36 | 22.3 | 0.03 | 381.026 | 32.869 | 16.654 | | |
| 12/9/2008 | 15:18:46 | 22.3 | 0.03 | 418.718 | 3.541 | 15.218 | | |
| 12/9/2008 | 15:18:56 | 17.761 | 0.03 | 441.538 | 0.244 | 12.889 | | |
| 12/9/2008 | 15:19:06 | 17.745 | 0.03 | 425.385 | 0.024 | 12.587 | | |
| 12/9/2008 | 15:19:16 | 17.715 | 0.03 | 387.949 | 0.024 | 13.551 | | |
| 12/9/2008 | 15:19:26 | 17.7 | 0.03 | 425.841 | 0.024 | 13.702 | | |
| 12/9/2008 | 15:19:36 | 17.73 | 0.03 | 461.026 | 0.024 | 12.188 | | |
| 12/9/2008 | 15:19:46 | 17.73 | 0.03 | 461.282 | 0.024 | 10.825 | | |
| 12/9/2008 | 15:19:56 | 17.715 | 0.03 | 402.564 | 0.024 | 10.977 | | |
| 12/9/2008 | 15:20:06 | 17.7 | 0.03 | 372.051 | 0.024 | 12.339 | | |
| 12/9/2008 | 15:20:16 | 17.715 | 0.03 | 381.538 | 31.258 | 12.112 | | |
| 12/9/2008 | 15:20:26 | 17.715 | 0.03 | 420.266 | 5.201 | 9.236 | | |
| 12/9/2008 | 15:20:36 | 17.715 | 0.03 | 377.179 | 1.807 | 10.068 | | |
| 12/9/2008 | 15:20:46 | 17.7 | 0.03 | 362.564 | 0.582 | 10.977 | | |
| 12/9/2008 | 15:20:56 | 17.715 | 0.03 | 399.744 | 0.024 | 10.144 | | |
| 12/9/2008 | 15:21:06 | 17.7 | 0.03 | 428.923 | 0.024 | 8.706 | | |
| 12/9/2008 | 15:21:16 | 17.7 | 0.03 | 432.564 | 0.024 | 8.554 | | |
| 12/9/2008 | 15:21:26 | 17.7 | 0.03 | 446.923 | 0.024 | 8.554 | | |
| 12/9/2008 | 15:21:36 | 17.7 | 0.03 | 428.974 | 0.024 | 8.479 | | |
| 12/9/2008 | 15:21:46 | 17.7 | 0.03 | 426.41 | 0.024 | 8.327 | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|----------|--------|-------|-----------------------------------|-----------------------------------|-----------------------------------|-------------------------|------------|
| | | % | % | ppm C ₂ H ₆ | ppm C ₂ H ₆ | ppm C ₂ H ₆ | | |
| 12/9/2008 | 15:21:06 | 17.7 | 0.03 | 396.41 | 33.187 | 8.327 | | 0.14% |
| 12/9/2008 | 15:22:06 | 17.7 | 0.03 | 392.051 | 3.223 | 8.327 | | |
| 12/9/2008 | 15:22:16 | 17.684 | 0.03 | 411.538 | 0.513 | 8.403 | | |
| 12/9/2008 | 15:22:26 | 17.684 | 0.03 | 416.41 | 0.024 | 8.63 | | |
| 12/9/2008 | 15:22:36 | 17.684 | 0.03 | 408.205 | 0.024 | 9.008 | | |
| 12/9/2008 | 15:22:46 | 17.684 | 0.03 | 402.051 | 0.024 | 9.009 | | |
| 12/9/2008 | 15:22:56 | 17.669 | 0.03 | 398.667 | 0.024 | 9.311 | | |
| 12/9/2008 | 15:23:06 | 17.669 | 0.03 | 420.256 | 0.024 | 10.825 | | |
| 12/9/2008 | 15:23:16 | 17.669 | 0.03 | 410 | 0.024 | 60.107 | | |
| 12/9/2008 | 15:23:26 | 17.654 | 0.03 | 413.077 | 0.024 | 66.845 | | |
| 12/9/2008 | 15:23:36 | 17.669 | 0.03 | 388.41 | 34.066 | 61.773 | | |
| 12/9/2008 | 15:23:46 | 17.669 | 0.03 | 423.077 | 6.74 | 64.195 | | |
| 12/9/2008 | 15:23:56 | 17.669 | 0.03 | 427.949 | 2.32 | 70.327 | | |
| 12/9/2008 | 15:24:06 | 17.654 | 0.03 | 404.103 | 0.708 | 77.14 | | |
| 12/9/2008 | 15:24:16 | 17.654 | 0.03 | 373.077 | 0.024 | 79.487 | | |
| 12/9/2008 | 15:24:26 | 17.654 | 0.03 | 379.231 | 0.024 | 76.308 | | |
| 12/9/2008 | 15:24:36 | 17.654 | 0.03 | 388.482 | 0.024 | 76.232 | | |
| 12/9/2008 | 15:24:46 | 17.654 | 0.03 | 385.897 | 0.024 | 76.686 | | |
| 12/9/2008 | 15:24:56 | 17.654 | 0.03 | 379.487 | 0.024 | 76.913 | | |
| 12/9/2008 | 15:25:06 | 17.654 | 0.03 | 386.154 | 0.024 | 76.988 | | |
| 12/9/2008 | 15:25:16 | 17.654 | 0.03 | 393.333 | 31.282 | 75.626 | | |
| 12/9/2008 | 15:25:26 | 17.654 | 0.03 | 388.482 | 3.394 | 75.929 | | |
| 12/9/2008 | 15:25:36 | 17.654 | 0.03 | 421.795 | 0.684 | 76.811 | | |
| 12/9/2008 | 15:25:46 | 17.669 | 0.03 | 446.718 | 0.024 | 75.929 | | |
| 12/9/2008 | 15:25:56 | 19.116 | 1.279 | 491.282 | 99.951 | 95.309 | | |
| 12/9/2008 | 15:26:06 | 17.654 | 0.03 | 435.897 | 12.063 | 75.096 | | |
| 12/9/2008 | 15:26:16 | 17.654 | 0.03 | 401.538 | 29.304 | 73.204 | | |
| 12/9/2008 | 15:26:26 | 17.654 | 0.03 | 405.897 | 30.745 | 73.355 | | |
| 12/9/2008 | 15:26:36 | 17.639 | 0.03 | 388.205 | 31.697 | 34.293 | | |
| 12/9/2008 | 15:26:46 | 17.639 | 0.03 | 404.872 | 32.063 | 1.363 | | |
| 12/9/2008 | 15:26:56 | 17.639 | 0.03 | 392.308 | 29.28 | 0.757 | | |
| 12/9/2008 | 15:27:06 | 17.639 | 0.03 | 405.385 | 26.569 | 0.227 | | |
| 12/9/2008 | 15:27:16 | 17.654 | 0.03 | 430 | 24.615 | 0.076 | | |
| 12/9/2008 | 15:27:26 | 17.654 | 0.03 | 444.359 | 24.444 | 0.076 | | |
| 12/9/2008 | 15:27:36 | 17.639 | 0.03 | 447.949 | 24.957 | 0.076 | | |
| 12/9/2008 | 15:27:46 | 17.654 | 0.03 | 452.308 | 24.591 | 0.076 | | |
| 12/9/2008 | 15:27:56 | 17.623 | 0.03 | 390.513 | 25.128 | 0.076 | | |
| 12/9/2008 | 15:28:06 | 17.623 | 0.03 | 429.231 | 25.617 | 0.076 | | |
| 12/9/2008 | 15:28:16 | 17.623 | 0.03 | 421.026 | 25.446 | 0.076 | | |
| 12/9/2008 | 15:28:26 | 17.639 | 0.03 | 431.795 | 24.786 | 0.076 | | |
| 12/9/2008 | 15:28:36 | 17.639 | 0.03 | 415.128 | 24.64 | 0.076 | | |
| 12/9/2008 | 15:28:46 | 17.623 | 0.03 | 409.744 | 2.002 | 0.076 | | |
| 12/9/2008 | 15:28:56 | 17.593 | 0.03 | 388.41 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:29:06 | 17.593 | 0.03 | 374.359 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:29:16 | 17.562 | 0.03 | 384.872 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:29:26 | 17.547 | 0.03 | 397.179 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:29:36 | 17.582 | 0.03 | 414.103 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:29:46 | 17.582 | 0.03 | 414.359 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:29:56 | 17.578 | 0.03 | 406.667 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:30:06 | 17.593 | 0.03 | 135.641 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:30:16 | 17.593 | 0.03 | 387.718 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:30:26 | 17.593 | 0.03 | 24.615 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:30:36 | 17.593 | 0.03 | 18.462 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:30:46 | 17.608 | 0.03 | 15.128 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:30:56 | 17.608 | 0.03 | 11.028 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:31:06 | 17.593 | 0.03 | 8.718 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:31:16 | 17.593 | 0.03 | 9.487 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:31:26 | 17.593 | 0.03 | 10 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:31:36 | 17.578 | 0.03 | 6.923 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:31:46 | 17.582 | 0.03 | 16.41 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:31:56 | 17.578 | 0.03 | 13.848 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:32:06 | 17.578 | 0.03 | 7.438 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:32:16 | 17.562 | 0.03 | 8.923 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:32:26 | 17.578 | 0.03 | 0.258 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:32:36 | 17.582 | 0.03 | 0.258 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:32:46 | 17.582 | 0.03 | 1.028 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:32:56 | 17.562 | 0.03 | 0.258 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:33:06 | 17.547 | 0.03 | 5.641 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:33:16 | 17.582 | 0.03 | 10.258 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:33:26 | 17.582 | 0.03 | 14.815 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:33:36 | 17.547 | 0.03 | 8.718 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:33:46 | 17.547 | 0.03 | 9.231 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:33:56 | 17.582 | 0.03 | 203.333 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:34:06 | 17.547 | 0.03 | 353.077 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:34:16 | 17.532 | 0.03 | 359.487 | 0.024 | 0.076 | | |

Yellow, highlighted data represents calibrations.

RAW TEST DATA FROM ATC DATA LOGGER

| Date | Time | O2 | CO2 | RTO Inlet | RTO Outlet | Baghouse | Calibration Comments | Error % |
|-----------|----------|--------|------|--|--|--|---|------------|
| | | % | % | VOC 3 ppm C ₂ H ₆ | VOC 1 ppm C ₂ H ₆ | VOC 2 ppm C ₂ H ₆ | | |
| 12/9/2008 | 15:34:26 | 17.547 | 0.03 | 358.462 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:34:36 | 17.547 | 0.03 | 360 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:34:46 | 17.562 | 0.03 | 355.641 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:34:56 | 17.562 | 0.03 | 401.795 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:35:06 | 17.562 | 0.03 | 463.846 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:35:16 | 17.517 | 0.03 | 477.692 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:35:26 | 17.562 | 0.03 | 503.077 | 0.024 | 0.076 | Post-test mid range calibration drift check | |
| 12/9/2008 | 15:35:36 | 17.547 | 0.03 | 507.436 | 0.024 | 0.076 | 0.25% | |
| 12/9/2008 | 15:35:46 | 17.562 | 0.03 | 508.923 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:35:56 | 17.547 | 0.03 | 515.897 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:36:06 | 17.502 | 0.03 | 512.82 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:36:16 | 17.502 | 0.03 | 505.897 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:36:26 | 17.456 | 0.03 | 513.846 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:36:36 | 17.471 | 0.03 | 505.128 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:36:46 | 17.502 | 0.03 | 518.462 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:36:56 | 17.486 | 0.03 | 145.641 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:37:06 | 17.486 | 0.03 | 8.205 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:37:16 | 17.471 | 0.03 | 5.385 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:37:26 | 17.456 | 0.03 | 4.615 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:37:36 | 17.425 | 0.03 | 3.077 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:37:46 | 17.425 | 0.03 | 3.077 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:37:56 | 17.425 | 0.03 | 3.077 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:38:06 | 17.425 | 0.03 | 2.821 | 0.024 | 0.076 | | |
| 12/9/2008 | 15:38:16 | 17.41 | 0.03 | 2.308 | 0.024 | 0.076 | | |

Yellow, highlighted data represents calibrations.

Styrene Response Factor Determinations

VOC 1 VOC 2

| | | | | | |
|------------|----------|-------|-------|---------|----------------------------|
| 11/10/2008 | 15:37:05 | 0.012 | 0.024 | 1.665 | |
| 11/10/2008 | 15:37:15 | 0 | 0.024 | 0.076 | |
| 11/10/2008 | 15:37:25 | 0.012 | 0.024 | 0.076 | |
| 11/10/2008 | 15:37:35 | 0.012 | 0.024 | 0.076 | |
| 11/10/2008 | 15:37:45 | 0.012 | 0.024 | 285.7 | |
| 11/10/2008 | 15:37:55 | 0.012 | 0.024 | 296.601 | |
| 11/10/2008 | 15:38:05 | 0.012 | 0.024 | 298.493 | |
| 11/10/2008 | 15:38:15 | 0.012 | 0.024 | 299.25 | |
| 11/10/2008 | 15:38:25 | 0 | 0.024 | 300.007 | High range calibration gas |
| 11/10/2008 | 15:38:35 | 0.012 | 0.024 | 300.689 | |
| 11/10/2008 | 15:38:45 | 0 | 0.024 | 300.764 | |
| 11/10/2008 | 15:38:55 | 0.012 | 0.024 | 301.748 | |
| 11/10/2008 | 15:39:05 | 0.012 | 0.024 | 152.237 | |
| 11/10/2008 | 15:39:15 | 0.012 | 0.024 | 151.707 | |
| 11/10/2008 | 15:39:25 | 0.012 | 0.024 | 151.631 | Mid range calibration gas |
| 11/10/2008 | 15:39:35 | 0.012 | 0.024 | 151.328 | |
| 11/10/2008 | 15:39:45 | 0.012 | 0.024 | 151.404 | |
| 11/10/2008 | 15:39:55 | 0.012 | 0.024 | 75.324 | |
| 11/10/2008 | 15:40:05 | 0.012 | 0.024 | 74.794 | Low range calibration gas |
| 11/10/2008 | 15:40:15 | 0.012 | 0.024 | 74.567 | |
| 11/10/2008 | 15:40:25 | 0.012 | 0.024 | 74.415 | |
| 11/10/2008 | 15:40:35 | 0.012 | 0.024 | 74.491 | |
| 11/10/2008 | 15:40:45 | 0 | 0.024 | 2.725 | |
| 11/10/2008 | 15:40:55 | 0.012 | 0.024 | 0.076 | |
| 11/10/2008 | 15:41:05 | 0.012 | 0.024 | 0.076 | |
| 11/10/2008 | 15:41:15 | 0.012 | 0.024 | 0.076 | Zero gas |
| 11/10/2008 | 15:41:25 | 0.012 | 0.024 | 0.076 | |
| 11/10/2008 | 15:41:35 | 0.012 | 0.024 | 0.076 | |
| 11/10/2008 | 15:41:45 | 0.012 | 0.024 | 4.164 | |
| 11/10/2008 | 15:41:55 | 0.012 | 0.024 | 145.197 | |
| 11/10/2008 | 15:42:05 | 0.012 | 0.024 | 152.918 | |
| 11/10/2008 | 15:42:15 | 0 | 0.024 | 154.811 | |
| 11/10/2008 | 15:42:25 | 0.012 | 0.024 | 156.325 | |
| 11/10/2008 | 15:42:35 | 0.012 | 0.024 | 157.309 | |
| 11/10/2008 | 15:42:45 | 0.012 | 0.024 | 157.612 | |
| 11/10/2008 | 15:42:55 | 0.012 | 0.024 | 157.99 | |
| 11/10/2008 | 15:43:05 | 0.012 | 0.024 | 158.293 | |
| 11/10/2008 | 15:43:15 | 0 | 0.024 | 158.672 | |
| 11/10/2008 | 15:43:25 | 0 | 0.024 | 158.672 | |
| 11/10/2008 | 15:43:35 | 0.012 | 0.024 | 159.201 | |
| 11/10/2008 | 15:43:45 | 0.012 | 0.024 | 159.201 | |
| 11/10/2008 | 15:43:55 | 0.012 | 0.024 | 159.277 | |
| 11/10/2008 | 15:44:05 | 0.012 | 0 | 159.353 | |
| 11/10/2008 | 15:44:15 | 0.012 | 0.024 | 159.58 | |
| 11/10/2008 | 15:44:25 | 0 | 0.024 | 159.731 | |
| 11/10/2008 | 15:44:35 | 0 | 0.024 | 159.277 | |
| 11/10/2008 | 15:44:45 | 0.012 | 0.024 | 159.656 | |
| 11/10/2008 | 15:44:55 | 0.012 | 0.024 | 159.656 | |

Styrene Response Factor Determinations

| | | VOC 1 | VOC 2 | |
|------------|----------|-------|-------|--|
| 11/10/2008 | 15:45:05 | 0 | 0.024 | 160.034 |
| 11/10/2008 | 15:45:15 | 0.012 | 0.024 | 160.034 |
| 11/10/2008 | 15:45:25 | 0.012 | 0.024 | 159.958 |
| 11/10/2008 | 15:45:35 | 0 | 0.024 | 160.186 |
| 11/10/2008 | 15:45:45 | 0.012 | 0.024 | 160.186 |
| 11/10/2008 | 15:45:55 | 0 | 0.024 | 160.261 |
| 11/10/2008 | 15:46:05 | 0.012 | 0.024 | 160.034 |
| 11/10/2008 | 15:46:15 | 0.012 | 0.024 | 160.186 |
| 11/10/2008 | 15:46:25 | 0.012 | 0.024 | 160.413 |
| 11/10/2008 | 15:46:35 | 0.012 | 0.024 | 160.488 |
| 11/10/2008 | 15:46:45 | 0.012 | 0.024 | 160.413 49.2 ppm styrene |
| 11/10/2008 | 15:46:55 | 0 | 0.024 | 160.337 |
| 11/10/2008 | 15:47:05 | 0.012 | 0.024 | 160.186 |
| 11/10/2008 | 15:47:15 | 0 | 0.024 | 160.034 |
| 11/10/2008 | 15:47:25 | 0 | 0.024 | 159.958 |
| 11/10/2008 | 15:47:35 | 0.012 | 0.024 | 19.531 |
| 11/10/2008 | 15:47:45 | 0.012 | 0.024 | 3.179 |
| 11/10/2008 | 15:47:55 | 0.012 | 0.024 | 0.303 |
| 11/10/2008 | 15:48:05 | 0 | 0.024 | 0.076 |
| 11/10/2008 | 15:48:15 | 0.012 | 0.024 | 0.076 |
| 11/10/2008 | 15:48:25 | 0.012 | 0.024 | 183.653 |
| 11/10/2008 | 15:48:35 | 0.012 | 0.024 | 173.585 |
| 11/10/2008 | 15:48:45 | 0 | 0.024 | 170.632 |
| 11/10/2008 | 15:48:55 | 0 | 0.024 | 168.134 |
| 11/10/2008 | 15:49:05 | 0.012 | 0.024 | 165.863 |
| 11/10/2008 | 15:49:15 | 0 | 0.024 | 164.198 |
| 11/10/2008 | 15:49:25 | 0.012 | 0.024 | 162.835 |
| 11/10/2008 | 15:49:35 | 0.012 | 0.024 | 161.7 |
| 11/10/2008 | 15:49:45 | 0.012 | 0.024 | 161.018 |
| 11/10/2008 | 15:49:55 | 0.012 | 0.024 | 160.186 |
| 11/10/2008 | 15:50:05 | 0.012 | 0.024 | 159.731 |
| 11/10/2008 | 15:50:15 | 0.012 | 0.024 | 158.899 |
| 11/10/2008 | 15:50:25 | 0.012 | 0.024 | 158.596 |
| 11/10/2008 | 15:50:35 | 0.012 | 0.024 | 157.99 |
| 11/10/2008 | 15:50:45 | 0.012 | 0.024 | 157.46 |
| 11/10/2008 | 15:50:55 | 0.012 | 0.024 | 157.006 |
| 11/10/2008 | 15:51:05 | 0.012 | 0.024 | 150.42 Mid range calibration drift check |
| 11/10/2008 | 15:51:15 | 0.012 | 0.024 | 0.37% |
| 11/10/2008 | 15:51:25 | 0.012 | 0.024 | 148.83 |
| 11/10/2008 | 15:51:35 | 0.012 | 0.024 | 143.758 |
| 11/10/2008 | 15:51:45 | 0 | 0.024 | 5.299 |
| 11/10/2008 | 15:51:55 | 0.012 | 0.024 | 2.195 |
| 11/10/2008 | 15:52:05 | 0.012 | 0.024 | 1.514 |
| 11/10/2008 | 15:52:15 | 0.012 | 0.024 | 0.908 |
| 11/10/2008 | 15:52:25 | 0.012 | 0.024 | 0.681 |
| 11/10/2008 | 15:52:35 | 0.012 | 0.024 | 0.076 |
| 11/10/2008 | 15:52:45 | 0.012 | 0.024 | 0.076 |
| 11/10/2008 | 15:52:55 | 0.012 | 0.024 | 0.076 |
| 11/10/2008 | 15:53:05 | 0.012 | 0.024 | 0.076 Zero calibration drift check |
| | | | | 0.02% |

Styrene Response Factor Determinations

| | | VOC 1 | VOC 2 | |
|------------|----------|-------|---------|----------------------------------|
| 11/10/2008 | 15:53:15 | 0 | 0.024 | 0.076 |
| 11/10/2008 | 15:53:25 | 0 | 0.024 | 0.076 |
| 11/10/2008 | 15:53:35 | 0.012 | 0.024 | 0.076 |
| 11/10/2008 | 15:53:45 | 0.012 | 0.024 | 0.076 |
| 11/10/2008 | 15:53:55 | 0.012 | 0.024 | 0.076 |
| 11/10/2008 | 15:54:05 | 0.012 | 0.024 | 0.076 |
| 11/10/2008 | 16:05:01 | 0.012 | 0.073 | 0.076 |
| 11/10/2008 | 16:05:11 | 0.012 | 0.073 | 0.076 |
| 11/10/2008 | 16:05:21 | 0.012 | 0.073 | 0.076 |
| 11/10/2008 | 16:05:31 | 0 | 0.073 | 0.076 |
| 11/10/2008 | 16:05:41 | 0.012 | 300 | 0.076 |
| 11/10/2008 | 16:05:51 | 0.012 | 300 | 0.076 |
| 11/10/2008 | 16:06:01 | 0.024 | 300 | 0.076 High range calibration gas |
| 11/10/2008 | 16:06:11 | 0.012 | 300 | 0 |
| 11/10/2008 | 16:06:21 | 0.012 | 294.579 | 0.076 |
| 11/10/2008 | 16:06:31 | 0.012 | 299.707 | 0.076 |
| 11/10/2008 | 16:06:41 | 0.024 | 300 | 0.076 |
| 11/10/2008 | 16:06:51 | 0.024 | 149.817 | 0.076 |
| 11/10/2008 | 16:07:01 | 0.024 | 148.205 | 0.076 |
| 11/10/2008 | 16:07:11 | 0.012 | 150.769 | 0.076 |
| 11/10/2008 | 16:07:21 | 0.012 | 150.842 | 0.076 |
| 11/10/2008 | 16:07:31 | 0 | 150.842 | 0.076 Mid range calibration gas |
| 11/10/2008 | 16:07:41 | 0.024 | 151.062 | 0.076 |
| 11/10/2008 | 16:07:51 | 0.024 | 73.26 | 0.076 |
| 11/10/2008 | 16:08:01 | 0.037 | 73.333 | 0.076 |
| 11/10/2008 | 16:08:11 | 0.037 | 73.7 | 0.076 |
| 11/10/2008 | 16:08:21 | 0.024 | 74.359 | 0.076 |
| 11/10/2008 | 16:08:31 | 0.024 | 74.945 | 0.076 |
| 11/10/2008 | 16:08:41 | 0.024 | 74.799 | 0.076 Low range calibration gas |
| 11/10/2008 | 16:08:51 | 0.012 | 74.872 | 0.076 |
| 11/10/2008 | 16:09:01 | 0.012 | 0.586 | 0.076 |
| 11/10/2008 | 16:09:11 | 0.012 | 0.073 | 0.076 |
| 11/10/2008 | 16:09:21 | 0.024 | 0.073 | 0.076 |
| 11/10/2008 | 16:09:31 | 0.024 | 0.073 | 0.076 |
| 11/10/2008 | 16:09:41 | 0.024 | 0.073 | 0.076 |
| 11/10/2008 | 16:09:51 | 0.012 | 0.073 | 0.076 Zero gas |
| 11/10/2008 | 16:10:01 | 0.012 | 0.073 | 0.076 |
| 11/10/2008 | 16:10:11 | 0.012 | 0.073 | 0.076 |
| 11/10/2008 | 16:10:21 | 0.024 | 140.293 | 0.076 |
| 11/10/2008 | 16:10:31 | 0.024 | 143.59 | 0.076 |
| 11/10/2008 | 16:10:41 | 0.024 | 145.055 | 0.076 |
| 11/10/2008 | 16:10:51 | 0.024 | 145.495 | 0.076 |
| 11/10/2008 | 16:11:01 | 0.024 | 145.714 | 0.076 |
| 11/10/2008 | 16:11:11 | 0.012 | 146.081 | 0.076 |
| 11/10/2008 | 16:11:21 | 0.012 | 146.3 | 0.076 |
| 11/10/2008 | 16:11:31 | 0.012 | 146.52 | 0.076 |
| 11/10/2008 | 16:11:41 | 0.024 | 146.74 | 0.076 |
| 11/10/2008 | 16:11:51 | 0.037 | 146.667 | 0.076 |

Styrene Response Factor Determinations

| | | VOC 1 | VOC 2 | |
|------------|----------|-------|---------|---|
| 11/10/2008 | 16:12:01 | 0.024 | 146.886 | 0.076 |
| 11/10/2008 | 16:12:11 | 0.012 | 147.033 | 0.076 |
| 11/10/2008 | 16:12:21 | 0.024 | 147.179 | 0.076 |
| 11/10/2008 | 16:12:31 | 0.024 | 147.326 | 0.076 |
| 11/10/2008 | 16:12:41 | 0.012 | 147.253 | 0.076 |
| 11/10/2008 | 16:12:51 | 0.024 | 147.399 | 0.076 |
| 11/10/2008 | 16:13:01 | 0.012 | 147.253 | 0.076 |
| 11/10/2008 | 16:13:11 | 0.024 | 147.619 | 0.076 |
| 11/10/2008 | 16:13:21 | 0.024 | 147.546 | 0.076 |
| 11/10/2008 | 16:13:31 | 0.024 | 147.692 | 0.076 |
| 11/10/2008 | 16:13:41 | 0.024 | 147.546 | 0.076 |
| 11/10/2008 | 16:13:51 | 0.024 | 147.546 | 0.076 |
| 11/10/2008 | 16:14:01 | 0.024 | 147.546 | 0.076 |
| 11/10/2008 | 16:14:11 | 0.037 | 147.546 | 0.076 |
| 11/10/2008 | 16:14:21 | 0.024 | 147.619 | 0.076 |
| 11/10/2008 | 16:14:31 | 0.024 | 147.619 | 0.076 |
| 11/10/2008 | 16:14:41 | 0.012 | 147.692 | 0.076 |
| 11/10/2008 | 16:14:51 | 0.012 | 147.766 | 0.076 |
| 11/10/2008 | 16:15:01 | 0.012 | 147.839 | 0.076 |
| 11/10/2008 | 16:15:11 | 0.012 | 147.912 | 0.076 49.2 ppm styrene 0.3326 |
| 11/10/2008 | 16:15:21 | 0.012 | 147.839 | 0.076 |
| 11/10/2008 | 16:15:31 | 0.024 | 147.985 | 0.076 |
| 11/10/2008 | 16:15:41 | 0.024 | 5.201 | 0.076 |
| 11/10/2008 | 16:15:51 | 0.024 | 0.073 | 0.076 |
| 11/10/2008 | 16:16:01 | 0.024 | 0.073 | 0.076 |
| 11/10/2008 | 16:16:11 | 0.012 | 177.582 | 0.076 |
| 11/10/2008 | 16:16:21 | 0.012 | 174.872 | 0.076 |
| 11/10/2008 | 16:16:31 | 0.012 | 172.015 | 0.076 |
| 11/10/2008 | 16:16:41 | 0.012 | 169.377 | 0.076 |
| 11/10/2008 | 16:16:51 | 0.012 | 167.473 | 0.076 |
| 11/10/2008 | 16:17:01 | 0.012 | 166.154 | 0.076 |
| 11/10/2008 | 16:17:11 | 0.024 | 164.908 | 0.076 |
| 11/10/2008 | 16:17:21 | 0.024 | 164.029 | 0.076 |
| 11/10/2008 | 16:17:31 | 0.024 | 159.853 | 0.076 |
| 11/10/2008 | 16:17:41 | 0.024 | 150.769 | 0.076 |
| 11/10/2008 | 16:17:51 | 0.024 | 150.842 | 0.076 Mid range calibration drift check 0.00% |
| 11/10/2008 | 16:18:01 | 0.024 | 150.256 | 0 |
| 11/10/2008 | 16:18:11 | 0.037 | 149.963 | 0.076 |
| 11/10/2008 | 16:18:21 | 0.024 | 6.007 | 0.076 |
| 11/10/2008 | 16:18:31 | 0.024 | 1.612 | 0.076 |
| 11/10/2008 | 16:18:41 | 0.012 | 0.806 | 0.076 |
| 11/10/2008 | 16:18:51 | 0.012 | 0.293 | 0.076 |
| 11/10/2008 | 16:19:01 | 0.012 | 0.073 | 0.076 |
| 11/10/2008 | 16:19:11 | 0 | 0.073 | 0.076 |
| 11/10/2008 | 16:19:21 | 0 | 0.073 | 0.076 Zero calibration drift check 0.00% |
| 11/10/2008 | 16:19:31 | 0.012 | 0.073 | 0.076 |
| 11/10/2008 | 16:19:41 | 0.012 | 0.073 | 0.076 |
| | | VOC 2 | | |
| 11/11/2008 | 11:59:16 | 0.073 | 0.076 | |

Styrene Response Factor Determinations

| | VOC 1 | VOC 2 | | |
|------------|----------|---------|-------|----------------------------|
| 11/11/2008 | 11:59:26 | 0.073 | 0.076 | |
| 11/11/2008 | 11:59:36 | 0.073 | 0.076 | |
| 11/11/2008 | 11:59:46 | 0.073 | 0.076 | |
| 11/11/2008 | 11:59:56 | 0.073 | 0.076 | |
| 11/11/2008 | 12:00:06 | 208.571 | 0.076 | |
| 11/11/2008 | 12:00:16 | 284.396 | 0.076 | |
| 11/11/2008 | 12:00:26 | 297.949 | 0.076 | |
| 11/11/2008 | 12:00:36 | 299.853 | 0.076 | |
| 11/11/2008 | 12:00:46 | 299.927 | 0.076 | |
| 11/11/2008 | 12:00:56 | 299.927 | 0.076 | |
| 11/11/2008 | 12:01:06 | 299.927 | 0.076 | High range calibration gas |
| 11/11/2008 | 12:01:16 | 299.927 | 0.076 | 0.02% |
| 11/11/2008 | 12:01:26 | 0.879 | 0.076 | |
| 11/11/2008 | 12:01:36 | 0.073 | 0.076 | |
| 11/11/2008 | 12:01:46 | 0.073 | 0.076 | |
| 11/11/2008 | 12:01:56 | 0.073 | 0.076 | |
| 11/11/2008 | 12:02:06 | 28.791 | 0.076 | |
| 11/11/2008 | 12:02:16 | 70.403 | 0.076 | |
| 11/11/2008 | 12:02:26 | 71.209 | 0.076 | |
| 11/11/2008 | 12:02:36 | 72.161 | 0.076 | |
| 11/11/2008 | 12:02:46 | 72.527 | 0.076 | |
| 11/11/2008 | 12:02:56 | 72.527 | 0.076 | |
| 11/11/2008 | 12:03:06 | 75.678 | 0.076 | |
| 11/11/2008 | 12:03:16 | 76.63 | 0.076 | |
| 11/11/2008 | 12:03:26 | 75.018 | 0.076 | |
| 11/11/2008 | 12:03:36 | 74.945 | 0.076 | |
| 11/11/2008 | 12:03:46 | 74.945 | 0.076 | Low range calibration gas |
| 11/11/2008 | 12:03:56 | 74.872 | 0.076 | 0.07% |
| 11/11/2008 | 12:04:06 | 154.579 | 0.076 | |
| 11/11/2008 | 12:04:16 | 153.26 | 0.076 | |
| 11/11/2008 | 12:04:26 | 153.187 | 0.076 | |
| 11/11/2008 | 12:04:36 | 150.623 | 0.076 | |
| 11/11/2008 | 12:04:46 | 150.549 | 0.076 | |
| 11/11/2008 | 12:04:56 | 149.89 | 0.076 | |
| 11/11/2008 | 12:05:06 | 149.67 | 0.076 | |
| 11/11/2008 | 12:05:16 | 148.791 | 0.076 | |
| 11/11/2008 | 12:05:26 | 148.352 | 0.076 | |
| 11/11/2008 | 12:05:36 | 148.132 | 0.076 | |
| 11/11/2008 | 12:05:46 | 148.205 | 0.076 | |
| 11/11/2008 | 12:05:56 | 150.476 | 0.076 | |
| 11/11/2008 | 12:06:06 | 149.597 | 0.076 | |
| 11/11/2008 | 12:06:16 | 148.938 | 0.076 | |
| 11/11/2008 | 12:06:26 | 148.571 | 0.076 | |
| 11/11/2008 | 12:06:36 | 151.795 | 0.076 | |
| 11/11/2008 | 12:06:46 | 150.037 | 0.076 | |
| 11/11/2008 | 12:06:56 | 149.377 | 0.076 | |
| 11/11/2008 | 12:07:06 | 150.476 | 0.076 | Mid range calibration gas |
| 11/11/2008 | 12:07:16 | 149.744 | 0.076 | 0.32% |
| 11/11/2008 | 12:07:26 | 149.231 | 0.076 | |

Styrene Response Factor Determinations

| | VOC 1 | VOC 2 | |
|------------|----------|---------|-------|
| 11/11/2008 | 12:07:36 | 149.158 | 0.076 |
| 11/11/2008 | 12:07:46 | 152.747 | 0 |
| 11/11/2008 | 12:07:56 | 0.073 | 0.076 |
| 11/11/2008 | 12:08:06 | 0.073 | 0.076 |
| 11/11/2008 | 12:08:16 | 0.073 | 0.076 |
| 11/11/2008 | 12:08:26 | 0.073 | 0.076 |
| 11/11/2008 | 12:08:36 | 0.073 | 0.076 |
| 11/11/2008 | 12:08:46 | 0.073 | 0.076 |
| 11/11/2008 | 12:08:56 | 0.073 | 0.076 |
| 11/11/2008 | 12:09:06 | 0.073 | 0.076 |
| 11/11/2008 | 12:09:16 | 131.722 | 0.076 |
| 11/11/2008 | 12:09:26 | 138.681 | 0.076 |
| 11/11/2008 | 12:09:36 | 139.414 | 0.076 |
| 11/11/2008 | 12:09:46 | 141.685 | 0.076 |
| 11/11/2008 | 12:09:56 | 143.516 | 0.076 |
| 11/11/2008 | 12:10:06 | 145.055 | 0.076 |
| 11/11/2008 | 12:10:16 | 145.495 | 0.076 |
| 11/11/2008 | 12:10:26 | 147.766 | 0.076 |
| 11/11/2008 | 12:10:36 | 148.205 | 0.076 |
| 11/11/2008 | 12:10:46 | 148.205 | 0.076 |
| 11/11/2008 | 12:10:56 | 147.985 | 0.076 |
| 11/11/2008 | 12:11:06 | 147.985 | 0.076 |
| 11/11/2008 | 12:11:16 | 148.205 | 0.076 |
| 11/11/2008 | 12:11:26 | 148.571 | 0.076 |
| 11/11/2008 | 12:11:36 | 148.498 | 0.076 |
| 11/11/2008 | 12:11:46 | 148.718 | 0.076 |
| 11/11/2008 | 12:11:56 | 148.718 | 0.076 |
| 11/11/2008 | 12:12:06 | 149.084 | 0.076 |
| 11/11/2008 | 12:12:16 | 149.084 | 0.076 |
| 11/11/2008 | 12:12:26 | 149.084 | 0.076 |
| 11/11/2008 | 12:12:36 | 149.011 | 0.076 |
| 11/11/2008 | 12:12:46 | 148.864 | 0.076 |
| 11/11/2008 | 12:12:56 | 148.645 | 0.076 |
| 11/11/2008 | 12:13:06 | 148.645 | 0.076 |
| 11/11/2008 | 12:13:16 | 148.645 | 0.076 |
| 11/11/2008 | 12:13:26 | 148.498 | 0.076 |
| 11/11/2008 | 12:13:36 | 148.645 | 0.076 |
| 11/11/2008 | 12:13:46 | 148.718 | 0.076 |
| 11/11/2008 | 12:13:56 | 148.864 | 0.076 |
| 11/11/2008 | 12:14:06 | 149.011 | 0.076 |
| 11/11/2008 | 12:14:16 | 148.938 | 0.076 |
| 11/11/2008 | 12:14:26 | 149.011 | 0.076 |
| 11/11/2008 | 12:14:36 | 149.084 | 0.076 |
| 11/11/2008 | 12:14:46 | 149.084 | 0.076 |
| 11/11/2008 | 12:14:56 | 149.158 | 0.076 |
| 11/11/2008 | 12:15:06 | 149.011 | 0.076 |
| 11/11/2008 | 12:15:16 | 149.304 | 0.076 |
| 11/11/2008 | 12:15:26 | 149.158 | 0.076 |
| 11/11/2008 | 12:15:36 | 149.084 | 0.076 |

Styrene Response Factor Determinations

| | VOC 1 | VOC 2 | |
|------------|----------|---------|-------|
| 11/11/2008 | 12:15:46 | 149.231 | 0.076 |
| 11/11/2008 | 12:15:56 | 149.304 | 0.076 |
| 11/11/2008 | 12:16:06 | 149.158 | 0.076 |
| 11/11/2008 | 12:16:16 | 149.304 | 0.076 |
| 11/11/2008 | 12:16:26 | 149.231 | 0.076 |
| 11/11/2008 | 12:16:36 | 149.304 | 0.076 |
| 11/11/2008 | 12:16:46 | 149.377 | 0.076 |
| 11/11/2008 | 12:16:56 | 149.231 | 0.076 |
| 11/11/2008 | 12:17:06 | 149.084 | 0.076 |
| 11/11/2008 | 12:17:16 | 149.084 | 0.076 |
| 11/11/2008 | 12:17:26 | 149.084 | 0.076 |
| 11/11/2008 | 12:17:36 | 148.938 | 0.076 |
| 11/11/2008 | 12:17:46 | 149.084 | 0.076 |
| 11/11/2008 | 12:17:56 | 149.011 | 0.076 |
| 11/11/2008 | 12:18:06 | 149.084 | 0.076 |
| 11/11/2008 | 12:18:16 | 149.304 | 0.076 |
| 11/11/2008 | 12:18:26 | 149.304 | 0.076 |
| 11/11/2008 | 12:18:36 | 149.304 | 0.076 |
| 11/11/2008 | 12:18:46 | 149.231 | 0.076 |
| 11/11/2008 | 12:18:56 | 149.304 | 0.076 |
| 11/11/2008 | 12:19:06 | 149.377 | 0.076 |
| 11/11/2008 | 12:19:16 | 149.377 | 0.076 |
| 11/11/2008 | 12:19:26 | 149.451 | 0.076 |
| 11/11/2008 | 12:19:36 | 149.597 | 0.076 |
| 11/11/2008 | 12:19:46 | 149.67 | 0.076 |
| 11/11/2008 | 12:19:56 | 149.963 | 0.076 |
| 11/11/2008 | 12:20:06 | 149.89 | 0.076 |
| 11/11/2008 | 12:20:16 | 149.963 | 0.076 |
| 11/11/2008 | 12:20:26 | 150.11 | 0.076 |
| 11/11/2008 | 12:20:36 | 150.11 | 0.076 |
| 11/11/2008 | 12:20:46 | 22.198 | 0.076 |
| 11/11/2008 | 12:20:56 | 0.073 | 0.076 |
| 11/11/2008 | 12:21:06 | 0.073 | 0.076 |
| 11/11/2008 | 12:21:16 | 244.689 | 0.076 |
| 11/11/2008 | 12:21:26 | 175.385 | 0.076 |
| 11/11/2008 | 12:21:36 | 174.725 | 0.076 |
| 11/11/2008 | 12:21:46 | 171.209 | 0.076 |
| 11/11/2008 | 12:21:56 | 168.571 | 0.076 |
| 11/11/2008 | 12:22:06 | 166.74 | 0.076 |
| 11/11/2008 | 12:22:16 | 165.421 | 0.076 |
| 11/11/2008 | 12:22:26 | 164.615 | 0.076 |
| 11/11/2008 | 12:22:36 | 164.249 | 0.076 |
| 11/11/2008 | 12:22:46 | 163.663 | 0.076 |
| 11/11/2008 | 12:22:56 | 163.736 | 0.076 |
| 11/11/2008 | 12:23:06 | 163.297 | 0.076 |
| 11/11/2008 | 12:23:16 | 163.223 | 0.076 |
| 11/11/2008 | 12:23:26 | 163.004 | 0.076 |
| 11/11/2008 | 12:23:36 | 162.564 | 0.076 |
| 11/11/2008 | 12:23:46 | 162.564 | 0.076 |

Styrene Response Factor Determinations

| | VOC 1 | VOC 2 |
|------------|----------|---------|
| 11/11/2008 | 12:23:56 | 162.271 |
| 11/11/2008 | 12:24:06 | 162.271 |
| 11/11/2008 | 12:24:16 | 161.978 |
| 11/11/2008 | 12:24:26 | 161.465 |
| 11/11/2008 | 12:24:36 | 161.172 |
| 11/11/2008 | 12:24:46 | 160.659 |
| 11/11/2008 | 12:24:56 | 160.586 |
| 11/11/2008 | 12:25:06 | 160.073 |
| 11/11/2008 | 12:25:16 | 159.707 |
| 11/11/2008 | 12:25:26 | 159.048 |
| 11/11/2008 | 12:25:36 | 158.535 |
| 11/11/2008 | 12:25:46 | 158.681 |
| 11/11/2008 | 12:25:56 | 158.315 |
| 11/11/2008 | 12:26:06 | 157.656 |
| 11/11/2008 | 12:26:16 | 157.436 |
| 11/11/2008 | 12:26:26 | 157.509 |
| 11/11/2008 | 12:26:36 | 157.143 |
| 11/11/2008 | 12:26:46 | 157.289 |
| 11/11/2008 | 12:26:56 | 156.923 |
| 11/11/2008 | 12:27:06 | 156.264 |
| 11/11/2008 | 12:27:16 | 156.19 |
| 11/11/2008 | 12:27:26 | 156.117 |
| 11/11/2008 | 12:27:36 | 156.044 |
| 11/11/2008 | 12:27:46 | 155.678 |
| 11/11/2008 | 12:27:56 | 155.678 |
| 11/11/2008 | 12:28:06 | 155.824 |
| 11/11/2008 | 12:28:16 | 155.678 |
| 11/11/2008 | 12:28:26 | 155.751 |
| 11/11/2008 | 12:28:36 | 155.751 |
| 11/11/2008 | 12:28:46 | 155.897 |
| 11/11/2008 | 12:28:56 | 155.751 |
| 11/11/2008 | 12:29:06 | 155.751 |
| 11/11/2008 | 12:29:16 | 156.484 |
| 11/11/2008 | 12:29:26 | 156.19 |
| 11/11/2008 | 12:29:36 | 155.971 |
| 11/11/2008 | 12:29:46 | 155.751 |
| 11/11/2008 | 12:29:56 | 155.824 |
| 11/11/2008 | 12:30:06 | 155.751 |
| 11/11/2008 | 12:30:16 | 155.751 |
| 11/11/2008 | 12:30:26 | 155.604 |
| 11/11/2008 | 12:30:36 | 155.531 |
| 11/11/2008 | 12:30:46 | 155.531 |
| 11/11/2008 | 12:30:56 | 155.824 |
| 11/11/2008 | 12:31:06 | 155.531 |
| 11/11/2008 | 12:31:16 | 155.531 |
| 11/11/2008 | 12:31:26 | 155.458 |
| 11/11/2008 | 12:31:36 | 155.238 |
| 11/11/2008 | 12:31:46 | 155.018 |
| 11/11/2008 | 12:31:56 | 155.311 |

Styrene Response Factor Determinations

| | VOC 1 | VOC 2 | |
|------------|----------|---------|-------|
| 11/11/2008 | 12:32:06 | 155.458 | 0.076 |
| 11/11/2008 | 12:32:16 | 155.531 | 0.076 |
| 11/11/2008 | 12:32:26 | 155.018 | 0.076 |
| 11/11/2008 | 12:32:36 | 154.945 | 0.076 |
| 11/11/2008 | 12:32:46 | 154.725 | 0.076 |
| 11/11/2008 | 12:32:56 | 154.505 | 0.076 |
| 11/11/2008 | 12:33:06 | 154.505 | 0.076 |
| 11/11/2008 | 12:33:16 | 154.652 | 0.076 |
| 11/11/2008 | 12:33:26 | 154.579 | 0.076 |
| 11/11/2008 | 12:33:36 | 154.286 | 0.076 |
| 11/11/2008 | 12:33:46 | 154.139 | 0.076 |
| 11/11/2008 | 12:33:56 | 153.993 | 0.076 |
| 11/11/2008 | 12:34:06 | 154.359 | 0.076 |
| 11/11/2008 | 12:34:16 | 154.139 | 0.076 |
| 11/11/2008 | 12:34:26 | 154.139 | 0.076 |
| 11/11/2008 | 12:34:36 | 153.773 | 0.076 |
| 11/11/2008 | 12:34:46 | 153.773 | 0.076 |
| 11/11/2008 | 12:34:56 | 153.773 | 0.076 |
| 11/11/2008 | 12:35:06 | 153.773 | 0.076 |
| 11/11/2008 | 12:35:16 | 153.773 | 0.076 |
| 11/11/2008 | 12:35:26 | 153.7 | 0.076 |
| 11/11/2008 | 12:35:36 | 153.553 | 0.076 |
| 11/11/2008 | 12:35:46 | 153.626 | 0.076 |
| 11/11/2008 | 12:35:56 | 153.7 | 0.076 |
| 11/11/2008 | 12:36:06 | 150.183 | 0.076 |
| 11/11/2008 | 12:36:16 | 151.136 | 0.076 |
| 11/11/2008 | 12:36:26 | 150.842 | 0.076 |
| 11/11/2008 | 12:36:36 | 150.989 | 0.076 |
| 11/11/2008 | 12:36:46 | 150.183 | 0.076 |
| 11/11/2008 | 12:36:56 | 150.476 | 0.076 |
| 11/11/2008 | 12:37:06 | 2.711 | 0.076 |
| 11/11/2008 | 12:37:16 | 24.689 | 0.076 |
| 11/11/2008 | 12:37:26 | 0.073 | 0.076 |
| 11/11/2008 | 12:37:36 | 0.073 | 0.076 |
| 11/11/2008 | 12:37:46 | 0.073 | 0.076 |
| 11/11/2008 | 12:37:56 | 0.073 | 0.076 |
| 11/11/2008 | 12:38:06 | 0.073 | 0.076 |
| 11/11/2008 | 12:38:16 | 0.073 | 0.076 |
| 11/11/2008 | 12:38:26 | 0.073 | 0.076 |
| | VOC 1 | | |
| 11/11/2008 | 12:43:02 | 0 | |
| 11/11/2008 | 12:43:12 | 0.076 | |
| 11/11/2008 | 12:43:22 | 0.076 | |
| 11/11/2008 | 12:43:32 | 0.076 | |
| 11/11/2008 | 12:43:42 | 0.076 | |
| 11/11/2008 | 12:43:52 | 0.076 | |
| 11/11/2008 | 12:44:02 | 0.076 | |
| 11/11/2008 | 12:44:12 | 309.394 | |
| 11/11/2008 | 12:44:22 | 309.924 | |

Styrene Response Factor Determinations

| | VOC 1 | VOC 2 | |
|------------|----------|---------|----------------------------|
| 11/11/2008 | 12:44:32 | 310 | |
| 11/11/2008 | 12:44:42 | 309.924 | |
| 11/11/2008 | 12:44:52 | 309.924 | |
| 11/11/2008 | 12:45:02 | 309.924 | |
| 11/11/2008 | 12:45:12 | 310 | |
| 11/11/2008 | 12:45:22 | 309.924 | |
| 11/11/2008 | 12:45:32 | 310 | |
| 11/11/2008 | 12:45:42 | 309.924 | |
| 11/11/2008 | 12:45:52 | 309.924 | |
| 11/11/2008 | 12:46:02 | 310 | |
| 11/11/2008 | 12:46:12 | 309.924 | |
| 11/11/2008 | 12:46:22 | 310 | |
| 11/11/2008 | 12:46:32 | 310 | |
| 11/11/2008 | 12:46:42 | 309.924 | |
| 11/11/2008 | 12:46:52 | 310 | |
| 11/11/2008 | 12:47:02 | 310 | |
| 11/11/2008 | 12:47:12 | 309.924 | |
| 11/11/2008 | 12:47:22 | 309.924 | |
| 11/11/2008 | 12:47:32 | 309.924 | |
| 11/11/2008 | 12:47:42 | 310 | |
| 11/11/2008 | 12:47:52 | 309.924 | |
| 11/11/2008 | 12:48:02 | 310 | |
| 11/11/2008 | 12:48:12 | 309.924 | |
| 11/11/2008 | 12:48:22 | 310 | |
| 11/11/2008 | 12:48:32 | 310 | |
| 11/11/2008 | 12:48:42 | 310 | |
| 11/11/2008 | 12:48:52 | 309.924 | |
| 11/11/2008 | 12:49:02 | 310 | |
| 11/11/2008 | 12:49:12 | 309.924 | |
| 11/11/2008 | 12:49:22 | 309.773 | |
| 11/11/2008 | 12:49:32 | 301.824 | |
| 11/11/2008 | 12:49:42 | 301.446 | High range calibration gas |
| 11/11/2008 | 12:49:52 | 301.597 | |
| 11/11/2008 | 12:50:02 | 302.43 | |
| 11/11/2008 | 12:50:12 | 303.035 | |
| 11/11/2008 | 12:50:22 | 303.868 | |
| 11/11/2008 | 12:50:32 | 305.306 | |
| 11/11/2008 | 12:50:42 | 301.219 | |
| 11/11/2008 | 12:50:52 | 302.278 | |
| 11/11/2008 | 12:51:02 | 20.137 | |
| 11/11/2008 | 12:51:12 | 3.709 | |
| 11/11/2008 | 12:51:22 | 1.817 | |
| 11/11/2008 | 12:51:32 | 1.136 | |
| 11/11/2008 | 12:51:42 | 0.681 | |
| 11/11/2008 | 12:51:52 | 0.53 | |
| 11/11/2008 | 12:52:02 | 0.379 | |
| 11/11/2008 | 12:52:12 | 0.076 | |
| 11/11/2008 | 12:52:22 | 0.076 | Zero gas |
| 11/11/2008 | 12:52:32 | 0.076 | |

Styrene Response Factor Determinations

| | VOC 1 | VOC 2 | |
|------------|----------|---------|---------------------------|
| 11/11/2008 | 12:52:42 | 49.661 | |
| 11/11/2008 | 12:52:52 | 67.072 | |
| 11/11/2008 | 12:53:02 | 70.554 | |
| 11/11/2008 | 12:53:12 | 71.917 | |
| 11/11/2008 | 12:53:22 | 72.22 | |
| 11/11/2008 | 12:53:32 | 77.897 | |
| 11/11/2008 | 12:53:42 | 76.611 | |
| 11/11/2008 | 12:53:52 | 76.383 | |
| 11/11/2008 | 12:54:02 | 75.475 | Low range calibration gas |
| 11/11/2008 | 12:54:12 | 75.324 | 0.63% |
| 11/11/2008 | 12:54:22 | 75.475 | |
| 11/11/2008 | 12:54:32 | 153.221 | |
| 11/11/2008 | 12:54:42 | 154.659 | |
| 11/11/2008 | 12:54:52 | 154.962 | |
| 11/11/2008 | 12:55:02 | 155.114 | |
| 11/11/2008 | 12:55:12 | 155.492 | |
| 11/11/2008 | 12:55:22 | 149.36 | |
| 11/11/2008 | 12:55:32 | 149.512 | |
| 11/11/2008 | 12:55:42 | 149.436 | Mid range calibration gas |
| 11/11/2008 | 12:55:52 | 149.285 | 0.38% |
| 11/11/2008 | 12:56:02 | 93.871 | |
| 11/11/2008 | 12:56:12 | 0.076 | |
| 11/11/2008 | 12:56:22 | 0.076 | |
| 11/11/2008 | 12:56:32 | 119.231 | |
| 11/11/2008 | 12:56:42 | 132.024 | |
| 11/11/2008 | 12:56:52 | 134.674 | |
| 11/11/2008 | 12:57:02 | 135.658 | |
| 11/11/2008 | 12:57:12 | 136.718 | |
| 11/11/2008 | 12:57:22 | 137.096 | |
| 11/11/2008 | 12:57:32 | 138.383 | |
| 11/11/2008 | 12:57:42 | 139.14 | |
| 11/11/2008 | 12:57:52 | 139.292 | |
| 11/11/2008 | 12:58:02 | 139.595 | |
| 11/11/2008 | 12:58:12 | 139.595 | |
| 11/11/2008 | 12:58:22 | 140.125 | |
| 11/11/2008 | 12:58:32 | 139.822 | |
| 11/11/2008 | 12:58:42 | 139.368 | |
| 11/11/2008 | 12:58:52 | 137.929 | |
| 11/11/2008 | 12:59:02 | 139.216 | |
| 11/11/2008 | 12:59:12 | 140.276 | |
| 11/11/2008 | 12:59:22 | 139.973 | |
| 11/11/2008 | 12:59:32 | 140.352 | |
| 11/11/2008 | 12:59:42 | 140.2 | |
| 11/11/2008 | 12:59:52 | 139.973 | |
| 11/11/2008 | 13:00:02 | 140.125 | |
| 11/11/2008 | 13:00:12 | 140.125 | |
| 11/11/2008 | 13:00:22 | 139.897 | |
| 11/11/2008 | 13:00:32 | 139.897 | |
| 11/11/2008 | 13:00:42 | 140.2 | |

Styrene Response Factor Determinations

| | VOC 1 | VOC 2 | |
|------------|----------|---------|------------------|
| 11/11/2008 | 13:00:52 | 140.2 | |
| 11/11/2008 | 13:01:02 | 140.125 | |
| 11/11/2008 | 13:01:12 | 139.973 | |
| 11/11/2008 | 13:01:22 | 140.503 | |
| 11/11/2008 | 13:01:32 | 140.276 | |
| 11/11/2008 | 13:01:42 | 140.2 | |
| 11/11/2008 | 13:01:52 | 140.049 | |
| 11/11/2008 | 13:02:02 | 140.2 | |
| 11/11/2008 | 13:02:12 | 140.125 | |
| 11/11/2008 | 13:02:22 | 140.276 | |
| 11/11/2008 | 13:02:32 | 140.049 | |
| 11/11/2008 | 13:02:42 | 140.125 | |
| 11/11/2008 | 13:02:52 | 140.503 | |
| 11/11/2008 | 13:03:02 | 140.503 | |
| 11/11/2008 | 13:03:12 | 140.427 | |
| 11/11/2008 | 13:03:22 | 140.427 | |
| 11/11/2008 | 13:03:32 | 140.427 | 49.2 ppm styrene |
| 11/11/2008 | 13:03:42 | 140.2 | 0.3504 |
| 11/11/2008 | 13:03:52 | 140.125 | |
| 11/11/2008 | 13:04:02 | 140.2 | |
| 11/11/2008 | 13:04:12 | 140.125 | |
| 11/11/2008 | 13:04:22 | 140.2 | |
| 11/11/2008 | 13:04:32 | 140.2 | |
| 11/11/2008 | 13:04:42 | 140.2 | |
| 11/11/2008 | 13:04:52 | 140.125 | |
| 11/11/2008 | 13:05:02 | 139.897 | |
| 11/11/2008 | 13:05:12 | 139.822 | |
| 11/11/2008 | 13:05:22 | 139.822 | |
| 11/11/2008 | 13:05:32 | 140.049 | |
| 11/11/2008 | 13:05:42 | 139.973 | |
| 11/11/2008 | 13:05:52 | 139.973 | |
| 11/11/2008 | 13:06:02 | 139.973 | |
| 11/11/2008 | 13:06:12 | 139.897 | |
| 11/11/2008 | 13:06:22 | 139.746 | |
| 11/11/2008 | 13:06:32 | 139.595 | |
| 11/11/2008 | 13:06:42 | 139.67 | |
| 11/11/2008 | 13:06:52 | 139.746 | |
| 11/11/2008 | 13:07:02 | 139.519 | |
| 11/11/2008 | 13:07:12 | 139.746 | |
| 11/11/2008 | 13:07:22 | 139.519 | |
| 11/11/2008 | 13:07:32 | 139.822 | |
| 11/11/2008 | 13:07:42 | 139.67 | |
| 11/11/2008 | 13:07:52 | 139.519 | |
| 11/11/2008 | 13:08:02 | 139.519 | |
| 11/11/2008 | 13:08:12 | 139.216 | |
| 11/11/2008 | 13:08:22 | 139.292 | |
| 11/11/2008 | 13:08:32 | 139.519 | |
| 11/11/2008 | 13:08:42 | 139.14 | |
| 11/11/2008 | 13:08:52 | 139.368 | |

Styrene Response Factor Determinations

VOC 1 VOC 2

| | | |
|------------|----------|---------|
| 11/11/2008 | 13:09:02 | 139.216 |
| 11/11/2008 | 13:09:12 | 139.065 |
| 11/11/2008 | 13:09:22 | 139.216 |
| 11/11/2008 | 13:09:32 | 139.292 |
| 11/11/2008 | 13:09:42 | 139.14 |
| 11/11/2008 | 13:09:52 | 139.368 |
| 11/11/2008 | 13:10:02 | 139.368 |
| 11/11/2008 | 13:10:12 | 139.368 |
| 11/11/2008 | 13:10:22 | 139.14 |
| 11/11/2008 | 13:10:32 | 139.065 |
| 11/11/2008 | 13:10:42 | 139.368 |
| 11/11/2008 | 13:10:52 | 139.519 |
| 11/11/2008 | 13:11:02 | 139.519 |
| 11/11/2008 | 13:11:12 | 139.443 |
| 11/11/2008 | 13:11:22 | 139.368 |
| 11/11/2008 | 13:11:32 | 139.216 |
| 11/11/2008 | 13:11:42 | 139.292 |
| 11/11/2008 | 13:11:52 | 139.292 |
| 11/11/2008 | 13:12:02 | 139.216 |
| 11/11/2008 | 13:12:12 | 139.292 |
| 11/11/2008 | 13:12:22 | 139.368 |
| 11/11/2008 | 13:12:32 | 138.838 |
| 11/11/2008 | 13:12:42 | 139.065 |
| 11/11/2008 | 13:12:52 | 139.14 |
| 11/11/2008 | 13:13:02 | 139.216 |
| 11/11/2008 | 13:13:12 | 139.065 |
| 11/11/2008 | 13:13:22 | 138.989 |
| 11/11/2008 | 13:13:32 | 139.065 |
| 11/11/2008 | 13:13:42 | 139.216 |
| 11/11/2008 | 13:13:52 | 140.806 |
| 11/11/2008 | 13:14:02 | 147.089 |
| 11/11/2008 | 13:14:12 | 147.089 |
| 11/11/2008 | 13:14:22 | 30.508 |
| 11/11/2008 | 13:14:32 | 2.195 |
| 11/11/2008 | 13:14:42 | 0.076 |
| 11/11/2008 | 13:14:52 | 0.076 |
| 11/11/2008 | 13:15:02 | 177.067 |
| 11/11/2008 | 13:15:12 | 180.247 |
| 11/11/2008 | 13:15:22 | 177.294 |
| 11/11/2008 | 13:15:32 | 173.736 |
| 11/11/2008 | 13:15:42 | 171.389 |
| 11/11/2008 | 13:15:52 | 169.421 |
| 11/11/2008 | 13:16:02 | 167.907 |
| 11/11/2008 | 13:16:12 | 166.999 |
| 11/11/2008 | 13:16:22 | 166.015 |
| 11/11/2008 | 13:16:32 | 164.955 |
| 11/11/2008 | 13:16:42 | 164.273 |
| 11/11/2008 | 13:16:52 | 163.744 |
| 11/11/2008 | 13:17:02 | 163.138 |

Styrene Response Factor Determinations

| | VOC 1 | VOC 2 | | |
|------------|----------|---------|-----------------------------------|-------|
| 11/11/2008 | 13:17:12 | 162.532 | | |
| 11/11/2008 | 13:17:22 | 161.548 | | |
| 11/11/2008 | 13:17:32 | 161.17 | | |
| 11/11/2008 | 13:17:42 | 160.715 | | |
| 11/11/2008 | 13:17:52 | 159.883 | | |
| 11/11/2008 | 13:18:02 | 159.05 | | |
| 11/11/2008 | 13:18:12 | 158.293 | | |
| 11/11/2008 | 13:18:22 | 157.839 | | |
| 11/11/2008 | 13:18:32 | 157.385 | | |
| 11/11/2008 | 13:18:42 | 156.93 | | |
| 11/11/2008 | 13:18:52 | 156.855 | | |
| 11/11/2008 | 13:19:02 | 156.476 | | |
| 11/11/2008 | 13:19:12 | 156.173 | | |
| 11/11/2008 | 13:19:22 | 155.795 | | |
| 11/11/2008 | 13:19:32 | 155.795 | | |
| 11/11/2008 | 13:19:42 | 155.871 | | |
| 11/11/2008 | 13:19:52 | 155.492 | | |
| 11/11/2008 | 13:20:02 | 155.492 | | |
| 11/11/2008 | 13:20:12 | 155.416 | | |
| 11/11/2008 | 13:20:22 | 155.189 | | |
| 11/11/2008 | 13:20:32 | 155.038 | | |
| 11/11/2008 | 13:20:42 | 155.114 | | |
| 11/11/2008 | 13:20:52 | 155.038 | | |
| 11/11/2008 | 13:21:02 | 154.886 | | |
| 11/11/2008 | 13:21:12 | 154.357 | | |
| 11/11/2008 | 13:21:22 | 154.508 | | |
| 11/11/2008 | 13:21:32 | 154.357 | | |
| 11/11/2008 | 13:21:42 | 154.129 | | |
| 11/11/2008 | 13:21:52 | 148.755 | | |
| 11/11/2008 | 13:22:02 | 149.663 | | |
| 11/11/2008 | 13:22:12 | 149.512 | | |
| 11/11/2008 | 13:22:22 | 149.436 | Mid range calibration drift check | 0.00% |
| 11/11/2008 | 13:22:32 | 149.587 | | |
| 11/11/2008 | 13:22:42 | 149.209 | | |
| 11/11/2008 | 13:22:52 | 160.488 | | |
| 11/11/2008 | 13:23:02 | 3.709 | | |
| 11/11/2008 | 13:23:12 | 1.06 | | |
| 11/11/2008 | 13:23:22 | 0.076 | | |
| 11/11/2008 | 13:23:32 | 0.076 | | |
| 11/11/2008 | 13:23:42 | 0.076 | | |
| 11/11/2008 | 13:23:52 | 0.076 | Zero calibration drift check | 0.00% |
| 11/11/2008 | 13:24:02 | 0.076 | | |
| 11/11/2008 | 13:24:12 | 0.076 | | |
| 11/11/2008 | 13:24:22 | 0.076 | | |

CEM Event Log

Client: E Stone/Grove

Date: 11/10/08

Project No. 8192

Location: Seminole, FL

Techician: F Smith

| Task | Start Time | End Time | Notes |
|---------------|------------|----------|----------------------|
| VOC 2 CA1 | 1537 | 1541 | |
| VOC 2 Styrene | 1542 | 1547 | |
| VOC 2 CA1 | 1548 | 1554 | |
| VOC 1 CA1 | 1605 | 1609 | 1605-1609 |
| VOC 1 Styrene | 1610 | 1615 | |
| VOC 1 CA1 | 1616 | 1620 | |
| VOC 1 CA1 | 1200 | 1208 | 11/11/08 |
| VOC 1 Styrene | 1209 | 1220 | |
| VOC 1 CA1 | 1221 | 1238 | |
| VOC 2 CA1 | 1243 | 1255 | |
| VOC 2 Styrene | 1256 | 1314 | |
| VOC 2 CA1 | 1315 | 1324 | |

SYSTEM CALIBRATION ERROR DATA

Client: E Stone / Grove Date: 11/10/08
 Location: Sorbering, FL Project No.: 8192
 Calibration Gas: 10110 ppm LPG Cylinder No.: S69140087CA1 Exp. Date: 9/27/09
 US EPA Method: OSA Analyzer ID: CAT 300M Cylinder Pressure (PSI): 500
 Was instrument stable prior to beginning calibrations? YES

Initial Analyzer Calibration using Dilution System

| Range | Dilution Target Level (ppm or %) | Instrument Response (ppm or %) | Difference (ppm or %) | Allowable Difference (ppm or %) | Specification |
|------------|----------------------------------|--------------------------------|-----------------------|---------------------------------|--------------------------------|
| Zero | <u>0.00</u> | <u>0.08</u> | <u>0.08</u> | <u>6.60</u> | <u>± 2% of Span</u> |
| Low Range | <u>75.00</u> | <u>74.79</u> | <u>-0.21</u> | <u>3.75</u> | <u>± 5% of Gas Value-25A/B</u> |
| Mid Range | <u>150.00</u> | <u>151.63</u> | <u>1.63</u> | <u>7.50</u> | <u>± 5% of Gas Value-25A/B</u> |
| High Range | <u>300.00</u> | <u>300.01</u> | <u>0.01</u> | <u>15.00</u> | <u>± 5% of Gas Value-25A/B</u> |
| Span Value | <u>330.00</u> | | | | <u>=110% of High Range Gas</u> |

Hourly System Calibration Error and Zero Drift Checks

| | Run Time (24 Hour Clock) | Initial System Response (ppm or %) | | Final System Response (ppm or %) | | Drift Difference (ppm or %) | | Calibration Drift (percent error) | |
|-------|-----------------------------|------------------------------------|---------------|----------------------------------|---------------|-----------------------------|-------------|-----------------------------------|-------------|
| | | Zero | Midscale | Zero | Midscale | Zero | Midscale | Zero | Midscale |
| Run 1 | <u>1548</u> | <u>0.08</u> | <u>151.63</u> | <u>0.08</u> | <u>150.42</u> | <u>0.00</u> | <u>1.21</u> | <u>0.00</u> | <u>0.37</u> |
| Run 2 | | | | | | | | | |
| Run 3 | | | | | | | | | |
| Run 4 | | | | | | | | | |
| Run 5 | | | | | | | | | |
| Run 6 | | | | | | | | | |

Specification-All must be within $\pm 3\%$ of span

Field Notes: 50 ppm St. severe = 160.41 ppm Response as per P4105 (1548)

VOC 2

QA/QC Check

Completeness Legibility Accuracy Specifications Reasonableness

L.S.H. 11/10/08
Technician (Signature/Date)

W. Kiel Rohr 12/16/08
Project Manager (Signature/Date)

SYSTEM CALIBRATION ERROR DATA

Client: E-Stone/Grove Date: 11/16/08
 Location: Seminole FL Project No.: 8192
 Calibration Gas: 10110 ppm Acetone Cylinder No. 56914008764L Exp. Date: 9/27/09
 US EPA Method: 2014 Analyzer ID: CAT 300 Cylinder Pressure (PSI): 500
 Was instrument stable prior to beginning calibrations? Yes

Initial Analyzer Calibration using Dilution System

| Range | Dilution Target Level (ppm or %) | Instrument Response (ppm or %) | Difference (ppm or %) | Allowable Difference (ppm or %) | Specification |
|------------|----------------------------------|--------------------------------|-----------------------|---------------------------------|-------------------------|
| Zero | 0.00 | 0.07 | 0.07 | 0.60 | ± 2% of Span |
| Low Range | 75.00 | 74.80 | -0.20 | 3.75 | ± 5% of Gas Value-25A/B |
| Mid Range | 150.00 | 150.84 | 0.84 | 7.50 | ± 5% of Gas Value-25A/B |
| High Range | 300.00 | 300.00 | 0.00 | 15.00 | ± 5% of Gas Value-25A/B |
| Span Value | 330.00 | | | | =110% of High Range Gas |

Hourly System Calibration Error and Zero Drift Checks

| | Run Time (24 Hour Clock) | Initial System Response (ppm or %) | | Final System Response (ppm or %) | | Drift Difference (ppm or %) | | Calibration Drift (percent error) | |
|-------|-----------------------------|------------------------------------|----------|----------------------------------|----------|-----------------------------|----------|-----------------------------------|----------|
| | | Zero | Midscale | Zero | Midscale | Zero | Midscale | Zero | Midscale |
| Run 1 | 1616 | 0.07 | 150.84 | 0.07 | 150.84 | 0.00 | 0.00 | 0.00 | 0.00 |
| Run 2 | | | | | | | | | |
| Run 3 | | | | | | | | | |
| Run 4 | | | | | | | | | |
| Run 5 | | | | | | | | | |
| Run 6 | | | | | | | | | |

Specification-All must be within ± 3% of span

Field Notes: 50 ppm Span = 147.91 ppm Response vs. Response(1615)

VOC 1

QA/QC Check

| Completeness | Legibility | Accuracy | Specifications | Reasonableness |
|------------------------|------------|----------|------------------------------|----------------|
| <u>L.S.H.</u> 11/16/08 | | | <u>W. Kirk Pyle</u> 12/16/08 | |

SYSTEM CALIBRATION ERROR DATA

Client: E-Grove / Grove Date: 11/11/08
 Location: Scrubbing PL Project No.: 8192
 Calibration Gas: 1010ppm propane, Inc. Cylinder No. 569140087BAL Exp. Date: 9/27/09
 US EPA Method: 25A Analyzer ID: CAI 300 Cylinder Pressure (PSI): 500

Was instrument stable prior to beginning calibrations? YES

Initial Analyzer Calibration using Dilution System

| Range | Dilution Target Level (ppm or %) | Instrument Response (ppm or %) | Difference (ppm or %) | Allowable Difference (ppm or %) | Specification |
|------------|----------------------------------|--------------------------------|-----------------------|---------------------------------|-------------------------|
| Zero | 0.00 | 0.07 | 0.07 | 6.60 | ± 2% of Span |
| Low Range | 75.00 | 74.95 | 0.05 | 3.75 | ± 5% of Gas Value-25A/B |
| Mid Range | 150.00 | 150.48 | 0.48 | 7.50 | ± 5% of Gas Value-25A/B |
| High Range | 300.00 | 299.93 | 0.07 | 15.00 | ± 5% of Gas Value-25A/B |
| Span Value | 330.00 | | | | =110% of High Range Gas |

Hourly System Calibration Error and Zero Drift Checks

| | Run Time (24 Hour Clock) | Initial System Response (ppm or %) | | Final System Response (ppm or %) | | Drift Difference (ppm or %) | | Calibration Drift (percent error) | |
|-------|-----------------------------|------------------------------------|----------|----------------------------------|----------|-----------------------------|----------|-----------------------------------|----------|
| | | Zero | Midscale | Zero | Midscale | Zero | Midscale | Zero | Midscale |
| Run 1 | 12:21 | 0.07 | 150.48 | 0.07 | 150.48 | 0.00 | 0.00 | 0.00 | 0.00 |
| Run 2 | | | | | | | | | |
| Run 3 | | | | | | | | | |
| Run 4 | | | | | | | | | |
| Run 5 | | | | | | | | | |
| Run 6 | | | | | | | | | |

Specification-All must be within ± 3% of span

Field Notes: 50 ppm St. propane = 149.96 ppm Response vs Propane (12.19)

VOC 1

QA/QC Check

| Completeness | Legibility | Accuracy | Specifications | Reasonableness |
|--------------|------------|----------|----------------|----------------|
| | | | | |

SYSTEM CALIBRATION ERROR DATA

| | | | |
|---|------------------------------|--------------------------|---------------------|
| Client: | <u>E Stone / Grove</u> | Date: | <u>11/11/08</u> |
| Location: | <u>Seabrook, FL</u> | Project No.: | <u>8192</u> |
| Calibration Gas: | <u>1000 ppm Argon in Air</u> | Cylinder No.: | <u>SC91400876AC</u> |
| US EPA Method: | <u>205</u> | Analyzer ID: | <u>CAT 3000</u> |
| | | Cylinder Pressure (PSI): | <u>500</u> |
| Was instrument stable prior to beginning calibrations? <u>YES</u> | | | |

Initial Analyzer Calibration using Dilution System

| Range | Dilution Target Level (ppm or %) | Instrument Response (ppm or %) | Difference (ppm or %) | Allowable Difference (ppm or %) | Specification |
|------------|----------------------------------|--------------------------------|-----------------------|---------------------------------|------------------------------|
| Zero | <u>0.00</u> | <u>0.08</u> | <u>0.08</u> | <u>6.60</u> | $\pm 2\%$ of Span |
| Low Range | <u>25.00</u> | <u>25.43</u> | <u>0.43</u> | <u>3.75</u> | $\pm 5\%$ of Gas Value-25A/B |
| Mid Range | <u>150.00</u> | <u>149.44</u> | <u>0.56</u> | <u>7.50</u> | $\pm 5\%$ of Gas Value-25A/B |
| High Range | <u>300.00</u> | <u>301.45</u> | <u>1.45</u> | <u>15.00</u> | $\pm 5\%$ of Gas Value-25A/B |
| Span Value | <u>350.00</u> | | | | $\pm 10\%$ of High Range Gas |

Hourly System Calibration Error and Zero Drift Checks

| | Run Time (24 Hour Clock) | Initial System Response (ppm or %) | | Final System Response (ppm or %) | | Drift Difference (ppm or %) | | Calibration Drift (percent error) | |
|-------|-----------------------------|------------------------------------|---------------|----------------------------------|---------------|-----------------------------|-------------|-----------------------------------|-------------|
| | | Zero | Midscale | Zero | Midscale | Zero | Midscale | Zero | Midscale |
| Run 1 | <u>1315</u> | <u>0.03</u> | <u>149.44</u> | <u>0.08</u> | <u>149.44</u> | <u>0.00</u> | <u>0.00</u> | <u>0.00</u> | <u>0.00</u> |
| Run 2 | | | | | | | | | |
| Run 3 | | | | | | | | | |
| Run 4 | | | | | | | | | |
| Run 5 | | | | | | | | | |
| Run 6 | | | | | | | | | |

Specification-All must be within $\pm 3\%$ of span

Field Notes: 50 ppm Span = 140.43 ppm Response at Range 15 (503)

VOC 2

QA/QC Check

| Completeness | Legibility | Accuracy | Specifications | Reasonableness |
|--------------|------------|----------|-----------------|-----------------|
| <u>ZS</u> | <u>✓</u> | <u>✓</u> | <u>W. Bentz</u> | <u>12/16/08</u> |

Technician (Signature/Date)

Project Manager (Signature/Date)

CEM Event Log

Client: E Stone / Grove
 Location: Sembawang, 1E

Date: 12/8/08
 Technician: F.S.m.Fh

Project No. 8192

| Task | Start Time | End Time | Notes |
|-----------------------------|------------|----------|------------------|
| 205 | 1150 | 1224 | |
| VOC 3 CAH | 1236 | 1306 | and Styrene Cenr |
| Sys CA / Co | 1316 | 1325 | |
| D.rect CA / CO ₂ | 1326 | 1330 | |
| Sys CA / CO ₂ | 1331 | 1336 | |
| STRAT CK | 1350 | 1400 | |
| CA / | 1401 | 1406 | |
| Init CA / | 0647 | 0754 | 12/9/08 |
| CA / | 1015 | 1115 | |
| CA / | 1116 | 1147 | |
| CA / | 1155 | 1255 | |
| CA / | 1256 | 1350 | |
| CA / | 1405 | 1505 | |
| CA / | 1506 | 1538 | |

SYSTEM CALIBRATION ERROR DATA

Protocol Gases

Client: E Stone/Grove Date: 12/18/08
 Location: Sabiney, FL Method: 3A
 Analyzer: Servomex 1400B Technician: F Smith
 ATC Project No.: 8192 Instrument stable prior to calibrations? Yes

PROTOCOL GAS DATA

| Protocol Gas Concentration, % | Pollutant Gas | Dilution Gas | Cylinder Number | Expiration Date |
|-------------------------------|---|--------------|-----------------|-----------------|
| 10.50 | Oxygen | Nitrogen | CC185468 | 08/27/11 |
| 20.9 | Oxygen | Nitrogen | CC166921 | 08/20/11 |
| 20.9 | Span Value (100% of high range calibration gas) | | | |

INITIAL CALIBRATION

| RANGE | Cylinder Pressure (psi) | Cylinder Value (%) | System Response (%) | Difference (%) | Calibration Error (%) |
|-------|-------------------------|--------------------|---------------------|----------------|-----------------------|
| ZERO | 1600 | 0.0 | 0.02 | 0.02 | 0.10 |
| MID | 1900 | 10.50 | 10.48 | 0.02 | 0.10 |
| HIGH | 1300 | 20.9 | 20.96 | 0.06 | 0.29 |

Specification-Methods 3a, 6c, 7e & 10 = $\pm 2\%$ of span value

Field Notes: _____

QA/QC Check

Completeness

Legibility

Accuracy

Specifications

Reasonableness

ZSF 12/18/08
Technician (Signature/Date)

W. Keish Parker 12/16/08
Project Manager (Signature/Date)

Dilution System Verification

US EPA Method 205-40CFR51, Appendix M

ATC Project No.

8192

| Client: <i>E-Stone/ Grove</i> | Location: <i>Sacramento, CA</i> | Date: <i>12/18/08</i> | Technician(s): <i>P. Kish</i> | Instrument Used: Servomex 1400 B High Level Gas Type: Oxygen in Nitrogen Gas Concentration: 20.9% (Cylinder No. CC166921) exp. 8/20/11 US EPA Method (s): 3A | | | | | |
|----------------------------------|------------------------------------|----------------------------|------------------------------------|---|-------|-------|------------------|------------------|-------------|
| Cylinder Number | Gas Type | Protocol Gas Concentration | Actual Reading (ppm or %) | 1 | 2 | 3 | Average Response | Within ± 2% | |
| CC166921 | Mid-level audit | 10.50% | 10.50 | 10.50 | 10.50 | 10.50 | 0.00 | Precision | Accuracy |
| Dilution Number | MFC Flowrate | Dilution Concentration | Trial (record reading in ppm or %) | | 1 | 2 | 3 | Average Response | Within ± 2% |
| 1 | 2.999.3 | 10.0% | 9.98 | 9.99 | 9.99 | 9.987 | 0.07 | 0.13 | 0.12 |
| 2 | 2.999.5 | 2.5% | 2.48 | 2.51 | 2.50 | 2.497 | 0.68 | | |
| 3 | | | | | | | | | |
| 4 | | | | | | | | | |
| 5 | | | | | | | | | |
| 6 | | | | | | | | | |
| 7 | | | | | | | | | |
| 8 | | | | | | | | | |
| 9 | | | | | | | | | |
| 10 | | | | | | | | | |

Precision-Calculate the % difference between the average response and the individual reading that most deviates.

Accuracy-Calculate the % difference between the average response and the predicted response.

QA/QC Check:

✓
Completeness✓
Legibility✓
Accuracy✓
Specifications✓
Reasonableness

Signatures:


W. Karl Pohl 12/16/08

Project Manager (Signature/Date)

SYSTEM CALIBRATION ERROR DATA

Client: E Stone/Grove Date: 12/8/08
 Location: Scrubbing, FL Project No.: 8192
 Calibration Gas: ~~nitrogen propane~~ Cylinder No. 391400873AC Exp. Date: 9/27/09
 US EPA Method: 25A Analyzer ID: BA1 300 Cylinder Pressure (PSI): 500
 Was instrument stable prior to beginning calibrations? YES

Initial Analyzer Calibration using Dilution System

| Range | Dilution Target Level (ppm or %) | Instrument Response (ppm or %) | Difference (ppm or %) | Allowable Difference (ppm or %) | Specification |
|------------|----------------------------------|--------------------------------|-----------------------|---------------------------------|-------------------------------|
| Zero | 0.00 | 0.07 | 0.07 | 6.60 | $\pm 2\%$ of Span |
| Low Range | 75.00 | 75.53 | 0.53 | 3.75 | $\pm 5\%$ of Gas Value-25A/B |
| Mid Range | 150.00 | 149.60 | -0.40 | 7.50 | $\pm 5\%$ of Gas Value-25A/B |
| High Range | 300.00 | 297.80 | -2.20 | 15.00 | $\pm 5\%$ of Gas Value-25A/B |
| Span Value | 330.00 | | | | $\pm 110\%$ of High Range Gas |

Hourly System Calibration Error and Zero Drift Checks

| | Run Time (24 Hour Clock) | Initial System Response (ppm or %) | | Final System Response (ppm or %) | | Drift Difference (ppm or %) | | Calibration Drift (percent error) | |
|-------|-----------------------------|------------------------------------|----------|----------------------------------|----------|-----------------------------|----------|-----------------------------------|----------|
| | | Zero | Midscale | Zero | Midscale | Zero | Midscale | Zero | Midscale |
| Run 1 | 1257 | 0.07 | 149.60 | 0.07 | 150.04 | 0.00 | 0.44 | 0.00 | 0.13 |
| Run 2 | | | | | | | | | |
| Run 3 | | | | | | | | | |
| Run 4 | | | | | | | | | |
| Run 5 | | | | | | | | | |
| Run 6 | | | | | | | | | |

Specification-All must be within $\pm 3\%$ of span

Field Notes: $50 \text{ ppm styrene} = 150.26 \text{ ppm response as propane (1255)}$

VOC 3

QA/QC Check

| Completeness | Legibility | Accuracy | Specifications | Reasonableness |
|-----------------------|------------|----------|------------------------------|----------------|
| <u>T.S.H.</u> 12/8/08 | | | <u>W. Kirk Pool</u> 12/16/08 | |

Technician (Signature/Date)

Project Manager (Signature/Date)

Determination of Stratification

Client: E-Stone/Grove Date: 12/8/08
 Location: Scrubbing, FL Project No.: 8192
 Analyzer ID: SERVO 1400 Analyte: O₂

| | | | |
|-----------------------|-------|-----------------------|-------|
| System Response Time: | 1 min | Minimum Sampling Time | 2 min |
|-----------------------|-------|-----------------------|-------|

| | | | |
|----------------------|-------|-------------|-------|
| Stack Diameter (in): | 22.5 | Port Depth: | 6 |
| Point 1: | 25.58 | Point 2: | 17.25 |

| | | | | | |
|-------------------|-------|--------------------------|-------|------------------|-------|
| Point 1 Average: | 20.85 | Point 2 Average: | 20.90 | Point 3 Average: | 20.95 |
| Combined Average: | 20.90 | Largest Precision Error: | 0.24 | | |

Points used for test:

- If the Largest Precision Error is 5.0% or less or if the greatest difference is less than +/- 0.5 ppm (0.3% O₂/CO₂) a single point traverse may be used.
- If the Largest Precision Error is more than 5.0% but 10.0% or less or if the greatest difference is less than +/- 1.0 ppm (0.5% O₂/CO₂) a three point traverse may be used.
*If stack is larger than 2.4 meters three point sampling can be placed at .4, 1.0 and 2.0 meters from the duct wall.
- If the Largest Precision Error is more than 10.0% and the greatest difference is more than +/- 1.0 ppm (0.5% O₂/CO₂) a twelve point traverse must be used.

Field Notes:

Pf 1/350 - 1557

Pf 2/352 - 1353

Pf 3/354 - 1355

Analyst:

Date: 12/8/08

Data Reviewed By:

W. Kish Pal

Date: 12/16/08

Determination of Stratification

Client: E Stone / Grove Date: 12/8/08
 Location: Scrubbing, FL Project No.: 8192
 Analyzer ID: 5000A 1440 Analyte: CO₂

| | | | |
|-----------------------|-------|-----------------------|-------|
| System Response Time: | 1 min | Minimum Sampling Time | 2 min |
|-----------------------|-------|-----------------------|-------|

| | | | |
|----------------------|-------|-------------|-------|
| Stack Diameter (in): | 22.5 | Port Depth: | 6 |
| Point 1: | 25.58 | Point 2: | 17.25 |

| | | | | | |
|-------------------|-------|--------------------------|------|------------------|------|
| Point 1 Average: | 0.17 | Point 2 Average: | 0.18 | Point 3 Average: | 0.18 |
| Combined Average: | 0.177 | Largest Precision Error: | 3.95 | | |

Points used for test:

- If the Largest Precision Error is 5.0% or less or if the greatest difference is less than +/- 0.5 ppm (0.3% O₂/CO₂) a single point traverse may be used.
- If the Largest Precision Error is more than 5.0% but 10.0% or less or if the greatest difference is less than +/- 1.0 ppm (0.5% O₂/CO₂) a three point traverse may be used.
*If stack is larger than 2.4 meters three point sampling can be placed at .4, 1.0 and 2.0 meters from the duct wall.
- If the Largest Precision Error is more than 10.0% and the greatest difference is more than +/- 1.0 ppm (0.5% O₂/CO₂) a twelve point traverse must be used.

Field Notes: PT1 1350-1351 (Geostat diff. is .007)
 PT2 1352-1353
 PT3 1354-1355

| | |
|------------------------------|----------------|
| Analyst: ZH | Date: 12/8/08 |
| Data Reviewed By: W.Kirk.Pot | Date: 12/16/08 |

SYSTEM CALIBRATION ERROR DATA

Client: E. Stone / Grove Location: Scrubbing, FL Date: 12/8/08 Project No: 8192
 Calibration Gas: 20.9% O₂ in N₂ Cylinder No.: CC166921 Exp. Date: 8/20/11 Cylinder Pressure (PSI): 1300
 US EPA Method: 3A Analyzer ID: SERVO 1400 Was Instrument stable prior to beginning calibration? YES

| Initial Analyzer Direct Calibration using Dilution System | | | | | |
|---|-------------------------------------|-----------------------------------|--------------------------|------------------------------------|-----------------------------|
| Range | Dilution Target Level (ppm or %) | Instrument Response (ppm or %) | Difference (ppm or %) | Allowable Difference (ppm or %) | Specification |
| Low Range (Zero) | 0.00 | 0.02 | 0.02 | 0.42 | ± 2% of Span |
| Mid Range | 10.00 | 9.99 | 0.01 | 0.42 | ± 2% of Span-3a, 6c, 7e, 10 |
| High Range (Span) | 20.90 | 20.96 | 0.06 | 0.42 | ± 2% of Span-3a, 6c, 7e, 10 |

Initial and Post System Bias and Drift Checks

| Run Time (24 Hour Clock) | Direct Response (ppm or %) | | System Response (ppm or %) | | System Bias (ppm or %) | | System Bias (percent error) | | Calibration Drift (ppm or %) | | Calibration Drift (percent error) | |
|--------------------------------|-------------------------------|----------|-------------------------------|----------|---------------------------|----------|--------------------------------|----------|---------------------------------|----------|--------------------------------------|----------|
| | Zero | Midscale | Zero | Midscale | Zero | Midscale | Zero | Midscale | Zero | Midscale | Zero | Midscale |
| Pre | 1316 | 0.00 | 1000 | 0.02 | 10.01 | 0.02 | 0.01 | 0.10 | 0.05 | | | |
| Run 1 | 1401 | 0.00 | 20.90 | 0.02 | 20.91 | 0.02 | 0.01 | 0.10 | 0.05 | 0.00 | NA | 0.00 |
| Run 2 | | | | | | | | | | | | |
| Run 3 | | | | | | | | | | | | |
| Run 4 | | | | | | | | | | | | |
| Run 5 | | | | | | | | | | | | |

Specification - System Bias: must be within ± 5% of Direct Response; Calibration Drift: must be within ± 3% of span of previous System Response

Field Notes: * Shot High Range due to #'s from Stack

QA/QC Check

Completeness ✓ Legibility ✓ Accuracy ✓ Specifications ✓ Reasonableness ✓

Technician (Signature/Date)

12/8/08

Project Manager (Signature/Date)

ATC @ 1-800-733-3193

SYSTEM CALIBRATION ERROR DATA

Client: E Stone / Grove Location: SARASOTA, FL Date: 12/8/08 Project No: B192
 Calibration Gas: 20.99% C₂H₆ Cylinder No.: CC10006 Exp. Date: 2/12/11 Cylinder Pressure (PSI): 800
 US EPA Method: 3A Analyzer ID: SORVO 1440 Was Instrument stable prior to beginning calibration? YES

Initial Analyzer Direct Calibration using Dilution System

| Range | Dilution Large Level (ppm or %) | Instrument Response (ppm or %) | Difference (ppm or %) | Allowable Difference (ppm or %) | Specification |
|-------------------|---------------------------------|--------------------------------|-----------------------|---------------------------------|-----------------------------|
| Low Range (Zero) | 0.00 | 0.03 | 0.03 | 0.42 | ± 2% of Span |
| Midscale | 10.00 | 10.11 | 0.11 | 0.42 | ± 2% of Span-3a, 6c, 7e, 10 |
| High Range (Span) | 20.99 | 20.99 | 0.00 | 0.42 | ± 2% of Span-3a, 6c, 7e, 10 |

Initial and Post System Bias and Drift Checks

| Run Time (24-Hour Clock) | Direct Response (ppm or %) | | System Response (ppm or %) | | System Bias (ppm or %) | | Calibration Drift (ppm or %) | | Calibration Drift (percent error) | |
|--------------------------|----------------------------|----------|----------------------------|----------|------------------------|----------|------------------------------|----------|-----------------------------------|----------|
| | Zero | Midscale | Zero | Midscale | Zero | Midscale | Zero | Midscale | Zero | Midscale |
| Pre | 1310 | 0.00 | 10.00 | 0.03 | 10.02 | 0.03 | 0.02 | 0.14 | 0.10 | |
| Run 1 | 1401 | 0.00 | 10.00 | 0.03 | 10.05 | 0.03 | 0.05 | 0.14 | 0.24 | 0.00 |
| Run 2 | | | | | | | | | | |
| Run 3 | | | | | | | | | | |
| Run 4 | | | | | | | | | | |
| Run 5 | | | | | | | | | | |

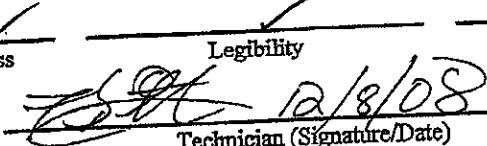
Specification - System Bias: must be within ± 5% of Direct Response; Calibration Drift: must be within ± 3% of span of previous System Response

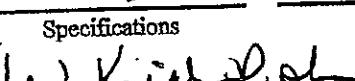
Field Notes:

QA/QC Check

Completeness ✓ Legibility ✓ Accuracy ✓ Specifications ✓ Reasonableness ✓

Technician (Signature/Date)


 12/8/08


 12/16/08

Project Manager (Signature/Date)

ATC @ 1-800-733-3193

SYSTEM CALIBRATION ERROR DATA

Client: E Stone/Grove Date: 12/9/08
 Location: Seabrook, FL Project No.: 8192
 Calibration Gas: 1000 ppm Argon/air Cylinder No.: SF914008734 Exp. Date: 9/27/09
 US EPA Method: 25A Analyzer ID: CAT 300 Cylinder Pressure (PSI): 500

Was instrument stable prior to beginning calibrations? YES

Initial Analyzer Calibration using Dilution System

| Range | Dilution Target Level (ppm or %) | Instrument Response (ppm or %) | Difference (ppm or %) | Allowable Difference (ppm or %) | Specification |
|------------|----------------------------------|--------------------------------|-----------------------|---------------------------------|-------------------------|
| Zero | 0.00 | 0.02 | 0.02 | ±2.00 | +10% of Span |
| Low Range | 25.00 | 25.01 | 0.01 | ±0.50 | ±5% of Gas Value-25A/B |
| Mid Range | 50.00 | 50.50 | 0.50 | ±5.00 | ±5% of Gas Value-25A/B |
| High Range | 100.00 | 98.76 | 1.24 | ±5.00 | ±5% of Gas Value-25A/B |
| Span Value | 110.00 | | | | =110% of High Range Gas |

Hourly System Calibration Error and Zero Drift Checks

| | Run Time (24 Hour Clock) | Initial System Response (ppm or %) | | Final System Response (ppm or %) | | Drift Difference (ppm or %) | | Calibration Drift (percent error) | |
|-------|-----------------------------|------------------------------------|----------|----------------------------------|----------|-----------------------------|----------|-----------------------------------|----------|
| | | Zero | Midscale | Zero | Midscale | Zero | Midscale | Zero | Midscale |
| Run 1 | 116 | 0.02 | 25.01 | 0.02 | 25.45 | 0.44 | 0.44 | 0.00 | 0.40 |
| Run 2 | 1256 | 0.02 | 25.01 | 0.02 | 25.20 | 0.00 | 0.19 | 0.00 | 0.17 |
| Run 3 | 1506 | 0.02 | 25.01 | 0.02 | 25.13 | 0.00 | 0.12 | 0.00 | 0.17 |
| Run 4 | | | | | | | | | |
| Run 5 | | | | | | | | | |
| Run 6 | | | | | | | | | |

Specification-All must be within +3% of span

Field Notes: VOC

QA/QC Check

| Completeness | Legibility | Accuracy | Specifications | Reasonableness |
|-------------------|------------|----------|--------------------------|----------------|
| <u>KH</u> 12/9/08 | | | <u>W. Kline</u> 12/16/08 | |

Technician (Signature/Date) Project Manager (Signature/Date)

SYSTEM CALIBRATION ERROR DATA

| | |
|---|--|
| Client: <u>E-Stone/Grove</u> | Date: <u>12/9/08</u> |
| Location: <u>Sarasota, FL</u> | Project No.: <u>8192</u> |
| Calibration Gas: <u>1000 ppm LPG</u> | Cylinder No.: <u>58940087BAC</u> Exp. Date: <u>9/27/09</u> |
| US EPA Method: <u>25A</u> | Analyzer ID: <u>CAI 300M</u> Cylinder Pressure (PSI): <u>500</u> |
| Was instrument stable prior to beginning calibrations? <u>YES</u> | |

Initial Analyzer Calibration using Dilution System

| Range | Dilution Target Level (ppm or %) | Instrument Response (ppm or %) | Difference (ppm or %) | Allowable Difference (ppm or %) | Specification |
|------------|----------------------------------|--------------------------------|-----------------------|---------------------------------|-------------------------|
| Zero | 0.00 | 0.08 | 0.08 | 6.60 | ± 2% of Span |
| Low Range | 75.00 | 75.10 | 0.10 | 3.75 | ± 5% of Gas Value-25A/B |
| Mid Range | 150.00 | 150.72 | 0.72 | 7.50 | ± 5% of Gas Value-15A/B |
| High Range | 300.00 | 300.84 | 0.84 | 15.00 | ± 5% of Gas Value-25A/B |
| Span Value | 350.00 | | | | =110% of High Range Gas |

Hourly System Calibration Error and Zero Drift Checks

| | Run Time (24 Hour Clock) | Initial System Response (ppm or %) | | Final System Response (ppm or %) | | Drift Difference (ppm or %) | | Calibration Drift (percent error) | |
|-------|-----------------------------|------------------------------------|----------|----------------------------------|----------|-----------------------------|----------|-----------------------------------|----------|
| | | Zero | Midscale | Zero | Midscale | Zero | Midscale | Zero | Midscale |
| Run 1 | 1116 | 0.08 | 75.10 | 0.08 | 74.87 | 0.00 | 0.23 | 0.00 | 0.07 |
| Run 2 | 1256 | 0.08 | 75.10 | 9.40 | 76.91 | 9.38 | -0.38 | 2.84 | 0.55 |
| Run 3 | 1506 | 0.08 | 75.10 | 8.33 | 75.10 | 8.25 | -0.81 | 2.50 | 0.00 |
| Run 4 | | | | | | | | | |
| Run 5 | | | | | | | | | |
| Run 6 | | | | | | | | | |

Specification-All must be within + 3% of span

Field Notes: VOC 2

QA/QC Check

| | | | | | | | | |
|-----------------------------|-------------------------------------|------------|-------------------------------------|----------------------------------|-------------------------------------|----------------|-------------------------------------|----------------|
| Completeness | <input checked="" type="checkbox"/> | Legibility | <input checked="" type="checkbox"/> | Accuracy | <input checked="" type="checkbox"/> | Specifications | <input checked="" type="checkbox"/> | Reasonableness |
| <u>L. Kirk 12/9/08</u> | | | | <u>W. Kirk Pote 12/16/08</u> | | | | |
| Technician (Signature/Date) | | | | Project Manager (Signature/Date) | | | | |

SYSTEM CALIBRATION ERROR DATA

Client: E Stone Grove Date: 12/9/08
 Location: Seraberg, FL Project No.: 8192
 Calibration Gas: 1010 ppm ~~Keynes w/ 8%~~ Cylinder No. 56-914-0087541 Exp. Date: 9/27/09
 US EPA Method: 25A Analyzer ID: CA.I.300 Cylinder Pressure (PSI): 500
 Was instrument stable prior to beginning calibrations? YES

Initial Analyzer Calibration using Dilution System

| Range | Dilution Target Level (ppm or %) | Instrument Response (ppm or %) | Difference (ppm or %) | Allowable Difference (ppm or %) | Specification |
|------------|----------------------------------|--------------------------------|-----------------------|---------------------------------|-------------------------|
| Zero | 0.00 | 0.24 | 0.24 | 22.00 | ± 2% of Span |
| Low Range | 250.00 | 248.35 | 1.65 | 12.50 | ± 5% of Gas Value-25A/B |
| Mid Range | 500.00 | 500.37 | 0.37 | 25.00 | ± 5% of Gas Value-25A/B |
| High Range | 1000.00 | 999.76 | 0.24 | 50.00 | ± 5% of Gas Value-25A/B |
| Span Value | 1.100.00 | | | | =110% of High Range Gas |

Hourly System Calibration Error and Zero Drift Checks

| | Run Time (24 Hour Clock) | Initial System Response (ppm or %) | | Final System Response (ppm or %) | | Drift Difference (ppm or %) | | Calibration Drift (percent error) | |
|-------|-----------------------------|------------------------------------|----------|----------------------------------|----------|-----------------------------|----------|-----------------------------------|----------|
| | | Zero | Midscale | Zero | Midscale | Zero | Midscale | Zero | Midscale |
| Run 1 | 11/6 | 0.24 | 500.37 | 0.26 | 501.06 | 0.02 | 0.91 | 0.002 | 0.08 |
| Run 2 | 12/5/08 | 0.24 | 500.37 | 0.26 | 503.85 | 0.02 | 3.48 | 0.002 | 0.32 |
| Run 3 | 150/0 | 0.24 | 500.37 | 0.26 | 503.08 | 0.02 | 2.71 | 0.002 | 0.25 |
| Run 4 | | | | | | | | | |
| Run 5 | | | | | | | | | |
| Run 6 | | | | | | | | | |

Specification-All must be within ± 3% of span

Field Notes: VOC 3

QA/QC Check

| Completeness | Legibility | Accuracy | Specifications | Reasonableness |
|--------------|------------|----------|----------------|----------------|
| | | | | |

SYSTEM CALIBRATION ERROR DATA

Client: E STONE/GROVE Location: Seabreeze, FL Date: 12/9/08 Project No: 8192
 Calibration Gas: 20.9% O₂ in N₂ Cylinder No.: CC1666921 Exp. Date: 8/20/11 Cylinder Pressure (PSI): 1300
 US EPA Method: 3A Analyzer ID: SERVO 400 Was Instrument stable prior to beginning calibration? YES

Initial Analyzer Direct Calibration using Dilution System

| Range | Dilution Target Level (ppm or %) | Instrument Response (ppm or %) | Difference (ppm or %) | Allowable Difference (ppm or %) | Specification |
|-------------------|----------------------------------|--------------------------------|-----------------------|---------------------------------|-----------------------------|
| Low Range (Zero) | 0.00 | 0.02 | 0.02 | 0.42 | ± 2% of Span |
| Mid Range | 10.00 | 10.01 | 0.01 | 0.42 | ± 2% of Span-3a, 6c, 7e, 10 |
| High Range (Span) | 20.90 | 20.87 | 0.03 | 0.42 | ± 2% of Span-3a, 6c, 7e, 10 |

Initial and Post System Bias and Drift Checks

| Run Time 24 Hour Clock | Direct Response (ppm or %) | System Response (ppm or %) | | System Bias (ppm or %) | | Calibration Drift (ppm or %) | | Calibration Drift (percent error) | |
|------------------------------|-------------------------------|-------------------------------|----------|---------------------------|----------|---------------------------------|----------|--------------------------------------|----------|
| | | Zero | Midscale | Zero | Midscale | Zero | Midscale | Zero | Midscale |
| Pre | 0700 | 0.00 | 20.90 | 0.02 | 20.88 | 0.02 | 0.02 | 0.10 | 0.10 |
| Run 1 | 1116 | 0.00 | 20.90 | 0.02 | 20.90 | 0.02 | 0.00 | 0.10 | 0.02 |
| Run 2 | 1256 | 0.00 | 20.90 | 0.02 | 20.90 | 0.02 | 0.00 | 0.10 | 0.02 |
| Run 3 | 1501 | 0.00 | 20.90 | 0.02 | 20.87 | 0.02 | 0.03 | 0.10 | 0.14 |
| Run 4 | | | | | | | | | |
| Run 5 | | | | | | | | | |

Specification - System Bias: must be within ± 5% of Direct Response; Calibration Drift: must be within ± 3% of span of previous System Response

Field Notes:

QA/QC Check

Completeness

Legibility

Accuracy

Specifications

Reasonableness

✓ ✓ ✓ ✓ ✓ ✓

12/9/08 12/9/08 12/9/08 12/9/08 12/9/08 12/9/08

Technician (Signature/Date)

Project Manager (Signature/Date)

ATC @ 1-800-733-3193

SYSTEM CALIBRATION ERROR DATA

Client: E-Stone / Grove Location: Seabrook, FL Date: 12/9/08 Project No: 8192
 Calibration Gas: 29997LCB.i16 Cylinder No.: CC100061 Exp. Date: 2/12/11 Cylinder Pressure (PSI): 800
 US EPA Method: 3A Analyzer ID: S0200 1440 Was Instrument stable prior to beginning calibration? YES

Initial Analyzer Direct Calibration using Dilution System

| Range | Dilution Target Level (ppm or %) | Instrument Response (ppm or %) | Difference (ppm or %) | Allowable Difference (ppm or %) | Specification (ppm or %) |
|-------------------|-------------------------------------|-----------------------------------|--------------------------|------------------------------------|-----------------------------|
| Low Range (Zero) | 0.00 | 0.03 | 0.03 | 0.42 | ± 2% of Span |
| Mid Range | 10.00 | 9.96 | 0.04 | 0.42 | ± 2% of Span-3a, 6c, 7e, 10 |
| High Range (Span) | 20.99 | 20.96 | 0.03 | 0.42 | ± 2% of Span-3a, 6c, 7e, 10 |

Initial and Post System Bias and Drift Checks

| Run Time (24 Hour clock) | Direct Response (ppm or %) | | System Response (ppm or %) | | System Bias (ppm or %) | | System Bias (percent error) | | Calibration Drift (ppm or %) | | Calibration Drift (percent error) | |
|-----------------------------------|-------------------------------|----------|-------------------------------|----------|---------------------------|----------|--------------------------------|----------|---------------------------------|----------|--------------------------------------|----------|
| | Zero | Midscale | Zero | Midscale | Zero | Midscale | Zero | Midscale | Zero | Midscale | Zero | Midscale |
| Pre | 0.02 | 10.00 | 0.03 | 9.99 | 0.03 | 0.01 | 0.14 | 0.05 | | | | |
| Run 1 | 1114 | 0.00 | 10.00 | 0.03 | 10.02 | 0.03 | 0.02 | 0.14 | 0.10 | 0.00 | 0.03 | 0.00 |
| Run 2 | 1256 | 0.00 | 10.00 | 0.03 | 10.02 | 0.03 | 0.02 | 0.14 | 0.10 | 0.00 | 0.00 | 0.00 |
| Run 3 | 1506 | 0.00 | 10.00 | 0.03 | 10.02 | 0.03 | 0.02 | 0.14 | 0.10 | 0.00 | 0.00 | 0.00 |
| Run 4 | | | | | | | | | | | | |
| Run 5 | | | | | | | | | | | | |

Specification - System Bias: must be within $\pm 5\%$ of Direct Response; Calibration Drift: must be within $\pm 3\%$ of span of previous System Response

Field Notes:

QA/QC Check

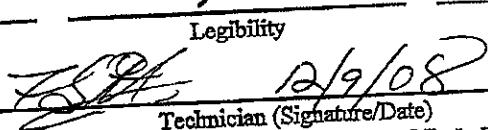
Completeness

Legibility

Accuracy

Specifications

Reasonableness

 12/9/08 W. K. Jr. Jr. 12/16/08
 Technician (Signature/Date) Project Manager (Signature/Date)

ATC @ 1-800-733-3193

Analytical Testing Consultants, Inc.

Kannapolis, NC (1-800-733-3193)

Traverse Data and Flow Computations

| | | | |
|-------------|------------------------|----------------|------------------|
| Client | <u>E-Stone / Grove</u> | Date | <u>12/9/08</u> |
| Location | <u>SCHENKES PL</u> | Source | <u>BoatHouse</u> |
| Test Team | <u>BK JTB'</u> | Run # | <u>PRELIM.</u> |
| Project No. | <u>8792</u> | | |
| Pbar | <u>-</u> | Dry Bulb, °F | |
| Time | <u>12:00</u> | sp, "Hg or "Wg | <u>-0.52</u> |
| Pitot # | <u>57</u> | Fs for Pitot | <u>0.81</u> |

| Traverse Point | Vp, in. H ₂ O | Square Root,Vp | Stack Temp, °F | Cyclonic Flow Data | |
|----------------|--------------------------|----------------|----------------|--------------------|--------------|
| | | | | dP @ 0° | Angle @ 0 dP |
| A1 | 0.52 | | 59 | 0 | |
| A2 | 0.71 | | 61 | | |
| A3 | 0.74 | | 61 | | 5 |
| A4 | 0.76 | | 62 | | |
| A5 | 0.81 | | 63 | | 0 |
| A6 | 0.80 | | 64 | | |
| A7 | 0.82 | | 65 | | 5 |
| A8 | 0.70 | | 66 | | |
| A9 | | | | | |
| A10 | | | | | |
| A11 | | | | | |
| A12 | | | | | |
| B1 | 0.51 | | 68 | 0 | 5 |
| B2 | 0.60 | | 68 | | |
| B3 | 0.66 | | 67 | | 2 |
| B4 | 0.85 | | 67 | | |
| B5 | 0.90 | | 67 | | 5 |
| B6 | 0.67 | | 67 | | |
| B7 | 0.65 | | 67 | | |
| B8 | 0.65 | | 67 | | |
| B9 | | | | | |
| B10 | | | | | |
| B11 | | | | | |
| B12 | | | | | |

Verify
Not
cyclonic
Previously
tested
source
-Bk

Equations

Ts(Rankin) = ts(avg) + 459.69 =

Duct Area (A = pi*r²) Ft² A =

Ps = Pbar + sp

Rho x (530/Ts) x (Ps/29.92) = (lbs/ft³)

K = 1098.5(Gas Density^{1/2}) =

Velocity (ft/min)=K x Fs x (Vp avg)^{1/2}=

Volume (avg ACFM)= A x V =

SCFM(wet)=Volx(530/Ts)x(Ps/29.92)=

SCFM(Dry)=A x V x MD x 17.647 x (Ps/Ts)=

**Rho=0.075 lbs/ft³

Pm=Pbar+(avg.dH/13.6)=

Vm =

Vv std = (0.04708*SIO₂ in gms)+(0.04717*VLQ in ml)=

Vm std=Y*(Vm*528*Pm)/(Tm*29.92)=

V std = Vm std + Vv std =

%M=Vv std/V std * 100=

MD=(100-%M)/100 =

Pitot Tube Leak Checks

Pre-test Post-test

A A

B B

2006
16092
88F

QA/QC Check:

Completeness

Legibility

Accuracy

Specifications

Reasonableness

Signatures:

Technician (Signature/Date)

Project Manager (Signature/Date)

Analytical Testing Consultants, Inc.

Kannapolis, NC (1-800-733-3193)

Traverse Data and Flow Computations

| | | | | | |
|-------------|----------------------|----------------|--------------|------------------|----------------|
| Client | <u>E-Stone/Grove</u> | | Date | <u>12/9/08</u> | |
| Location | <u>Spring, NC</u> | | Source | <u>Boathouse</u> | |
| Test Team | <u>BL SD</u> | | Run # | <u>1</u> | |
| Project No. | <u>8192</u> | | | | |
| Pbar | <u>30.05</u> | Dry Bulb, °F | <u>88</u> | Wet Bulb, °F | <u>76</u> |
| Time | <u>1135</u> | sp. "Hg or "Wg | <u>-0.25</u> | Pitot Type | <u>3. TYPE</u> |
| Pitot # | <u>57</u> | Fs for Pitot | <u>0.84</u> | Stack I.D. | <u>32.5</u> |

| Traverse Point | Vp, in. H ₂ O | Square Root,Vp | Stack Temp, °F | Cyclonic Flow Data | |
|----------------|--------------------------|----------------|----------------|--------------------|--------------|
| | | | | dP @ 0o | Angle @ 0 dP |
| A1 | 0.53 | | 88 | | |
| A2 | 0.69 | | 89 | | |
| A3 | 0.83 | | 89 | | |
| A4 | 0.90 | | 89 | | |
| A5 | 0.89 | | 89 | | |
| A6 | 0.87 | | 89 | | |
| A7 | 0.89 | | 89 | | |
| A8 | 0.87 | | 89 | | |
| A9 | | | | | |
| A10 | | | | | |
| A11 | | | | | |
| A12 | | | | | |
| B1 | 0.55 | | 88 | | |
| B2 | 0.58 | | 88 | | |
| B3 | 0.59 | | 88 | | |
| B4 | 0.58 | | 88 | | |
| B5 | 0.57 | | 88 | | |
| B6 | 0.58 | | 89 | | |
| B7 | 0.62 | | 89 | | |
| B8 | 0.70 | | 89 | | |
| B9 | | | | | |
| B10 | | | | | |
| B11 | | | | | |
| B12 | | | | | |

Equations

Ts(Rankin) = Ts(avg) + 459.69 =

Duct Area (A = πr^2) ft² A =

Ps = Pbar + sp

Rho x (530/Ts) x (Ps/29.92) = (lbs/ft³)

K = 1096.5/(Gas Density^{1/2}) =

Velocity (ft/min)=K x Fs x (Vp avg)^{1/2}=

Volume (avg ACFM)= A x V =

SCFM(wet)=Volx(S30/Ts)x(Ps/29.92)=

SCFM(Dry)=A x V x MD x 17.647 x (Ps/Ts)=

**Rho=0.075 lbs/ft³

Pm=Pbar+(avg.dH/13.6)*

Vm =

Vv std = (0.04708*SO₂ in gms)+(0.04717*VLQ in ml)=

Vm std=Y*(Vm*6281Pm)/(Tr*29.92)=

V std=Vm std +Vv std =

%M=Vv std/V std * 100=

MD=(100-%M)/100 =

Pitot Tube Leak Checks

Pre-test Post-test

| | | | |
|---|---|---|---|
| A | ✓ | A | ✓ |
| B | ✓ | B | ✓ |

QA/QC Check:

Completeness

Legibility

Accuracy

Specifications

Reasonableness

Signatures:

Technician (Signature/Date)

Project Manager (Signature/Date)

Analytical Testing Consultants, Inc.

Kannapolis, NC (1-800-733-3193)

Traverse Data and Flow Computations

| | | | |
|-------------|-----------------------|----------------|-----------------|
| Client | <u>E-Stone /Grove</u> | Date | <u>12-9-08</u> |
| Location | <u>Selbyville, FL</u> | Source | <u>Baghouse</u> |
| Test Team | <u>BL, JB</u> | Run # | <u>2</u> |
| Project No. | <u>8192</u> | | |
| Pbar | <u>30.05</u> | Dry Bulb, °F | <u>89</u> |
| Time | <u>12:57</u> | sp, "Hg or "Wg | <u>-0.24</u> |
| Pitot # | <u>57</u> | Fs for Pitot | <u>0.54</u> |

| Traverse Point | Vp, in. H ₂ O | Square Root,Vp | Stack Temp, °F | Cyclonic Flow Data | |
|----------------|--------------------------|----------------|----------------|--------------------|--------------|
| | | | | dP @ 0o | Angle @ 0 dP |
| A1 | 0.44 | | 82 | 100 | 89 |
| A2 | 0.51 | | 83 | 100 | 88 |
| A3 | 0.53 | | 84 | 100 | 89 |
| A4 | 0.56 | | 82 | 100 | 89 |
| A5 | 0.72 | | 82 | 100 | 89 |
| A6 | 0.77 | | 82 | 100 | 89 |
| A7 | 0.78 | | 82 | 100 | 89 |
| A8 | 0.80 | | 82 | 100 | 89 |
| A9 | | | | | |
| A10 | | | | | |
| A11 | | | | | |
| A12 | | | | | |
| B1 | 0.46 | | 82 | 100 | 89 |
| B2 | 0.55 | | 82 | 100 | 89 |
| B3 | 0.76 | | 82 | 100 | 89 |
| B4 | 0.80 | | 82 | 100 | 89 |
| B5 | 0.80 | | 82 | 100 | 90 |
| B6 | 0.79 | | 82 | 100 | 89 |
| B7 | 0.76 | | 82 | 100 | 88 |
| B8 | 0.76 | | 82 | 100 | 88 |
| B9 | | | | | |
| B10 | | | | | |
| B11 | | | | | |
| B12 | | | | | |

Equations

Ts(Rankin) = Ts(avg) + 458.68 =

Duct Area (A = pi*r²) Ft² A =

Ps = Pbar + sp

Rho x (530/Ts) x (Ps/29.92) = (lbs/ft³)

K = 1096.6/(Gas Density)^{1/2} =

Velocity (ft/min)=K x Fs x (Vp avg)^{1/2}=

Volume (avg ACFM)= A x V =

SCFM(wet)=Volx(530/Ts)x(Ps/29.92)=

SCFM(Dry)=A x V x MD x 17.647 x (Ps/Ts)=

**Rho=0.075 lbs/ft³

Pm=Pbar+(avg.dH/13.6)=

Vm =

Vv std = (0.04708*SiO₂ in gms)+(0.04717*VLQ in ml)=

Vm std=Y*(Vm*528*Pm)/(Tm*29.92)=

V std = Vm std + Vv std =

%M=V/v std/V std * 100=

MD=(100-%M)/100 =

Pitot Tube Leak Checks

Pre-test Post-test

A A
B B

QA/QC Check:

Completeness

Legibility

Accuracy

Specifications

Reasonableness

Signatures:

Technician (Signature/Date)

Project Manager (Signature/Date)

Analytical Testing Consultants, Inc.

Kannapolis, NC (1-800-733-3193)

Traverse Data and Flow Computations

| | | | |
|-------------|-----------------------|----------------|-----------------|
| Client | <u>E-Stone /Grove</u> | Date | <u>12.5.08</u> |
| Location | <u>Sebring, FL</u> | Source | <u>BAGHOUSE</u> |
| Test Team | <u>BK PD</u> | Run # | <u>3</u> |
| Project No. | <u>8192</u> | | |
| Pbar | <u>30.05</u> | Dry Bulb, °F | <u>88</u> |
| Time | <u>1525</u> | sp. "Hg or "Wg | <u>-0.25</u> |
| Pilot # | <u>57</u> | Fs for Pilot | <u>0.87</u> |

| Traverse Point | Vp, in. H ₂ O | Square Root,Vp | Stack Temp, oF | Cyclonic Flow Data | |
|----------------|--------------------------|----------------|----------------|--------------------|--------------|
| | | | | dP @ 0o | Angle @ 0 dP |
| A1 | 0.46 | | 95 | | |
| A2 | 0.55 | | 95 | | |
| A3 | 0.57 | | 95 | | |
| A4 | 0.59 | | 94 | | |
| A5 | 0.64 | | 94 | | |
| A6 | 0.65 | | 94 | | |
| A7 | 0.65 | | 94 | | |
| A8 | 0.65 | | 94 | | |
| A9 | | | | | |
| A10 | | | | | |
| A11 | | | | | |
| A12 | | | | | |
| B1 | 0.50 | | 84 | | |
| B2 | 0.57 | | 94 | | |
| B3 | 0.60 | | 94 | | |
| B4 | 0.71 | | 94 | | |
| B5 | 0.74 | | 95 | | |
| B6 | 0.71 | | 94 | | |
| B7 | 0.72 | | 95 | | |
| B8 | 0.74 | | 96 | | |
| B9 | | | | | |
| B10 | | | | | |
| B11 | | | | | |
| B12 | | | | | |

Equations

Ts(Rankin) = ts(avg) + 469.69 =

Duct Area (A = pi*r²) F₁² A=

Ps= Pbar + sp

Rho x (530/Ts) x (Ps/29.92) = (lbs/ft³)

K = 1096.5/(Gas Density)^{1/2} =

Velocity (ft/min)=K x F₁ x (Vp avg)^{1/2}=

Volume (avg ACFM)= A x V =

SCFM(wet)=Volx(530/Ts)x(Ps/29.92)=

SCFM(Dry)=A x V x MD x 17.647 x (Ps/Ts)=

**Rho=0.075 lbs/ft³

Pm=Pbar+(avg.dH/13.6)=

Vm =

Vv std = (0.04708*SIO₂ in gms)+(0.04717*VLQ in ml)=

Vm std=Y*(Vm*528*Pm)/(Tm*29.92)=

V std=Vm std +Vv std =

%M=Vv std/V std * 100=

MD=(100-%M)/100 =

Pilot Tube Leak Checks

Pre-test Post-test

| | | | |
|---|---|---|---|
| A | ✓ | A | ✓ |
| B | ✓ | B | ✓ |

QA/QC Check:

Completeness

Legibility

Accuracy

Specifications

Reasonableness

Signatures:

Technician (Signature/Date)

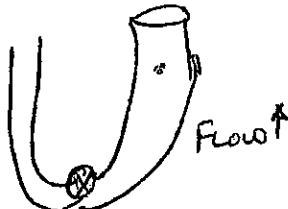
Project Manager (Signature/Date)

SOURCE SURVEY AND DESCRIPTION

CLIENT: E-Stone /Grove Project No. 8192PERSONNEL COMPLETING SURVEY: BAL DATE: 12/8/08SYSTEM TYPE: BOILER PROCESS X OTHER BAGHOUSE
NARRATIVE DESCRIPTION:*Baghouse outlet*

PURPOSE OF TESTING: COMPLIANCE EVALUATION _____
 PROCESS RATE OR CAPACITY: 1351485 l/hr ± 10% DETERMINED BY: FACILITY
 CONTROL EQUIPMENT: MULTI-CLONE SCRUBBER BAGHOUSE X
ELECTROSTATIC PRECIPITATOR OTHER
 CONTROL EQUIPMENT OPERATING PARAMETERS:
 PRESSURE DROP OTHER _____
 SAMPLING LOCATION DATA:
 DISTANCE DOWNSTREAM FROM FLOW DISTURBANCE: 187
 NATURE OF DISTURBANCE: BEND, FAN, EXPANSION, BYPASS, DUCT,
 OTHER 187 ft
 DISTANCE UPSTREAM FROM FLOW DISTURBANCE: 112
 NATURE OF DISTURBANCE: STACK EXHAUST, FAN, EXPANSION, DUCT,
 OTHER _____
 INDIVIDUAL STACK COMMON STACK _____
 STACK DIAMETER OR DIMENSIONS: 32.5
 NUMBER OF PORTS: 2 POINTS PER PORT: 8

SKETCH:

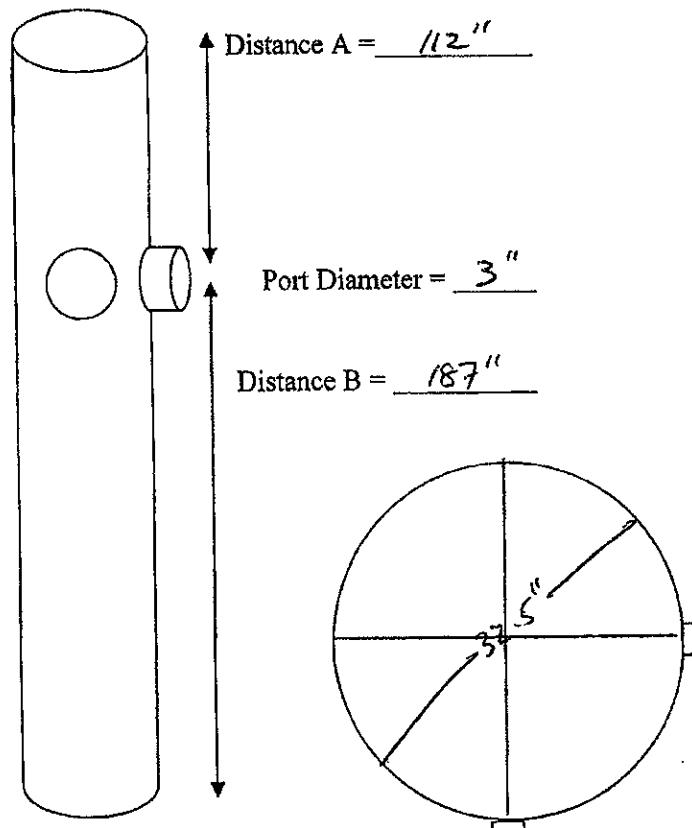


ESTIMATED TEMPERATURE: Ambient ESTIMATED MOISTURE: 2-3%
 GAS COMPOSITION BY: FYRITE OXYGEN METER
INSTRUMENTAL OTHER
 LABORATORY INFORMATION:
 SAMPLE RECOVERY: ATC LABORATORY CLEAN FIELD AREA
ATC VAN OTHER
 SAMPLE SHIPMENT: ATC VAN OTHER
 SAMPLE ANALYSIS: ATC OTHER
 FILTER MATERIAL: GELMAN A/E WHATMAN 934AH OTHER

ANALYTICAL TESTING CONSULTANTS, INC.
EQUAL AREA CALCULATIONS
ROUND DUCT-8 POINT TRAVERSE

Project No.: 8192

| | | | |
|---------|-----------------------|-----------|--------------------|
| Client: | <u>E-Stone /Grove</u> | Location: | <u>Sebring, FL</u> |
| Unit: | <u>BattHouse Out.</u> | Date: | <u>12/8/08</u> |



BLUE

| Stack I.D. = | | <u>32.5</u> |
|--------------|---------------|-------------------|
| Port Depth = | | <u>4</u> |
| Point No. | % of Diameter | Distance (Inches) |
| 1 | 3.2% | <u>5.04</u> |
| 2 | 10.5% | <u>7.41</u> |
| 3 | 19.4% | <u>10.31</u> |
| 4 | 32.3% | <u>14.50</u> |
| 5 | 67.7% | <u>26.00</u> |
| 6 | 80.6% | <u>30.20</u> |
| 7 | 89.5% | <u>33.09</u> |
| 8 | 96.8% | <u>35.46</u> |

If a port depth is entered, then the measurements include that port depth.

Please note if adjustments are required to the outermost points.

QA/QC Check:

| | | | | |
|--------------|-----------------------------|----------------------------------|----------------|---------------------------|
| Completeness | Legibility | Accuracy | Specifications | Reasonableness |
| <i>Bill</i> | <i>12/8/08</i> | | | <i>W. Keeler 12/15/08</i> |
| Signatures: | Technician (Signature/Date) | Project Manager (Signature/Date) | | |

Analytical Testing Consultants, Inc.

Kannapolis, NC (1-800-733-3193)

Traverse Data and Flow Computations

| | | | |
|-------------|-----------------------|----------------|------------------|
| Client | <u>E-Stone /Grove</u> | Date | <u>12/10/08</u> |
| Location | <u>RTO INLET</u> | Source | <u>RTO INLET</u> |
| Test Team | <u>BL /TD</u> | Run # | <u>Prelim.</u> |
| Project No. | <u>8742</u> | | |
| Pbar | <u>—</u> | Dry Bulb, °F | |
| Time | <u>12:10</u> | sp. "Hg or "Wg | <u>+0.50</u> |
| Pilot # | <u>57</u> | Fs for Pilot | <u>0.84</u> |

| Traverse Point | Vp, in. H ₂ O | Square Root,Vp | Stack Temp, °F | Cyclonic Flow Data | |
|----------------|--------------------------|----------------|----------------|--------------------|--------------|
| | | | | dP @ 0° | Angle @ 0 dP |
| A1 | 0.16 | | 44 | φ | 0 |
| A2 | 0.17 | | 44 | | |
| A3 | 0.12 | | 47 | | 2 |
| A4 | 0.08 | | 59 | | |
| A5 | 0.15 | | 60 | | 5 |
| A6 | 0.12 | | 66 | | |
| A7 | 0.14 | | 67 | | 0 |
| A8 | 0.10 | | 69 | | |
| A9 | — | | | | |
| A10 | — | | | | |
| A11 | — | | | | |
| A12 | — | | | | |
| B1 | 0.16 | | 48 | φ | 0 |
| B2 | 0.22 | | 47 | | |
| B3 | 0.20 | | 48 | | |
| B4 | 0.18 | | 48 | | 0 |
| B5 | 0.17 | | 50 | | |
| B6 | 0.17 | | 53 | | 0 |
| B7 | 0.12 | | 57 | | |
| B8 | 0.10 | | 65 | | |
| B9 | — | | | | |
| B10 | — | | | | |
| B11 | — | | | | |
| B12 | — | | | | |

Equations

Ts(Rankin) = Ts(avg) + 459.69 =

Duct Area (A = pi*r²) Ft² A=

Ps= Pbar + sp

Rho x (530/Ts) x (Ps/29.92) = (lbs/ft³)

K = 1006.5/(Gas Density)^{1/2} =

Velocity (ft/min)=K x Fs x (Vp avg)^{1/2}=

Volume (avg ACFM)= A x V =

SCFM(wet)=Volx(530/Ts)x(Ps/29.92)=

SCFM(Dry)=A x V x MD x 17.647 x (Ps/Ts)=

**Rho=0.075 lbs/ft³

Pm=Pbar+(avg.dH/13.6)=

Vm =

Vv std = (0.04708*SiO₂ in gms)+(0.04717*VLQ in ml)=

Vm std=Y*(Vm*528*Pm)/(Tm*29.92)=

V std = Vm std+Vv std =

%M=Vv std/V std * 100=

MD=(100-%M)/100 =

Pilot Tube Leak Checks

Pre-test Post-test

A ✓ A ✓

B ✓ B ✓

QA/QC Check:

Completeness

Legibility

Accuracy

Specifications

Reasonableness

Signatures:

Technician (Signature/Date)

Project Manager (Signature/Date)

Analytical Testing Consultants, Inc.

Kannapolis, NC (1-800-733-3193)

Traverse Data and Flow Computations

Client E-Stone / Grove
 Location Selma, NC
 Test Team BK, JD
 Project No. 8192
 Pbar 30.05
 Time 1125
 Pitot # 57

Date 12/9/08
 Source RD Inlet
 Run # 1

Dry Bulb, °F 86
 sp. "Hg or "Wg - 1.10
 Es for Pitot 0.84

Wet Bulb, °F 78
 Pilot Type STYRE
 Stack I.D. 18.55

| Traverse Point | Vp, in. H ₂ O | Square Root,Vp | Stack Temp, °F | Cyclonic Flow Data | |
|----------------|--------------------------|----------------|----------------|--------------------|--------------|
| | | | | dP @ 0o | Angle @ 0 dP |
| A1 | 0.29 | | 108 | | |
| A2 | 0.34 | | 107 | | |
| A3 | 0.38 | | 107 | | |
| A4 | 0.37 | | 107 | | |
| A5 | 0.33 | | 107 | | |
| A6 | 0.30 | | 105 | | |
| A7 | 0.31 | | 104 | | |
| A8 | 0.28 | | 100 | | |
| A9 | | | | | |
| A10 | | | | | |
| A11 | | | | | |
| A12 | | | | | |
| B1 | 0.26 | | 104 | | |
| B2 | 0.32 | | 105 | | |
| B3 | 0.31 | | 105 | | |
| B4 | 0.25 | | 106 | | |
| B5 | 0.28 | | 105 | | |
| B6 | 0.24 | | 101 | | |
| B7 | 0.23 | | 100 | | |
| B8 | 0.26 | | 100 | | |
| B9 | | | | | |
| B10 | | | | | |
| B11 | | | | | |
| B12 | | | | | |

Equations

Ts(Rankin) = Ts(avg) + 459.69 =

Pm=Pbar+(avg.dH/13.6)=
Vm =

Duct Area (A = pi*r²) Ft² A =

Vv std = (0.04708*SiO₂ in gms)*(0.04717*VLQ in ml)=
Vm std=Y*(Vm⁵²⁸*Pm)/(Tm^{29.92})=

Ps= Pbar + sp

V std = Vm std + Vv std =
%M = Vv std/V std * 100 =

Rho x (530/Ts) x (Ps/29.92) = (lbs/ft³)

MD=(100-%M)/100 =

K = 1096.5/(Gas Density^{1/2}) =

Pilot Tube Leak Checks

Velocity (ft/min)=K x Es x (Vp avg)^{1/2}=

Pre-test Post-test

Volume (avg ACFM) A x V =

SCFM(wet)=Volx(530/Ts)x(Ps/29.92)=

SCFM(Dry)=A x V x MD x 17,847 x (Ps/Ts)=

**Rho=0.075 lbs/ft³

QA/QC Check:

Completeness

Legibility

Accuracy

Specifications

Reasonableness

Signatures:

Technician (Signature/Date)

Project Manager (Signature/Date)

Analytical Testing Consultants, Inc.

Kannapolis, NC (1-800-733-3193)

Traverse Data and Flow Computations

| | | | |
|-------------|-----------------------|----------------|------------------|
| Client | <u>E-Stone /Grove</u> | Date | <u>12.9.08</u> |
| Location | <u>BSP INC., NC</u> | Source | <u>RTO INLET</u> |
| Test Team | <u>BL</u> | Run # | <u>2</u> |
| Project No. | <u>8192</u> | | |
| Pbar | <u>30.05</u> | Dry Bulb, °F | <u>93</u> |
| Time | <u>1310</u> | sp, "Hg or "Wg | <u>-0.2</u> |
| Pilot # | <u>57</u> | Fs for Pitot | <u>0.84</u> |

| Traverse Point | Vp, in. H ₂ O | Square Root,Vp | Stack Temp, °F | Cyclonic Flow Data | |
|----------------|--------------------------|----------------|----------------|--------------------|--------------|
| | | | | dP @ 0o | Angle @ 0 dP |
| A1 | 0.34 | | 111 | | |
| A2 | 0.35 | | 112 | | |
| A3 | 0.34 | | 111 | | |
| A4 | 0.33 | | 113 | | |
| A5 | 0.30 | | 113 | | |
| A6 | 0.29 | | 113 | | |
| A7 | 0.34 | | 108 | | |
| A8 | 0.32 | | 108 | | |
| A9 | | | | | |
| A10 | | | | | |
| A11 | | | | | |
| A12 | | | | | |
| B1 | 0.29 | | 111 | | |
| B2 | 0.40 | | 112 | | |
| B3 | 0.38 | | 112 | | |
| B4 | 0.34 | | 112 | | |
| B5 | 0.35 | | 112 | | |
| B6 | 0.29 | | 112 | | |
| B7 | 0.25 | | 112 | | |
| B8 | 0.25 | | 112 | | |
| B9 | | | | | |
| B10 | | | | | |
| B11 | | | | | |
| B12 | | | | | |

Equations

Ts(Rankin) = Ts(avg) + 459.69 =

Duct Area (A = pi*r^2) R^2 A =

Ps = Pbar + sp

Rho x (530/Ts) x (Ps/29.92) = (lbs/ft^3)

K = 1096.5/(Gas Density^1/2) =

Velocity (ft/min)=K x Fs x (Vp avg)^1/2=

Volume (avg ACFM)= A x V =

SCFM(wet)=Volx(530/Ts)x(Ps/29.92)=

SCFM(Dry)=A x V x MD x 17.647 x (Ps/Ts)=

**Rho=0.075 lbs/ft^3

Pm=Pbar+(avg.dH/13.6)=

Vm =

Vv std = (0.04708*SiO₂ in gms)/(0.04717*VLQ in ml)=

Vm std=Y*(Vm^528*Pm)/(Tm^29.92)=

V std = Vm std + Vv std =

%M=V std/V std * 100=

MD=(100-%M)/100 =

Pitot Tube Leak Checks

Pre-test Post-test

| | | | |
|---|---|---|---|
| A | ✓ | A | ✓ |
| B | ✓ | B | ✓ |

QA/QC Check:

Completeness

✓

Legibility

✓

Accuracy

✓

Specifications

✓

Reasonableness

✓

Signatures:

Technician (Signature/Date)

Project Manager (Signature/Date)

Analytical Testing Consultants, Inc.

Kannapolis, NC (1-800-733-3193)

Traverse Data and Flow Computations

| | | | |
|-------------|-----------------------|----------------|------------------|
| Client | <u>E-Stone /Grove</u> | Date | <u>12-9-08</u> |
| Location | <u>Gebring, Pa</u> | Source | <u>RTO INLET</u> |
| Test Team | <u>BKR ID</u> | Run # | <u>3</u> |
| Project No. | <u>8772</u> | | |
| Pbar | <u>30.05</u> | Dry Bulb, °F | <u>77</u> |
| Time | <u>1512</u> | sp. "Hg or "Wg | <u>-1.10</u> |
| Pilot # | <u>57</u> | Fs for Pilot | <u>0.84</u> |

| Traverse Point | Vp, in. H ₂ O | Square Root,Vp | Stack Temp, °F | Cyclonic Flow Data | |
|----------------|--------------------------|----------------|----------------|--------------------|--------------|
| | | | | dP @ 0o | Angle @ 0 dP |
| A1 | 0.34 | | 113 | | |
| A2 | 0.35 | | 113 | | |
| A3 | 0.33 | | 113 | | |
| A4 | 0.32 | | 113 | | |
| A5 | 0.30 | | 113 | | |
| A6 | 0.28 | | 113 | | |
| A7 | 0.27 | | 113 | | |
| A8 | 0.26 | | 113 | | |
| A9 | | | | | |
| A10 | | | | | |
| A11 | | | | | |
| A12 | | | | | |
| B1 | 0.31 | | 111 | | |
| B2 | 0.34 | | 111 | | |
| B3 | 0.33 | | 112 | | |
| B4 | 0.33 | | 112 | | |
| B5 | 0.27 | | 113 | | |
| B6 | 0.24 | | 112 | | |
| B7 | 0.24 | | 113 | | |
| B8 | 0.24 | | 110 | | |
| B9 | | | | | |
| B10 | | | | | |
| B11 | | | | | |
| B12 | | | | | |

Equations

Ts(Rankin) = Is(avg) + 459.69 =

Duct Area (A = πl^2) ft² A =

Ps = Pbar + sp

Rho x (530/Ts) x (Ps/29.92) = (lbs/ft³)

K = 1096.5/(Gas Density)^{1/2} =

Velocity (ft/min)=K x Fs x (Vp avg)^{1/2}=

Volume (avg ACFM)= A x V =

SCFM(wet)=Volx(530/Ts)x(Ps/29.92)=

SCFM(Dry)=A x V x MD x 17.647 x (Ps/Ts)=

**Rho=0.075 lbs/ft³

Pm=Pbar+(avg.dH/13.6)=

Vm =

Vv std = (0.04708*SiO₂ in gms)+(0.04717*VLQ in ml)=

Vm std=Y*(Vm*528*Pm)/(Tm*29.92)=

V std = Vm std + Vv std =

%M=Vv std/V std * 100=

MD=(100-%M)/100 =

Pitot Tube Leak Checks

Pre-test Post-test

| | | | |
|---|---|---|---|
| A | ✓ | A | ✓ |
| B | ✓ | B | ✓ |

QA/QC Check:

Completeness

Legibility

Accuracy

Specifications

Reasonableness

Signatures:

Technician (Signature/Date)

Project Manager (Signature/Date)

SOURCE SURVEY AND DESCRIPTIONCLIENT: E-Stone /Grove Project No. 8192PERSONNEL COMPLETING SURVEY: BR DATE: 12/8/08SYSTEM TYPE: BOILER PROCESS OTHER RTO
NARRATIVE DESCRIPTION:RTO INLETPURPOSE OF TESTING: COMPLIANCE EVALUATION PROCESS RATE OR CAPACITY: 135483/HR ± 10% DETERMINED BY: FACILITY
CONTROL EQUIPMENT: MULTI-CLONE SCRUBBER BAGHOUSEELECTROSTATIC PRECIPITATOR OTHER PRO

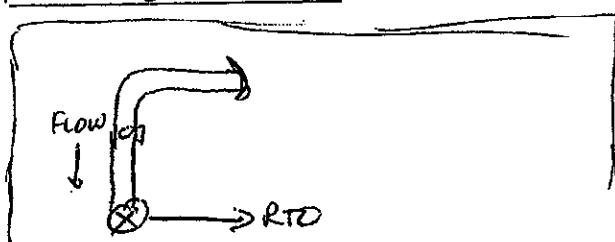
CONTROL EQUIPMENT OPERATING PARAMETERS:

PRESSURE DROP OTHER Temperature

SAMPLING LOCATION DATA:

DISTANCE DOWNSTREAM FROM FLOW DISTURBANCE: NATURE OF DISTURBANCE: BEND FAN, EXPANSION, BYPASS, DUCT,
OTHER 77.5 109.5DISTANCE UPSTREAM FROM FLOW DISTURBANCE: 7 77.5NATURE OF DISTURBANCE: STACK EXHAUST, FAN, EXPANSION, DUCT,
OTHER DAMPERINDIVIDUAL STACK COMMON STACK STACK DIAMETER OR DIMENSIONS: 18.5NUMBER OF PORTS: 2 POINTS PER PORT: 8

SKETCH:

ESTIMATED TEMPERATURE: Boiler ± 10° ESTIMATED MOISTURE: 2-3%GAS COMPOSITION BY: FYRITE OXYGEN METER
INSTRUMENTAL OTHER

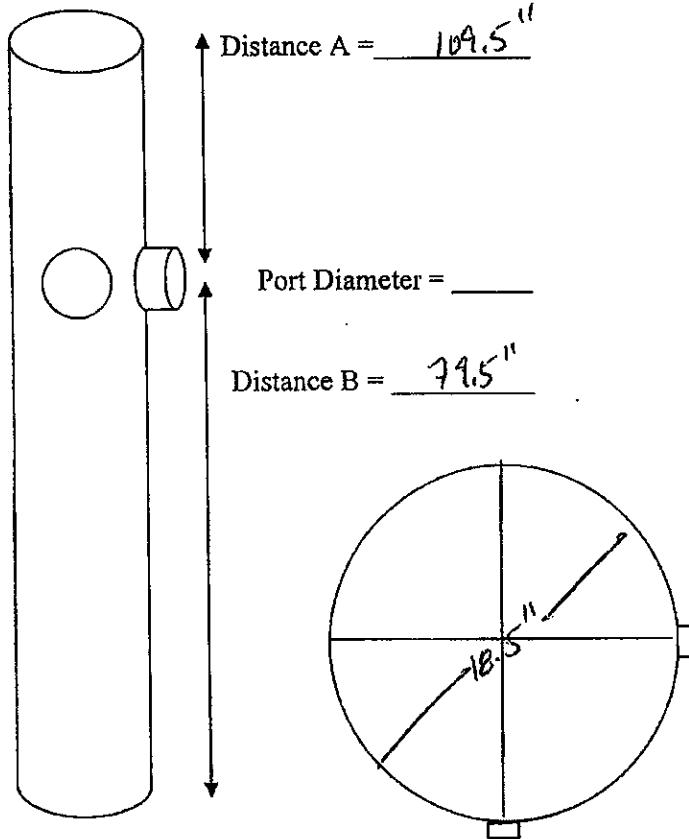
LABORATORY INFORMATION:

SAMPLE RECOVERY: ATC LABORATORY CLEAN FIELD AREA
ATC VAN OTHER N/ASAMPLE SHIPMENT: ATC VAN OTHER 1SAMPLE ANALYSIS: ATC OTHER FILTER MATERIAL: GELMAN A/E WHATMAN 934AH OTHER

ANALYTICAL TESTING CONSULTANTS, INC.
EQUAL AREA CALCULATIONS
ROUND DUCT-8 POINT TRAVERSE

Project No.: 8792

| | | | |
|---------|-----------------------|-----------|--------------------|
| Client: | <u>E-Stone /Grove</u> | Location: | <u>Sabring, FL</u> |
| Unit: | <u>RTO Inlet</u> | Date: | <u>12/8/08</u> |

**ReD**

| Stack I.D. = | | <u>18.5</u> |
|--------------|---------------|-------------------|
| Port Depth = | | <u>0"</u> |
| Point No. | % of Diameter | Distance (Inches) |
| 1 | 3.2% | <u>0.59</u> |
| 2 | 10.5% | <u>1.94</u> |
| 3 | 19.4% | <u>3.59</u> |
| 4 | 32.3% | <u>5.98</u> |
| 5 | 67.7% | <u>12.52</u> |
| 6 | 80.6% | <u>14.91</u> |
| 7 | 89.5% | <u>16.56</u> |
| 8 | 96.8% | <u>17.91</u> |

If a port depth is entered, then the measurements include that port depth.
Please note if adjustments are required to the outermost points.

QA/QC Check:

| Completeness | Legibility | Accuracy | Specifications | Reasonableness |
|--------------|------------|----------|----------------|----------------|
| ✓ | ✓ | ✓ | ✓ | ✓ |

Signatures:

Bill F. 12/8/08 W. Bill Fosh 12/15/08
 Technician (Signature/Date) Project Manager (Signature/Date)

Analytical Testing Consultants, Inc.

Kannapolis, NC (1-800-733-3193)

Traverse Data and Flow Computations

Client E-Stone / Grove Date 12/8/08
 Location Syrinx, FL Source RTD OUTLET
 Test Team BLC 3D Run # PIPELINE
 Project No. 8192

| Pbar | Dry Bulb, °F | Wet Bulb, °F |
|-------|----------------|--------------|
| 12.13 | sp, "Hg or "Wg | -0.12 |
| 57 | Fs for Pitot | 0.84 |

| Traverse Point | Vp, in. H ₂ O | Square Root,Vp | Stack Temp, °F | Cyclonic Flow Data | |
|----------------|--------------------------|----------------|----------------|--------------------|--------------|
| | | | | dP @ 0° | Angle @ 0 dP |
| A1 | 0.30 | | 238 | | |
| A2 | 0.36 | | 251 | | 0 |
| A3 | 0.36 | | 262 | | |
| A4 | 0.35 | | 240 | | 0 |
| A5 | 0.24 | | 236 | | |
| A6 | 0.30 | | 250 | | |
| A7 | 0.27 | | 246 | | 0 |
| A8 | 0.26 | | 237 | | |
| A9 | | | | | |
| A10 | | | | | |
| A11 | | | | | |
| A12 | | | | | |
| B1 | 0.32 | | 266 | 0 | |
| B2 | 0.30 | | 236 | | 5 |
| B3 | 0.31 | | 230 | | |
| B4 | 0.31 | | 216 | | 5 |
| B5 | 0.30 | | 214 | | |
| B6 | 0.28 | | 214 | | 0 |
| B7 | 0.25 | | 212 | | |
| B8 | 0.20 | | 212 | | 0 |
| B9 | | | | | |
| B10 | | | | | |
| B11 | | | | | |
| B12 | | | | | |

Verify
not cyclonic
Previously
tested
Source -

Equations

Ts(Rankin) = Ts(avg) + 459.69 =

Duct Area (A = πl^2) Ft² A =

Ps = Pbar + sp

Rho x (530/Ts) x (Ps/29.92) = (lbs/ft³)

K = 1096.5/(Gas Density)^{1/2} =

Velocity (ft/min)=K x Fs x (Vp avg)^{1/2}=

Volume (avg ACFM)= A x V =

SCFM(wet)=Volx(530/Ts)x(Ps/29.92)=

SCFM(Dry)=A x V x MD x 17.647 x (Ps/Ts)=

**Rho=0.075 lbs/ft³

Pm=Pbar*(avg.dH/13.6)=

Vm =

Vv std = (0.04708*SiO₂ in gms)*(0.04717*VLQ in ml)=

Vm std=Y*(Vm*528*Pm)/(Tm*29.92)=

V std= Vm std+Vv std =

%M=Vv std/V std * 100=

MD=(100-%M)/100=

Pitot Tube Leak Checks

Pre-test Post-test

| | | | |
|---|---|---|---|
| A | ✓ | A | ✓ |
| B | ✓ | B | ✓ |

QA/QC Check:

✓

Completeness

✓

Legibility

✓

Accuracy

✓

Specifications

✓

Reasonableness

Signatures:

Technician (Signature/Date)

Project Manager (Signature/Date)

Analytical Testing Consultants, Inc.

Kannapolis, NC (1-800-733-3193)

Traverse Data and Flow Computations

| | | | |
|-------------|----------------------|----------------|----------------|
| Client | <u>E-STONE/GROVE</u> | Date | <u>12/9/08</u> |
| Location | <u>Sebring, FL</u> | Source | <u>RTO OUT</u> |
| Test Team | <u>BK TM</u> | Run # | <u>1</u> |
| Project No. | <u>8192</u> | | |
| Pbar | <u>30.05</u> | Dry Bulb, °F | <u>—</u> |
| Time | <u>115</u> | sp. "Hg or "Wg | <u>-0.26</u> |
| Pitot # | <u>57</u> | Fs for Pitot | <u>0.94</u> |

| Traverse Point | Vp, in. H ₂ O | Square Root,Vp | Stack Temp, °F | Cyclonic Flow Data | |
|----------------|--------------------------|----------------|----------------|--------------------|--------------|
| | | | | dP @ 0o | Angle @ 0 dP |
| A1 | 0.10 | | 277 | | |
| A2 | 0.38 | | 218 | | |
| A3 | 0.52 | | 222 | | |
| A4 | 0.54 | | 226 | | |
| A5 | 0.46 | | 229 | | |
| A6 | 0.41 | | 238 | | |
| A7 | 0.35 | | 240 | | |
| A8 | 0.12 | | 236 | | |
| A9 | | | | | |
| A10 | | | | | |
| A11 | | | | | |
| A12 | | | | | |
| B1 | 0.47 | | 236 | | |
| B2 | 0.50 | | 239 | | |
| B3 | 0.50 | | 250 | | |
| B4 | 0.51 | | 259 | | |
| B5 | 0.47 | | 263 | | |
| B6 | 0.39 | | 271 | | |
| B7 | 0.33 | | 250 | | |
| B8 | 0.29 | | 229 | | |
| B9 | | | | | |
| B10 | | | | | |
| B11 | | | | | |
| B12 | | | | | |

Equations

Ts(Rankin) = ts(avg) + 459.69 =

Duct Area (A = $\pi r^2 Fc^2$) A =

Ps = Pbar + sp

Rho x (530/Ts) x (Ps/29.92) = (lbs/ft³)

K = 1098.5/(Gas Density^{1/2}) =

Velocity (ft/min)=K x Fs x (Vp avg)^{1/2}=

Volume (avg ACFM)= A x V =

SCFM(wet)=Volx(630/Ts)x(Ps/29.92)=

SCFM(Dry)=A x V x MD x 17.647 x (Ps/Ts)=

**Rho=0.075 lbs/ft³

Pm=Pbar+(avg.dH/13.6)=

Vm =

Vv std = (0.04708*SiO₂ in gms)+(0.04717*VLQ in ml)=

Vm std=Y*(Vm*528*Pm)/(Tr*29.92)=

V std=Vm std+Vv std =

%M=Vv std/V std * 100=

MD=(100-%M)/100 =

Pitot Tube Leak Checks

Pre-test Post-test

A A

B B

QA/QC Check:

Completeness

Logibility

Accuracy

Specifications

Reasonableness

Signatures:

Technician (Signature/Date)

Project Manager (Signature/Date)

Analytical Testing Consultants, Inc.

Kannapolis, NC (1-800-733-3193)

Traverse Data and Flow Computations

| | | | |
|-------------|------------------------|----------------|----------------|
| Client | <u>E-Stone / Grove</u> | Date | <u>12.9.08</u> |
| Location | <u>Sebring, FL</u> | Source | <u>RTO OUT</u> |
| Test Team | <u>BL TDO</u> | Run # | <u>2</u> |
| Project No. | <u>S992</u> | | |
| Pbar | <u>30.05</u> | Dry Bulb, °F | <u>—</u> |
| Time | <u>1305</u> | sp, "Hg or "Wg | <u>-0.22</u> |
| Pilot # | <u>S7</u> | Fs for Pilot | <u>0.84</u> |
| | | Wet Bulb, °F | <u>—</u> |
| | | Pilot Type | <u>S TYPE</u> |
| | | Stack I.D. | <u>22.5</u> |

| Traverse Point | Vp, in. H ₂ O | Square Root,Vp | Stack Temp, °F | Cyclonic Flow Data | |
|----------------|--------------------------|----------------|----------------|--------------------|--------------|
| | | | | dP @ 0o | Angle @ 0 dP |
| A1 | 0.54 | | 241 | | |
| A2 | 0.53 | | 225 | | |
| A3 | 0.51 | | 220 | | |
| A4 | 0.49 | | 220 | | |
| A5 | 0.46 | | 221 | | |
| A6 | 0.37 | | 227 | | |
| A7 | 0.35 | | 226 | | |
| A8 | 0.32 | | 220 | | |
| A9 | | | | | |
| A10 | | | | | |
| A11 | | | | | |
| A12 | | | | | |
| B1 | 0.42 | | 227 | | |
| B2 | 0.44 | | 212 | | |
| B3 | 0.45 | | 209 | | |
| B4 | 0.44 | | 209 | | |
| B5 | 0.40 | | 210 | | |
| B6 | 0.35 | | 211 | | |
| B7 | 0.37 | | 212 | | |
| B8 | 0.29 | | 200 | | |
| B9 | | | | | |
| B10 | | | | | |
| B11 | | | | | |
| B12 | | | | | |

Equations

Ts(Rank(n) = Ts(avg) + 459.69 =

Duct Area (A = pi*r^2) Ft^2 A=

Ps = Pbar + sp

Rho x (530/Ts) x (Ps/29.92) = (lbs/ft^3)

K = 1096.5/(Gas Density^{1/2}) =

Velocity (ft/min)=K x Fe x (Vp avg)^{1/2}=

Volume (avg ACFM)= A x V =

SCFM(wet)=Volx(530/Ts)x(Ps/29.92)=

SCFM(Dry)=A x V x MD x 17.647 x (Ps/Ts)=

**Rho=0.075 lbs/ft³

Pm=Pbar+(avg.dH/13.6)=

Vm =

Vv std = (0.04708*SiO₂ in gms)+(0.04717*VLQ in ml)=

Vm std=Y*(Vm*528*Pm)/(Tm*29.92)=

V std = Vm std +Vv std =

%M=Vv std/V std * 100=

MD=(100-%M)/100 =

Pilot Tube Leak Checks

Pre-test Post-test

| | | | |
|---|---|---|---|
| A | ✓ | A | ✓ |
| B | ✓ | B | ✓ |

QA/QC Check:

Completeness

Legibility

Accuracy

Specifications

Reasonableness

Signatures:

Technician (Signature/Date)

Project Manager (Signature/Date)

Analytical Testing Consultants, Inc.

Kannapolis, NC (1-800-733-3193)

Traverse Data and Flow Computations

| | | | |
|-------------|------------------------|----------------|----------------|
| Client | <u>E-Stone / Grove</u> | Date | <u>12.9.08</u> |
| Location | <u>Burns, NC</u> | Source | <u>RIO out</u> |
| Test Team | <u>PK TD</u> | Run # | <u>3</u> |
| Project No. | <u>8192</u> | | |
| Pbar | <u>30.05</u> | Dry Bulb, °F | <u>—</u> |
| Time | <u>1520</u> | sp. "Hg or "Wg | <u>-0.22</u> |
| Pitot # | <u>51</u> | Fs for Pitot | <u>0.84</u> |

| Traverse Point | Vp, in. H ₂ O | Square Root,Vp | Stack Temp, °F | Cyclonic Flow Data | |
|----------------|--------------------------|----------------|----------------|--------------------|--------------|
| | | | | dP @ 0o | Angle @ 0 dP |
| A1 | 0.62 | | 260 | | |
| A2 | 0.53 | | 227 | | |
| A3 | 0.52 | | 218 | | |
| A4 | 0.50 | | 215 | | |
| A5 | 0.48 | | 215 | | |
| A6 | 0.40 | | 215 | | |
| A7 | 0.33 | | 215 | | |
| A8 | 0.29 | | 211 | | |
| A9 | | | | | |
| A10 | | | | | |
| A11 | | | | | |
| A12 | | | | | |
| B1 | 0.35 | | 235 | | |
| B2 | 0.41 | | 225 | | |
| B3 | 0.44 | | 226 | | |
| B4 | 0.45 | | 225 | | |
| B5 | 0.45 | | 221 | | |
| B6 | 0.44 | | 223 | | |
| B7 | 0.44 | | 227 | | |
| B8 | 0.43 | | 233 | | |
| B9 | | | | | |
| B10 | | | | | |
| B11 | | | | | |
| B12 | | | | | |

Equations

Ts(Rankin) = Ts(avg) + 459.69 =

Duct Area (A = pi*r²) Ft² A =

Ps = Pbar + sp

Rho x (530/Ts) x (Ps/29.92) = (lbs/ft³)

K = 1096.5/(Gas Density^{1/2}) =

Velocity (ft/min)=K x Ps x (Vp avg)^{1/2}=

Volume (avg ACFM)= A x V =

SCFM(wet)=Volx(530/Ts)x(Ps/29.92)=

SCFM(Dry)=A x V x MD x 17.647 x (Ps/Ts)=

**Rho=0.075 lbs/ft³

Pm=Pbar+(avg.dH/13.6)=

Vm =

Vv std = (0.04708*SiO₂ in gms)+(0.04717*VLQ in ml)=

Vm std=Y*(Vm⁵²⁸*Pm)/(Tm^{29.92})=

V std= Vm std+Vv std =

%M=Vv std/V std * 100=

MD=(100-%M)/100 =

Pitot Tube Leak Checks

Pre-test Post-test

| | | | |
|---|---|---|---|
| A | ✓ | A | ✓ |
| B | ✓ | B | ✓ |

QA/QC Check:

Completeness

Legibility

Accuracy

Specifications

Reasonableness

Signatures:

Technician (Signature/Date)

Project Manager (Signature/Date)



ISOKINETIC SAMPLING DATA SHEET

CLIENT E-Stone/Grove DATE 12/9/08 Module No. ATC 1
 LOCATION Sebring, FL SOURCE RTO Outlet Filter No. /
 TEST TEAM BL SD RUN # 1 Methods 1-4 Pitot No. /

| | | | | | |
|-----------------------|------------------|---------------------|--------------------------|--|--|
| MODULE LEAK RATE | | SAMPLING RATE SETUP | | Comments (list other personnel on site): | |
| start <u>200</u> | @ <u>14</u> "Hg | ▲H@ <u>1.806</u> | NOZZLE <u>(#)</u> | | |
| end <u>0.000</u> | @ <u>10</u> "Hg | T _m | % H ₂ O | | |
| pitot leak check: | | T _s | Cal. Factor <u>0.962</u> | | |
| start | end | Md | Pm | | |
| A <u>"</u> A <u>"</u> | H ₂ O | K | Y _c | | |
| B <u>"</u> B <u>"</u> | H ₂ O | | | | |

ATC Project No. 8792
 Start 1015 Finish 1115

| Time | Point | Line Vacuum | T _m °F | T _s °F | T _p °F | T _f °F | T _i °F | △P _s (in.) H ₂ O | △H (in.) H ₂ O | V _s Ft ³ | REMARKS |
|------|-------|-------------|----------------------|----------------------|----------------------|----------------------|----------------------|---|------------------------------|-----------------------------------|--------------|
| 0 | 1 | 2.0 | 59 | 1 | 1 | 1 | 46 | 1 | 2.0 | 401.368 | 78/86 RTO IN |
| 5 | | 2.0 | 61 | | | | 45 | | 1 | 405.100 | 76/88 BH |
| 10 | | 2.0 | 63 | | | | 49 | | 1 | 409.600 | |
| 15 | | 2.0 | 63 | | | | 50 | | 1 | 413.200 | |
| 20 | | 2.0 | 64 | | | | 57 | | 1 | 417.200 | |
| 25 | | 2.0 | 66 | | | | 59 | | 1 | 421.200 | |
| 30 | | 2.0 | 68 | | | | 59 | | 1 | 425.700 | |
| 35 | | 2.0 | 68 | | | | 58 | | 1 | 429.100 | |
| 40 | | 2.0 | 70 | | | | 59 | | 1 | 433.000 | |
| 45 | | 2.0 | 70 | | | | 59 | | 1 | 437.500 | |
| 50 | | 2.0 | 72 | | | | 60 | | 1 | 441.400 | |
| 55 | | 2.0 | 73 | | | | 60 | | 1 | 445.500 | |
| 60 | | | | | | | | | 1 | 449.605 | |

T_m=meter temperature T_s=stack temperature T_p=probe temperature T_f=filter temperature, V_s(ft³)=gas sample volume

T_i=exhaust temperature of last impinger, △P_s=velocity head differential pressure △H=pressure differential across the orifice meter

QA/QC Check: Complete Legibility Accuracy Specifications Reasonableness
 Checked by: W.L. Date 12/15/08

Module Operator (Signature/Date)

Data Review (Signature/Date)

ATC 9 1-800-733-3193

ATC Form 16-revision 5.1 (7/13/07)
 F:\Work\All Forms-Field Data Sheets.Calc Formulas.Nomenclature.etc\Field\16-Isokinetic Sampling Data Sheet.dot



ISOKINETIC SAMPLING DATA SHEET

CLIENT E-Stone/Grove DATE 12/9/08 Module No. ATC 1
 LOCATION Sebring, FL SOURCE RDO OUTLET Filter No. 1
 TEST TEAM BK JD RUN # 2 Methods 1-4 Pitot No. 1

| | | | | | |
|---------------------|---------------------|---------------------|--------------------|--|--------------------|
| MODULE LEAK RATE | | SAMPLING RATE SETUP | | Comments (list other personnel on site): | |
| start | end | $\Delta H @$ | NOZZLE | | |
| <u>1000@ 16 "Hg</u> | <u>0.00@ 10 "Hg</u> | <u>1.806</u> | <u>(#)</u> | | |
| Pitot Leak Check | | T _m | % H ₂ O | | |
| start | end | <u>/</u> | <u>/</u> | | |
| A | A | T _s | Cal. Factor | | |
| " | "H ₂ O | <u>/</u> | <u>0.962</u> | | |
| B | B | Md | Pm | ATC Project No. <u>8192</u> | |
| " | "H ₂ O | K | Y _c | Start <u>1155</u> | Finish <u>1255</u> |

| Time | Point | Line vacuum | T _m °F | T _s °F | T _p °F | T _f °F | T _c °F | ΔP _s (in.)H ₂ O | ΔH (in.)H ₂ O | V _m Ft ³ | REMARKS |
|------|-------|----------------|----------------------|----------------------|----------------------|----------------------|----------------------|--|-----------------------------|-----------------------------------|---------|
| 0 | | 2.0 | 75 | | | | 53 | | 2.0 | 450.142 | |
| 5 | | 2.0 | 75 | | | | 53 | | | 454.000 | |
| 10 | | 2.0 | 76 | | | | 55 | | | 458.500 | |
| 15 | | 2.0 | 76 | | | | 55 | | | 462.500 | |
| 20 | | 2.0 | 77 | | | | 58 | | | 467.100 | |
| 25 | | 2.0 | 78 | | | | 62 | | | 471.200 | |
| 30 | | 2.0 | 78 | | | | 64 | | | 475.400 | |
| 35 | | 2.0 | 79 | | | | 59 | | | 479.200 | |
| 40 | | 2.0 | 80 | | | | 60 | | | 483.500 | |
| 45 | | 2.0 | 80 | | | | 60 | | | 487.800 | |
| 50 | | 2.0 | 81 | | | | 60 | | | 491.200 | |
| 55 | | 2.0 | 82 | | | | 60 | | | 496.400 | |
| 60 | | | | | | | | | | 499.642 | |

T_m=meter temperature T_s=stack temperature T_p=probe temperature T_f=filter temperature, V_m (ft³)=gas sample volume

T_c=exhaust temperature of last impinger, ΔP_s=velocity head differential pressure ΔH=pressure differential across the orifice meter

QA/QC Check: Completeness ✓ Legibility ✓ Accuracy ✓ Specifications ✓ Reasonableness ✓
 Checked by: W.L.Woolf Date Review (Signature/Date) 12/15/08

Module Operator (Signature/date)

Date Review (Signature/Date)

ATC # 1-800-733-3193



ISOKINETIC SAMPLING DATA SHEET

CLIENT E-Stone/Grove DATE 12.9.08 Module No. ATC 1
 LOCATION Sebring, FL SOURCE RIO OUT Filter No. /
 TEST TEAM BK ID RUN # 3 Methods 1-4 Pitot No. /

| | | | | | |
|-------------------|-------------------|---------------------|--------------------|--|--------------|
| MODULE LEAK RATE | | SAMPLING RATE SETUP | | Comments (list other personnel on site): | |
| start 0.0 | 16 "Hg | $\Delta H @ 1.806$ | Nozzle (#) | | |
| end 0.0 @ 5 "Hg | | Tm | % H ₂ O | | |
| Pitot Leak Check: | | Ts | Cal. Factor 0.962 | | |
| start A | end A | Md | Pm | ATC Project No. 8192 | |
| A | "H ₂ O | K | Y _c | Start 14/05 | Finish 15/05 |
| B | "H ₂ O | | | | |

| Time | Point | Line Vacuum | T _m °F | T _s °F | T _p °F | T _f °F | T _i °F | ΔP _s (in.) H ₂ O | ΔH (in.) H ₂ O | V _m ft ³ | REMARKS |
|------|-------|-------------|-------------------|-------------------|-------------------|-------------------|-------------------|--|---------------------------|--------------------------------|---------|
| 0 | 2 | 82 | | | | | 50 | | 2.0 | 499.781 | |
| 5 | 2 | 81 | | | | | 43 | | | 503.1 | |
| 10 | 2 | 81 | | | | | 43 | | | 506.7 | |
| 15 | 2 | 82 | | | | | 48 | | | 510.8 | |
| 20 | 2 | 83 | | | | | 54 | | | 515.7 | |
| 25 | 2 | 83 | | | | | 56 | | | 519.7 | |
| 30 | 2 | 84 | | | | | 58 | | | 523.9 | |
| 35 | 2 | 84 | | | | | 59 | | | 528.1 | |
| 40 | 2 | 85 | | | | | 61 | | | 533.1 | |
| 45 | 2 | 85 | | | | | 61 | | | 536.5 | |
| 50 | 2 | 85 | | | | | 62 | | | 34541.3 | |
| 55 | 2 | 86 | | | | | 62 | | | 545.3 | |
| 60 | 2 | 86 | | | | | 62 | | | 549.460 | |

T_m=meter temperature T_s=stack temperature T_p=probe temperature T_f=filter temperature, V_m(ft³)=gas sample volume

T_i=exhaust temperature of last impinger ΔP_s=Velocity head differential pressure ΔH=pressure differential across the orifice meter

QA/QC Check: Completeness Legibility Accuracy Specifications Reasonableness
 Checked by: BK Date: 12/15/08
 Module Operator (Signature/Date)

ATC 8 1-800-733-3193

E-Stone USA Inc., Gypsum Testing and Consulting Project No. P-6192

ANALYTICAL TESTING CONSULTANTS, INC.

KANNAPOLIS, N.C.

Project No. 8192

IMPIINGER DATA SHEET

CLIENT E-Stone / Grove

LOCATION SEBRING, FL

UNIT RD Outer

| RUN# | | DATE <u>12/9</u> | IMPIINGER CONTENTS | | | | TOTAL (VLQ) | CONDENSATE | REMARKS |
|------|-------|---------------------|-------------------------------|-------------------------------|---------------|------------------|----------------|------------|---------|
| | | | DH ₂ O <u>1</u> | DH ₂ O <u>2</u> | P <u>3</u> | S.G. <u>4</u> | | | |
| 1 | START | | 100 | 100 | Ø | 300 | | | M 1-4 |
| | END | | 110 | 102 | Ø | 305.0 | | | |
| | dV | | 10 | 2 | Ø | 5.0 | 17.0 | ML | |
| 2 | START | | 100 | 100 | Ø | 300 | | | |
| | END | | 104 | 100 | Ø | 310 | | | |
| | dV | | 4 | Ø | Ø | 10.0 | 14.0 | ML | |
| 3 | START | | 100 | 100 | 0 | 305.0 | | | |
| | END | | 110 | 105 | 0 | 315 | | | |
| | dV | | 10 | 5 | 0 | 10.5 | 3.5 | ML | |
| | START | | | | | | | | |
| | END | | | | | | | | |
| | dV | | | | | | | ML | |
| | START | | | | | | | | |
| | END | | | | | | | | |
| | dV | | | | | | | ML | |
| | START | | | | | | | | |
| | END | | | | | | | | |
| | dV | | | | | | | ML | |

Data by Bill

Approved by WCR

Date 12/9/08

Date 12/15/08

SOURCE SURVEY AND DESCRIPTIONCLIENT: E-Stone /Grove Project No. 8792PERSONNEL COMPLETING SURVEY: BK DATE: 12/8/08SYSTEM TYPE: BOILER PROCESS OTHER RTO
NARRATIVE DESCRIPTION:*RTO OUTLET*PURPOSE OF TESTING: COMPLIANCE EVALUATION PROCESS RATE OR CAPACITY: 13 Shms/hr ± 10% DETERMINED BY: CONTROL EQUIPMENT: MULTI-CLONE SCRUBBER BAGHOUSE ELECTROSTATIC PRECIPITATOR OTHER RTO

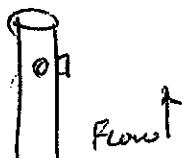
CONTROL EQUIPMENT OPERATING PARAMETERS:

PRESSURE DROP OTHER Temperature

SAMPLING LOCATION DATA:

DISTANCE DOWNSTREAM FROM FLOW DISTURBANCE: 125" NATURE OF DISTURBANCE: BEND, FAN, EXPANSION, BYPASS, DUCT,
OTHER DISTANCE UPSTREAM FROM FLOW DISTURBANCE: 106.5" NATURE OF DISTURBANCE: STACK EXHAUST, FAN, EXPANSION, DUCT,
OTHER INDIVIDUAL STACK COMMON STACK STACK DIAMETER OR DIMENSIONS: 22.5 NUMBER OF PORTS: 2 POINTS PER PORT: 8

SKETCH:

ESTIMATED TEMPERATURE: 250° F ESTIMATED MOISTURE: 10% GAS COMPOSITION BY: FYRITE OXYGEN METER INSTRUMENTAL OTHER

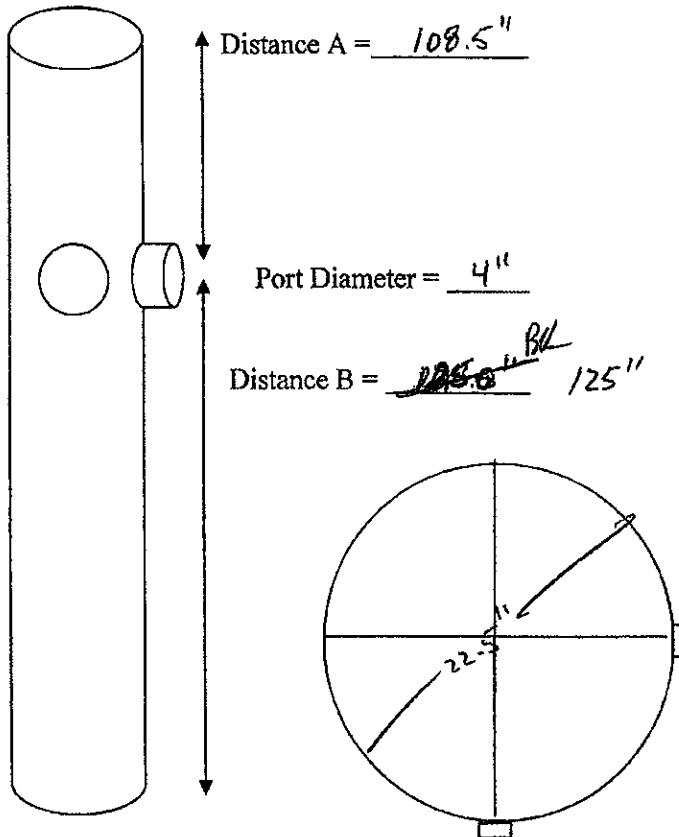
LABORATORY INFORMATION:

SAMPLE RECOVERY: ATC LABORATORY CLEAN FIELD AREA N/A
ATC VAN OTHER SAMPLE SHIPMENT: ATC VAN OTHER SAMPLE ANALYSIS: ATC OTHER FILTER MATERIAL: GELMAN A/E WHATMAN 934AH OTHER

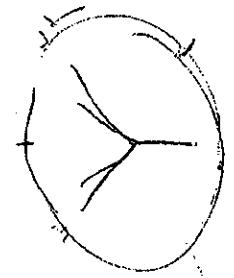
ANALYTICAL TESTING CONSULTANTS, INC.
EQUAL AREA CALCULATIONS
ROUND DUCT-8 POINT TRAVERSE

Project No.: 8192

| | | | |
|---------|------------------------|-----------|--------------------|
| Client: | <u>E-stone / Grove</u> | Location: | <u>Sebring, FL</u> |
| Unit: | <u>RTD Owner</u> | Date: | <u>12/10/08</u> |



| Point No. | % of Diameter | Distance (Inches) |
|-----------|---------------|-------------------|
| 1 | 3.2% | 6.72 |
| 2 | 10.5% | 8.36 |
| 3 | 19.4% | 10.37 |
| 4 | 32.3% | 13.27 |
| 5 | 67.7% | 21.23 |
| 6 | 80.6% | 24.14 |
| 7 | 89.5% | 26.14 |
| 8 | 96.8% | 27.78 |



If a port depth is entered, then the measurements include that port depth.
Please note if adjustments are required to the outermost points.

QA/QC Check:

| Completeness | Legibility | Accuracy | Specifications | Reasonableness |
|---------------|-----------------------------|----------------------------------|-----------------|----------------|
| <u>R.H.K.</u> | <u>12/10/08</u> | <u>W. Price, P.E.</u> | <u>12/15/08</u> | |
| Signatures: | Technician (Signature/Date) | Project Manager (Signature/Date) | | |

Report on Calibration of Field Barometers

The following barometers were calibrated:

By: KENT CHODERS
Date: 12-1-08

| | <u>Pre-Calibration Reading</u> | <u>Adjustment Needed</u> |
|-------|--------------------------------|--------------------------|
| ATC 1 | <u>28.80</u> | <u>+0.045</u> |
| ATC 2 | <u>28.95</u> | <u>-0.055</u> |
| ATC 3 | <u>28.82</u> | <u>+0.075</u> |
| ATC 4 | <u>29.50</u> | <u>-0.605</u> |

Barometer adjusted to reading obtained from National Weather Service website. Reading adjusted for elevation of 835 ft.

National Weather Service Barometer reading, adjusted= 28.895

Calibration of ATC Field Barometers¹

| Barometer #1 | | | | |
|---------------------|--------------------------|---------------------------|-------------------|-------------|
| Date | Station Pressure, in. Hg | Barometer Reading, in. Hg | Adjustment Needed | Technician |
| 12/17/2007 | 29.365 | 29.400 | 0.035 | Childers, K |
| 1/4/2008 | 29.895 | 29.820 | 0.075 | Childers, K |
| 3/31/2008 | 29.515 | 29.560 | 0.045 | Childers, K |
| 4/7/2008 | 29.345 | 29.420 | 0.075 | Childers, K |
| 5/5/2008 | 29.205 | 29.240 | 0.035 | Burgess, T |
| 6/23/2008 | 29.205 | 29.140 | 0.065 | Poole, K |
| 7/1/2008 | 29.235 | 29.280 | 0.045 | Childers, K |
| 9/8/2008 | 29.285 | 29.250 | 0.035 | Burgess, T |
| 10/17/2008 | 29.145 | 29.100 | 0.045 | Poole, K |
| 11/10/2008 | 29.355 | 29.220 | 0.135 | Poole, M |
| 12/1/2008 | 28.895 | 28.800 | 0.095 | Childers, K |

| Barometer #3 | | | | |
|---------------------|--------------------------|---------------------------|-------------------|-------------|
| Date | Station Pressure, in. Hg | Barometer Reading, in. Hg | Adjustment Needed | Technician |
| 12/17/2007 | 29.365 | 29.620 | 0.255 | Childers, K |
| 1/4/2008 | 29.895 | 30.050 | 0.155 | Childers, K |
| 3/31/2008 | 29.515 | 29.350 | 0.165 | Childers, K |
| 4/7/2008 | 29.345 | Out of service | | Childers, K |
| 5/5/2008 | 29.205 | 29.180 | 0.025 | Burgess, T |
| 6/23/2008 | 29.205 | 29.355 | 0.150 | Poole, K |
| 7/1/2008 | 29.235 | 29.180 | 0.055 | Childers, K |
| 9/8/2008 | 29.285 | 29.300 | 0.015 | Burgess, T |
| 10/17/2008 | 29.145 | 29.550 | 0.405 | Poole, K |
| 11/10/2008 | 29.355 | 29.480 | 0.125 | Poole, M |
| 12/1/2008 | 28.895 | 28.820 | 0.075 | Childers, K |

| Barometer #2 | | | | |
|---------------------|--------------------------|---------------------------|-------------------|-------------|
| Date | Station Pressure, in. Hg | Barometer Reading, in. Hg | Adjustment Needed | Technician |
| 12/17/2007 | 29.365 | 29.400 | 0.035 | Childers, K |
| 1/4/2008 | 29.895 | 29.950 | 0.055 | Childers, K |
| 3/31/2008 | 29.515 | Unavailable | #VALUE! | Childers, K |
| 4/7/2008 | 29.345 | 29.420 | 0.075 | Childers, K |
| 5/5/2008 | 29.205 | Out of service | | Burgess, T |
| 6/23/2008 | 29.205 | 29.390 | 0.185 | Poole, K |
| 7/1/2008 | 29.235 | 29.280 | 0.045 | Childers, K |
| 9/8/2008 | 29.285 | 29.490 | 0.205 | Burgess, T |
| 10/17/2008 | 29.145 | Unavailable | #VALUE! | Poole, K |
| 11/10/2008 | 29.355 | 29.550 | 0.195 | Poole, M |
| 12/1/2008 | 28.895 | 28.950 | 0.055 | Childers, K |

| Barometer #4 (new 12/17/2007) | | | | |
|--------------------------------------|--------------------------|---------------------------|-------------------|-------------|
| Date | Station Pressure, in. Hg | Barometer Reading, in. Hg | Adjustment Needed | Technician |
| 12/17/2007 | 29.365 | 29.160 | 0.205 | Childers, K |
| 1/4/2008 | 29.895 | Unavailable | #VALUE! | Childers, K |
| 3/31/2008 | 29.515 | | 29.515 | Childers, K |
| 4/7/2008 | 29.345 | 29.350 | 0.005 | Childers, K |
| 5/5/2008 | 29.205 | 29.240 | 0.035 | Burgess, T |
| 6/23/2008 | 29.205 | 29.030 | 0.175 | Poole, K |
| 7/1/2008 | 29.235 | 29.260 | 0.025 | Childers, K |
| 9/8/2008 | 29.285 | 29.320 | 0.035 | Burgess, T |
| 10/17/2008 | 29.145 | 29.200 | 0.055 | Poole, K |
| 11/10/2008 | 29.355 | 29.330 | 0.025 | Poole, M |
| 12/1/2008 | 28.895 | 29.500 | 0.605 | Childers, K |

Shop Elevation = 835
Charlotte-Douglas Airport Elevation= 836

¹ Data provided by NOAA National Weather Service for Charlotte-Douglas Airport.

Primary Module Calibration Calculation

Date: **1/3/2008**
 Pbar: **29.22**
 Module ID: **ATC 1**

Calibrations by: **Kent Childers**
 Wet Test Serial No. or DGM #: **17562**
 Pre-test Calibration Factor **0.984**

| Orifice | Vw, ft ³ | Vd, ft ³ | Tw, °F | Td, °F | Time, minutes | dH@i | Yi |
|---------|---------------------|---------------------|--------|--------|---------------|--------------|--------------|
| 0.50 | 5.72 | 5.89 | 60.0 | 59.0 | 14.0 | 1.705 | 0.968 |
| 1.00 | 5.70 | 5.93 | 60.0 | 62.0 | 10.0 | 1.744 | 0.963 |
| 1.50 | 6.26 | 6.53 | 60.0 | 64.0 | 9.0 | 1.752 | 0.962 |
| 2.00 | 5.61 | 5.86 | 60.0 | 65.5 | 7.0 | 1.757 | 0.962 |
| 3.00 | 6.86 | 7.27 | 60.0 | 67.5 | 7.0 | 1.761 | 0.950 |
| 4.00 | 5.66 | 5.92 | 60.0 | 68.5 | 5.0 | 1.760 | 0.963 |
| | | | | | | 1.746 | 0.961 |

Specifications (QA Handbook-Vol III CD5-1, 9/30/94)

- 1) No value of ΔH@i shall vary from the average ΔH@ by more than 0.20.
- 2) No value of Yi shall vary from Yavg by more than 0.02.

$$dH @ = \frac{0.0319 \Delta H \left(P_b + \frac{\Delta H}{13.6} \right)}{(t_d + 459.69)} \left[\frac{(t_w + 459.69) \Theta}{V_w P_b} \right]^2$$

$$Y_i = \frac{V_w P_b (t_d + 459.69)}{V_d \left(P_b + \frac{\Delta H}{13.6} \right) (t_w + 459.69)}$$

QA/QC Check

Completeness Legibility Accuracy Specifications Reasonableness

Checked by: Kent Childers 1-2-08
 Personnel (Signature/Date)

W. Stewart Meader 1-28-08
 Team Leader (Signature/Date)

PRIMARY MODULE CALIBRATION CALCULATION

| | |
|----------------------------------|-------|
| Module I.D. | ATC 1 |
| Barometric Pressure, Pt | 29.22 |
| Pre-test Calibration Factor, Y = | 0.984 |

| | |
|-------------------------|-------------|
| Personnel | Kent Colder |
| Date | 1-2-2008 |
| Wet Test Meter Serial # | 17562 |

| Orifice Setting | V _w | | V _d | | T _w | | T _d | |
|-----------------|--------------------------|------------------------|--------------------------|------------------------|----------------|-----------|----------------|-----------|
| | Initial, ft ³ | Final, ft ³ | Initial, ft ³ | Final, ft ³ | Initial, °F | Final, °F | Initial, °F | Final, °F |
| 0.50 | 88.900 | 94.620 | 249.235 | 255.124 | 60 | 60 | 58 | 60 |
| 1.00 | 95.200 | 100.700 | 255.725 | 261.653 | 60 | 60 | 61 | 63 |
| 1.50 | 2.030 | 8.290 | 262.830 | 269.362 | 60 | 60 | 63 | 65 |
| 2.00 | 9.610 | 15.220 | 270.745 | 276.609 | 60 | 60 | 65 | 66 |
| 3.00 | 18.521 | 25.380 | 280.060 | 287.333 | 60 | 60 | 67 | 69 |
| 4.00 | 26.610 | 32.270 | 288.520 | 294.485 | 60 | 60 | 68 | 69 |

Specifications (QA Handbook-Vol III CD5-1, 9/30/94)

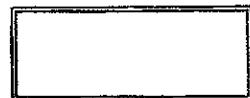
1) No value of ΔH@i shall vary from the average ΔH@ by more than 0.20

2) No value of Y_i shall vary from the average Y by more than 0.02.

$$\Delta H @ i = \frac{0.0319 \Delta H \left(P_b + \frac{\Delta H}{13.6} \right)}{(t_d + 459.69)} \left[\frac{(t_w + 459.69) @}{V_w P_b} \right]^2$$

$$Y_i = \frac{V_w P_b (t_d + 459.69)}{V_d \left(P_b + \frac{\Delta H}{13.6} \right) (t_w + 459.69)}$$

| Orifice Setting | TIME min. | ΔH@i | Y _i |
|-----------------|--------------|-------|----------------|
| 0.50 | 14 | 1.705 | 0.968 |
| 1.00 | 10 | 1.744 | 0.963 |
| 1.50 | 9 | 1.752 | 0.962 |
| 2.00 | 7 | 1.757 | 0.962 |
| 3.00 | 7 | 1.761 | 0.960 |
| 4.00 | 5 | 1.760 | 0.963 |
| | | 1.746 | 0.961 |

LegendV_w = Volume of Wet Test Meter, ft³V_d = Volume of Dry Gas Meter, ft³T_w = Temperature of Wet Test Meter, °FT_d = Temperature of Dry Gas Meter, °FΔH@i = Pressure differential across the orifice meter, in. H₂OY_i = Dry Gas Meter Calibration Coefficient, dimensionless

QA/QC Check:

Completeness

Legibility

Accuracy

Specifications

Reasonableness

Signatures:

Technician (Signature/Date)

W. Stewart MacLaren 1-2-08

Project Manager (Signature/Date)

POST-TEST MODULE CALIBRATION CALCULATION

| | |
|----------------------------------|--------|
| Module I.D. | ATC |
| Barometric Pressure, Pb | 29.638 |
| Pre-test Calibration Factor, Y = | 0.962 |

| | |
|-------------------------|----------|
| Personnel | m. Poole |
| Date | 12/11/08 |
| Wet Test Meter Serial # | 17562 |

| Orifice | Vacuum | V _w | | V _d | | T _w | | T _d | |
|---------|--------|--------------------------|------------------------|--------------------------|------------------------|----------------|-----------|----------------|-----------|
| | | Initial, ft ³ | Final, ft ³ | Initial, ft ³ | Final, ft ³ | Initial, °F | Final, °F | Initial, °F | Final, °F |
| 2.0 | 5 | 68.26 | 76.41 | 590.790 | 599.166 | 65 | 65 | 69 | 70 |
| 2.0 | 5 | 76.41 | 84.57 | 599.166 | 607.569 | 65 | 65 | 70 | 71 |
| 2.0 | 5 | 84.57 | 92.73 | 607.569 | 615.988 | 65 | 65 | 71 | 71 |

Specifications (QA Handbook-Vol III CDB-1, 9/30/94)

- 1) The average post-test meter calibration factor (Y_1) shall be within $\pm 5\%$ of the pre-test calibration factor, as stated by the equation below.

$$0.95 \times Y < Y_{avg} < 1.05 \times Y$$

$$Y_1 = \frac{V_w P_b (t_d + 459.69)}{V_d \left(P_b + \frac{\Delta H}{13.6} \right) (t_w + 459.69)}$$

| Orifice Setting | TIME min. | $\Delta H@I$ | Y_1 |
|-----------------|-----------|--------------|-------|
| 2.0 | 10 | 1.694 | 0.977 |
| 2.0 | 10 | 1.687 | 0.976 |
| 2.0 | 10 | 1.685 | 0.975 |
| | | 1.689 | 0.976 |

Post-test calibration factor acceptable? LegendV_w = Volume of Wet Test Meter, ft³V_d = Volume of Dry Gas Meter, ft³T_w = Temperature of Wet Test Meter, °FT_d = Temperature of Dry Gas Meter, °FΔH@I = Pressure differential across the orifice meter, in. H₂OY₁ = Dry Gas Meter Calibration Coefficient, dimensionlessProject No.

8192

QA/QC Check:

| | |
|--------------|---|
| Completeness | ✓ |
|--------------|---|

| | |
|------------|---|
| Legibility | ✓ |
|------------|---|

| | |
|----------|---|
| Accuracy | ✓ |
|----------|---|

| | |
|----------------|---|
| Specifications | ✓ |
|----------------|---|

| | |
|----------------|---|
| Reasonableness | ✓ |
|----------------|---|

Signatures: Mason Poole 12/11/08

Technician (Signature/Date)

W. Kier Poole 12/15/08

Project Manager (Signature/Date)

POST TEST MODULE CALIBRATION CALCULATION

E-Stone/Grove

Date: **12/11/2008**
 Pbar: **29.64**
 Module ID: **ATC 1**
 Calibration by: **Mallory Poole**

8192 Client Project Number
17562 Wet Test Serial No. or DGM #
0.962 Pre-test Calibration Factor
Acceptable Post-test Calibration Acceptable?¹

| Orifice | Vac, "Hg | Vw | Vd | Tw | Td | Time | dH@ | Y |
|-------------------------|----------|------|------|------|------|------|-------|-------|
| 2.00 | 5.00 | 8.15 | 8.38 | 65.0 | 69.5 | 10.0 | 1.694 | 0.977 |
| 2.00 | 5.00 | 8.16 | 8.40 | 65.0 | 70.5 | 10.0 | 1.687 | 0.976 |
| 2.00 | 5.00 | 8.16 | 8.42 | 65.0 | 71.0 | 10.0 | 1.685 | 0.975 |
| 1.689 0.976 | | | | | | | | |

¹Requirement-40CFR60 App A Method 5 10.3.1.1

$$dH @ = \frac{0.0319 \Delta H \left(P_b + \frac{\Delta H}{13.6} \right) \left[(t_w + 459.69) \Theta \right]^2}{(t_d + 459.69) \left[V_w P_b \right]}$$

$$Y_i = \frac{V_w P_b (t_d + 459.69)}{V_d \left(P_b + \frac{\Delta H}{13.6} \right) (t_w + 459.69)}$$

STANDARD GAS METER SALES AND REPAIR INC
537 WEST MAIN ST ~
PO BOX 273
ALBEMARLE NC 28001
704-982-9601 FAX 704-982-9705
standard gas@ctc.net

Analytical Testing Consultants
Kannapolis NC

03-19-08

Testing conditions for American AL19#17562:

Barometer--30.15", Prover Air Temp 70.75F, Meter Water Temp 69.75F"
1.5" WC pressure.

With meter at exact level position, meter water level was adjusted to give a reading of exactly 2 CF on the meter and exactly 2CF on the prover. Meniscus indicator was then set to this point and checked after operation. All tests were satisfactory.

Calibrated on RW Prover#81, Certified tape #26727.

Douglas P Miller
Douglas P Miller---SGM

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MAR 19 2008

BY: WKF

Thermocouple Post-test Calibration Data Form

according to Alternative Method 2 Procedures (ALT-011)

| | | | | |
|-------------------|----------------------------------|--------------------------------|--|--|
| Client: | <u>E-Stone /Grove</u> | | | |
| Test Location: | <u>Seminole, FL</u> | | | |
| Ambient Temp., °F | <u>64°</u> | | | |
| Technician | <u>M. Poole</u> | | | |
| Thermocouple | Source ² (Specify) | Reference Temperature °F | Thermocouple Potentiometer Temperature, °F | Temperature Difference °F ³ |
| Stack | | | | |
| Probe | Ambient | 64° | 63° | 1° F |

¹ Reference thermometer-mercury in glass

² May be ambient air or other

³ Difference must be 2 °F or less.

QA/QC Check

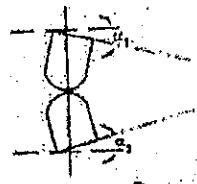
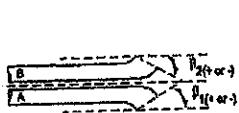
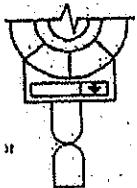
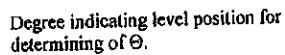
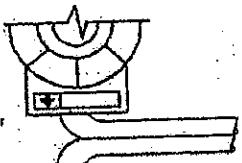
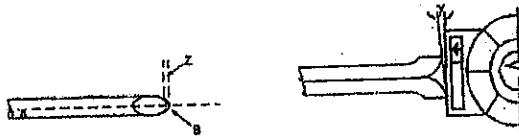
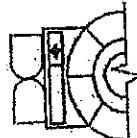
Completeness Legibility Accuracy Specifications Reasonableness

Checked by: Mallory Poole
 Calibration Technician 12/11/08
 (Signature/Date)

W. Kiel Poole 12/15/08
 Test Team Leader
 (Signature/Date)

Analytical Testing Consultants, Inc.

Post-test Type S Pitot Tube Inspection Sheet

Degree indicating level position for determining α_1 and α_2 .Degree indicated level position for determining β_1 and β_2 .Degree indicating level position for determining θ .Degrees indicating level position for determining γ then calculate Z .

| | |
|--|-------|
| <i>Level and Perpendicular?</i> | Y |
| <i>Obstruction?</i> | N |
| <i>Damaged?</i> | N |
| $\alpha_1 (-10^\circ \leq \alpha_1 \leq +10^\circ)$ | 2 |
| $\alpha_2 (-10^\circ \leq \alpha_2 \leq +10^\circ)$ | 2 |
| $\beta_1 (-5^\circ \leq \beta_1 \leq +5^\circ)$ | 0 |
| $\beta_2 (-5^\circ \leq \beta_2 \leq +5^\circ)$ | 0 |
| γ | 1 |
| Θ | 1 |
| $Z = A \tan \gamma (\leq 0.125")$ | 0.015 |
| $W = A \tan \Theta (\leq 0.03125")$ | 0.015 |
| $D_t (3/16" \leq D_t \leq 3/8")$ | .385 |
| A | .864 |
| $A/2D_t (1.05 \leq P_t/D_t \leq 1.50)$ | 1.122 |
| <i>If temperature sensor is flush with pitot tube opening, is $Z \geq \frac{3}{4}''$?</i> | Y |
| <i>If temperature sensor is set back from pitot tube opening, is $W > 2''$?</i> | N/A |
| <i>Is $X \geq \frac{1}{4}$" for $D_t = \frac{1}{2}$"</i> | Y |
| <i>Is impact side of pitot tube even with or above nozzle entry plane?</i> | Y |
| <i>Is $Y \geq 3"$ for $3/16" < D_t < 3/8"$?</i> | Y |

QA/QC CheckCompleteness Legibility Accuracy Specifications Reasonableness **Certification**

I certify that the Type S pitot tube/probe ID # 57 meets or exceeds all specifications, criteria and/or applicable design features and is hereby assigned a pitot tube calibration factor C_p of 0.84¹.

Certified by: Mallory Poole 12/11/08 W. Keith Peeler 12/15/08

¹ This certification also applies to the specifications of EPA Method 2, section 10.1.4.1.1 regarding inter-component spacing of pitot tube-sampling probe assemblies. Refer to the figures on the reverse side of this page for specifics.



P. O. Box 12013
Research Triangle Park, NC 27709
Phone 919/544-3777

CERTIFICATE OF ANALYSIS: EPA PROTOCOL GAS MIXTURE

| | | | |
|--------------|-------------------------------|---------------------|--------------|
| Customer: | National Welders, Concord, NC | Reference # | 88-106317 |
| NSG PO# | 5667067 | Certification Date: | 09/27/06 |
| Customer PO# | | Expiration Date: | 09/27/09 |
| Cylinder # | SG-9140087-BAL | Pressure, psig* | 2000 CGA 590 |

ANALYTICAL INFORMATION

METHOD: This standard was analyzed according to EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards.
Procedure G1 (September 1997)

ANALYZED CYLINDER

Components

Certified Concentration

Analytical Accuracy**

| | | |
|---------------|-----------|-------|
| Propane | 10110 ppm | +/-1% |
| Balance - Air | | |

| REFERENCE STANDARD | Cylinder # | Concentration |
|--|------------|-------------------|
| Type/SRM Sample # GMIS (Traceable to SRM # 2648a) | CC35920 | 5000 ppm C3H8/AIR |

| INSTRUMENTATION | Last Date Calibrated | Analytical Method |
|---|----------------------|---------------------------|
| Instrument/Model/Serial # Rosemount 400A THC 2000335 | 08/28/06 | Flame Ionization Detector |

Analyst: Nicole Ishak Nicole Ishak

This report states accurately the results of the investigation made upon the material submitted to the analytical laboratory. Every effort has been made to determine objectively the information requested. However, in connection with this report, National Specialty Gases shall have no liability in excess of established charge for this service. Assayed at National Specialty Gases, 630 United Drive, Durham, NC 27713 (919) 544-3772

*Do not use this standard when cylinder pressure is below 150 psig.

NSG 020149L

**Analytical accuracy includes typical known error sources which, at least, include precision of the analytical instrument.



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SEP 9 2008

BY: WKP

**CERTIFICATE OF ANALYSIS
EPA PROTOCOL GAS MIXTURE**

Manufactured and Assayed at:
NATIONAL WELDERS SUPPLY CO.
 4236 STATESVILLE RD
 CHARLOTTE, NC 28269
 704-596-6262

Produced for customer:
NATIONAL WELDERS SUPPLY CO., 94 - Concord
 287 EXECUTIVE PARK DRIVE
 CONCORD, NC 28025
 704-788-6615

| | | | |
|----------------------|-----------------------------|---------------------|-----------------|
| Product Code: | 780981 | Certification Date: | 08/26/08 |
| Product Description: | EPA PROTOCOL MIX 2PT BAL N2 | Expiration Date: | 08/27/11 |
| Lot # | CU99H8200DA | Pressure, psig* | 2000 |
| Order # | 6943906 | CGA | CGA 590 |
| Cylinder # | CC185468 | Certificate # | LC1-CU99H8200DA |
| Page # | 1 of 1 | | |

This standard was analyzed according to EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards: Procedure G1 (September 1997)

| Components | Requested Concentration | Certified Concentration and Expanded Uncertainty | | Units | Analytical Accuracy | Procedure |
|------------|-------------------------|--|---------|-------|---------------------|--------------------|
| Oxygen | 10.5 | 10.5 | +/- 0.1 | % | +/- 1% | 304.LAB.0030, R-00 |

Nitrogen Balance

| Reference Standard # | Standard Type | Cylinder # | Concentration | Expiration Date |
|----------------------|---------------|------------|-----------------|-----------------|
| 2349 | GMIS | 112347 | 10.01 % O2 / N2 | 01/17/10 |

| Instrument # | Instrument | Serial # | Analytical Method | Calibration Date |
|--------------|----------------|----------|-------------------|------------------|
| 154 | Teledyne 3000M | 240141 | Paramagnetic | 08/26/08 |

Analytical Report Approved by: Lance Crayton

Lance Crayton

Lab Analyst

All analyses are performed under controlled environmental conditions. This product is manufactured using equipment which has been calibrated with NIST traceable, or equivalent, standards, weights, or equipment.

*Do not use this standard when cylinder pressure is below 150 psig.

CU.LAB.0100.B
Rev 01



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AUG 26 2008

BY: WGP

CERTIFICATE OF ANALYSIS EPA PROTOCOL GAS MIXTURE

Manufactured and Assayed at:
NATIONAL WELDERS SUPPLY CO.
 4236 STATESVILLE RD
 CHARLOTTE, NC 28269
 704-596-6262

Produced for customer:
NATIONAL WELDERS SUPPLY CO., 94 - Concord
 287 EXECUTIVE PARK DRIVE
 CONCORD, NC 28025
 704-788-6615

| | | | |
|----------------------|--------------|---------------------|-----------------|
| Product Code: | 780981 | Certification Date: | 08/19/08 |
| Product Description: | EPA PROTOCOL | Expiration Date: | 08/20/11 |
| Lot # | CU99H8150DA | Pressure, psig* | 2000 |
| Order # | 6935693 | CGA | CGA 590 |
| Cylinder # | CC166921 | Certificate # | LC1-CU99H8150DA |
| Page # | 1 of 1 | | |

This standard was analyzed according to EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards: Procedure G1 (September 1997)

| Components | Requested Concentration | Certified Concentration and Expanded Uncertainty | Units | Analytical Accuracy | Procedure |
|------------|-------------------------|--|-------|---------------------|--------------------|
| Oxygen | 20.9 | 20.9 +/- 0.2 % | % | +/- 1% | 304.LAB.0030, R-00 |

Nitrogen Balance

| Reference Standard # | Standard Type | Cylinder # | Concentration | Expiration Date |
|----------------------|---------------|------------|---------------|------------------|
| 2291 | GMIS | AT9284 | 21.03 % | O2 / N2 01/17/10 |

| Instrument | Manufacturer | Serial # | Analytical Method | Calibration Date |
|------------|----------------|----------|-------------------|------------------|
| 154 | Teledyne 3000M | 240141 | Paramagnetic | 08/19/08 |

Analytical Report Approved by: Z. S.

Lance Crayton
Lab Analyst

All analyses are performed under controlled environmental conditions. This product is manufactured using equipment which has been calibrated with NIST traceable, or equivalent, standards, weights, or equipment.

*Do not use this standard when cylinder pressure is below 150 psig.

CU.LAB.0100.B
Rev 01



P. O. Box 12013
 Research Triangle Park, N.C. 27709
 Phone 919/544-3772

CERTIFICATE OF ANALYSIS: EPA PROTOCOL GAS MIXTURE

| | | | |
|---|-------------------------------|---------------------|--------------|
| Customer: | National Welders, Concord, NC | Reference # | 88-115014 |
| NSG PO# | 6541039 | Certification Date: | 02/12/08 |
| Customer PO# | | Expiration Date: | 02/12/11 |
| Cylinder # | CC100061 | Pressure, psig* | 2000 CGA 580 |
| ANALYTICAL INFORMATION | | | |
| METHOD: This standard was analyzed according to EPA Traceability Protocol for Assay and Certification of Gaseous Calibration Standards: Procedure G1 (September 1997) | | | |

ANALYZED CYLINDER

| Components | Certified Concentration | Analytical Accuracy** |
|--------------------|-------------------------|-----------------------|
| Carbon Dioxide | 20.99% | +/-1% |
| Balance - Nitrogen | | |

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FEB 22 2008

BY: W.K.P.

REFERENCE STANDARD

| Type/SRM Sample # | Cylinder # | Concentration | |
|-------------------------------------|------------|---------------|--------|
| GMIS (Traceable to NTRM # 82745x) | CC117299 | 19.02 % | CO2/N2 |

INSTRUMENTATION

| Instrument/Model/Serial # | Last Date Calibrated | Analytical Method |
|---------------------------|----------------------|----------------------------|
| KVB Analect EN-844A | 01/12/08 | Fourier Transform Infrared |

Analyst: Richard Sykes Richard Sykes

This report states accurately the results of the investigation made upon the material submitted to the analytical laboratory. Every effort has been made to determine objectively the information requested. However, in connection with this report, National Specialty Gases shall have no liability in excess of established charge for this service. Assayed at National Specialty Gases, 630 United Drive, Durham, NC 27713 (919) 544-3772

*Do not use this standard when cylinder pressure is below 150 psig.

**Analytical accuracy includes typical known error sources which, at least, include precision of the analytical instrument.

NSG 020149L



**MATHESON
TRI-GAS**

ask...The Gas Professionals™

Certified Mixture Grade

TO: Enthalpy Analytical
2202 Ellis Rd Suite A
Durham, NC 27703

PHONE:
FAX:

PRODUCT:

CYLINDER NUMBER: SX18013
SIZE: 1R
CGA/DISS OUTLET: 350
CONTENT: 29.7 cu. ft.
PRESSURE: 420 psig

**TO AVOID BACKFILL, CYLINDER PRESSURE MUST BE
GREATER THAN PROCESS PRESSURE**

SALES ORDER NUMBER: 429723

P.O. NUMBER: C-BDT0108-01

LOT NUMBER: 1057610195

FILL DATE: Dec 11, 2007

CERTIFICATION DATE: Dec 11, 2007

EXPIRATION DATE: Dec 11, 2008.

TRACEABLE TO REFERENCE STANDARD SOURCE/NUMBER:
TRACEABLE TO NIST TRACEABLE WEIGHT CERTIFICATE:

SPECIAL INFORMATION / ADDITIONAL COMMENTS

The product listed above and furnished under the referenced purchase order has been tested and found to contain the component concentration listed above. All values in mole/mole basis gas phase unless otherwise indicated. Matheson Tri-Gas Inc. warrants that the above product(s) conform at the time of shipment to the above description. Matheson Tri-Gas Inc. liability does not exceed the value of the product purchased.

Derek Stuck
ANALYST

SIGNATURE

Dec 11, 2007

DATE SIGNED

Page 1 of 1



Series 2020

System S/N 1549

ENVIRONICS FLOW CONTROLLER CALIBRATION SHEET

MFC#: 1

Size: 10000 SCCM

SERIAL NUMBER AW9404312

This flow controller was calibrated using a Sierra Cal Bench™, a NIST traceable Primary Flow Standard Calibration System. This calibration was performed with Nitrogen at a standard reference temperature and pressure of 32° and 29.92 in.HG. This is not performance data. This data is used by the system operating modes to improve the flow accuracy.

| | | <u>Set Flow</u> | <u>True Flow</u> | RECEIVED |
|-----|---|-----------------|------------------|-----------------|
| 5 | % | 500.0 CCM | 498.037 CCM | OCT 13 2008 |
| 10 | % | 1000.0 CCM | 998.684 CCM | BY: <u>WKF</u> |
| 20 | % | 2000.0 CCM | 1999.357 CCM | |
| 30 | % | 3000.0 CCM | 3007.361 CCM | |
| 40 | % | 4000.0 CCM | 4018.146 CCM | |
| 50 | % | 5000.0 CCM | 5026.669 CCM | |
| 60 | % | 6000.0 CCM | 6030.894 CCM | |
| 70 | % | 7000.0 CCM | 7137.938 CCM | |
| 80 | % | 8000.0 CCM | 8103.815 CCM | |
| 90 | % | 9000.0 CCM | 9089.607 CCM | |
| 100 | % | 10000.0 CCM | 10093.105 CCM | |

Verified by:

Date: 10-9-08

Computerized Gas Mixing / Dilution / Calibration Systems

Environics Inc. • 69 Industrial Park Road East • Tolland, CT 06084 • (860) 872-1111 • Fax (860) 870-9333
World Wide Web: <http://www.environics.com> E-mail: info@environics.com
Report Appendix Page 122 of 131



Series 2020

System S/N 1549

ENVIRONICS FLOW CONTROLLER CALIBRATION SHEET

MFC#: 2 Size: 10000 SCCM

SERIAL NUMBER 2278700001

This flow controller was calibrated using a Sierra Cal Bench™, a NIST traceable Primary Flow Standard Calibration System. This calibration was performed with Nitrogen at a standard reference temperature and pressure of 32° and 29.92 in.HG. This is not performance data. This data is used by the system operating modes to improve the flow accuracy.

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OCT 13 2008

BY: WKP

| | <u>Set Flow</u> | | <u>True Flow</u> | |
|-------|-----------------|-----|------------------|-----|
| 5 % | 500.0 | CCM | 520.811 | CCM |
| 10 % | 1000.0 | CCM | 1047.725 | CCM |
| 20 % | 2000.0 | CCM | 2064.903 | CCM |
| 30 % | 3000.0 | CCM | 3076.453 | CCM |
| 40 % | 4000.0 | CCM | 4076.480 | CCM |
| 50 % | 5000.0 | CCM | 5066.699 | CCM |
| 60 % | 6000.0 | CCM | 6051.525 | CCM |
| 70 % | 7000.0 | CCM | 7039.665 | CCM |
| 80 % | 8000.0 | CCM | 8020.777 | CCM |
| 90 % | 9000.0 | CCM | 8987.212 | CCM |
| 100 % | 10000.0 | CCM | 10080.691 | CCM |

Verified by: WKP

Date: 10-9-08

**Series 2020**

System S/N 1549

ENVIRONICS FLOW CONTROLLER CALIBRATION SHEET

MFC#: 3 Size: 1000 SCCM

SERIAL NUMBER AW9603228

This flow controller was calibrated using a Sierra Cal Bench™, a NIST traceable Primary Flow Standard Calibration System. This calibration was performed with Nitrogen at a standard reference temperature and pressure of 32° and 29.92 in.HG. This is not performance data. This data is used by the system operating modes to improve the flow accuracy.

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OCT 13 2008

BY: WICP

| | | <u>Set Flow</u> | <u>True Flow</u> |
|-----|---|-----------------|------------------|
| 5 | % | 50.0 CCM | 50.480 CCM |
| 10 | % | 100.0 CCM | 101.310 CCM |
| 20 | % | 200.0 CCM | 202.296 CCM |
| 30 | % | 300.0 CCM | 302.715 CCM |
| 40 | % | 400.0 CCM | 403.698 CCM |
| 50 | % | 500.0 CCM | 504.749 CCM |
| 60 | % | 600.0 CCM | 605.013 CCM |
| 70 | % | 700.0 CCM | 705.543 CCM |
| 80 | % | 800.0 CCM | 807.418 CCM |
| 90 | % | 900.0 CCM | 914.259 CCM |
| 100 | % | 1000.0 CCM | 1017.477 CCM |

Verified by: Date: 10-9-08

**Series 2020**

System S/N 1549

ENVIRONICS FLOW CONTROLLER CALIBRATION SHEET

MFC#: 4 Size: 100 SCCM

SERIAL NUMBER AW9804034

This flow controller was calibrated using a Sierra Cal Bench™, a NIST traceable Primary Flow Standard Calibration System. This calibration was performed with Nitrogen at a standard reference temperature and pressure of 32° and 29.92 in.HG. This is not performance data. This data is used by the system operating modes to improve the flow accuracy.

| | | <u>Set Flow</u> | <u>True Flow</u> |
|-----|---|-----------------|------------------|
| 5 | % | 5.0 CCM | 5.160 CCM |
| 10 | % | 10.0 CCM | 10.124 CCM |
| 20 | % | 20.0 CCM | 20.076 CCM |
| 30 | % | 30.0 CCM | 30.140 CCM |
| 40 | % | 40.0 CCM | 40.023 CCM |
| 50 | % | 50.0 CCM | 49.984 CCM |
| 60 | % | 60.0 CCM | 60.292 CCM |
| 70 | % | 70.0 CCM | 70.461 CCM |
| 80 | % | 80.0 CCM | 80.329 CCM |
| 90 | % | 90.0 CCM | 90.898 CCM |
| 100 | % | 100.0 CCM | 101.009 CCM |

RECEIVED

OCT 13 2008

BY: WJP

Verified by:

Date: 10-9-08

Computerized Gas Mixing / Dilution / Calibration Systems

Environics Inc. • 69 Industrial Park Road East • Tolland, CT 06084 • (860) 872-1111 • Fax (860) 870-9333

World Wide Web: <http://www.environics.com>E-mail: info@environics.com

Report Appendix Page 125 of 131

**Series 2020**

System S/N 1549

ENVIRONICS FLOW CONTROLLER CALIBRATION SHEET

MFC#: 5 Size: 10 SCCM

SERIAL NUMBER AW9711212

This flow controller was calibrated using a Sierra Cal Bench™, a NIST traceable Primary Flow Standard Calibration System. This calibration was performed with Nitrogen at a standard reference temperature and pressure of 32° and 29.92 in.HG. This is not performance data. This data is used by the system operating modes to improve the flow accuracy.

| | <u>Set Flow</u> | <u>True Flow</u> |
|-------|-----------------|------------------|
| 5 % | 0.5 CCM | 0.535 CCM |
| 10 % | 1.0 CCM | 1.042 CCM |
| 20 % | 2.0 CCM | 2.063 CCM |
| 30 % | 3.0 CCM | 3.075 CCM |
| 40 % | 4.0 CCM | 4.078 CCM |
| 50 % | 5.0 CCM | 5.085 CCM |
| 60 % | 6.0 CCM | 6.077 CCM |
| 70 % | 7.0 CCM | 7.080 CCM |
| 80 % | 8.0 CCM | 8.084 CCM |
| 90 % | 9.0 CCM | 9.080 CCM |
| 100 % | 10.0 CCM | 10.072 CCM |

RECEIVED

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BY: WKR

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Report Appendix Page 126 of 131

BOBBY JINDAL
GOVERNOR



HAROLD LEGGETT, PH.D.
SECRETARY

State of Louisiana
DEPARTMENT OF ENVIRONMENTAL QUALITY
OFFICE OF ENVIRONMENTAL ASSESSMENT
LABORATORY SERVICES DIVISION

CERTIFIED MAIL #7007 0710 0005 6108 4374

Return Receipt Requested

June 23, 2008

AI #94216

LELAP Lab ID #04044

Mr. W. Keith Poole
Analytical Testing Consultants, Inc.
301 Brookdale Street
Kannapolis, NC 28083-2787

RE: Accreditation Certificate

Dear Mr. Poole:

In accordance with Louisiana Administrative Code, Title 33, Part I, Subpart 3, Laboratory Accreditation, the State of Louisiana formally recognizes that this laboratory has successfully completed the accreditation process and is technically competent to perform the environmental analyses listed on the scope of accreditation detailed in the attachment. Accreditation does not constitute an endorsement of the suitability of the listed methods for any specific purpose. Parameters or analytes that the laboratory has applied for accreditation not included in the scope of accreditation attachment are not accredited. The laboratory will be accredited for the method as identified on the application for accreditation; if the method is partially identified on the application for accreditation, the laboratory will be accredited for all versions of the method.

NELAP accreditation is granted only for those methods/analytes for which "NELAP" is indicated as the type of accreditation. "STATE" is indicated as the type of accreditation for those methods/analytes for which NELAP accreditation is not available. Accreditation is dependent on the laboratory's successful ongoing compliance with regulations as outlined in the Louisiana Administrative Code, Title 33, Part I, Subpart 3, Laboratory Accreditation.

The enclosed accreditation certificate is property of the State of Louisiana. Should a change in accreditation status occur, the Department may recall the original accreditation certificate and attachments. The recalled certificate and attachments should be returned

Mr. W. Keith Poole
Analytical Testing Consultants, Inc.
June 23, 2008
Page 2 of 2

to the Office of Environmental Assessment, Louisiana Environmental Laboratory Accreditation Program, P.O. Box 4314, Baton Rouge, LA 70821-4314, Attention: Paul Bergeron.

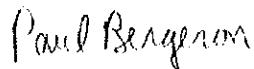
LAC 33:I.5313.A requires that the laboratory report must include all relevant information. Therefore, the certificate number shall be placed in the upper right corner of all laboratory reports. If the test report includes results of any test for which the laboratory is not accredited, the unaccredited results must be clearly identified as such.

Please be advised that it is your responsibility to examine the scope of accreditation attachment for accuracy and completeness. If you find that an analyte for which you expected to be accredited is not listed, please examine your records to ensure that:

1. You have met the requirements for successful participation in proficiency test studies as outlined in LAC 33:I.4711 and in the NELAC Standard 2.7.2.
2. In the case of accreditation by recognition, the requested analyte must be listed for the requested method and matrix on both the certificate issued by the Primary Accreditation Body *and* on the Louisiana application form.

If you have any questions, please contact the Louisiana Environmental Laboratory Accreditation Program at (225) 219-9800.

Sincerely,



Paul Bergeron, Supervisor
Louisiana Environmental Laboratory Accreditation Program

PB:clg

Enclosure

*Laboratory Scope of Accreditation*

Organization

04044

Analytical Testing Consultants Inc.
301 Brookdale Street
Kannapolis, NC 28083-2787

(704) 932-3193

Louisiana Stack Testing Program Certification

| Method Code | Method Ref | Analyte | Status | Date Effective | Type | AA |
|--------------|--|---|------------|----------------|-------|----|
| 764 | Performance Specification 2 | Oxides of nitrogen | Accredited | 6/2/2004 | STATE | LA |
| R754 | Performance Specification 2 | Sulfur dioxide | Accredited | 6/2/2004 | STATE | LA |
| Report 755 | Performance Specification 3 | Carbon dioxide | Accredited | 6/2/2004 | STATE | LA |
| Report 755 | Performance Specification 3 | Oxygen | Accredited | 6/2/2004 | STATE | LA |
| R756 | Performance Specification 4 | Carbon monoxide (CO) | Accredited | 6/2/2004 | STATE | LA |
| Report 759 | Performance Specification 6 | Emission Rate | Accredited | 6/2/2004 | STATE | LA |
| Appendix 761 | Performance Specification 8 | VOC's | Accredited | 6/2/2004 | STATE | LA |
| 1117 | ALT-008 | Moisture Midget Impingers | Accredited | 6/2/2004 | STATE | LA |
| Page 1217 | Method 1 40 CFR 60 App. A | Traverse Points | Accredited | 6/2/2004 | STATE | LA |
| 1245 | Method 17 40 CFR 60 App. A | Particulates | Accredited | 6/2/2004 | STATE | LA |
| 1248 | Method 1A 40 CFR 60 App. A | Traverse Points | Accredited | 6/2/2004 | STATE | LA |
| 1249 | Method 2 40 CFR 60 App. A | Stack gas velocity volume flow rate | Accredited | 6/2/2004 | STATE | LA |
| 1251 | Method 201A 40 CFR 51 App. M | Particulates <10 um | Accredited | 6/2/2004 | STATE | LA |
| 1252 | Method 202 40 CFR 51 App. M | Particulate Matter <2.5 um | Accredited | 6/2/2004 | STATE | LA |
| 1271 | Method 2A 40 CFR 60 App. A | Stack gas velocity volume flow rate in small stacks/ducts | Accredited | 6/2/2004 | STATE | LA |
| 1272 | Method 2B 40 CFR 60 App. A | Stack gas velocity volume flow rate | Accredited | 6/2/2004 | STATE | LA |
| 1279 | Method 3 40 CFR 60 App. A | Carbon dioxide oxygen dry molecular weight | Accredited | 6/2/2004 | STATE | LA |
| 1296 | Method 3A 40 CFR 60 App. A | Carbon dioxide | Accredited | 6/2/2004 | STATE | LA |
| 1296 | Method 3A 40 CFR 60 App. A | Oxygen | Accredited | 6/2/2004 | STATE | LA |
| 1297 | Method 3B 40 CFR 60 App. A | Emission Rate Correction Factors | Accredited | 6/2/2004 | STATE | LA |
| 1302 | Method 4 40 CFR 60 App. A | Moisture content | Accredited | 6/2/2004 | STATE | LA |
| 1303 | Method 5 40 CFR 60 App. A | Particulates | Accredited | 6/2/2004 | STATE | LA |
| 1304 | Method 5A 40 CFR 60 App. A | Particulates from asphalt processing | Accredited | 6/2/2004 | STATE | LA |
| 1305 | Method 5B 40 CFR 60 App. A | Particulates | Accredited | 6/2/2004 | STATE | LA |
| 1306 | Method 5D 40 CFR 60 App. A | Particulates from fabric filters | Accredited | 6/2/2004 | STATE | LA |
| 1308 | Method 5F 40 CFR 60 App. A | Particulates | Accredited | 6/2/2004 | STATE | LA |
| 1757 | Method 10 40 CFR 60 App. A (Sample Only) | Carbon monoxide (CO) | Accredited | 7/1/2003 | STATE | LA |

Issue Date: July 1, 2008

Expiration Date: June 30, 2009

Print Date

6/17/2008 9:22:25 AM

*Laboratory Scope of Accreditation*

Organization

04044
Analytical Testing Consultants Inc.
301 Brookdale Street
Kannapolis, NC 28083-2787

(704) 932-3193

Louisiana Stack Testing Program Certification

| Method Code | Method Ref | Analyte | Status | Date Effective | Type | AA |
|-------------|---|---|------------|----------------|-------|----|
| 1813 | Method 18 40 CFR 60 App. A (Sample Only) | Gaseous Organic Compound Emissions | Accredited | 6/2/2004 | STATE | LA |
| 1841 | Method 205 40 CFR 51 App. M (Sample Only) | Verification of Gas Dilution Systems for Field Instrument Calibration | Accredited | 6/2/2004 | STATE | LA |
| 1851 | Method 25A 40 CFR 60 App. A (Sample Only) | Gaseous Organic Emissions | Accredited | 6/2/2004 | STATE | LA |
| 1951 | Method 6C 40 CFR 60 App. A (Sample Only) | Sulfur dioxide | Accredited | 6/2/2004 | STATE | LA |
| 1963 | Method 7E 40 CFR 60 App. A (Sample Only) | Nitrogen Oxides (NOx) | Accredited | 6/2/2004 | STATE | LA |
| 2163 | Method 25B 40 CFR 60 App. A | Total Organic Compounds | Accredited | 6/2/2004 | STATE | LA |

Issue Date: July 1, 2008

Expiration Date: June 30, 2009

Print Date

6/17/2008 9:22:25 AM



STATE OF LOUISIANA
DEPARTMENT OF ENVIRONMENTAL QUALITY

Is hereby granting a Louisiana Environmental Laboratory Accreditation to



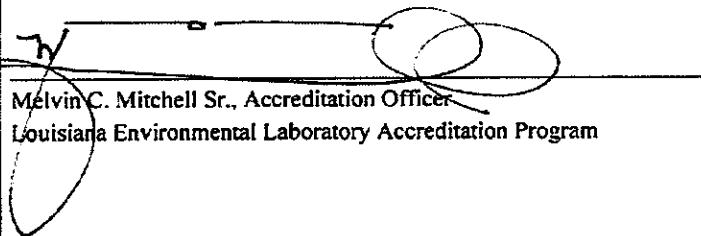
Analytical Testing Consultants Inc.
301 Brookdale Street
Kannapolis, NC 28083-2787

Agency Interest No. 94216

According to the Louisiana Administrative Code, Title 33, Part I, Subpart 3, LABORATORY ACCREDITATION, the State of Louisiana formally recognizes that this laboratory is technically competent to perform the environmental analyses listed on the scope of accreditation detailed in the attachment.

The laboratory agrees to perform all analyses listed on this scope of accreditation according to the Part I, Subpart 3 requirements and acknowledges that continued accreditation is dependent on successful ongoing compliance with the applicable requirements of Part I. Please contact the Department of Environmental Quality, Louisiana Environmental Laboratory Accreditation Program (LELAP) to verify the laboratory's scope of accreditation and accreditation status. Accreditation by the State of Louisiana is not an endorsement or a guarantee of validity of the data generated by the laboratory, and does not constitute an endorsement of the suitability of the listed methods for any specific application.

To be accredited initially and maintain accreditation, the laboratory agrees to participate in two single-blind, single-concentration PT studies, where available, per year for each field of testing for which it seeks accreditation or maintains accreditation as required in LAC 33:1.4711.


Melvin C. Mitchell Sr., Accreditation Officer
Louisiana Environmental Laboratory Accreditation Program

Certificate Number: 04044
Expiration Date: June 30, 2009
Issued On: July 1, 2008

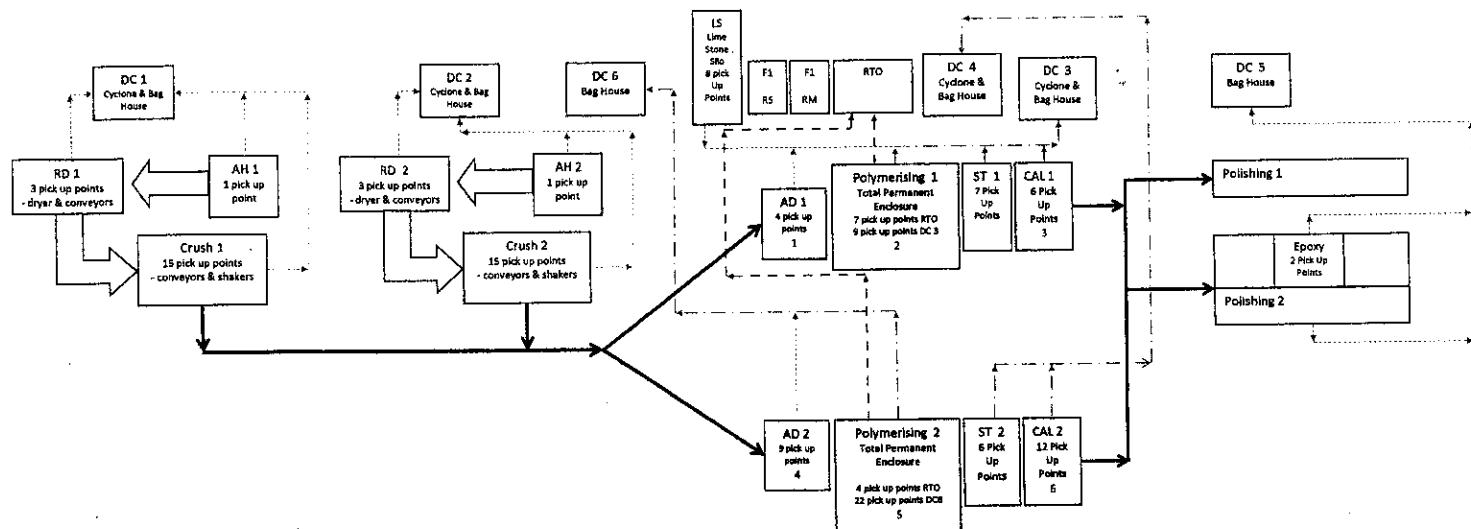
Attachment D
List of Insignificant Activities

List of Insignificant Activities:

- Fire extinguishers
- Cleaning and sweeping of streets & paved surfaces
- Emergency backup generators (4)
- Non-routine clean out of tanks and equipment for the purposes of worker entry or in preparation for maintenance or decommissioning
- Research and development, quality control
- Water treatment
- Bulk propane storage tank
- Bulk resin storage tank
- Portable totes of aggregate
- Polishing Line 1 – wet process and no ovens or dryers
- Slab cutting – wet saw
- Product packaging
- Aggregate storage bins (outdoors)

Attachment E
Process Flow

E-Stone USA Corporation
Process Layout
Revised 1-23-08



| Emission Unit | Emission Point | Emission Point Description | Equipment Identification | Equipment Description | # of Pick Up Points | Pick Up Point Location | Pick Up Point Internal to PTE | Emission | |
|---------------|----------------|-------------------------------|--------------------------|-----------------------|---------------------|---|-------------------------------|-------------------------|--|
| 01 | DC 1 | Cyclone & Bag House | AH1 | Aggregate Hopper #1 | 1 | Hopper | — | Particulate Matter (PM) | |
| | | | BD1 | Rotary Dryer #1 | 3 | Dryer & Conveyors | — | Particulate Matter (PM) | |
| | | | Crush 1 | Mill #1 | 15 | Conveyores & Shakers | — | Particulate Matter (PM) | |
| 02 | DC 2 | Cyclone & Bag House | AH2 | Aggregate Hopper #2 | 1 | Hopper | — | Particulate Matter (PM) | |
| | | | RD2 | Rotary Dryer #2 | 3 | Dryer & Conveyors | — | Particulate Matter (PM) | |
| | | | Crush 2 | Mill #2 | 15 | Conveyores & Shakers | — | Particulate Matter (PM) | |
| 03 | DC 6 | Bag House | AD2 [4] | Aggregate Dosing #1 | 8 | Aggregate Dosing | — | Particulate Matter (PM) | |
| | | | Polymerising 2 (5) | Polymerising 2 | 22 | Mixers, Upper Trolley (Loading Area) | Yes | PM & VOC/HAP | |
| 04 | DC 4 | Cyclone & Bag House | ST 2 | Slab Take Off Area | 6 | Slab Take Off Area | — | Particulate Matter (PM) | |
| 05 | DC3 | Cyclone & Bag House | CAL 2 (6) | Calibrator 2 | 12 | Calibrator | — | Particulate Matter (PM) | |
| | | | LS | Limestone Silo | 8 | Conveyors & Hopper | — | Particulate Matter (PM) | |
| | | | ST 1 | Slab Take Off Area | 7 | Slab Take Off Area | — | Particulate Matter (PM) | |
| | | | AD 1 [1] | Aggregate Dosing 1 | 4 | Aggregate Dosing | — | Particulate Matter (PM) | |
| | | | Polymerising 1 | Polymerising 1 | 9 | Upper oven, mixers, Limestone hopper, conveyors | Yes | PM & VOC/HAP | |
| 06 | RTO | Regenerative Thermal Oxidizer | CAL 1 (3) | Calibrator 1 | 6 | Calibrator | — | Particulate Matter (PM) | |
| | | | Polymerising 1 (2) | Polymerising 1 | 1 | Robot Station | Yes | PM & VOC/HAP | |
| | | | | | 2 | Limestone & Fiberglass Station | Yes | PM & VOC/HAP | |
| | | | Polymerising 2 | Polymerising 2 | 4 | Upper Trolley System (load area) | Yes | PM & VOC/HAP | |
| | | | | | 1 | Limestone Station | Yes | PM & VOC/HAP | |
| 07 | DC 5 | Bag House | | | 1 | Fiberglass Station | Yes | PM & VOC/HAP | |
| | | | | Polishing 2 | 2 | Robot Station | Yes | PM & VOC/HAP | |
| 08 | F1 | Fugitive Emission | Polishing 2 | Polishing 2 | 4 | Edge Grinding Booth | Yes | Particulate Matter (PM) | |
| | | | Epoxy | Epoxy Touch Up | 2 | Epoxy Touch Up | Yes | Epoxy Odor | |
| | | | RS | Resin Storage | 0 | | Yes | VOC/HAP | |
| | | | RM | Resin Mix Tanks | 0 | | Yes | VOC/HAP | |

Key

- Material Flow - Mill
- Process Flow
- Particulate Matter (PM) Emission
- → VOC/HAP Emission
- → PM & VOC/HAP Emission

RECEIVED - D.E.P.
FEB 05 2009
SOUTH DISTRICT

Attachment F

OM&M



**OPERATION, MAINTENANCE AND MONITORING PLAN
STARTUP, SHUTDOWN AND MALFUNCTION PLAN
FOR E-STONE'S MANUFACTURING PROCESS**

**PREPARED
JANUARY 2009**

**TITLE V PERMIT
0550049-004-AV**



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| Attachment B | Lockout Tagout Procedure |
| Attachment C | Recordkeeping Spreadsheet |
| Attachment D | Calibration Procedures |



CERTIFICATION

Based upon information and belief formed after a reasonable inquiry, I, as a responsible official of E-Stone USA Corporation certify that the information in this Operation, Maintenance and Monitoring Plan and Startup, Shutdown and Malfunction Plan is true, accurate and complies with the requirements as set forth in 40 CFR Part 63 Subpart WWWW, National Emission Standards for Hazardous Air Pollutants: Reinforced Plastics Composites Production and Subpart SS, National Emission Standards for Hazardous Air Pollutants: Closed Vent Systems, Control Devices, Recovery Devices and Routing to a fuel Gas System or a Process.

Name of Responsible Official: **James Gorsuch**

Title of Responsible Official: **Chief Financial Officer**



A handwritten signature in black ink, appearing to read "James Gorsuch CFO".

Signature

JAN 26, 2009

Date



SECTION 1.0

INTRODUCTION

1.1 Purpose and Scope

The purpose of this manual is to establish a uniform procedure for operation and maintenance of the mill area and operations with dust collection units, at E-Stone USA, regarding air emissions. The steps outlined in this plan are applicable for all E-Stone employees. This “Plan” is required by FDEP Permit 0550049-003-AC in Specific Condition B.9. Also, 40 CFR Part 63 Subpart SS, “National Emission Standards for Closed-vent Systems, Control Devices, Recovery Devices and Routing to a Fuel Gas System or a Process”, requires E-Stone to establish operating parameters of certain processes during our successful emission compliance test, and maintain records of these as part of our routing compliance demonstration.

1.2 Startup, Shutdown and Malfunction Plan

This plan is written in a manner consistent with safety and good air pollution control practices for minimizing emissions at all times. To the extent that an unexpected event arises during startup, shutdown or malfunction, E-Stone will comply by minimizing emissions during startup, shutdown or malfunction event consistent with safety and good air pollution control practices as a priority.



SECTION 2.0

MILLS 1 AND 2

2.1 Startup Procedures for the Mill

Before **ANY** production or processing of materials begins the following procedures must be taken:

1. Turn on the “Main Power” switch on the electric panel.
2. Reset the “Restore Button” on the electric panel.
3. Check to ensure that the dust collection bags are in place and secured to the ventilation outlet (Outside).
4. Check that the Ventilation arm is set correctly “Open and Close”, (outside).
5. Make sure that the “Demand/Continuous” switch on the ventilation panel is set to “Demand” to insure proper air flow through the dust tubes.
6. Press the “Start Button” to start the entire ventilation system.
7. Insure the Indicator (LED) is reading 1.0 or below (located on the ventilation electrical panel).
8. If the Indicator (LED) is reading above 1.0 switch the “Demand/Continuous” switch to “Continuous” until the

LED reads below 1.0. This usually takes 2-3 minutes.

Return the switch back to the demand position.

9. Once the ventilation system is started, visibly check for negative pressure by watching the operation of the vapor locks and suction on the bags.
10. Once all of the above steps are complete, the Milling machine is started and the “grinding” process begins.
11. During the process view the outlet of the dust collector stack to assure there are no visible emission of dust. If dust is noted, check the bags in the dust collector for leaks.

2.2 Operation and Maintenance

The following maintenance procedures are to be performed and documented weekly to insure proper function of the entire ventilation systems for both mills. These documents are maintained and filed in the Maintenance office for future reference:

1. Inspect and replace (if needed) all drive belts
2. Inspect and replace (if needed) all drive bearings and main shaft.
3. Insure that the 4 vapor lock valves are properly opening and closing to insure that there is no “blow-by”.
4. Inspect and replace (if needed) any bearings on the vapor locks.

5. Check for proper air supply to the vacuum system (gauged).
6. Inspect all duct work for air leaks and repair as needed.
7. Follow the dust collector manufacturer's schedule for daily, weekly, monthly and annual maintenance. A copy of this RTO manual is adopted by reference as part of this OM&M Plan.

2.3 Monitoring and Malfunction

1. Once the operation begins, the pressure gauge (LED readout on panel) is monitored periodically by the Lead Operators to ensure that it maintains a read out of 1.0 or less.
2. If in the event that the LED readout is greater than 1.0 during Operation, the “Demand/Continuous” switch should be switched over to “Continuous” until the proper LED readout level is achieved and then switched back to the “Demand” position.
3. The dust bags underneath the system outside are checked hourly by the lead operator for any visible emissions and changed when the bags are $\frac{3}{4}$ full to avoid any emissions of material and to insure proper ventilation during the run.
4. In order to change the dust bags during operation, the “grinding” process must be shut down, as well as the ventilation system.

5. Once all operations are properly shut down, the bags are changed and the start up procedures is followed beginning with step #6 in the "Start Up" procedures

2.3 Shutdown

To shutdown the ventilation system after all grinding operations have stopped, activate the "Stop" switch on the panel .This stops all ventilation and shuts down the entire system. The large dust collection sacks are replaced with empty ones for a smooth start up the following shift or day. The full sacks are closed and staged for pick up by our waste management company.

If visible emissions were noted from the exhaust stack, inspect the dust collector while the system is down and replace the dust tubes as necessary.

2.4 Recordkeeping Forms

A form is to be filled out as part of E-Stone's recordkeeping procedures. A copy of this form is included in Attachment A.



SECTION 3.0

REGENERATIVE THERMAL OXIDIZER and DUST COLLECTOR 3

3.1 Startup Procedure for the RTO

Before **ANY** production or processing of materials begins the following procedures must be taken:

1. Verify power at the main control panel located on the RTO is “ON”.
2. To prepare the RTO for start-up at the PLC (which is located behind the oven by the door closest to the RTO) the following steps must be done:
 - a. From “Alarms” screen, upon start up you need to acknowledge and reset any alarms that are present. Press “Alarm Silence” and then “Alarm Reset” and hold for 10 seconds. If everything is correct all indicators will be green. Green=OK Blue=Off Red=Failure
 - b. Screens - Select “Valve Position” to verify that Line #1 valve is open. To open, touch the “white square” and

- drag upward to 100%. A red line will indicate “as open” as well as “Valve #1 POS Feedback” will read “100%”.
- c. System Start Screen - turn chart recorder on by pressing blue chart recorder icon. Set process to online; now startup procedures can begin from this screen.
 - 1) Set system to on (Green) burner fan and process fan will activate (Green)
 - 2) Enable burner (Green). If all is ok, remaining icons will activate automatically.
 - d. Select Overview - From this screen you can monitor the poppet valve cycling and that the burner is on.

(Note: At 1575 °F the ISO (damper isolation) valve will open and the RTO is ready to go. Turn on the dust collection system (DC3) and start production.

3.1.2 DC3 Startup Procedure

Before ANY production or processing of materials begins the following procedures must be taken:

1. First verify that the main power is on (this can be found at the outside wall where the DC3 is located).
2. After main power is verified, return to the oven control panel and from the main screen select the “Utility” icon.
3. Select “Suction On”. This will automatically start all of the components. The operator is then to verify and check for alarms. If there are no alarms production may proceed.

3.2 RTO Maintenance

1. The RTO is to be turned off during cleaning and maintenance.
2. During color changes that require intense cleaning (blowing down inside the enclosure). The operator MUST close the line valve (enclosure exhaust damper) to prevent dust from being suctioned into RTO. The dust collector must be kept operating during enclosure or equipment cleaning.
3. Follow the RTO manufacturer's schedule for daily, weekly, monthly and annual maintenance. A copy of this RTO manual is adopted by reference as part of this OM&M Plan.
4. The structured ceramic media will require period cleaning when the airflow in the RTO starts to drop. Follow the RTO manufacturer's procedure for this cleaning process.

3.2.1 DC3 Maintenance

Follow the Maintenance supervisor's schedule for daily, weekly, monthly and annual maintenance. A copy can be obtained from the Maintenance supervisor. It is located in the Maintenance office inside the plant.

3.3 RTO Monitoring

During polymerization the operator must monitor the following:

- hourly verification of alarms screen,

- overview screen for average temp,
- poppet cycling,
- ISO Process valve.
- Magnehelic readings as instructed by OMM plan.

3.3.1 DC3 Monitoring

During production the operator must monitor the following:

- Every 30 minutes the operator must verify visually that the dust bags are secured properly and changed as needed
- Hourly verify visually that the airlocks are cycling properly
- Daily verifications for visible emissions at all collection points - this includes airlocks and dust bags
- Daily verification of the magnehelic gauge

3.4 RTO Shutdown

To shutdown the RTO at the end of production,

1. Go to the “System Start” screen and press the “Retained Heat Shutdowns” and then select “Chart Recorder Off” and “Process Off-Line.”
2. Turn off main power supply only if performing maintenance on the machine and follow “Lockout/Tagout Procedures” (see Attachment B).

3.4.1 DC3 Shutdown

At the Oven Control Panel, access the utility screen and select “Suction Off”. This will automatically shut down all components.

3.5 RTO and DC3 Malfunction

If the RTO or DC3 ventilation systems malfunctions during startup, shutdown or normal operation E-Stone will immediately cease all polymerization and processing of organic HAP containing materials until the RTO and ventilation system are back in operation and functioning properly.

The operator will correct malfunctions as soon as practicable after the occurrence in order to minimize excess emissions of hazardous air pollutants and restore malfunctioning process and air pollution control equipment to its normal manner of operation.

When actions taken to address problems during a startup, shutdown or malfunction are consistent with the procedures specified in the plan, E-Stone will keep records for that event which demonstrate that the procedures specified in this plan were followed.

The operator will keep records of the malfunction events including records of the occurrence and duration of each startup, shutdown and malfunction of operation and each malfunction of the RTO and/or dust collection systems. E-Stone has a form to record all of the required information for such an occurrence.

The operator will confirm that actions taken during the relevant reporting period during periods of startup, shutdown and malfunction were consistent

with this plan in the semiannual startup, shutdown and malfunction report required in 40 CFR 63.10(d)(5).

If an action taken by the operator during a startup, shutdown or malfunction (including an action taken to correct a malfunction) is not consistent with the procedures specified in this plan, and the facility exceeds any applicable emission limitation in the relevant emission standard, then the operator must record the actions taken for that event and must report such actions within 2 working days after commencing actions inconsistent with the plan (Correction Action Record Sheet is attached), followed by a letter within 7 working days after the end of the event, in accordance with 40 CFR 63.10(d)(5).

Note: If a malfunction occurs during operation and the RTO is shut down for repairs, upon verification of completion of work, the operator can restart the RTO as per the Start Up procedure. If the RTO was down for less than 8 hours, when the temperature is it's set point (1575°F) the operator can select the "Purge Bypass" by selecting "Screens" at the panel view screen and then select "Time Adjust" and finally select "Purge Bypass".

3.6 RTO and DC3 Recordkeeping Forms

Copy of this form is included in Attachment A.



SECTION 4.0

PARAMETRIC MONITORING REQUIREMENTS

4.1 Purpose

Parametric monitoring is required by Subpart SS as referenced in E-Stone's Title V air permit. These are parameters that were established during the December 2008 compliance test that demonstrated compliance with the emission limiting standards of subpart WWW that regulates E-Stones polymerization process.

During this compliance test, these parameters were monitored and reported to the Florida Department of Environmental Protection (FDEP) and are used as surrogate parameters to assure continued compliance. E-Stone must operate the referenced processes and equipment within these parameters, record the required data at the frequency stated in this plan and when necessary correct systems when they deviate from these parameters.

4.2 Parametric Monitoring Limits

The parametric monitoring requirements are summarized below in Table 4-1. They have been established as part of the continuous compliance program for the manufacturing process and required by E-Stones Title V permit.

Table 4-1: Parametric Monitoring Limits

| E.U. No. | Control Device | Monitoring Device | Minimum Parameter Limit |
|----------|----------------|--------------------------------|--|
| 003 | DC3 | Magnehelic outlet stack | +0.4 inches water gauge or 2400 ft/min |
| 003 | PTE | Magnehelic 1 | -0.005 inches water gauge |
| 003 | PTE | Magnehelic 2 | -0.02 inches water gauge |
| 003 | PTE | Slab production | Maximum 16 slabs/hr |
| 005 | RTO | Inlet magnehelic | 0.175 inches water gauge or 1800 ft/min |
| 005 | RTO | Outlet magnehelic | 0.25 inches water gauge or 2000 ft/min |
| 005 | RTO | Combustion chamber temperature | 1577 deg F 15-minute block average temperature |
| 005 | RTO | Inlet vacuum setting | -0.6 inches water gauge |

Recordkeeping forms for these parameters and the PTE are included in Attachment A as previously stated.

4.3 Raw Material Usage Recordkeeping

The air permit requires E-Stone to keep monthly records of chemical usage and calculations of emissions. An Excel spreadsheet has been prepared for this purpose and is included in Attachment C for reference purpose only.

Operators complete the daily log sheets and send them to the Chief Document Coordinator (Polly Mandrell) for entering into the spreadsheet. The following data must be maintained for a period of five (5) years in a manner suitable for inspection by a regulatory inspector:

Mills 1 and 2

- The amount of aggregate throughput (processed)
- Rotary dryer operating rates
- Fuel usage rate
- Hours of operation

Polymerization Line 1

- The amount of all raw materials used (resin, aggregate, catalyst, ect)
- RTO fuel usage
- Production rate slabs/hr

Polishing Line No. 2 Epoxy Station

- Type and amount of fuel burned

4.4 Weekly Calibration Procedures

The parametric monitoring is dependent on accurate measurement of the device doing the measuring. E-Stone has a routine calibration program and procedure for each of these categories of measurement devices. A copy of this procedure is included in Attachment D.

ATTACHMENT A

MILLS 1 AND 2 /RTO/DC3/PTE RECORDKEEPING

FORMS



E-Stone USA

Shift Supervisors Daily Production Report

Shift: _____

Date: _____

Supervisor: _____

Mill #1

of Pounds Ground/Color

of Pounds Blended

Hours of Operation

Fuel Meter Reading

Start

End

of Pounds Regrinding

Natural Gas

1

Comments:

Mill #2

of Pounds Ground/Color

of Pounds Blended

Hours of Operation

Fuel Meter Reading

Start

End

of Pounds Regrinding

Natural Gas

1

Comments:

Oven 1

of Slabs Produced/Color

RTO Fuel Meter Reading

Start

End

Natural Gas

1

Magnehelic Readings

DC3 _____

RTO

Inlet

Differential Pressure Gauge Reading

1

Time Read _____

Time Read _____

Time Read _____

RTO

Outlet

2

Time Read _____

Time Read _____

Comments:

Polish Line #2

Total Slabs Polished _____

Fuel Meter Readings - Natural Gas

Oven 1: Start _____

End _____

Dryer 1: Start _____

End _____

Oven 2: Start _____

End _____

Dryer 2: Start _____

End _____

Oven 3: Start _____

End _____

Dryer 3: Start _____

End _____

Dryer 4: Start _____

End _____

ATTACHMENT B

LOCKOUT TAGOUT PROCEDURE



E-Stone USA

Lockout/Tagout Procedures

PURPOSE

This procedure establishes the minimum requirements for the lockout or tagout of energy isolating devices. Lockout is the preferred method of isolating fixtures, equipment or machinery from energy sources. It shall be used to ensure that the fixture, equipment, or machinery is isolated from all potentially hazardous energy and locked out or tagged out before employees perform any servicing or maintenance activities where the unexpected energization, start-up or release of stored energy could cause bodily injury and/or to prevent damage to fixtures, equipment, machinery or the environment. (Ref. 29CFR 1910.147)

DEFINITIONS

Affected Employee - An employee who works in an area where servicing or maintenance operations are performed. An affected employee does not perform servicing or maintenance on machines or equipment and, consequently, is not responsible for implementing lockout/tagout procedures. However, an authorized employee and an affected employee may be the same person when the affected employee's duties also involve performing maintenance or service. An affected employee becomes an authorized employee whenever he or she performs servicing or maintenance functions.

Authorized Employee - An employee who performs servicing or maintenance on equipment and machinery. This employee implements lockout/tagout procedures to guarantee his or her own protection.

Capability of being locked out - an energy-isolating device is considered capable of being locked out if it meets one of the following requirements:

1. It is designed with a hasp to which a lock can attached.
2. It is designed with any other integral part through which a lock can be affixed.
3. It has a locking mechanism built into it.
4. It can be locked without dismantling, rebuilding, or replacing the energy-isolating device or permanently altering its energy control capability.

Energized - Equipment and machinery is energized when they are connected to an energy source or contain residual or stored energy.

Energy Control Procedure - A written document (See Attachment 1.) that contains the steps an authorized employee must follow to safely control hazardous energy during servicing or maintenance of equipment or machinery.

Energy Control Program - A program intended to prevent the unexpected energizing or the release of stored energy in equipment or machinery. The program consists of:

1. Energy Control Procedures.
2. An employee training program.
3. A Lockout/Tagout work station
4. Periodic inspections of the employees using the procedures and a procedure review.

Energy Isolating Device - A mechanical device that physically prevents the transmission or release of energy.

Energy Source - Any source of electrical, mechanical, hydraulic, pneumatic, chemical, steam, thermal or other energy.

Lockout - Placing a lock on an energy-isolating device according to an established procedure, that ensures that the fixture, equipment or machinery cannot be energized until the lock is removed by the person who placed it there.

Lockout Device - A device that utilizes a positive means such as a lock to hold an energy-isolating device in a safe position and prevent the energizing of fixtures, equipment or machinery.

Tagout - The placement of a tagout device on an energy-isolating device, according to an established procedure, clearly marked by means of a tag that states who has the fixture, equipment, or machinery shut down and that the equipment or machinery must not be operated until the tagout device is removed by the employee who places it there.

Tagout Device - Any prominent warning device, such as a tag and a means of attachment that can be securely fastened to an energy-isolating device according to established procedure. The tag indicates that the equipment or machinery to which it is attached must not be operated until the tagout device is removed according to the energy control procedure. The attachment method must be substantial and not easily removed.

Zero Energy State - All sources of energy have been controlled and/or dissipated.

RESPONSIBILITIES

Plant Manager:

Overall responsibility for this procedure.

Maintenance Manager:

Responsible to ensure that all maintenance employees are aware of this procedure and are trained in its use and application. Names and Job Titles of employees who are authorized to lockout or tagout shall be documented and copies placed in the Lockout/Tagout Documentation File. Each new or transferred employee and other employees whose work operations are or may be in the area shall be trained in the purpose and use of this lockout or tagout procedure. The Maintenance Manager shall verify the accuracy of existing written Energy Control (shutdown/startup) Procedures, write them if they are non-existent, obtain adequate supplies, maintain the inventory and document the issuance of locks, tags, and locking devices. All training is to be documented and signed by employees attending training. The original signed copy will be kept in the Lockout/Tagout Training Documentation Folder, which is located in the locked Personnel File, and a copy of the documentation is to be placed in each trained employee. An up-to-date schedule of training dates and employees attending each training session shall also be kept in the Lockout/Tagout Training Documentation Folder. It is also the responsibility of the Maintenance Manager to ensure that contractors are aware of E-Stone's Lockout/Tagout procedures.

Safety Manager:

The Senior Accountant shall be responsible for auditing this procedure, that procedures are consistent throughout the plant, that Energy Control Procedure is posted, that the Lockout/Tagout checklist is used as required and included in the documentation file, that training occurs and is scheduled for employees in a timely manner, and that the Lockout/Tagout Procedures are documented properly.

Maintenance Employees:

Responsible to know and to understand the important safety significance of this procedure and its proper application. If violations of this procedure are observed notify your supervisor and the Plant Manager immediately.

HAZARD ANALYSIS

- A written Hazard Analysis shall be performed by Scheduled Maintenance employees for each piece of equipment and machinery that is used, serviced or maintained. Be sure to include stored equipment and machinery. This begins with an inventory to be recorded on the ENERGY HAZARD ASSESSMENT INVENTORY FORM, attachment 2 of this procedure. Send copy of this form to the Safety Manager.
- As the inventory is completed for each building, a more detailed evaluation of each piece of equipment or machinery shall be completed. Document all energy sources (direct and hidden), the hazards posed, the magnitude or measurable degree of danger, any special or unusual conditions, and the proper isolation methods and devices. Record these items on the DETAILED ENERGY HAZARD ASSESSMENT FORM, attachment 3 of this procedure. (Attachments 2 & 3 may be filled out at the same time) Send a copy of this form to the Safety Manager.

- Attachments 2 & 3, when used together, serve as the building blocks for developing written Energy Control (shutdown and startup) Procedures. As these Energy Control Procedures are completed send them to the Safety Manager for review.

PROCEDURE

Basic Rules for Using Lockout or Tagout System Procedures

- ALL energy sources to fixtures, equipment and/or machinery shall be locked out or tagged out to protect against accidental or inadvertent operation when such operation could cause injury to personnel.

NOTE: Isolating a piece of equipment from its source may not eliminate all potential hazards. Stored energy may be present within the equipment or machinery.

- Do not attempt to operate any switch, valve or other energy isolation device when it is locked or tagged out.
- Never remove a lock or tag for another employee. Only the employee placing the lock or tag may remove it. If there is a need to remove another employee's lock or tag in an emergency, ONLY the maintenance manager may do so AFTER MAKING EVERY EFFORT TO CONTACT THE OWNER OF THE LOCK OR TAG.

Sequence to lockout or tagout:

1. The Maintenance Supervisor shall make a survey to locate and identify all isolating devices to be certain which switch(s), valve(s) or other energy isolating devices apply to the equipment to be locked or tagged out. More than one energy source (electrical, mechanical or others) may be involved. (See LOCKOUT/TAGOUT FLOWCHART).
2. Verify the written Energy Control (shutdown/startup) Procedure attached to the equipment or machinery, make necessary changes, supply the written procedure in the absence thereof, and send a copy of the procedure or changes to an existing procedure to the Safety Manager for review.
3. The maintenance supervisor or shop leadman shall notify all affected employees and customers that a lockout or tagout system is going to be utilized and the reason therefore. The authorized employee shall know the type and magnitude of energy that the machine or equipment utilizes and shall understand the hazards thereof.

4. If the machine or equipment is operating, shut it down by the written Energy Control (shutdown) Procedure attached to the equipment or machine (depress stop button, open toggle switch, etc.).
5. Operate the switch, valve or other energy isolating device(s) to ensure that the equipment is isolated from its energy source(s). Stored energy (such as that in spring, elevated machine members, rotating flywheels, hydraulic systems and air, gas, steam and water pressure, etc.) MUST be dissipated or restrained by methods such as repositioning, double blocking and bleeding down, etc.
6. Lockout and/or tagout the energy isolating devices with assigned individual lock(s) or tag(s). Tags shall indicate that the energy-isolated device(s) shall not be operated until after the removal of the tag.
7. After ensuring that no personnel are exposed, and as a check on having disconnected the energy sources, operate the push button or other normal operating controls to make certain the equipment will not operate.

CAUTION: Return operating control(s) to "neutral" or "off" position after the test.
8. The equipment is now locked out or tagged out.

Restoring Machines or Equipment to Normal Production Operations.

1. After servicing and/or maintenance is completed and the fixture, equipment or machinery is ready for normal operation, check the area around the fixture, equipment or machinery to ensure that no one is exposed.
2. After all tools have been removed from the fixture, equipment, or machinery, guards have been reinstalled and employees are in the clear, remove all lockout or tagout devices. Notify all affected persons that the Lockout or Tagout has been removed. Operate the energy isolating devices to restore energy to the fixture, equipment or machinery following the written Energy Control (startup) Procedure.

Procedure Involving More Than One Person

- In the preceding steps, if more than one individual is required to work on the equipment or machinery, each shall place his/her own personal lockout device and/or tagout device on the energy isolating device(s). When an energy-isolating

device cannot accept multiple locks and tags, a multiple lockout or tagout device (box or hasp) may be used.

- If lockout is used, a single lock may be used to lockout the machine or equipment with the key being placed in a lockout box or cabinet which allows the use of multiple locks to secure it. Each employee will then use his/her own lock to secure the box or cabinet. As each person no longer needs to maintain his or her lockout protection, that person will remove his/her lock from the box or cabinet.
- When work must continue over a shift change the supervisor or lead worker must ensure that all employees are aware of which locks are to be replaced or left in place. All employees in the oncoming shift must be informed of the Lockout/Tagout conditions.

Additional Requirements

- Plant Manager, Maintenance Managers and Supervisors should annually verify that all employees are in compliance with the requirements of this procedure. The Periodic Lockout/Tagout Inspection Form (Attachment 6) shall be used and a copy of the completed form sent to the Safety Manager.
- Initial training must be provided for all authorized and affected employees, repeated annually and documented. Additional retraining for all authorized and affected employees must be provided whenever there is a change in equipment, machinery, procedures or whenever there is evidence that this procedure is being violated.
- Locks provided by E-Stone are the ONLY authorized locks to be used for equipment or machine lockout. Each lock should be keyed separately. One key issued to the authorized employee possessing the lock and the other key kept by the supervisor for emergency situations only.
- Each lock should be identified as to its owner. In lieu of identification on the lock, an authorized employee's personal tag can be applied in addition to his/her lock when locking out the equipment or machinery so that the lock's owner can be readily identified.
- The tags, padlocks and lockout devices used for locking out machinery and equipment should ONLY be used for lockout and not for any other activity.
- All equipment or machinery should be provided with appropriate energy isolating devices. Each such energy isolating device should be clearly identified by a label. ONLY where such devices are not now existent, may TAGOUT be used.

1. Whenever the equipment or machinery is modified or rebuilt, the energy control device must be altered to allow the incorporation of a lock for lockout purposes.
 2. When new or replacement equipment or machinery is ordered the specifications shall include the capability of locking out the energy source(s). NOTE: After October 31, 1989, whenever renovation, major replacement, repair, or modification of machines or equipment is performed, and whenever new machines or equipment are installed, energy isolating devices for such machines or equipment shall be designed to accept a lockout device. (VOSH: 1910.147, (c), 2,iii)
- All equipment or machinery that is required to be locked or tagged out shall have a written Energy Control (shutdown/startup) Procedure attached to or near the main power switch for that equipment or machinery. This procedure is to identify all the energy sources which may be acting on this equipment and detail how each energy source is to be locked or tagged out. A copy of these procedures is to be sent to the Safety Manager for review.
 - The removal of a lock or tag by anyone other than the assigned employee who placed the lock or tag on the equipment or machinery is a very serious event and shall be documented with a copy of the documentation being sent to the Safety Manager. The supervisor should make every effort to locate the responsible employee to be sure that he/she is not present on site, make a thorough examination of all machinery or equipment protected by the lockout or tagout to ensure that personnel, tools, and equipment are clear, and notify the Manager before removing the lock or tag. Continue to make all reasonable efforts to contact the employee to inform him/her that his/her lockout or tagout device has been removed and to ensure that the employee has this knowledge before he/she resumes work at the site.
 - A tagout device, including the means of attachment, shall be substantial enough to prevent inadvertent or accidental removal. Tagout device attachment shall meet the following:
 - 1.1.4.1. Be able to be affixed by hand.
 - 1.1.4.2. Be non-reusable.
 - 1.1.4.3. Be self locking.
 - 1.1.4.4. Requires a minimum unlocking strength of 50 pounds.
 - Cord and plug equipment is exempt from the provisions of this procedure provided that the following two conditions are met.
 - Power to the equipment or machine must be completely removed by unplugging.

- The authorized employee must have the plug under his or her exclusive control (i.e. in sight at all times). If not, the plug must be locked out.
- An audit shall be performed annually by the Safety Manager to ensure compliance with this written procedure.
- Violations of this procedure shall be considered a serious conduct violation and may lead to dismissal of the employee.
- This procedure shall be reviewed annually.

TRAINING

- All personnel authorized to do maintenance and affected employees (those using or capable of starting a machine or any equipment) shall be trained annually on this procedure.
- All new employees shall be properly trained on this procedure before working in an area where lockout or tagout is in use.
- Supervisors must document that employee training has been accomplished. Copies of this documentation are to be sent to the Safety Manager.
- Documentation must include the names of all employees participating, the date of the training, a copy of the curriculum, and the name of the trainer.
- To ensure that the necessary information has been learned a written test shall be administered by the trainer and the results recorded. Employees who do not achieve at least a 75% score on the written test must be retrained.
- Written test results are to be retained by the Safety Manager.
- Training should include the following:
 1. Ensure that all employees know the details of this procedure and that they know what to do and what not to do when they encounter a lock or a tag on a switch or a device they wish to operate. See Quiz, Attachment 4 & 5.
 2. Employees must be aware that a tag is not a physical restraint. They must be aware of the false sense of security that tagout systems can present.
- Retraining should take place:

1. When an employee is re-assigned to a different area or machine.
2. When there is a change in the tag and lockout procedure.
3. When there is a change in equipment or machinery.
4. When a periodic inspection or audit reveals inadequacies in the employee's knowledge or use of Energy Control Procedures or this Energy Control Program.

ENERGY CONTROL PROCEDURE

The purpose of this procedure is to prevent injuries to employees from the unexpected energizing, start-up, or release of stored energy from machines, equipment, or processes when such employees are engaged in activities where they are at risk. Only Authorized personnel having an intimate knowledge of the work to be performed shall perform this ENERGY CONTROL PROCEDURE.

- 1) An Authorized person is considered a qualified person to whom the authority and responsibility to perform a specific lockout and/or tagout assignment has been given by E-Stone. An example of an Authorized person may Maintenance Manager. This person would be considered qualified if they can demonstrate by experience or training the ability to recognize potentially hazardous energy and its potential impact on workplace conditions, and has the knowledge to implement adequate methods and means for the control and isolation of such energy.
- 2) All lockouts and tagouts shall be recorded in a log book maintained in the Maintenance Manager's area. The log book shall be used to identify lockouts in sequential order, name and location of equipment and/or system affected, authorized persons involved, dates, times, and supplies. Only approved locks, hasps, and tags shall be used.
- 3) The first step of any lockout is to have a qualified person determine what needs to be locked out. The latest drawings, sketches, and/or notes should be analyzed to identify all energy sources to the equipment. Drawings typically reviewed are electrical single-lines and mechanical piping and instrument diagrams (P&IDs). Particular attention should be given to temporary feeds, back-feeds and alternate feeds including all sources of control voltage.
- 4) After identifying all the energy sources and isolation points, the equipment shall be shutdown and the disconnecting means (breakers, switches, valves, etc) shall be opened or positioned in the "OFF" position for all of the energy sources using the Personal Protective Equipment (PPE) designated to accomplish this safely.
- 5) Verification that all potential energy sources are eliminated must be made before applying the Lock and Tag. These energy sources may be electrical, mechanical, or both. Mechanics must follow procedures unique to each equipment or system that are designed to eliminate both of these energy sources.
 - i) Electrical - A visual inspection by a Qualified electrician must be made to verify the circuit is open. Where possible, disconnect switches shall be inspected to assure that all blades are in the full open position. Where visual verification is not possible, other means of providing a visible break may be necessary, for example a Qualified electrician will test for the absence of voltage and remove the fuses or lift the wires. An example may be a foreign disconnect switch provided by a vendor and no prints or manuals are available.

- (b) Mechanical - Release any residual energy by opening drains, vents, and bleeds employed with double-block valving arrangements inside the lockout boundary. Release any chemical energy by draining any remaining material in pipes and equipment into controlled containers while proper personnel protective equipment (PPE) is utilized. Latch in place any travel stops necessary to prevent the release of any potential or stored energy. Engaging travel stops may be required to protect against any sudden movement of an elevator.
- 6) Try the electrical circuit and/or mechanical system to verify that it is isolated, de-energized, and free from stored energies. Once the verification is made, then the Authorized person shall install his/her Lock and Tag:
- The Tag must have the person's name, shop, radio # (if the person is assigned radio) and reason for the tag. The time and date must be on the Tag as well.
- (a) If a change of shift should occur while the equipment and/or system is locked and tagged and work must continue, the next shift Authorized individual shall put their lock on and former shift shall remove theirs. In the case where work is continued the next day or at some future time, then the equipment and/or system shall remain locked and tagged for the duration.
- 7) · **NO ONE** shall remove another person's lock.
- 8) PROCEDURE INVOLVING MORE THAN ONE PERSON In the preceding steps, if more than one individual is required to lockout or tagout equipment, each shall place his/her own personal lockout/tagout device on the energy isolating device(s). When an energy isolating device cannot accept multiple locks or tags, a multiple lockout or tagout device (hasp) may be used. If lockout is used, a single lock may be used to lockout the machine or equipment with the key being placed in a lockout box or cabinet which allows the use of multiple locks to secure it. Each employee will then use his/her own lock to secure the box or cabinet. As each person no longer needs to maintain his or her lockout protection, that person will remove his/her lock from the box or cabinet.
- 9) TEMPORARY REMOVAL OF LOCKOUT/TAGOUT DEVICES in situations where lockout/tagout devices must be temporarily removed from the energy isolating device and the machine or equipment energized to test or position the machine, equipment or component thereof, the following sequence of actions will be followed:
- i) Remove non-essential items and ensure that machine or equipment components are operationally intact.

- ii) Notify affected employees that lockout/tagout devices have been removed and ensure that all employees have been safely positioned or removed from the area.
 - iii) Have employees who applied the lockout/tagout devices remove the lockout/tagout devices.
 - iv) Energize and proceed with testing or positioning.
 - v) Deenergize all systems and reapply energy control measures in accordance with section 5.2 of these procedures.
- 10) MAINTENANCE REQUIRING UNDISRUPTED ENERGY SUPPLY where maintenance, repairing, cleaning, servicing, adjusting, or setting up operations cannot be accomplished with the prime mover or energy source disconnected, such operations may only be performed under the following conditions:
- i) The operating station (e.g. external control panel) where the machine may be activated must at all times be under the control of a qualified operator.
 - ii) All participants must be in clear view of the operator or in positive communication with each other.
 - iii) All participants must be beyond the reach of machine elements which may move rapidly and present a hazard.
 - iv) Where machine configuration or size requires that the operator leave the control station to install tools, and where there are machine elements which may move rapidly, if activated, such elements must be separately locked out.
 - v) During repair procedures where mechanical components are being adjusted or replaced, the machine shall be de-energized or disconnected from its power source.



E-Stone USA

**LOCKOUT/TAGOUT
ENERGY CONTROL PROCEDURE CHECKLIST**

Machine/Area:

| | | |
|-------|-------|----------------|
| Date: | Time: | Technician(s): |
|-------|-------|----------------|

- Notify affected employees that a lockout or tagout system is going to be utilized and the reason therefore.
- If the machine or equipment is operating, shut it down by the normal stopping procedure (depress stop button, open toggle switch, etc.)
- Operate the switch, valve, or other energy isolating device(s) so that the equipment is isolated from its energy source(s). Stored energy (such as that in springs, elevated machine members, rotating flywheels, hydraulic systems, and air, gas, steam, or water pressure, etc.) must be dissipated or restrained by methods such as repositioning, blocking, bleeding down, etc.
- Lockout/Tagout the energy isolating devices with assigned individual lock(s) or tag(s).
- After ensuring that no personnel are exposed, and as a check on having disconnected the energy sources, operate the push button or other normal operating controls to make certain the equipment will not operate. CAUTION: Return operating control(s) to neutral or off position after the test.
- The equipment is now locked out or tagged out.

RESTORING MACHINES OR EQUIPMENT TO NORMAL OPERATIONS

- After the servicing and/or maintenance is complete and equipment is ready for normal production operations, check the area around the machines or equipment to ensure that no one is exposed.
- After all tools have been removed from the machine or equipment, guards have been reinstalled and employees are in the clear, remove all lockout or tagout devices. Operate the energy isolating devices to restore energy to the machine or equipment.

SIGNATURE _____ **DATE** _____

ATTACHMENT C

RECORDKEEPING SPREADSHEET

E-Stone USA Corporation

Facility-wide Monthly VOC & HAP Emissions
Controlled by 7000 scfm Crawford RTO

EXAMPLE ONLY

| Material | E-Stone Item Number | Material Usage (lbs) | VOC Content (%) | Emission Factor ¹ (%) | VOC Emissions (Tons) | VOS Content (%) | VOS Emissions (Tons) | Styrene Content (%) | Styrene Emissions (Tons) | Dimethyl Phthalate Content (%) | Dimethyl Phthalate Emissions (Tons) | Methanol Content (%) | Methanol Emissions (Tons) | MIBK Content (%) | MIBK Emissions (Tons) | Total HAPs (Tons) |
|--------------------------------------|---------------------|----------------------|-----------------|----------------------------------|----------------------|-----------------|----------------------|---------------------|--------------------------|--------------------------------|-------------------------------------|----------------------|---------------------------|------------------|-----------------------|-------------------|
| Resin & Styrene ³ | RM0002 | | 36.198% | 1.77% | 0.0000 | | | 36.198% | 0.0000 | | | | | | | |
| Epoxy Resin 4030 Transparent | CN0043 | | 0.00% | | | | | | | | | | | | | |
| Epoxy Resin 4030 White | CN0045 | | 0.00% | | | | | | | | | | | | | |
| Epoxy Hardner MR50L | CN0045 | | 0.00% | | | | | | | | | | | | | |
| Styrene - (add to resin) | CN0002 | | 100.00% | | 0.0000 | | | 100.00% | 0.0000 | | | | | | | |
| Tinuvin | RM0005 | | 100.00% | | 0.0000 | | | | | 40.00% | 0.0000 | | | | | |
| Initiator Norox MEKP-SH ² | RM0012 | | 100.00% | 0.04% | 0.0000 | | | | | | | 0.20% | 0.0000 | | | |
| Surfactant (CoatOsil 7500) | RM0001 | | 1.00% | | 0.0000 | | | | | | | | | | | |
| Accelerator (Westdry Cobalt 6%) | RM0003 | | 100.00% | | 0.0000 | | | | | | | | | | | |
| Accelerator (NL51 P) | RM0017 | | 100.00% | | 0.0000 | | | | | | | | | | | |
| Accelerator (12% Cobalt Hex-Cem) | RM0025 | | 100.00% | | 0.0000 | | | | | | | | | | | |
| Silane | RM0005 | | 100.00% | | 0.0000 | | | | | | | | | | | |
| Tronox CR-826 | RM0020 | | 2.00% | | 0.0000 | | | | | | | | | | | |
| Alcohol (IPA) (gallons X 8.8) | CN0057 | | 100.00% | | 0.0000 | | | | | | | | | | | |
| Acetone (gallons X 8.8) | CN000100 | | 60.00% | | 0.0000 | | | | | | | | | | | |
| Acetone | CN0001 | | | | | 100.00% | 0.00 | | | | | | | | | |
| Monthly Total | | 0 | | | 0.0000 | | | 0.0000 | 0.0000 | | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | |
| Year-To-Date Total | | 0 | | | 0.0000 | | | 0.0000 | 0.0000 | | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | |
| 12 Month Rolling Total | | 0 | | | 0.0000 | | | 0.0000 | 0.0000 | | 0.0000 | | 0.0000 | 0.0000 | 0.0000 | |

Notes:

1. Per CFR 40 Part 63 Subpart WWWWW, 65.5799(b)(1) for non-atomized mechanical resin application, the calculated emission factor is 4.03% (calculation = $(10.157 \times .36198) \times 2000 = 80.66 \text{ lbs styrene / ton resin} \times .0403 = 4.03\%$)

Actual measured emission factor is 1.768% based on a measured emission rate of 35.36 lbs organic HAP/ton resin used. Data from December 2008 stack test.

2. Emission factor for Initiator VOC & DMP is 0.04%, see engineering calculations provided by AOC, resin supplier.

3. 22,800 pounds of styrene will be added to the general purpose resin. The styrene content of the resin was raised from 35.9% to 36.198% to account for the addition of the used styrene as a diluent.

According to the permit, page 13 of 19, "the limits in the table are not enforceable limits. The enforceable HAP limits are defined in 40 CFR 63 Subpart WWWWW. Table 3 in Subpart WWWWW for open molding - non-CRHS, mechanical resin application the HAP emissions limit is 88 lbs/ton

*emission calculation for chemicals used in the enclosure - 44.63% are uncontrolled (vented to baghouse end mold cooling vent) and 55.37% are vented to RTO with 99.04% destruction efficiency based on the stack test conducted December 2008

| Product Usage: (lbs) | Year-to-Date (lbs) | 12 Month Rolling Total (lbs) |
|----------------------------------|-----------------------|---------------------------------|
| Resin & Styrene | 0 | 0 |
| Epoxy Resin 4030 Transparent | 0 | 0 |
| Epoxy Resin 4030 White | 0 | 0 |
| Epoxy Hardner MR50L | 0 | 0 |
| Styrene - (added to resin) | 0 | 0 |
| Tinuvin | 0 | 0 |
| Initiator Norox MEKP-SH | 0 | 0 |
| Surfactant (CoatOsil 7500) | 0 | 0 |
| Accelerator (Westdry Cobalt 6%) | 0 | 0 |
| Accelerator (NL51 P) | 0 | 0 |
| Accelerator (12% Cobalt Hex-Cem) | 0 | 0 |
| Silane | 0 | 0 |
| Tronox CR-826 | 0 | 0 |
| Alcohol (IPA) | 0 | 0 |
| Acetone | 0 | 0 |

| Aggregate Thruput | Monthly | 12-months | Limit |
|--------------------|---------|-----------|-------|
| line 1 (tons) | | 30,530 | |
| line 2 (tons) | | 30,530 | |
| Hours of Operation | | | |
| line 1 (hours) | | 6,106 | |
| line 2 (hours) | | 6,106 | |

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SOUTH DISTRICT

Table 1 Calculated Emissions from Combustion of Natural Gas for RTO
Emission factors from AP-42 Table 1.5-1

EXAMPLE ONLY

| 2008 Period | SC306 | ST775 | Heat Input Therms/Month | MMBTU/Month | Emission Factor, lb/1,000,000 scf* | | | | | Emissions, lb/month | | | | | |
|--------------------|-----------------|-------|----------------------------|-------------|------------------------------------|-----|----|-----|----|---------------------|-------------|-------------|-------------|-------------|-------------|
| | | | | | NOx | VOC | CO | SO2 | PM | PM10 | NOx | VOC | CO | SO2 | PM |
| January | | | 0.00 | 0.00 | 100 | 5.5 | 84 | 0.6 | 3 | 3 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| February | | | 0.00 | 0.00 | 100 | 5.5 | 84 | 0.6 | 3 | 3 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| March | | | 0.00 | 0.00 | 100 | 5.5 | 84 | 0.6 | 3 | 3 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| April | 2241.7 | | 0.00 | 0.00 | 100 | 5.5 | 84 | 0.6 | 3 | 3 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| May | 860.2 | | 0.00 | 0.00 | 100 | 5.5 | 84 | 0.6 | 3 | 3 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| June | 547 | | 0.00 | 0.00 | 100 | 5.5 | 84 | 0.6 | 3 | 3 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| July | 658.8 | | 0.00 | 0.00 | 100 | 5.5 | 84 | 0.6 | 3 | 3 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| August | 1195.9 | | 0.00 | 0.00 | 100 | 5.5 | 84 | 0.6 | 3 | 3 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| September | 1322 | | 0.00 | 0.00 | 100 | 5.5 | 84 | 0.6 | 3 | 3 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| October | 1874.3 | | 0.00 | 0.00 | 100 | 5.5 | 84 | 0.6 | 3 | 3 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| November | 1321.8 | | 0.00 | 0.00 | 100 | 5.5 | 84 | 0.6 | 3 | 3 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| December | 2231.7 | | 0.00 | 0.00 | 100 | 5.5 | 84 | 0.6 | 3 | 3 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| Annual | 12253.40 | | 0.00 | 0.00 | 0.00 | | | | | | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| TOTALS, TPY | | | | | | | | | | | | | | | 0.00 |

*Emission factor is lb/1,000,000 scf

| Rolling Totals | Heat Input MMBTU/year | NOx | VOC | CO | SO2 | PM | PM10 |
|----------------|--------------------------|--------|--------|--------|--------|--------|--------|
| January | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| February | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| March | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| April | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| May | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| June | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| July | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| August | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| September | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| October | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| November | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| December | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |

| Permitted Limit | September (cubic feet) | October (cubic feet) | November (cubic feet) | December (cubic feet) |
|-----------------|---------------------------------|-------------------------|--------------------------|--------------------------|
| 0.11 mmcf | Fuel Rotary Dryer #1 | | | |
| 0.11 mmcf | Fuel Rotary Dryer #2 | | | |
| 0.76 mmcf | Fuel for RTO | | | |
| 0.06 mmcf | Fuel for Dryer 1- Polish Line 2 | | | |
| 0.06 mmcf | Fuel for Dryer 2- Polish Line 2 | | | |
| 0.06 mmcf | Fuel for Oven - Polish Line 2 | | | |

ATTACHMENT D

CALIBRATION PROCEDURES



E-Stone Calibration and Monitoring System Checklist

Purpose

The purpose of these procedures is to confirm that the various monitoring systems used to demonstrate compliance with E-Stone's Title V permit are operating correctly and if not, replaced and re-calibrated according to manufacturer's specifications.

Thermocouples

Thermocouples are electronic and calibrated by the manufacturer. They are read by the operators daily and included in the daily record keeping system. E-Stone verifies temperature stability by using a Fluke Infrared Thermometer. If a thermocouple fails, it will register an error message on the digital readout or fail to register a temperature on the chart recorder.

Replace thermocouples when they fail. Thermocouples may be checked quarterly for proper function following the manufacturer's procedure. As part of E-Stone's recordkeeping program, document all service, replacement and calibration of these systems.

Magnehelic and Differential Pressure Gauges

Magnehelic and differential pressure gauges are monitored daily and the data entered into the recordkeeping system. During this daily reading, the observer should do the following:

- Make sure the Pitot tube is facing the correct direction and is perpendicular to the airflow.
- Make sure the air tubes are free of dust and are not clogged.
- Check for condensation in the gauge and clean if necessary.
- If the pressure changes from the expected range, check to make sure the Pitot tube is not clogged with dust.

As part of E-Stone's recordkeeping program, document all service, replacement and calibration of these systems.

Fuel Meters

Fuel meters come calibrated from the manufacturer and are not to be calibrated by E-Stone personnel due to safety issues handling natural gas lines. A simple calibration check is to add up all the monthly readings and compare them with the monthly fuel bill.

Weekly flow checks are performed on all fuel meters.

Scales and Load Cells

On a semi-annual basis, load cells and scales used to weigh product and raw materials should be calibrated by a qualified service company. This calibration record must be maintained as part of E-Stone's compliance recordkeeping.

Thermocouples Weekly Checklist

I.

| | |
|------------|-------|
| Date | _____ |
| Time | _____ |
| As Found | _____ |
| As Left | _____ |
| Start Time | _____ |
| Duration | _____ |

II.

| | |
|------------|-------|
| Date | _____ |
| Time | _____ |
| As Found | _____ |
| As Left | _____ |
| Start Time | _____ |
| Duration | _____ |

Comments:

Magnehelic Gauges Weekly Checklist

I. DC3

| | |
|------------|-------|
| Date | _____ |
| Time | _____ |
| As Found | _____ |
| As Left | _____ |
| Start Time | _____ |
| Duration | _____ |

II. RTO Inlet

| | |
|------------|-------|
| Date | _____ |
| Time | _____ |
| As Found | _____ |
| As Left | _____ |
| Start Time | _____ |
| Duration | _____ |

III. RTO Outlet

| | |
|------------|-------|
| Date | _____ |
| Time | _____ |
| As Found | _____ |
| As Left | _____ |
| Start Time | _____ |
| Duration | _____ |

Comments:

Differential Pressure Gauge Weekly Checklist

I.

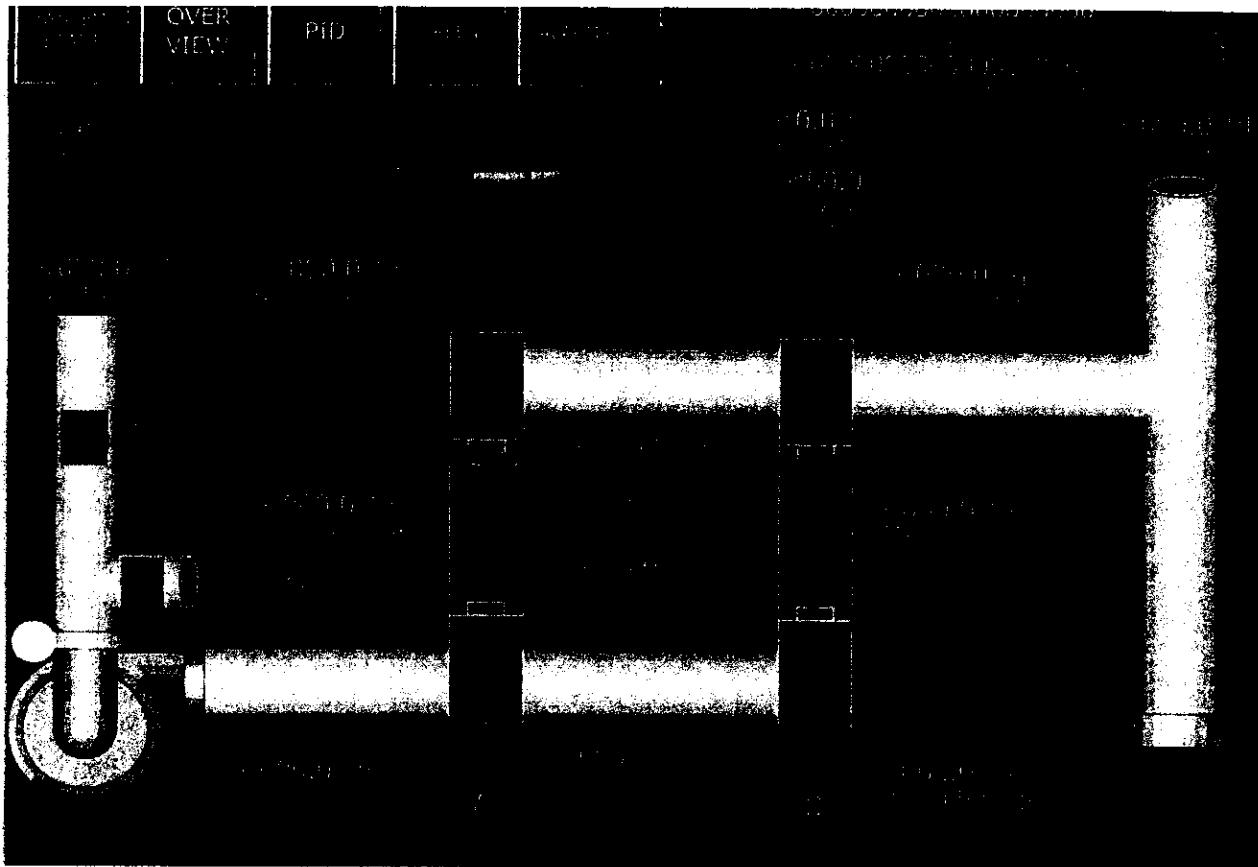
| | |
|------------|-------|
| Date | _____ |
| Time | _____ |
| As Found | _____ |
| As Left | _____ |
| Start Time | _____ |
| Duration | _____ |

II.

| | |
|------------|-------|
| Date | _____ |
| Time | _____ |
| As Found | _____ |
| As Left | _____ |
| Start Time | _____ |
| Duration | _____ |

Comments:

| |
|-------|
| _____ |
| _____ |
| _____ |



| | | | |
|------------------------------|-----------|---------|------|
| Check ISO Valve | OPEN | CLOSED | |
| Poppets A&B | OPERATING | | |
| Fresh Air Valve | OPEN | CLOSED | |
| Outlet Temp | | | |
| Inlet Temp | | | |
| Chart Recorder | ONLINE | OFFLINE | |
| Chart Recorder Print Quality | GOOD | MEDIUM | POOR |
| Chamber Temp Average | | | |
| Main Screen | | | |
| Alarm Screen | | | |
| Rubber Airlines to Poppets | | | |
| Flame Scanner | | | |
| Actuator and Linkage | | | |
| Air Supply | | | |
| Inlet Air Blower | | | |
| Bed A Temp | | | |
| Bed B Temp | | | |
| Comments: | | | |

E-Stone USA Corporation
Corrective Action Record Sheet

- Occurrence of startup, shutdown or malfunction of operation (process equipment)
- Occurrence of malfunction of required air pollution control & monitoring equipment

Date: _____

Name: _____

Time occurrence began _____ Time occurrence was resolved _____

Description of occurrence

Action taken during periods of startup, shutdown and malfunction, including corrective actions to restore malfunctioning process and air pollution control devices back to normal operation

Were procedures consistent with procedures outlined in the Operation & Maintenance Plan? YES / NO (circle one)

If no, explain and attach copy of notification to the Department

Does the corrective action require a revision of the operation & maintenance plan?
YES / NO (circle one)

If yes, explain

Attachment G
2008 Record Keeping

E-Stone USA Corporation

Facility-wide Monthly VOC & HAP Emissions

Controlled by 7000 scfm Crawford RTO

January-08

| Material | E-Stone Item Number | Material Usage (lbs) | VOC Content (%) | Emission Factor ¹ (%) | VOC Emissions (Tons) | VOS Content (%) | VOS Emissions (Tons) | Styrene Content (%) | Styrene Emissions (Tons) | Dimethyl Phthalate Content (%) | Dimethyl Phthalate Emissions (Tons) | Methanol Content (%) | Methanol Emissions (Tons) | MIBK Content (%) | MIBK Emissions (Tons) | Total HAPs (Tons) |
|---------------------------------------|---------------------|----------------------|-----------------|----------------------------------|----------------------|-----------------|----------------------|---------------------|--------------------------|--------------------------------|-------------------------------------|----------------------|---------------------------|------------------|-----------------------|-------------------|
| Resin & Styrene ³ | RM0002 | 144,471 | 36.198% | 1.79% | 1.2930 | | | 35.198% | 1.2930 | | | | | | | |
| Epoxy Resin 4030 Transparent | CN0044 | 439 | 0.00% | | | | | | | | | | | | | |
| Epoxy Resin 4030 White | CN0045 | 154 | 0.00% | | | | | | | | | | | | | |
| Epoxy Hardner MR5CL | CN0046 | 147 | 0.00% | | | | | | | | | | | | | |
| Styrene - (add to resin) | CN0002 | 100.00% | | | 0.0000 | | | 100.00% | 0.0000 | | | | | | | |
| Tinuvin | RM0006 | 513 | 100.00% | | 0.0863 | | | | | | | | | | | |
| Initiator Norox MEKP-9-H ² | RM0012 | 1,587 | 100.00% | 0.04% | 0.0001 | | | | | 40.00% | 0.0000 | | | | | |
| Surfactant (CoatCell 7500) | RM0001 | 41 | 1.00% | | 0.0001 | | | | | | | | | | | |
| Accelerator (Westdry Cobalt 6%) | RM0003 | | 100.00% | | 0.0000 | | | | | | | | | | | |
| Accelerator (NL51 P) | RM0017 | 13 | 100.00% | | 0.0022 | | | | | | | | | | | |
| Accelerator (12% Cobalt Hex-Cern) | RM0025 | | 100.00% | | 0.0000 | | | | | | | 0.20% | 0.0001 | | | |
| Silane | RM0005 | 411 | 100.00% | | 0.0681 | | | | | | | | | | | |
| Tronox CR-826 | RM0020 | 2,230 | 2.00% | | 0.0075 | | | | | | | | | | | |
| Alcohol (IPA) (gallons X 6.8) | CN0057 | 34 | 100.00% | | 0.0170 | | | | | | | | | | | |
| Acetone | CN0001 | 793 | | | 0.0000 | | | 100.00% | 0.40 | | | | | | | |
| Monthly Total | | 150,816 | | | 1.4763 | | | 0.3965 | 1.2930 | | 0.0000 | 0.0001 | 0.0000 | 1.2932 | | |
| Year-To-Date Total | | 150,816 | | | 1.4763 | | | 0.3965 | 1.2930 | | 0.0000 | 0.0001 | 0.0000 | 1.2932 | | |
| 12 Month Rolling Total | | 1,570,964 | | | 19.7369 | | | 4.9580 | 16.8481 | | 0.0004 | 0.0016 | 0.0000 | 16.8481 | | |

Notes:

1. HAP emission rate was 35.88 lbs organic HAP/ton resin used from engineering test dates 12-08

2. Emission factor for Initiator VOC & DMP is 0.04%, see engineering calculations provided by AOC, resin supplier.

3. 22,800 pounds of styrene will be added to the general purpose resin. The styrene content of the resin was raised from 35.9% to 36.198% to account for the addition of the used styrene as a diluent.

¹emission calculation for chemicals used in the enclosure - 32.6% are uncontrolled (vented to beghouse and mold cooling vent) and 67.4% are vented to RTO with 98.5% destruction efficiency

E-Stone USA Corporation

Facility-wide Monthly VOC & HAP Emissions
 Controlled by 7000 scfm Crawford RTO
 February-08

| Material | E-Stone Item Number | Material Usage (lbs) | VOC Content (%) | Emission Factor ¹ (%) | VOC Emissions (Tons) | VOS Content (%) | VOS Emissions (Tons) | Styrene Content (%) | Styrene Emissions (Tons) | Dimethyl Phthalate Content (%) | Dimethyl Phthalate Emissions (Tons) | Methanol Content (%) | Methanol Emissions (Tons) | MIBK Content (%) | MIBK Emissions (Tons) | Total HAPs (Tons) |
|--------------------------------------|---------------------|----------------------|-----------------|----------------------------------|----------------------|-----------------|----------------------|---------------------|--------------------------|--------------------------------|-------------------------------------|----------------------|---------------------------|------------------|-----------------------|-------------------|
| Resin & Styrene ³ | RM0002 | 133,455 | 36.198% | 1.79% | 1.1944 | | | 36.198% | 1.1944 | | | | | | | |
| Epoxy Resin 4030 Transparent | CN0044 | 1,730 | 0.00% | | | | | | | | | | | | | |
| Epoxy Resin 4030 White | CN0045 | 0 | 0.00% | | | | | | | | | | | | | |
| Epoxy Hardner MR50L | CN0046 | 0 | 0.00% | | | | | | | | | | | | | |
| Styrene - (add to resin) | CN0002 | | 100.00% | | 0.0000 | | | 100.00% | 0.0000 | | | | | | | |
| Thiuvin | RM0006 | 431 | 100.00% | | 0.0724 | | | | | | | | | | | |
| Initiator Norox MEKP-9H ² | RM0012 | 1,643 | 100.00% | 0.04% | 0.0001 | | | | | 40.00% | 0.0000 | | | | | |
| Surfactant (CoatOil 7500) | RM0001 | 36 | 1.00% | | 0.0001 | | | | | | | | | | | |
| Accelerator (Westdry Cobalt 6%) | RM0003 | | 100.00% | | 0.0000 | | | | | | | | | | | |
| Accelerator (NL 51 P) | RM0017 | 11 | 100.00% | | 0.0019 | | | | | | | | | | | |
| Accelerator (12% Cobalt Hex-Cem) | RM0025 | | 100.00% | | 0.0000 | | | | | | | 0.20% | 0.0001 | | | |
| Silane | RM0005 | 359 | 100.00% | | 0.0603 | | | | | | | | | | | |
| Tronox CR-826 | RM0020 | 2,050 | 2.00% | | 0.0069 | | | | | | | | | | | |
| Alcohol (IPA) (gallons X 6.8) | CN0057 | 0 | 100.00% | | 0.0000 | | | | | | | | | | | |
| Acrastrip | | | 60.00% | | 0.0000 | | | | | | | | | | | |
| Acetone | CN0001 | 358 | | | 100.00% | 0.18 | | | | | | | | | | 1.1946 |
| Monthly Total | | 140,073 | | | 1.3361 | | 0.1790 | | 1.1944 | | 0.0000 | | 0.0001 | | 0.0000 | 2.4878 |
| Year-To-Date Total | | 290,888 | | | 2.8114 | | 0.6755 | | 2.4874 | | 0.0001 | | 0.0005 | | 0.0000 | 16.0706 |
| 12 Month Rolling Total | | 1,623,488 | | | 19.3975 | | 4.4080 | | 16.0685 | | | | | | | |

Notes:

1. HAP emission rate was 35.88 lbs organic HAP/ton resin used from engineering test dates 12-06

2. Emission factor for Initiator VOC & DMP is 0.04%, see engineering calculations provided by ACC, resin supplier.

3. 22,800 pounds of styrene will be added to the general purpose resin. The styrene content of the resin was raised from 35.9% to 36.198% to account for the addition of the used styrene as a diluent.

*Emission calculation for chemicals used in the enclosure - 32.6% are uncontrolled (vented to baghouse and mold cooling vent) and 67.4% are vented to RTO with 98.5% destruction efficiency

E-Stone USA Corporation

Facility-wide Monthly VOC & HAP Emissions
Controlled by 7000 scfm Crawford RTO

March-08

| Material | E-Stone Item Number | Material Usage (lbs) | VOC Content (%) | Emission Factor ¹ (%) | VOC Emissions (Tons) | VOS Content (%) | VOS Emissions (Tons) | Styrene Content (%) | Styrene Emissions (Tons) | Dimethyl Phthalate Content (%) | Dimethyl Phthalate Emissions (Tons) | Methanol Content (%) | Methanol Emissions (Tons) | MIBK Content (%) | MIBK Emissions (Tons) | Total HAPs (Tons) |
|--------------------------------------|---------------------|----------------------|-----------------|----------------------------------|----------------------|-----------------|----------------------|---------------------|--------------------------|--------------------------------|-------------------------------------|----------------------|---------------------------|------------------|-----------------------|-------------------|
| Resin & Styrene ³ | RM0002 | 122,099 | 36.198% | 1.79% | 1.0928 | | | 36.198% | 1.0928 | | | | | | | |
| Epoxy Resin 4030 Transparent | CN0044 | 1,071 | 0.00% | | | | | | | | | | | | | |
| Epoxy Resin 4030 White | CN0045 | 492 | 0.00% | | | | | | | | | | | | | |
| Epoxy Hardner MR50L | CN0046 | 155 | 0.00% | | | | | | | | | | | | | |
| Styrene - (add to resin) | CN0002 | | 100.00% | | 0.0000 | | | 100.00% | 0.0000 | | | | | | | |
| Tinuvin | RM0008 | 477 | 100.00% | | 0.0801 | | | | | 40.00% | 0.0000 | | | | | |
| Initiator Norox MEKP-9H ² | RM0012 | 1,584 | 100.00% | 0.04% | 0.0001 | | | | | | | | | | | |
| Surfactant (CoalOsil 7500) | RM0001 | 77 | 1.00% | | 0.0001 | | | | | | | | | | | |
| Accelerator (Westdry Cobalt 6%) | RM0003 | | 100.00% | | 0.0000 | | | | | | | | | | | |
| Accelerator (NL51 P) | RM0017 | 38 | 100.00% | | 0.0064 | | | | | | | | | | | |
| Accelerator (12% Cobalt Hex-Cem) | RM0025 | | 100.00% | | 0.0000 | | | | | | | 0.20% | 0.0001 | | | |
| Silane | RM0005 | 425 | 100.00% | | 0.0713 | | | | | | | | | | | |
| Tronox CR-826 | RM0020 | 5,203 | 2.00% | | 0.0175 | | | | | | | | | | | |
| Alcohol (IPA) (gallons X 6.8) | CN0057 | 2 | 100.00% | | 0.0009 | | | | | | | | | | | |
| Acrastrip | | | 60.00% | | 0.0000 | | | | | | | | | | | |
| Acetone | CN0001 | 716 | | | 100.00% | 0.36 | | | | | | | | | | |
| Monthly Total | | 132,318 | | | 1.2692 | | | 0.3680 | 1.0928 | | 0.0000 | | 0.0001 | | 0.0000 | |
| Year-To-Date Total | | 423,206 | | | 4.0806 | | | 0.9335 | 3.6902 | | 0.0001 | | 0.0004 | | 0.0000 | |
| 12 Month Rolling Total | | 1,632,241 | | | 18.9743 | | | 4.3836 | 15.9704 | | 0.0005 | | 0.0015 | | 15.9724 | |

Notes:

1. HAP emission rate was 35.88 lbs organic HAP/ton resin used from engineering test dates 12-06

2. Emission factor for initiator VOC & DMP is 0.04%, see engineering calculations provided by AOC, resin supplier.

3. 22,800 pounds of styrene will be added to the general purpose resin. The styrene content of the resin was raised from 35.9% to 36.198% to account for the addition of the used styrene as a diluent.

*emission calculation for chemicals used in the enclosure - 32.6% are uncontrolled (vented to baghouse and mold cooling vent) and 67.4% are vented to RTO with 98.5% destruction efficiency

E-Stone USA Corporation

Facility-wide Monthly VOC & HAP Emissions
Controlled by 7000 scfm Crawford RTO

April-08

| Material | E-Stone Item Number | Material Usage (lbs) | VOC Content (%) | Emission Factor ¹ (%) | VOC Emissions (Tons) | VOS Content (%) | VOS Emissions (Tons) | Styrene Content (%) | Styrene Emissions (Tons) | Dimethyl Phthalate Content (%) | Dimethyl Phthalate Emissions (Tons) | Methanol Content (%) | Methanol Emissions (Tons) | MIBK Content (%) | MIBK Emissions (Tons) | Total HAPs (Tons) |
|--------------------------------------|---------------------|----------------------|-----------------|----------------------------------|----------------------|-----------------|----------------------|---------------------|--------------------------|--------------------------------|-------------------------------------|----------------------|---------------------------|------------------|-----------------------|-------------------|
| Resin & Styrene ³ | RM0002 | 85,718 | 36.198% | 1.79% | 0.7672 | | | 36.198% | 0.7672 | | | | | | | |
| Epoxy Resin 4030 Transparent | CN0044 | 1,082 | 0.00% | | | | | | | | | | | | | |
| Epoxy Resin 4030 White | CN0045 | 0 | 0.00% | | | | | | | | | | | | | |
| Epoxy Hardner MR50L | CN0046 | 76 | 0.00% | | | | | 100.00% | 0.0000 | | | | | | | |
| Styrene - (add to resin) | CN0002 | | 100.00% | | 0.0000 | | | | | | | | | | | |
| Tiruvin | RM0006 | 301 | 100.00% | | 0.0507 | | | | | 40.00% | 0.0000 | | | | | |
| Initiator Norox MEKP-SH ² | RM0012 | 1,003 | 100.00% | 0.04% | 0.0001 | | | | | | | | | | | |
| Surfactant (CoatOsil 7500) | RM0001 | 24 | 1.00% | | 0.0000 | | | | | | | | | | | |
| Accelerator (Westdry Cobalt 6%) | RM0003 | | 100.00% | | 0.0000 | | | | | | | | | | | |
| Accelerator (NL51 P) | RM0017 | 8 | 100.00% | | 0.0013 | | | | | | | | | | | |
| Accelerator (12% Cobalt Hex-Cern) | RM0025 | | 100.00% | | 0.0000 | | | | | | | 0.20% | 0.0001 | | | |
| Silane | RM0005 | 242 | 100.00% | | 0.0406 | | | | | | | | | | | |
| Tronox CR-826 | RM0020 | 37 | 2.00% | | 0.0001 | | | | | | | | | | | |
| Alcohol (IPA) (gallons x 6.8) | CN0057 | 2 | 100.00% | | 0.0009 | | | | | | | | | | | |
| Acetrip | | | 60.00% | | 0.0000 | | | | | | | | | | | |
| Acetone | CN0001 | 358 | | | 100.00% | 0.18 | | | | | 0.0000 | 0.0001 | 0.0000 | 0.7673 | | |
| Monthly Total | | 86,851 | | | 0.8608 | 0.1790 | 0.7672 | | | | 0.0000 | 0.0005 | 0.0000 | 4.3480 | | |
| Year-To-Date Total | | 612,067 | | | 4.9414 | 1.1125 | 4.3474 | | | | 0.0002 | 0.0016 | 0.0000 | 15.5573 | | |
| 12 Month Rolling Total | | 1,596,577 | | | 18.2402 | 4.1976 | 15.5554 | | | | 0.0006 | | | | | |

Notes:

1. HAP emission rate was 35.88 lbs organic HAP/ton resin used from engineering test dates 12-06

2. Emission factor for initiator VOC & DMP is 0.04%, see engineering calculations provided by AOC, resin supplier.

3. 22,800 pounds of styrene will be added to the general purpose resin. The styrene content of the resin was raised from 35.9% to 36.198% to account for the addition of the used styrene as a diluent.

*emission calculation for chemicals used in the enclosure - 32.6% are uncontrolled (vented to baghouse and mold cooling vent) and 67.4% are vented to RTO with 98.5% destruction efficiency

E-Stone USA Corporation

Facility-wide Monthly VOC & HAP Emissions
Controlled by 7000 scfm Crawford RTO

May-08

| Material | E-Stone Item Number | Material Usage (lbs) | VOC Content (%) | Emission Factor ¹ (%) | VOC Emissions (Tons) | VOS Content (%) | VOS Emissions (Tons) | Styrene Content (%) | Styrene Emissions (Tons) | Dimethyl Phthalate Content (%) | Dimethyl Phthalate Emissions (Tons) | Methanol Content (%) | Methanol Emissions (Tons) | MIBK Content (%) | MIBK Emissions (Tons) | Total HAPs (Tons) |
|--------------------------------------|---------------------|----------------------|-----------------|----------------------------------|----------------------|-----------------|----------------------|---------------------|--------------------------|--------------------------------|-------------------------------------|----------------------|---------------------------|------------------|-----------------------|-------------------|
| Resin & Styrene ³ | RM0002 | 100,863 | 36.198% | 1.79% | 0.9027 | | | 36.198% | 0.9027 | | | | | | | |
| Epoxy Resin 4030 Transparent | CN0044 | 1,094 | 0.00% | | | | | | | | | | | | | |
| Epoxy Resin 4030 White | CN0045 | 0 | 0.00% | | | | | | | | | | | | | |
| Epoxy Hardner MR50L | CN0046 | 244 | 0.00% | | | | | | | | | | | | | |
| Styrene - (add to resin) | CN0002 | | 100.00% | | 0.0000 | | | 100.00% | 0.0000 | | | | | | | |
| Tinuvin | RM0006 | 382 | 100.00% | | 0.0608 | | | | | | | | | | | |
| Initiator Norox MEKP-9H ² | RM0012 | 1,070 | 100.00% | 0.04% | 0.0001 | | | | | 40.00% | 0.0000 | | | | | |
| Surfactant (CoatOsil 7500) | RM0001 | 28 | 1.00% | | 0.0000 | | | | | | | | | | | |
| Accelerator (Westdry Cobalt 6%) | RM0003 | | 100.00% | | 0.0000 | | | | | | | | | | | |
| Accelerator (NL51 P) | RM0017 | 100 | 100.00% | | 0.0168 | | | | | | | | | | | |
| Accelerator (12% Cobalt Hex-Cem) | RM0025 | | 100.00% | | 0.0000 | | | | | | | 0.20% | 0.0001 | | | |
| Silane | RM0005 | 335 | 100.00% | | 0.0563 | | | | | | | | | | | |
| Tronox CR-826 | RM0020 | 350 | 2.00% | | 0.0012 | | | | | | | | | | | |
| Alcohol (IPA) (gallons X 6.8) | CN0057 | 0 | 100.00% | | 0.0000 | | | | | | | | | | | |
| Acrastrip | | | 60.00% | | 0.0000 | | | | | | | | | | | |
| Acetone | CN0001 | 716 | | | 100.00% | 0.36 | | | | | 0.0000 | | 0.0001 | | 0.0000 | 0.9029 |
| Monthly Total | | 106,164 | | | 1.0380 | | 0.3580 | | 0.9027 | | | | | | | 6.2509 |
| Year-To-Date Total | | 617,220 | | | 6.9794 | | 1.4706 | | 5.2601 | | | | 0.0002 | | 0.0006 | 0.0000 |
| 12 Month Rolling Total | | 1,569,311 | | | 17.6877 | | 4.3730 | | 15.1607 | | | | 0.0008 | | 0.0015 | 0.0000 |

Notes:

1. HAP emission rate was 35.88 lbs organic HAP/ton resin used from engineering test dates 12-06

2. Emission factor for Initiator VOC & DMP is 0.04%, see engineering calculations provided by AOC, resin supplier.

3. 22,800 pounds of styrene will be added to the general purpose resin. The styrene content of the resin was raised from 35.9% to 36.198% to account for the addition of the used styrene as a diluent.

*emission calculation for chemicals used in the enclosure - 32.6% are uncontrolled (vented to baghouse and mold cooling vent) and 67.4% are vented to RTO with 98.6% destruction efficiency

E-Stone USA Corporation

Facility-wide Monthly VOC & HAP Emissions
Controlled by 7000 scfm Crawford RTO
June-08

| Material | E-Stone Item Number | Material Usage (lbs) | VOC Content (%) | Emission Factor ¹ (%) | VOC Emissions (Tons) | VOS Content (%) | VOS Emissions (Tons) | Styrene Content (%) | Styrene Emissions (Tons) | Dimethyl Phthalate Content (%) | Dimethyl Phthalate Emissions (Tons) | Methanol Content (%) | Methanol Emissions (Tons) | MIBK Content (%) | MIBK Emissions (Tons) | Total HAPs (Tons) |
|--------------------------------------|---------------------|----------------------|-----------------|----------------------------------|----------------------|-----------------|----------------------|---------------------|--------------------------|--------------------------------|-------------------------------------|----------------------|---------------------------|------------------|-----------------------|-------------------|
| Resin & Styrene ² | RM0002 | 80,345 | 36.198% | 1.79% | 0.7191 | | | 36.198% | 0.7191 | | | | | | | |
| Epoxy Resin 4030 Transparent | CN0044 | 1,046 | 0.00% | | | | | | | | | | | | | |
| Epoxy Resin 4030 White | CN0045 | 356 | 0.00% | | | | | | | | | | | | | |
| Epoxy Hardiner MR50L | CN0046 | 0 | 0.00% | | | | | | | | | | | | | |
| Styrene - (add to resin) | CN0002 | | 100.00% | | 0.0000 | | | 100.00% | 0.0000 | | | | | | | |
| Tinuvin | RM0006 | 282 | 100.00% | | 0.0473 | | | | | | | | | | | |
| Initiator Norox MEKP-9H ³ | RM0012 | 1,011 | 100.00% | 0.04% | 0.0001 | | | | | 40.00% | 0.0000 | | | | | |
| Surfactant (CoatOsil 7500) | RM0001 | 23 | 1.00% | | 0.0000 | | | | | | | | | | | |
| Accelerator (Westdry Cobalt 6%) | RM0003 | | 100.00% | | 0.0000 | | | | | | | | | | | |
| Accelerator (NL51 P) | RM0017 | 7 | 100.00% | | 0.0012 | | | | | | | | | | | |
| Accelerator (12% Cobalt Hex-Cem) | RM0025 | | 100.00% | | 0.0000 | | | | | | | 0.20% | 0.0001 | | | |
| Silane | RM0005 | 226 | 100.00% | | 0.0379 | | | | | | | | | | | |
| Tronox CR-826 | RM0020 | 5,659 | 2.00% | | 0.0190 | | | | | | | | | | | |
| Alcohol (IPA) (gallons x 6.8) | CN0057 | 2 | 100.00% | | 0.0009 | | | | | | | | | | | |
| Acrastrip | | | 60.00% | | 0.0000 | | | | | | | | | | | |
| Acetone | CN0001 | 715 | | | | 100.00% | 0.36 | | | | | | | | | |
| Monthly Total | | 89,673 | | | 0.8255 | | 0.3675 | | 0.7191 | | 0.0000 | | 0.0001 | | 0.0000 | |
| Year-To-Date Total | | 706,893 | | | 6.8049 | | 1.8280 | | 5.9892 | | 0.0002 | | 0.0007 | | 0.0000 | |
| 12 Month Rolling Total | | 1,482,061 | | | 15.1179 | | 4.0006 | | 14.1868 | | 0.0004 | | 0.0014 | | 0.0000 | |
| <hr/> | | | | | | | | | | | | | | | | |

Notes:

1. HAP emission rate was 35.88 lbs organic HAP/ton resin used from engineering test dates 12-06

2. Emission factor for Initiator VOC & DMP is 0.04%, see engineering calculations provided by ADC, resin supplier.

3. 22,800 pounds of styrene will be added to the general purpose resin. The styrene content of the resin was raised from 35.9% to 36.198% to account for the addition of the used styrene as a diluent.

*emission calculation for chemicals used in the enclosure - 32.6% are uncontrolled (vented to baghouse and mold cooling vent) and 67.4% are vented to RTO with 98.5% destruction efficiency

E-Stone USA Corporation

Facility-wide Monthly VOC & HAP Emissions

Controlled by 7000 scfm Crawford RTO

July-08

| Material | E-Stone Item Number | Material Usage (lbs) | VOC Content (%) | Emission Factor ¹ (%) | VOC Emissions (Tons) | VOS Content (%) | VOS Emissions (Tons) | Styrene Content (%) | Styrene Emissions (Tons) | Dimethyl Phthalate Content (%) | Dimethyl Phthalate Emissions (Tons) | Methanol Content (%) | Methanol Emissions (Tons) | MIBK Content (%) | MIBK Emissions (Tons) | Total HAPs (Tons) |
|--------------------------------------|---------------------|----------------------|-----------------|----------------------------------|----------------------|-----------------|----------------------|---------------------|--------------------------|--------------------------------|-------------------------------------|----------------------|---------------------------|------------------|-----------------------|-------------------|
| Resin & Styrene ² | RM0002 | 60,251 | 36.198% | 1.78% | 0.5392 | | | 36.198% | 0.5392 | | | | | | | |
| Epoxy Resin 4030 Transparent | CN0044 | 1,292 | 0.00% | | | | | | | | | | | | | |
| Epoxy Resin 4030 White | CN0045 | 134 | 0.00% | | | | | | | | | | | | | |
| Epoxy Hardner MR50L | CN0046 | 0 | 0.00% | | | | | | | | | | | | | |
| Styrene - (add to resin) | CN0062 | | 100.00% | | 0.0000 | | | 100.00% | 0.0000 | | | | | | | |
| Tinuvin | RM0006 | 215 | 100.00% | | 0.0362 | | | | | 40.00% | 0.0000 | | | | | |
| Initiator Norox MEKP-9H ³ | RM0012 | 667 | 100.00% | 0.04% | 0.0000 | | | | | | | | | | | |
| Surfactant (CoatOil 7500) | RM0001 | 17 | 1.00% | | 0.0000 | | | | | | | | | | | |
| Accelerator (Westdry Cobalt 6%) | RM0003 | | 100.00% | | 0.0000 | | | | | | | | | | | |
| Accelerator (NL51 P) | RM0017 | 5 | 100.00% | | 0.0009 | | | | | | | | | | | |
| Accelerator (12% Cobalt Hex-Cem) | RM0025 | | 100.00% | | 0.0000 | | | | | | | 0.20% | 0.0001 | | | |
| Silane | RM0005 | 173 | 100.00% | | 0.0281 | | | | | | | | | | | |
| Tronox CR-B26 | RM0020 | 2,917 | 2.00% | | 0.0698 | | | | | | | | | | | |
| Alcohol (IPA) (gallons X 6.8) | CN0057 | 36 | 100.00% | | 0.0179 | | | | | | | | | | | |
| Acrastrip | | | | | 60.00% | | | | | | | | | | | |
| Acetone | CN0001 | 714 | | | | 100.00% | 0.36 | | | | | | 0.0001 | 0.0000 | 0.5393 | |
| Monthly Total | | 66,422 | | | 0.5332 | | 0.3570 | | 0.5392 | | 0.0000 | | 0.0007 | 0.0000 | 6.5094 | |
| Year-To-Date Total | | 773,316 | | | 7.4381 | | 2.1860 | | 6.5086 | | 0.0002 | | 0.0014 | 0.0000 | 13.7146 | |
| 12 Month Rolling Total | | 1,437,578 | | | 15.4807 | | 4.1760 | | 13.7128 | | 0.0004 | | | | | |

Notes:

1. HAP emission rate was 35.68 lbs organic HAP/ton resin used from engineering test dates 12-06

2. Emission factor for Initiator VOC & DMP is 0.04%, see engineering calculations provided by AOC, resin supplier.

3. 22,800 pounds of styrene will be added to the general purpose resin. The styrene content of the resin was raised from 35.9% to 36.198% to account for the addition of the used styrene as a diluent.

*emission calculation for chemicals used in the enclosure - 32.6% are uncontrolled (vented to baghouse and mold cooling vent) and 67.4% are vented to RTO with 99.5% destruction efficiency

E-Stone USA Corporation

Facility-wide Monthly VOC & HAP Emissions
Controlled by 7000 scfm Crawford RTO

August-08

| Material | E-Stone Item Number | Material Usage (lbs) | VOC Content (%) | Emission Factor ¹ (%) | VOC Emissions (Tons) | VOS Content (%) | VOS Emissions (Tons) | Styrene Content (%) | Styrene Emissions (Tons) | Dimethyl Phthalate Content (%) | Dimethyl Phthalate Emissions (Tons) | Methanol Content (%) | Methanol Emissions (Tons) | MIBK Content (%) | MIBK Emissions (Tons) | Total HAPs (Tons) |
|--------------------------------------|---------------------|----------------------|-----------------|----------------------------------|----------------------|-----------------|----------------------|---------------------|--------------------------|--------------------------------|-------------------------------------|----------------------|---------------------------|------------------|-----------------------|-------------------|
| Resin & Styrene ³ | RMO002 | 64,676 | 36.198% | 1.79% | 0.5789 | | | 36.198% | 0.5789 | | | | | | | |
| Epoxy Resin 4030 Transparent | CN0044 | 572 | 0.00% | | | | | | | | | | | | | |
| Epoxy Resin 4030 White | CN0045 | 18 | 0.00% | | | | | | | | | | | | | |
| Epoxy Hardner MRSOL | CN0046 | 107 | 0.00% | | | | | | | | | | | | | |
| Styrene - (add to resin) | CN0002 | | 100.00% | | 0.0000 | | | 100.00% | 0.0000 | | | | | | | |
| Tinuvin | RMO006 | 233 | 100.00% | | 0.0391 | | | | | | | | | | | |
| Initiator Norox MEKP-9H ² | RMO012 | 725 | 100.00% | 0.04% | 0.0000 | | | | | 40.00% | 0.0000 | | | | | |
| Surfactant (CoatOsil 7500) | RMO001 | 19 | 1.00% | | 0.0000 | | | | | | | | | | | |
| Accelerator (Westdry Cobalt 6%) | RMO003 | | 100.00% | | 0.0000 | | | | | | | | | | | |
| Accelerator (NL51 P) | RMO017 | 15 | 100.00% | | 0.0025 | | | | | | | | | | | |
| Accelerator (12% Cobalt Hex-Cern) | RMO025 | | 100.00% | | 0.0000 | | | | | | | 0.20% | 0.0001 | | | |
| Silane | RMO005 | 186 | 100.00% | | 0.0313 | | | | | | | | | | | |
| Tronox CR-826 | RMO020 | 1,105 | 2.00% | | 0.0037 | | | | | | | | | | | |
| Alcohol (IPA) (gallons X 6.8) | CN0057 | 49 | 100.00% | | 0.0245 | | | | | | | | | | | |
| Acrastrip | | | 60.00% | | 0.0000 | | | | | | | | | | | |
| Acetone | CN0001 | 714 | | | 100.00% | 0.36 | | | | | | | | | | 0.5789 |
| Monthly Total | | 68,418 | | | 0.5800 | | 0.3670 | | 0.6789 | | 0.0000 | | 0.0001 | | 0.0000 | 7.0883 |
| Year-To-Date Total | | 841,733 | | | 8.1182 | | 2.5420 | | 7.0873 | | 0.0002 | | 0.0008 | | 0.0000 | 11.3882 |
| 12 Month Rolling Total | | 1,355,057 | | | 13.0654 | | 4.1495 | | 11.3866 | | 0.0004 | | 0.0013 | | 0.0000 | |

Notes:

1. HAP emission rate was 35.88 lbs organic HAP/ton resin used from engineering test dates 12-06

2. Emission factor for Initiator VOC & DMP is 0.04%, see engineering calculations provided by AOC, resin supplier.

3. 22,800 pounds of styrene will be added to the general purpose resin. The styrene content of the resin was raised from 35.9% to 36.198% to account for the addition of the used styrene as a diluent.

*emission calculation for chemicals used in the enclosure - 32.6% are uncontrolled (vented to baghouse and mold cooling vent) and 67.4% are vented to RTO with 98.6% destruction efficiency

E-Stone USA Corporation

Facility-wide Monthly VOC & HAP Emissions
Controlled by 7000 scfm Crawford RTO

September-08

| Material | E-Stone Item Number | Material Usage (lbs) | VOC Content (%) | Emission Factor ¹ (%) | VOC Emissions (Tons) | VOS Content (%) | VOS Emissions (Tons) | Styrene Content (%) | Styrene Emissions (Tons) | Dimethyl Phthalate Content (%) | Dimethyl Phthalate Emissions (Tons) | Methanol Content (%) | Methanol Emissions (Tons) | MIBK Content (%) | MIBK Emissions (Tons) | Total HAPs (Tons) |
|--------------------------------------|---------------------|----------------------|-----------------|----------------------------------|----------------------|-----------------|----------------------|---------------------|--------------------------|--------------------------------|-------------------------------------|----------------------|---------------------------|------------------|-----------------------|-------------------|
| Resin & Styrene ³ | RM0002 | 65,383 | 36.198% | 1.79% | 0.5852 | | | 36.198% | 0.5852 | | | | | | | |
| Epoxy Resin 4030 Transparent | CN0044 | 1,243 | 0.00% | | | | | | | | | | | | | |
| Epoxy Resin 4030 White | CN0045 | 0 | 0.00% | | | | | | | | | | | | | |
| Epoxy Hardner MR50L | CN0046 | 0 | 0.00% | | | | | | | | | | | | | |
| Styrene - (add to resin) | CN0002 | | 100.00% | | 0.0000 | | | 100.00% | 0.0000 | | | | | | | |
| Tinuvin | RM0006 | 226 | 100.00% | | 0.0380 | | | | | 40.00% | 0.0000 | | | | | |
| Initiator Norox MEKP-9H ² | RM0012 | 716 | 100.00% | 0.04% | 0.0000 | | | | | | | | | | | |
| Surfactant (CoatOsil 7500) | RM0001 | 18 | 1.00% | | 0.0000 | | | | | | | | | | | |
| Accelerator (Westdry Cobalt 6%) | RM0003 | | 100.00% | | 0.0000 | | | | | | | | | | | |
| Accelerator (NL51 P) | RM0017 | 6 | 100.00% | | 0.0010 | | | | | | | | | | | |
| Accelerator (12% Cobalt Hex-Cem) | RM0025 | | 100.00% | | 0.0000 | | | | | | | 0.20% | 0.0001 | | | |
| Silane | RM0005 | 181 | 100.00% | | 0.0304 | | | | | | | | | | | |
| Tronox CR-826 | RM0020 | 1,601 | 2.00% | | 0.0054 | | | | | | | | | | | |
| Alcohol (IPA) (gallons x 8.8) | CN0057 | 112 | 100.00% | | 0.0561 | | | | | | | | | | | |
| Acastrip (gallons x 8.8) | CN000100 | 172 | 60.00% | | 0.0516 | | | | | | | | | | | |
| Acetone | CN0001 | 0 | | | 100.00% | 0.00 | | | | | | | | | | |
| Monthly Total | | 69,858 | | | 0.7677 | | 0.0000 | | 0.5852 | | 0.0000 | | 0.0001 | | 0.0000 | 0.5853 |
| Year-to-Date Total | | 911,391 | | | 8.8859 | | 2.5420 | | 7.8725 | | 0.0003 | | 0.0009 | | 0.0000 | 7.8736 |
| 12 Month Rolling Total | | 1,294,362 | | | 12.5621 | | 3.7845 | | 10.8645 | | 0.0004 | | 0.0012 | | 0.0000 | 10.8561 |

Notes:

1. HAP emission rate was 35.88 lbs organic HAP/ton resin used from engineering test dates 12-06

2. Emission factor for Initiator VOC & DMP is 0.04%, see engineering calculations provided by AOC, resin supplier.

3. 22,800 pounds of styrene will be added to the general purpose resin. The styrene content of the resin was raised from 35.9% to 36.198% to account for the addition of the used styrene as a diluent.

E-Stone USA Corporation

Facility-wide Monthly VOC & HAP Emissions
Controlled by 7000 scfm Crawford RTO

October-08

| Material | E-Stone Item Number | Material Usage (lbs) | VOC Content (%) | Emission Factor ¹ (%) | VOC Emissions (Tons) | VOS Content (%) | VOS Emissions (Tons) | Styrene Content (%) | Styrene Emissions (Tons) | Dimethyl Phthalate Content (%) | Dimethyl Phthalate Emissions (Tons) | Methanol Content (%) | Methanol Emissions (Tons) | MIBK Content (%) | MIBK Emissions (Tons) | Total HAPs (Tons) |
|--------------------------------------|---------------------|----------------------|-----------------|----------------------------------|----------------------|-----------------|----------------------|---------------------|--------------------------|--------------------------------|-------------------------------------|----------------------|---------------------------|------------------|-----------------------|-------------------|
| Resin & Styrene ² | RM0002 | 47,059 | 36.198% | 1.79% | 0.4212 | | | 36.198% | 0.4212 | | | | | | | |
| Epoxy Resin 4030 Transparent | CN0044 | 263 | 0.00% | | | | | | | | | | | | | |
| Epoxy Resin 4030 White | CN0045 | 81 | 0.00% | | | | | | | | | | | | | |
| Epoxy Hardner MRSOL | CN0046 | 0 | 0.00% | | | | | | | | | | | | | |
| Styrene - (add to resin) | CN0002 | | 100.00% | | | 0.0000 | | 100.00% | 0.0000 | | | | | | | |
| Tinuvin | RM0006 | 168 | 100.00% | | 0.0282 | | | | | | | | | | | |
| Initiator Norox MEKP-9H ³ | RM0012 | 517 | 100.00% | 0.04% | 0.0000 | | | | | 40.00% | 0.0000 | | | | | |
| Surfactant (CoatSolv 7500) | RM0001 | 13 | 1.00% | | 0.0000 | | | | | | | | | | | |
| Accelerator (Westdry Cobalt 6%) | RM0003 | | 100.00% | | | 0.0000 | | | | | | | | | | |
| Accelerator (NL51 P) | RM0017 | 4 | 100.00% | | 0.0007 | | | | | | | | | | | |
| Accelerator (12% Cobalt Hex-Cern) | RM0025 | | 100.00% | | 0.0000 | | | | | | | 0.20% | 0.0000 | | | |
| Silane | RM0005 | 135 | 100.00% | | 0.0227 | | | | | | | | | | | |
| Tronox CR-828 | RM0020 | 1,407 | 2.00% | | 0.0447 | | | | | | | | | | | |
| Alcohol (IPA) (gallons X 6.6) | CN0057 | 56 | 100.00% | | 0.0281 | | | | | | | | | | | |
| Acrastrip (gallons X 6.6) | CN000100 | 0 | 60.00% | | 0.0000 | | | | | | | | | | | |
| Acetone | CN0001 | 0 | | | | 100.00% | 0.00 | | | | | | | | | |
| Monthly Total | | 49,704 | | | 0.5057 | | 0.0000 | | 0.4212 | | 0.0000 | | 0.0000 | | 0.0000 | 0.4212 |
| Year-To-Date Total | | 981,095 | | | 9.3916 | | 2.5420 | | 8.0937 | | 0.0003 | | 0.0009 | | 0.0000 | 8.0948 |
| 12 Month Rolling Total | | 1,194,286 | | | 11.6148 | | 3.7845 | | 10.0001 | | 0.0003 | | 0.0011 | | 0.0000 | 10.0015 |

Notes:

1. HAP emission rate was 35.88 lbs organic HAP/ton resin used from engineering test dates 12-06

2. Emission factor for Initiator VOC & DMP is 0.04%, see engineering calculations provided by AOC, resin supplier.

3. 22,800 pounds of styrene will be added to the general purpose resin. The styrene content of the resin was raised from 35.9% to 36.198% to account for the addition of the used styrene as a diluent.

According to the permit, page 13 of 19, "the limits in the table are not enforceable limits. The enforceable HAP limits are defined in 40 CFR 63 Subpart WWWWW. Table 3 in Subpart WWWWW for open molding - non-CR/HS, mechanical resin application the HAP emissions limit is 88 lb/ton.

*emission calculation for chemicals used in the enclosure - 32.6% are uncontrolled (vented to baghouse and mold cooling vent) and 67.4% are vented to RTO with 98.5% destruction efficiency based on the engineering test conducted December 2006

E-Stone USA Corporation

Facility-wide Monthly VOC & HAP Emissions
Controlled by 7000 scfm Crawford RTO

November-08

| Material | E-Stone Item Number | Material Usage (lbs) | VOC Content (%) | Emission Factor ¹ (%) | VOC Emissions (Tons) | VOS Content (%) | VOS Emissions (Tons) | Styrene Content (%) | Styrene Emissions (Tons) | Dimethyl Phthalate Content (%) | Dimethyl Phthalate Emissions (Tons) | Methanol Content (%) | Methanol Emissions (Tons) | MIBK Content (%) | MIBK Emissions (Tons) | Total HAPs (Tons) |
|--------------------------------------|---------------------|----------------------|-----------------|----------------------------------|----------------------|-----------------|----------------------|---------------------|--------------------------|--------------------------------|-------------------------------------|----------------------|---------------------------|------------------|-----------------------|-------------------|
| Resin & Styrene ³ | RM0002 | 38,233 | 36.198% | 1.79% | 0.3243 | | | 36.198% | 0.3243 | | | | | | | |
| Epoxy Resin 4030 Transparent | CN0044 | 392 | 0.00% | | | | | | | | | | | | | |
| Epoxy Resin 4030 White | CN0045 | 0 | 0.00% | | | | | | | | | | | | | |
| Epoxy Hardner MRSOL | CN0046 | 0 | 0.00% | | | | | | | | | | | | | |
| Styrene - (add to resin) | CN0002 | | 100.00% | | | | | 100.00% | 0.0000 | | | | | | | |
| Tinuvin | RM0008 | 129 | 100.00% | | 0.0217 | | | | | 40.00% | 0.0000 | | | | | |
| Initiator Norox MEKP-9H ⁴ | RM0012 | 391 | 100.00% | 0.04% | 0.0000 | | | | | | | | | | | |
| Surfactant (CoatOsil 7500) | RM0001 | 9 | 1.00% | | 0.0000 | | | | | | | | | | | |
| Accelerator (Westdry Cobalt 6%) | RM0003 | | 100.00% | | 0.0000 | | | | | | | | | | | |
| Accelerator (NL51 P) | RM0017 | 3 | 100.00% | | 0.0006 | | | | | | | | | | | |
| Accelerator (12% Cobalt Hex-Cem) | RM0025 | | 100.00% | | 0.0000 | | | | | | | 0.20% | 0.0000 | | | |
| Silane | RM0005 | 103 | 100.00% | | 0.0173 | | | | | | | | | | | |
| Tronox CR-826 | RM0020 | 1,150 | 2.00% | | 0.0039 | | | | | | | | | | | |
| Alcohol (IPA) (gallons X 6.8) | CN0057 | 36 | 100.00% | | 0.0180 | | | | | | | | | | | |
| Acrastrip (gallons X 8.6) | CN000100 | 43 | 60.00% | | 0.0128 | | | | | | | | | | | |
| Acetone | CN0001 | 0 | | | 100.00% | 0.00 | | | | | | | | | | |
| Monthly Total | | 38,490 | | | 0.3987 | | 0.0000 | | 0.3243 | | 0.0000 | | 0.0000 | | 0.0000 | 0.3243 |
| Year-To-Date Total | | 989,685 | | | 9.7902 | | 2.6420 | | 8.4179 | | 0.0003 | | 0.0009 | | 0.0000 | 8.4192 |
| 12 Month Rolling Total | | 1,097,425 | | | 10.7283 | | | | 9.2084 | | 0.0003 | | 0.0010 | | 0.0000 | 9.2078 |

Notes:

1. HAP emission rate was 35.88 lbs organic HAP/ton resin used from engineering test dates 12-08

2. Emission factor for Initiator VOC & DMP is 0.04%, see engineering calculations provided by AOC, resin supplier.

3. 22,800 pounds of styrene will be added to the general purpose resin. The styrene content of the resin was raised from 35.9% to 36.198% to account for the addition of the used styrene as a diluent.

4. According to the permit, page 13 of 19, "the limits in the table are not enforceable limits. The enforceable HAP limits are defined in 40 CFR 63 Subpart WWWWW. Table 3 in Subpart WWWWW for open molding - non-CR/HS, mechanical resin application the HAP emissions limit is 95 lbs/ton

*emission calculation for chemicals used in the enclosure - 32.6% are uncontrolled (vented to baghouse and mold cooling vent) and 67.4% are vented to RTO with 98.5% destruction efficiency based on the engineering test conducted December 2006

E-Stone USA Corporation

Facility-wide Monthly VOC & HAP Emissions
Controlled by 7000 scfm Crawford RTO

December-08

| Material | E-Stone Item Number | Material Usage (lbs) | VOC Content (%) | Emission Factor ¹ (%) | VOC Emissions (Tons) | VOC Content (%) | Emissions (Tons) | Styrene Content (%) | Styrene Emissions (Tons) | Dimethyl Phthalate Content (%) | Dimethyl Phthalate Emissions (Tons) | Methanol Content (%) | Methanol Emissions (Tons) | MIBK Content (%) | MIBK Emissions (Tons) | Total HAPs (Tons) |
|--------------------------------------|---------------------|----------------------|-----------------|----------------------------------|----------------------|-----------------|------------------|---------------------|--------------------------|--------------------------------|-------------------------------------|----------------------|---------------------------|------------------|-----------------------|-------------------|
| Resin & Styrene ² | RM0002 | 36,936 | 36.198% | 1.79% | 0.3306 | | | 36.198% | 0.3306 | | | | | | | |
| Epoxy Resin 4030 Transparent | CN0044 | 486 | 0.00% | | | | | | | | | | | | | |
| Epoxy Resin 4030 White | CN0045 | 0 | 0.00% | | | | | | | | | | | | | |
| Epoxy Hardner MR50L | CN0046 | 0 | 0.00% | | | | | | | | | | | | | |
| Styrene - (add to resin) | CN0002 | | 100.00% | | 0.0000 | | | 100.00% | 0.0000 | | | | | | | |
| Tinuvin | RM0006 | 149 | 100.00% | | 0.0251 | | | | | 40.00% | 0.0000 | | | | | |
| Initiator Norox MEKP-9H ² | RM0012 | 432 | 100.00% | 0.04% | 0.0000 | | | | | | | | | | | |
| Surfactant (CoatOsil 7500) | RM0001 | 7 | 1.00% | | 0.0000 | | | | | | | | | | | |
| Accelerator (Westdry Cobalt 6%) | RM0003 | | 100.00% | | 0.0000 | | | | | | | | | | | |
| Accelerator (NL51 P) | RM0017 | 4 | 100.00% | | 0.0006 | | | | | | | | | | | |
| Accelerator (12% Cobalt Hex-Cem) | RM0025 | | 100.00% | | 0.0000 | | | | | | | 0.20% | 0.0000 | | | |
| Silane | RM0005 | 119 | 100.00% | | 0.0200 | | | | | | | | | | | |
| Trionox CR-826 | RM0020 | 1,050 | 2.00% | | 0.0035 | | | | | | | | | | | |
| Alcohol (IPA) (gallons x 6.5) | CN0057 | 131 | 100.00% | | 0.0655 | | | | | | | | | | | |
| Acetone (gallons x 6.0) | CN000100 | 5 | 60.00% | | 0.0015 | | | | | | | | | | | |
| Acetone | CN0001 | 0 | | | | 100.00% | 0.00 | | | | | | | | | |
| Monthly Total: | | 39,320 | | | 0.4468 | | 0.0000 | | 0.3306 | | 0.0000 | | 0.0000 | | 0.0000 | 0.3306 |
| Year-To-Date Total: | | 1,038,906 | | | 10.2370 | | 2.6420 | | 8.7486 | | 0.0003 | | 0.0010 | | 0.0000 | 8.7486 |
| 12 Month Rolling Total: | | 1,038,906 | | | 10.2370 | | 2.6420 | | 8.7486 | | 0.0003 | | 0.0010 | | 0.0000 | 8.7486 |

Notes:

1. HAP emission rate was 35.88 lbs organic HAP/ton resin used from engineering test dates 12-06

2. Emission factor for initiator VOC & DMP is 0.04%, see engineering calculations provided by AOC, resin supplier.

3. 22,800 pounds of styrene will be added to the general purpose resin. The styrene content of the resin was raised from 35.9% to 36.198% to account for the addition of the used styrene as a diluent.

* According to the permit, page 13 of 19, "the limits in the table are not enforceable limits. The enforceable HAP limits are defined in 40 CFR 63 Subpart WWWWW. Table 3 in Subpart WWWWW for open molding - non-CR/HS, mechanical resin application the HAP emissions limit is 88 lb/ton.

*emission calculation for chemicals used in the enclosure - 32.6% are uncontrolled (vented to baghouse and mold cooling vent) and 67.4% are vented to RTO with 98.5% destruction efficiency based on the engineering test conducted December 2006

Attachment H
Potential Emissions
With Controls

E-Stone USA Corporation

Facility-wide Potential VOC & HAP Emissions
Controlled by 7000 scfm Crawford RTO

E-Stone's 5-Year Projection - based on 4,900,065 lbs of resin for both Line 1 and Line 2**

| Material | E-Stone Item Number | Material Usage (lbs) | VOC Content (%) | Emission Factor (%) | VOC Emissions (Tons) | VOS Content (%) | VOS Emissions (Tons) | Styrene Content (%) | Styrene Emissions (Tons) | Dimethyl Phthalate Content (%) | Dimethyl Phthalate Emissions (Tons) | Methanol Content (%) | Methanol Emissions (Tons) | Total HAPs (Tons) |
|--------------------------------|---------------------|----------------------|-----------------|---------------------|----------------------|-----------------|----------------------|---------------------|--------------------------|--------------------------------|-------------------------------------|----------------------|---------------------------|-------------------|
| Polyester Resin | RM0002 | 4,900,065 | 36.198% | 1.77% | 43.3656 | | | 36.198% | 43.3656 | | | | | |
| Epoxy Resin 4030 Transparent | CN0043 | 20,648 | 0.00% | | 0.0000 | | | | | | | | | |
| Epoxy Hardner MR50L | CN0046 | 10,240 | 0.00% | | 0.0000 | | | | | | | | | |
| Styrene | CN0002 | 0 | 100.00% | | 0.0000 | | | 100.00% | 0.0000 | | | | | |
| Tinuvin 328 | RM0006 | 17,437 | 100.00% | | 3.9348 | | | | | | | | | |
| Initiator Norox MEKP-9H | RM0012 | 54,163 | 100.00% | 0.04% | 0.0049 | | | | | 43.00% | 0.0021 | | | |
| Surfactant (CoatOsil 7500) | RM0001 | 1,398 | 1.00% | | 0.0032 | | | | | | | | | |
| Accelerator NL51-P | RM0017 | 439 | 100.00% | | 0.0991 | | | | | | | | | |
| Silane Silquest A174 NT | RM0005 | 14,047 | 100.00% | | 3.1719 | | | | | | | 0.20% | 0.0063 | |
| Titanium Dioxide Tronox CR-826 | RM0020 | 50,966 | 2.00% | | 0.2302 | | | | | | | | | |
| Isopropyl Alcohol | CN0057 | 2,350 | 100.00% | | 1.1750 | | | | | | | | | |
| Acetone | CN0001 | 18,771 | | | | 100.00% | 9.39 | | | | | | | |
| Yearly Total | | 5,090,524 | | | 51.9847 | | 9.3855 | | 43.3656 | | 0.0021 | | 0.0063 | 43.3740 |

Destruction efficiency measured 99.04% December 2008 → 55.37% of emissions vented to RTO with a destruction efficiency of 99.04% and 44.63% vented to duct collector with no controls

Emission Factor based on actual emissions taken from stack test 12-08 → 35.36 lbs of organic HAP/ton of resin used.

Allowable Limit is 88 lbs organic HAP/ton of resin used

**Polymerizing Line 2 is not in operation at this time. It must be tested and then E-Stone will apply for an operating permit amendment to include Line 2.

Attachment I
Potential Emissions
Before Controls

E-Stone USA Corporation

Facility-wide Potential VOC & HAP Emissions With No Controls

E-Stone's 5-Year Projection based on 4,900,065 lbs of resin

| Material | E-Stone Item Number | Material Usage (lbs) | VOC Content (%) | Emission Factor (%) | VOC Emissions (Tons) | VOS Content (%) | VOS Emissions (Tons) | Styrene Content (%) | Styrene Emissions (Tons) | Ethyl Phthaethyl Phtha Emissions (Tons) | Methanol Content (%) | Methanol Emissions (Tons) | Total HAPs (Tons) |
|-------------------------------|---------------------|----------------------|-----------------|---------------------|----------------------|-----------------|----------------------|---------------------|--------------------------|---|----------------------|---------------------------|-------------------|
| Polyester Resin see note | RM0002 | 4,900,065 | 36.198% | 4.03% | 98.7853 | | | 36.198% | 98.7853 | | | | |
| Epoxy Resin 4030 Trans | CN0043 | 20,648 | 0.00% | | 0.0000 | | | | | | | | |
| Epoxy Hardner MR50L | CN0046 | 10,240 | 0.00% | | 0.0000 | | | | | | | | |
| Styrene see note ³ | CN0002 | 0 | 100.00% | | 0.0000 | | | 100.00% | 0.0000 | | | | |
| Tinuvin 328 | RM0006 | 17,437 | 100.00% | | 8.7185 | | | | | | | | |
| Initiator Norox MEKP-9H | RM0012 | 54,163 | 100.00% | 0.04% | 0.0108 | | | | | 43.00% | 0.0047 | | |
| Surfactant (CoatOsil 750 | RM0001 | 1,398 | 1.00% | | 0.0070 | | | | | | | | |
| Accelerator NL51-P | RM0017 | 439 | 100.00% | | 0.2195 | | | | | | | 0.20% | 0.0140 |
| Silane Silquest A174 NT | RM0005 | 14,047 | 100.00% | | 7.0235 | | | | | | | | |
| Titanium Dioxide Tronox | RM0020 | 50,966 | 2.00% | | 0.5097 | | | | | | | | |
| Isopropyl Alcohol | CN0057 | 2,350 | 100.00% | | 1.1750 | | | | | | | | |
| Acetone | CN0001 | 18,771 | | | | 100.00% | 9.39 | | | | | | |
| Yearly Total: | | 5,090,524 | | | 116.4493 | | 9.3855 | | 98.7853 | | 0.0047 | | 0.0140 |
| | | | | | | | | | | | | | 98.8040 |

Notes:

1. Per CFR 40 Part 63 Subpart W W W W, 65.5799(b)(1) for non-atomized mechanical resin application, the calculated emission factor is 4.03% (calculation = ((0.157 x .36198)-.0165) x 2000 = 80.66 lbs styrene / ton resin = .0403 = 4.03%)
2. Emission factor for Initiator VOC & DMP is 0.04%, see engineering calculations provided by AOC, resin supplier.
3. 22,800 pounds of styrene will be added to the general purpose resin. The styrene content of the resin was raised from 35.9% to 36.198% to account for the addition of the used styrene as a diluent.

Attachment J
Summary of Criteria Pollutants

E-Stone Summary of Criteria Pollutants After Controls

| | Potential Emissions After Controls (TPY) | | | | | | Corresponding Control Equipment | Allowable Emissions |
|-----------------------------|--|--------------|---------------|---------------|---------------|----------------|---------------------------------|--|
| | CO | NOX | SOX | PM | PM10 | VOC | | |
| MILL #1 | | | | | | | | |
| Rotary dryer (fuel) | 0.2566 | 0.3055 | 0.0018 | 0.0092 | 0.0092 | 0.0168 | | Visible Emissions for all cyclones and baghouses shall not exceed 5% opacity |
| Crushing | | | | 0.6167 | 0.5175 | | DC 1 | |
| Drying | | | | 0.4091 | 0.2229 | | DC 1 | |
| Classifying | | | | 0.3435 | 0.1588 | | DC 1 | |
| sub-total for mill#1 | 0.2566 | 0.3055 | 0.0018 | 1.3786 | 0.9084 | 0.0168 | | |
| MILL #2 | | | | | | | | |
| Rotary dryer (fuel) | 0.2566 | 0.3055 | 0.0018 | 0.0092 | 0.0092 | 0.0168 | | Visible Emissions for all cyclones and baghouses shall not exceed 5% opacity |
| Crushing | | | | 0.6167 | 0.5175 | | DC 2 | |
| Drying | | | | 0.4091 | 0.2229 | | DC 2 | |
| Classifying | | | | 0.3435 | 0.1588 | | DC 2 | |
| sub-total for mill#2 | 0.2566 | 0.3055 | 0.0018 | 1.3786 | 0.9084 | 0.0168 | | |
| Polymerizing #1 | | | | | | | | |
| RTO (fuel) | 0.3679 | 0.438 | 0.0026 | 0.0131 | 0.0131 | 0.0241 | | 88 lbs/ton of HAP AND under 100 tpy HAP before controls Visible Emissions for all shall not exceed 5% opacity |
| Polymerization | | | | | | 17.33 | RTO | |
| Classifying -drop point 1 | | | | 0.229 | 0.106 | | DC 3 | |
| Classifying -drop point 2 | | | | 0.229 | 0.106 | | DC 3 | |
| Classifying -drop point 3 | | | | 0.229 | 0.106 | | DC 3 | |
| sub-total for poly. Line #1 | 0.3679 | 0.438 | 0.0026 | 0.7001 | 0.3311 | 17.3541 | | |
| Polymerizing #2 | | | | | | | | |
| RTO (fuel)** | | | | | | | | 88 lbs/ton of HAP AND under 100 tpy HAP before controls Visible Emissions for all shall not exceed 5% opacity |
| Polymerization | | | | | | 34.66 | RTO | |
| Classifying -drop point 4 | | | | 0.458 | 0.212 | | DC 6 | |
| Classifying -drop point 5 | | | | 0.458 | 0.212 | | DC 6 | |
| Classifying -drop point 6 | | | | 0.458 | 0.212 | | DC 4 | |
| sub-total for poly. Line #2 | 0 | 0 | 0 | 1.374 | 0.636 | 34.66 | | |
| Polishing Line #2 | | | | | | | | |
| 1 Oven | 0.4603 | 0.548 | 0.0033 | 0.0164 | 0.0164 | 0.0301 | DC 5 | Visible Emissions for all shall not exceed 5% opacity |
| 2 Dryers | 0.2251 | 0.268 | 0.0018 | 0.008 | 0.008 | 0.0147 | DC 5 | |
| Grinding edges of slabs | | | | 0.3 | 0.3 | | DC 5 | |
| sub-total for polishing #2 | 0.6854 | 0.816 | 0.0049 | 0.3244 | 0.3244 | 0.0448 | | |
| Facility-Wide (TPY) | 1.5665 | 1.865 | 0.0111 | 5.1555 | 3.1083 | 52.0925 | | |

**RTO fuel emission accounted for in polymerizing line 1

Emissions from combustion of natural gas for Rotary Dryer is based on operating 6106 hour/year

Emissions from combustion of natural gas for the RTO is based on operating 8760 hour/year

Emissions from combustion of natural gas for the ovens & dryers on polishing line2 are based on operating 8760 hour/year