

Title V
CRIST ELECTRIC
GENERATING

PLANT PERMIT
APPLICATION

Volume IV

EUS-5

SANDERS ENGINEERING & ANALYTICAL SERVICES, INC.

**PARTICULATE EMISSIONS TEST REPORT
STEADY STATE OPERATIONS**

FOR

GULF POWER COMPANY

*Plant Crist, Unit 4
Pensacola, Florida*



April 26, 1995

1568 LEROY STEVENS ROAD

MOBILE, ALABAMA 36695 • 205/633-4120



SANDERS ENGINEERING & ANALYTICAL SERVICES, INC.

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ENVIRONMENTAL ENGINEERING
AIR & WATER QUALITY MODELING
ENVIRONMENTAL ASSESSMENTS
PSD ANALYSIS
EMERGENCY RESPONSE MONITORING

AMBIENT AIR MONITORING
CONTINUOUS IN-STACK MONITORING
SOURCE TESTING
VISIBLE EMISSIONS TESTING
CONSULTING SERVICES

TEST REPORT CERTIFICATION

In regard to this test, we certify that to the best of our knowledge, all of the data regarding the testing performed by our agents is true and correct.

Dated: 5/5/95

Sanders Engineering & Analytical Services, Inc.

By: Edward R. Harris

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1. INTRODUCTION

Sanders Engineering & Analytical Services, Inc. (SEAS) performed a particulate emissions test during steady state operations at Gulf Power Company, Plant Crist, Unit 4, located in Pensacola, Florida. The testing was conducted on April 26, 1995. The testing was performed in accordance with the applicable U.S. EPA procedures specified at **40 CFR, Part 60, Appendix A, Methods 1, 2, 3, 4, and 17.**

The purpose of the test was to demonstrate compliance with the rules and regulations of the Florida Department of Environmental Protection, and to meet the necessary requirements contained in the permit to operate issued by the Florida Department of Environmental Protection.

The test was conducted by Mr. Edward Harris, Mr. John Wilson, and Mr. Dean Holmes of Sanders Engineering & Analytical Services, Inc., and was coordinated with Mr. John McPherson of Gulf Power Company. The Florida Department of Environmental Protection was notified so their representative could be present to observe the testing.

The test was conducted in accordance with the guidelines of the Florida Department of Environmental Protection. Further discussion of the test methods are included later in the report.

2. SUMMARY AND DISCUSSION OF RESULTS

The results of the particulate emissions test for the steady state runs, along with the results of the computations, are summarized in Table I. The equations used in the calculations of the results, along with the completed field data sheets for the testing, are presented in Appendix A. The sample calculations of the first run are presented in Appendix B. The quality control checks of the equipment used in the sampling program are included in Appendix C.

The results of the testing indicate the particulate emission rate during steady state for Plant Crist, Unit 4, is 0.012 LBS/MMBTU. The applicable Florida Department of Environmental Protection rules and regulations require an emission rate of no greater than 0.10 LBS/MMBTU. The results of the testing indicate that the unit is in compliance with the particulate emission condition of the permit to operate issued by the Florida Department of Environmental Protection.

**TABLE I. PARTICULATE EMISSIONS TEST RESULTS
GULF POWER COMPANY
PLANT CRIST, UNIT 4, STEADY STATE
4/28/95**

Title of Run		<u>RUN 1</u>	<u>RUN 2</u>	<u>RUN 3</u>
Sampling Time -Start	Military	0752	0918	1045
Sampling Time -Stop	Military	0858	1023	1151
F Factor	SDCF/BTU	9820	9820	9820
Plant Load	Megawatts	82.0	82.0	82.0
Static Pressure	In. H2O	-1.20	-1.20	-1.20
Barometric Pressure	In. Hg	30.21	30.21	30.21
Average dH	In. H2O	1.1	1.0	1.1
Meter correction		0.999	0.999	0.999
Avg. Meter Temp.	Deg. F	61.5	69.8	73.4
% O2	%	6.4	6.4	6.6
%CO2	%	12.0	11.5	11.5
Volume Metered	ACF	40.409	38.913	40.766
Volume Water	Ml	68.0	77.0	69.0
Sampling Time	Minutes	64	64	64
Nozzle Diameter	Inches	0.222	0.222	0.222
Avg. Stack Temp.	Deg. F	298.2	302.0	305.2
Area of Stack	Sq. Feet	92.1350	92.1350	92.1350
Wt. of Part.	Mg.	24.0	12.0	9.4
Number of Points		32	32	32
Avg. Sqrt dP	In. H2O	0.9029	0.8488	0.8926

RESULTS OF COMPUTATIONS

		<u>RUN 1</u>	<u>RUN 2</u>	<u>RUN 3</u>	<u>Average</u>
Volume of Gas Sampled	SDCF	41.362	39.193	40.794	40.450
H2O vapor in Gas Stream	PERCENT	7.2	8.5	7.4	7.7
Avg. Stack Gas Velocity	FT/SEC	60.1	56.9	59.8	58.9
Volumetric Flow Rate	SDCF/M	216193	200709	212613	209838
Volumetric Flow Rate	ACF/M	332214	314339	330439	325664
Particulate Conc.	Grs/SDCF	0.009	0.005	0.004	0.006
Particulate Conc.	Grs/ACF	0.006	0.003	0.002	0.004
Particulate Mass Rate	Lb/Hr	16.6	8.1	6.5	10.4
Particulate Mass Rate	Lb/MMBtu F Factor	0.018	0.010	0.007	0.012
Heat Input	MMBTU/Hr	916.44	850.80	888.83	885.36
Percent of Isokinetic	%	102.5	104.6	102.8	

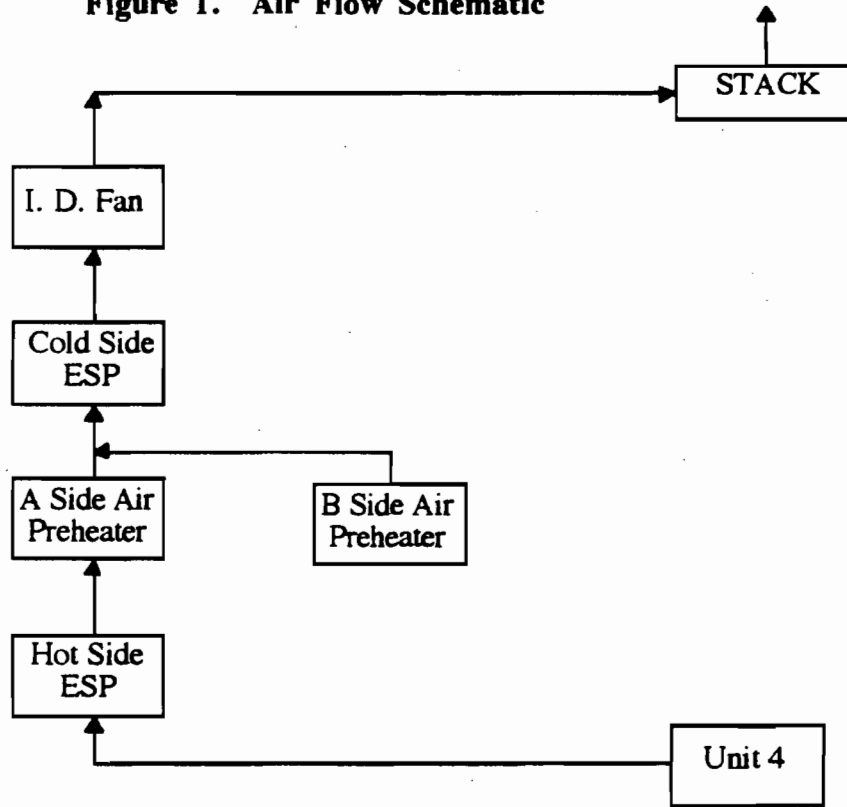
3. PROCESS DESCRIPTION

The process consists of a steam electric generating unit firing bituminous coal for the production of electric energy. The coal is received by barge, and loaded directly onto the conveyor feeding the plant, or onto the stockpile and later loaded onto the conveyor belt transporting the coal to the plant. The coal from the conveyor is loaded into bunkers capable of holding between 36 to 48 hours supply of coal. The coal is then fed to pulverizing mills before being fired in the unit through the burners. Upon combustion of the coal in the fire box, approximately 20 percent of the ash falls to the bottom of the boiler and is removed by the ash removal system. The remaining 80 percent exits with the flue gases through the heat exchange and economizer sections of the furnace, and is collected by electrostatic precipitators.

3.1. Source Air Flow

As shown in Figure I, the flue gases exit the boiler and flow through a hot side precipitator. The exhaust gases are separated into ducts A and B before entering air preheaters. The exhaust gases are combined before entering a cold side ESP. The flue gases exiting the cold side ESP are exhausted through a stack into the atmosphere.

Figure 1. Air Flow Schematic

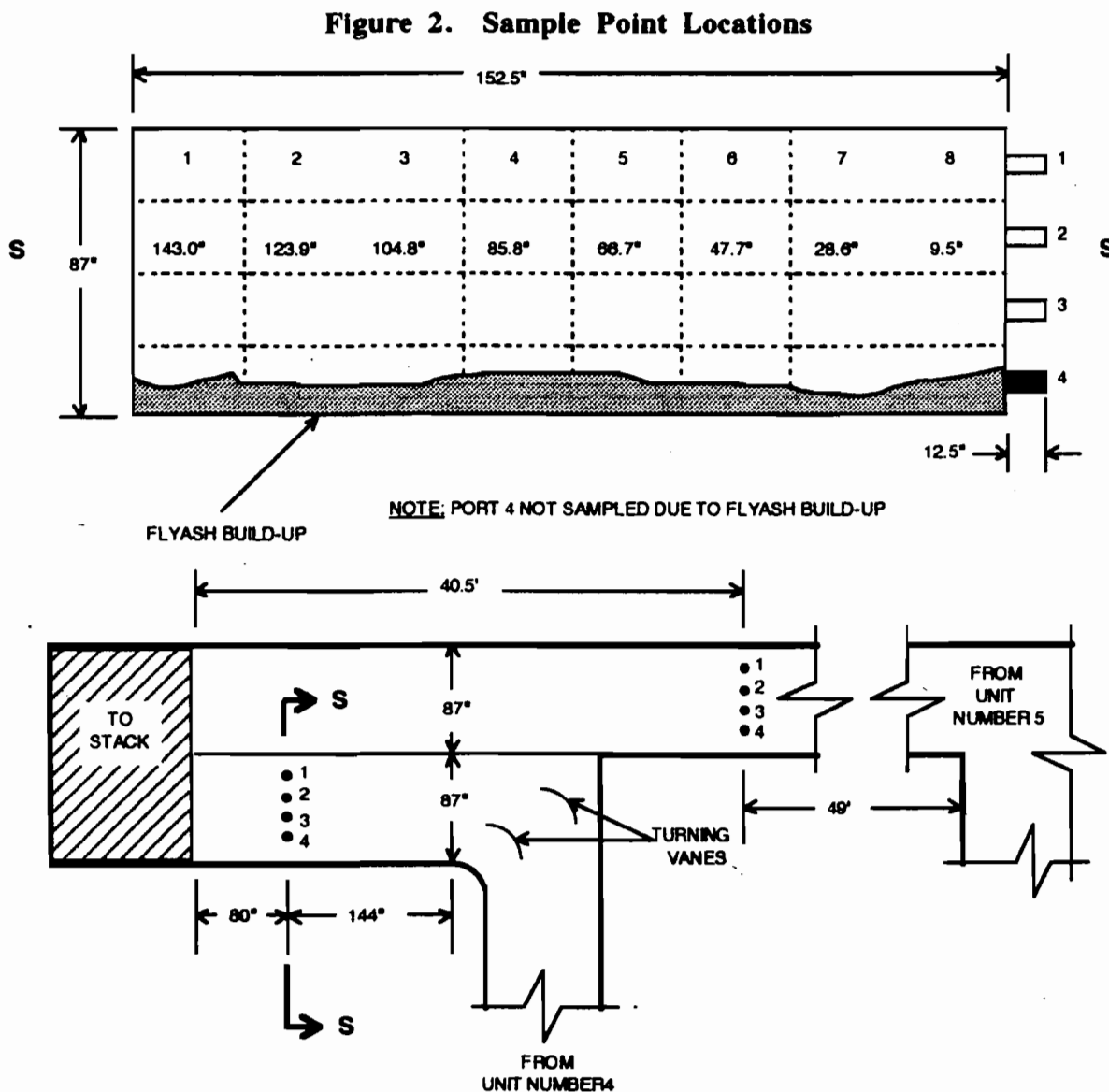


3.2. Operation During Testing

The average heat input during steady state operation, as based on F-factor calculations, was 885.36 million BTU per hour resulting in the production of approximately 82 megawatts of electricity. Precipitator data supplied by Gulf Power personnel is given in Appendix D.

4. SAMPLE POINT LOCATION

The sample point locations and outlet duct schematic are presented in Figure 2. Method 1 was used for determination of the number and location of sampling points. The minimum number of points (25) required for rectangular stacks was met by sampling a total of 32 points.

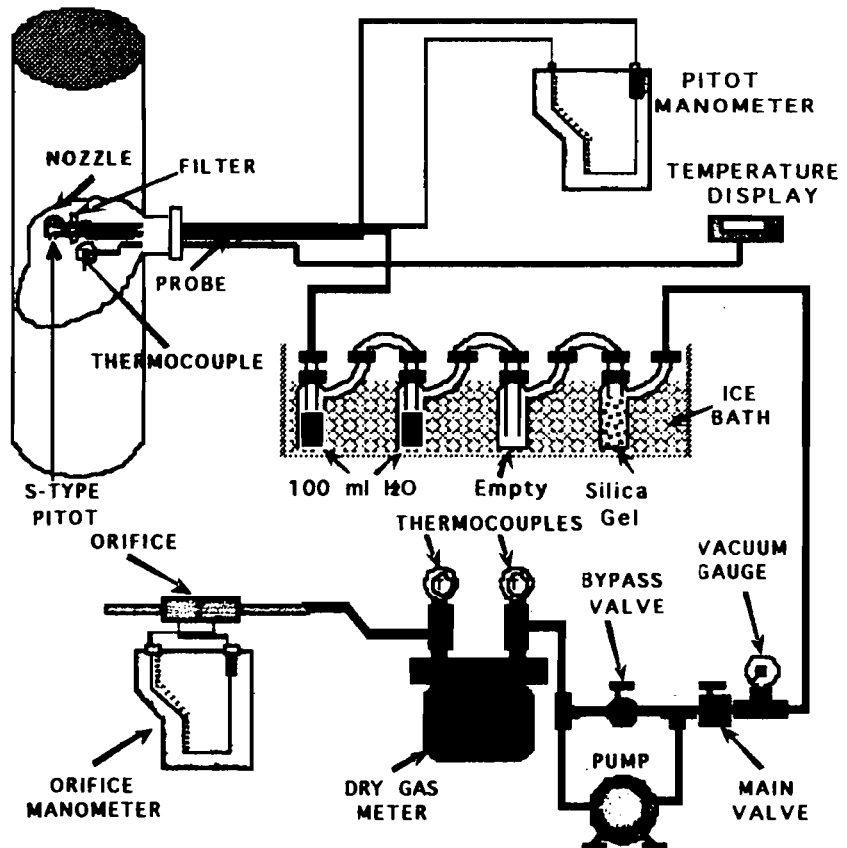


5. PARTICULATE SAMPLING PROCEDURE (EPA Method 17)

The sampling procedure utilized is that specified in 40 CFR, Part 60, Appendix A, Method 17, as modified by the governing regulatory agency. A brief description of this procedure is as follows:

The first impingers were partially filled with 100 milliliters of deionized water. The next impinger was left empty to act as a moisture trap. Preweighed 6 to 16 mesh indication silica gel was added to the last impinger. The sampling equipment manufactured by Lear Siegler (Model 100) or Sanders Engineering

Figure 3. Particulate Sampling Train



(Model 200) was assembled as shown in the attached drawing. The system was leak checked by plugging the inlet to the nozzle and pulling a 15 inch mercury vacuum. A leakage rate not in excess of 0.02 cubic feet per minute was considered acceptable.

The inside dimensions of the stack liner were measured and recorded. The required number of sampling points were marked on the probe for easy visibility. The range of velocity pressure, the percent moisture, and the temperature of the effluent gases were determined. From this data, the correct nozzle size and the nomograph multiplication factor were determined.

Crushed ice was placed around the impingers. The nozzle was placed on the first traverse point with the tip pointing directly into the gas stream. The pump was started immediately and the flow was adjusted to isokinetic sampling conditions. After the required time interval had elapsed, the probe was repositioned to the next traverse point and isokinetic sampling was re-established. This was performed for each point until the run was completed. Readings were taken at each point and recorded on the field data sheet. At the conclusion of each run, the pump was turned off and the final readings were recorded.

5.1. Particulate Sample Recovery

Care was exercised in moving the collection train to the sample recovery area to minimize the loss of collected sample, or the gain of extraneous particulate matter. The volume of water in the impingers was measured, the silica gel impinger was weighed and recorded on the field data sheet. The nozzle, and all sample-exposed surfaces were washed with reagent grade acetone into a clean sample container. A brush was used to loosen any adhering particulate matter and subsequent washings were placed into the container. The filter was carefully removed from the fritted support and placed in a clean separate sample container. A sample of the acetone used in the washing was saved for a blank laboratory analysis.

5.2. Particulate Analytical Procedures

The filter and any loose particulate matter were transferred from the sample container to a clean, tared weighing dish. The filter was placed in a desiccator for at least 24 hours and then weighed to the nearest 0.1 milligram until a constant weight was obtained. The original weight of the filter was deducted, and the weight gain was recorded to the nearest 0.1 milligram.

The wash solution was transferred to a clean, tared beaker. The solution was evaporated to dryness, desiccated to a constant weight, and the weight gain was recorded to the nearest 0.1 milligram.

APPENDIX A EQUATIONS AND FIELD DATA SHEETS

EQUATIONS

$$1. \quad P_s = P_{\text{bar}} + \frac{P_g}{13.6}$$

$$2. \quad P_m = P_{\text{bar}} + \frac{\overline{\Delta H}}{13.6}$$

$$3. \quad V_s = K_p C_p \sqrt{\overline{\Delta P}} \sqrt{\frac{\overline{T_s}}{M_s P_s}}$$

$$4. \quad V_{m(\text{Std})} = K_1 V_m Y \left[\frac{P_{\text{bar}} + \frac{\overline{\Delta H}}{13.6}}{\overline{T_m}} \right]$$

$$5. \quad V_{w(\text{Std})} = 0.04707 V_{lc}$$

$$6. \quad B_{ws} = \frac{V_{w(\text{Std})}}{V_{m(\text{Std})} + V_{w(\text{Std})}}$$

$$7. \quad M_d = 0.44 (\%CO_2) + 0.32 (\%O_2) + 0.28 (\%N_2 + \%CO)$$

$$8. \quad M_s = M_d (1 - B_{ws}) + 18 (B_{ws})$$

$$9. \quad EA = \left[\frac{(\%O_2 - 0.5 (\%CO))}{0.264 (\%N_2) - ((\%O_2) - 0.5 (\%CO))} \right] 100$$

$$10. \quad Q_a = (V_s) (A_s) (60)$$

$$11. \quad Q_s = Q_a (1 - B_{ws}) \frac{(528)}{\bar{T}_s} \frac{(P_s)}{29.92}$$

$$12. \quad E_H = \left(\frac{PMR}{H_I} \right)$$

$$13. \quad E = C_d F_{O_2} \left(\frac{20.9}{20.9 - \%O_2} \right)$$

$$14. \quad C_s = 0.0154 \frac{M_n}{V_{m(Std)}}$$

$$15. \quad C_{50} = \frac{21 C_s}{21 - [(1.5) (\%O_2) - 0.133 (N_2) - 0.75 (\%CO)]}$$

$$16. \quad C_{12} = \frac{C_s (12)}{\%CO_2}$$

$$17. \quad PMR = (C_s) (Q_s) \frac{(60)}{7000}$$

$$18. \quad V_n = \left[(0.002669) (V_{1c}) + \frac{V_m Y}{T_m} \left(p_{bar} + \frac{\bar{\Delta H}}{13.6} \right) \right] \frac{\bar{T}_s}{P_s}$$

$$19. \quad I = \frac{100 V_n}{(60) \phi V_s A_n}$$

NOMENCLATURE

- A_n = Cross-sectional area of nozzle, ft²
- A_s = Cross sectional area of stack, ft²
- B_{we} = Water vapor in the gas stream,
proportion by volume (dimensionless)
- C_p = Pitot tube coefficient (dimensionless) (0.84)
- C_s = Particulate concentration, grains/SDCF
- C_d = Particulate concentration, lbs/SDCF
- C_{12} = Particulate concentration (C_s adjusted to 12% CO)
grains/SDCF
- C_{50} = Particulate concentration (C_s adjusted to 50% excess air)
grains/SDCF
- EA = Excess air, %
- E = Emission in lb/mmBTU
- E_H = Emission in lb/mmBTU, based on heat input
- H_I = Total Heat Input, Million BTU per Hour (MMBTU/hr)
- I = Percent of isokinetic sampling
- K_1 = 17.64 °R/ inches Hg
- K_p = Pitot tube constant,
$$85.49 \text{ ft/sec} \left[\frac{(\text{lb/lb-mole}) (\text{in. Hg})}{(^\circ\text{R}) (\text{inc. H}_2\text{O})} \right]^{\frac{1}{2}}$$
- M_n = Total amount of particulate collected, mg'
- M_d = Molecular weight of stack gas; dry basis, lb/lb mole
- M_s = Molecular weight of stack gas; wet basis, lb/lb mole
- P_{bar} = Barometric pressure at the sampling site, in. Hg

NOMENCLATURE (continued)

- P_m = Meter pressure, in. Hg
- P_s = Absolute stack pressure, in. Hg
- P_g = Stack static pressure, in. H₂O
- PMR** = Particulate mass rate, lb/Hr
- Q_a = Volumetric flow rate ACFM
- Q_s = Volumetric flow rate SDCFM
- V_s = Average stack gas velocity, ft/sec
- V_{lc} = Total volume of liquid collected in impingers & silica gel, ml
- V_m = Volume of gas sample as measured by dry gas meter, ACF
- $V_{m(std)}$ = Volume of gas sample measured by dry gas meter,
corrected to standard conditions, SDCF
- $V_{w(std)}$ = Volume of water vapor in gas sample, corrected to standard
conditions, SCF
- V_n = Volume collected at stack conditions through nozzle, ACF
- Y = Dry gas meter calibration factor (dimensionless)
- ΔH = Average pressure difference of orifice, in. H₂O
- ΔP = Velocity head of stack gas, in. H₂O
- $\sqrt{\Delta P}$ = Average of square roots of the velocity pressure, in. H₂O
- \emptyset = Total sampling time, minutes
- $\%CO_2, \%O_2, N_2, \%CO$ - Number % by volume, dry basis, from gas analysis
- F_{O_2} = Oxygen based F factor (9820 SDCF/mmBTU for bituminous coal)
- T_s = Temperature of the stack, °R (°F + 460)



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FIELD DATA SHEET

COMPANY GPCO DATE 4/26/95 DGM# S-101
 PLANT Crist OPERATOR ELH ΔH_a 0.75
 UNIT #4 SS. METHOD 17 PROBE N/A 14'
liner length

RUN 1

NOZZLE CALIBRATION

PRE	POST	FILTER NUMBER
.222	.222	
.222	.222	
.222	.222	
.222	.222	
AVERAGE	AVERAGE	<u>612</u>

RUN 2

NOZZLE CALIBRATION

PRE	POST	FILTER NUMBER
.222	.222	
.222	.222	
.222	.222	
.222	.222	
AVERAGE	AVERAGE	<u>613</u>

RUN 3

NOZZLE CALIBRATION

PRE	POST	FILTER NUMBER
.222	.222	
.222	.222	
.222	.221	
.222	.222	
AVERAGE	AVERAGE	<u>614</u>

METER READING

<u>964.509</u>	FINAL
<u>924.100</u>	INITIAL
<u>40.409</u>	NET

METER READING

<u>1008.313</u>	FINAL
<u>969.400</u>	INITIAL
<u>38.913</u>	NET

METER READING

<u>49.366</u>	FINAL
<u>8.600</u>	INITIAL
<u>40.766</u>	NET

LEAK CHECK

SYSTEM		PITOT	
Pre	Post	Pre	Post
<u>15</u>	<u>10</u>	<input checked="" type="checkbox"/> impact	<input checked="" type="checkbox"/> impact
<u>0.000</u>	<u>0.000</u>	<input checked="" type="checkbox"/> static	<input checked="" type="checkbox"/> static
<small>in. hg</small>	<small>in. hg</small>		
<small>cfm</small>	<small>cfm</small>		

LEAK CHECK

SYSTEM		PITOT	
Pre	Post	Pre	Post
<u>75</u>	<u>10</u>	<input checked="" type="checkbox"/> impact	<input checked="" type="checkbox"/> impact
<u>0.000</u>	<u>0.000</u>	<input checked="" type="checkbox"/> static	<input checked="" type="checkbox"/> static
<small>in. hg</small>	<small>in. hg</small>		
<small>cfm</small>	<small>cfm</small>		

LEAK CHECK

SYSTEM		PITOT	
Pre	Post	Pre	Post
<u>15</u>	<u>10</u>	<input checked="" type="checkbox"/> impact	<input checked="" type="checkbox"/> impact
<u>0.000</u>	<u>0.000</u>	<input checked="" type="checkbox"/> static	<input checked="" type="checkbox"/> static
<small>in. hg</small>	<small>in. hg</small>		
<small>cfm</small>	<small>cfm</small>		

VOLUME OF LIQUID WATER COLLECTED

IMP. 1	IMP. 2	IMP. 3	IMP. 4
<u>158</u>	<u>100</u>	<u>0</u>	<u>1475.0</u>
<u>100</u>	<u>100</u>	<u>0</u>	<u>1465.0</u>
<u>58</u>	<u>0</u>	<u>0</u>	<u>10.0</u>
NET	NET	NET	NET
			TOTAL <u>68.0</u>

VOLUME OF LIQUID WATER COLLECTED

IMP. 1	IMP. 2	IMP. 3	IMP. 4
<u>168</u>	<u>100</u>	<u>0</u>	<u>1385.0</u>
<u>100</u>	<u>100</u>	<u>0</u>	<u>1376.0</u>
<u>68</u>	<u>100</u>	<u>0</u>	<u>9.0</u>
NET	NET	NET	NET
			TOTAL <u>77.0</u>

VOLUME OF LIQUID WATER COLLECTED

IMP. 1	IMP. 2	IMP. 3	IMP. 4
<u>164</u>	<u>100</u>	<u>0</u>	<u>1480.0</u>
<u>100</u>	<u>100</u>	<u>0</u>	<u>1476.0</u>
<u>64</u>	<u>0</u>	<u>0</u>	<u>5.0</u>
NET	NET	NET	NET
			TOTAL <u>69.0</u>

GAS ANALYSIS

O ₂ <u>6.4%</u>	STATIC <u>-1.20</u>
CO ₂ <u>12.0%</u>	BAROMETRIC <u>30.21</u>
CO <u>-</u>	<small>in. hg</small>

GAS ANALYSIS

O ₂ <u>6.4%</u>	STATIC <u>-1.20</u>
CO ₂ <u>11.5%</u>	BAROMETRIC <u>30.21</u>
CO <u>-</u>	<small>in. hg</small>

GAS ANALYSIS

O ₂ <u>6.6%</u>	STATIC <u>-1.20</u>
CO ₂ <u>11.5%</u>	BAROMETRIC <u>30.21</u>
CO <u>-</u>	<small>in. hg</small>

PORT #	POINT #	TIME	GAS METER VOL. (cu. ft.)	VEL. HEAD ΔP in. H ₂ O	ORIFICE HEAD ΔH in. H ₂ O	TEMPERATURE °F					VAC. in. H _g	
						STACK	PROBE	HOT BOX	IMP.	GAS METER		
									IN	OUT		
1 -	1	7:52	924.100	1.20	1.58	299	N/A	N/A	50	58	58	5
	2	:54	925.500	1.20	1.58	299			✓	58	58	4.5
	3	:56	926.900	1.06	1.39	298			✓	59	59	4
	4	:58	928.300	1.0	1.31	298			✓	59	59	4
	5	8:00	929.600	1.0	1.31	298			✓	59	59	4
	6	:02	931.100	0.78	1.02	297			47	60	59	3
	7	:04	932.350	0.75	0.98	298			✓	60	59	3
	8	:06	933.600	0.76	1.00	297			✓	60	59	3
1 -	1	:08	934.850	1.35	1.77	298			✓	60	59	5
	2	:10	936.200	0.99	1.30	298			✓	60	59	4
	3	:12	937.800	1.05	1.38	298	N/A	N/A	✓	60	60	4
	4	:14	939.100	1.09	1.43	298			✓	61	61	4.5
	5	:16	940.500	0.86	1.13	297			✓	61	61	4
	6	:18	941.900	0.75	0.98	298			✓	61	61	3
	7	:20	943.000	0.75	0.98	298			50	61	61	3
	8	:22	944.100	0.72	0.94	297			✓	61	61	3
2 -	1	8:25	945.492	0.96	1.26	298			✓	62	62	4
	2	:27	946.700	0.87	1.14	298			✓	62	62	4
	3	:29	948.000	1.09	1.43	299			✓	62	62	5
	4	:31	949.400	0.92	1.21	299			✓	62	62	4
	5	:33	950.750	0.75	0.98	299			✓	63	62	3.5
	6	:35	952.000	0.70	0.92	299			✓	63	62	3.5
	7	:37	953.250	0.60	0.79	299			50	64	63	3.0
	8	:39	954.350	0.69	0.91	298			✓	64	63	3.5

CHECK INDICATES TEMPERATURES MEET REQUIRED LIMITS.

COMPANY GPO DATE 4/26/95
 SITE Cist #4 S.S. RUN # 1 PAGE 2 OF 7

PORT #	POINT #	TIME	GAS METER VOL. (cu. ft.)	VEL. HEAD ΔP in. H ₂ O	ORIFICE HEAD ΔH in. H ₂ O	TEMPERATURE °F					VAC. in. H _g	
						STACK	PROBE	HOT BOX	IMP.	GAS METER		
										IN		OUT
3-	1	9:18	969.400	0.69	0.91	300	N/A	N/A	50	67	67	2
	2	:20	970.500	0.70	0.93	300			✓	67	67	2
	3	:22	971.750	0.45	0.59	301			✓	67	67	2
	4	:24	972.800	0.43	0.57	301			✓	67	67	2
	5	:26	973.800	0.55	0.73	301			✓	68	68	2
	6	:28	974.950	0.60	0.79	302			✓	68	68	2
	7	:30	976.000	0.60	0.79	301			✓	68	68	2
	8	:32	977.100	0.73	0.97	299			49	68	68	3
3-	1	:34	978.250	0.71	0.94	299			✓	69	69	3
	2	:36	979.400	0.60	0.79	301			✓	69	69	3
	3	:38	980.600	0.49	0.65	301			✓	69	69	2
	4	:40	981.600	0.45	0.59	301			✓	69	69	2
	5	:42	982.600	0.61	0.81	302			✓	70	69	2.5
	6	:44	983.800	0.58	0.77	302			✓	70	70	2.5
	7	:46	984.800	0.55	0.73	301			✓	70	70	2.5
	8	9:48	985.900	0.63	0.83	300			✓	70	70	3
2-	1	9:51	987.088	0.83	1.10	303			✓	70	70	3.5
	2	:53	988.300	0.95	1.26	303			52	70	70	4
	3	:55	989.600	1.0	1.33	304			✓	70	70	4
	4	:57	991.100	0.78	1.03	303			✓	70	70	4
	5	:59	992.500	0.74	0.98	303			✓	71	70	4
	6	10:01	993.700	0.65	0.86	303			✓	71	70	3
	7	:03	994.800	0.65	0.86	302			✓	71	71	3
	8	10:05	996.000	0.71	0.94	302			✓	71	71	3.5

CHECK INDICATES TEMPERATURES MEET REQUIRED LIMITS.

COMPANY GPCO DATE 4/26/95
 SITE Crist #4 SS. RUN # 2 PAGE 4 OF 7

PORT #	POINT #	TIME	GAS METER VOL. (cu. ft.)	VEL. HEAD ΔP in. H ₂ O	ORIFICE HEAD ΔH in. H ₂ O	TEMPERATURE °F					VAC. in. H _g	
						STACK	PROBE	HOT BOX	IMP.	GAS METER		
										IN		OUT
1-	1	10:45	8.600	1.55	2.04	306	N/A	N/A	50	72	72	7
	2	:47	10.300	1.14	1.50	305			✓	72	72	5
	3	:49	11.900	1.15	1.51	306			✓	72	72	5
	4	:51	13.300	1.03	1.34	306			✓	73	72	5
	5	:53	14.800	1.08	1.48	306			✓	73	72	5
	6	:55	16.400	0.71	0.92	306			✓	73	72	4
	7	:57	17.500	0.67	0.87	305			✓	73	73	3.5
	8	:59	18.800	0.64	0.83	305			✓	73	73	3
2-	1	11:02	19.810	1.25	1.63	305			✓	73	73	5
	2	:04	21.400	1.0	1.30	306			47	73	72	5
	3	:06	22.700	1.04	1.36	306			✓	73	72	5
	4	:08	24.300	0.80	1.04	306			✓	74	73	4
	5	:10	25.500	0.75	0.98	305			✓	74	73	4
	6	:12	26.600	0.61	0.79	305			✓	74	74	3
	7	:14	27.800	0.55	0.72	305			✓	74	74	3
	8	:16	28.900	0.72	0.94	303			✓	74	74	4
2-	1	11:18	30.100	1.28	1.68	305			✓	74	74	6
	2	:20	31.600	0.85	1.11	305			✓	74	74	5
	3	:22	33.000	1.05	1.38	306			49	74	73	5
	4	:24	34.300	0.79	1.03	306			✓	74	73	4
	5	:26	35.500	0.74	0.97	306			✓	74	74	4
	6	:28	36.700	0.63	0.82	306			✓	74	73	4
	7	:30	37.850	0.60	0.78	305			✓	74	73	3
	8	:32	39.100	0.70	0.92	304			✓	74	74	4

CHECK INDICATES TEMPERATURES MEET REQUIRED LIMITS.

COMPANY GPCO DATE 4/26/95
 SITE Crist #4 S.S. RUN # 3 PAGE 6 OF 7

LABORATORY ANALYSIS & CHAIN OF CUSTODY

COMPANY/PLANT: Gulf Power / Crist

UNIT #: 4 DATE OF TEST: 4/25 - 4/26/95 TYPE OF TEST: M-5 M-17 OTHER _____

SAMPLE #	RELINQUISHED BY	RECEIVED BY	TIME	DATE	REASON FOR CHANGE
609	Wash				
610	Wash				
611	Wash				
612	Wash				
613	Wash				
614	Wash				

UNIT # 4 Soot Blow
UNIT # 4 Steady State

RUN # <u>1</u>	FILTER # <u>609</u>	BEAKER # <u>3</u>	WASH (ML) <u>45</u>
FINAL WEIGHT	134.40 mg	64480.8 mg	
INITIAL WEIGHT	122.3 mg	64477.5 mg	
DIFFERENCE	12.1	3.3	
CORRECTED TOTAL WEIGHT		15.4	
RUN # <u>2</u>	FILTER # <u>610</u>	BEAKER # <u>6</u>	WASH (ML) <u>40</u>
FINAL WEIGHT	132.30 mg	68390.9 mg	
INITIAL WEIGHT	123.6 mg	68389.2 mg	
DIFFERENCE	8.7	1.7	
CORRECTED TOTAL WEIGHT		10.4	
RUN # <u>3</u>	FILTER # <u>611</u>	BEAKER # <u>21</u>	WASH (ML) <u>50</u>
FINAL WEIGHT	131.0 mg	70058.8 mg	
INITIAL WEIGHT	123.2 mg	70056.6 mg	
DIFFERENCE	7.8	2.2	
CORRECTED TOTAL WEIGHT		10.0	
RUN # _____	FILTER # _____	BEAKER # _____	WASH (ML) _____
FINAL WEIGHT			
INITIAL WEIGHT			
DIFFERENCE			
CORRECTED TOTAL WEIGHT			

RUN # <u>1</u>	FILTER # <u>612</u>	BEAKER # <u>32</u>	WASH (ML) <u>60</u>
FINAL WEIGHT	142.20 mg	64728.3 mg	
INITIAL WEIGHT	121.7 mg	64724.8 mg	
DIFFERENCE	20.5	3.5	
CORRECTED TOTAL WEIGHT		24.0	
RUN # <u>2</u>	FILTER # <u>613</u>	BEAKER # <u>35</u>	WASH (ML) <u>60</u>
FINAL WEIGHT	131.4 mg	68566.2 mg	
INITIAL WEIGHT	122.1 mg	68563.5 mg	
DIFFERENCE	9.3	2.7	
CORRECTED TOTAL WEIGHT		12.0	
RUN # <u>3</u>	FILTER # <u>614</u>	BEAKER # <u>36</u>	WASH (ML) <u>65</u>
FINAL WEIGHT	129.4 mg	67936.9	
INITIAL WEIGHT	122.1 mg	67934.8 mg	
DIFFERENCE	7.3	2.1	
CORRECTED TOTAL WEIGHT		9.4	
WASH SOLVENT BLANK (ML) _____		BEAKER # <u>47</u>	WASH (ML) <u>100</u>
FINAL WEIGHT		68998.9 mg	
INITIAL WEIGHT		68998.9 mg	
DIFFERENCE		0.0	
CORRECTION FACTOR (MG/ML)			

ALL WEIGHTS ARE IN MILLIGRAMS (MG)

APPENDIX B SAMPLE CALCULATIONS

Input and Constants

```

          3
    9820 ft
f := -----
      mm btu

pg := -(1.2 in. H2O)
pbar := 30.21 in. Hg.
Δhavg := 1.1 in. H2O
y := 0.999
tm := 61.5 °F
o2 := 6.4
co2 := 12.

          3
vm := 40.409 ft
vlc := 68. ml
theta := 64 min
nozdia := 0.222 in.
ts := 298.2 °F

          2
as := 92.135 ft
mn := 24. mg
numberofpoints := 32

          0.5
sqrtΔp := 0.9029 in. H2O

          lb in. Hg.    0.5
      85.49 1 ft 1 (-----)
          lb-mole °R in. H2O
kp := -----
          1 sec

cp := 0.84

      17.64 °R
k1 := -----
      in. Hg.

```

$$t_s = \frac{(t_s + 460 \text{ } ^\circ\text{F}) \text{ } ^\circ\text{R}}{\text{ } ^\circ\text{F}}$$

758.2 °R

$$t_m = \frac{(t_m + 460 \text{ } ^\circ\text{F}) \text{ } ^\circ\text{R}}{\text{ } ^\circ\text{F}}$$

521.5 °R

$$n_2 = 100 - o_2 - co_2$$

81.6

$$a_n = \frac{\text{nozdia } 3.1416}{\frac{12 \text{ in. }^2}{4 \text{ (-----)}} \text{ ft}}$$

0.000268803 ft²

Calculations

Equation 1

$$p_s = p_{bar} + \frac{\rho g}{13.6 \text{ in. H}_2\text{O}} \times 1 \text{ in. Hg.}$$

30.1218 in. Hg.

Equation 2

$$p_m = p_{bar} + \frac{\Delta h_{avg}}{13.6 \text{ in. H}_2\text{O}} \times \text{in. Hg.}$$

30.2909 in. Hg.

Equation 3

$$k_1 v_m y \left(p_{bar} + \frac{\Delta h_{avg}}{13.6 \text{ in. H}_2\text{O}} \right) \times \text{in. Hg.}$$

$$v_{mstd} = \frac{\text{-----}}{t_m}$$

41.3618 ft³

Equation 4

$$v_{wstd} = \frac{0.04707 \text{ ft}^3 v_{lc}}{m_l}$$

3.20076 ft³

Equation 5

$$b_{ws} = \frac{v_{wstd}}{v_{mstd} + v_{wstd}}$$

0.0718262

Equation 6

$$md = \frac{(0.44 \text{ co}_2 + 0.32 \text{ o}_2 + 0.28 \text{ n}_2) \text{ lb}}{\text{lb-mole}}$$

$$\frac{30.176 \text{ lb}}{\text{lb-mole}}$$

Equation 7

$$ms = md (1 - bws) + \frac{bws \text{ 18 lb}}{\text{lb-mole}}$$

$$\frac{29.3014 \text{ lb}}{\text{lb-mole}}$$

Equation 8

$$vs = kp \text{ cp } \sqrt{\Delta p} \left(\frac{ts \text{ 0.5}}{ms \text{ ps}} \right)$$

$$\frac{60.0954 \text{ ft}}{\text{sec}}$$

Equation 9

$$qa = \frac{vs \text{ as } 60 \text{ sec}}{\text{min}}$$

$$\frac{332214. \text{ ft}^3}{\text{min}}$$

Equation 10

$$qs = \frac{qa (1 - bws) 528 \text{ }^\circ\text{R ps}}{ts \text{ 29.92 in. Hg.}}$$

$$\frac{216180. \text{ ft}^3}{\text{min}}$$

Equation 11

$$cs = \frac{0.0154 \text{ gr mn}}{\text{mg vmstd}}$$

$$\frac{0.00893577 \text{ gr}}{\text{ft}^3}$$

Equation 12

$$pmr = \frac{cs \text{ qs } 60 \text{ min}}{\text{hour} \frac{7000 \text{ gr}}{\text{lb}}}$$

$$\frac{16.5577 \text{ lb}}{\text{hour}}$$

Equation 13

$$e = \frac{cs \text{ f } 20.9 \text{ } 1 \text{ lb}}{(20.9 - o_2) 7000 \text{ gr}}$$

$$\frac{0.0180686 \text{ lb}}{\text{mm btu}}$$

Equation 14

$$vn = \frac{ts \left(\frac{0.002669 \text{ in. Hg. ft}^3 \text{ vlc}}{\text{ml } ^\circ\text{R}} + \frac{\text{vm y pm}}{\text{tm}} \right)}{\text{ps}^3}$$

$$63.5891 \text{ ft}^3$$

Equation 15

$$i = \frac{100 \% \text{ vn}}{60 \text{ sec theta vs an}} \text{ min}$$

102.512 %

Equation 16

$$hi = \frac{\text{par}}{e} \text{ hour}$$

916.383 mm btu

APPENDIX C QUALITY CONTROL

**INITIAL
METER CALIBRATION FORM - DGM**

DATE: 12-27-94 Box No. S-101

Ref. DGM Ser. #	1044456	Calibrated By			EDWARD HARRIS	
RUN #		1	2	3	4	5
DELTA H (DGM)	0.50	1.00	1.50	2.00	2.50	
Y (Ref. DGM)	0.985	0.985	0.985	0.985	0.985	
Reference DGM						
Gas Vol. Initial	973.200	979.920	985.000	990.895	996.540	
Gas Vol. Final	979.920	985.000	990.895	996.540	1003.024	
Meter Box DGM						
Gas Vol. Initial	878.100	884.800	889.855	895.700	901.300	
Gas Vol. Final	884.800	889.855	895.700	901.300	907.700	
Reference DGM						
Temp.		Avg.	Avg.	Avg.	Avg.	Avg.
Deg F Initial		44	49	54	57	57
Deg F Final		49	49	57	57	57
Meter Box DGM						
Temp. Initial In	43	47	50	54	54	
Temp. Initial Out	43	47	50	54	54	
Temp. Final In	47	47	54	54	54	
Temp. Final Out	47	47	54	54	54	
P Bar IN: Hg	30.20	30.20	30.20	30.20	30.20	
Time (sec.)	959	527	502	416	432	
Meter Calibration						
Factor (Y)	0.999	0.999	0.998	0.997	1.001	
Qm (C.F.M.)	0.442	0.606	0.729	0.839	0.928	
Km (Std Pressure)	0.825	0.797	0.779	0.777	0.769	
DELTA Ha	1.51	1.60	1.65	1.65	1.68	
Average Y (Meter Calibration Factor)				0.999		
Average Km (Standard Pressure)				0.789		
Average DELTA Ha of Orifice				1.617		

Y = \leq .03
Max & Min \leq .02 from Avg
Final Avg within 5% of Initial Avg
 Δ Ha = Max & Min \leq .2 from Avg

**FINAL
METER CALIBRATION FORM - DGM**

DATE:	05-05-95	Box No.	S-101
Ref. DGM Ser. #	1044453	Calibrated By	Edward Harris
RUN #	1	2	3
DELTA H (DGM)	1.5	1.5	1.5
Y (Ref. DGM)	0.995	0.995	0.995
Reference DGM			
Gas Vol. Initial	716.400	722.300	728.395
Gas Vol. Final	722.300	728.395	735.398
Meter Box DGM			
Gas Vol. Initial	778.600	784.484	790.565
Gas Vol. Final	784.484	790.565	797.520
Reference DGM			
Temp.	Avg.	Avg.	Avg.
Deg F Initial	79	79	80
Deg F Final	79	79	80
Meter Box DGM			
Temp. Initial In	80	80	80
Temp. Initial Out	80	80	80
Temp. Final In	80	80	80
Temp. Final Out	80	80	80
P Bar IN. Hg	30.10	30.10	30.10
Time (sec.)	488	506	580
Meter Calibration			
Factor (Y)	0.996	0.995	0.998
Qm (C.F.M.)	0.711	0.709	0.709
Km (Std Pressure)	0.740	0.737	0.738
DELTA Ha	1.63	1.64	1.64
Average Y (Meter Calibration Factor)			0.997
Initial Y (Meter Calibration Factor)			0.999
Percent Error			0.20%
Average Km (Standard Pressure)			0.738
Average DELTA Ha of Orifice			1.64

MAGHELIC CALIBRATION

BOX	173	S101	173	S-318	C-133
SER. NO.	R01126 YC2	R-22D	R20208 A617	R74D	91126A M91
RANGE	0-2	0-2	0-2	0-5	0-2
REFERENCE READING	FIELD DEVICE READING				
0.000	0.00	0.00	0.00	0.00	0.00
0.050					
0.150					
0.200					
0.250					
0.450					
0.50	0.49	0.50			0.500
1.00	1.00	0.97			1.000
1.30					
1.80	1.77	1.77			1.83
2.50					
4.50					
5.0					
9.0					
13.0					
22.0					

SIGNATURE: Edward A. Harris

DATE: 12/23/94

MAGEHELIC CALIBRATION

BOX	460	S-100	2879
SER. NO.	91127W W137		R-33D
RANGE	0-2	0-2	0-2
REFERENCE READING	FIELD DEVICE READING		
0.000	0.00	0.00	0.00
0.050			
0.150			
0.200			
0.250			
0.450			
0.50	0.50	0.52	0.51
1.00	1.00	1.02	1.00
1.30			
1.80	1.83	1.83	1.77
2.50			
4.50			
5.0			
9.0			
13.0			
22.0			

SIGNATURE:

Edmond L. Kloss

DATE:

12/27/74

MAGEHELIC CALIBRATION
BOX #1

SER. NO.	10720- AB68	R1061- 6AG48	RS031- SE376	R1062- 9JA82	R1051- 3MR42	R90124 RI119
RANGE	0-0.25	0-0.50	0-2	0-5	0-10	0-25
REFERENCE READING	FIELD DEVICE READING					
0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.050	0.050					
0.150	0.150	0.150				
0.200	0.200					
0.250		0.250				
0.450		0.450				
0.50			0.50			
1.00			1.00			
1.30				1.30		
1.80			1.80			
2.50				2.50	2.5	
4.50				4.50		
5.0					5.0	5.0
9.0					9.0	
13.0						14.0
22.0						21.0

SIGNATURE:

Edward L. Klaus

DATE:

12/22/92

MAGEHELIC CALIBRATION
BOX #2

SER. NO.	10819-DR2	R1090-2AG18	R50315-EB93	R1062-9TA87	30830-AM79	R1072-2MCS
RANGE	0-0.25	0-0.50	0-2	0-5	0-10	0-25
REFERENCE READING	FIELD DEVICE READING					
0.000	0.000	0.000	0.00	0.00	0.0	0.0
0.050	0.058					
0.150	0.161	0.151				
0.200	0.210					
0.250		0.255				
0.450		0.450				
0.50			0.51			
1.00			1.02			
1.30				1.32		
1.80			1.82			
2.50				2.61	2.6	
4.50				4.52		
5.0					5.0	5.2
9.0					8.9	
13.0						13.0
22.0						21.7

SIGNATURE:

Edward L. Harris

DATE:

12/22/91

Best Available Copy

MAGEHELIC CALIBRATION
BOX #3

SER. NO.	R900723	R0112642	R10608
	MRR1		CF20
RANGE	0-0.50	0-2.0	0-10
REFERENCE READING	FIELD DEVICE READING		
0.000	0.001	0.00	0.0
0.050			
0.150	0.15		
0.200			
0.250	0.240		
0.450	0.450		
0.50		0.52	
1.00		1.00	
1.50			
1.80		1.85	
2.50			2.5
4.50			
5.0			5.0
9.0			9.2
13.0			
22.0			

SIGNATURE:

Edward R. Harris

DATE:

10/27/94

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MAGEHELIC CALIBRATION

BOX #4

SER. NO.	R22D	R90051 6GT21	R90101 5CD102
RANGE	0-0.50	0-5	0-25
REFERENCE READING	FIELD DEVICE READING		
0.000	0.000	0.00	0.0
0.050			
0.150	0.154		
0.200			
0.250	0.256		
0.450	0.455		
0.50			
1.00			
1.30		1.32	
1.80			
2.50		2.55	
4.50		4.59	
5.0			5.0
9.0			
13.0			13.0
22.0			22.0

SIGNATURE:

[Handwritten Signature]

DATE:

12/02/24

TEMPERATURE CALIBRATIONS - DEGREES FAHRENHEIT

REFERENCE DEVICE READING*	0 DEG. F	210 DEG.	420 DEG.	630 DEG.	840 DEG.	1050 DEG.	1260 DEG.	1470 DEG.	1680 DEG.	1900 DEG.
2879	-2	209	420	629	838	1049	1259	1469	1679	1899
METER BOX #1 C-133 11580	0	209	416	624	833	1044	1255	1462	1674	1900
METER BOX #3 C-173 811-24										
METER BOX #2 C-175 15982	0	208	417	628	839	1052	1265	1474	1678	1905
METER BOX #4 D-460 15751	0	206	417	624	839	1057	1273	1486	1690	1903
METER BOX #5 S-100 15751	-2	203	412	622	837	1055	1272	1484	1690	1900
METER BOX #8 S-101 15751	0	209	416	624	833	1045	1255	1463	1679	1904
PORTABLE THERMOCOUPLE # 1 (Yellow)	0	210	419	632	840	1050	1260	1470	1680	1900
PORTABLE THERMOCOUPLE # 2 (Blue)	0	209	416	625	839	1055	1270	1480	1684	1891
PORTABLE THERMOCOUPLE # 2 (Green)										
PINK T83658	0	209	417	629	843	1060	1275	1490	1693	1903

DATE: 12-27-94

SIGNATURE: *Edward R. Harris*

* Reference Device is an Omega Engineering CL505-A calibrated reference thermocouple-potentiometer system.

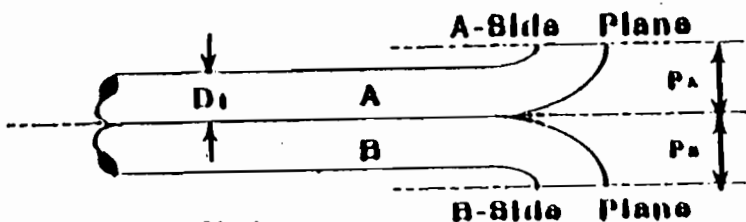
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SANDERS ENGINEERING & ANALYTICAL SERVICES, Inc.

1500 Leroy Stevens Rd. Office: (205) 833-4120
 Mobile, Al. 36686 FAX#: (205) 833-2285

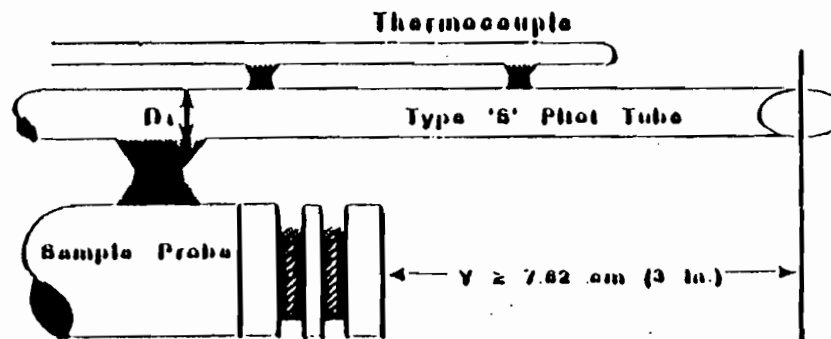
The Pilot used was within the following geometric specifications:
 D_i between 0.48 and 0.65 cm (3/16 and 3/8 in.)
 $G_p = 0.84$



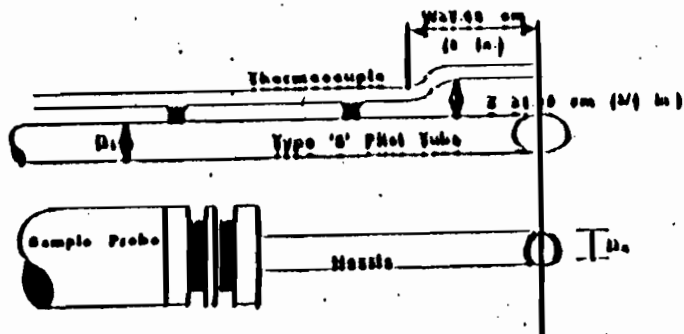
Note:

$1.05 D_i \leq 1.50 D_i$

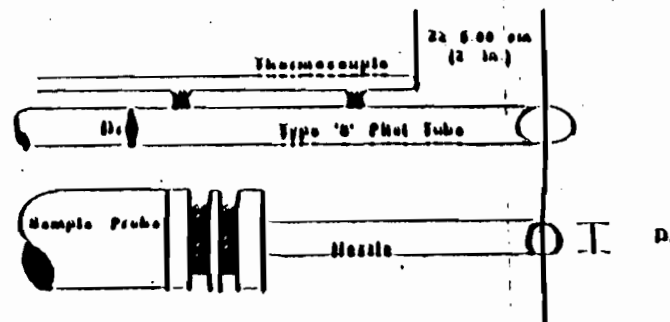
$P_A = P_B$



Minimum pilot-sample probe separation needed to prevent interference



OR



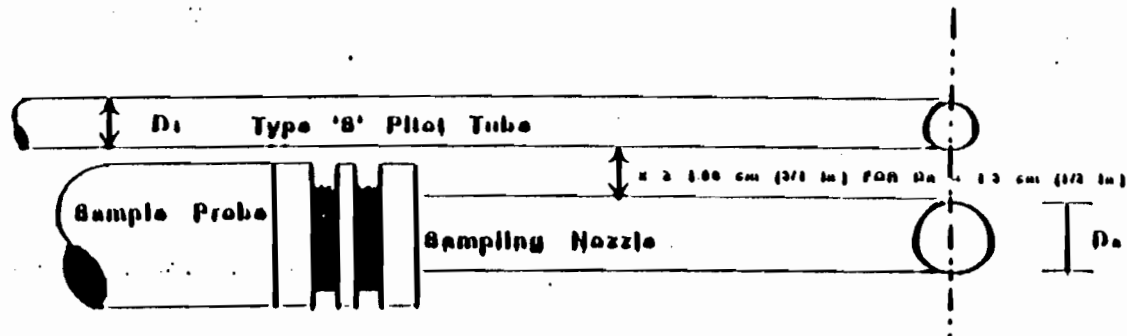
Proper thermocouple placement to prevent interference.



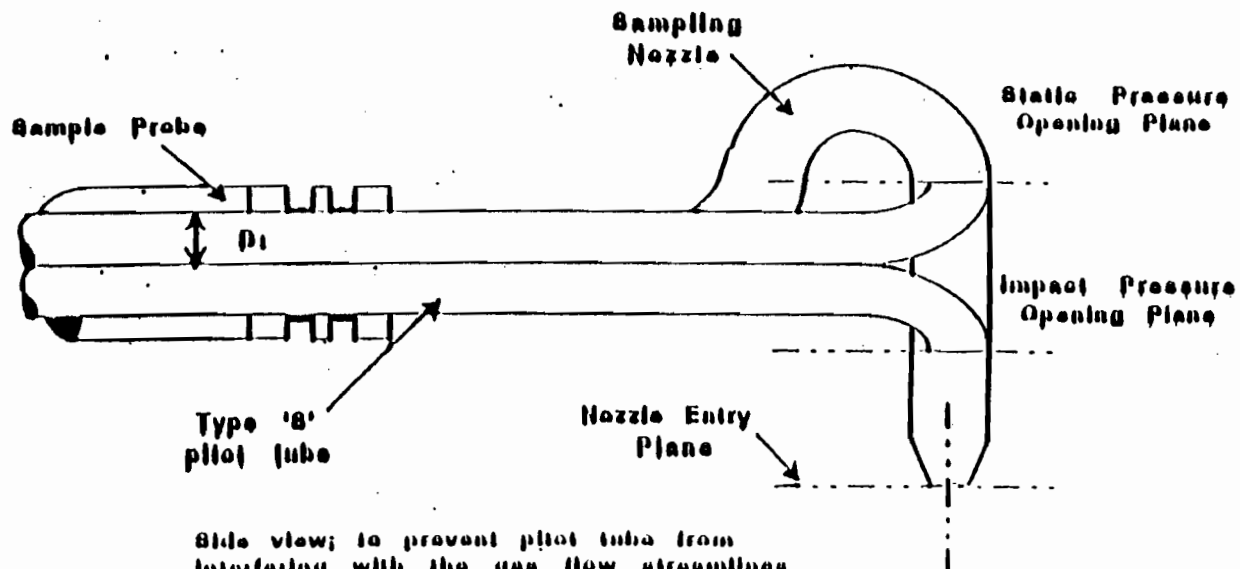
**SANDERS ENGINEERING &
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McMaha, AL 36605 FAX: (205) 833-2285

Proper pilot tube-sampling nozzle configuration to prevent aero-dynamic interference; bottomhook type nozzle; centers of nozzle and pilot opening aligned; D_1 between 0.48 and 0.65 cm (3/16 and 3/8 in.)



Bottom view showing minimum pilot/nozzle separation



Side view; to prevent pilot tube from interfering with the gas flow streamlines approaching the nozzle, the impact pressure opening plane of the pilot tube shall be even with or above the nozzle entry plane.

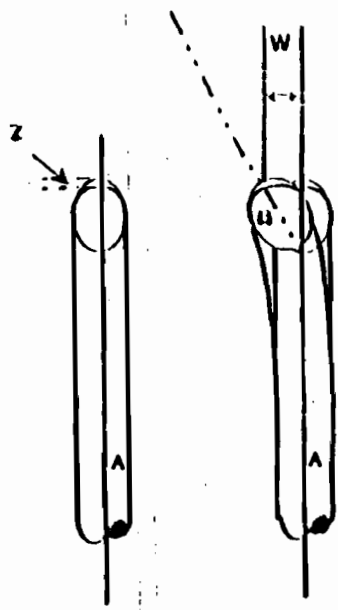
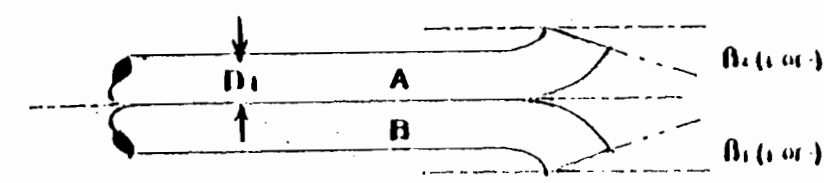
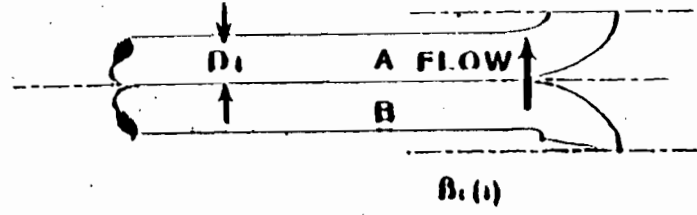
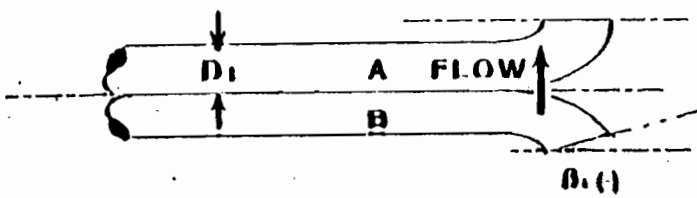
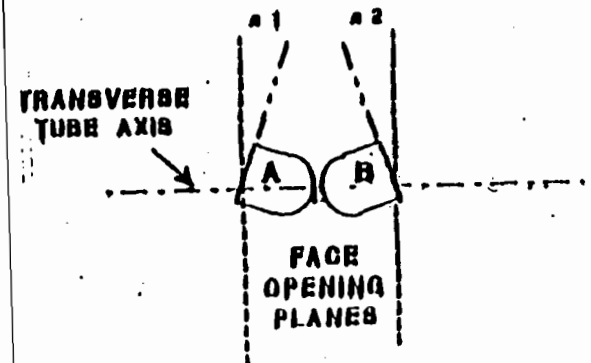
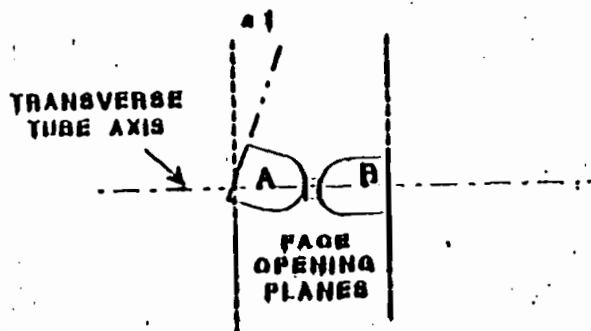
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Types of face-opening misalignment that can result from field use or improper construction of type 'S' pitot tubes. These will not affect the baseline value of $C_p(a)$ so long as θ_1 and $\theta_2 < 10^\circ$, θ_1 and $\theta_2 < 5^\circ$, $d < 0.32$ cm (1/8 in.)



APPENDIX D OPERATIONAL DATA

**CRIST ELECTRIC GENERATING PLANT
PARTICULATE COMPLIANCE TEST CHRONOLOGY
UNIT # 4
SOOTBLOWING CONDITIONS
April 25, 1995**

RUN # 1	START	9:06 a.m.	No problems noted at beginning of run.
	STOP	10:12 a.m.	No problems noted at end of run.
RUN # 2	START	10:55 a.m.	No problems noted at beginning of run.
	STOP	11:56 a.m.	No problems noted at end of run.
RUN # 3	START	12:36 p.m.	No problems noted at beginning of run.
	STOP	1:42 p.m.	No problems noted at end of run.

**CRIST ELECTRIC GENERATING PLANT
PARTICULATE COMPLIANCE TEST CHRONOLOGY
UNIT # 4
STEADY STATE CONDITIONS
April 26,1995**

RUN # 1	START STOP	7:52 a.m. 8:58 a.m.	No problems noted at beginning of run. No problems noted at end of run.
RUN # 2	START STOP	.9:18 a.m. 10:23 a.m.	No problems noted at beginning of run. No problems noted at end of run.
RUN # 3	START STOP	10:45 a.m. 11:51 p.m.	No problems noted at beginning of run. No problems noted at end of run.

**CRIST ELECTRIC GENERATING PLANT
 PARTICULATE COMPLIANCE TEST
 SIX - MINUTE OPACITY AVERAGES
 UNIT #4
 SOOT BLOWING CONDITIONS
 April 25, 1995**

TIME OF 6 MIN. AVERAGE	OPACITY (%)
(RUN # 1)	(RUN # 1)
8:01 - 8:06	4.0
8:07 - 8:12	4.1
8:13 - 8:18	4.5
8:19 - 9:24	4.3
9:25 - 9:30	4.3
9:31 - 9:36	4.2
(RUN # 2)	(RUN # 2)
10:55 - 11:00	3.7
11:01 - 11:06	3.6
11:07 - 11:12	3.6
11:13 - 11:18	3.5
11:19 - 11:24	3.4
11:25 - 11:30	4.0
11:31 - 11:36	3.7
11:37 - 11:42	3.3
11:43 - 11:48	3.5
11:49 - 11:54	3.6
11:55 - 12:00	3.4

**CRIST ELECTRIC GENERATING PLANT
PARTICULATE COMPLIANCE TEST
SIX - MINUTE OPACITY AVERAGES
UNIT # 4
SOOT BLOWING CONDITIONS
April 25, 1995**

(RUN # 3)	(RUN # 3)
12:31.- 12:36	3.5
12:37.- 12:42	3.7
12:43 - 12:48	4.0
12:49 - 12:54	3.9
12:55 - 13:00	3.7
13:01 - 13:06	3.4
13:07 - 13:12	3.6
13:13 - 13:18	3.4
13:19 - 13:24	3.8
13:25 - 13:30	3.6
13:31 - 13:36	3.5
13:37 - 13:42	4.0

CRIST ELECTRIC GENERATING PLANT
PARTICULATE COMPLIANCE TEST
SIX - MINUTE OPACITY AVERAGES

UNIT # 4

STEADY STATE CONDITIONS

April 26, 1995

TIME OF 6 MIN. AVERAGE	OPACITY (%)
(RUN # 1)	(RUN # 1)
7:49 - 7:54	4.2
7:55 - 8:00	4.0
8:01 - 8:06	3.8
8:07 - 8:12	3.6
8:13 - 8:18	3.4
8:19 - 8:24	3.4
8:25 - 8:30	3.2
8:31 - 8:36	3.3
8:37 - 8:42	3.2
8:43 - 8:48	3.4
8:49 - 8:54	3.3
8:55 - 9:00	3.7
(RUN # 2)	(RUN # 2)
9:13 - 9:18	3.3
9:19 - 9:24	3.3
9:25 - 9:30	3.3
9:31 - 9:36	3.2
9:37 - 9:42	4.5
9:43 - 9:48	3.4
9:49 - 9:54	3.4
6:55 - 10:00	3.3
10:01 - 10:06	3.5
10:07 - 10:12	3.2
10:13 - 10:18	3.3
10:19 - 10:24	3.3

**CRIST ELECTRIC GENERATING PLANT
PARTICULATE COMPLIANCE TEST
SIX - MINUTE OPACITY AVERAGES**

UNIT # 4

STEADY STATE CONDITIONS

April 26, 1995

(RUN # 3)	(RUN # 3)
10:43 - 10:48	3.3
10:49 - 10:54	3.1
10:55 - 11:00	3.2
11:01 - 11:06	3.1
11:07 - 11:12	3.2
11:13 - 11:18	3.1
11:19 - 11:24	3.2
11:25 - 11:30	3.0
11:31 - 11:36	3.1
11:37 - 11:42	3.0
11:43 - 11:48	3.0
11:49 - 11:54	3.4

**CRIST ELECTRIC GENERATING PLANT
PARTICULATE COMPLIANCE TEST: UNIT # 4
PRECIPITATOR READINGS**

COLD PRECIPITATOR

TEST: Steady State

DATE: 05/26/95

RUN # : 1

Start or End Start

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4-A	31	420	370	18
4-B	28	340	300	NO READING
4-C	34	NO READING	190	19

TEST: Steady State

DATE: 05/26/95

RUN # : 1

Start or End End

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4-A	31	420	370	18
4-B	28	340	300	NO READING
4-C	34	NO READING	190	19

**CRIST ELECTRIC GENERATING PLANT
PARTICULATE COMPLIANCE TEST: UNIT # 4
PRECIPITATOR READINGS**

HOT PRECIPITATOR

TEST: Steady State

DATE: 5/26/95

RUN #: 1

Start or End Start

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4A	25	270	210	NO READING
4B	25	250	200	36
4C	80	340	480	52
4D	80	300	660	58
4E	60	320	440	50
4F	70	300	500	50

RUN #: 1

Start or End End

4A	25	270	210	NO READING
4B	40	260	250	36
4C	80	340	480	52
4D	80	300	660	58
4E	60	320	440	50
4F	70	300	500	55

CRIST ELECTRIC GENERATING PLANT
PARTICULATE COMPLIANCE TEST: UNIT # 4
PRECIPITATOR READINGS

COLD PRECIPITATOR

TEST: Steady State

DATE: 05/26/95

RUN #: 2

Start or End Start

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4-A	31	420	370	18
4-B	28	340	300	NO READING
4-C	34	NO READING	190	19

TEST: Steady State

DATE: 05/26/95

RUN #: 2

Start or End End

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4-A	31	420	370	18
4-B	28	340	300	NO READING
4-C	34	NO READING	190	19

**CRIST ELECTRIC GENERATING PLANT
PARTICULATE COMPLIANCE TEST: UNIT # 4
PRECIPITATOR READINGS**

HOT PRECIPITATOR

TEST: Steady State

DATE: 5/26/95

RUN #: 2

Start or End Start

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4A	25	270	210	NO READING
4B	40	260	250	36
4C	80	340	480	52
4D	80	300	660	58
4E	60	320	440	50
4F	70	300	500	52

RUN #: 2

Start or End End

4A	40	260	280	NO READING
4B	30	250	210	40
4C	80	340	480	52
4D	80	300	650	58
4E	74	375	580	52
4F	70	310	500	52

**CRIST ELECTRIC GENERATING PLANT
PARTICULATE COMPLIANCE TEST: UNIT # 4
PRECIPITATOR READINGS**

COLD PRECIPITATOR

TEST: Steady State

DATE: 05/26/95

RUN #: 3

Start or End Start

Transformer
Box
A

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4-A	31	420	370	18
4-B	28	340	300	NO READING
4-C	34	NO READING	190	19

TEST: Steady State

DATE: 05/26/95

RUN #: 3

Start or End End

Transformer
Box
B

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4-A	31	420	370	18
4-B	28	340	300	NO READING
4-C	34	NO READING	190	19

**CRIST ELECTRIC GENERATING PLANT
PARTICULATE COMPLIANCE TEST: UNIT # 4
PRECIPITATOR READINGS**

COLD PRECIPITATOR

TEST: Steady State

DATE: 05/26/95

RUN #: 3

Start or End Start

Transformer
Box
A

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4-A	31	420	370	18
4-B	28	340	300	NO READING
4-C	34	NO READING	190	19

TEST: Steady State

DATE: 05/26/95

RUN #: 3

Start or End End

Transformer
Box
B

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4-A	31	420	370	18
4-B	28	340	300	NO READING
4-C	34	NO READING	190	19

**CRIST ELECTRIC GENERATING PLANT
PARTICULATE COMPLIANCE TEST: UNIT # 4
PRECIPITATOR READINGS**

HOT PRECIPITATOR

TEST: Steady State

DATE: 5/26/95

Transformer
Box
A

RUN #: 3

Start or End Start

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4A	40	270	280	NO READING
4B	30	250	210	40
4C	80	340	480	52
4D	80	300	650	58
4E	74	375	500	52
4F	70	310	740	52

Transformer
Box
B

RUN #: 3

Start or End End

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4A	35	270	200	NO READING
4B	30	250	480	40
4C	85	350	660	52
4D	80	300	570	58
4E	74	350	520	52
4F	70	300	500	52

CRIST ELECTRIC GENERATING PLANT
PARTICULATE COMPLIANCE TEST: UNIT # 4
PRECIPITATOR READINGS

COLD PRECIPITATOR

TEST: Soot Blowing

DATE: 05/25/95

RUN #: 1

Start or End Start

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4-A	30	400	360	18
4-B	28	340	300	NO READING
4-C	34	NO READING	190	19

TEST: Soot Blowing

DATE: 05/25/95

RUN #: 1

Start or End End

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4-A	31	420	370	18
4-B	28	340	300	NO READING
4-C	34	NO READING	190	19

**CRIST ELECTRIC GENERATING PLANT
PARTICULATE COMPLIANCE TEST: UNIT # 4
PRECIPITATOR READINGS**

HOT PRECIPITATOR

TEST: Soot Blowing

DATE: 05/25/95

RUN #: 1

Start or End Start

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4A	50	230	200	NO READING
4B	35	240	160	38
4C	85	340	700	55
4D	80	310	640	58
4E	78	375	580	54
4F	68	300	500	54

RUN #: 1

Start or End End

4A	30	250	200	NO READING
4B	40	270	300	38
4C	75	340	480	50
4D	80	300	630	58
4E	74	350	580	54
4F	68	300	500	54

**CRIST ELECTRIC GENERATING PLANT
PARTICULATE COMPLIANCE TEST: UNIT # 4
PRECIPITATOR READINGS**

COLD PRECIPITATOR

TEST: Soot Blowing

DATE: 05/25/95

RUN #: 2

Start or End Start

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4-A	31	420	370	18
4-B	28	340	300	NO READING
4-C	34	NO READING	190	19

TEST: Steady State

DATE: 05/26/95

RUN #: 2

Start or End End

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4-A	31	420	360	18
4-B	28	340	300	NO READING
4-C	34	NO READING	190	19

**CRIST ELECTRIC GENERATING PLANT
PARTICULATE COMPLIANCE TEST: UNIT # 4
PRECIPITATOR READINGS**

HOT PRECIPITATOR

TEST: Soot Blowing

DATE: 05/25/95

RUN #: 2

Start or End Start

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4A	30	250	200	NO READING
4B	40	270	300	38
4C	75	340	480	50
4D	80	300	630	58
4E	74	350	580	54
4F	68	300	500	54

RUN #: 2

Start or End End

4A	35	260	240	NO READING
4B	30	260	300	42
4C	80	340	400	52
4D	80	310	660	58
4E	70	330	560	52
4F	68	300	500	54

CRIST ELECTRIC GENERATING PLANT
 PARTICULATE COMPLIANCE TEST: UNIT # 4
 PRECIPITATOR READINGS

COLD PRECIPITATOR

TEST: Soot Blowing

DATE: 05/25/95

RUN #: 3

Start or End Start

Transformer
Box
A

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4-A	31	420	360	18
4-B	28	340	300	NO READING
4-C	34	NO READING	190	19

TEST: Soot Blowing

DATE: 05/25/95

RUN #: 3

Start or End End

Transformer
Box
B

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4-A	31	420	365	18
4-B	28	335	300	NO READING
4-C	34	NO READING	190	19

**CRIST ELECTRIC GENERATING PLANT
PARTICULATE COMPLIANCE TEST: UNIT # 4
PRECIPITATOR READINGS**

HOT PRECIPITATOR

TEST: Soot Blowing

DATE: 05/25/95

Transformer
Box
A

RUN #: 3

Start or End Start

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4A	35	260	240	NO READING
4B	30	260	300	42
4C	80	340	400	52
4D	80	310	660	58
4E	70	330	560	52
4F	68	300	500	54

Transformer
Box
B

RUN #: 3

Start or End End

4A	30	240	240	NO READING
4B	30	240	260	42
4C	75	340	360	48
4D	80	300	680	52
4E	72	350	550	52
4F	68	300	520	52

SANDERS ENGINEERING & ANALYTICAL SERVICES, INC.

**PARTICULATE EMISSIONS TEST REPORT
SOOT BLOWING OPERATIONS**

FOR

GULF POWER COMPANY

*Plant Crist, Unit 4
Pensacola, Florida*



April 25, 1995

1568 LEROY STEVENS ROAD

MOBILE, ALABAMA 36695 • 205/633-4120



SANDERS ENGINEERING & ANALYTICAL SERVICES, INC.

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ENVIRONMENTAL ENGINEERING
AIR & WATER QUALITY MODELING
ENVIRONMENTAL ASSESSMENTS
PSD ANALYSIS
EMERGENCY RESPONSE MONITORING

AMBIENT AIR MONITORING
CONTINUOUS IN-STACK MONITORING
SOURCE TESTING
VISIBLE EMISSIONS TESTING
CONSULTING SERVICES

TEST REPORT CERTIFICATION

In regard to this test, we certify that to the best of our knowledge, all of the data regarding the testing performed by our agents is true and correct.

Dated: 5/5/95

Sanders Engineering & Analytical Services, Inc.

By: Edward K. James

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1. INTRODUCTION

Sanders Engineering & Analytical Services, Inc. (SEAS) performed a particulate emissions test during soot blowing operations at Gulf Power Company, Plant Crist, Unit 4, located in Pensacola, Florida. The testing was conducted on April 25, 1995. The testing was performed in accordance with the applicable U.S. EPA procedures specified at **40 CFR, Part 60, Appendix A, Methods 1, 2, 3, 4, and 17.**

The purpose of the test was to demonstrate compliance with the rules and regulations of the Florida Department of Environmental Protection, and to meet the necessary requirements contained in the permit to operate issued by the Florida Department of Environmental Protection.

The test was conducted by Mr. Edward Harris, Mr. John Wilson, and Mr. Dean Holmes of Sanders Engineering & Analytical Services, Inc., and was coordinated with Mr. John McPherson of Gulf Power Company. The Florida Department of Environmental Protection was notified so their representative could be present to observe the testing.

The test was conducted in accordance with the guidelines of the Florida Department of Environmental Protection. Further discussion of the test methods are included later in the report.

2. SUMMARY AND DISCUSSION OF RESULTS

The results of the particulate emissions test for the soot blowing runs, along with the results of the computations, are summarized in Table I. The equations used in the calculations of the results, along with the completed field data sheets for the testing, are presented in Appendix A. The sample calculations of the first run are presented in Appendix B. The quality control checks of the equipment used in the sampling program are included in Appendix C.

The results of the testing indicate the particulate emission rate during soot blowing for Plant Crist, Unit 4, is 0.009 LBS/MMBTU. The applicable Florida Department of Environmental Protection rules and regulations require an emission rate of no greater than 0.30 LBS/MMBTU. The results of the testing indicate that the unit is in compliance with the particulate emission condition of the permit to operate issued by the Florida Department of Environmental Protection.

**TABLE I. PARTICULATE EMISSIONS TEST RESULTS
GULF POWER COMPANY
PLANT CRIST, UNIT 4, SOOT BLOWING
4/25/95**

Title of Run		<u>RUN 1</u>	<u>RUN 2</u>	<u>RUN 3</u>
Sampling Time -Start	Military	0906	1050	1236
Sampling Time -Stop	Military	1012	1156	1342
F Factor	SDCF/BTU	9820	9820	9820
Plant Load	Megawatts	82.0	82.0	82.0
Static Pressure	In. H2O	-1.20	-1.20	-1.20
Barometric Pressure	In. Hg	30.25	30.25	30.25
Average dH	In. H2O	0.9	1.0	1.0
Meter correction		0.999	0.999	0.999
Avg. Meter Temp.	Deg. F	62.9	67.6	71.4
% O2	%	5.9	5.8	5.9
%CO2	%	11.5	12.0	12.0
Volume Metered	ACF	37.557	39.044	39.825
Volume Water	Ml	52.0	75.0	58.0
Sampling Time	Minutes	64	64	64
Nozzle Diameter	Inches	0.222	0.222	0.219
Avg. Stack Temp.	Deg. F	296.8	296.8	298.6
Area of Stack	Sq. Feet	92.1350	92.1350	92.1350
Wt. of Part.	Mg.	15.4	10.4	10.0
Number of Points		32	32	32
Avg. Sqrt dP	In. H2O	0.8670	0.8681	0.9031

RESULTS OF COMPUTATIONS

		<u>RUN 1</u>	<u>RUN 2</u>	<u>RUN 3</u>	<u>Average</u>
Volume of Gas Sampled	SDCF	38.370	39.544	40.049	39.321
H2O vapor in Gas Stream	PERCENT	6.0	8.2	6.4	6.9
Avg. Stack Gas Velocity	FT/SEC	57.6	57.8	60.0	58.5
Volumetric Flow Rate	SDCF/M	210390	206419	217884	211565
Volumetric Flow Rate	ACF/M	318203	319716	331687	323202
Particulate Conc.	Grs/SDCF	0.006	0.004	0.004	0.005
Particulate Conc.	Grs/ACF	0.004	0.003	0.003	0.003
Particulate Mass Rate	Lb/Hr	11.1	7.2	7.2	8.5
Particulate Mass Rate	Lb/MMBtu	0.012	0.008	0.008	0.009
Heat Input	F Factor MMBTU/Hr	922.59	911.21	955.46	929.75
Percent of Isokinetic	%	97.7	102.6	101.2	

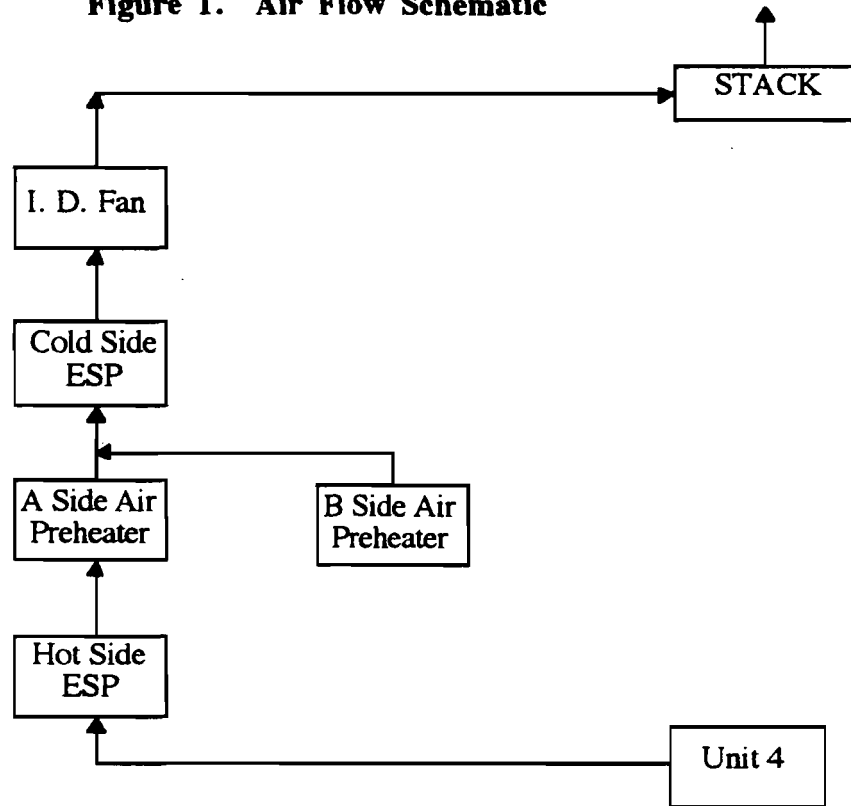
3. PROCESS DESCRIPTION

The process consists of a steam electric generating unit firing bituminous coal for the production of electric energy. The coal is received by barge, and loaded directly onto the conveyor feeding the plant, or onto the stockpile and later loaded onto the conveyor belt transporting the coal to the plant. The coal from the conveyor is loaded into bunkers capable of holding between 36 to 48 hours supply of coal. The coal is then fed to pulverizing mills before being fired in the unit through the burners. Upon combustion of the coal in the fire box, approximately 20 percent of the ash falls to the bottom of the boiler and is removed by the ash removal system. The remaining 80 percent exits with the flue gases through the heat exchange and economizer sections of the furnace, and is collected by electrostatic precipitators.

3.1. Source Air Flow

As shown in Figure 1, the flue gases exit the boiler and flow through a hot side precipitator. The exhaust gases are separated into ducts A and B before entering air preheaters. The exhaust gases are combined before entering a cold side ESP. The flue gases exiting the cold side ESP are exhausted through a stack into the atmosphere.

Figure 1. Air Flow Schematic



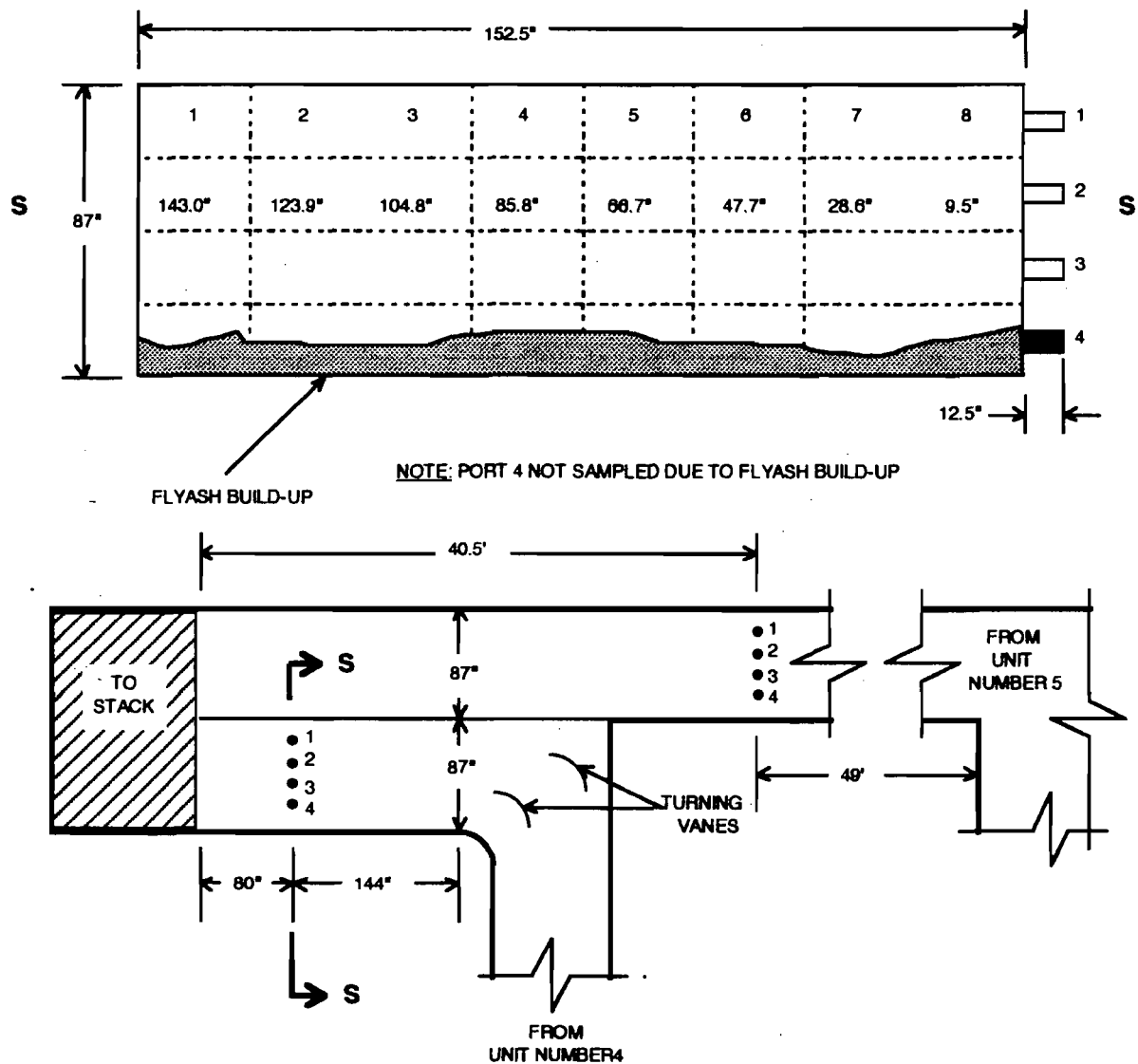
3.2. Operation During Testing

The average heat input during soot blowing operation, as based on F-factor calculations, was 929.75 million BTU per hour resulting in the production of approximately 82 megawatts of electricity. Precipitator data supplied by Gulf Power personnel is given in Appendix D.

4. SAMPLE POINT LOCATION

The sample point locations and outlet duct schematic are presented in Figure 2. Method 1 was used for determination of the number and location of sampling points. The minimum number of points (25) required for rectangular stacks was met by sampling a total of 32 points.

Figure 2. Sample Point Locations

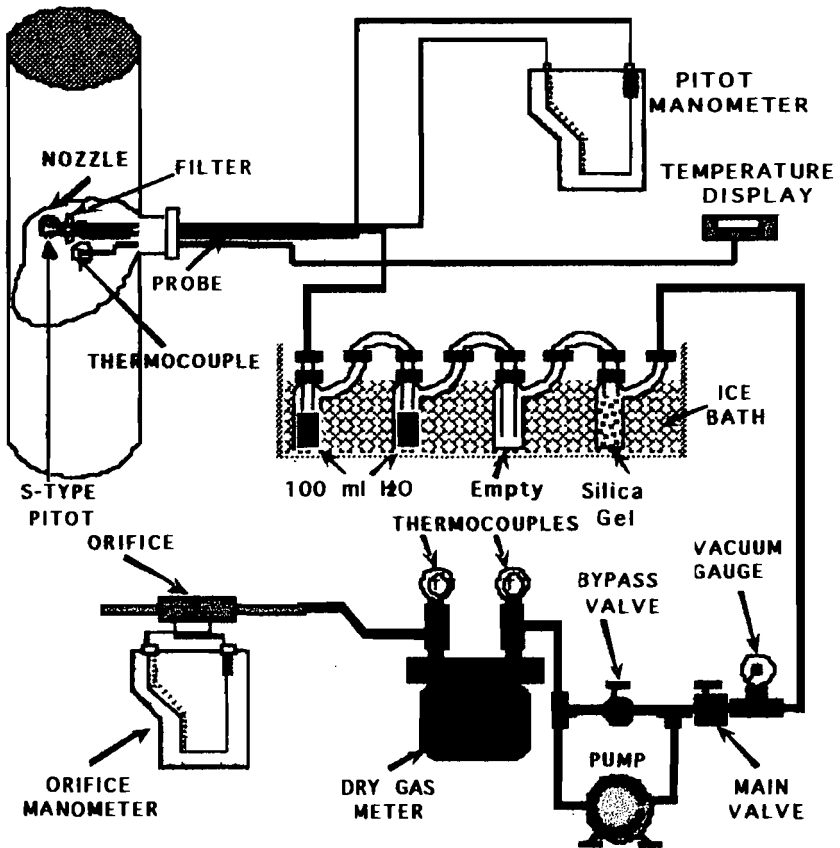


5. PARTICULATE SAMPLING PROCEDURE (EPA Method 17)

The sampling procedure utilized is that specified in 40 CFR, Part 60, Appendix A, Method 17, as modified by the governing regulatory agency. A brief description of this procedure is as follows:

The first impingers were partially filled with 100 milliliters of deionized water. The next impinger was left empty to act as a moisture trap. Preweighed 6 to 16 mesh indication silica gel was added to the last impinger. The sampling equipment manufactured by Lear Siegler (Model 100) or Sanders Engineering

Figure 3. Particulate Sampling Train



(Model 200) was assembled as shown in the attached drawing. The system was leak checked by plugging the inlet to the nozzle and pulling a 15 inch mercury vacuum. A leakage rate not in excess of 0.02 cubic feet per minute was considered acceptable.

The inside dimensions of the stack liner were measured and recorded. The required number of sampling points were marked on the probe for easy visibility. The range of velocity pressure, the percent moisture, and the temperature of the effluent gases were determined. From this data, the correct nozzle size and the nomograph multiplication factor were determined.

Crushed ice was placed around the impingers. The nozzle was placed on the first traverse point with the tip pointing directly into the gas stream. The pump was started immediately and the flow was adjusted to isokinetic sampling conditions. After the required time interval had elapsed, the probe was repositioned to the next traverse point and isokinetic sampling was re-established. This was performed for each point until the run was completed. Readings were taken at each point and recorded on the field data sheet. At the conclusion of each run, the pump was turned off and the final readings were recorded.

5.1. Particulate Sample Recovery

Care was exercised in moving the collection train to the sample recovery area to minimize the loss of collected sample, or the gain of extraneous particulate matter. The volume of water in the impingers was measured, the silica gel impinger was weighed and recorded on the field data sheet. The nozzle, and all sample-exposed surfaces were washed with reagent grade acetone into a clean sample container. A brush was used to loosen any adhering particulate matter and subsequent washings were placed into the container. The filter was carefully removed from the fritted support and placed in a clean separate sample container. A sample of the acetone used in the washing was saved for a blank laboratory analysis.

5.2. Particulate Analytical Procedures

The filter and any loose particulate matter were transferred from the sample container to a clean, tared weighing dish. The filter was placed in a desiccator for at least 24 hours and then weighed to the nearest 0.1 milligram until a constant weight was obtained. The original weight of the filter was deducted, and the weight gain was recorded to the nearest 0.1 milligram.

The wash solution was transferred to a clean, tared beaker. The solution was evaporated to dryness, desiccated to a constant weight, and the weight gain was recorded to the nearest 0.1 milligram.

APPENDIX A EQUATIONS AND FIELD DATA SHEETS

EQUATIONS

$$1. \quad P_s = P_{\text{bar}} + \frac{P_g}{13.6}$$

$$2. \quad P_m = P_{\text{bar}} + \frac{\overline{\Delta H}}{13.6}$$

$$3. \quad V_s = K_p C_p \sqrt{\Delta P} \sqrt{\frac{\overline{T_s}}{M_s P_s}}$$

$$4. \quad V_{m(\text{Std})} = K_1 V_m Y \left[\frac{P_{\text{bar}} + \frac{\overline{\Delta H}}{13.6}}{\overline{T_m}} \right]$$

$$5. \quad V_{w(\text{Std})} = 0.04707 V_{1c}$$

$$6. \quad B_{ws} = \frac{V_{w(\text{Std})}}{V_{m(\text{Std})} + V_{w(\text{Std})}}$$

$$7. \quad M_d = 0.44 (\%CO_2) + 0.32 (\%O_2) + 0.28 (\%N_2 + \%CO)$$

$$8. \quad M_s = M_d(1 - B_{ws}) + 18(B_{ws})$$

$$9. \quad EA = \left[\frac{(\%O_2 - 0.5 (\%CO))}{0.264 (\%N_2) - ((\%O_2) - 0.5 (\%CO))} \right] 100$$

$$10. \quad Q_a = (V_s) (A_s) (60)$$

$$11. \quad Q_s = Q_a (1 - B_{ws}) \frac{(528)}{\bar{T}_s} \frac{(P_s)}{29.92}$$

$$12. \quad E_H = \left(\frac{PMR}{H_1} \right)$$

$$13. \quad E = C_d F_{O_2} \left(\frac{20.9}{20.9 - \%O_2} \right)$$

$$14. \quad C_s = 0.0154 \frac{M_n}{V_{m(Std)}}$$

$$15. \quad C_{50} = \frac{21 C_s}{21 - [(1.5) (\%O_2) - 0.133 (N_2) - 0.75 (\%CO)]}$$

$$16. \quad C_{12} = \frac{C_s (12)}{\%CO_2}$$

$$17. \quad PMR = (C_s) (Q_s) \frac{(60)}{7000}$$

$$18. \quad V_n = \left[(0.002669) (V_{1c}) + \frac{V_m Y}{\bar{T}_m} \left(p_{bar} + \frac{\bar{\Delta H}}{13.6} \right) \right] \frac{\bar{T}_s}{P_s}$$

$$19. \quad I = \frac{100 V_n}{(60) \emptyset V_s A_n}$$

NOMENCLATURE

- A_n = Cross-sectional area of nozzle, ft²
- A_s = Cross sectional area of stack, ft²
- B_{ws} = Water vapor in the gas stream,
proportion by volume (dimensionless)
- C_p = Pitot tube coefficient (dimensionless) (0.84)
- C_s = Particulate concentration, grains/SDCF
- C_d = Particulate concentration, lbs/SDCF
- C_{12} = Particulate concentration (C_s adjusted to 12% CO)
grains/SDCF
- C_{50} = Particulate concentration (C_s adjusted to 50% excess air)
grains/SDCF
- EA = Excess air, %
- E = Emission in lb/mmBTU
- E_H = Emission in lb/mmBTU, based on heat input
- H_1 = Total Heat Input, Million BTU per Hour (MMBTU/hr)
- I = Percent of isokinetic sampling
- K_1 = 17.64 °R/ inches Hg
- K_p = Pitot tube constant,
$$85.49 \text{ ft/sec} \left[\frac{(\text{lb/lb-mole}) (\text{in. Hg})}{(^{\circ}\text{R}) (\text{Inc. H}_2\text{O})} \right]^{\frac{1}{2}}$$
- M_n = Total amount of particulate collected, mg
- M_d = Molecular weight of stack gas; dry basis, lb/lb mole
- M_s = Molecular weight of stack gas; wet basis, lb/lb mole
- P_{bar} = Barometric pressure at the sampling site, in. Hg

NOMENCLATURE (continued)

- P_m = Meter pressure, in. Hg
- P_s = Absolute stack pressure, in. Hg
- P_g = Stack static pressure, in. H₂O
- PMR = Particulate mass rate, lb/Hr
- Q_a = Volumetric flow rate ACFM
- Q_s = Volumetric flow rate SDCFM
- V_s = Average stack gas velocity, ft/sec
- V_{lc} = Total volume of liquid collected in impingers & silica gel, ml
- V_m = Volume of gas sample as measured by dry gas meter, ACF
- $V_{m(std)}$ = Volume of gas sample measured by dry gas meter,
corrected to standard conditions, SDCF
- $V_{w(std)}$ = Volume of water vapor in gas sample, corrected to standard
conditions, SCF
- V_n = Volume collected at stack conditions through nozzle, ACF
- Y = Dry gas meter calibration factor (dimensionless)
- ΔH = Average pressure difference of orifice, in. H₂O
- ΔP = Velocity head of stack gas, in. H₂O
- $\sqrt{\Delta P}$ = Average of square roots of the velocity pressure, in. H₂O
- \emptyset = Total sampling time, minutes
- %CO₂, %O₂, N₂, %CO - Number % by volume, dry basis, from gas analysis
- F_{O_2} = Oxygen based F factor (9820 SDCF/mmBTU for bituminous coal)
- T_s = Temperature of the stack, °R (°F + 460)



SANDERS ENGINEERING & ANALYTICAL SERVICES, Inc.

1568 Leroy Stevens Rd.
Mobile, AL 36695

Office: (205) 633-4120
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FIELD DATA SHEET

COMPANY GPCO DATE 4-25-95 DGM# S-101
 PLANT Crist OPERATOR ELH ΔHa 0.75
 UNIT 4 S.B. METHOD 17 PROBE N/A cu. ft./min. 14'
 liner length

RUN 1

NOZZLE CALIBRATION		FILTER NUMBER
PRE	POST	
.222	.222	609
.222	.222	
.221	.222	
.222	.222	
AVERAGE	AVERAGE	

RUN 2

NOZZLE CALIBRATION		FILTER NUMBER
PRE	POST	
.221	.221	610
.222	.222	
.222	.222	
.222	.222	
AVERAGE	AVERAGE	

RUN 3

NOZZLE CALIBRATION		FILTER NUMBER
PRE	POST	
.219	.219	611
.219	.219	
.220	.220	
.219	.219	
AVERAGE	AVERAGE	

METER READING

819.257	
FINAL	FINAL
781.700	
INITIAL	INITIAL
37.557	
NET	NET

METER READING

857.404	
FINAL	FINAL
820.400	
INITIAL	INITIAL
39.004	
NET	NET

METER READING

900.425	
FINAL	FINAL
860.600	
INITIAL	INITIAL
39.825	
NET	NET

LEAK CHECK

SYSTEM		PITOT	
Pre	Post	Pre	Post
15	7	Impact	Impact
in. hg	in. hg	static	static
0.000	0.000		
cim	cim		

LEAK CHECK

SYSTEM		PITOT	
Pre	Post	Pre	Post
15	10	Impact	Impact
in. hg	in. hg	static	static
0.000	0.000		
cim	cim		

LEAK CHECK

SYSTEM		PITOT	
Pre	Post	Pre	Post
15	10	Impact	Impact
in. hg	in. hg	static	static
0.000	0.000		
cim	cim		

VOLUME OF LIQUID WATER COLLECTED

IMP. 1	IMP. 2	IMP. 3	IMP. 4
144	100	0	1457.0
FINAL	FINAL	FINAL	FINAL
100	100	0	1449.0
INITIAL	INITIAL	INITIAL	INITIAL
44	0	0	8.0
NET	NET	NET	NET
TOTAL			52.0

VOLUME OF LIQUID WATER COLLECTED

IMP. 1	IMP. 2	IMP. 3	IMP. 4
164	100	0	1376.0
FINAL	FINAL	FINAL	FINAL
100	100	0	1365.0
INITIAL	INITIAL	INITIAL	INITIAL
64	0	0	11.0
NET	NET	NET	NET
TOTAL			75.0

VOLUME OF LIQUID WATER COLLECTED

IMP. 1	IMP. 2	IMP. 3	IMP. 4
150	100	0	1465.0
FINAL	FINAL	FINAL	FINAL
100	100	0	1457.0
INITIAL	INITIAL	INITIAL	INITIAL
50	0	0	8.0
NET	NET	NET	NET
TOTAL			58.0

GAS ANALYSIS

O ₂ <u>5.9 %</u>	STATIC <u>-1.20</u>
CO ₂ <u>11.5 %</u>	BAROMETRIC
CO <u>-</u>	<u>30.25</u>
	in. hg

GAS ANALYSIS

O ₂ <u>5.8 %</u>	STATIC <u>-1.20</u>
CO ₂ <u>12.0 %</u>	BAROMETRIC
CO <u>-</u>	<u>30.25</u>
	in. hg

GAS ANALYSIS

O ₂ <u>5.9 %</u>	STATIC <u>-1.20</u>
CO ₂ <u>12.0 %</u>	BAROMETRIC
CO <u>-</u>	<u>30.25</u>
	in. hg

PORT #	TIME	GAS METER VOL. (cu. ft.)	VEL. HEAD ΔP in. H ₂ O	ORIFICE HEAD ΔH in. H ₂ O	TEMPERATURE °F					VAC. in. H _g	
					STACK	PROBE	HOT BOX	IMP.	GAS METER		
POINT #									IN	OUT	
3 - 1	9:06	781.700	0.60	0.77	295	N/A	N/A	60	61	61	1
2	:08	782.800	0.69	0.88	296			✓	61	61	1
3	:10	783.950	0.61	0.78	297			✓	61	61	1
4	:12	785.000	0.45	0.58	298			✓	61	61	1
5	:14	785.900	0.56	0.72	298			✓	61	61	1
6	:16	787.000	0.69	0.88	298			53	61	61	2
7	:18	788.000	0.60	0.77	297			✓	61	61	2
8	:20	789.100	0.75	0.96	296			✓	61	61	2
3 - 1	9:22	790.200	0.60	0.77	297			✓	61	61	2
2	:24	791.100	0.60	0.77	297			✓	63	62	2
3	:26	792.300	0.58	0.74	297			✓	63	62	2
4	:28	793.400	0.45	0.57	298			✓	63	62	2
5	:30	794.300	0.60	0.77	298			52	63	62	2
6	:32	795.300	0.65	0.83	298			✓	63	63	2
7	:34	796.400	0.60	0.77	298			✓	63	63	2
8	:36	797.500	0.75	0.96	294			✓	64	63	2.5
2 - 1	9:40	798.629	0.95	1.22	297			✓	64	63	3.5
2	:42	800.000	1.30	1.67	298			51	64	63	4
3	:44	801.600	1.0	1.29	298			✓	64	63	3.5
4	:46	802.900	0.80	1.03	298			✓	64	63	3
5	:48	804.100	0.75	0.96	297			✓	64	63	2
6	:50	805.300	0.68	0.87	297			✓	64	63	2
7	:52	806.300	0.68	0.87	296			✓	64	63	2
8	:54	807.400	0.80	1.03	295			✓	64	63	2.5

CHECK INDICATES TEMPERATURES MEET REQUIRED LIMITS.

COMPANY GPCO DATE 4/25/95
 SITE Crist 4 S.B. RUN # 1 PAGE 2 OF 7

Bottom Port not sampled due to Ash buildup
 (Port #1)

PORT #	POINT #	TIME	GAS METER VOL. (cu. ft.)	VEL. HEAD ΔP in. H ₂ O	ORIFICE HEAD ΔH in. H ₂ O	TEMPERATURE °F					VAC. in. H _g	
						STACK	PROBE	HOT BOX	IMP.	GAS METER		
										IN	OUT	
1	1	9:56	808.729	1.40	1.80	296	N/A	N/A	55	65	64	5
2	2	:58	810.250	1.12	1.44	297			✓	65	64	4.5
3	3	10:00	811.700	1.24	1.60	297			✓	65	64	4.5
4	4	:02	813.300	0.95	1.22	296			✓	65	64	4
5	5	:04	814.550	0.84	1.08	296			✓	65	64	4
6	6	:06	815.750	0.71	0.91	295			✓	65	65	3
7	7	:08	816.900	0.80	1.03	296			✓	65	65	3
8	8	:10	818.200	0.71	0.91	295			✓	65	65	3
End		10:12	819.257									
				0.866	0.983	296.8						

CHECK INDICATES TEMPERATURES MEET REQUIRED LIMITS.

COMPANY GPCO DATE 4/25/95
 SITE Crist #4 SB RUN # 1 PAGE 3 OF 7

PORT #	POINT #	TIME	GAS METER VOL. (cu. ft.)	VEL. HEAD ΔP in. H ₂ O	ORIFICE HEAD ΔH in. H ₂ O	TEMPERATURE °F					VAC. in. H _g	
						STACK	PROBE	HOT BOX	IMP.	GAS METER		
									IN	OUT		
1.29	1-1	10:50	820.400	0.70	0.90	297	N/A	N/A	50	66	66	2.5
	2	:52	821.600	1.05	1.35	298			✓	66	66	2.5
	3	:54	823.000	1.10	1.42	298			✓	66	66	4
	4	:56	824.400	0.99	1.30	298			✓	66	66	4
1.32	5	:58	825.700	0.93	1.22	297			✓	66	66	4
	6	11:00	827.100	0.74	0.97	297			52	67	66	3
	7	:02	828.350	0.75	0.99	297			✓	67	66	3
	8	:04	829.400	0.66	0.87	297			✓	67	66	3
	2-1	11:07	830.655	0.91	1.20	296			✓	67	67	2.5
	2	:09	831.900	0.98	1.29	297			✓	67	67	3.5
	3	:11	833.200	1.05	1.38	297			✓	67	67	4
	4	:13	834.700	0.76	1.00	297			51	67	67	3
	5	:15	836.100	0.76	1.0	297			✓	67	67	3
	6	:17	837.100	0.66	0.87	297			✓	68	67	3
	7	:19	838.300	0.63	0.83	296			✓	68	67	3
	8	:21	839.400	0.70	0.92	295			✓	68	67	3
	2-1	11:23	840.650	0.93	1.22	297			✓	68	67	3.5
	2	:25	841.900	0.96	1.27	297			✓	68	67	4
	3	:27	843.300	0.87	1.15	297			50	68	68	3
	4	:29	844.500	0.80	1.06	297			✓	68	68	3.5
	5	:31	845.700	0.70	0.93	297			✓	68	68	3
	6	:33	846.900	0.66	0.87	297			✓	69	68	2.5
	7	:35	848.200	0.61	0.81	297			✓	69	68	3
	8	:37	849.200	0.77	1.02	297			✓	69	68	3

CHECK INDICATES TEMPERATURES MEET REQUIRED LIMITS.

COMPANY GPCO

DATE 4/25/95

SITE Crist #4

S.B.

RUN # 2

PAGE 4 OF 7

PORT #	TIME	GAS METER VOL. (cu. ft.)	VEL. HEAD ΔP in. H_2O	ORIFICE HEAD ΔH in. H_2O	TEMPERATURE $^{\circ}F$						VAC. in. H_g
					STACK	PROBE	HOT BOX	IMP.	GAS METER		
									IN	OUT	
3 - 1	11:40	850.600	0.75	0.999	293	N/A	N/A	50	69	68	4
2	:42	851.700	0.63	0.83	297			✓	69	68	3.5
3	:44	852.900	0.57	0.75	297			✓	69	69	3
4	:46	854.100	0.41	0.54	298			✓	69	69	2
5	:48	854.900	0.55	0.73	298			✓	69	69	3
6	:50	856.000	0.62	0.82	298			✓	70	69	3
7	:52	857.100	0.55	0.73	297			-	70	69	3
8	:54	858.200	0.66	0.87	294			-	70	69	3
Final	11:56	859.444									
				0.868							

CHECK INDICATES TEMPERATURES MEET REQUIRED LIMITS.

COMPANY GPCO DATE 4/25/95

SITE Crist #4 S.B. RUN # 2 PAGE 5 OF 7

PORT #	POINT #	TIME	GAS METER VOL. (cu. ft.)	VEL. HEAD ΔP in. H ₂ O	ORIFICE HEAD ΔH in. H ₂ O	TEMPERATURE °F					VAC. in. H _g	
						STACK	PROBE	HOT BOX	IMP.	GAS METER		
										IN	OUT	
3	1	12:36	860.600	0.70	0.87	296	NA	N/A	SC	70	70	2.5
	2	:38	861.800	0.62	0.77	297			✓	70	70	2.5
	3	:40	862.950	0.47	0.59	297			✓	70	70	2
	4	:42	863.800	0.45	0.56	298			✓	70	70	2
	5	:44	864.800	0.58	0.72	299			✓	70	70	2
	6	:46	865.700	0.58	0.72	299			✓	70	70	2
	7	:48	866.800	0.60	0.75	298			✓	70	70	2
	8	:50	868.000	0.75	0.94	295			49	71	70	3.5
2	1	12:53	869.500	1.07	1.34	298			✓	71	70	5
	2	:55	870.800	0.95	1.19	299			✓	71	70	4
	3	:57	872.100	1.03	1.29	299			✓	71	70	4
	4	:59	873.500	0.80	1.00	300			✓	71	71	4
	5	13:01	874.700	0.70	0.87	299			✓	71	71	3.5
	6	:03	875.900	0.71	0.89	299			✓	71	71	3.5
	7	:05	877.000	0.71	0.89	298			47	71	71	3.5
	8	:07	878.200	0.75	0.94	299			✓	71	71	3.5
1	1	13:10	879.378	1.25	1.57	299			✓	72	71	5.5
	2	:12	880.800	1.16	1.45	299			✓	72	71	5
	3	:14	882.350	1.10	1.38	299			✓	72	71	5
	4	:16	883.700	1.0	1.25	300			✓	72	71	5
	5	:18	885.100	0.77	0.96	299			✓	73	72	4
	6	:20	886.200	0.86	1.08	299			✓	73	72	4
	7	:22	887.500	0.80	1.01	297			✓	73	72	4
	8	:24	888.700	0.74	0.93	297			✓	73	72	4

CHECK INDICATES TEMPERATURES MEET REQUIRED LIMITS.

COMPANY GPCO DATE 4/25/95
 S.B.
 SITE Crist #4 RUN # 3 PAGE 6 OF 7

PORT #	TIME	GAS METER VOL. (cu. ft.)	VEL. HEAD ΔP in. H ₂ O	ORIFICE HEAD ΔH in. H ₂ O	TEMPERATURE °F					VAC. in. H _g	
					STACK	PROBE	HOT BOX	IMP.	GAS METER		
POINT #									IN	OUT	
1-1	126	890.000	1.20	1.51	299	N/A	N/A	54	73	72	5
2	128	891.300	1.05	1.32	300			✓	73	72	5
3	130	892.700	0.96	1.21	300			✓	73	73	5
4	132	894.100	0.98	1.23	300			✓	73	73	5
5	134	895.500	0.85	1.07	299			✓	73	73	5
6	136	896.900	0.76	0.96	299			✓	73	73	4
7	138	898.000	0.80	1.01	299			✓	73	73	4.5
8	140	899.200	0.75	0.94	299			✓	73	73	4.5
Final	13:42	900.425									

CHECK INDICATES TEMPERATURES MEET REQUIRED LIMITS.

COMPANY GPCO DATE 4/25/95

SITE Crist #4 S.B. RUN # 3 PAGE 7 OF 7

LABORATORY ANALYSIS & CHAIN OF CUSTODY

COMPANY/PLANT: Gulf Power / Crist

UNIT #: 4 DATE OF TEST: 4/25 - 4/26/95 TYPE OF TEST: M-5 M-17 OTHER _____

SAMPLE #	RELINQUISHED BY	RECEIVED BY	TIME	DATE	REASON FOR CHANGE
609 Wash	EFT	EFT	1000 am	4/28/95	No Change
610 Wash					
611 Wash					
612 Wash					
613 Wash					
614 Wash					

UNIT # 4 Soot Blow

RUN # <u>1</u>	FILTER # <u>609</u>	BEAKER # <u>3</u> WASH (ML) <u>45</u>
FINAL WEIGHT	134.40 mg	644 80.8 mg
INITIAL WEIGHT	122.3 mg	644 77.5 mg
DIFFERENCE	12.1	3.3
CORRECTED TOTAL WEIGHT		15.4
RUN # <u>2</u>	FILTER # <u>610</u>	BEAKER # <u>6</u> WASH (ML) <u>40</u>
FINAL WEIGHT	132.30 mg	683 90.9 mg
INITIAL WEIGHT	123.6 mg	683 89.2 mg
DIFFERENCE	8.7	1.7
CORRECTED TOTAL WEIGHT		10.4
RUN # <u>3</u>	FILTER # <u>611</u>	BEAKER # <u>21</u> WASH (ML) <u>50</u>
FINAL WEIGHT	131.0 mg	700 58.8 mg
INITIAL WEIGHT	123.2 mg	700 56.6 mg
DIFFERENCE	7.8	2.2
CORRECTED TOTAL WEIGHT		10.0
RUN # _____	FILTER # _____	BEAKER # _____ WASH (ML) _____
FINAL WEIGHT		
INITIAL WEIGHT		
DIFFERENCE		
CORRECTED TOTAL WEIGHT		

UNIT # 4 Steady State

RUN # <u>1</u>	FILTER # <u>612</u>	BEAKER # <u>32</u> WASH (ML) <u>60</u>
FINAL WEIGHT	142.20 mg	647 28.3 mg
INITIAL WEIGHT	121.7 mg	647 24.8 mg
DIFFERENCE	20.5	3.5
CORRECTED TOTAL WEIGHT		24.0
RUN # <u>2</u>	FILTER # <u>613</u>	BEAKER # <u>35</u> WASH (ML) <u>60</u>
FINAL WEIGHT	131.4 mg	685 66.2 mg
INITIAL WEIGHT	122.1 mg	685 63.5 mg
DIFFERENCE	9.3	2.7
CORRECTED TOTAL WEIGHT		12.0
RUN # <u>3</u>	FILTER # <u>614</u>	BEAKER # <u>36</u> WASH (ML) <u>65</u>
FINAL WEIGHT	129.4 mg	679 36.9
INITIAL WEIGHT	122.1 mg	679 34.8 mg
DIFFERENCE	7.3	2.1
CORRECTED TOTAL WEIGHT		9.4
WASH SOLVENT BLANK (ML) _____		BEAKER # <u>47</u> WASH (ML) <u>100</u>
FINAL WEIGHT		689 98.9 mg
INITIAL WEIGHT		689 98.9 mg
DIFFERENCE		0.0
CORRECTION FACTOR (MG/ML)		

ALL WEIGHTS ARE IN MILLIGRAMS (MG)

APPENDIX B SAMPLE CALCULATIONS

Input and Constants

```

          3
    9820 ft
f := -----
    mm btu

pg := -(1.2 in. H2O)
pbar := 30.25 in. Hg.
Ahavg := 0.9 in. H2O
y := 0.999
tm := 62.9 °F
o2 := 5.9
co2 := 11.5

          3
vm := 37.557 ft
vlc := 52. ml
theta := 64 min
nozdia := 0.222 in.
ts := 296.8 °F

          2
as := 92.135 ft
mn := 15.4 mg
numberofpoints := 32

          0.5
sqrtAp := 0.867 in. H2O

          lb in. Hg.    0.5
    85.49 1 ft 1 (-----)
          lb-mole °R in. H2O
kp := -----
          1 sec

cp := 0.84

    17.64 °R
k1 := -----
    in. Hg.
    
```

$$ts = \frac{(ts + 460 \text{ } ^\circ\text{F}) \text{ } ^\circ\text{R}}{\text{ } ^\circ\text{F}}$$

756.8 °R

$$tm = \frac{(tm + 460 \text{ } ^\circ\text{F}) \text{ } ^\circ\text{R}}{\text{ } ^\circ\text{F}}$$

522.9 °R

$$n2 = 100 - o2 - co2$$

82.6

$$an = \frac{\text{nozdia}^2 \text{ } 3.1416}{4 \left(\frac{12 \text{ in.}^2}{\text{ft}} \right)}$$

0.000268803 ft²

Calculations

Equation 1

$$ps = pbar + \frac{pg}{13.6 \text{ in. H}_2\text{O}}$$

$$1 \text{ in. Hg.}$$

30.1618 in. Hg.

Equation 2

$$pm = pbar + \frac{\Delta h_{avg}}{13.6 \text{ in. H}_2\text{O}}$$

$$\text{in. Hg.}$$

30.3162 in. Hg.

Equation 3

$$k_1 v_m y \left(pbar + \frac{\Delta h_{avg}}{13.6 \text{ in. H}_2\text{O}} \right)$$

$$\text{in. Hg.}$$

$$vmstd = \frac{\quad}{tm}$$

³
38.3717 ft

Equation 4

$$vwstd = \frac{0.04707 \text{ ft} \cdot vlc^3}{ml}$$

³
2.44764 ft

Equation 5

$$bws = \frac{vwstd}{vmstd + vwstd}$$

0.0599628

Equation 6

$$md = \frac{(0.44 \text{ co}_2 + 0.32 \text{ o}_2 + 0.28 \text{ n}_2) \text{ lb}}{\text{lb-mole}}$$

$$\frac{30.076 \text{ lb}}{\text{lb-mole}}$$

Equation 7

$$ms = md (1 - bws) + \frac{bws \text{ 18 lb}}{\text{lb-mole}}$$

$$\frac{29.3519 \text{ lb}}{\text{lb-mole}}$$

Equation 8

$$vs = kp \text{ cp } \sqrt{ts} \left(\frac{0.5}{ms \text{ ps}} \right)$$

$$\frac{57.5649 \text{ ft}}{\text{sec}}$$

Equation 9

$$qa = \frac{vs \text{ as } 60 \text{ sec}}{\text{min}}$$

$$\frac{318225. \text{ ft}^3}{\text{min}}$$

Equation 10

$$qs = \frac{qa (1 - bws) 528 \text{ }^\circ\text{R ps}}{ts \text{ 29.92 in. Hg.}}$$

$$\frac{210391. \text{ ft}^3}{\text{min}}$$

Equation 11

$$cs = \frac{0.0154 \text{ gr mn}}{\text{mg vmstd}}$$

$$\frac{0.0061806 \text{ gr}}{\text{-----}}$$

$$\frac{3}{\text{ft}}$$

Equation 12

$$pmr = \frac{cs \text{ qs } 60 \text{ min}}{\text{-----}}$$

$$\frac{7000 \text{ gr}}{\text{hour -----}}$$

$$\text{lb}$$

$$\frac{11.1458 \text{ lb}}{\text{-----}}$$

$$\text{hour}$$

Equation 13

$$e = \frac{cs \text{ f } 20.9 \text{ l lb}}{\text{-----}}$$

$$\frac{(20.9 - o_2) 7000 \text{ gr}}{\text{-----}}$$

$$\frac{0.0120809 \text{ lb}}{\text{-----}}$$

$$\text{mm btu}$$

Equation 14

$$vn = \frac{0.002669 \text{ in. Hg. ft}^3 \text{ vlc} \text{ vm y pm}}{\text{ts} \left(\frac{\text{-----}}{\text{ml } ^\circ\text{R}} + \frac{\text{-----}}{\text{tm}} \right)}$$

$$\text{ps}$$

$$\frac{3}{58.0628 \text{ ft}}$$

Equation 15

$$i = \frac{100 \% \text{ vn}}{60 \text{ sec theta vs an}} \text{ min}$$

97.7179 %

Equation 16

$$hi = \frac{\text{par}}{e} \text{ hour}$$

922.596 mm btu

APPENDIX C QUALITY CONTROL

**INITIAL
METER CALIBRATION FORM - DGM**

DATE:	12-27-94	Box No.	S-101		
Ref. DGM Ser. #	1044456	Calibrated By	EDWARD HARRIS		
RUN #	1	2	3	4	5
DELTA H (DGM)	0.50	1.00	1.50	2.00	2.50
Y (Ref. DGM)	0.985	0.985	0.985	0.985	0.985
Reference DGM					
Gas Vol. Initial	973.200	979.920	985.000	990.895	996.540
Gas Vol. Final	979.920	985.000	990.895	996.540	1003.024
Meter Box DGM					
Gas Vol. Initial	878.100	884.800	889.855	895.700	901.300
Gas Vol. Final	884.800	889.855	895.700	901.300	907.700
Reference DGM					
Temp.	Avg.	Avg.	Avg.	Avg.	Avg.
Deg F Initial	44	49	54	57	57
Deg F Final	49	49	57	57	57
Meter Box DGM					
Temp. Initial In	43	47	50	54	54
Temp. Initial Out	43	47	50	54	54
Temp. Final In	47	47	54	54	54
Temp. Final Out	47	47	54	54	54
P Bar IN.-Hg	30.20	30.20	30.20	30.20	30.20
Time (sec.)	959	527	502	416	432
Meter Calibration					
Factor (Y)	0.999	0.999	0.998	0.997	1.001
Qm (C.F.M.)	0.442	0.606	0.729	0.839	0.928
Km (Std Pressure)	0.825	0.797	0.779	0.777	0.769
DELTA Ha	1.51	1.60	1.65	1.65	1.68
Average Y (Meter Calibration Factor)				0.999	
Average Km (Standard Pressure)				0.789	
Average DELTA Ha of Orifice				1.617	

Y = ≤ .03
Max & Min ≤ .02 from Avg
Final Avg within 5% of Initial Avg
ΔHa = Max & Min ≤ .2 from Avg

**FINAL
METER CALIBRATION FORM - DGM**

DATE:	05-05-95	Box No.	S-101
Ref. DGM Ser. #	1044453	Calibrated By	Edward Harris
RUN #	1	2	3
DELTA H (DGM)	1.5	1.5	1.5
Y (Ref. DGM)	0.995	0.995	0.995
Reference DGM			
Gas Vol. Initial	716.400	722.300	728.395
Gas Vol. Final	722.300	728.395	735.398
Meter Box DGM			
Gas Vol. Initial	778.600	784.484	790.565
Gas Vol. Final	784.484	790.565	797.520
Reference DGM			
Temp.	Avg.	Avg.	Avg.
Deg F Initial	79	79	80
Deg F Final	79	79	80
Meter Box DGM			
Temp. Initial In	80	80	80
Temp. Initial Out	80	80	80
Temp. Final In	80	80	80
Temp. Final Out	80	80	80
P Bar IN. Hg	30.10	30.10	30.10
Time (sec.)	488	506	580
Meter Calibration			
Factor (Y)	0.996	0.995	0.998
Qm (C.F.M.)	0.711	0.709	0.709
Km (Std Pressure)	0.740	0.737	0.738
DELTA Ha	1.63	1.64	1.64
Average Y (Meter Calibration Factor)			0.997
Initial Y (Meter Calibration Factor)			0.999
Percent Error			0.20%
Average Km (Standard Pressure)			0.738
Average DELTA Ha of Orifice			1.64

MAGEHELIC CALIBRATION

BOX	175	S101	173	S-318	C-133
SER. NO.	R01126 YC2	R-22D	R20208 A617	R74D	91126A M91
RANGE	0-2	0-2	0-2	0-5	0-2
REFERENCE READING	FIELD DEVICE READING				
0.000	0.00	0.00	0.00	0.00	0.00
0.050					
0.150					
0.200					
0.250					
0.450					
0.50	0.49	0.50			0.500
1.00	1.00	0.97			1.000
1.30					
1.80	1.77	1.77			1.83
2.50					
4.50					
5.0					
9.0					
13.0					
22.0					

SIGNATURE: Edward A. Harris

DATE: 12/27/94

MAGEHELIC CALIBRATION

BOX	460	S-100	2879
SER. NO.	91127W W137		R-33D
RANGE	0-2	0-2	0-2
REFERENCE READING	FIELD DEVICE READING		
0.000	0.00	0.00	0.00
0.050			
0.150			
0.200			
0.250			
0.450			
0.50	0.50	0.52	0.51
1.00	1.00	1.02	1.00
1.30			
1.80	1.83	1.83	1.77
2.50			
4.50			
5.0			
9.0			
13.0			
22.0			

SIGNATURE:

Edward A. Klemis

DATE:

12/27/94

MAGEHELIC CALIBRATION

BOX #1

SER. NO.	10720- AB68	R1061- 6AG48	R5031- SE376	R1062- 9JA82	R1051- 3MR42	R90124 RI119
RANGE	0-0.25	0-0.50	0-2	0-5	0-10	0-25
REFERENCE READING	FIELD DEVICE READING					
0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.050	0.050					
0.150	0.150	0.150				
0.200	0.200					
0.250		0.250				
0.450		0.450				
0.50			0.50			
1.00			1.00			
1.30				1.30		
1.80			1.80			
2.50				2.50	2.5	
4.50				4.50		
5.0					5.0	5.0
9.0					9.0	
13.0						14.0
22.0						21.0

SIGNATURE: Edward L. Harris

DATE: 12/27/94

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MAGEHELIC CALIBRATION
BOX #2

SER. NO.	10819-DR2	R1090-2AG18	R50315-EB93	R1062-9TA87	30830-AM79	R1072-2MCS
RANGE	0-0.25	0-0.50	0-2	0-5	0-10	0-25
REFERENCE READING	FIELD DEVICE READING					
0.000	0.000	0.000	0.00	0.00	0.0	0.0
0.050	0.058					
0.150	0.161	0.151				
0.200	0.210					
0.250		0.255				
0.450		0.450				
0.50			0.51			
1.00			1.02			
1.30				1.32		
1.80			1.82			
2.50				2.61	2.6	
4.50				4.52		
5.0					5.0	5.2
9.0					8.9	
13.0						13.0
22.0						21.7

SIGNATURE:

Edward L. Harris

DATE:

12/27/91

MAGEHELIC CALIBRATION
BOX #3

SER. NO.	R900723	R0112542	R10608
	MRR1		CF20
RANGE	0-0.50	0-2.0	0-10
REFERENCE READING	FIELD DEVICE READING		
0.000	0.00	0.00	0.0
0.050			
0.150	0.15		
0.200			
0.250	0.240		
0.450	0.450		
0.50		0.52	
1.00		1.00	
1.50			
1.80		1.85	
2.50			2.5
4.50			
5.0			5.0
9.0			9.2
13.0			
22.0			

SIGNATURE:

Edward R. Harris

DATE:

12/22/84

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MAGEHELIC CALIBRATION
BCX #4

SER. NO.	R22D	R90051	R90101
		6GT21	5CD102
RANGE	0-0.50	0-5	0-25
REFERENCE READING	FIELD DEVICE READING		
0.000	0.000	0.00	0.0
0.050			
0.150	0.154		
0.200			
0.250	0.256		
0.450	0.455		
0.50			
1.00			
1.30		1.32	
1.80			
2.50		2.55	
4.50		4.59	
5.0			5.0
9.0			
13.0			13.0
22.0			22.0

SIGNATURE: Edward A. Harris

DATE: 12/03/94

TEMPERATURE CALIBRATIONS - DEGREES FAHRENHEIT

REFERENCE DEVICE READING*	0 DEG. F	210 DEG.	420 DEG.	630 DEG.	840 DEG.	1050 DEG.	1260 DEG.	1470 DEG.	1680 DEG.	1900 DEG.
2879	-2	209	420	629	838	1049	1259	1469	1679	1899
METER BOX #1 C-133 11580	0	209	416	624	833	1044	1255	1462	1674	1900
METER BOX #3 C-173 S11-24										
METER BOX #2 C-175 15982	0	208	417	628	839	1052	1265	1474	1678	1905
METER BOX #4 D-460 15751	0	206	417	624	839	1057	1273	1486	1690	1903
METER BOX #5 S-100 15751	-2	203	412	622	837	1055	1272	1484	1690	1900
METER BOX #8 S-101 15751	0	209	416	624	833	1045	1255	1463	1679	1904
PORTABLE THERMOCOUPLE # 1 (Yellow)	0	210	419	632	840	1050	1260	1470	1680	1900
PORTABLE THERMOCOUPLE # 2 (Blue)	0	209	416	625	839	1055	1270	1480	1684	1891
PORTABLE THERMOCOUPLE # 2 (Green)										
PINK T83658	0	209	417	629	843	1060	1275	1490	1693	1903

DATE: 12-27-94

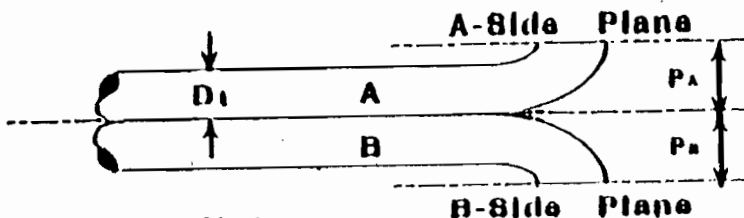
SIGNATURE: *Edward R. Harris*

* Reference Device is an Omega Engineering CL505-A calibrated reference thermocouple-potentiometer system.



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 Mobile, Al. 36686 FAX: (205) 833-2285

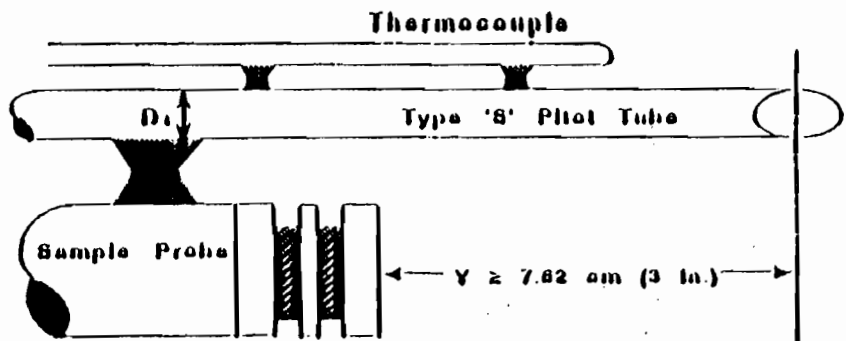


Notes:

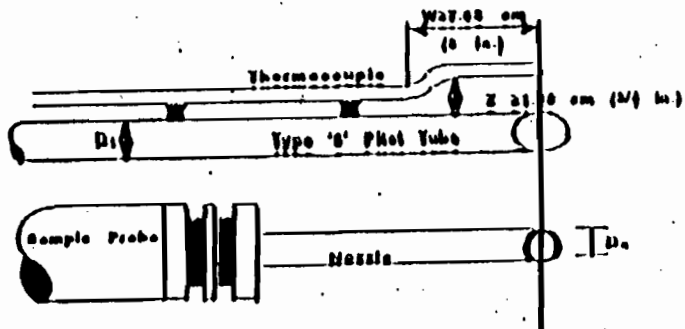
$1.05 D_1 \leq 1.50 D_2$

$P_1 = P_2$

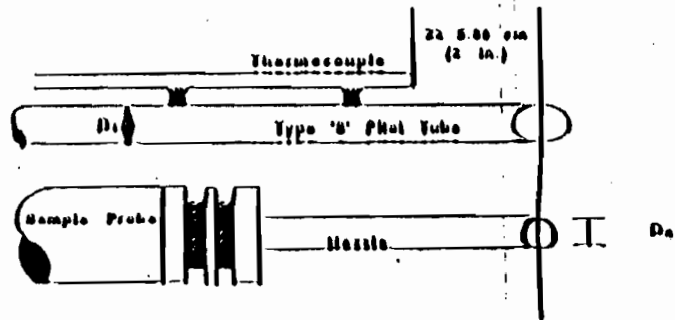
The Pilot used was within the following geometric specifications:
 D_1 between 0.48 and 0.95 cm (3/16 and 3/8 in.)
 $C_p = 0.84$



Minimum pilot-sample probe separation needed to prevent interference



OR



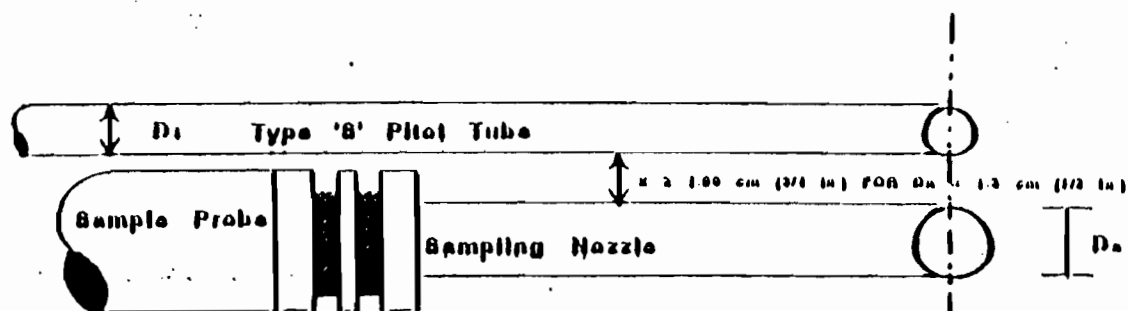
Proper thermocouple placement to prevent interference.



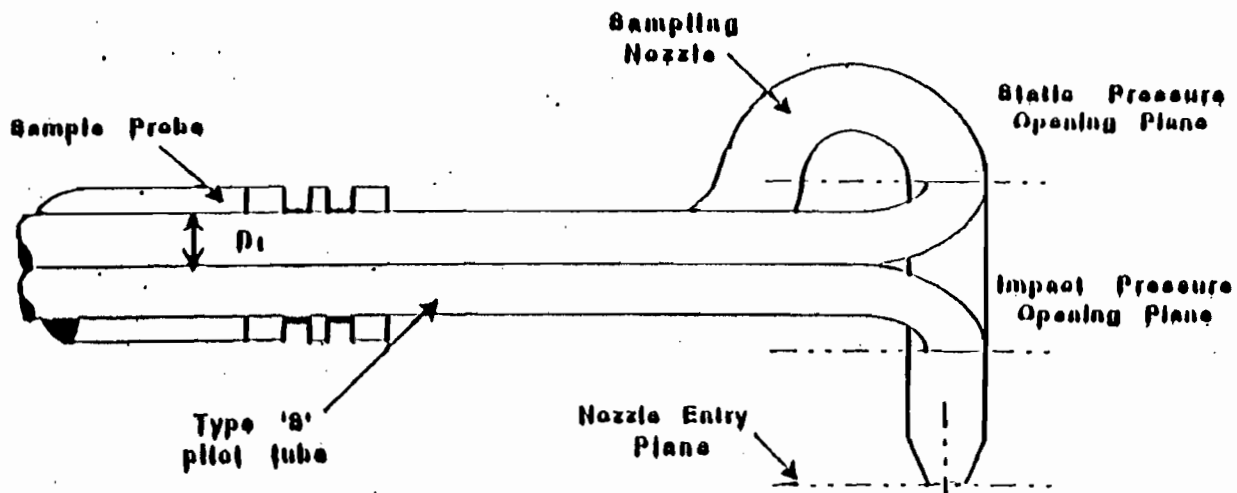
**SANDERS ENGINEERING &
ANALYTICAL SERVICES, Inc.**

1668 J.eroy Stevens Rd. Office: (205) 833-4120
McAlle, AL 36605 FAX: (205) 833-2265

Proper pilot tube-sampling nozzle configuration to prevent aero-dynamic interference; hollowhook type nozzle; centers of nozzle and pilot opening aligned; D_1 between 0.48 and 0.85 cm (3/16 and 3/8 in.)



Bottom view showing minimum pilot/nozzle separation



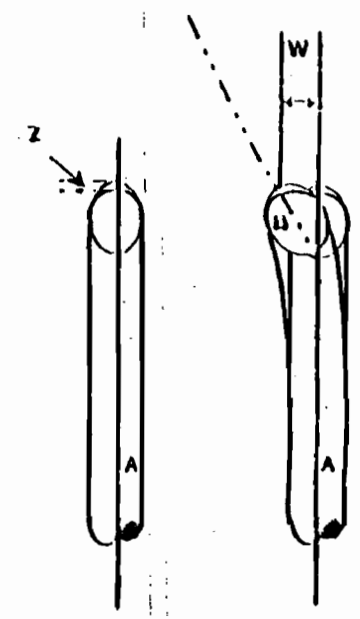
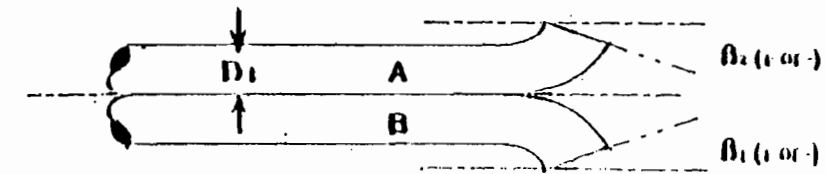
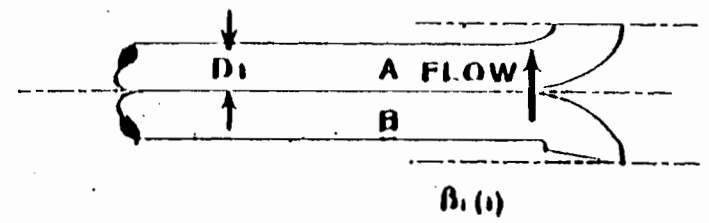
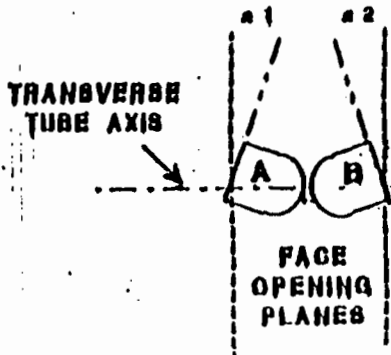
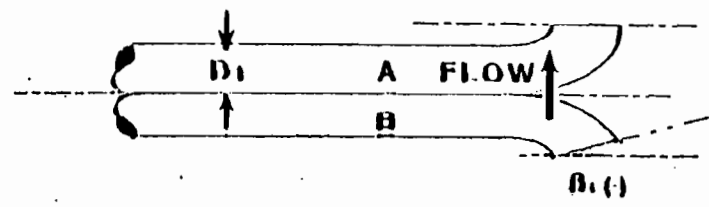
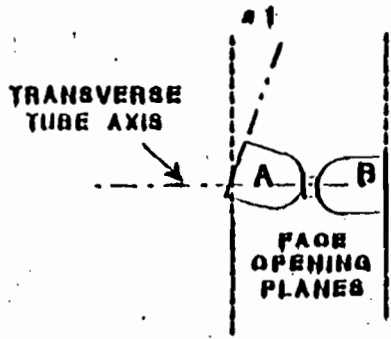
Side view; to prevent pilot tube from interfering with the gas flow streamlines approaching the nozzle, the impact pressure opening plane of the pilot tube shall be even with or above the nozzle entry plane.

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 Mobile, AL 36686 FAX#: (205) 833-2286

Types of face-opening misalignment that can result from field use or improper construction of type 'S' pilot tubes. These will not affect the baseline value of $C_p(\alpha)$ so long as α_1 and $\alpha_2 < 10^\circ$, θ_1 and $\theta_2 < 6^\circ$, and $d < 0.32$ cm (1/8 in.)



APPENDIX D OPERATIONAL DATA

**CRIST ELECTRIC GENERATING PLANT
PARTICULATE COMPLIANCE TEST CHRONOLOGY
UNIT # 4
SOOTBLOWING CONDITIONS
April 25, 1995**

RUN # 1	START	9:06 a.m.	No problems noted at beginning of run.
	STOP	10:12 a.m.	No problems noted at end of run.
RUN # 2	START	10:55 a.m.	No problems noted at beginning of run.
	STOP	11:56 a.m.	No problems noted at end of run.
RUN # 3	START	12:36 p.m.	No problems noted at beginning of run.
	STOP	1:42 p.m.	No problems noted at end of run.

**CRIST ELECTRIC GENERATING PLANT
PARTICULATE COMPLIANCE TEST CHRONOLOGY
UNIT # 4
STEADY STATE CONDITIONS
April 26,1995**

RUN # 1	START STOP	7:52 a.m. 8:58 a.m.	No problems noted at beginning of run. No problems noted at end of run.
RUN # 2	START STOP	.9:18 a.m. 10:23 a.m.	No problems noted at beginning of run. No problems noted at end of run.
RUN # 3	START STOP	10:45 a.m. 11:51 p.m.	No problems noted at beginning of run. No problems noted at end of run.

**CRIST ELECTRIC GENERATING PLANT
 PARTICULATE COMPLIANCE TEST
 SIX - MINUTE OPACITY AVERAGES
 UNIT #4
 SOOT BLOWING CONDITIONS
 April 25, 1995**

TIME OF 6 MIN. AVERAGE	OPACITY (%)
(RUN # 1)	(RUN # 1)
8:01 - 8:06	4.0
8:07 - 8:12	4.1
8:13 - 8:18	4.5
8:19 - 9:24	4.3
9:25 - 9:30	4.3
9:31 - 9:36	4.2
(RUN # 2)	(RUN # 2)
10:55 - 11:00	3.7
11:01 - 11:06	3.6
11:07 - 11:12	3.6
11:13 - 11:18	3.5
11:19 - 11:24	3.4
11:25 - 11:30	4.0
11:31 - 11:36	3.7
11:37 - 11:42	3.3
11:43 - 11:48	3.5
11:49 - 11:54	3.6
11:55 - 12:00	3.4

**CRIST ELECTRIC GENERATING PLANT
PARTICULATE COMPLIANCE TEST
SIX - MINUTE OPACITY AVERAGES
UNIT # 4
SOOT BLOWING CONDITIONS
April 25, 1995**

(RUN # 3)	(RUN # 3)
12:31.- 12:36	3.5
12:37.- 12:42	3.7
12:43 - 12:48	4.0
12:49 - 12:54	3.9
12:55 - 13:00	3.7
13:01 - 13:06	3.4
13:07 - 13:12	3.6
13:13 - 13:18	3.4
13:19 - 13:24	3.8
13:25 - 13:30	3.6
13:31 -.13:36	3.5
13:37 - 13:42	4.0

**CRIST ELECTRIC GENERATING PLANT
PARTICULATE COMPLIANCE TEST
SIX - MINUTE OPACITY AVERAGES**

UNIT # 4

STEADY STATE CONDITIONS

April 26, 1995

TIME OF 6 MIN. AVERAGE	OPACITY (%)
(RUN # 1)	(RUN # 1)
7:49 - 7:54	4.2
7:55 - 8:00	4.0
8:01 - 8:06	3.8
8:07 - 8:12	3.6
8:13 - 8:18	3.4
8:19 - 8:24	3.4
8:25 - 8:30	3.2
8:31 - 8:36	3.3
8:37 - 8:42	3.2
8:43 - 8:48	3.4
8:49 - 8:54	3.3
8:55 - 9:00	3.7
(RUN # 2)	(RUN # 2)
9:13 - 9:18	3.3
9:19 - 9:24	3.3
9:25 - 9:30	3.3
9:31 - 9:36	3.2
9:37 - 9:42	4.5
9:43 - 9:48	3.4
9:49 - 9:54	3.4
6:55 - 10:00	3.3
10:01 - 10:06	3.5
10:07 - 10:12	3.2
10:13 - 10:18	3.3
10:19 - 10:24	3.3

**CRIST ELECTRIC GENERATING PLANT
PARTICULATE COMPLIANCE TEST
SIX - MINUTE OPACITY AVERAGES**

UNIT # 4

STEADY STATE CONDITIONS

April 26, 1995

(RUN # 3)	(RUN # 3)
10:43 - 10:48	3.3
10:49 - 10:54	3.1
10:55 - 11:00	3.2
11:01 - 11:06	3.1
11:07 - 11:12	3.2
11:13 - 11:18	3.1
11:19 - 11:24	3.2
11:25 - 11:30	3.0
11:31 - 11:36	3.1
11:37 - 11:42	3.0
11:43 - 11:48	3.0
11:49 - 11:54	3.4

CRIST ELECTRIC GENERATING PLANT
 PARTICULATE COMPLIANCE TEST: UNIT # 4
 PRECIPITATOR READINGS

COLD PRECIPITATOR

TEST: Steady State

DATE: 05/26/95

RUN #: 1

Start or End Start

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4-A	31	420	370	18
4-B	28	340	300	NO READING
4-C	34	NO READING	190	19

TEST: Steady State

DATE: 05/26/95

RUN #: 1

Start or End End

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4-A	31	420	370	18
4-B	28	340	300	NO READING
4-C	34	NO READING	190	19

**CRIST ELECTRIC GENERATING PLANT
PARTICULATE COMPLIANCE TEST: UNIT # 4
PRECIPITATOR READINGS**

HOT PRECIPITATOR

TEST: Steady State

DATE: 5/26/95

RUN #: 1

Start or End Start

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4A	25	270	210	NO READING
4B	25	250	200	36
4C	80	340	480	52
4D	80	300	660	58
4E	60	320	440	50
4F	70	300	500	50

RUN #: 1

Start or End End

4A	25	270	210	NO READING
4B	40	260	250	36
4C	80	340	480	52
4D	80	300	660	58
4E	60	320	440	50
4F	70	300	500	55

CRIST ELECTRIC GENERATING PLANT
 PARTICULATE COMPLIANCE TEST: UNIT # 4
 PRECIPITATOR READINGS

COLD PRECIPITATOR

TEST: Steady State

DATE: 05/26/95

RUN #: 2

Start or End Start

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4-A	31	420	370	18
4-B	28	340	300	NO READING
4-C	34	NO READING	190	19

TEST: Steady State

DATE: 05/26/95

RUN #: 2

Start or End End

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4-A	31	420	370	18
4-B	28	340	300	NO READING
4-C	34	NO READING	190	19

**CRIST ELECTRIC GENERATING PLANT
PARTICULATE COMPLIANCE TEST: UNIT # 4
PRECIPITATOR READINGS**

HOT PRECIPITATOR

TEST: Steady State

DATE: 5/26/95

RUN #: 2

Start or End Start

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4A	25	270	210	NO READING
4B	40	260	250	36
4C	80	340	480	52
4D	80	300	660	58
4E	60	320	440	50
4F	70	300	500	52

RUN #: 2

Start or End End

4A	40	260	280	NO READING
4B	30	250	210	40
4C	80	340	480	52
4D	80	300	650	58
4E	74	375	580	52
4F	70	310	500	52

**CRIST ELECTRIC GENERATING PLANT
PARTICULATE COMPLIANCE TEST: UNIT # 4
PRECIPITATOR READINGS**

COLD PRECIPITATOR

TEST: Steady State

DATE: 05/26/95

RUN #: 3

Start or End Start

Transformer
Box
A

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4-A	31	420	370	18
4-B	28	340	300	NO READING
4-C	34	NO READING	190	19

TEST: Steady State

DATE: 05/26/95

RUN #: 3

Start or End End

Transformer
Box
B

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4-A	31	420	370	18
4-B	28	340	300	NO READING
4-C	34	NO READING	190	19

**CRIST ELECTRIC GENERATING PLANT
PARTICULATE COMPLIANCE TEST: UNIT # 4
PRECIPITATOR READINGS**

COLD PRECIPITATOR

TEST: Steady State

DATE: 05/26/95

RUN #: 3

Start or End Start

Transformer
Box
A

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4-A	31	420	370	18
4-B	28	340	300	NO READING
4-C	34	NO READING	190	19

TEST: Steady State

DATE: 05/26/95

RUN #: 3

Start or End End

Transformer
Box
B

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4-A	31	420	370	18
4-B	28	340	300	NO READING
4-C	34	NO READING	190	19

**CRIST ELECTRIC GENERATING PLANT
PARTICULATE COMPLIANCE TEST: UNIT # 4
PRECIPITATOR READINGS**

HOT PRECIPITATOR

TEST: Steady State

DATE: 5/26/95

Transformer
Box
A

RUN #: 3

Start or End Start

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4A	40	270	280	NO READING
4B	30	250	210	40
4C	80	340	480	52
4D	80	300	650	58
4E	74	375	500	52
4F	70	310	740	52

Transformer
Box
B

RUN #: 3

Start or End End

4A	35	270	200	NO READING
4B	30	250	480	40
4C	85	350	660	52
4D	80	300	570	58
4E	74	350	520	52
4F	70	300	500	52

CRIST ELECTRIC GENERATING PLANT
 PARTICULATE COMPLIANCE TEST: UNIT # 4
 PRECIPITATOR READINGS

COLD PRECIPITATOR

TEST: Soot Blowing

DATE: 05/25/95

RUN #: 1

Start or End Start

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4-A	30	400	360	18
4-B	28	340	300	NO READING
4-C	34	NO READING	190	19

TEST: Soot Blowing

DATE: 05/25/95

RUN #: 1

Start or End End

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4-A	31	420	370	18
4-B	28	340	300	NO READING
4-C	34	NO READING	190	19

**CRIST ELECTRIC GENERATING PLANT
PARTICULATE COMPLIANCE TEST: UNIT # 4
PRECIPITATOR READINGS**

HOT PRECIPITATOR

TEST: Soot Blowing

DATE: 05/25/95

RUN #: 1

Start or End Start

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4A	50	230	200	NO READING
4B	35	240	160	38
4C	85	340	700	55
4D	80	310	640	58
4E	78	375	580	54
4F	68	300	500	54

RUN #: 1

Start or End End

4A	30	250	200	NO READING
4B	40	270	300	38
4C	75	340	480	50
4D	80	300	630	58
4E	74	350	580	54
4F	68	300	500	54

CRIST ELECTRIC GENERATING PLANT
 PARTICULATE COMPLIANCE TEST: UNIT # 4
 PRECIPITATOR READINGS

COLD PRECIPITATOR

TEST: Soot Blowing

DATE: 05/25/95

RUN #: 2

Start or End Start

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4-A	31	420	370	18
4-B	28	340	300	NO READING
4-C	34	NO READING	190	19

TEST: Steady State

DATE: 05/26/95

RUN #: 2

Start or End End

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4-A	31	420	360	18
4-B	28	340	300	NO READING
4-C	34	NO READING	190	19

**CRIST ELECTRIC GENERATING PLANT
PARTICULATE COMPLIANCE TEST: UNIT # 4
PRECIPITATOR READINGS**

HOT PRECIPITATOR

TEST: Soot Blowing

DATE: 05/25/95

RUN #: 2

Start or End Start

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4A	30	250	200	NO READING
4B	40	270	300	38
4C	75	340	480	50
4D	80	300	630	58
4E	74	350	580	54
4F	68	300	500	54

RUN #: 2

Start or End End

4A	35	260	240	NO READING
4B	30	260	300	42
4C	80	340	400	52
4D	80	310	660	58
4E	70	330	560	52
4F	68	300	500	54

**CRIST ELECTRIC GENERATING PLANT
PARTICULATE COMPLIANCE TEST: UNIT # 4
PRECIPITATOR READINGS**

COLD PRECIPITATOR

TEST: Soot Blowing

DATE: 05/25/95

RUN #: 3

Start or End Start

Transformer
Box
A

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4-A	31	420	360	18
4-B	28	340	300	NO READING
4-C	34	NO READING	190	19

TEST: Soot Blowing

DATE: 05/25/95

RUN #: 3

Start or End End

Transformer
Box
B

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4-A	31	420	365	18
4-B	28	335	300	NO READING
4-C	34	NO READING	190	19

**CRIST ELECTRIC GENERATING PLANT
PARTICULATE COMPLIANCE TEST: UNIT # 4
PRECIPITATOR READINGS**

HOT PRECIPITATOR

TEST: Soot Blowing

DATE: 05/25/95

Transformer
Box
A

RUN #: 3

Start or End Start

	Primary Amps (AC AMPS)	Primary Volts (AC Volts)	Secondary Amps (DC mAmps)	Secondary Volts (DC KVolts)
4A	35	260	240	NO READING
4B	30	260	300	42
4C	80	340	400	52
4D	80	310	660	58
4E	70	330	560	52
4F	68	300	500	54

Transformer
Box
B

RUN #: 3

Start or End End

4A	30	240	240	NO READING
4B	30	240	260	42
4C	75	340	360	48
4D	80	300	680	52
4E	72	350	550	52
4F	68	300	520	52

SANDERS ENGINEERING & ANALYTICAL SERVICES, INC.

PARTICULATE EMISSIONS TEST REPORT
STEADY STATE OPERATIONS

FOR

GULF POWER COMPANY

Plant Crist, Unit 5
Pensacola, Florida



April 18, 1996

1568 LEROY STEVENS ROAD

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SANDERS ENGINEERING & ANALYTICAL SERVICES, INC.

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ENVIRONMENTAL ENGINEERING
AIR & WATER QUALITY MODELING
ENVIRONMENTAL ASSESSMENTS
PSD ANALYSIS
EMERGENCY RESPONSE MONITORING

AMBIENT AIR MONITORING
CONTINUOUS IN-STACK MONITORING
SOURCE TESTING
VISIBLE EMISSIONS TESTING
CONSULTING SERVICES

REPORT CERTIFICATION

The sampling and analysis for this report was carried out under my direction and supervision.

Date: 4-30-96

Signature: Edward L. Harris
Edward L. Harris
Environmental Specialist

I have reviewed the testing details and results in this report and hereby certify that the test report is authentic and accurate to the best of my knowledge.

Date: 4-30-96

Signature: Joseph C. Sanders
Joseph C. Sanders
Manager

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1. INTRODUCTION

Sanders Engineering & Analytical Services, Inc. (SEAS) performed particulate emissions testing during steady state operations at Gulf Power Company, Plant Crist, Unit 5, located in Pensacola, Florida. The testing was conducted on April 18, 1996. The testing was performed in accordance with the applicable U.S. EPA procedures specified at **40 CFR, Part 60, Appendix A, Methods 1, 2, 3, 4, and 17.**

The purpose of the test was to demonstrate compliance with the rules and regulations of the Florida Department of Environmental Protection, and to meet the necessary requirements contained in the permit to operate issued by the Florida Department of Environmental Protection.

The test was conducted by Mr. Edward Harris and Mr. Dean Holmes of Sanders Engineering & Analytical Services, Inc., and was coordinated with Mr. John McPherson of Gulf Power Company. The Florida Department of Environmental Protection was notified so their representative could be present to observe the testing.

The test was conducted in accordance with the guidelines of the Florida Department of Environmental Protection. Further discussion of the test methods are included later in the report.

2. SUMMARY AND DISCUSSION OF RESULTS

The results of the particulate emissions test for the steady state runs, along with the results of the computations, are summarized in Table I. The equations used in the calculations of the results, along with the completed field data sheets for the testing, are presented in Appendix A. The sample calculations of the first run are presented in Appendix B. The quality control checks of the equipment used in the sampling program are included in Appendix C.

There were no problems encountered during the performance of the test. The bottom port of the duct was not sampled due to ash build-up. One of the other ports was alternately sampled twice on each run to compensate for the port not sampled. At the completion of each run, the filter and probe were removed to a relatively clean, draft-free area for clean-up.

The results of the testing indicate the particulate emission rate during steady state for Plant Crist, Unit 5, is 0.029 LBS/MMBTU. The applicable Florida Department of Environmental Protection rules and regulations require an emission rate of no greater than 0.10 LBS/MMBTU. The results of the testing indicate that the unit is in compliance with the particulate emission condition of the permit to operate issued by the Florida Department of Environmental Protection.

**TABLE I. PARTICULATE EMISSIONS TEST RESULTS
GULF POWER COMPANY
PLANT CRIST, UNIT 5, STEADY STATE
4/18/96**

Title of Run		<u>RUN 1</u>	<u>RUN 2</u>	<u>RUN 3</u>
Sampling Time -Start	Military	0914	1258	1526
Sampling Time -Stop	Military	1020	1403	1631
F Factor	SDCF/MMBTU	9820	9820	9820
Plant Load	Megawatts	88.0	88.0	88.0
Static Pressure	In. H2O	-0.35	-0.35	-0.35
Barometric Pressure	In. Hg	30.05	30.05	30.05
Average dH	In. H2O	0.966	1.141	1.098
Meter correction		1.024	1.024	1.024
Avg. Meter Temp.	Deg. F	62.1	65.7	68.4
% O2	%	5.3	5.1	5.3
%CO2	%	12.5	12.5	12.5
Volume Metered	ACF	35.676	38.566	37.930
Volume Water	Ml	78.0	82.0	82.0
Sampling Time	Minutes	64	64	64
Nozzle Diameter	Inches	0.222	0.221	0.221
Avg. Stack Temp.	Deg. F	301.4	304.4	306.6
Area of Stack	Sq. Feet	92.1350	92.1350	92.1350
Wt. of Part.	Mg.	41.7	41.3	33.5
Number of Points		32	32	32
Avg. Sqrt dP	In. H2O	0.8161	0.8906	0.8712

RESULTS OF COMPUTATIONS

		<u>RUN 1</u>	<u>RUN 2</u>	<u>RUN 3</u>	<u>Average</u>
Volume of Gas Sampled	SDCF	37.177	39.929	39.068	
H2O vapor in Gas Stream	PERCENT	9.0	8.8	9.0	8.9
Avg. Stack Gas Velocity	FT/SEC	54.7	59.8	58.6	57.7
Volumetric Flow Rate	SDCFM	191,484	208,924	203,728	201,379
Volumetric Flow Rate	ACF/M	302,348	330,553	323,870	318,923
Particulate Conc.	Grs/SDCF	0.017	0.016	0.013	0.015
Particulate Conc.	Grs/ACF	0.011	0.010	0.008	0.010
Particulate Mass Rate	Lb/Hr	28.4	28.5	23.1	26.6
Particulate Mass Rate	Lb/MMBtu	0.032	0.030	0.025	0.029
Heat Input	MMBTU/Hr	873.28	965.02	929.11	922.47
Percent of Isokinetic	%	104.0	103.3	103.7	

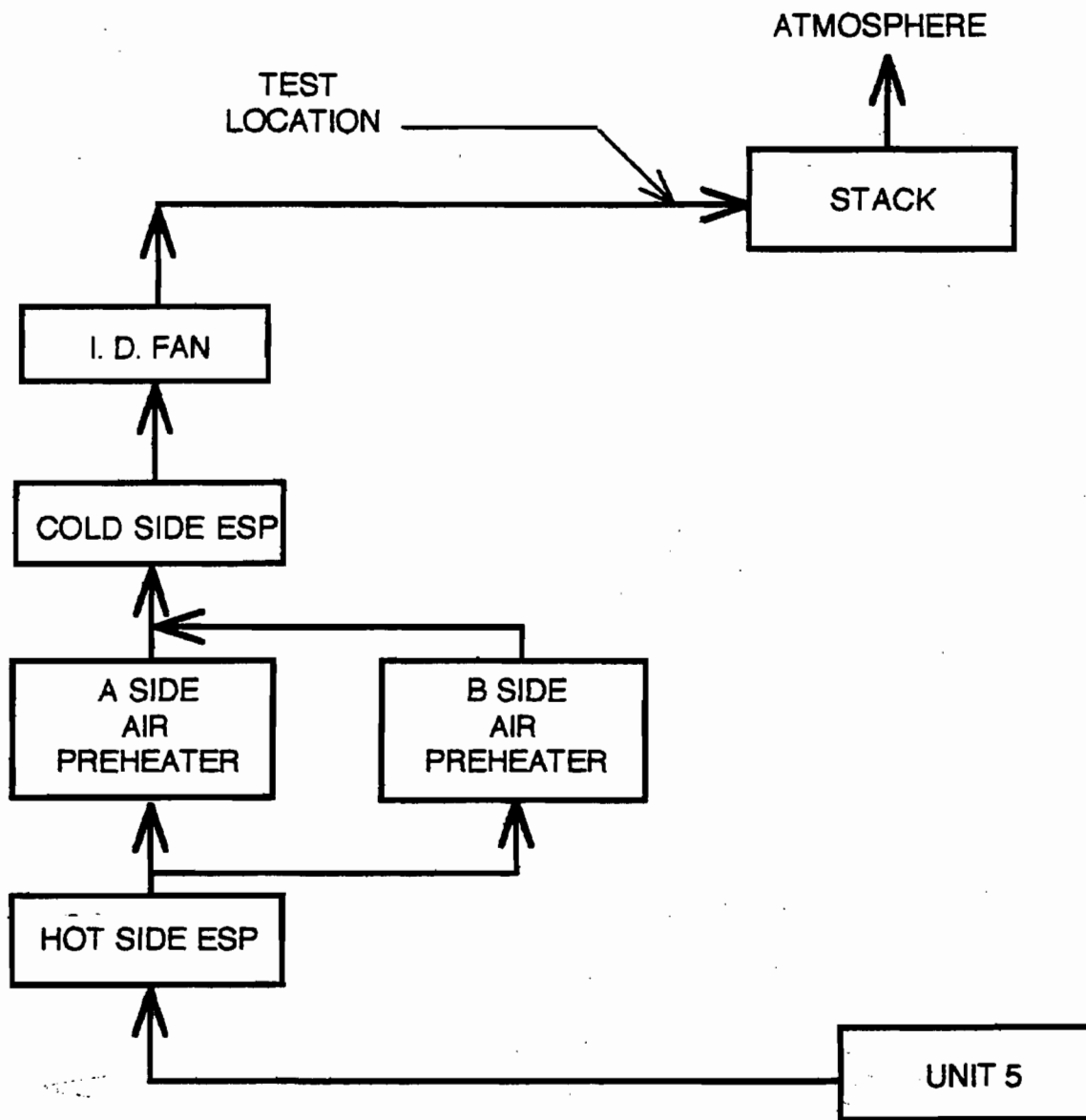
3. PROCESS DESCRIPTION

The process consists of a steam electric generating unit firing bituminous coal for the production of electric energy. The coal is received by barge, and loaded directly onto the conveyor feeding the plant, or onto the stockpile and later loaded onto the conveyor belt transporting the coal to the plant. The coal from the conveyor is loaded into bunkers capable of holding between 36 to 48 hours supply of coal. The coal is then fed to pulverizing mills before being fired in the unit through the burners. Upon combustion of the coal in the fire box, approximately 20 percent of the ash falls to the bottom of the boiler and is removed by the ash removal system. The remaining 80 percent exits with the flue gases through the heat exchange and economizer sections of the furnace, and is collected by electrostatic precipitators.

3.1. Source Air Flow

As shown in Figure 1, the flue gases exit the boiler and flow through a hot side precipitator. The exhaust gases are separated into ducts A and B before entering air preheaters. The exhaust gases are combined before entering a cold side ESP. The flue gases exiting the cold side ESP are exhausted through a stack into the atmosphere.

Figure 1. Air Flow Schematic



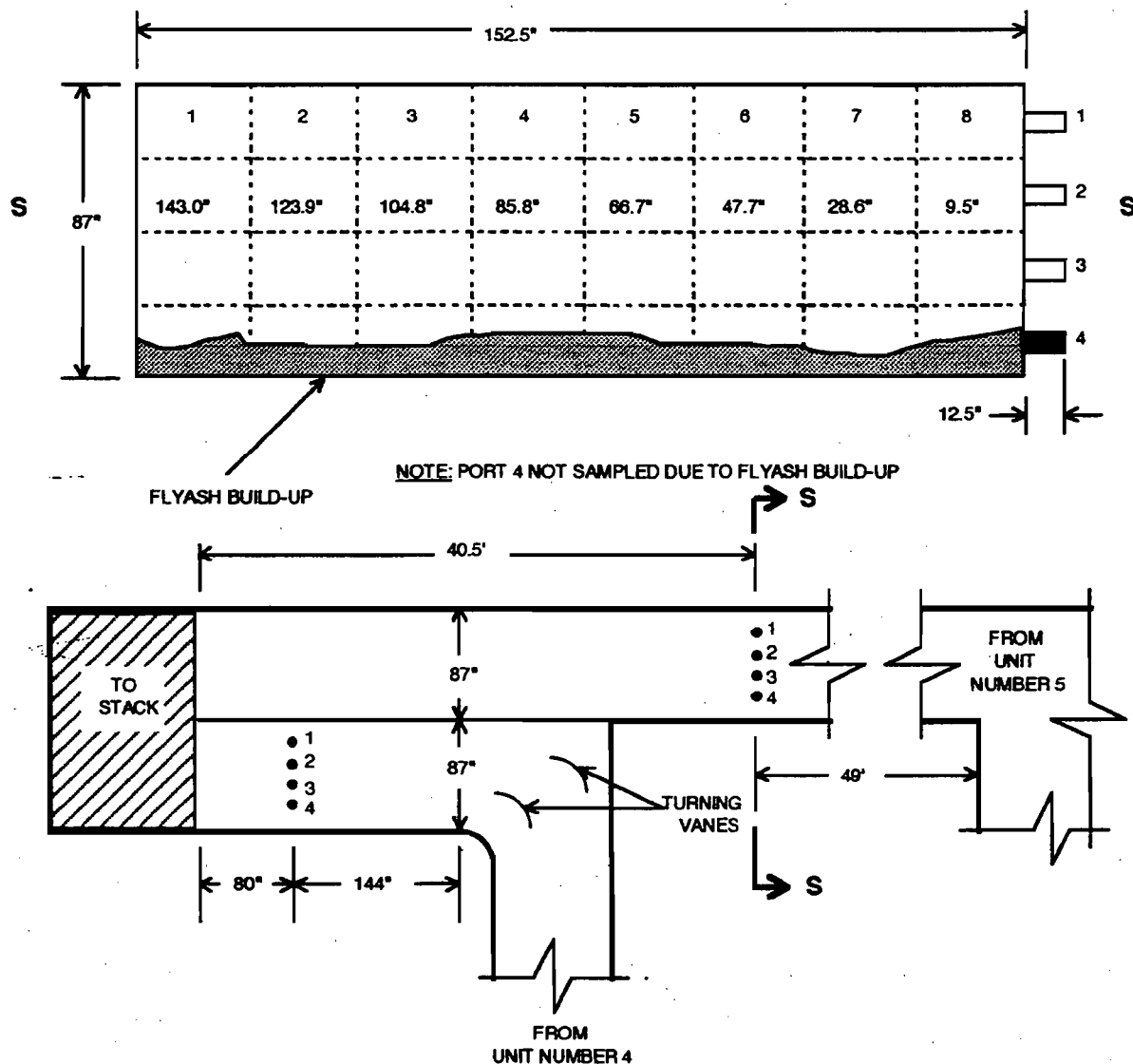
3.2. Operation During Testing

The average heat input during steady state operation, as based on F-factor calculations, was 922.47 million BTU per hour resulting in the production of approximately 88 megawatts of electricity. Precipitator data supplied by Gulf Power personnel is given in Appendix D.

4. SAMPLE POINT LOCATION

The sample point locations and outlet duct schematic are presented in Figure 2. Method 1 was used for determination of the number and location of sampling points. The minimum number of points (25) required for rectangular stacks was met by sampling a total of 32 points.

Figure 2. Sample Point Locations

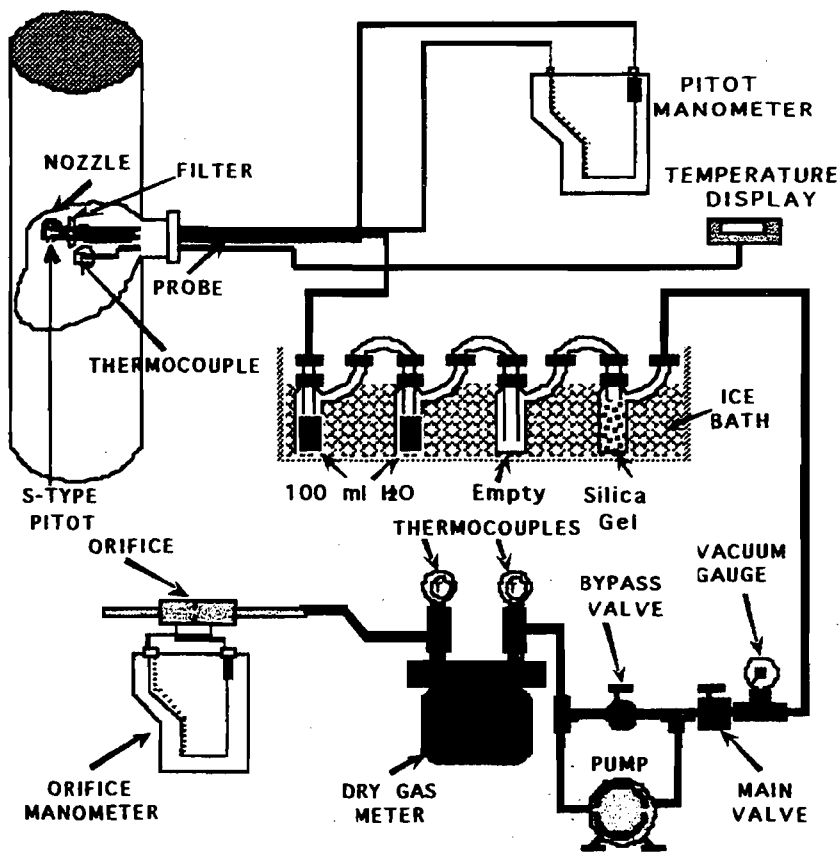


5. PARTICULATE SAMPLING PROCEDURE (EPA Method 17)

The sampling procedure utilized is that specified in 40 CFR, Part 60, Appendix A, Method 17, as modified by the governing regulatory agency. A brief description of this procedure is as follows:

The first impingers were partially filled with 100 milliliters of deionized water. The next impinger was left empty to act as a moisture trap. Preweighed 6 to 16 mesh indication silica gel was added to the last impinger. The sampling equipment manufactured by Lear Siegler (Model 100) or Sanders Engineering

Figure 3. Particulate Sampling Train



(Model 200) was assembled as shown in the attached drawing. The system was leak checked by plugging the inlet to the nozzle and pulling a 15 inch mercury vacuum. A leakage rate not in excess of 0.02 cubic feet per minute was considered acceptable.

The inside dimensions of the stack liner were measured and recorded. The required number of sampling points were marked on the probe for easy visibility. The range of velocity pressure, the percent moisture, and the temperature of the effluent gases were determined. From this data, the correct nozzle size and the nomograph multiplication factor were determined.

Crushed ice was placed around the impingers. The nozzle was placed on the first traverse point with the tip pointing directly into the gas stream. The pump was started immediately and the flow was adjusted to isokinetic sampling conditions. After the required time interval had elapsed, the probe was repositioned to the next traverse point and isokinetic sampling was re-established. This was performed for each point until the run was completed. Readings were taken at each point and recorded on the field data sheet. At the conclusion of each run, the pump was turned off and the final readings were recorded.

5.1. Particulate Sample Recovery

Care was exercised in moving the collection train to the sample recovery area to minimize the loss of collected sample, or the gain of extraneous particulate matter. The volume of water in the impingers was measured, the silica gel impinger was weighed and recorded on the field data sheet. The nozzle, and all sample-exposed surfaces were washed with reagent grade acetone into a clean sample container. A brush was used to loosen any adhering particulate matter and subsequent washings were placed into the container. The filter was carefully removed from the fritted support and placed in a clean separate sample container. A sample of the acetone used in the washing was saved for a blank laboratory analysis.

5.2. Particulate Analytical Procedures

The filter and any loose particulate matter were transferred from the sample container to a clean, tared weighing dish. The filter was placed in a desiccator for at least 24 hours and then weighed to the nearest 0.1 milligram until a constant weight was obtained. The original weight of the filter was deducted, and the weight gain was recorded to the nearest 0.1 milligram.

The wash solution was transferred to a clean, tared beaker. The solution was evaporated to dryness, desiccated to a constant weight, and the weight gain was recorded to the nearest 0.1 milligram.

APPENDIX A EQUATIONS AND FIELD DATA SHEETS

EQUATIONS

1.
$$P_s = P_{bar} + \frac{P_g}{13.6}$$
2.
$$P_m = P_{bar} + \frac{\overline{\Delta H}}{13.6}$$
3.
$$V_s = K_p C_p \sqrt{\Delta P} \sqrt{\frac{\overline{T_s}}{M_s P_s}}$$
4.
$$V_{m(Std)} = K_1 V_m Y \left[\frac{P_{bar} + \frac{\overline{\Delta H}}{13.6}}{\overline{T_m}} \right]$$
5.
$$V_w(Std) = 0.04707 V_{1c}$$
6.
$$B_{ws} = \frac{V_w(Std)}{V_{m(Std)} + V_w(Std)}$$
7.
$$M_d = 0.44 (\%CO_2) + 0.32 (\%O_2) + 0.28 (\%N_2 + \%CO)$$
8.
$$M_s = M_d(1 - B_{ws}) + 18(B_{ws})$$
9.
$$EA = \left[\frac{(\%O_2 - 0.5 (\%CO))}{0.264 (\%N_2) - ((\%O_2) - 0.5 (\%CO))} \right] 100$$

$$10. \quad Q_a = (V_s) (A_s) (60)$$

$$11. \quad Q_s = Q_a (1 - B_{ws}) \frac{(528)}{T_s} \frac{(P_s)}{29.92}$$

$$12. \quad E_H = \left(\frac{PMR}{H_1} \right)$$

$$13. \quad E = C_d F_{O_2} \left(\frac{20.9}{20.9 - \%O_2} \right)$$

$$14. \quad C_s = 0.0154 \frac{M_n}{V_{m(Std)}}$$

$$15. \quad C_{50} = \frac{21 C_s}{21 - [(1.5) (\%O_2) - 0.133 (N_2) - 0.75 (\%CO)]}$$

$$16. \quad C_{12} = \frac{C_s (12)}{\%CO_2}$$

$$17. \quad PMR = (C_s) (Q_s) \frac{(60)}{7000}$$

$$18. \quad V_n = \left[(0.002669) (V_{1c}) + \frac{V_m Y}{T_m} \left(P_{bar} + \frac{\overline{\Delta H}}{13.6} \right) \right] \frac{\overline{T_s}}{P_s}$$

$$19. \quad I = \frac{100 V_n}{(60) \emptyset V_s A_n}$$

NOMENCLATURE

- A_n = Cross-sectional area of nozzle, ft²
- A_s = Cross sectional area of stack, ft²
- B_{wa} = Water vapor in the gas stream,
proportion by volume (dimensionless)
- C_p = Pitot tube coefficient (dimensionless) (0.84)
- C_s = Particulate concentration, grains/SCDF
- C_d = Particulate concentration, lbs/SCDF
- C_{12} = Particulate concentration (C_s adjusted to 12% CO)
grains/SCDF
- C_{50} = Particulate concentration (C_s adjusted to 50% excess air)
grains/SCDF
- EA = Excess air, %
- E = Emission in lb/mmBTU
- E_H = Emission in lb/mmBTU, based on heat input
- H_I = Total Heat Input, Million BTU per Hour (MMBTU/hr)
- I = Percent of isokinetic sampling
- K_1 = 17.64 °R/ inches Hg
- K_p = Pitot tube constant,
$$85.49 \text{ ft/sec} \left[\frac{(\text{lb/lb-mole}) (\text{in. Hg})}{(^\circ\text{R}) (\text{inc. H}_2\text{O})} \right]^{\frac{1}{2}}$$
- M_n = Total amount of particulate collected, mg
- M_d = Molecular weight of stack gas; dry basis, lb/lb mole
- M_s = Molecular weight of stack gas; wet basis, lb/lb mole
- P_{bar} = Barometric pressure at the sampling site, in. Hg

NOMENCLATURE (continued)

- P_m = Meter pressure, in. Hg
- P_s = Absolute stack pressure, in. Hg
- P_g = Stack static pressure, in. H₂O
- PMR = Particulate mass rate, lb/Hr
- Q_a = Volumetric flow rate ACFM
- Q_s = Volumetric flow rate SDCFM
- V_s = Average stack gas velocity, ft/sec
- V_{lc} = Total volume of liquid collected in impingers & silica gel, ml
- V_m = Volume of gas sample as measured by dry gas meter, ACF
- $V_{m(std)}$ = Volume of gas sample measured by dry gas meter,
corrected to standard conditions, SDCF
- $V_{w(std)}$ = Volume of water vapor in gas sample, corrected to standard
conditions, SCF
- V_n = Volume collected at stack conditions through nozzle, ACF
- Y = Dry gas meter calibration factor (dimensionless)
- ΔH = Average pressure difference of orifice, in. H₂O
- ΔP = Velocity head of stack gas, in. H₂O
- $\sqrt{\Delta P}$ = Average of square roots of the velocity pressure, in. H₂O
- \emptyset = Total sampling time, minutes
- %CO₂, %O₂, N₂, %CO - Number % by volume, dry basis, from gas analysis
- F_{O_2} = Oxygen based F factor (9820 SDCF/mmBTU for bituminous coal)
- T_s = Temperature of the stack, °R (° F + 460)



SANDERS ENGINEERING & ANALYTICAL SERVICES, Inc.

1568 Leroy Stevens Rd.
Mobile, AL 36695

Office: (205) 533-4120
FAX#: (205) 633-2285

FIELD DATA SHEET

COMPANY GPCO DATE 4-18-96 DGM# S-101
 PLANT Crist OPERATOR ELH ΔHa 0.74
 UNIT # S ^{Seal} ~~Steady State~~ METHOD 17 PROBE N/A _{liner} ^{12'} _{length}

RUN 1

NOZZLE DATA RUN 8

NOZZLE CALIBRATION	PRE	POST	FILTER NUMBER
	.222	.222	
	.222	.222	
	.222	.222	<u>1365</u>
	.222	.222	
AVERAGE	AVERAGE		

RUN 2

NOZZLE DATA RUN 10

NOZZLE CALIBRATION	PRE	POST	FILTER NUMBER
	.221	.221	
	.221	.221	
	.221	.221	<u>1366</u>
	.221	.221	
AVERAGE	AVERAGE		

RUN 3

NOZZLE DATA RUN 11

NOZZLE CALIBRATION	PRE	POST	FILTER NUMBER
	.221	.221	
	.221	.221	
	.221	.221	<u>1367</u>
	.221	.221	
AVERAGE	AVERAGE		

METER READING

FINAL	403.576
INITIAL	367.900
NET	35.676

METER READING

FINAL	443.966
INITIAL	405.400
NET	38.566

METER READING

FINAL	483.230
INITIAL	445.300
NET	37.930

LEAK CHECK

SYSTEM		PITOT	
Pre	Post	Pre	Post
15	10	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>
0.000	0.000	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>
in. Hg	in. Hg	static	static
cm	cm		

LEAK CHECK

SYSTEM		PITOT	
Pre	Post	Pre	Post
15	12	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>
0.000	0.000	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>
in. Hg	in. Hg	static	static
cm	cm		

LEAK CHECK

SYSTEM		PITOT	
Pre	Post	Pre	Post
15	10	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>
0.000	0.000	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>
in. Hg	in. Hg	static	static
cm	cm		

VOLUME OF LIQUID WATER COLLECTED

IMP. 1	IMP. 2	IMP. 3	IMP. 4
1166	107	0	1579.0
100	100	0	1567.0
666	0	0	120
NET	NET	NET	NET
			TOTAL <u>78.0</u>

VOLUME OF LIQUID WATER COLLECTED

IMP. 1	IMP. 2	IMP. 3	IMP. 4
174	100	0	1587.6
100	100	0	1579.0
74	0	0	8.0
NET	NET	NET	NET
			TOTAL <u>82.0</u>

VOLUME OF LIQUID WATER COLLECTED

IMP. 1	IMP. 2	IMP. 3	IMP. 4
172	100	0	1431.0
100	100	0	1421.0
72	0	0	10.0
NET	NET	NET	NET
			TOTAL <u>82.0</u>

GAS ANALYSIS

O ₂	5.3 %	STATIC	-0.35
CO ₂	12.5 %	BAROMETRIC	30.05
CO	-		

GAS ANALYSIS

O ₂	5.1 %	STATIC	-0.35
CO ₂	12.5 %	BAROMETRIC	30.05
CO	-		

GAS ANALYSIS

O ₂	5.3 %	STATIC	-0.35
CO ₂	12.5 %	BAROMETRIC	30.05
CO	-		

Port #	Time	Gas Meter Vol. (cu. ft.)	Vel. Head ΔP in. H ₂ O	Orifice Head ΔH in. H ₂ O	Temperature (F)						Vac. in. H _g		
					Stack	Probe	Hot Box	Imp.	Gas Meter				
									In	Out			
3-1	9:14	367.900	.65	.94	297	N/A	N/A	53	60	60	2	.72	29
2	:16	369.100	.64	.92	301			✓	60	60	2	.70	30
3	:18	370.100	.52	.75	303			✓	60	60	2	.62	30
4	:20	371.100	.53	.76	303			✓	60	60	2	.32	30
5	:22	372.100	.64	.92	302			✓	61	60	2	.43	30
6	:24	373.200	.60	.86	302			✓	60	60	2	.59	30
7	:26	374.250	.65	.94	301			✓	61	60	2	.50	30
8	:28	375.350	.71	1.02	297			✓	61	61	2	.35	29
3-1	:30	376.500	.70	1.01	296			✓	61	61	2		
2	:32	377.700	.68	.98	303			✓	62	61	2		
3	:34	378.800	.52	.75	303			✓	62	61	2		
4	:36	379.800	.50	.72	303			✓	62	62	2		
5	:38	380.800	.65	.94	303			55	62	62	2		
6	:40	381.900	.60	.86	302			✓	62	62	2		
7	:42	382.900	.65	.94	301			✓	62	62	2		
8	:44	383.950	.75	1.08	297			✓	62	62	2		
2-1	9:47	385.120	.70	1.01	297			54	63	62	3		
2	:49	386.300	.59	.85	302			✓	63	62	3		
3	:51	387.500	.75	1.08	304			✓	63	62	3		
4	:53	388.600	.62	.89	303			✓	63	63	3		
5	:55	389.600	.69	1.0	303			✓	63	62	3		
6	:57	390.750	.57	.82	303			✓	64	63	3		
7	:59	391.800	.67	.97	302			✓	64	63	3		
8	10:01	392.900	.70	1.01	299			✓	64	63	3		
1-1	:04	394.010	.90	1.30	299			✓	64	63	4		
2	:06	394.300	.73	1.06	304			56	64	63	4		
3	:08	396.500	.89	1.29	304			✓	64	63	4		
4	:10	397.800	.85	1.23	304			✓	64	63	4		
5	:12	399.050	.70	1.01	303			✓	64	63	4		
6	:14	400.100	.85	1.23	303			✓	64	63	4		
7	:16	401.400	.68	.98	302			✓	64	63	4		
8	:18	402.400	.55	.79	299			✓	64	64	3		

Final 10:20 403.574

Check indicates Temperatures Meet Required Limits.

Company GPCO

Date 4-18-96

Site Crist #5 Steady State

Run # 1

Page 2 Of

DATA RUN #8

DO NOT USE FOR DATA CALCS

9:08
Port 4

Port #	Time	Gas Meter Vol. (cu. ft.)	Vel. Head ΔP in. H ₂ O	Orifice Head ΔH in. H ₂ O	Temperature (F)						Vac. in. H ₂	12:52 Port 4	
					Stack	Probe	Hot Box	Imp.	Gas Meter				
									In	Out			
1-1	12:58	405.400	1.02	1.45	296	N/A	N/A	50	64	64	4	.75	29
2	13:06	406.700	.85	1.21	302			✓	64	64	4	.74	30
3	:02	408.000	1.13	1.61	306			✓	64	64	4	.52	30
4	:04	409.450	.90	1.28	306			✓	64	64	3	.40	30
5	:06	410.600	.75	1.07	305			✓	64	64	3	.50	30
6	:08	411.800	.97	1.38	305			✓	64	64	3	.40	30
7	:10	413.200	.80	1.14	305			✓	65	65	3	.36	30
8	:12	414.400	.60	.85	304			52	65	65	3	.35	30
1-1	:14	415.450	1.01	1.44	305			✓	65	65	4		
2	:16	416.700	.88	1.25	307			✓	65	65	4		
3	:18	418.000	1.25	1.78	306			✓	65	65	5		
4	:20	419.600	.94	1.34	306			✓	66	65	4		
5	:22	420.800	.75	1.07	305			✓	66	65	4		
6	:24	422.000	.96	1.37	305			✓	66	66	5		
7	:26	423.300	.83	1.18	307			✓	66	65	4		
8	:28	424.650	.60	.86	303			✓	66	65	4		
2-1	13:31	425.630	.78	1.11	301			✓	66	66	4		
2	:33	426.800	.68	.97	306			54	66	66	4		
3	:35	427.950	.83	1.18	306			✓	66	66	4		
4	:37	429.200	.63	.90	306			✓	67	66	4		
5	:39	430.300	.72	1.03	306			✓	66	66	4		
6	:41	431.450	.65	.93	305			✓	67	66	4		
7	:43	432.500	.78	1.11	305			✓	67	66	4		
8	:45	433.750	.70	1.00	299			✓	67	66	4		
3-1	:47	434.928	.77	1.10	301			✓	67	66	4		
2	:49	436.100	.74	1.06	304			✓	67	66	4		
3	:51	437.250	.60	.86	306			✓	67	66	4		
4	:53	438.300	.55	.78	307			56	68	67	4		
5	:55	439.350	.75	1.07	306			✓	67	67	4		
6	:57	440.550	.69	.98	306			✓	68	67	4		
7	:59	441.600	.71	1.01	305			✓	68	67	4		
8	:01	442.750	.80	1.14	301			✓	68	67	5		

Do NOT USE FOR RATE CALCS.

Final 14:03 443.966

Check Indicates Temperatures Meet Required Limits.

Company GPCO

Date 4-18-96

Site Crist #5 Steady State

Run # 2

Page 3 Of

* Run 10 For DATA

Port # Point #	Time	Gas Meter Vol. (cu. ft.)	Vel. Head ΔP in. H ₂ O	Orifice Head ΔH in. H ₂ O	Temperature (F)						Vac. in. H ₂	15:21 Port 4	
					Stack	Probe	Hot Box	Imp.	Gas Meter				
									In	Out			
1-1	15:26	445.300	1.10	1.57	300	N/A	N/A	50	67	67	5	.85	30
2	:28	446.600	.85	1.21	304			✓	67	67	4	.73	30
3	:30	447.900	1.23	1.76	308			✓	67	67	5	.60	30
4	:32	449.350	1.02	1.46	309			✓	67	67	4	.40	30
5	:34	450.800	.80	1.15	308			✓	67	67	4	.30	30
6	:36	452.000	.95	1.36	308			✓	67	67	4	.53	30
7	:38	453.300	.74	1.06	307			✓	68	67	4	.30	30
8	:40	454.500	.60	.86	306			✓	68	67	3	.30	30
2-1	:43	455.564	.75	1.07	300			52	68	67	2		
2	:45	456.800	.67	.96	308			✓	68	68	3		
3	:47	457.800	.80	1.15	309			✓	68	68	4		
4	:49	459.050	.60	.86	309			✓	68	68	3		
5	:51	460.100	.70	1.00	309			✓	69	68	3		
6	:53	461.200	.64	.92	309			✓	69	68	3		
7	:55	462.350	.74	1.06	307			✓	69	68	3		
8	:57	463.500	.78	1.12	303			✓	69	68	4		
2-1	:59	464.750	.76	1.09	301			✓	69	68	4		
2	16:01	465.900	.66	.95	308			✓	69	68	4		
3	:03	467.000	.82	1.10	309			✓	69	68	4.5		
4	:05	468.300	.65	.93	309			✓	70	69	4		
5	:07	469.350	.73	1.05	309			✓	70	69	4		
6	:09	470.500	.65	.93	308			✓	70	69	4		
7	:11	471.600	.75	1.08	307			✓	70	69	4		
8	:13	472.750	.79	1.14	302			✓	70	69	5		
3-1	16:15	474.000	.80	1.15	302			57	70	69	5		
2	:17	475.250	.74	1.06	308			✓	70	69	4.5		
3	:19	476.500	.57	.82	309			✓	70	69	4		
4	:21	477.400	.57	.82	309			✓	70	69	4		
5	:23	478.500	.78	1.12	308			✓	69	68	5		
6	:25	479.600	.70	1.01	308			✓	69	69	5		
7	:27	481.050	.75	1.08	307			✓	69	69	5		
8	:29	482.000	.79	1.14	302			✓	69	69	5		

Kelvin
DO NOT USE
FOR DATA
CALCS.

Time 16:31 483.230

Check indicates Temperatures Meet Required Limits.

Company GPCO

Date 4-19-94

Site Crist #5 Steady State

Run # 3

Page 4 Of

Run 11

LABORATORY ANALYSIS & CHAIN OF CUSTODY

COMPANY/PLANT: Hull Power Co.
 UNIT #: 5 DATE OF TEST: 4/18/96 TYPE OF TEST: M-5 M-17 OTHER _____

SAMPLE #	RELINQUISHED BY	RECEIVED BY	TIME	DATE	REASON FOR CHANGE
1365	<i>ETA</i>	<i>JCA</i>	8:30	4/18/96	<i>Analysis</i>
1366					
1367					

UNIT # 5 - Dual Blowing Steady State

RUN # <u>1</u>	FILTER # <u>1365</u>	BEAKER # <u>36</u> WASH (ML) <u>29</u>
FINAL WEIGHT	<u>144.1</u>	<u>67954.2</u>
INITIAL WEIGHT	<u>123.8</u>	<u>67932.8</u>
DIFFERENCE	<u>20.3</u>	<u>21.4</u>
CORRECTED TOTAL WEIGHT		<u>41.7</u>
RUN # <u>2</u>	FILTER # <u>1366</u>	BEAKER # <u>47</u> WASH (ML) <u>34</u>
FINAL WEIGHT	<u>152.0</u>	689690.8 <u>68996.8</u>
INITIAL WEIGHT	<u>122.3</u>	<u>68996.8</u>
DIFFERENCE	<u>29.7</u>	<u>11.6</u>
CORRECTED TOTAL WEIGHT		<u>41.3</u>
RUN # <u>3</u>	FILTER # <u>1367</u>	BEAKER # <u>49</u> WASH (ML) <u>27</u>
FINAL WEIGHT	<u>151.8</u>	<u>65922.1</u>
INITIAL WEIGHT	<u>121.0</u>	<u>65919.4</u>
DIFFERENCE	<u>30.8</u>	<u>2.7</u>
CORRECTED TOTAL WEIGHT		<u>33.5</u>
RUN # _____	FILTER # _____	BEAKER # _____ WASH (ML) _____
FINAL WEIGHT		
INITIAL WEIGHT		
DIFFERENCE		
CORRECTED TOTAL WEIGHT		

UNIT # _____

RUN # _____	FILTER # _____	BEAKER # _____ WASH (ML) _____
FINAL WEIGHT		
INITIAL WEIGHT		
DIFFERENCE		
CORRECTED TOTAL WEIGHT		
RUN # _____	FILTER # _____	BEAKER # _____ WASH (ML) _____
FINAL WEIGHT		
INITIAL WEIGHT		
DIFFERENCE		
CORRECTED TOTAL WEIGHT		
WASH SOLVENT BLANK (ML)	<u>100</u>	BEAKER # <u>18</u> WASH (ML) <u>100</u>
FINAL WEIGHT		<u>67341.7</u>
INITIAL WEIGHT		<u>67341.6</u>
DIFFERENCE		<u>0.1</u>
CORRECTION FACTOR (MG/ML)		<u>0.001</u>

ALL WEIGHTS ARE IN MILLIGRAMS (MG)

APPENDIX B SAMPLE CALCULATIONS

Input and Constants

```

          3
    9820 ft
f := -----
    mm btu

pg := -(0.35 in. H2O)
pbar := 30.05 in. Hg.
Ahavg := 0.966 in. H2O
y := 1.024
tm := 62.1 °F
o2 := 5.3
co2 := 12.5

          3
vm := 35.676 ft
vlc := 78. ml
theta := 64 min
nozdia := 0.222 in.
ts := 301.4 °F

          2
as := 92.135 ft
mn := 41.7 mg
numberofpoints := 32

          0.5
sqrtAp := 0.8161 in. H2O

          lb in. Hg.    0.5
    85.49 1 ft 1 (-----)
          lb-mole °R in. H2O
kp := -----
          1 sec

cp := 0.84

    17.64 °R
k1 := -----
    in. Hg.

```

$$ts = \frac{(ts + 460 \text{ } ^\circ\text{F}) \text{ } ^\circ\text{R}}{\text{ } ^\circ\text{F}}$$

761.4 °R

$$tm = \frac{(tm + 460 \text{ } ^\circ\text{F}) \text{ } ^\circ\text{R}}{\text{ } ^\circ\text{F}}$$

522.1 °R

$$n2 = 100 - o2 - co2$$

82.2

$$an = \frac{\text{nozdia}^2 \text{ } 3.1416}{\frac{12 \text{ in.}^2}{4 \text{ (-----)}} \text{ ft}}$$

0.000268803 ft²

Calculations

Equation 1

$$ps = pbar + \frac{pg}{13.6 \text{ in. H}_2\text{O}}$$

$$\frac{1 \text{ in. Hg.}}$$

30.0243 in. Hg.

Equation 2

$$pm = pbar + \frac{Ahavg}{13.6 \text{ in. H}_2\text{O}}$$

$$\frac{\text{in. Hg.}}$$

30.121 in. Hg.

Equation 3

$$k1 \text{ vm y } (pbar + \frac{Ahavg}{13.6 \text{ in. H}_2\text{O}})$$

$$\frac{\text{in. Hg.}}$$

$$vmstd = \frac{\text{-----}}{tm}$$

37.1784 ft³

Equation 4

$$vwstd = \frac{0.04707 \text{ ft vlc}^3}{ml}$$

3.67146 ft³

Equation 5

$$bws = \frac{vwstd}{vmstd + vwstd}$$

0.0898769

Equation 6

$$md = \frac{(0.44 \text{ co}_2 + 0.32 \text{ o}_2 + 0.28 \text{ n}_2) \text{ lb}}{\text{lb-mole}}$$

$$\frac{30.212 \text{ lb}}{\text{lb-mole}}$$

Equation 7

$$ms = md (1 - bws) + \frac{bws \text{ 18 lb}}{\text{lb-mole}}$$

$$\frac{29.1144 \text{ lb}}{\text{lb-mole}}$$

Equation 8

$$vs = kp \text{ cp } \sqrt{t\Delta p} \left(\frac{ts \text{ 0.5}}{ms \text{ ps}} \right)$$

$$\frac{54.6958 \text{ ft}}{\text{sec}}$$

Equation 9

$$qa = \frac{vs \text{ as } 60 \text{ sec}}{\text{min}}$$

$$\frac{302364. \text{ ft}^3}{\text{min}}$$

Equation 10

$$qs = \frac{qa (1 - bws) 528 \text{ }^\circ\text{R ps}}{ts \text{ 29.92 in. Hg.}}$$

$$\frac{191497. \text{ ft}^3}{\text{min}}$$

Equation 11

$$cs = \frac{0.0154 \text{ gr mn}}{mg \text{ vmstd}}$$

$$\frac{0.0172729 \text{ gr}}{\text{-----}}$$

$$\frac{3}{ft}$$

Equation 12

$$par = \frac{cs \text{ qs } 60 \text{ min}}{\text{-----}}$$

$$\frac{7000 \text{ gr}}{\text{hour -----}}$$

$$\frac{lb}{\text{-----}}$$

$$\frac{28.3518 \text{ lb}}{\text{-----}}$$

$$\text{hour}$$

Equation 13

$$e = \frac{cs \text{ f } 20.9 \text{ l lb}}{\text{-----}}$$

$$\frac{(20.9 - o2) 7000 \text{ gr}}{\text{-----}}$$

$$\frac{0.0324639 \text{ lb}}{\text{-----}}$$

$$\text{mm btu}$$

Equation 14

$$vn = \frac{0.002669 \text{ in. Hg. ft}^3 \text{ vlc} \text{ vm y pm}}{\text{ts} \left(\frac{\text{-----}}{\text{ml } ^\circ\text{R}} + \frac{\text{-----}}{\text{tm}} \right)}$$

$$\frac{\text{-----}}{\text{ps}}$$

$$\frac{3}{58.7275 \text{ ft}}$$

Equation 15

$$i = \frac{100 \% \text{ vn}}{60 \text{ sec theta vs an}} \text{ min}$$

104.021 %

Equation 16

$$hi = \frac{\text{par}}{e} \text{ hour}$$

873.333 mm btu

APPENDIX C QUALITY CONTROL

**INITIAL
METER CALIBRATION FORM - DGM**

DATE: 12-05-95 Box No. S-101

Ref. DGM Ser. #	1044453	Calibrated By			EDWARD HARRIS	
RUN #		1	2	3	4	5
DELTA H (DGM)		0.50	1.00	1.50	2.00	3.00
Y (Ref. DGM)		1.014	1.014	1.014	1.014	1.014
Reference DGM						
Gas Vol. Initial		19.500	25.177	31.500	38.100	45.000
Gas Vol. Final		25.177	31.500	38.100	45.000	51.466
Meter Box DGM						
Gas Vol. Initial		24.400	30.000	36.261	42.805	49.615
Gas Vol. Final		30.000	36.261	42.805	49.615	56.004
Reference DGM						
Temp.		Avg.	Avg.	Avg.	Avg.	Avg.
Deg F Initial		66	67	67	67	67
Deg F Final		67	67	67	67	67
Meter Box DGM						
Temp. Initial In		66	67	68	69	69
Temp. Initial Out		66	67	68	69	69
Temp. Final In		66	67	69	69	69
Temp. Final Out		66	67	69	69	69
P Bar IN. Hg		30.08	30.08	30.08	30.08	30.08
Time (sec.)		873	688	582	525	404
Meter Calibration						
Factor (Y)		1.026	1.022	1.022	1.026	1.023
Qm (C.F.M.)		0.399	0.563	0.695	0.806	0.981
Km (Std Pressure)		0.727	0.726	0.730	0.733	0.730
DELTA Ha		1.77	1.78	1.75	1.73	1.75
Average Y (Meter Calibration Factor)					1.024	
Average Km (Standard Pressure)					0.729	
Average DELTA Ha of Orifice					1.755	

Y = $\leq .03$
 Max & Min $\leq .02$ from Avg
 Final Avg within 5% of Initial Avg
 ΔH_a = Max & Min $\leq .2$ from Avg

POST TEST QUALITY ASSURANCE

Date: 4/30/96

BOX #: S-101

Ref. Meter: 1044453

Calibrated By: Edward Harris

DRY GAS METER

		Unit	Run 1	Run 2	Run 3
FIELD METER	ΔH	In. H ₂ O	1.50	1.50	1.50
	<i>Initial Gas Volume</i>	Ft. ³	52.300	57.450	62.660
	<i>Final Gas Volume</i>	Ft. ³	57.450	62.660	68.750
	<i>Initial Temp. In</i>	°F	70	71	72
	<i>Initial Temp. Out</i>	°F	71	71	72
	<i>Final Temp. In</i>	°F	71	72	73
	<i>Final Temp. Out</i>	°F	70	72	73
REF. METER	Y	<i>Dimensionless</i>	1.014	1.014	1.014
	<i>Initial Gas Volume</i>	Ft. ³	31.300	36.500	41.750
	<i>Final Gas Volume</i>	Ft. ³	36.500	41.750	48.000
	<i>Initial Temp.</i>	°F	70	71	71
	<i>Final Temp.</i>	°F	70	71	71
	Barometric Pressure	In. Hg	29.95	29.95	29.95
	Time	sec	460	465	535
	Meter Calibration Factor	<i>Dimensionless</i>	1.021	1.019	1.040
	ΔH_s	In. H ₂ O	1.777	1.785	1.664
	Average Y	<i>Dimensionless</i>	1.027		
	Initial Y	<i>Dimensionless</i>	1.024		
	Percent Error	%	0.3 (Allowed 5.0%)		

DIFFERENTIAL PRESSURE GAUGE

Ref. Pressure In H ₂ O	Magnehelic Pressure In H ₂ O	Percent Error (+/- 5%)
0.00	0.00	0
0.50	0.51	2
1.50	1.50	0

TEMPERATURE SENSOR

Ref. Temp. (°F)	Thermocouple Temp. (°F)	Percent Error (Allowed 1.5% of Absolute)
280	281	0.14

ARENOLD BAROMETER

Reference Barometer	Test Barometer	0.1 Diff. Allowed
29.70	29.68	-0.02

MAGEHELIC CALIBRATION

BOX	2879	S-100	C-133	C-175	S-102	S-101	S-103
SER. NO.	91126AM 91	9126A M91	R90125 MR6	R74D	R22D	R20208 A617	
RANGE	0-2	0-2	0-2	0-2	0-5	0-2	0-2
REFERENCE READING	FIELD DEVICE READING						
0.000		0.00	0.00	0.00	0.00	0.00	0.00
0.050							
0.150							
0.200							
0.250							
0.450							
0.50	0.50	0.51	0.50	0.51	0.51	0.50	0.50
1.00	0.99	1.01	0.98	1.01	1.01	0.98	1.01
1.30							
1.80	1.80	1.82	1.79	1.82	1.81	1.79	1.82
2.50							
4.50							
5.0							
9.0							
13.0							
22.0							

SIGNATURE:

Edward L. Harris

DATE:

12-5-95

MAGEHELIC CALIBRATION
BOX #1

SER. NO.	10720- AB68	R1061- 6AG48	R5031- SEB76	R1062- 9JA82	R1051- 3MR42	R90124 RI119
RANGE	0-0.25	0-0.50	0-2	0-5	0-10	0-25
REFERENCE READING	FIELD DEVICE READING					
0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.050	0.050					
0.150	0.150	0.140				
0.200	0.190					
0.250		0.250				
0.450		0.450				
0.50			0.50			
1.00			1.00			
1.30				1.30		
1.80			1.80			
2.50				2.50	2.48	
4.50				4.50		
5.0					5.0	5.0
9.0					9.02	
13.0						13.0
22.0						22.0

SIGNATURE:

Edward L. Harris

DATE:

12/22/95

MAGEHELIC CALIBRATION
BOX #2

SER. NO.	10819-DR2	R1090-2AG18	RS0315-EB93	R1062-9TA87	30830-AM79	R1072-2MC5
RANGE	0-0.25	0-0.50	0-2	0-5	0-10	0-25
REFERENCE READING	FIELD DEVICE READING					
0.000	0.000	0.000	0.00	0.00	0.0	0.0
0.050	0.050					
0.150	0.155	0.152				
0.200	0.205					
0.250		0.256				
0.450		0.456				
0.50			0.52			
1.00			1.04			
1.30				1.32		
1.80			1.83			
2.50				2.55	2.49	
4.50				4.50		
5.0					4.9	5.2
9.0					8.8	
13.0						12.9
22.0						22.0

SIGNATURE:

Edward R. Harris

DATE:

12/22/95

MAGEHELIC CALIBRATION
BOX #3

SER. NO.	R10908AG71 MRR1	R0112642	R10608CF20 CF20
RANGE	0-0.50	0-2.0	0-10
REFERENCE READING	FIELD DEVICE READING		
0.000	0.00	0.00	0.0
0.050			
0.150	0.149		
0.200			
0.250	0.240		
0.450	0.450		
0.50		0.50	
1.00		0.98	
1.50			
1.80		1.78	
2.50			2.5
4.50			
5.0			5.0
9.0			9.0
13.0			
22.0			

SIGNATURE:

Edward L. Harris

DATE:

12/22/95

MAGEHELIC CALIBRATION
BOX #4

SER. NO.	R22D	R90051	R90101
RANGE	0-0.50	0-5	0-25
REFERENCE READING	FIELD DEVICE READING		
0.000	0.000	0.00	0.0
0.050			
0.150	0.151		
0.200			
0.250	0.251		
0.450	0.455		
0.50			
1.00			
1.30		1.27	
1.80			
2.50		2.52	
4.50		4.55	
5.0			5.0
9.0			
13.0			13.0
22.0			21.6

SIGNATURE:

Edward J. Harris

DATE:

12/22/95

TEMPERATURE CALIBRATIONS - DEGREES FAHRENHEIT

REFERENCE DEVICE READING*	0 DEG. F	210 DEG.	420 DEG.	630 DEG.	840 DEG.	1050 DEG.	1260 DEG.	1470 DEG.	1680 DEG.	1900 DEG.
2879	0	217	421	630	839	1050	1260	1471	1681	1900
METER BOX #1 C-133 11580	0	212	423	635	842	1053	1264	1475	1679	1910
METER BOX #2 C-175 15862	0	211	423	627	839	1052	1265	1475	1687	1903
METER BOX #5 S-100 15751	2	211	417	628	844	1062	1279	1491	1698	1907
METER BOX #8 S-101 15751	0	210	419	628	839	1058	1255	1473	1691	1900
PORTABLE THERMOCOUPLE # 2 (Blue)	2	209	415	628	837	1053	1260	1468	1679	1908
PORTABLE THERMOCOUPLE # 2 (Green)	2	211	417	627	842	1058	1273	1484	1688	1896
PINK T140293	-1	208	415	624	840	1056	1272	1482	1687	1894
PORTABLE THERMOCOUPLE (Yellow)	0	210	419	632	840	1050	1259	1470	1680	1901
PORTABLE THERMOCOUPLE T-105898 (Black)	1	209	416	625	839	1055	1270	1481	1684	1891
METER BOX S-102	-2	209	417	625	837	1049	1259	1462	1658	1890
METER BOX S-103	4	215	423	632	844	1057	1266	1471	1667	1895

DATE:

12-05-95

SIGNATURE:

Edward L. Harris

* Reference Device is an Omega Engineering CL505-A calibrated reference thermocouple-potentiometer system.

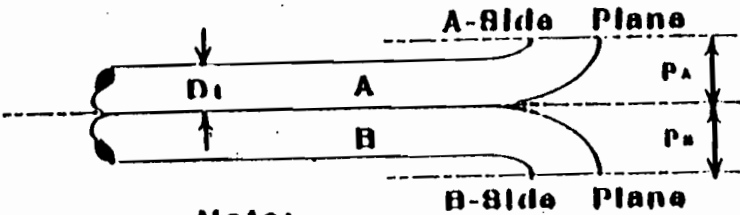
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SANDERS ENGINEERING & ANALYTICAL SERVICES, Inc.

1606 Leroy Stevens Rd. Office: (205) 833-4120
 Mobile, AL 36606 FAX#: (205) 833-8286

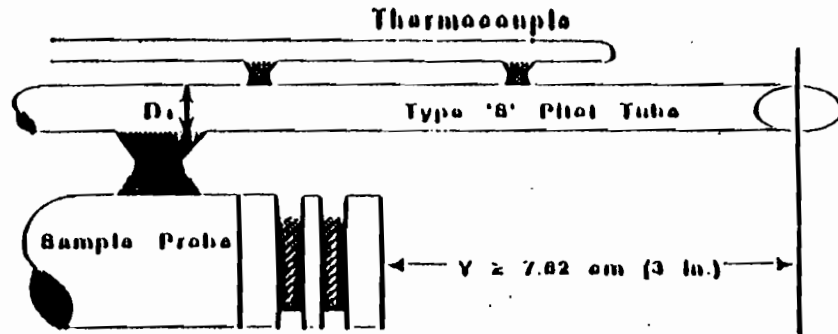
The Pilot used was within the following geometric specifications:
 D_i between 0.48 and 0.66 cm (3/16 and 3/8 in.)
 $C_p = 0.84$



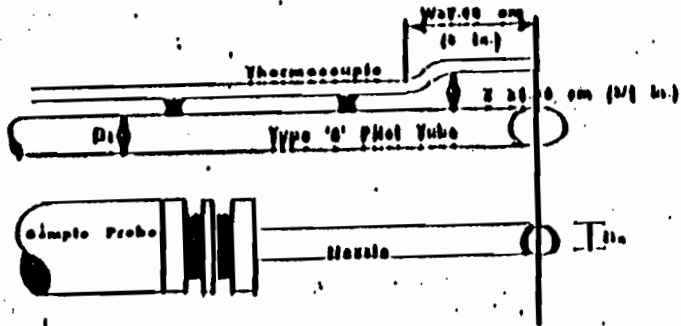
Notes:

$1.05 D_i \leq 1.50 D_i$

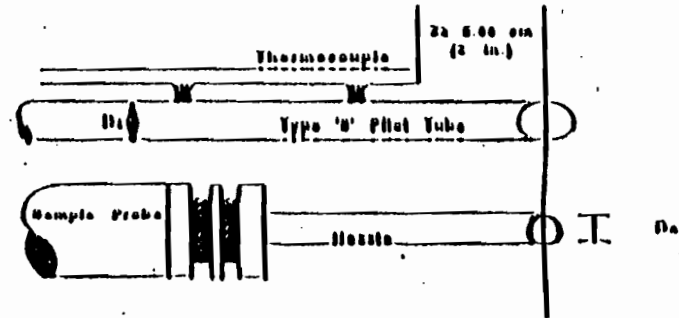
$P_A = P_B$



Minimum pilot-sample probe separation needed to prevent interference



OR



Proper thermocouple placement to prevent interference.

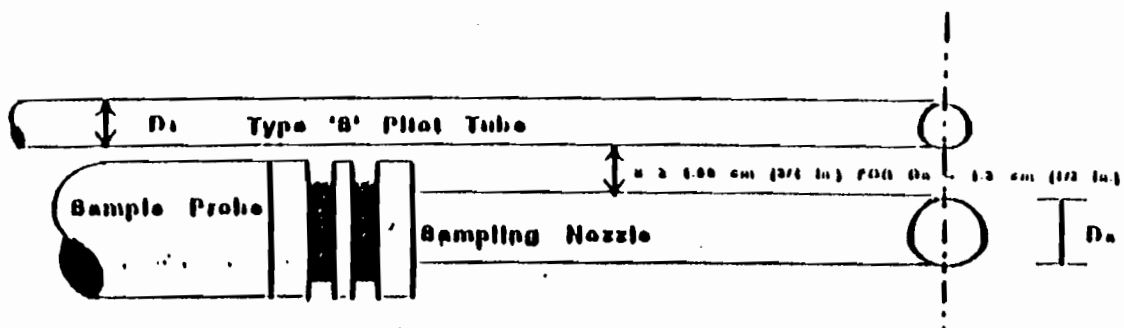


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ANALYTICAL SERVICES, Inc.**

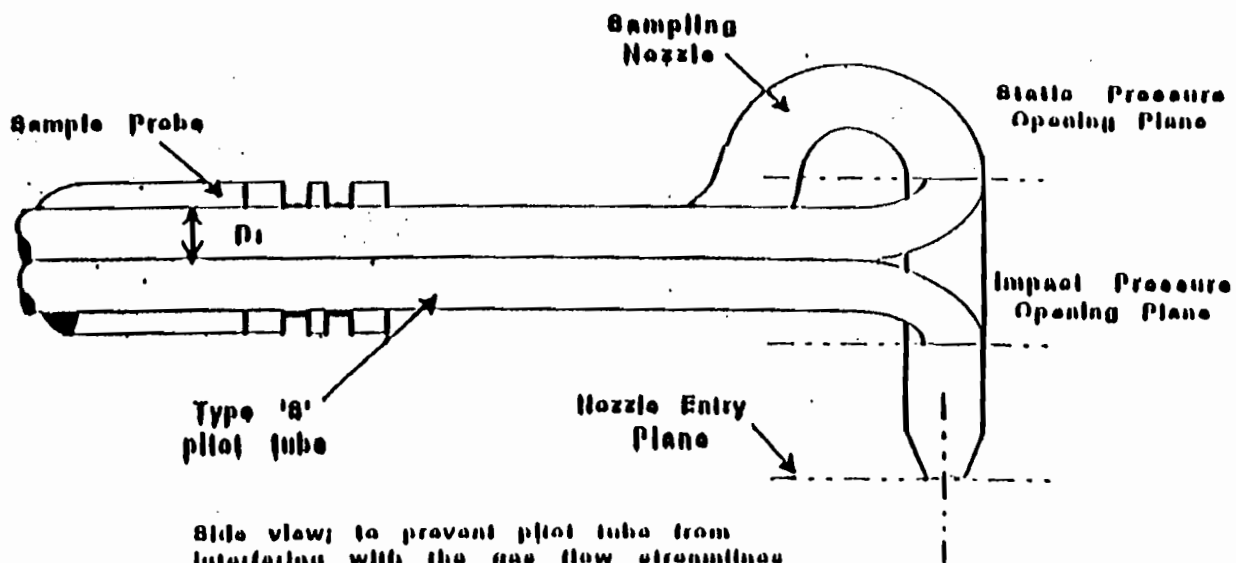
1500 Jerry Stevens Rd.
Mobile, AL 36608

Office: (205) 833-4120
FAX: (205) 833-2208

Proper pilot tube-sampling nozzle configuration to prevent aero-dynamic interference; bottomhook type nozzle; centers of nozzle and pilot opening aligned; D_1 between 0.48 and 0.65 cm (3/16 and 3/8 in.)



Bottom view showing minimum pilot/nozzle separation



Side view; to prevent pilot tube from interfering with the gas flow streamlines approaching the nozzle, the impact pressure opening plane of the pilot tube shall be even with or above the nozzle entry plane.

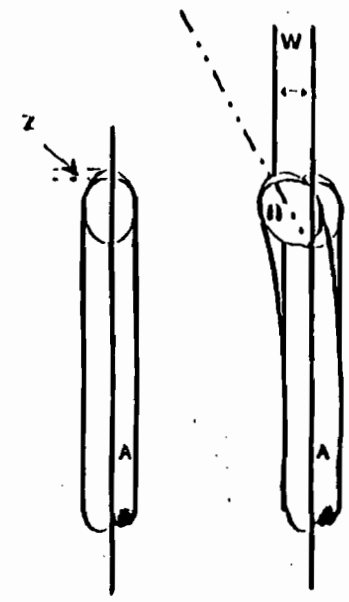
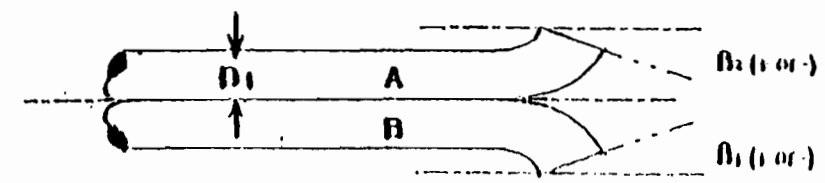
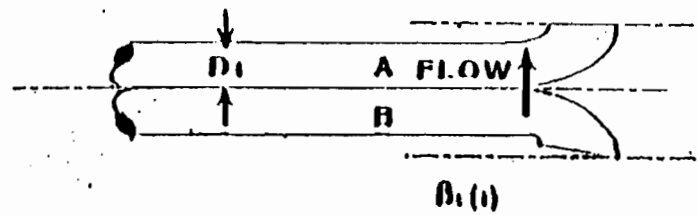
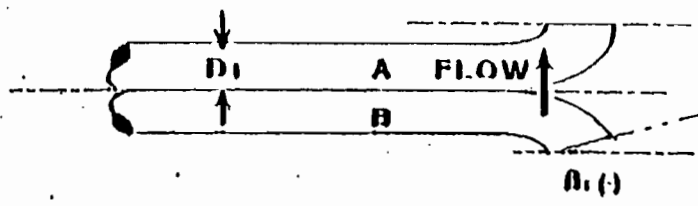
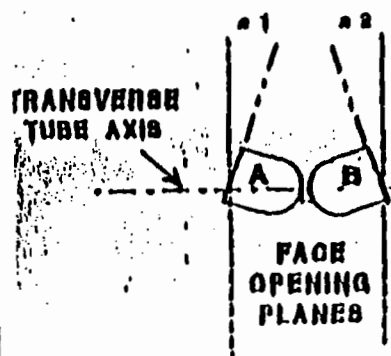
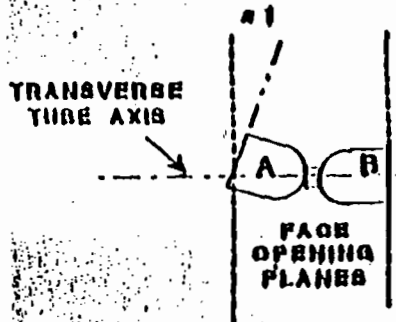
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Types of face-opening misalignment that can result from field use or improper construction of type 'B' pilot tubes. These will not affect the baseline value of $C_p(u)$ so long as α_1 and $\alpha_2 \leq 10^\circ$, D_1 and $D_2 \leq 6^\circ$, and 0.32 cm (1/8 in.)



APPENDIX D OPERATIONAL DATA

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CUST ELECTRIC GENERATING PLANT

STEADY STATE

UNIT 5
DATE 4-18

start of flow
end
0908
252
521

TIME	RUN NUMBER	MAIN STEAM FLOW (LBS/HR)	MW LOAD	BOILER AIR FLOW	PULVERIZER MILLS COAL FLOW 10 ³ LB/HR				GEN	SS	% O ₂		EMS	% OPACITY	FAN AMPS			GAS TEMP (°F) AIR PREHEATER			PULVERIZER MILLS TEMPERATURES °F			
											FD				l.d.	F.D.		A	B		A	B	C	D
094	1	723	88	687	53640	532830	25871	614650	248810	20824	3.8	6.5		6.9	245	100		296	296		150	136	150	140
1020	END	723	88	696	53830	533124	26048	616912	248983	20830	4.1	6.6		7.9	247	100		297	298		150	136	150	140
1158	2	723	88	695	54226	533728	26425	617398	249212	20842	3.7	6.4		9.5	248	100		298	298		150	136	150	140
1403	END	723	88	687	54443	534063	26032	617667	249330	20847	3.8	6.4		9.9	248	150		299	299		150	136	150	140
1526	3	722	88	686	54609	534317	26784	617868	249430	20853	4.2	6.4		13.2	249	100		300	300		150	136	150	140
1621	END	721	88	688	54811	534625	26967	618120	249545	20859	3.8	6.4		12.2	245	150		300	301		150	136	150	140

CRIST ELECTRIC GENERATING PLANT

Precipitator Readings

Unit 5
 Date 4-18-96
 Load 88

Run # THREE
 Start Time _____
 Finish Time _____

Precipitator Cabinet	Primary AMPS	Primary Volts	Secondary AMPS	Secondary Voltage
Start	A	111	370	1.42
	B	113	∅	.85
	C	40	270	.25
	D	54	340	.30
	E	52	335	.36
	F	73	360	.60
Finish	A	111	370	1.42
	B	124	∅	.84
	C	40	280	.3
	D	55	330	.32
	E	46	320	.3
	F	80	370	.58

SANDERS ENGINEERING & ANALYTICAL SERVICES, INC.

PARTICULATE EMISSIONS TEST REPORT
SOOT BLOWING OPERATIONS

FOR

GULF POWER COMPANY

Plant Crist, Unit 5
Pensacola, Florida



April 17, 1996

1568 LEROY STEVENS ROAD

MOBILE, ALABAMA 36695 • 205/633-4120



SANDERS ENGINEERING & ANALYTICAL SERVICES, INC.

1568 LEROY STEVENS ROAD MOBILE, ALABAMA 36695 • OFFICE 334 / 633-4120
FAX 334 / 633-2285

ENVIRONMENTAL ENGINEERING
AIR & WATER QUALITY MODELING
ENVIRONMENTAL ASSESSMENTS
PSD ANALYSIS
EMERGENCY RESPONSE MONITORING

AMBIENT AIR MONITORING
CONTINUOUS IN-STACK MONITORING
SOURCE TESTING
VISIBLE EMISSIONS TESTING
CONSULTING SERVICES

REPORT CERTIFICATION

The sampling and analysis for this report was carried out under my direction and supervision.

Date: 4-30-96

Signature: Edward L. Harris
Edward L. Harris
Environmental Specialist

I have reviewed the testing details and results in this report and hereby certify that the test report is authentic and accurate to the best of my knowledge.

Date: 4-30-96

Signature: Joseph C. Sanders
Joseph C. Sanders
Manager

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1. INTRODUCTION

Sanders Engineering & Analytical Services, Inc. (SEAS) performed particulate emissions testing during soot blowing operations at Gulf Power Company, Plant Crist, Unit 5, located in Pensacola, Florida. The testing was conducted on April 17, 1996. The testing was performed in accordance with the applicable U.S. EPA procedures specified at **40 CFR, Part 60, Appendix A, Methods 1, 2, 3, 4, and 17.**

The purpose of the test was to demonstrate compliance with the rules and regulations of the Florida Department of Environmental Protection, and to meet the necessary requirements contained in the permit to operate issued by the Florida Department of Environmental Protection.

The test was conducted by Mr. Edward Harris and Mr. Dean Holmes of Sanders Engineering & Analytical Services, Inc., and was coordinated with Mr. John McPherson of Gulf Power Company. The Florida Department of Environmental Protection was notified so their representative could be present to observe the testing.

The test was conducted in accordance with the guidelines of the Florida Department of Environmental Protection. Further discussion of the test methods are included later in the report.

2. SUMMARY AND DISCUSSION OF RESULTS

The results of the particulate emissions test for the soot blowing runs, along with the results of the computations, are summarized in Table I. The equations used in the calculations of the results, along with the completed field data sheets for the testing, are presented in Appendix A. The sample calculations of the first run are presented in Appendix B. The quality control checks of the equipment used in the sampling program are included in Appendix C.

There were no problems encountered during the performance of the test. The bottom port of the duct was not sampled due to ash build-up. One of the other ports was alternately sampled twice on each run to compensate for the port not sampled. At the completion of each run, the filter and probe were removed to a relatively clean, draft-free area for clean-up.

The results of the testing indicate the particulate emission rate during soot blowing for Plant Crist, Unit 5, is 0.015 LBS/MMBTU. The applicable Florida Department of Environmental Protection rules and regulations require an emission rate of no greater than 0.30 LBS/MMBTU. The results of the testing indicate that the unit is in compliance with the particulate emission condition of the permit to operate issued by the Florida Department of Environmental Protection.

**TABLE I. PARTICULATE EMISSIONS TEST RESULTS
GULF POWER COMPANY
PLANT CRIST, UNIT 5, SOOT BLOWING
4/17/96**

Title of Run		<u>RUN 1</u>	<u>RUN 2</u>	<u>RUN 3</u>
Sampling Time -Start	Military	0817	1008	1426
Sampling Time -Stop	Military	0923	1113	1531
F Factor	SDCF/MMBTU	9820	9820	9820
Plant Load	Megawatts	88.0	88.0	88.0
Static Pressure	In. H2O	-0.35	-0.35	-0.35
Barometric Pressure	In. Hg	30.31	30.31	30.31
Average dH	In. H2O	1.017	0.999	0.992
Meter correction		1.024	1.024	1.024
Avg. Meter Temp.	Deg. F	58.6	66.3	71.3
% O2	%	5.2	5.3	5.5
%CO2	%	13.5	13.0	13.5
Volume Metered	ACF	36.665	36.310	36.400
Volume Water	Ml	70.0	79.0	79.0
Sampling Time	Minutes	64	64	64
Nozzle Diameter	Inches	0.225	0.221	0.221
Avg. Stack Temp.	Deg. F	292.9	299.4	303.9
Area of Stack	Sq. Feet	92.1350	92.1350	92.1350
Wt. of Part.	Mg.	18.4	19.4	21.4
Number of Points		32	32	32
Avg. Sqrt dP	In. H2O	0.8449	0.8252	0.8286

RESULTS OF COMPUTATIONS

		<u>RUN 1</u>	<u>RUN 2</u>	<u>RUN 3</u>	<u>Average</u>
Volume of Gas Sampled	SDCF	38.802	37.862	37.603	
H2O vapor in Gas Stream	PERCENT	7.8	8.9	9.0	8.6
Avg. Stack Gas Velocity	FT/SEC	55.8	54.9	55.2	55.3
Volumetric Flow Rate	SDCFM	201,813	194,554	194,413	196,927
Volumetric Flow Rate	ACF/M	308,446	303,607	305,385	305,813
Particulate Conc.	Grs/SDCF	0.007	0.008	0.009	0.008
Particulate Conc.	Grs/ACF	0.005	0.005	0.006	0.005
Particulate Mass Rate	Lb/Hr	12.6	13.2	14.6	13.5
Particulate Mass Rate	Lb/MMBtu	0.014	0.015	0.017	0.015
Heat Input	MMBTU/Hr	926.28	887.28	875.26	896.27
Percent of Isokinetic	%	100.3	105.2	104.6	

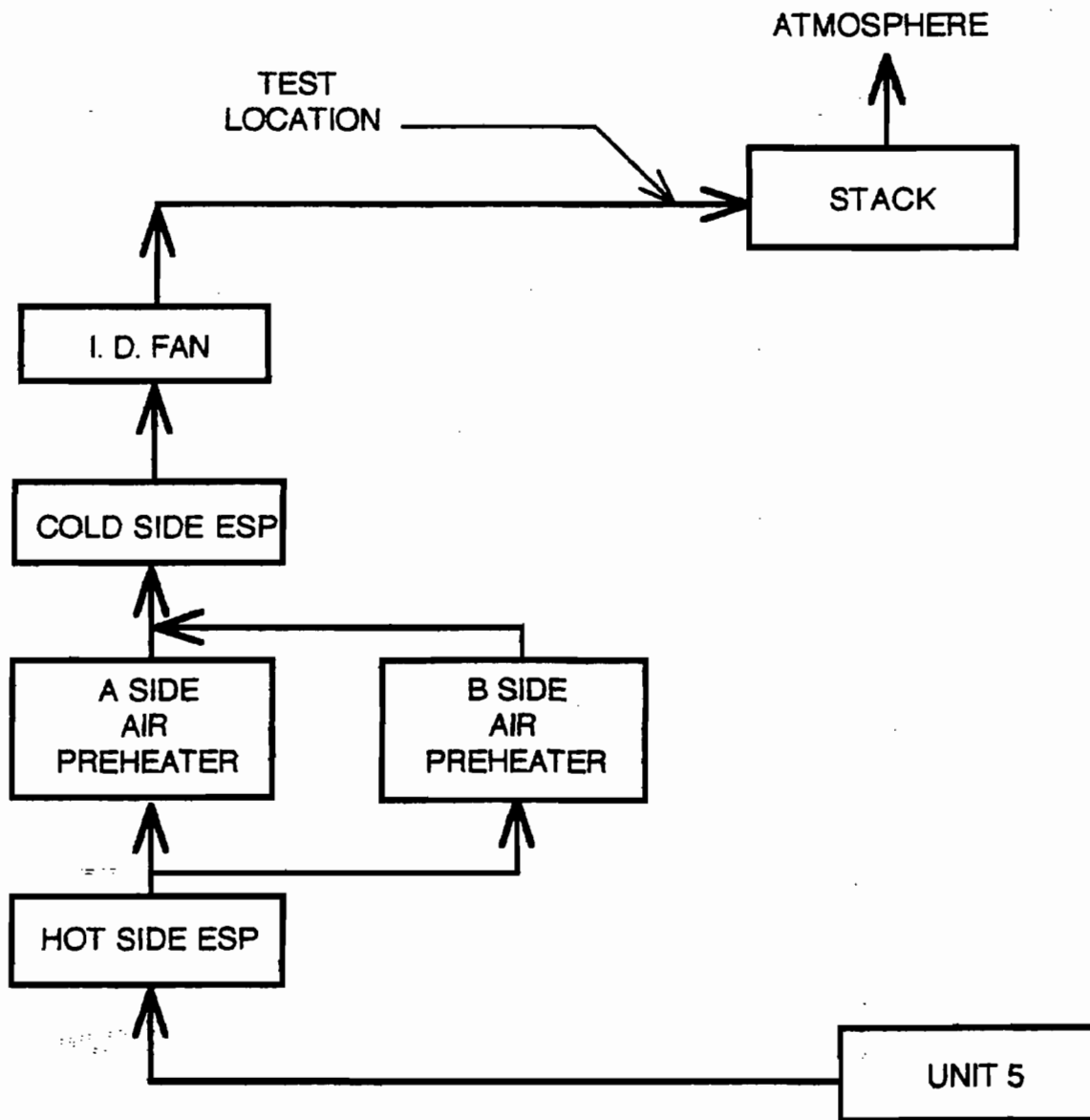
3. PROCESS DESCRIPTION

The process consists of a steam electric generating unit firing bituminous coal for the production of electric energy. The coal is received by barge, and loaded directly onto the conveyor feeding the plant, or onto the stockpile and later loaded onto the conveyor belt transporting the coal to the plant. The coal from the conveyor is loaded into bunkers capable of holding between 36 to 48 hours supply of coal. The coal is then fed to pulverizing mills before being fired in the unit through the burners. Upon combustion of the coal in the fire box, approximately 20 percent of the ash falls to the bottom of the boiler and is removed by the ash removal system. The remaining 80 percent exits with the flue gases through the heat exchange and economizer sections of the furnace, and is collected by electrostatic precipitators.

3.1. Source Air Flow

As shown in Figure 1, the flue gases exit the boiler and flow through a hot side precipitator. The exhaust gases are separated into ducts A and B before entering air preheaters. The exhaust gases are combined before entering a cold side ESP. The flue gases exiting the cold side ESP are exhausted through a stack into the atmosphere.

Figure 1. Air Flow Schematic



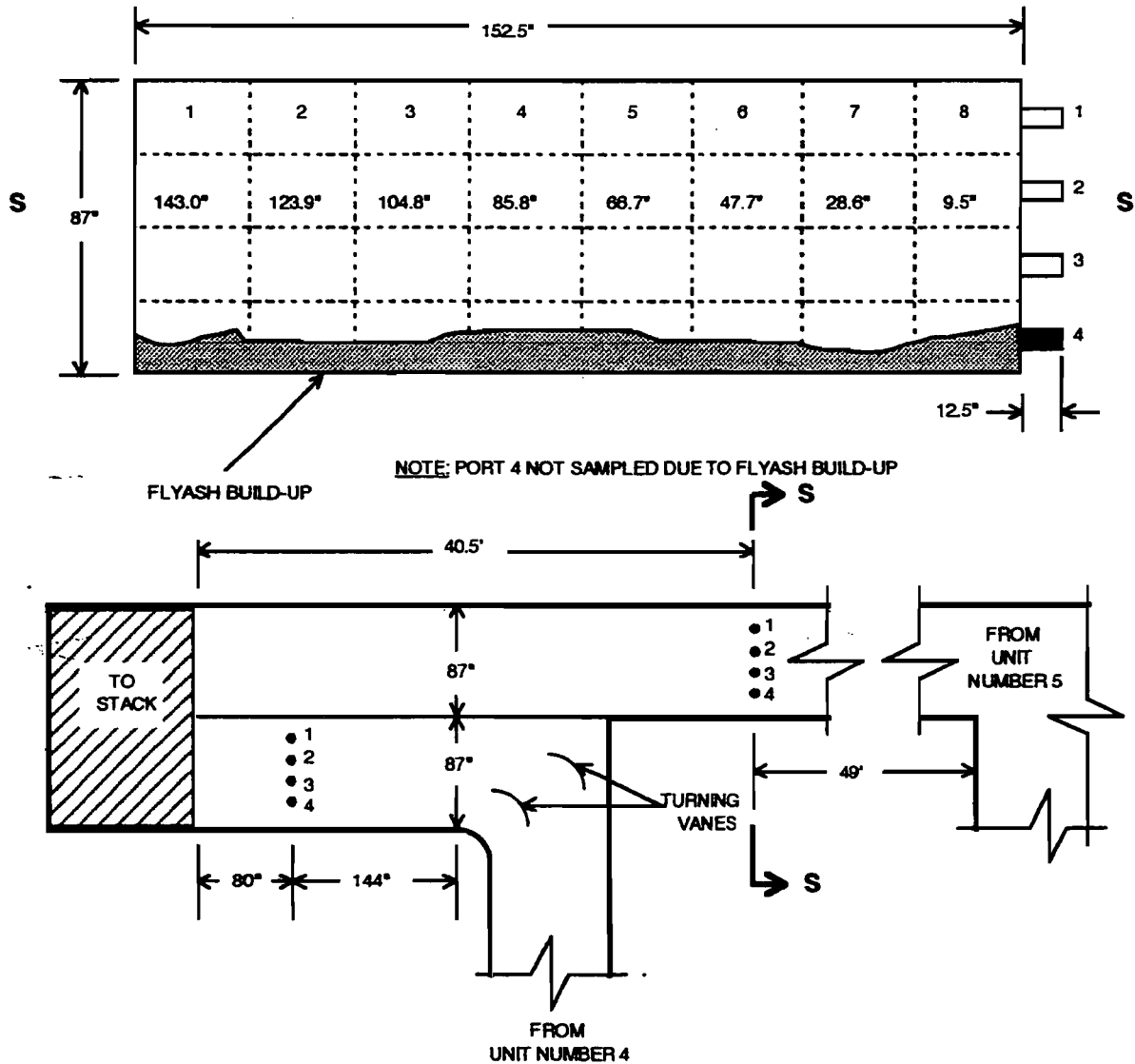
3.2. Operation During Testing

The average heat input during soot blowing operation, as based on F-factor calculations, was 896.27 million BTU per hour resulting in the production of approximately 88 megawatts of electricity. Precipitator data supplied by Gulf Power personnel is given in Appendix D.

4. SAMPLE POINT LOCATION

The sample point locations and outlet duct schematic are presented in Figure 2. Method 1 was used for determination of the number and location of sampling points. The minimum number of points (25) required for rectangular stacks was met by sampling a total of 32 points.

Figure 2. Sample Point Locations

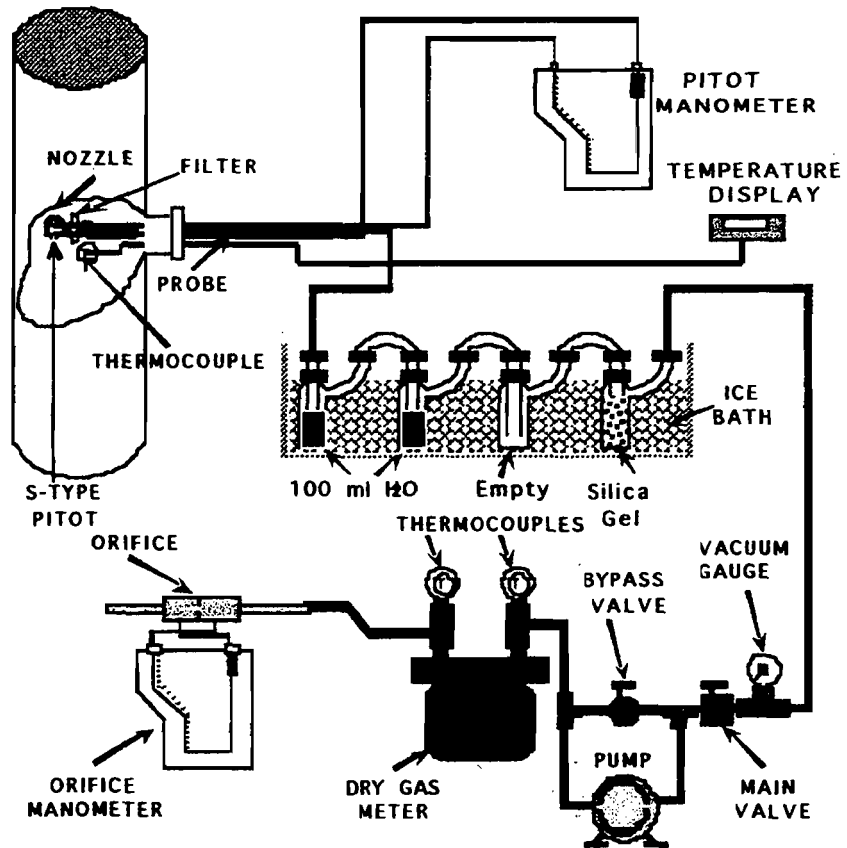


5. PARTICULATE SAMPLING PROCEDURE (EPA Method 17)

The sampling procedure utilized is that specified in 40 CFR, Part 60, Appendix A, Method 17, as modified by the governing regulatory agency. A brief description of this procedure is as follows:

The first impingers were partially filled with 100 milliliters of deionized water. The next impinger was left empty to act as a moisture trap. Preweighed 6 to 16 mesh indication silica gel was added to the last impinger. The sampling equipment manufactured by Lear Siegler (Model 100) or Sanders Engineering

Figure 3. Particulate Sampling Train



(Model 200) was assembled as shown in the attached drawing. The system was leak checked by plugging the inlet to the nozzle and pulling a 15 inch mercury vacuum. A leakage rate not in excess of 0.02 cubic feet per minute was considered acceptable.

The inside dimensions of the stack liner were measured and recorded. The required number of sampling points were marked on the probe for easy visibility. The range of velocity pressure, the percent moisture, and the temperature of the effluent gases were determined. From this data, the correct nozzle size and the nomograph multiplication factor were determined.

Crushed ice was placed around the impingers. The nozzle was placed on the first traverse point with the tip pointing directly into the gas stream. The pump was started immediately and the flow was adjusted to isokinetic sampling conditions. After the required time interval had elapsed, the probe was repositioned to the next traverse point and isokinetic sampling was re-established. This was performed for each point until the run was completed. Readings were taken at each point and recorded on the field data sheet. At the conclusion of each run, the pump was turned off and the final readings were recorded.

5.1. Particulate Sample Recovery

Care was exercised in moving the collection train to the sample recovery area to minimize the loss of collected sample, or the gain of extraneous particulate matter. The volume of water in the impingers was measured, the silica gel impinger was weighed and recorded on the field data sheet. The nozzle, and all sample-exposed surfaces were washed with reagent grade acetone into a clean sample container. A brush was used to loosen any adhering particulate matter and subsequent washings were placed into the container. The filter was carefully removed from the fritted support and placed in a clean separate sample container. A sample of the acetone used in the washing was saved for a blank laboratory analysis.

5.2. Particulate Analytical Procedures

The filter and any loose particulate matter were transferred from the sample container to a clean, tared weighing dish. The filter was placed in a desiccator for at least 24 hours and then weighed to the nearest 0.1 milligram until a constant weight was obtained. The original weight of the filter was deducted, and the weight gain was recorded to the nearest 0.1 milligram.

The wash solution was transferred to a clean, tared beaker. The solution was evaporated to dryness, desiccated to a constant weight, and the weight gain was recorded to the nearest 0.1 milligram.

APPENDIX A EQUATIONS AND FIELD DATA SHEETS

EQUATIONS

$$1. \quad P_s = P_{\text{bar}} + \frac{P_g}{13.6}$$

$$2. \quad P_m = P_{\text{bar}} + \frac{\overline{\Delta H}}{13.6}$$

$$3. \quad V_s = K_p C_p \sqrt{\Delta P} \sqrt{\frac{\overline{T_s}}{M_s P_s}}$$

$$4. \quad V_{m(\text{Std})} = K_1 V_m Y \left[\frac{P_{\text{bar}} + \frac{\overline{\Delta H}}{13.6}}{\overline{T_m}} \right]$$

$$5. \quad V_{w(\text{Std})} = 0.04707 V_{1c}$$

$$6. \quad B_{ws} = \frac{V_{w(\text{Std})}}{V_{m(\text{Std})} + V_{w(\text{Std})}}$$

$$7. \quad M_d = 0.44 (\%CO_2) + 0.32 (\%O_2) + 0.28 (\%N_2 + \%CO)$$

$$8. \quad M_s = M_d (1 - B_{ws}) + 18 (B_{ws})$$

$$9. \quad EA = \left[\frac{(\%O_2 - 0.5 (\%CO))}{0.264 (\%N_2) - ((\%O_2) - 0.5 (\%CO))} \right] 100$$

$$10. \quad Q_a = (V_s) (A_s) (60)$$

$$11. \quad Q_s = Q_a (1 - B_{ws}) \frac{(528)}{T_s} \frac{(P_s)}{29.92}$$

$$12. \quad E_H = \left(\frac{PMR}{H_1} \right)$$

$$13. \quad E = C_d F_{O_2} \left(\frac{20.9}{20.9 - \%O_2} \right)$$

$$14. \quad C_s = 0.0154 \frac{M_n}{V_m(Std)}$$

$$15. \quad C_{s0} = \frac{21 C_s}{21 - [(1.5) (\%O_2) - 0.133 (N_2) - 0.75 (\%CO)]}$$

$$16. \quad C_{12} = \frac{C_s (12)}{\%CO_2}$$

$$17. \quad PMR = (C_s) (Q_s) \frac{(60)}{7000}$$

$$18. \quad V_n = \left[(0.002669) (V_{1c}) + \frac{V_m Y}{T_m} \left(P_{bar} + \frac{\Delta H}{13.6} \right) \right] \frac{\bar{T}_s}{P_s}$$

$$19. \quad I = \frac{100 V_n}{(60) \emptyset V_s A_n}$$

NOMENCLATURE

- A_n = Cross-sectional area of nozzle, ft²
- A_s = Cross sectional area of stack, ft²
- B_{ws} = Water vapor in the gas stream,
proportion by volume (dimensionless)
- C_p = Pitot tube coefficient (dimensionless) (0.84)
- C_s = Particulate concentration, grains/SDCF
- C_d = Particulate concentration, lbs/SDCF
- C_{12} = Particulate concentration (C_s adjusted to 12% CO)
grains/SDCF
- C_{50} = Particulate concentration (C_s adjusted to 50% excess air)
grains/SDCF
- EA = Excess air, %
- E = Emission in lb/mmBTU
- E_H = Emission in lb/mmBTU, based on heat input
- H_I = Total Heat Input, Million BTU per Hour (MMBTU/hr)
- I = Percent of isokinetic sampling
- K_1 = 17.64 °R/ inches Hg
- K_p = Pitot tube constant,
$$85.49 \text{ ft/sec} \left[\frac{(\text{lb/lb-mole}) (\text{in. Hg})}{(^\circ\text{R}) (\text{inc. H}_2\text{O})} \right]^{\frac{1}{2}}$$
- M_n = Total amount of particulate collected, mg
- M_d = Molecular weight of stack gas; dry basis, lb/lb mole
- M_s = Molecular weight of stack gas; wet basis, lb/lb mole
- P_{bar} = Barometric pressure at the sampling site, in. Hg

NOMENCLATURE (continued)

- P_m = Meter pressure, in. Hg
- P_s = Absolute stack pressure, in. Hg
- P_g = Stack static pressure, in. H₂O
- PMR = Particulate mass rate, lb/Hr
- Q_a = Volumetric flow rate ACFM
- Q_s = Volumetric flow rate SDCFM
- V_s = Average stack gas velocity, ft/sec
- V_{lc} = Total volume of liquid collected in impingers & silica gel, ml
- V_m = Volume of gas sample as measured by dry gas meter, ACF
- $V_{m(std)}$ = Volume of gas sample measured by dry gas meter,
corrected to standard conditions, SDCF
- $V_{w(std)}$ = Volume of water vapor in gas sample, corrected to standard
conditions, SCF
- V_n = Volume collected at stack conditions through nozzle, ACF
- Y = Dry gas meter calibration factor (dimensionless)
- ΔH = Average pressure difference of orifice, in. H₂O
- ΔP = Velocity head of stack gas, in. H₂O
- $\overline{\sqrt{\Delta P}}$ = Average of square roots of the velocity pressure, in. H₂O
- \emptyset = Total sampling time, minutes
- %CO₂, %O₂, %N₂, %CO - Number % by volume, dry basis, from gas analysis
- F_{O_2} = Oxygen based F factor (9820 SDCF/mmBTU for bituminous coal)
- T_s = Temperature of the stack, °R (° F + 460)



SANDERS ENGINEERING & ANALYTICAL SERVICES, Inc.

1568 Larcy Stevens Rd.
Mobile, AL 36695

Office: (205) 633-4120
FAX#: (205) 633-2225

FIELD DATA SHEET

COMPANY GPCO DATE 4-17-96 DGM# S-101
 PLANT Crist OPERATOR ELM ΔHa 0.74
 UNIT # 5 ^{Sheddy} ~~State~~ _{SOOT} ^{slow} METHOD 17 PROBE N/A _{liner} 12' _{length}

RUN 1

NOZZLE DATA RUN 1

CALIBRATION		FILTER NUMBER
PRE	POST	
.225	.225	1636
.225	.225	
.225	.224	
.225	.225	
AVERAGE	AVERAGE	

RUN 2

NOZZLE DATA RUN 2

CALIBRATION		FILTER NUMBER
PRE	POST	
.221	.221	1637
.221	.221	
.221	.221	
.221	.221	
AVERAGE	AVERAGE	

RUN 3

NOZZLE DATA RUN 5

CALIBRATION		FILTER NUMBER
PRE	POST	
.221	.221	1638
.221	.221	
.221	.221	
.221	.221	
AVERAGE	AVERAGE	

METER READING

220.965	FINAL
184.300	INITIAL
36.665	NET

METER READING

258.810	FINAL
222.500	INITIAL
36.310	NET

METER READING

322.300	FINAL
285.900	INITIAL
36.400	NET

LEAK CHECK

SYSTEM		PITOT	
Pre	Post	Pre	Post
15	10	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>
0.000	0.000	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>

LEAK CHECK

SYSTEM		PITOT	
Pre	Post	Pre	Post
15	10	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>
0.000	0.000	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>

LEAK CHECK

SYSTEM		PITOT	
Pre	Post	Pre	Post
15	10	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>
0.000	0.000	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>

VOLUME OF LIQUID WATER COLLECTED

IMP. 1	IMP. 2	IMP. 3	IMP. 4
164	100	0	1466.6
100	100	0	1462.6
64	0	0	6.0
NET	NET	NET	NET
TOTAL			70.0

VOLUME OF LIQUID WATER COLLECTED

IMP. 1	IMP. 2	IMP. 3	IMP. 4
174	100	0	1473.0
100	100	0	1468.0
74	0	0	5.0
NET	NET	NET	NET
TOTAL			79.0

VOLUME OF LIQUID WATER COLLECTED

IMP. 1	IMP. 2	IMP. 3	IMP. 4
168	100	0	1567.0
100	100	0	1556.0
68	0	0	11.0
NET	NET	NET	NET
TOTAL			79.0

GAS ANALYSIS

O ₂ <u>5.2%</u>	STATIC <u>-0.35</u>
CO ₂ <u>13.5%</u>	BAROMETRIC
CO <u>-</u>	<u>30.31</u>

GAS ANALYSIS

O ₂ <u>5.3%</u>	STATIC <u>-0.35</u>
CO ₂ <u>13.0%</u>	BAROMETRIC
CO <u>-</u>	<u>30.31</u>

GAS ANALYSIS

O ₂ <u>5.5%</u>	STATIC <u>-0.35</u>
CO ₂ <u>13.5%</u>	BAROMETRIC
CO <u>-</u>	<u>30.31</u>

Port #	Time	Gas Meter Vol. (cu. ft.)	Vel. Head ΔP in. H ₂ O	Orifice Head ΔH in. H ₂ O	Temperature (F)						Vac. in. H ₂	8:12 Port 4	
					Stack	Probe	Hot Box	Imp.	Gas Meter				
									In	Out			
1-1	8:17	184.300	.84	1.19	293	N/A	N/A	55	57	57	3	.70	29
2	:19	185.400	.72	1.02	295			✓	57	57	2	.76	29
3	:21	186.600	.91	1.29	295			✓	57	57	3	.60	29
4	:23	187.900	.78	1.11	294			✓	57	57	3	.40	29
5	:25	189.100	.73	1.04	293			✓	57	57	3	.30	29
6	:27	190.300	.87	1.24	294			✓	57	57	3	.44	28
7	:29	191.500	.76	1.08	292			✓	58	58	3	.29	28
8	:31	192.750	.60	0.85	292			✓	58	58	3	.40	28
2-1	:33	193.800	.84	1.19	294			✓	58	58	3		
2	:35	195.100	.74	1.05	295			✓	58	58	3		
3	:37	196.200	.92	1.31	294			59	58	58	3		
4	:39	197.500	.80	1.14	294			✓	58	58	3		
5	:41	198.800	.73	1.04	293			✓	59	58	3		
6	:43	199.900	.85	1.21	293			✓	59	58	3		
7	:45	201.200	.76	1.08	292			✓	59	58	3		
8	:47	202.300	.62	.88	287			✓	59	58	3		
2-1	:50	203.000	.68	.97	291			59	59	58	2		
2	:52	204.400	.64	.90	292			✓	59	58	2.5		
3	:54	205.500	.75	1.06	292			✓	59	58	3		
4	:56	206.700	.65	.92	292			✓	59	59	3		
5	:58	207.000	.64	.90	293			✓	59	59	3		
6	9:00	208.900	.65	.92	293			✓	60	59	3		
7	:02	210.000	.58	.82	292			✓	60	59	3		
8	:04	211.000	.55	.78	290			✓	60	59	3		
3-1	9:07	212.064	.75	1.06	291			✓	60	59	3		
2	:09	213.200	.73	1.03	294			✓	60	59	3		
3	:11	214.400	.60	.85	295			✓	60	59	3		
4	:13	215.500	.58	.82	294			✓	60	59	3		
5	:15	216.600	.66	.93	294			✓	61	60	3		
6	:17	217.600	.66	.93	294			✓	61	60	3		
7	:19	218.900	.66	.93	293			✓	61	60	3		
8	:21	219.900	.70	.99	292			✓	61	60	3		

Didn't use for flow calcs.

Final 9:23 220.965

Check indicates Temperatures Meet Required Limits.

Company GPCO

Date 4-17-96

Site Crist #5 Soot Blow

Run # 1

Page 2 Of

~~DO NOT~~ USE FOR RATA RUN 1

Best Available Copy

Port #	Time	Gas Meter Vol. (cu. ft.)	Vel. Head ΔP in. H ₂ O	Orifice Head ΔH in. H ₂ O	Temperature (F)						Vac. in. H _g	10.01 Part 4
					Stack	Probe	Hot Box	Imp.	Gas Meter			
Point #									In	Out		
1- 1	10:08	222.500	.85	1.24	298	N/A	N/A	53	63	63	4	.82 29
2	:10	223.900	.74	1.07	298			✓	63	63	4	.84 29
3	:12	225.050	.90	1.31	301			✓	63	63	4	.77 29
4	:14	226.200	.70	1.02	300			✓	63	63	4	.45 29
5	:16	227.400	.73	1.06	300			✓	63	63	4	.30 29
6	:18	228.500	.87	1.26	300			✓	63	63	4	.45 29
7	:20	229.800	.79	1.15	299			✓	64	63	4	.30 29
8	:22	231.100	.60	.87	296			✓	64	63	4	.36 29
2- 1	10:24	232.185	.67	.97	295			55	65	65	3	
2	:26	233.250	.63	.91	300			✓	65	65	3	
3	:28	234.400	.75	1.09	301			✓	65	65	3	
4	:30	235.500	.62	.90	301			✓	65	65	3	
5	:32	236.650	.68	.99	301			✓	66	66	3	
6	:34	237.700	.65	.95	300			✓	66	66	3	
7	:36	238.800	.58	.85	300			✓	66	66	3	
8	:38	239.900	.60	.88	295			✓	67	67	3	
2- 1	:40	240.950	.68	1.00	293			✓	67	67	3	
2	:42	242.000	.64	.94	301			✓	68	67	4	
3	:44	243.350	.70	1.03	302			✓	68	67	4	
4	:46	244.200	.58	.85	302			✓	68	67	4	
5	:48	245.400	.67	.98	302			✓	68	68	4	
6	:50	246.480	.70	1.03	301			✓	68	68	4	
7	:52	247.600	.56	.82	300			✓	69	68	4	
8	:54	248.700	.65	.96	298			✓	69	68	4	
3- 1	:57	249.800	.77	1.13	295			59	69	68	5	
2	:59	250.975	.73	1.07	302			✓	69	68	5	
3	11:01	252.200	.60	.88	303			✓	69	68	4	
4	:03	253.300	.57	.84	302			✓	69	68	4	
5	:05	254.300	.65	.96	301			✓	69	69	4	
6	:07	255.450	.64	.94	301			✓	69	69	4	
7	:09	256.500	.65	.96	301			✓	69	69	4	
8	:11	257.650	.72	1.06	292			✓	69	69	4	

Final 11:13 258.810

Check indicates Temperatures Meet Required Limits.

Company GPCO

Date 4-17-96

Site Crist #5 Soot Blow

Run # 2

Page 3 Of

~~START DATA RUN HERE~~

Q-2

K=1.458

2
PART.
NOT FOR
DISP
USE FOR
CROSS

Port # Point #	Time	Gas Meter Vol. (cu. ft.)	Vel. Head ΔP in. H ₂ O	Orifice Head ΔH in. H ₂ O	Temperature (F)						Vac. in. H _g	14:20 Port 4	
					Stack	Probe	Hot Box	Imp.	Gas Meter				
									In	Out			
1-1	14:24	285.900	.84	1.22	294	N/A	N/A	52	70	70	3	.70	29
2	:28	287.200	.77	1.12	303			✓	70	70	3	.75	29
3	:30	288.400	.98	1.42	307			✓	70	70	3	.62	29
4	:32	289.750	.78	1.13	307			✓	70	70	3	.41	29
5	:34	290.900	.70	1.01	306			✓	71	70	3	.30	29
6	:36	292.100	.84	1.22	305			✓	71	70	3	.45	29
7	:38	293.500	.79	1.15	305			✓	71	70	3	.25	29
8	:40	294.800	.63	.91	303			✓	71	70	3	.35	29
2-1	14:42	295.740	.65	.94	300			✓	71	70	3		
2	:44	296.850	.63	.91	305			✓	71	70	2		
3	:46	297.900	.74	1.07	306			✓	71	70	2		
4	:48	299.100	.59	.84	306			✓	71	70	3		
5	:50	300.150	.68	.97	305			56	72	71	3		
6	:52	301.300	.73	1.04	305			✓	72	71	3		
7	:54	302.400	.60	.86	304			✓	72	71	3		
8	:56	303.475	.62	0.89	303			✓	72	71	3		
3-1	14:59	304.555	.74	1.06	302			✓	72	71	3		
2	:01	305.600	.70	1.00	306			✓	72	71	3		
3	:03	306.800	.62	.89	306			✓	72	71	3		
4	:05	306.950	.54	.77	305			✓	72	72	3		
5	:07	308.950	.65	.93	304			✓	72	72	3		
6	:09	309.900	.65	.93	304			✓	72	72	3		
7	:11	311.100	.66	.95	304			58	72	72	3		
8	:13	312.350	.68	.98	299			✓	72	72	3		
3-1	:15	313.450	.75	1.08	302			✓	72	72	3		
2	:17	314.500	.70	1.00	305			✓	72	72	3		
3	:19	315.600	.64	.92	306			✓	72	72	3		
4	:21	316.800	.53	.76	305			✓	72	72	3		
5	:23	317.800	.64	.92	305			✓	72	72	3		
6	:25	318.900	.65	.93	304			✓	72	72	3		
7	:27	320.100	.66	.95	303			✓	72	72	3		
8	:29	321.300	.68	.98	302			✓	72	72			

Final 15:31 322.300
RATA RUN # 5

Check indicates Temperatures Meet Required Limits.

Company GPCO

Date 4-17-96

Site Crist #5 Soot Blows

Particulate
Run # 3

Page 4 Of 4

RATA RUN # 5

Didn't
use for
RATA
CALCS.

LABORATORY ANALYSIS & CHAIN OF CUSTODY

COMPANY/PLANT: Huff Power Co.
 UNIT #: 5 DATE OF TEST: 4-17-96 TYPE OF TEST: M-5 M-17 OTHER _____

SAMPLE #	RELINQUISHED BY	RECEIVED BY	TIME	DATE	REASON FOR CHANGE
1636	SAH	JCA	8:30 AM	4-19-96	Analytical
1637	SAH	JCA	8:30 AM	4-19-96	Analytical
1638	SAH	JCA	8:30 AM	4-19-96	Analytical

UNIT # Unit 5 - Study Site ^{Soot} _{Blow}

RUN # <u>1</u>	FILTER # <u>1636</u>	BEAKER # <u>16</u>	WASH (ML) _____
FINAL WEIGHT	<u>141.4</u>	<u>70158.0</u>	
INITIAL WEIGHT	<u>127.8</u>	<u>70153.2</u>	
DIFFERENCE	<u>13.6</u>	<u>4.8</u>	
CORRECTED TOTAL WEIGHT		<u>18.4</u>	
RUN # <u>2</u>	FILTER # <u>1637</u>	BEAKER # <u>23</u>	WASH (ML) _____
FINAL WEIGHT	<u>141.5</u>	<u>63355.1</u>	
INITIAL WEIGHT	<u>127.3</u>	<u>63349.9</u>	
DIFFERENCE	<u>14.2</u>	<u>5.2</u>	
CORRECTED TOTAL WEIGHT		<u>19.4</u>	
RUN # <u>3</u>	FILTER # <u>1638</u>	BEAKER # <u>45</u>	WASH (ML) _____
FINAL WEIGHT	<u>141.5</u>	<u>67596.2</u>	
INITIAL WEIGHT	<u>127.8</u>	<u>67589.5</u>	
DIFFERENCE	<u>13.7</u>	<u>7.7</u>	
CORRECTED TOTAL WEIGHT		<u>21.4</u>	
RUN # _____	FILTER # _____	BEAKER # _____	WASH (ML) _____
FINAL WEIGHT			
INITIAL WEIGHT			
DIFFERENCE			
CORRECTED TOTAL WEIGHT			

RUN # _____	FILTER # _____	BEAKER # _____	WASH (ML) _____
FINAL WEIGHT			
INITIAL WEIGHT			
DIFFERENCE			
CORRECTED TOTAL WEIGHT			
RUN # _____	FILTER # _____	BEAKER # _____	WASH (ML) _____
FINAL WEIGHT			
INITIAL WEIGHT			
DIFFERENCE			
CORRECTED TOTAL WEIGHT			
WASH SOLVENT BLANK (ML)	<u>100</u>	BEAKER # _____	WASH (ML) _____
FINAL WEIGHT		<u>67341.7</u>	
INITIAL WEIGHT		<u>67341.6</u>	
DIFFERENCE		<u>0.1</u>	
CORRECTION FACTOR (MG/ML)		<u>0.121</u>	

ALL WEIGHTS ARE IN MILLIGRAMS (MG)

APPENDIX B SAMPLE CALCULATIONS

Input and Constants

```

          3
    9820 ft
f := -----
      mm btu

pg := -(0.35 in. H2O)
pbar := 30.31 in. Hg.
Ahavg := 1.017 in. H2O
y := 1.024
tm := 58.6 °F
o2 := 5.2
co2 := 13.5

          3
vm := 36.665 ft
vlc := 70. ml
theta := 64 min
nozdia := 0.225 in.
ts := 292.9 °F

          2
as := 92.135 ft
mn := 18.4 mg
numberofpoints := 32

          0.5
sqrtAp := 0.8449 in. H2O

          lb in. Hg.      0.5
      85.49 1 ft 1 (-----)
          lb-mole °R in. H2O
kp := -----
          1 sec

cp := 0.84

      17.64 °R
k1 := -----
      in. Hg.
    
```

$$ts = \frac{(ts + 460 \text{ } ^\circ\text{F}) \text{ } ^\circ\text{R}}{^\circ\text{F}}$$

752.9 °R

$$tm = \frac{(tm + 460 \text{ } ^\circ\text{F}) \text{ } ^\circ\text{R}}{^\circ\text{F}}$$

518.6 °R

$$n2 = 100 - o2 - co2$$

81.3

$$an = \frac{\text{nozdia}^2 \text{ } 3.1416}{4 \left(\frac{12 \text{ in.}^2}{\text{ft}} \right)}$$

0.000276117 ft²

Calculations

Equation 1

$$p_s = p_{bar} + \frac{p_g}{\frac{13.6 \text{ in. H}_2\text{O}}{1 \text{ in. Hg.}}}$$

30.2843 in. Hg.

Equation 2

$$p_m = p_{bar} + \frac{\Delta h_{avg}}{\frac{13.6 \text{ in. H}_2\text{O}}{\text{in. Hg.}}}$$

30.3848 in. Hg.

Equation 3

$$k_1 v_m y \left(p_{bar} + \frac{\Delta h_{avg}}{\frac{13.6 \text{ in. H}_2\text{O}}{\text{in. Hg.}}} \right)$$

$$v_{mstd} = \frac{\text{-----}}{t_m}$$

38.8038 ft³

Equation 4

$$v_{wstd} = \frac{0.04707 \text{ ft}^3 \text{ vlc}}{m_l}$$

3.2949 ft³

Equation 5

$$bws = \frac{v_{wstd}}{v_{mstd} + v_{wstd}}$$

0.0782662

Equation 6

$$md = \frac{(0.44 \text{ co}_2 + 0.32 \text{ o}_2 + 0.28 \text{ n}_2) \text{ lb}}{\text{lb-mole}}$$

$$\frac{30.368 \text{ lb}}{\text{lb-mole}}$$

Equation 7

$$ms = md (1 - bws) + \frac{bws \text{ 18 lb}}{\text{lb-mole}}$$

$$\frac{29.4 \text{ lb}}{\text{lb-mole}}$$

Equation 8

$$vs = kp \text{ cp } \sqrt{\Delta p} \left(\frac{ts \text{ 0.5}}{ms \text{ ps}} \right)$$

$$\frac{55.7939 \text{ ft}}{\text{sec}}$$

Equation 9

$$qa = \frac{vs \text{ as } 60 \text{ sec}}{\text{min}}$$

$$\frac{308434. \text{ ft}^3}{\text{min}}$$

Equation 10

$$qs = \frac{qa (1 - bws) 528 \text{ }^\circ\text{R ps}}{ts \text{ 29.92 in. Hg.}}$$

$$\frac{201799. \text{ ft}^3}{\text{min}}$$

Equation 11

$$cs = \frac{0.0154 \text{ gr mn}}{\text{mg vmstd}}$$

$$\frac{0.00730239 \text{ gr}}{\text{ft}^3}$$

Equation 12

$$pmr = \frac{cs \text{ qs } 60 \text{ min}}{\text{hour} \frac{7000 \text{ gr}}{\text{lb}}}$$

$$\frac{12.631 \text{ lb}}{\text{hour}}$$

Equation 13

$$e = \frac{cs \text{ f } 20.9 \text{ } 1 \text{ lb}}{(20.9 - o_2) 7000 \text{ gr}}$$

$$\frac{0.0136372 \text{ lb}}{\text{mm}^3 \text{ btu}}$$

Equation 14

$$vn = \frac{0.002669 \text{ in. Hg. ft}^3 \text{ vlc} \text{ } \text{vm y pm}}{\text{ts} \left(\frac{\text{ml } ^\circ\text{R}}{\text{tm}} + \right)}{\text{ps}}$$

$$59.3332 \text{ ft}^3$$

Equation 15

$$i = \frac{100 \% \text{ vn}}{60 \text{ sec theta vs an}} \text{ min}$$

100.297 %

Equation 16

$$hi = \frac{\text{par}}{e} \text{ 926.217 mm btu} \text{ hour}$$

APPENDIX C QUALITY CONTROL

**INITIAL
METER CALIBRATION FORM - DGM**

DATE: 12-05-95 Box No. S-101

Ref. DGM Ser. #	1044453	Calibrated By			EDWARD HARRIS	
RUN #		1	2	3	4	5
DELTA H (DGM)		0.50	1.00	1.50	2.00	3.00
Y (Ref. DGM)		1.014	1.014	1.014	1.014	1.014
Reference DGM						
Gas Vol. Initial		19.500	25.177	31.500	38.100	45.000
Gas Vol. Final		25.177	31.500	38.100	45.000	51.466
Meter Box DGM						
Gas Vol. Initial		24.400	30.000	36.261	42.805	49.615
Gas Vol. Final		30.000	36.261	42.805	49.615	56.004
Reference DGM						
Temp.		Avg.	Avg.	Avg.	Avg.	Avg.
Deg F Initial		66	67	67	67	67
Deg F Final		67	67	67	67	67
Meter Box DGM						
Temp. Initial In		66	67	68	69	69
Temp. Initial Out		66	67	68	69	69
Temp. Final In		66	67	69	69	69
Temp. Final Out		66	67	69	69	69
P Bar IN. Hg		30.08	30.08	30.08	30.08	30.08
Time (sec.)		873	688	582	525	404
Meter Calibration						
Factor (Y)		1.026	1.022	1.022	1.026	1.023
Qm (C.F.M.)		0.399	0.563	0.695	0.806	0.981
Km (Std Pressure)		0.727	0.726	0.730	0.733	0.730
DELTA Ha		1.77	1.78	1.75	1.73	1.75
Average Y (Meter Calibration Factor)					1.024	
Average Km (Standard Pressure)					0.729	
Average DELTA Ha of Orifice					1.755	

Y = $\leq .03$
 Max & Min $\leq .02$ from Avg
 Final Avg within 5% of Initial Avg
 $\Delta H_a =$ Max & Min $\leq .2$ from Avg

POST TEST QUALITY ASSURANCE

Date: 4/30/96

BOX #: S-101

Ref. Meter: 1044453

Calibrated By: Edward Harris

DRY GAS METER

		Unit	Run 1	Run 2	Run 3
FIELD METER	ΔH	In. H ₂ O	1.50	1.50	1.50
	<i>Initial Gas Volume</i>	Ft. ³	52.300	57.450	62.660
	<i>Final Gas Volume</i>	Ft. ³	57.450	62.660	68.750
	<i>Initial Temp. In</i>	°F	70	71	72
	<i>Initial Temp. Out</i>	°F	71	71	72
	<i>Final Temp. In</i>	°F	71	72	73
	<i>Final Temp. Out</i>	°F	70	72	73
REF. METER	Y	<i>Dimensionless</i>	1.014	1.014	1.014
	<i>Initial Gas Volume</i>	Ft. ³	31.300	36.500	41.750
	<i>Final Gas Volume</i>	Ft. ³	36.500	41.750	48.000
	<i>Initial Temp.</i>	°F	70	71	71
	<i>Final Temp.</i>	°F	70	71	71
	Barometric Pressure	In. Hg	29.95	29.95	29.95
	Time	sec	460	465	535
	Meter Calibration Factor	<i>Dimensionless</i>	1.021	1.019	1.040
	ΔH_s	In. H ₂ O	1.777	1.785	1.664
	Average Y	<i>Dimensionless</i>	1.027		
	Initial Y	<i>Dimensionless</i>	1.024		
	Percent Error	%	0.3 (Allowed 5.0%)		

DIFFERENTIAL PRESSURE GAUGE

Ref. Pressure in H ₂ O	Magnehelic Pressure in H ₂ O	Percent Error (+/- 5%)
0.00	0.00	0
0.50	0.51	2
1.50	1.50	0

TEMPERATURE SENSOR

Ref. Temp. (°F)	Thermocouple Temp. (°F)	Percent Error (Allowed 1.5% of Absolute)
280	281	0.14

ARENOLD BAROMETER

Reference Barometer	Test Barometer	0.1 Diff. Allowed
29.70	29.68	-0.02

MAGEHELIC CALIBRATION

BOX	2879	S-100	C-133	C-175	S-102	S-101	S-103
SER. NO.	91126AM	9126A	R90125	R74D	R22D	R20208	
	91	M91	MR6			A617	
RANGE	0-2	0-2	0-2	0-2	0-5	0-2	0-2
REFERENCE READING	FIELD DEVICE READING						
0.000		0.00	0.00	0.00	0.00	0.00	0.00
0.050							
0.150							
0.200							
0.250							
0.450							
0.50	0.50	0.51	0.50	0.51	0.51	0.50	0.50
1.00	0.99	1.01	0.98	1.01	1.01	0.98	1.01
1.30							
1.80	1.80	1.82	1.79	1.82	1.81	1.79	1.82
2.50							
4.50							
5.0							
9.0							
13.0							
22.0							

SIGNATURE: Edward L. Harris

DATE: 12-5-95

MAGEHELIC CALIBRATION
BOX #1

SER. NO.	10720- AB68	R1061- 6AG48	R5031- SEB76	R1062- 9JA82	R1051- 3MR42	R90124 RI119
RANGE	0-0.25	0-0.50	0-2	0-5	0-10	0-25
REFERENCE READING	FIELD DEVICE READING					
0.000	0.000	0.000	0.000	0.000	0.000	0.000
0.050	0.050					
0.150	0.150	0.140				
0.200	0.190					
0.250		0.250				
0.450		0.450				
0.50			0.50			
1.00			1.00			
1.30				1.30		
1.80			1.80			
2.50				2.50	2.48	
4.50				4.50		
5.0					5.0	5.0
9.0					9.02	
13.0						13.0
22.0						22.0

SIGNATURE:

Edward R. Harris

DATE:

12/22/95

MAGEHELIC CALIBRATION
BOX #2

SER. NO.	10819-DR2	R1090-2AG18	R50315-EB93	R1062-9TA87	30830-AM79	R1072-2MC5
RANGE	0-0.25	0-0.50	0-2	0-5	0-10	0-25
REFERENCE READING	FIELD DEVICE READING					
0.000	0.000	0.000	0.00	0.00	0.0	0.0
0.050	0.050					
0.150	0.155	0.152				
0.200	0.205					
0.250		0.256				
0.450		0.456				
0.50			0.52			
1.00			1.04			
1.30				1.32		
1.80			1.83			
2.50				2.55	2.49	
4.50				4.50		
5.0					4.9	5.2
9.0					8.8	
13.0						12.9
22.0						22.0

SIGNATURE:

Edward L. Harris

DATE:

12/22/95

MAGEHELIC CALIBRATION
BOX #3

SER. NO.	R10908AG71 MRR1	R0112642	R10608CF20 CF20
RANGE	0-0.50	0-2.0	0-10
REFERENCE READING	FIELD DEVICE READING		
0.000	0.000	0.00	0.0
0.050			
0.150	0.149		
0.200			
0.250	0.240		
0.450	0.450		
0.50		0.50	
1.00		0.98	
1.50			
1.80		1.78	
2.50			2.5
4.50			
5.0			5.0
9.0			9.0
13.0			
22.0			

SIGNATURE:

Edward L. Harris

DATE:

12/22/95

MAGEHELIC CALIBRATION
BOX #4

SER. NO.	R22D	R90051 6GT21	R90101 5CD102
RANGE	0-0.50	0-5	0-25
REFERENCE READING	FIELD DEVICE READING		
0.000	0.000	0.00	0.0
0.050			
0.150	0.151		
0.200			
0.250	0.251		
0.450	0.455		
0.50			
1.00			
1.30		1.27	
1.80			
2.50		2.52	
4.50		4.55	
5.0			5.0
9.0			
13.0			13.0
22.0			21.6

SIGNATURE:

Edward L. Harris

DATE:

12/22/75

TEMPERATURE CALIBRATIONS - DEGREES FAHRENHEIT

REFERENCE DEVICE READING*	0 DEG. F	210 DEG.	420 DEG.	630 DEG.	840 DEG.	1050 DEG.	1260 DEG.	1470 DEG.	1680 DEG.	1900 DEG.
2879	0	217	421	630	839	1050	1260	1471	1681	1900
METER BOX #1 C-133 11680	0	212	423	635	842	1053	1264	1475	1679	1910
METER BOX #2 C-176 15962	0	211	423	627	839	1052	1265	1475	1687	1903
METER BOX #5 S-100 16751	2	211	417	628	844	1062	1279	1491	1698	1907
METER BOX #6 S-101 15751	0	210	419	628	839	1058	1255	1473	1691	1900
PORTABLE THERMOCOUPLE # 2 (Blue)	2	209	415	628	837	1053	1260	1468	1679	1908
PORTABLE THERMOCOUPLE # 2 (Green)	2	211	417	627	842	1058	1273	1484	1688	1896
PINK T140293	-1	208	415	624	840	1056	1272	1482	1687	1894
PORTABLE THERMOCOUPLE (Yellow)	0	210	419	632	840	1050	1259	1470	1680	1901
PORTABLE THERMOCOUPLE T-105998 (Black)	1	209	416	625	839	1055	1270	1481	1684	1891
METER BOX S-102	-2	209	417	625	837	1049	1259	1462	1658	1890
METER BOX S-103	4	215	423	632	844	1057	1266	1471	1667	1895

DATE:

12-05-95

SIGNATURE:

Edward L. Harris

* Reference Device is an Omega Engineering CL505-A calibrated reference thermocouple-potentiometer system.

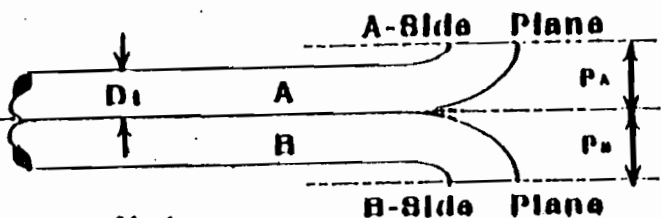
Best Available Copy



SANDERS ENGINEERING & ANALYTICAL SERVICES, Inc.

1600 Leroy Stevens Rd. Office: (205) 833-4120
 Mobile, AL 36608 FAX: (205) 833-8285

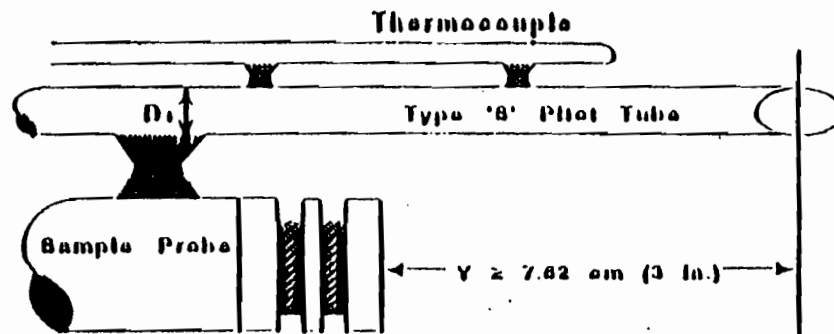
The Pilot used was within the following geometric specifications:
 D_i between 0.48 and 0.56 cm (3/16 and 3/8 in.)
 $O_p = 0.84$



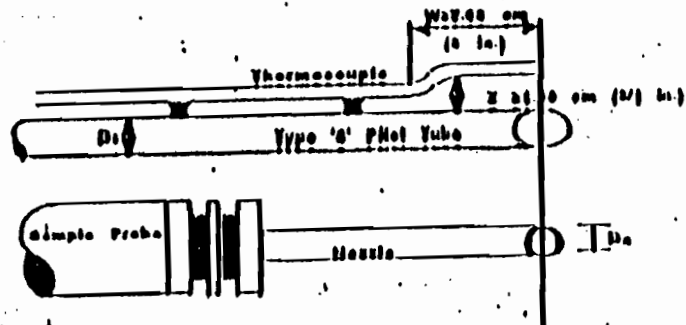
Notes:

1.05 $D_i \leq 1.50 D_i$

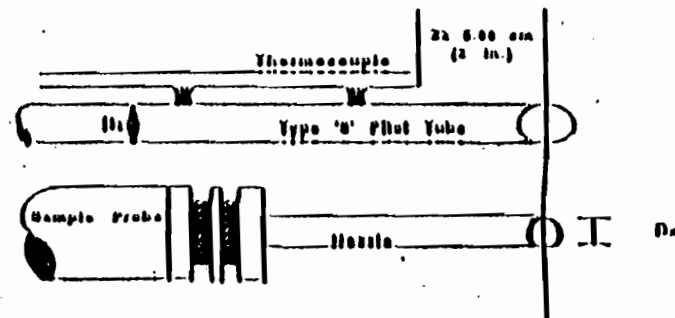
$P_A = P_B$



Minimum pilot-sample probe separation needed to prevent interference



OR



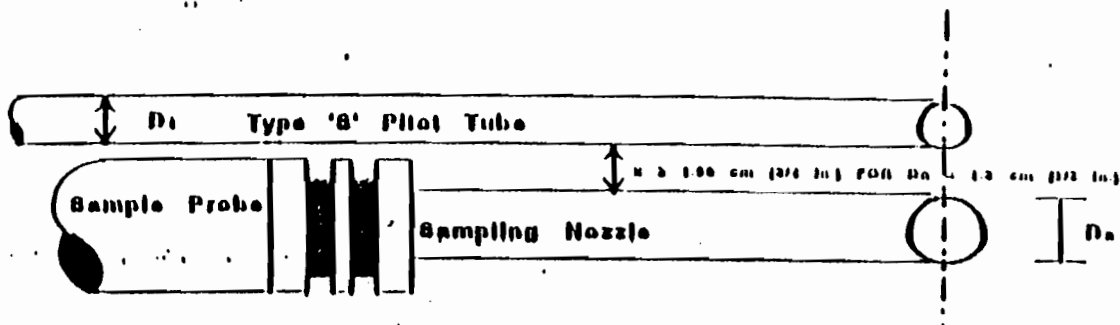
Proper thermocouple placement to prevent interference.



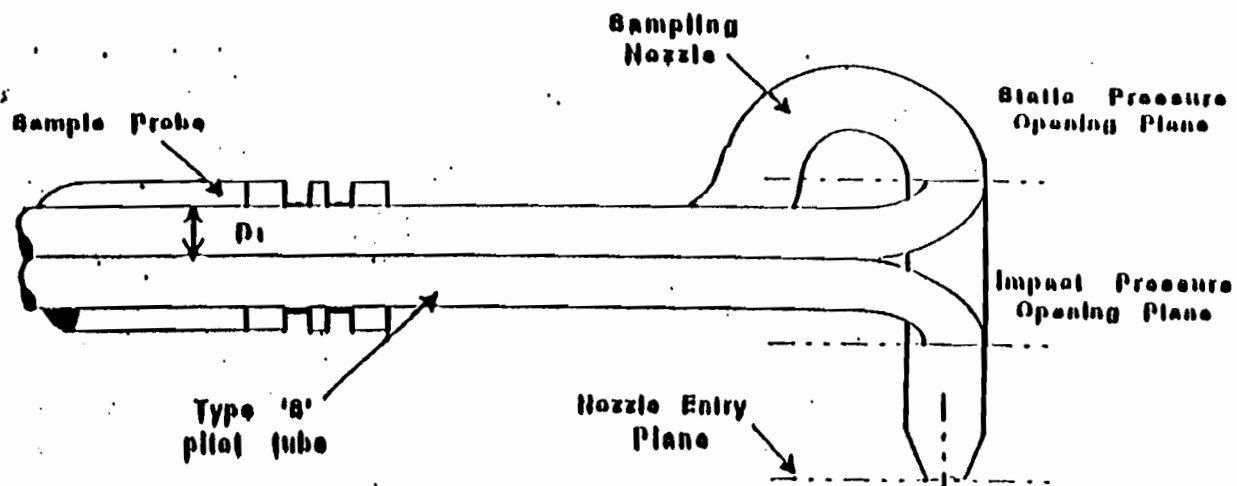
**SANDERS ENGINEERING &
ANALYTICAL SERVICES, Inc.**

1566 Jaroy Stevens Rd. Office: (205) 633-4120
Mobile, AL 36608 FAX#: (205) 633-2206

Proper pilot tube-sampling nozzle configuration to prevent aero-dynamic interference; bottomhook type nozzle; centers of nozzle and pilot opening aligned; D_1 between 0.48 and 0.66 cm (3/16 and 3/8 in.)



Bottom view showing minimum pilot/nozzle separation



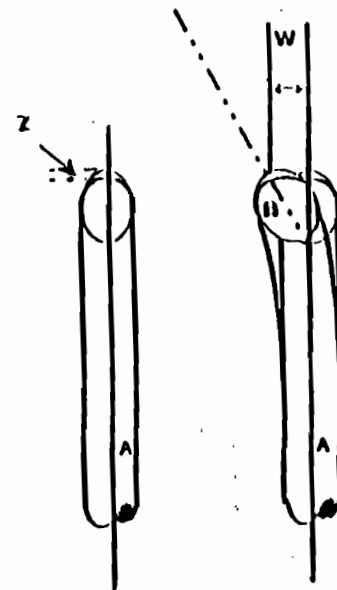
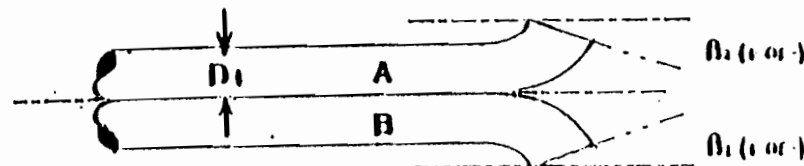
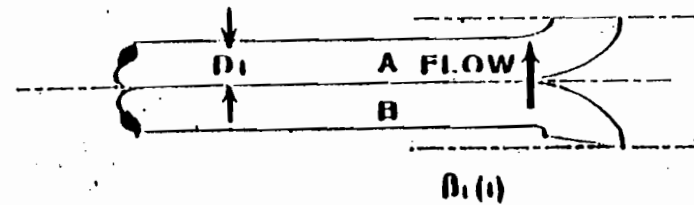
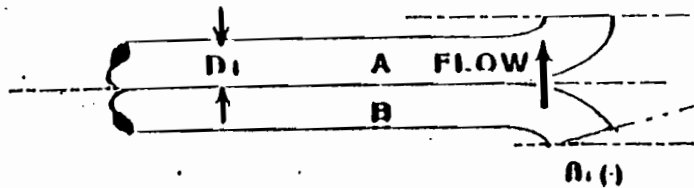
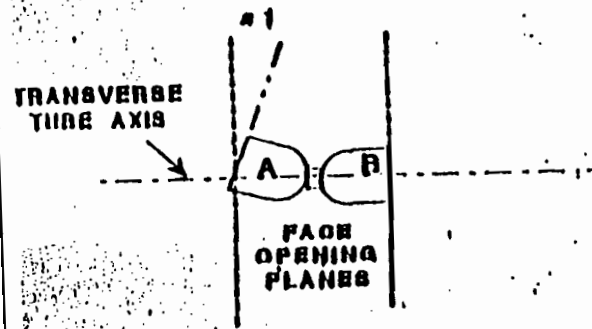
Side view; to prevent pilot tube from interfering with the gas flow streamlines approaching the nozzle, the impact pressure opening plane of the pilot tube shall be even with or above the nozzle entry plane.

Best Available Copy

SANDERS ENGINEERING & ANALYTICAL SERVICES, Inc.

1588 Leroy Stevens Rd. Office: (205) 833-4120
 Mobile, Al. 36685 FAX#1: (205) 833-2288

Types of face-opening misalignment that can result from field use or improper construction of type 'B' pitot tubes. These will not affect the baseline value of $C_p(\alpha)$ so long as α_1 and $\alpha_2 \leq 10^\circ$, θ_1 and $\theta_2 \leq 6^\circ$, and $\delta \leq 0.32$ cm (1/8 in.)



Criet ELECTRIC GENERATING PLANT

SOOTBLOWING

UNIT 5
DATE 4-17-96

TIME	RUN NUMBER	MAIN STEAM FLOW (LBS/HR)	MW LOAD	BOILER AIR FLOW	PULVERIZER MILLS COAL FLOW 10 ³ LB/HR					% O ₂		% OPACITY	I.D. FAN AMPS			GAS TEMP (°F) AIR PREHEATER		PULVERIZER MILLS TEMPERATURES °F												
					A	B	C	D			F.R.		EMS	A					A	B	C	D								
Start	817	1	719	98	703	51281	527669	22657	612877			6.5	4.3	5.0	250			292	275					162	135	160	162			
Finish	923					51470	527953	22846	613111																					
Start	1000	2	721	98	702	51570	528103	22956	613224			6.5	4.1	4.7	250			295	292						162	135	159	162		
Finish	1143					51760	528387	23137	613441																					
Start	1420	3				52263	529140	23645	614011			6.5	4.0	4.7	250			299	299						162	135	159	162		
Finish	1531					52428	529399	23816	614267																					

Opacity Percent	01-06	5.1	31-36	5.4
	07-12	5.2	37-42	5.6
	13-18	5.0	43-48	5.1
	19-24	4.8	49-54	4.8
	25-30	5.1	55-60	5.2

Hourly Averages	S02		NOX		CO2
Measured	616.7 ppm		293.4 ppm		13.0 %
Bias Adjusted	624.7 ppm		300.7 ppm		13.0 %
Rate	1.4 lb/mmbtu		0.4 lb/mmbtu		
Bias Adjusted	1.4 lb/mmbtu		0.4 lb/mmbtu		
3 Hr Avg					
Mass Emissions	1401.1 lb/mmbtu				101.4 ton/hr
Bias Adjusted	1419.2 lb/hr				101.4 ton/hr
Bias Factor	1.012		1.024		0.999
Source	1		1		1
Heat Input	988.4				
Load Range	2.6				
Zero Calibration	0.9 ppm		1.1 ppm		0.0 %
Expected Value	0.0 ppm		0.0 ppm		0.0 %
Span Calibration	2647.8 ppm		877.5 ppm		17.3 %
Expected Value	2620.0 ppm		876.0 ppm		16.9 %

Hourly Averages	Flow		Gross Generation		Opacity
Measured	13686000 scfh		89.5 MWge		
Bias Adjusted	13685589 scfh				
Bias Factor	0.999				
Source	1				
Zero Calibration	-0.8 scfh				0.1 %
Expected Value	0.0 scfh				0.0 %
Span Calibration	261.2 scfh				42.1 %
Expected Value	262.5 scfh				42.7 %

Instrument Status	Opacity Monitor	Normal
	S02 Analyzer	Normal
	NOX Analyzer	Normal
	CO2 Analyzer	Normal
	Flow Monitor	Normal

Legend ** Excess Emissions ## Insufficient Data
 !! Fans Off \$\$ Boiler Off

=====

Crist Unit 5
Pensacola, Florida

Today's Date: 04/18/96
Today's Time: 17:14:01

Report Date: 04/17/96
Report Hour: 08 - 09

Opacity Percent	01-06	5.1	31-36	5.5
	07-12	5.0	37-42	5.1
	13-18	5.1	43-48	5.1
	19-24	5.0	49-54	5.2
	25-30	5.2	55-60	4.7

Hourly Averages	S02	NOX	CO2
Measured	618.2 ppm	306.5 ppm	12.9 %
Bias Adjusted	626.2 ppm	314.2 ppm	12.9 %
Rate	1.4 lb/mmbtu	0.5 lb/mmbtu	
Bias Adjusted	1.4 lb/mmbtu	0.5 lb/mmbtu	
3 Hr Avg			
Mass Emissions	1368.8 lb/mmbtu		98.0 ton/hr
Bias Adjusted	1386.4 lb/hr		98.0 ton/hr
Bias Factor	1.012	1.024	0.999
Source	1	1	1
Heat Input	955.8		
Load Range	2.6		
Zero Calibration	1.2 ppm	1.1 ppm	0.0 %
Expected Value	0.0 ppm	0.0 ppm	0.0 %
Span Calibration	2629.9 ppm	875.0 ppm	17.2 %
Expected Value	2620.0 ppm	876.0 ppm	16.9 %

Hourly Averages	Flow	Gross Generation	Opacity
Measured	13338000 scfh	89.8 MWge	
Bias Adjusted	13337599 scfh		
Bias Factor	0.999		
Source	1		
Zero Calibration	-0.8 scfh		0.1 %
Expected Value	0.0 scfh		0.0 %
Span Calibration	258.3 scfh		42.1 %
Expected Value	262.5 scfh		42.7 %

Instrument Status	Opacity Monitor	Normal
	S02 Analyzer	Normal Calibration
	NOX Analyzer	Normal Calibration
	CO2 Analyzer	Normal Calibration
	Flow Monitor	Normal Calibration

Legend	** Excess Emissions	## Insufficient Data
	!! Fans Off	\$\$ Boiler Off

Crist Unit 5
Pensacola, Florida

Today's Date: 04/18/96
Today's Time: 17:16:21

Report Date: 04/17/96
Report Hour: 09 - 10

Opacity Percent	01-06	5.0	31-36	5.8
	07-12	5.1	37-42	5.0
	13-18	4.9	43-48	4.8
	19-24	5.3	49-54	5.8
	25-30	4.8	55-60	4.9

Hourly Averages	S02	NOX	CO2
Measured	609.5 ppm	291.7 ppm	13.1 %
Bias Adjusted	617.4 ppm	299.0 ppm	13.1 %
Rate	1.3 lb/mmbtu	0.4 lb/mmbtu	
Bias Adjusted	1.4 lb/mmbtu	0.4 lb/mmbtu	
3 Hr Avg			
Mass Emissions	1347.1 lb/mmbtu		99.4 ton/hr
Bias Adjusted	1364.5 lb/hr		99.4 ton/hr
Bias Factor	1.012	1.024	0.999
Source	1	1	1
Heat Input	968.9		
Load Range	2.6		
Zero Calibration	1.2 ppm	1.1 ppm	0.0 %
Expected Value	0.0 ppm	0.0 ppm	0.0 %
Span Calibration	2629.9 ppm	875.0 ppm	17.2 %
Expected Value	2620.0 ppm	876.0 ppm	16.9 %

Hourly Averages	Flow	Gross Generation	Opacity
Measured	13314000 scfh	89.8 MWge	
Bias Adjusted	13313600 scfh		
Bias Factor	0.999		
Source	1		
Zero Calibration	-0.8 scfh		0.1 %
Expected Value	0.0 scfh		0.0 %
Span Calibration	258.3 scfh		42.1 %
Expected Value	262.5 scfh		42.7 %

Instrument Status	Opacity Monitor	Normal
	S02 Analyzer	Normal
	NOX Analyzer	Normal
	CO2 Analyzer	Normal
	Flow Monitor	Normal

Legend	** Excess Emissions	## Insufficient Data
	!! Fans Off	\$\$ Boiler Off

Crist Unit 5
Pensacola, Florida

Today's Date: 04/18/96
Today's Time: 17:18:18

Report Date: 04/17/96
Report Hour: 10 - 11

Opacity Percent	01-06	4.8	31-36	5.2
	07-12	5.2	37-42	5.7
	13-18	5.0	43-48	5.8
	19-24	5.6	49-54	5.7
	25-30	6.5	55-60	5.7

Hourly Averages	S02	NOX	CO2
Measured	605.9 ppm	291.5 ppm	13.1 %
Bias Adjusted	613.8 ppm	298.8 ppm	13.1 %
Rate	1.3 lb/mmbtu	0.4 lb/mmbtu	
Bias Adjusted	1.4 lb/mmbtu	0.4 lb/mmbtu	
3 Hr Avg			
Mass Emissions	1340.9 lb/mmbtu		99.5 ton/hr
Bias Adjusted	1358.4 lb/hr		99.5 ton/hr
Bias Factor	1.012	1.024	0.999
Source	1	1	1
Heat Input	970.2		
Load Range	2.6		
Zero Calibration	1.2 ppm	1.1 ppm	0.0 %
Expected Value	0.0 ppm	0.0 ppm	0.0 %
Span Calibration	2629.9 ppm	875.0 ppm	17.2 %
Expected Value	2620.0 ppm	876.0 ppm	16.9 %

Hourly Averages	Flow	Gross Generation	Opacity
Measured	13332000 scfh	89.8 MWge	
Bias Adjusted	13331600 scfh		
Bias Factor	0.999		
Source	1		
Zero Calibration	-0.8 scfh		0.1 %
Expected Value	0.0 scfh		0.0 %
Span Calibration	258.3 scfh		42.1 %
Expected Value	262.5 scfh		42.7 %

Instrument Status	Opacity Monitor	Normal
	S02 Analyzer	Normal
	NOX Analyzer	Normal
	CO2 Analyzer	Normal
	Flow Monitor	Normal

Legend ** Excess Emissions ## Insufficient Data
 !! Fans Off \$\$ Boiler Off

Crist Unit 5
Pensacola, Florida

Today's Date: 04/18/96
Today's Time: 17:22:13

Report Date: 04/17/96
Report Hour: 13 - 14

Opacity Percent	01-06	5.5	31-36	6.3
	07-12	5.7	37-42	6.4
	13-18	5.7	43-48	5.4
	19-24	6.4	49-54	5.3
	25-30	6.3	55-60	5.3

Hourly Averages	S02	NOX	CO2
Measured	596.2 ppm	296.0 ppm	13.0 %
Bias Adjusted	603.9 ppm	303.4 ppm	13.0 %
Rate	1.3 lb/mmbtu	0.4 lb/mmbtu	
Bias Adjusted	1.3 lb/mmbtu	0.5 lb/mmbtu	
3 Hr Avg			
Mass Emissions	1312.3 lb/mmbtu		98.2 ton/hr
Bias Adjusted	1329.2 lb/hr		98.2 ton/hr
Bias Factor	1.012	1.024	0.999
Source	1	1	1
Heat Input	957.6		
Load Range	2.6		
Zero Calibration	1.2 ppm	1.1 ppm	0.0 %
Expected Value	0.0 ppm	0.0 ppm	0.0 %
Span Calibration	2629.9 ppm	875.0 ppm	17.2 %
Expected Value	2620.0 ppm	876.0 ppm	16.9 %

Hourly Averages	Flow	Gross Generation	Opacity
Measured	13260000 scfh	89.6 MWge	
Bias Adjusted	13259602 scfh		
Bias Factor	0.999		
Source	1		
Zero Calibration	-0.8 scfh		0.1 %
Expected Value	0.0 scfh		0.0 %
Span Calibration	258.3 scfh		42.1 %
Expected Value	262.5 scfh		42.7 %

Instrument Status	Opacity Monitor	Normal
	S02 Analyzer	Normal
	NOX Analyzer	Normal
	CO2 Analyzer	Normal
	Flow Monitor	Normal

Legend ** Excess Emissions ## Insufficient Data
 !! Fans Off \$\$ Boiler Off

Crist Unit 5
Pensacola, Florida

Today's Date: 04/18/96
Today's Time: 17:24:28

Report Date: 04/17/96
Report Hour: 14 - 15

Opacity Percent	01-06	5.5	31-36	5.6
	07-12	5.1	37-42	8.4
	13-18	5.9	43-48	5.9
	19-24	5.6	49-54	6.5
	25-30	5.9	55-60	5.8

Hourly Averages	S02	NOX	CO2
Measured	596.8 ppm	295.1 ppm	13.1 %
Bias Adjusted	604.5 ppm	302.5 ppm	13.1 %
Rate	1.3 lb/mmbtu	0.4 lb/mmbtu	
Bias Adjusted	1.3 lb/mmbtu	0.4 lb/mmbtu	
3 Hr Avg			
Mass Emissions	1310.7 lb/mmbtu		98.7 ton/hr
Bias Adjusted	1327.6 lb/hr		98.7 ton/hr
Bias Factor	1.012	1.024	0.999
Source	1	1	1
Heat Input	962.8		
Load Range	2.6		
Zero Calibration	1.2 ppm	1.1 ppm	0.0 %
Expected Value	0.0 ppm	0.0 ppm	0.0 %
Span Calibration	2629.9 ppm	875.0 ppm	17.2 %
Expected Value	2620.0 ppm	876.0 ppm	16.9 %

Hourly Averages	Flow	Gross Generation	Opacity
Measured	13230000 scfh	89.6 MWge	
Bias Adjusted	13229603 scfh		
Bias Factor	0.999		
Source	1		
Zero Calibration	-0.8 scfh		0.1 %
Expected Value	0.0 scfh		0.0 %
Span Calibration	258.3 scfh		42.1 %
Expected Value	262.5 scfh		42.7 %

Instrument Status	Opacity Monitor	Normal
	S02 Analyzer	Normal
	NOX Analyzer	Normal
	CO2 Analyzer	Normal
	Flow Monitor	Normal

Legend ** Excess Emissions ## Insufficient Data
 !! Fans Off \$\$ Boiler Off

CRIST ELECTRIC GENERATING PLANT

Precipitator Readings

Unit 5
 Date 4-17-96
 Load 88 MW

Run # 1
 Start Time 0812
 Finish Time 0923

Precipitator Cabinet	Primary AMPS	Primary Volts	Secondary AMPS	Secondary Voltage
Start	A	54	360	340
	B	58	390	550
	C	58	330	280
Finish	A	52	360	.34
	B	59	385	.54
	C	58	330	.28

CRIST ELECTRIC GENERATING PLANT

Precipitator Readings

Unit 5
 Date 4-17-96
 Load 88 MW

Run # 1
 Start Time 0812
 Finish Time 0923

Precipitator Cabinet	Primary AMPS	Primary Volts	Secondary AMPS	Secondary Voltage
Start	A	112	370	1420
	B	123	0	860
	C	50	280	340
	D	90	380	550
	E	80	360	640
	F	94	370	740

Finish	A	100	370	1420
	B	123	0	.84
	C	50	280	.28
	D	90	360	.46
	E	80	360	.64
	F	94	370	.74

CRIST ELECTRIC GENERATING PLANT

Precipitator Readings

Unit 5
 Date 4-17-96
 Load 88 MW

Run # 2
 Start Time 10:08
 Finish Time 11:13

Precipitator Cabinet	Primary AMPS	Primary Volts	Secondary AMPS	Secondary Voltage
Start	A	52	360	.34
	B	59	385	.54
	C	58	330	.28
Finish	A	52	360	.34
	B	58	385	.54
	C	58	330	.28

CRIST ELECTRIC GENERATING PLANT

Precipitator Readings

Unit 5
 Date 4-17-96
 Load 88 MW

Run # 2
 Start Time 10:08
 Finish Time 11:13

Precipitator Cabinet	Primary AMPS	Primary Volts	Secondary AMPS	Secondary Voltage
Start	A	100	370	1.420
	B	123	0	.84
	C	50	280	.28
	D	70	360	.46
	E	80	360	.64
	F	94	370	.74
Finish	A	110	370	1.420
	B	125	0	.84
	C	50	340	.28
	D	50	320	.26
	E	80	360	.64
	F	94	370	.74

CRIST ELECTRIC GENERATING PLANT

Precipitator Readings

Unit 5
 Date 4-17-96
 Load 88 MW

Run # 3
 Start Time 1420
 Finish Time _____

Precipitator Cabinet	Primary AMPS	Primary Volts	Secondary AMPS	Secondary Voltage
Start	A	52	360	.34
	B	58	380	.54
	C	58	330	.28
	.			
Finish	A	52	360	.34
	B	58	380	.54
	C	58	330	.28

CRIST ELECTRIC GENERATING PLANT

Precipitator Readings

Unit 5
 Date 4-17-96
 Load 88MW

Run # 3
 Start Time 1426
 Finish Time 1531

Precipitator Cabinet	Primary AMPS	Primary Volts	Secondary AMPS	Secondary Voltage
Start	A	110	370	1.42
	B	123	0	.84
	C	45	260	.26
	D	80	370	.56
	E	80	360	.64
	F	94	370	.74
Finish	A	110	370	1.42
	B	123	0	.84
	C	45	260	.28
	D	45	300	.24
	E	78	360	.62
	F	94	370	.74

APPENDIX D OPERATIONAL DATA