#### DEPARTMENT OF PUBLIC UTILITIES

Solid Waste Disposal Division February 13, 1992

Mr. Steve Smallwood, P.E. FDER 2600 Blair Stone Road Tallahassee, Florida 32399-2400

RECEIVE FEB 20 1992

Division of Air Resources Management

AC 16-186047

REF: DER Flare Construction Permit

Your Letter of June 3, 1991

Dear Mr. Smallwood:

We are nearing construction of our East Landfill closure and expect bids to be received Wednesday, February 26, 1992. As a part of that closure project, the contractor will be constructing a gas collection and flare system. We expect construction to begin in late March or early April, and be completed in early 1993.

We definitely concur with the second paragraph of your June 3 letter, and in fact, have designed our system, with a built-in gas access point, for connection to other future disposal methods. As designed, the system would burn the gas until appropriate alternate methods were found, constructed and made available. At that time, the blind flange could be removed from this point in our system, a pipeline installed to this new process facility, and the valve opened up for recovery of the landfill gas. We would retain the flare system as a back up disposal method.

The purpose of this letter is to request a one year extension to the construction permit. This permit now expires on February 15, 1992. We will have the system completed and operational by February 15, 1993.

Your favorable consideration and approval of this request would be appreciated. We look forward to commencing construction in approximately one month.

Sincerely,

William C. Boyle

Manager

WCB:rsz

cc:

Reading File

M. 13acq a. Kutynd R. Robelown,



AREA CODE 904 / 630-0973 / 37-2 WEST 1st STREET / JACKSONVILLE, FLORIDA 32206



# Florida Department of Environmental Regulation

Twin Towers Office Bldg. • 2600 Blair Stone Road • Tallahassee, Florida 32399-2400 Lawton Chiles, Governor Carol M. Browner, Secretary

February 21, 1992

#### CERTIFIED MAIL-RETURN RECEIPT REQUESTED

Mr. William C. Boyle, Manager City of Jacksonville Department of Public Utilities Solid Waste Disposal Division 37-2 West 1st Street Jacksonville, FL 32206

Dear Mr. Boyle:

RE: Flare Construction Permit AC 16-186047 East Landfill, Duval County

The Bureau of Air Regulation received your request to extend the above referenced air construction permit. On October 30, 1991, Rule 17-4.050(4)(o), F.A.C., (copy enclosed) was changed to require a \$50 fee per permit to process extension requests; therefore, we will not be able to take action on your request until the fee is received. If you have any questions, please call Patty Adams at (904)488-1344.

Sincerely,

C. H. Fancy, P.E.

Chief

Bureau of Air Regulation

CHF/pa

Enclosure

Department of Environmental Regulation Routing and Transmittal Slip To: (Name, Office, Location) Remarks: From: Phone



	TO MR.	TOW	1	CASCIO DATE 11/10/92
	BURG	w of	An	IR QUALITY MUNT JOB NO. 07-421.05
	_ FDE	٤		RE TACKSONVICLE EAST
	TWIN	TOWS. AAAS	e5 6F <del>≥==</del>	The building
		***************************************		3230/
- 1V	WE DE SE	NDING Yo	OU 🎘	RE TACKSONVICCE EAST  3230/  Attached   Under separate cover via  Prints   Plans   Samples  Change Order   Specifications
CCE.	പ്പാര്യു Shop Dra	wings	□₽	Prints □ Plans □ Samples
Br NON TO	Of Acopyret L	etter	□ c	Prints
Divisio	Mariab	DATE	NO.	DESCRIPTION
Resour	1			FLARE PARKAGE
				·
	THESE ARE	TRANSM	IITTED	As Checked Below:
	☐ For a	pproval		☐ Approved as submitted ☐ Resubmit copies for approval
	For y			☐ Approved as noted ☐ Submit copies for distribution
				☐ Returned for corrections ☐ Return corrected prints
	☐ For re	eview and o	comment	t 🗆
	☐ For b	ids due		_19
	☐ Prints	returned a	ıfter loan	n to us
	REMARKS	PER	ou e	TEREPHONE CONVERSATION ON
				E IS THE INFORMATION ON
		_		SED Frank FOR THE JACKSONVILLE
				PROJECT,
	PLEASE	CA	u	IF YOU HAVE ANY FURTHER
	QUESTR	<u>ځک</u>	OR	COMMENTS.
	•	any.		
	SIGNED	Kan	2.	A Selmis
	DISTRIBUTI			
FORM NO. CIS070.01	ון טפוח ו פוט	∪IN		If enclosures are not as noted, kindly notify us at once

(407)647-7275

## THE CITY OF JACKSONVILLE DEPARTMENT OF PUBLIC UTILITIES SOLID WASTE DISPOSAL DIVISION

## EAST DUVAL SANITARY LANDFILL AIR POLLUTION SOURCE (LANDFILL GAS FLARE) INFORMATION PACKAGE

**Includes:** 

- 1. Original Submittal (August 1990)
- 2. Response to FDER's RAI (December 1991)
- 3. Misc. Supporting Documents from Manufacturer

November 10, 1992

### Prepared For:

Department of Environmental Regulations Bureau of Air Quality Management Tallahassee, Florida

### Prepared By:

Post, Buckley, Schuh & Jernigan, Inc. Solid Waste Division 1560 Orange Avenue, Suite 700 Winter Park, Florida 3278

THE CITY OF JACKSONVILLE DEPARTMENT OF PUBLIC UTILITIES SOLID WASTE DISPOSAL DIVISION

EAST DUVAL SANITARY LANDFILL APPLICATION TO CONSTRUCT AIR POLLUTION SOURCE (LANDFILL GAS FLARE)

# THE CITY OF JACKSONVILLE DEPARTMENT OF PUBLIC UTILITIES SOLID WASTE DISPOSAL DIVISION

# EAST DUVAL SANITARY LANDFILL APPLICATION TO CONSTRUCT AIR POLLUTION SOURCE (LANDFILL GAS FLARE)

August 1990

Prepared by:

POST, BUCKLEY, SCHUH & JERNIGAN, INC. Engineering - Planning - Architecture 6635 E. Colonial Drive Orlando, Florida 32807



#### ENVIRONMENTAL LABORATORIES

6635 EAST COLONIAL DRIVE ORLANDO, FLORIDA 32807 407/277-4443

August 27, 1990

Mr. Clair Fancy, P.E.
Bureau of Air Quality Management
Florida Department of Environmental Regulation
2600 Blair Stone Road
Twin Towers Office Building
Tallahassee, Florida 32301

Reference: East Duval Sanitary Landfill
Application to Construct Air Pollution
Source (Landfill Gas Flare)

Dear Mr. Fancy:

Pursuant to the requirement of specific condition Number 9 of the East Duval Sanitary Landfill Closure Permit Number SF16-155245, the City of Jacksonville, Solid Waste Disposal Division is pleased to submit four (4) copies of this Application to Construct Air Pollution Source (Landfill Gas Flare).

A check in the amount of \$2,500 is enclosed as specified in Florida Administrative Code Rule 17-4.050.

If you have any questions or comments regarding this application, please do not hesitate to call.

Very truly yours,

PBS&J ENVIRONMENTAL LABORATORIES

Jerome J. Guidry, P.E. Vice President

JJG:kf

cc: G. Threlkeld

# DEPARTMENT OF ENVIRONMENTAL REGULATION **BEST AVAILABLE COPY**

CENTRAL FLORIDA, DISTRICT 3319 MAGUIRE BOULEVARD SUITE 232 ORLANDO, FLORIDA 32863-3767



**BOB MARTINEZ** RCHESTOD DALE TWACHTMANN SECRETARY ALEX ALEXANDER C STRICT MANAGER

APPLICATION TO OPERATE/	CONSTRUCT AIR POLLUTION SOURCES
SOURCE TYPE: Landfill Gas	[X] New <sup>1</sup> [ ] Existing <sup>1</sup>
APPLICATION TYPE: [X] Construction [ ]	Operation [ ] Modification
COMPANY NAME: City of Jacksonville	COUNTY: Duyal
Identify the specific emission point sour	ce(s) addressed in this application (i.e. Lime
Kiln No. 4 with Venturi Scrubber; Peaking	Unit No. 2, Gas Fired) Landfill Gas Flare
SOURCE LOCATION: Street 515 Girvin Road	
UTM: East 454.95 km	58" Morth 3355.57 km - 394
Latitude 30 ° 16	58" 90" 0780" 140" N Longitude 81 ° 28 ' 36 "W
APPLICANT NAME AND TITLE: George R. K	Inecht, P.E. Manager of Disposal
APPLICANT ADDRESS: Solid Waste Disposal Divi	sion, 1931 East Beaver Street Jacksonville, FL 32202
SECTION I: STATEMENT	S BY APPLICANT AND ENGINEER
A. APPLICANT	•
I am the undersigned owner or authoriz	ed representative* of <u>City of Jacksonville</u>
I agree to maintain and operate the facilities in such a manner as to co Statutes, and all the rules and regula also understand that a permit, if gra and I will promptly notify the departmestablishment.	to the best of my knowledge and belief. Further pollution control source and pollution control mply with the provision of Chapter 403, Floridations of the department and revisions thereof. Intendigue the department, will be non-transferable and upon sale or legal transfer of the permittent.
*Attach letter of authorization	Signed: / Lyck Presht
	George R. Knecht, P.E. Manager of Disposal Name and Title (Please Type)
	Date: 6/25/90 Telephone No. (904) 630-0973
B. PROFESSIONAL ENGINEER REGISTERED IN FL	ORIDA (where required by Chapter 471, F.S.)

This is to certify that the engineering features of this pollution control project have been NEXESTENDED examined by me and found to be in conformity with modern engineering principles applicable to the treatment and disposal of pollutants characterized in the permit application. There is reasonable assurance, in my professional judgment, the

1 See Florida Administrative Code Rule 17-2.100(57) and (104)

DER Form 17-1.202(1) Effective October 31, 1982

	Signed Jerome J. Guidry, P.E.
	Post, Buckley, Schuh & Jernigan, Inc.
	Name (Please Type)
	6635 E. Colonial Drive, Orlando, Florida 32807  Company Name (Please Type)
	Company Name (Flease (ype)
•	Mailing Address (Please Type)
ida Registration No. 32589	Date: Telephone No. (904) 277-4443
	N II: GENERAL PROJECT INFORMATION
3201106	A II: GENERAL PROJECT INFORMATION
	n source performance as a result of installation. State sult in full compliance. Attach additional sheet if
The East Duval Sanitary I	andfill will incompand an active are a constant and active are
The East Buvar baintary 1	bandin win incorporate an active gas management system to cone
	use of a flare, landfill gases. This project will result in full
and burn off, through the	
and burn off, through the	use of a flare, landfill gases. This project will result in full
and burn off, through the	use of a flare, landfill gases. This project will result in full
and burn off, through the  compliance with F.A.C. R  Schedule of project covered	use of a flare, landfill gases. This project will result in full
and burn off, through the  compliance with F.A.C. R  Schedule of project covered  Start of Construction Marc  Costs of pollution control s for individual components/un  Information on actual costs	use of a flare, landfill gases. This project will result in full Rule 17-3, See Section IIA Attachment.  in this application (Construction Permit Application Only th, 1991
and burn off, through the  compliance with F.A.C. R  Schedule of project covered  Start of Construction Marc  Costs of pollution control s for individual components/un Information on actual costs	use of a flare, landfill gases. This project will result in full Rule 17-3, See Section IIA Attachment.  in this application (Construction Permit Application Only th, 1991 Completion of Construction June, 1991  system(s): (Note: Show breakdown of estimated costs only pits of the project serving pollution control purposes. shall be furnished with the application for operation
and burn off, through the  compliance with F.A.C. R  Schedule of project covered  Start of Construction Marc  Costs of pollution control s  for individual components/un  Information on actual costs  permit.)	use of a flare, landfill gases. This project will result in full Rule 17-3, See Section IIA Attachment.  in this application (Construction Permit Application Only th, 1991 Completion of Construction June, 1991  system(s): (Note: Show breakdown of estimated costs only pits of the project serving pollution control purposes. shall be furnished with the application for operation
and burn off, through the  compliance with F.A.C. R  Schedule of project covered  Start of Construction Marc  Costs of pollution control s  for individual components/un  Information on actual costs  permit.)	use of a flare, landfill gases. This project will result in full Rule 17-3, See Section IIA Attachment.  in this application (Construction Permit Application Only th, 1991 Completion of Construction June, 1991  system(s): (Note: Show breakdown of estimated costs only pits of the project serving pollution control purposes. shall be furnished with the application for operation
and burn off, through the  compliance with F.A.C. R  Schedule of project covered  Start of Construction Marc  Costs of pollution control s  for individual components/un  Information on actual costs  permit.)	in this application (Construction Permit Application Only  th, 1991 Completion of Construction June, 1991  system(s): (Note: Show breakdown of estimated costs only  sits of the project serving pollution control purposes.  shall be furnished with the application for operation
and burn off, through the  compliance with F.A.C. R  Schedule of project covered  Start of Construction Marc  Costs of pollution control s  for individual components/un  Information on actual costs  permit.)	use of a flare, landfill gases. This project will result in full Rule 17-3, See Section IIA Attachment.  in this application (Construction Permit Application Only th, 1991 Completion of Construction June, 1991  system(s): (Note: Show breakdown of estimated costs only pits of the project serving pollution control purposes. shall be furnished with the application for operation
and burn off, through the  compliance with F.A.C. R  Schedule of project covered  Start of Construction Marc  Costs of pollution control s for individual components/un  Information on actual costs permit.)  Enclosed Ground Flare -	use of a flare, landfill gases. This project will result in full  Rule 17-3, See Section IIA Attachment.  in this application (Construction Permit Application Only th, 1991
and burn off, through the  compliance with F.A.C. R  Schedule of project covered  Start of Construction Marc  Costs of pollution control s for individual components/un  Information on actual costs permit.)  Enclosed Ground Flare -	use of a flare, landfill gases. This project will result in full cule 17-3, See Section IIA Attachment.  in this application (Construction Permit Application Only th, 1991

	this is a new source or major modification, answer the following questes or No)	ions.
١.	Is this source in a non-attainment area for a particular pollutant?	NO
	a. If yes, has "offset" been applied?	N/A
	b. If yes, has "Lowest Achievable Emission Rate" been applied?	N/A
	c. If yes, list non-attainment pollutants.	N/A
٠.	Does best available control technology (BACT) apply to this source? If yes, see Section VI.	NO_
	Does the State "Prevention of Significant Deterioriation" (PSD) requirement apply to this source? If yes, see Sections VI and VII.	NO
•	Do "Standards of Performance for New Stationary Sources" (NSPS) apply to this source?	NO
•	Do "National Emission Standards for Hazardous Air Pollutants" (NESHAP) apply to this source?	NO
	"Reasonably Available Control Technology" (RACT) requirements apply this source?	NO
	a. If yes, for what pollutants?	

#### SECTION III: AIR POLLUTION SOURCES & CONTROL DEVICES (Other than Incinerators)

4. Raw Materials and Chemicals Used in your Process, if applicable: N/A

	Contam	inants	Utilization	
Description	Type	% Wt	Rate - lbs/hr	Relate to Flow Diagram
				· · · · · · · · · · · · · · · · · · ·
<u>-</u>				·
	-			
		<u>.</u>		

₽.	Process Rate,	if	applicable:	(See Section V	Ι,	Item 1)	
----	---------------	----	-------------	----------------	----	---------	--

1.	Total Process	Input Rate	(lbs/hr):	N/A

N/A

. Airborne Contaminants Emitted: (Information in this table must be submitted for each emission point, use additional sheets as necessary)

Name of	Emission <sup>1</sup>	Allowed <sup>2</sup> Emission Rate per	Allowable <sup>3</sup> Emission	Potential <sup>4</sup> Emission	Relate to Flow
Contaminant	Maximum Actual lbs/hr T/yr	Rule 17-2	lbs/hr	lbs/yr T/yr	Diagram
CH4	55.4 242.7			See Section	
N Ox	5.36 23.48			III C Attachment	
CO2	14,621 64,040	-			·
СО	23.84 104.42	,	_		
N2	88,168 386,176		•		
O2	15,632 68,468				

H2O 7,188 31,483 See Section V, Item 2.

Product Weight (lbs/hr):\_\_

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Reference applicable emission standards and units (e.g. Rule 17-2.600(5)(b)2. Table II, E. (1) - 0.1 pounds per million BTU heat input)

<sup>&</sup>lt;sup>3</sup>Calculated from operating rate and applicable standard.

 $<sup>^{4}</sup>$ Emission, if source operated without control (See Section V, Item 3).

Name and Type (Model & Serial No		Contaminant	Eff	ciclency	Size (in	f Particles Collected microns) plicable)	Basis for Efficiency (Section V Item 5)
McGill Environmental	System	s, Inc.	98% I	Expected			
Model EGF-60 (or equi			Minir	num Destri	etion		
			Non-September 2000	iency		_	
	_					_	
. Fuels N/A							
	-	<del></del>	Consum	ption*			
Type (Be Specif	.c)	avq/hı			x./hr		Heat Input BIU/hr)
			· -				•
Inits: Natural Gas	MMCF/I	nr; Fuel Oils	gall	ons/hr; Co	oal, wood,	refuse, other	rlbs/hr.
uel Analysis:							
ercent Sulfur:				Percent	Ash:		
ensity:		1	bs/gal	Typical	Percent N.	itrogen:	
eat Capacity:	-		BTU/16				8TU/ga:
her Fuel Contaminan	ts (wi	nich may caus	e air	pollution)	:		·
					·		
If applicable, in	dicate	the percent	of fu	el used fo	or apace hi	eating.	
inual Average	/A		ма	eximum		<del>-</del>	
Indicate liquid o	r soli	id wastes gen	erated	and metho	d of disp	osal.	
N/A							

DER Form 17~1.202(1) Effective November 30, 1982

PERCK HOTO	ght:	40		ft. S	Stack Diame	ter:	7.6
Gas Flow f	Rate: 120.06	O ACEM	26,450	 DSCEM 0	lag Fyit Ta	moerature	1400°F Min. 1800°F Normal
							2000°F Max.
Water Vapo	or Content:	flue gas	eight of H2	<u>on</u> ; v	elocity: _	44	
	·	SECT	ION IV:	INCINERAT	OR INFORMA 	TION N/A	
Type of Waste							Gas (Solid By-pro
Actual lb/hr Inciner- ated							
Uncon- trolled (lbs/hr)		•					
Total Weig		ted (lbs/h					ps/hr)
Total Weig	ht Incinera	ted (lbs/h	Operation	per day			os/hr)wks/yr
Total Weig Approximat Manufactur	ht Incinera e Number of er	ted (lbs/h	Operation	per day	da	y/wk	
Total Weig Approximat Manufactur	ht Incinera e Number of er	ted (lbs/h	Operation	per day	da	y/wk	wks/yr
Total Weig Approximat Manufactur	ht Incinera e Number of er	ted (lbs/h	Operation	per day Model	da	y/wk	wks/yr
Total Weig Approximat Manufactur	ht Incinera e Number of er ructed	ted (lbs/h	Operation  Heat R	per day Model	No	y/wk	wks/yr
Total Weig Approximat Manufactur Date Const	ht Incinera e Number of er ructed hamber	ted (lbs/h	Operation  Heat R	per day Model	No	y/wk	wks/yr
Total Weig Approximat Manufactur Date Const  Primary C Secondary	ht Incinera e Number of er ructed hamber Chamber	Hours of ( Yolume (ft)3	Operation  Heat R  (BTU	Model elease	No	el BTU/hr	wks/yr
Total Weig Approximat Manufactur Date Const  Primary C Secondary Stack Heig	ht Incinera e Number of er ructed hamber Chamber	Volume (ft) 3	Heat R (BTU	Model elease /hr)	No	el BTU/hr	Temperature
Total Weig Approximat Manufactur Date Const  Primary C Secondary Stack Heig Gas Flow R:	ht Incinera e Number of er ructed hamber Chamber ht:	Volume (ft) 3	Heat R (BTU)	per day  Model  elease /hr)  ater:	No	el BTU/hr  Stack	Temperature (*F)
Total Weig Approximat Manufactur Date Const  Primary C Secondary Stack Heig Gas Flow R  *If 50 or dard cubic	ht Incinera e Number of er ructed hamber Chamber ht: ate:	Volume (ft)  ft. Ser day desires corrected	Heat R (BTU)  Stack Diag	mter:	No.  Furtype  DSCFM*  it the emistic.	Stack Velocity:	Temperature (*F)  Temp.  in grains per st

_	
r	ief description of operating characteristics of control devices:
<u> </u>	
	timate disposal of any effluent other than that emitted from the stack (scrubber water, h, etc.):
■{ _`йо; —	TE: Items 2, 3, 4, 6, 7, 8, and 10 in Section V must be included where applicable.
	SECTION V: SUPPLEMENTAL REQUIREMENTS
16	ease provide the following supplements where required for this application.
1.	Total process input rate and product weight show derivation [Rule 17-2.100(127)]
	To a construction application, attach basis of emission estimate (e.g., design calculations, design drawings, pertinent manufacturer's test data, etc.) and attach proposed methods (e.g., FR Part 60 Methods 1, 2, 3, 4, 5) to show proof of compliance with applicable standards. To an operation application, attach test results or methods used to show proof of compliance. Information provided when applying for an operation permit from a construction permit shall be indicative of the time at which the test was made.
١.	Attach basis of potential discharge (e.g., emission factor, that is, AP42 test).
4.	With construction' permit application, include design details for all air pollution control systems (e.g., for baghouse include cloth to air ratio; for scrubber include cross-section sketch, design pressure drop, etc.)
5.	With construction permit application, attach derivation of control device(s) efficiency. Include test or design data. Items 2, 3 and 5 should be consistent: actual emissions = potential (1-efficiency).
( *-	An 8 1/2" x 11" flow diagram which will, without revealing trade secrets, identify the individual operations and/or processes. Indicate where raw materials enter, where solid and liquid waste exit, where gaseous emissions and/or airborne particles are evolved and where finished products are obtained.

ER Form 17-1.202(1)

Iffective November 30, 1982

An 8 1/2" x 11" plot plan showing the location of the establishment, and points of airborne emissions, in relation to the surrounding area, residences and other permanent structures and roadways (Example: Copy of relevant portion of USGS topographic map).

An 8  $1/2^n \times 11^n$  plot plan of facility showing the location of manufacturing processes and outlets for airborne emissions. Relate all flows to the flow diagram.

ı	-	
	The appropriate application fee in accomade payable to the Department of Enviro	ordance with Rule 17~4.05. The check should be connected Regulation.
		it, attach a Certificate of Completion of Con was constructed as shown in the constructio
	SECTION VI: BEST AVA	ILABLE CONTROL TECHNOLOGY
	Are standards of performance for new stapplicable to the source?	ationary sources pursuant to 40 C.F.R. Part 6
•	[ ] Yes [ ] No	
	- Contaminant	Rate or Concentration
	N/A	·
<u> </u>		
	Has EPA declared the best available con yes, attach copy)	ntrol technology for this class of sources $\{ {f I} \}$
1	[ ] Yes [ ] No	
	Contaminant	Rate or Concentration
	N/A	
. W	that emission levels do you propose as b	est available control technology?
	Contaminant	Rate or Concentration
	N/A	
. 0	Describe the existing control and treatm	ent technology (if any). $N/A$
1	. Control Device/System:	2. Operating Principles:
3	. Efficiency:*	4. Capital Costs:
Expl	ain method of determining	
	orm 17-1.202(1) tive November 30, 1982 Page	8 of 12

·

Useful Life: Operating Costs: 7. Energy: 8. Maintenance Cost: 9. Emissions: Contaminant Rate or Concentration 10. Stack Parameters a. Height: ft. Diameter: ft. h. of. c. Flow Rate: ACFM d. Temperature: FPS e. Velocity: Describe the control and treatment technology available (As many types as applicable, use additional pages if necessary). N/Aı. Control Device: b. Operating Principles: Efficiency: 1 Capital Cost: Useful Life: Operating Cost: e. Energy: 2 g. h. Maintenance Cost: Availability of construction materials and process chemicals: Applicability to manufacturing processes: j. Ability to construct with control device, install in available space, and operate k. within proposed levels: 2. Control Device: b. Operating Principles: Efficiency:1 c. d. Capital Cost: Useful Life: Operating Cost: Energy: 2 g. h. Maintenance Cost: Availability of construction materials and process chemicals: 1Explain method of determining efficiency. <sup>2</sup>Energy to be reported in units of electrical power - KWH design rate. DER Form 17-1.202(1) Effective November 30, 1982 Page 9 of 12

Applicability to manufacturing processes: Ability to construct with control device, install in available space, and operate k. within proposed levels: 3. Control Device: Operating Principles: ь. Efficiency: 1 Capital Cost: ď. c. Useful Life: Operating Cost: e. Energy: 2 Maintenance Cost: g. Availability of construction materials and process chemicals: i. j. Applicability to manufacturing processes: Ability to construct with control device, install in available space, and operate k. within proposed levels: 4. Operating Principles: Control Device: Efficiency: 1 Capital Costs: c. Operating Cost: Useful Life: Energy: 2 h. Maintenance Cost: g. i. Availability of construction materials and process chemicals: Applicability to manufacturing processes: j. Ability to construct with control device, install in available space, and operate within proposed levels: Describe the control technology selected: Control Device: Enclosed Ground Flare 2. 98%+ -Efficiency: 1 Capital Cost: \$80.000 Useful Life: 3. 4. 30+ years-Energy: 2 N/A Operating Cost: \$5,000/year 5. 6. 7, Maintenance Cost: \$1.000/year Manufacturer: McGill Environmental Systems, 8. Inc. (or equivalent) Other locations where employed on similar processes: (1) Company: (2) Mailing Address: (4) State: (3) City: 1Explain method of determining efficiency. <sup>2</sup>Energy to be reported in units of electrical power - KWH design rate.

Page 10 of 12

DER Form 17-1.202(1)

Effective November 30, 1982

, ·							
•	(5) Environmental Manager:						
	(6) Telephone No.:						
•••	(7) Emissions: 1						
	Contaminant			Rate or	Concentrat	tion	
		<del></del>					
	(8) Process Rate: 1						
<b>-</b> r-	b. (1) Company:						
	(2) Mailing Address:						
<b>#</b> f**	(3) City:		(4) State:				
	(5) Environmental Manager:						
<b>æ</b> f	(6) Telephone No.:						
	(7) Emissions: <sup>1</sup>				•		
	Contaminant			Rate or	Concentrat	ion	
	<del></del>			<u> </u>			
-							
	(8) Process Rate: 1					1	
	10. Reason for selection and d	escription	of systems:		.•		
A	oplicant must provide this informations of the state the state the state that the state that the state the state that the state the state that the state tha	mation when e reason(s)	available.	Should	this info	)rmation no	t b
	SECTION VII - PR	EVENTION OF	SIGNIFICANT	DETERIO	PRATION N	/A ·	
Α.	Company Monitored Data						
[ .	1no. sites	TSP	()	so2+ _		Wind spd/di	. r
<b>.</b> /	Period of Monitoring		to		/ /		
					day year		
		Contaminant  Contaminant  Rate or Concentry  Process Rate:  (1) Company:  Mailing Address:  City:  Environmental Manager:  Telephone No.:  Emissions:  Contaminant  Rate or Concentry  Rate or Concentry  Process Rate:  Contaminant  Rate or Concentry  Process Rate:  Temperature of systems:  Contaminant  Rate or Concentry  Process Rate:  Temperature of systems:  Contaminant  Section VII - Prevention of systems:  Section VII - Prevention of Significant Deterioration of Significant					
, <b>+</b> Sp	ecify bubbler (B) or continuous	(c).					
	Form 17-1.202(1) ective November 30, 1982	Page 11	lof 12				

<b>a</b> .	Was instrumentation EPA referenced or its equivalent? [ ] Yes [ ] No
ь.	Was instrumentation calibrated in accordance with Department procedures?
	[] Yes [] No [] Unknown
et	eorological Data Used for Air Quality Modeling
•	Year(s) of data from / / to / / month day year month day year
•	Surface data obtained from (location)
	Upper air (mixing`height) data obtained from (location)
•	Stability wind rose (STAR) data obtained from (location)
0 10 1	puter Models Used
•	Modified? If yes, attach description.
	Modified? If yes, attach description.
	Hodified? If yes, attach description.
	Modified? If yes, attach description.
	ach copies of all final model runs showing input data, receptor locations, and prin- le output tables.
pp]	licants Maximum Allowable Emission Data_
o 1 1	lutant Emission Rate
7	rsp grams/sec
S	grams/sec
n i s	ssion Data Used in Modeling
in	, ach list of emission sources. Emission data required is source name, description of it source (on NEDS point number), UTM coordinates, stack data, allowable emissions, normal operating time.
tta	ach all other information supportive to the PSD review.
le	cuss the social and economic impact of the selected technology versus other applicatechnologies (i.e., jobs, payroll, production, taxes, energy, etc.). Include

Instrumentation, Field and Laboratory

the requested best available control technology.

Attach scientific, engineering, and technical material, reports, publications, jour-nals, and other competent relevant information describing the theory and application of

East Duval Sanitary Landfill Closure		
TO WHOM IT MAY CONCERN:  This is notification that George R. Knee	echt. Manag	er of Disposal, has the authority to
act on behalf of the City of Jacksonville appropriate and approvals for the project described.	as agent in a	applying for and obtaining site-related
It is understood that this representation time upon proper notice to the permitting		rminated by the undersigned at any
BY:	TITLE:	· .
FOR:		
STATE OF FLORIDA, COUNTY OF		· .
I, the undersigned authority, hereby certi of the instrument presented to me by as the original of such instrument.		
WITNESS my hand and official seal, this	day of	, 19
Notary Public		
My commission expires		<b>_</b> •

cla/58/016 22-092.00/3.0

PROJECT DESCRIPTION:

#### Section II A Attachment

#### NATURE AND EXTENT OF THE PROJECT

The City of Jacksonville began solid waste disposal operations at the East Duval Sanitary Landfill (the East Landfill) in November, 1974. Materials accepted at the East Landfill include Class I waste (residential, commercial, and industrial wastes) as well as Class III waste (construction and demolition debris). Less than 3,000 combined tons of both dry and wet ash from a Carbonaceous Fuel Boiler were also received from the Mayport Naval Station for disposal at the East Landfill. Additionally, a clay lined special waste pit was opened for a short time in which small quantities of special wastes were disposed of. Operations at the East Landfill are on-going and the landfill is expected to reach its capacity within 1-2 years.

The East Landfill (see Figure 1 for location) consists of approximately 136 acres with the waste disposal area occupying approximately 71 acres. The East Landfill is expected to achieve a 132' final height (this is approximately 110' above existing ground elevation).

The City of Jacksonville has committed to install an active landfill gas collection and flaring system (see Figures 2 and 3). Landfill gases will be actively withdrawn from the landfill through a system of specially designed extraction wells. Gases will be collected by producing a negative pressure in the wells with a system of blowers. The wells will be manifolded together and routed to a flare system where the gas will be burned to oxidize potential odor causing constituents and destroy the potentially explosive gases. Moisture will be removed from the collection system through a system of condensate traps located

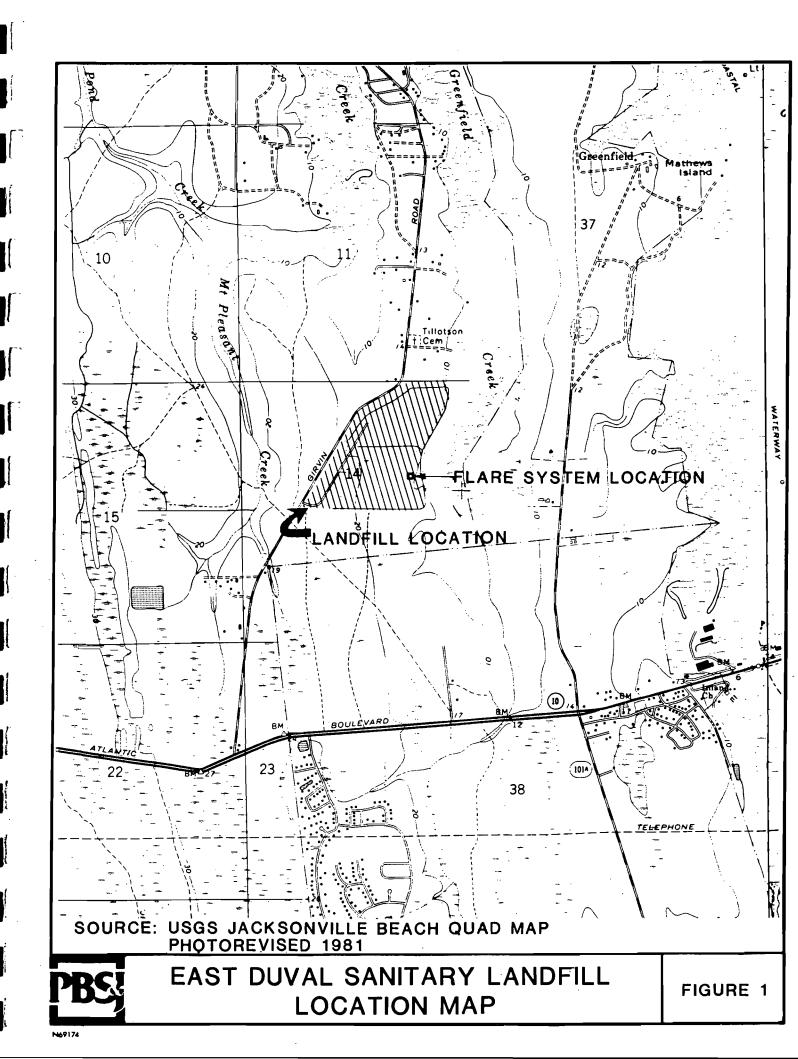
at low points of the collection pipe system and will be routed to an above ground condensate storage tank.

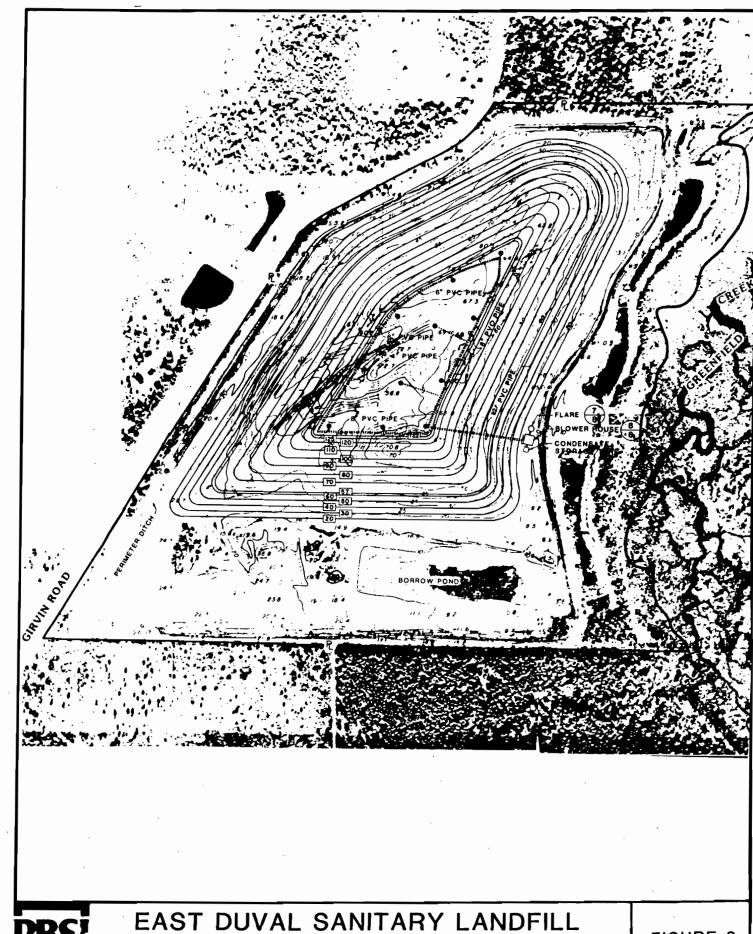
The blower system will be designed with three individual blower units connected in parallel between the well system manifold and the flare system. Two of the blower units will operate simultaneously under normal conditions, with the additional blower unit provided as stand-by for use during scheduled or unscheduled maintenance outages.

The McGill Environmental Systems, Inc. flare system (or equivalent) to be used will be an enclosed unit designed such that all combustion takes place in a refractory lined chamber. This will offer the greatest control of the combustion process, and no flame or lighting should be visible outside of the unit. A flame arrestor will be incorporated to prevent flame migration outside of the flare unit.

Sensors and alarms will be incorporated to monitor system performance. In the event of flame out or blower unit malfunction, responsible City personnel will be notified automatically, so that appropriate action will not be delayed.

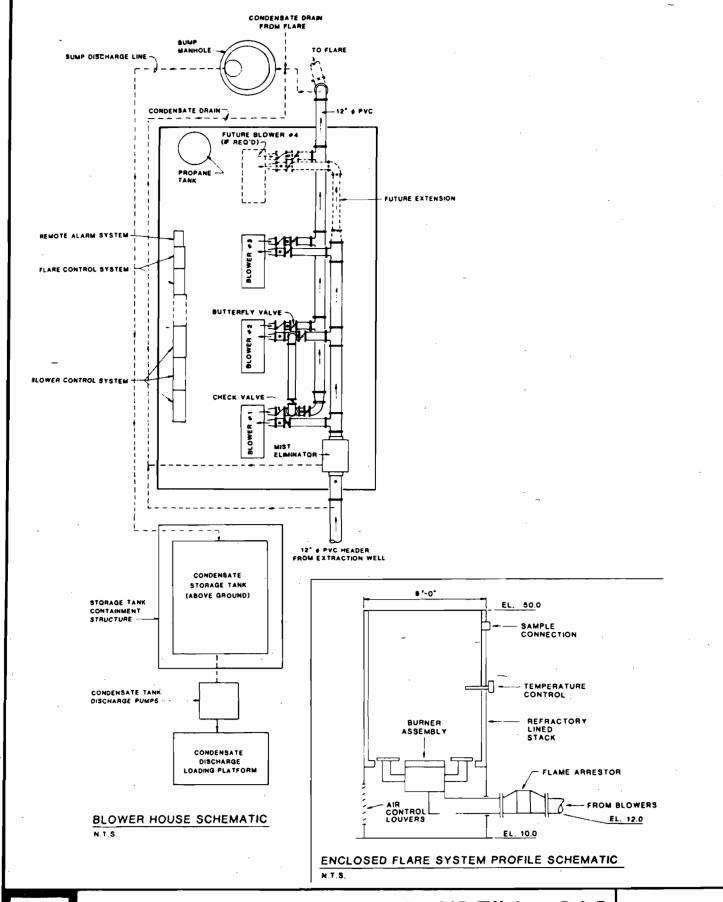
While the City of Jacksonville currently plans to burn off the landfill gases with a flare system, the City may, at a later date, elect to sell the gas. The primary consideration by the City on this alternative (and any other alternatives to flaring the gas) will be odor control.





GAS MANAGEMENT FACILITY PLOT PLAN

FIGURE 2



EAST DUVAL SANITARY LANDFILL - GAS MANAGEMENT FACILITY FLOW DIAGRAM

FIGURE 3

#### Section III C Attachment

#### AIRBORNE CONTAMINANTS EMITTED

The potential emissions of the landfill without the landfill cap (to contain the gas) and the active gas management system (to collect and burn the gas) are difficult to predict due to the varying nature and age of the garbage in the landfill. The attached landfill gas production model conservatively predicts a peak year average flow of approximately 2100 cfm. The composition of this gas can reasonably be expected to coincide with the values shown in Table 2-1, Typical Landfill Gas Composition at Various Sites. These are the potential emissions of the landfill without the landfill cap and active gas management system.

The emissions data for each contaminant in Section III C was provided by McGill Environmental Systems, Inc. based on an assumed 2100 cfm peak year average flow and an estimated 52% methane content.

KW/jdm/MISCII/018

22-092.00

East Landfill City of Jacksonville Jacksonville, Florida

LANDFILL GAS PRODUCTION MODEL BASED ON THE PALOS VERDES KINETIC MODEL VERSION 3.2 - MARCH 7, 1989

#### REFUSE QUANTITY & CHARACTERISTICS

ASSUMPTIONS: TOTAL TONS OF REFUSE REFUSE TEMPERATURE = INITIAL MOISTURE COM METHANE CONTENT = AVERAGE REFUSE THICK AVERAGE IN-PLACE DEM	: ITENT = NESS =	3,720,500 TC 85 DE 35% 52% 100 FE 1200 LE	GREES F	30.5 MET 711.7 KG/	YEA PEI ERS A	NAL MOISTURE CONTENT= ARS LANDFILL WAS OPEN RCENTAGE REDUCTION OF FTER CLOSURE =	BEFORE CLOSURE =	25% 0 13%		
REFUSE COMP	OSITION					% VOLATILE	% VOLATILE SOLIDS	METHANE GAS PER LB OF (cf-CH4	REFUSE	
DECOMPOSIBILITY CLASS	COMPONENT	•	% WET WEIGHT	% WATER	% DRY WEIGHT	SOLIDS (dry wt.)	BIODEGRAD. (dry wt.)	wet	by class	ADJUSTED FACTORS (cf-CH4/lb)
Readily	Food Waste		14%	63%	5%	60%	50%	0.131	0.131	0.146
Moderate	Garden Waste Paper Waste		12% 42%	48% 20%	6% 34%	70% 85%	35% 20%	0.129 0.481	0.610	0,679
Slowly	Plastic/Rubber Textiles Wood	٠	5% 2% 2%	13% 16% 14%	4% 2% 2%	95% 94% 85%	2% 5% 5%	0.007 0.007 0.006	0.020	0.022
Inert	Metal Glass/Ceramics Ash/Dirt/Rock		9% 11% 3%	3% 2% 8%	9% 11% 3%		:			
	TOTAL		100%		75%		Total	0.761	0.761	0.847
GAS GENERA	TION FACT	ORS				RADIUS	OF INFLUEN	CE		
DECOMPATIBILITY CLASS		READILY M	DERATELY	SLOWLY			TION RATE (r) =		cf/lb/day or	20.4 ml/kg/day or 143 cf-CH4/cy-yr
Total % Dry Weight Methane Yield Factor (cf/dry ton) Half-Life (yrs) UltLife (yrs) Lag-Time (yrs)	····	5% 5,627 2 6 0.2	40% 3,409 5 15 0.8	568 20 60 4.4		RADIUS OF INFL ROL: HORZ. RAD		200	FEET CY	143 CT-CH4/CY-YI
KINETIC FA	CTORS GEN	ERATIO	N ,			NO. OF WELLS I AVE. RECOVERY WELL FLOW RATE		11 70.07 114		53.7 L/SEC
DECOMPOSIBILITY CLASS	Assumed Half-Life (yrs)		Assumed ltLife (yrs)	k1 (yrs-1)	k2 (yrs-1)	MIN. WELL SIZE		81 = 14 8	CFM/WELL CFM/WELL INCHES INCHES	<del>-</del>
Readily	2		6	1.956	0.978		IGN RECOVERY RATE =	1,252		ELL 1.80 MMcfd Recovered
Moderate	5		15	0.782	0.391	MAXIMUM PRODUC AVERAGE PRODUC		2.846,238	CF-CH4/DAY CF-CH4/DAY OVE	D O YEADS
Slowly	20		60	0.196	0.098	AVERAGE PRODUC	III -	1,213,047	OI CITY/DAT OVE	n / ILANG

(una) Cantant Dan Vaca Dan Vaca Cartan	Time	Moisture	Moisture Content cure Factor	Methane Content		(cf-Cl	d Factors H4/lb)		(cf-	Yield Factor CH4/lb)	
0.42 33.2% 1.05 1.04 1.07   0.143 0.667 0.022 5524 3347 558	(yrs)	Content	Per Year	Per Year	Factor	Readily	Moderate	Slowly	Readily	Moderate	
0.2 34.2% 1.05 1.04 1.07   0.143 0.667 0.022 5524 3347 558   0.4 33.3% 1.051 1.054 1.07   0.140 0.654 0.021 5319 3222 537   0.6 32.5% 1.010 1.04 1.05 0.138 0.662 0.021 5319 3222 537   0.8 32.5% 1.010 1.04 1.05 0.138 0.662 0.021 5319 3222 537   1.0 31.7% 0.59 1.04 0.99 1.04 1.05 0.138 0.662 0.021 5316 3366 527   1.0 30.2% 0.99 1.04 1.09 0.132 0.627 0.620 5216 3316 527   1.2 30.2% 0.99 1.04 0.097 0.132 0.627 0.625 0.000 5407 5516 3366 527   1.2 30.2% 0.99 1.04 0.097 0.127 0.555 0.600 5407 5408 5516   1.4 22.5% 3.0 0.99 1.04 0.99 0.122 0.567 0.018 4007 5075 556   1.6 28.8% 0.991 1.04 0.93 0.122 0.567 0.018 4070 2008 2011 405   2.0 27.4% 0.887 1.04 0.991 0.110 0.555 0.018 4070 2008 477   2.0 27.4% 0.887 1.04 0.991 0.110 0.555 0.018 4090 2786 464   2.2 2.2 26.7% 0.887 1.04 0.99 0.116 0.553 0.018 4090 2786 464   2.2 2.2 25.7% 0.88 1.04 0.89 0.116 0.533 0.018 4090 2786 464   2.4 26.1 25.5 30 0.88 1.04 0.89 0.116 0.533 0.018 4090 2786 446   2.5 2.5 30 0.88 1.04 0.83 0.110 0.555 0.018 4090 2786 446   2.6 2.5 30 0.80 1.04 0.83 0.110 0.555 0.018 4090 2786 446   2.6 2.5 30 0.88 1.04 0.83 0.110 0.555 0.018 4090 2786 446   2.6 2.5 30 0.88 1.04 0.83 0.110 0.555 0.018 4090 2786 446   2.6 2.5 30 0.080 1.04 0.83 0.110 0.550 0.016 4212 2552 425   3.2 2.5 0.00 0.80 1.04 0.83 0.110 0.550 0.016 4212 2552 425   3.2 2.5 0.00 0.80 1.04 0.83 0.100 0.508 0.016 4212 2552 425   3.4 25.00 0.80 1.04 0.83 0.100 0.508 0.016 4212 2552 425   3.5 25.00 0.80 1.04 0.83 0.100 0.508 0.016 4212 2552 425   3.5 25.00 0.80 1.04 0.83 0.100 0.508 0.016 4212 2552 425   3.5 25.00 0.80 1.04 0.83 0.100 0.508 0.016 4212 2552 425   3.5 25.00 0.80 1.04 0.83 0.100 0.508 0.016 4212 2552 425   3.5 25.00 0.80 1.04 0.83 0.100 0.508 0.016 4212 2552 425   3.5 25.00 0.80 1.04 0.83 0.100 0.508 0.016 4212 2552 425   3.5 25.00 0.80 1.04 0.83 0.100 0.508 0.016 4212 2552 425   3.5 25.00 0.80 1.04 0.83 0.100 0.508 0.016 4212 2552 425   3.5 25.00 0.80 0.104 0.83 0.100 0.508 0.016 4212 2552 425   3.5 25.00 0.80 0.104 0.83 0.100 0.508 0.016 4212 2552 425   3.5 25.00 0.80 0.104 0.				1.04	1.11	0.146	0.679	0.022	5627		
0.4 33.3% 1.03 1.04 1.07   0.140 0.654 0.021 5319 3222 537   0.6 33.5% 1.09 1.04 1.05 0.138 0.642 0.021 5319 3222 537   0.8 31.7% 0.99 1.04 1.03 0.135 0.627 0.620 5216 3160 527   1.0 31.5% 0.99 1.04 1.03 0.135 0.627 0.620 5216 3160 527   1.0 31.5% 0.99 1.04 0.99 0.132 0.616 0.620 5216 3160 527   1.0 32.5% 0.99 1.04 0.99 0.132 0.616 0.620 5216 3160 527   1.1 4. 225.5% 0.99 1.04 0.99 0.132 0.616 0.620 500 500 500 500 500 500 500 1303 546   1.2 325.5% 0.99 1.04 0.99 0.122 0.520 0.520 0.00 400 400 5213 465   1.3 28.1% 0.89 1.04 0.99 0.116 0.95 0.122 0.550 0.018 4702 2248 475   2.0 27.4% 0.87 1.04 0.91 0.119 0.555 0.018 4702 2248 475   2.0 27.4% 0.87 1.04 0.91 0.119 0.555 0.018 4702 2248 475   2.0 27.4% 0.88 1.04 0.89 0.116 0.530 0.017 429 2599 433   2.2 2.2 26.7% 0.86 1.04 0.89 0.116 0.530 0.017 429 2599 433   2.8 25.0% 0.82 1.04 0.83 0.109 0.508 0.016 4212 2552 425   3.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425   3.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425   3.1 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425   3.2 2.5 0.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425   3.3 2.5 0.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425   3.4 2.5 0.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425   3.5 2.5 0.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425   3.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425   3.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425   3.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425   3.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425   3.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425   3.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425   3.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425   3.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425   3.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425   3.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425   3.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425   3.8 25.0% 0.80 0.104 0.80 0.80 0.109 0.508 0.016 4212 2552 425   3.8 25.0% 0.80 0.104 0.83 0.10					1.09						
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2.0 27.4% 0.87 1.04 0.91 0.119 0.555 0.018 4599 2786 444 2.2 26.7% 0.86 1.04 0.89 0.116 0.543 0.018 4599 2786 454 2.4 26.1% 0.84 1.04 0.87 0.114 0.530 0.017 4291 2599 433 2.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 3.0 22.0 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 3.1 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 3.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 3.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 3.5 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 3.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 3.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 3.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.5 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.5 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.5 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.5 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.5 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.5 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.5 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.5 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.5 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.5 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.5 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.5 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.5 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.5 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552					0.95	0.124	0.580		4805		485
2.2 26.7% 0.86 1.04 0.89 0.116 0.543 0.018 4406 27724 454 2.4 26.1% 0.84 1.04 0.87 0.114 0.530 0.017 4393 2662 444 2.6 25.5% 0.82 1.04 0.85 0.1111 0.518 0.017 4291 2599 433 2.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 3.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 3.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 3.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 3.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 3.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 3.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.4 2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.4 2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.4 2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.4 2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.4 2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.4 2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.5 2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.5 2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.5 2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.5 2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.5 2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.5 2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.5 2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.5 2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.5 2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.5 2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.5 2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.5 2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.5 2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 4.5 2 25.0%		.8 28.1%		1.04	0.93				4702		
2.4 26.1% 0.84 1.04 0.87 0.114 0.530 0.017 4393 2662 444 22.6 25.5% 0.80 1.04 0.85 0.111 0.518 0.017 4291 2559 433 2.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 3.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 3.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 3.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 3.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 3.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 3.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 3.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 425 425 425 425 425 425 425 4					0.91		0.555	0.018			
2.6		20.1%			0.89	0.116	0.543	0.018			
2.8		.4 20.1%	0.84		0.87	0.114	0.530	0.017	4393	2662	444
3.0		27.7%	0.02		0.65	0.111	0.518	0.01/		2599	
3.2		0 25.0%	0.00		0.63	0.109	0.508	0.016	4212	2552	425
3.4		25.0%	0.00	1.04	0.63	0.109	0.508	0.016	4212	2552 2552	425
3.6					0.63	0.109	0.508		4212	2552 2552	425
3.8					0.83	0.109			4212 4212	2002 2552	425
4.0 2 5.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 425 426 4.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 425 426 4.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 425 4.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 5.0 4.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 5.0 4.8 25.0 4.8					0.83	0.109	0.508	0.016	4212 4212	2772 2552	427
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4.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 425 4.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 5.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 5.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 5.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 5.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 5.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 5.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 5.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 6.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 6.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 6.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 6.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 6.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 6.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 6.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 6.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 6.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 6.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 6.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 7.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 7.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 7.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 7.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 7.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 7.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 7.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 7.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 7.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 7.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 7.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 7.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 7.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 7.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212			0.80		0.83	0.109	0.508		4212	2552	425 425
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5.0					0.83				4212	2552	425
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6.0	. 5			1.04	0.83	0.109	0.508		4212	2552	425
6.2					0.83	0.109	0.508		4212	2552	425
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6.8			0.80		0.83	0.109	0.508	0.016	4212	2552	425
7.0			0.80		0.83	0.109	0.508	0.016	4212	2552	425
7.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 7.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 7.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 8.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 8.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 8.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 8.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 8.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 8.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 8.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.2 25.0% 0.80 1.04 0.83 0.109 0.508		25.0%			0.83	0.109	0.508	. 0.016	4212	2552	425
7.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 7.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 7.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 8.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 8.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 8.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 8.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 8.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 8.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 8.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.2 25.0% 0.80 1.04 0.83 0.109 0.508					0.83	0.109	0.508	0.016	4212	2552	425
7.6				1.04	0.83	0.109	0.508		4212	2552	425
7.8			0.80		0.83	0.109	0.508	0.016	4212	2552	425
8.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 8.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 8.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 8.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 8.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.2 25.0% 0.80 1.04 0.83 0.10			0.80	1.04	0.83	0.109	0.508		4212	2552	425
8.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 8.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 8.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 8.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.0 25.0% 0.80 1.04 0.83 0.			0.00	1.04	0.63	0.107	0.500	0.016	4212 4212	200Z	425
8.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 8.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 8.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.5 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.4 25.0% 0.80 1.04 0.83 0		2 25.0%			7.03 7.8.0	0.109 0.100	0.508			200Z	425
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9.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.0 25.0% 0.80 1.04			0.80			0.107	0.508		4212 4212		425
9.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.4 25.0% 0.80 1.04			0.80	1.04	0.83	0.109	0.508		4212	2552	425
9.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 9.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.4 25.0% 0.80 1.0										2552	425
9.6       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425         9.8       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425         10.0       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425         10.2       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425         10.4       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425         10.6       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425         11.0       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425         11.2       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425         11.4       25.0%       0.80       1.04		.4 25.0%							4212	2552	
9.8       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425         10.0       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425         10.2       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425         10.4       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425         10.6       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425         11.0       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425         11.2       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425         11.4       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425         11.4       25.0%       0.80       1.04 <td< td=""><td>ģ</td><td>.6 25.0%</td><td>0.80</td><td>1.04</td><td>0.83</td><td>0.109</td><td>0.508</td><td>0.016</td><td>4212</td><td>2552</td><td>425</td></td<>	ģ	.6 25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
10.0       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425         10.2       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425         10.4       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425         10.6       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425         11.0       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425         11.2       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425         11.4       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425         11.4       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425					0.83		0.508		4212		425
10.2     25.0%     0.80     1.04     0.83     0.109     0.508     0.016     4212     2552     425       10.4     25.0%     0.80     1.04     0.83     0.109     0.508     0.016     4212     2552     425       10.6     25.0%     0.80     1.04     0.83     0.109     0.508     0.016     4212     2552     425       10.8     25.0%     0.80     1.04     0.83     0.109     0.508     0.016     4212     2552     425       11.0     25.0%     0.80     1.04     0.83     0.109     0.508     0.016     4212     2552     425       11.2     25.0%     0.80     1.04     0.83     0.109     0.508     0.016     4212     2552     425       11.4     25.0%     0.80     1.04     0.83     0.109     0.508     0.016     4212     2552     425		.0 25.0%	0.80	1.04	0.83	0.109	0.508		4212		425
10.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425			0.80		0.83	0.109	0.508		4212	2552	425
10.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 10.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.0 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.2 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.4 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425					0.83	0.109	0.508		4212	2552	425
10.8       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425         11.0       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425         11.2       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425         11.4       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425         11.6       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425         11.8       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425			0.80		0.83	0.109			4212	2552	425
11.0       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425         11.2       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425         11.4       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425         11.6       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425         11.8       25.0%       0.80       1.04       0.83       0.109       0.508       0.016       4212       2552       425			0.80	1.04	0.83		0.508		4212	2552	425
11.2     25.0%     0.80     1.04     0.83     0.109     0.508     0.016     4212     2552     425       11.4     25.0%     0.80     1.04     0.83     0.109     0.508     0.016     4212     2552     425       11.6     25.0%     0.80     1.04     0.83     0.109     0.508     0.016     4212     2552     425       11.8     25.0%     0.80     1.04     0.83     0.109     0.508     0.016     4212     2552     425	11	.0 25.0%	0.80	1.04	0.83	0.109	0.508		4212	2552	425
11.4     25.0%     0.80     1.04     0.83     0.109     0.508     0.016     4212     2552     425       11.6     25.0%     0.80     1.04     0.83     0.109     0.508     0.016     4212     2552     425       11.8     25.0%     0.80     1.04     0.83     0.109     0.508     0.016     4212     2552     425	11	.2 25.0%	0.80	1.04	0.83	0.109	0.508		4212	2552	425
11.6 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425 11.8 25.0% 0.80 1.04 0.83 0.109 0.508 0.016 4212 2552 425			0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
1.04 0.83 0.109 0.508 0.016 4212 2552 425 0.109 0.508 0.016 4212 2552 425			0.80		0.83	0.109	0.508	0.016	4212	2552	425
	11	.8 25.0%	. 0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425

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	05 00									
12.0	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
12.2	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
12.4	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
12.6	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
12.8	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
13.0	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
13.2	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
13.4	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
13.6	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
13.8	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
14.0	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
14.2	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
14.4	25.0% 25.0%	0.80 0.80	1.04 1.04	0.83 0.83	0.109	0.508	0.016	4212	2552 2552	425
14.6 14.8	25.0%	0.80	1.04	0.83	0.109 0.109	0.508	0.016	4212 4212	2002 2002	425
15.0	25.0%	0.80	1.04	0.83	0.109	0.508 0.508	0.016 0.016	4212 4212	2552 2552	425
15.2	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425 425
15.4	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
15.6	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425 425
15.8	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425 425
16.0	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
16.2	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425 425 425
16.4	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
16.6	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
16.8	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
17.0	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
17.2	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
17.4	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
17.6	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
17.8	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
18.0	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
18.2	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
18.4	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
18.6	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
18.8	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
19.0	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
19.2	25.0%	0.80 0.80	1.04	0.83 0.83	0.109	0.508	0.016	4212 (212	2552	425 425
19.4	25.0% 25.0%	0.80	1.04 1.04	0.83	0.109 0.109	0.508 0.508	0.016	4212 4212	2552 2552	425 425
19.6 19.8	25.0%	0.80	1.04	0.83	0.109	0.508	0.016 0.016	4212	2552	425
20.0	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
20.2	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
20.4	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
20.6	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
20.8	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
21.0	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
21.2	25.0%	0.80	1.04	0.83	0.109	0.508.	0.016	4212	2552	425
21.4	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
21.6	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
21.8	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
22.0	25.0%	0.80	1.04	0.83	. 0.109	0.508	0.016	4212	2552	425
22.2	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
22.4	25.0%	0.80	1.04	0.83 0.83	0.109	0.508 0.508	0.016	4212	2552	425 425
22.6	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
22.8	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
23.0	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
23.2 23.4	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552 2552	425 425 425 425 425 425 425 425 425
25.4	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212 4212	2052	425
23.6 23.8	25.0%	0.80	1.04	0.83 0.83	0.109	0.508	0.016	4212 (212	2552	425
۵.8	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212 4213	2552	442
24.0	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212 4212	2552	425
24.2	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212 4212	2552 2552	427 725
24.4	25.0%	0.80 <b>0.8</b> 0	1.04 1.04	0.83 0.83	0.109 0.109	0.508 0.508	0.016 0.016	4212 4212		427 425
24.6 24.8	25.0% 25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212 4212	2552 2552	425 425 425
24.0 25.0	25.0%	0.80	1.04	0.83	0.109	0.508	0.016	4212	2552	425
23.0	27.0%	0.00	1.04	0.00	0.107	0.500	0.010	7212	2002	763

	Tima			y - CH4 Production		4 Production	Slowly - CH4		Total - CH4	
==:	Time (yrs) =========	Content		um cf	cf	cum cf	######################################	cum cf	cf	cum cf
	0.0	35.0%	0	0 :	. 0	0	0	0	0	0
	0.2	34.2%		96,978	8,402,652	8,402,652	64,151	64,151	13,563, <i>7</i> 81	13563781
	0.4	33.3%		93,924	9,643,127	18,045,779	65,469	129,619	17,105,542	30669323
	0.6	32.5%		24,820	11,062,753	29,108,532	66,790	196,409	21,860,438	52529761
	0.8	31.7%	15,561,708 38,78		12,686,630	41,795,162	68,112	264,521	28,316,450	80846211
	1.0	31.0%	22,558,479 61,34		14,543,222	56,338,384	69,434	333,955	37, 171, 135	118017346
	1.2	30.2% 29.5%	32,687,885 94,03		16,664,774	73,003,158	70,752	404,707	49,423,411	167440757
	1.4 1.6	28.8%	47,345,747 141,37 68,546,384 209,97		19,087,779 21,853,488	92,090,937 113,944,425	72,065 73,371	476,772 550,143	66,505,592 90,473,243	233946349 324419592
	1.8	28.1%	99,194,888 309,11	19.012			74,665	624,808	124,278,034	448697626
	2.0	27.4%	95,742,655 404,86			167,558,187	75,947	700,755	124,423,884	573121510
	2.2	26.7%	76,973,296 481,83		32,703,042	200,261,229	77,212	777,967	109,753,549	682875059
	2.4	26.1%	61,851,132 543,68	86,995	37,368,272	237,629,501	78,456	856,423	99,297,861	782172919
	2.6	25.5%	49,672,661 593,35	59,657	42,675,645	280,305,146	79,678	936,101	92,427,983	874600903
	2.8	25.0%	40,098,917 633,45	58,574	48,989,455	329,294,601	81,337	1,017,438	89,169,710	963770613
	3.0	25.0%	32,974,950 666,43			386,582,304	84,582	1,102,020	90,347,235	1054117848
	3.2	25.0%	27,116,626 693,55			453,573,882	87,957	1,189,977	94, 196, 161	1148314009
	3.4	25.0%	22,299,090 715,84			531,913,060	91,466	1,281,443	100,729,734	1249043743
	3.6 3.8	25.0%	18,337,437 734,18		107,126,425	623,521,990	95,115	1,376,557	110,041,482	1359085225
	4.0	25.0% 25.0%	15,079,611 749,20 12,400,570 761,60		125,272,404	855 020 810	98,909 102,856	1,475,467 1,578, <b>3</b> 22	122,304,945 137,775,829	1481390170 1619166000
	4.2	25.0%	10,197,487 771,8			*****	106,959	1,685,281	156,796,548	1775962547
	4.4	25.0%	8,385,803 780,25	50,148	171.306.172	*****	111,226	1,796,508	179,803,201	1955765749
	4.6	25.0%	6,895,982 787,14	46,130	200.323.459	*****	115,664	1,912,171	207,335,105	2163100854
	4.8	25.0%	5,670,843 792,8	16,974	234,255,940	*****	120,278	2,032,449	240,047,061	2403147915
	5.0	25.0%	4,663,362 797,48	80,336	273,936,190	****	125,077	2,157,526	278,724,629	2681872544
	5.2	25.0%	3,834,870 801,3	15,206	142,323,587	*****	130,067	2,287,593	146,288,523	2828161067
	5.4	25.0%	3,153,568 804,46		151,612,605	******	135,256	2,422,848	134,901,427	2963062494
	5.6 5.8	25.0% 25.0%	2,593,305 807,00 2,132,579 809,19		121,707,707	*****	140,652 146,263	2,563,500	124,441,664	3087504158 3003331333
	6.0	25.0%	1,753,705 810,9		104 078 082	*****	152,098	2,709,763 2,861,862	114,827,075 105,983,886	3202331233 3308315119
	6.2	25.0%	1,442,142 812,39		96 245 377	*****	158,166	3,020,028	97,845,686	3406160805
	6.4	25.0%	1,185,932 813,5		89,002,146	*****	164,477	3,184,505	90,352,554	3496513360
	6.6	25.0%	975,239 814,59		82 304 026	*****	171,038	3,355,543	83,450,304	3579963663
	6.8	25.0%	801,978 815,3		76, 109, 993	*****	177,862	3,533,405	77,089,833	3657053496
	7.0	25.0%	659,499 816,0	13,154	70.382.110	*****	184,958	3,718,363	71,226,567	3728280063
	7.2	25.0%	542,333 816,5	55,486	65,085,295	****	192,337	3,910,700	65,819,965	3794100028
	7.4	25.0%	445,982 817,0	01,468	60,187,108	****	200,010	4,110,711	60,833,101	3854933128
	7.6	25.0%	366,749 817,36	68,217	55,657,549	****	207,990	4,318,701	56,232,288	3911165416
	7.8	25.0%	301,592 817,6		21,400,0/2 /7 505 /33	*****	216,288	4,534,989	51,986,755	3963152172 4011220577
	8.0 8.2	25.0% 25.0%	248,011 817,9 203,950 818,1		47,575,433 44,013,407	*****	224,917 233,890	4,759,905 4,993,795	48,068,361 44,451,337	4011220533 4055671869
	8.4	25.0%	167,716 818,2		40 701 131	*****	243,221	5,237,016	41,112,068	4096783938
	8.6	25.0%	137,920 818,4		37.638.047	*****	252,924	5,489,941	38,028,891	4134812829
	8.8	25.0%	113,417 818,5		34,805,484	*****	263,015	5,752,956	35, 181, 916	4169994745
	9.0	25.0%	93,267 818,6		32, 186, 094	*****	273,508	6,026,464	32,552,870	4202547614
	9.2	25.0%	76,697 818,7		29.763.834	*****	284,420	6,310,884	30,124,952	4232672566
	9.4	25.0%	63,071 818,7		27,523,869	*****	295,767	6,606,650	27,882,707	4260555273
	9.6	25.0%	51,866 818,8	25,725	25,452,478	*****	307,567	6,914,217	25,811,911	4286367184
	9.8	25.0%	42,652 818,8	68,376	23,536,977	*****	319,837	7,234,054	23,899,466	4310266650
	10.0	25.0%	35,074 818,9		21,765,632	*****	332,597	7,566,652	22,133,303	4332399953
	10.2	25.0%	28,843 818,9		20, 127,090	****	345,866 750,445	7,912,518 8,272,183	20,502,304	4352902257 4371898473
	10.4	25.0% 25.0%	23,719 818,9 19,505 818,9		17 212 060	*****	359,665 374,014	8,646,197	18,996,216 17,605,588	4389504061
	10.6 10.8	25.0%	16,040 818,9		15 916 724	*****	388,935	9,035,132	16,321,699	4405825760
	11.0	25.0%	13,190 819,0		14.718.863	*****	404,452	9,439,585	15,136,506	4420962265
	11.2	25.0%	10,847 819,0		13.611.152	*****	420,588	9,860,173	14,042,586	4435004852
	11.4	25.0%	8,920 819,0		12.586.804	*****	437,368	10,297,540	13,033,091	4448037943
	11.6	25.0%	7,335 819,0	31,848	11 639 547	*****	454,817	10.752.357	12,101,699	4460139642
	11.8	25.0%	6,032 819,0	37,879	10 763 578	*****	472,962	11,225,319	11,242,572	4471382214
	12.0	25.0%	4,960 819,0	42,840	9,953,533	*****	491,831	11,717,149	10,450,324	4481832538

42.2	35 00	/ 070 040 0// 040	0.00/ /5/ **********	F44 455 40 000 400	<b>4 -4</b>
12.2	25.0%	4,079 819,046,919	9,204,451 ********	511,453 12,228,602	9,719,982 4491552520
12.4	25.0%	3,354 819,050,273	8,511,743 ********	531,857 12,760,459	9,046,954 4500599474
12.6	25.0%	2,758 819,053,031	7,871,166 ********	553,076 13,313,535	8,427,000 4509026475
		2,268 819,055,300	7,278,798 ********		7 05/ 000 450/020475
12.8	25.0%		1,210,190	575,141 13,888,676	7,856,208 4516882683
13.0	25.0%	1,865 819,057,165	6,731,011 ********	598,087 14,486,763	7,330,963 4524213645
13.2	25.0%	1,534 819,058,699	6.224.448 *********	621,948 15,108,711	6,847,930 4531061576
13.4	25.0%		5,756,009 ********		
		1,261 819,059,960	5,730,009 **********************************	646,761 15,755,472	6,404,031 4537465607
13.6	25.0%	1,037 819,060,998	5,322,824 ********	672,564 16,428,035	5,996,424 4543462031
13.8	25.0%	853 819,061,851	4,922,239 *******	699,396 17,127,431	5,622,488 4549084519
14.0	25.0%		4,551,801 *******		E 370 004 /EE/7//730
		701 819,062,552	4,331,001	727,299 17,854,729	5,279,801 4554364320
14.2	25.0%	577 819,063,129	4,209,242 *********	756,314 18,611,044	4,966,133 4559330453
14.4	25.0%	474 819,063,603	3,892,463 *******	786,488 19,397,532	4,679,425 4564009878
14.6	25.0%	390 819,063,994	3,599,524 ********	817,865 20,215,397	4,417,779 4568427658
			3,328,631 *******		
14.8	25,0%	321 819,064,314	3,320,031	850,494 21,065,892	4,179,446 4572607104
15.0	25.0%	264 819,064,578	3,078,125 *********	884,425 21,950,317	<b>3,962,814</b> 4576569919
15.2	25.0%	217 819,064,795	2,846,472 ********	919,710 22,870,027	3,766,399 4580336317
	25.0%		2,632,252 ******		7 500 077 /507005450
15.4		178 819,064,973	2,002,202	956,402 23,826,429	3,588,833 4583925150
15.6	25.0%	147 819,065,120	2,434,154 *********	994,558 24,820,988	3,428,859 4587354009
15.8	25.0%	121 819,065,241	2,250,965 *******	1,034,237 25,855,225	3,285,322 4590639331
16.0	25.0%	99 819,065,340	2,081,562 ******	1,075,498 26,930,723	3,157,159 4593796490
			1 02/ 000 *******		7,171,177 4773170470
16.2	25.0%	82 819,065,422	1,924,908 *********	1,118,406 28,049,129	3,043,395 4596839885
16.4	25.0%	67 819,065,489	1,780,043 *********	1,163,025 29,212,154	2,943,135 4599783020
16.6	25.0%	55 819,065,544	1,646,081 ********	1,209,425 30,421,578	2,855,560 4602638581
16.8	25.0%	45 819,065,589	1,522,200 ******		
			1,522,200		2,779,920 4605418501
17.0	25.0%	37 819,065,627	1,407,642 ********	1,307,851 32,987,104	2,715,530 4608134032
17.2	25.0%	31 819,065,657	1,301,706 *********	1,360,028 34,347,132	2,661,765 4610795796
17.4	25.0%	25 819,065,682	1,203,742 ******	1,414,287 35,761,420	2,618,055 4613413851
			1,113,151 ********		
17.6	25.0%	21 819,065,703	1,113,131	1,470,711 37,232,130	2,583,883 4615997733
17.8	25.0%	17 819,065,720	1,029,378 ********	1,529,386 38,761,516	2,558,780 4618556514
18.0	25.0%	14 819,065,734	951,909 ********	1,590,401 40,351,917	2,542,324 4621098838
18.2	25.0%	12 819,065,746	880,270 *******	1,653,851 42,005,768	2,534,133 4623632970
			04/ 037 *****		
18.4	25.0%	9 819,065,755	814,023 *********	1,719,832 43,725,601	2,533,864 4626166834
18.6	25.0%	8 819,065,763	752,761 *********	1,788,446 45,514,047	2,541,215 4628708049
18.8	25.0%	6 819,065,770	696,110 ********	1,859,797 47,373,843	2,555,913 4631263962
			643,722 *******		
19.0	25.0%	5 819,065,775	043,722	1,933,994 49,307,838	2,577,722 4633841684
19.2	25.0%	4 819,065,779	595,277 ********	2,011,152 51,318,990	2,606,433 4636448117
19.4	25.0%	4 819,065,783	550,477 ********	2,091,388 53,410,378	2,641,869 4639089985
	25.0%	3 819,065,786	509,050 *******	2,174,825 55,585,203	2,683,877 4641773863
19.6			470,740 ********		
19.8	25.0%	2 819,065,788	470,740	2,261,591 57,846,793	2,732,333 4644506195
20.0	25.0%	2 819,065, <i>7</i> 90	435,313 *********	1,210,864 59,057,657	1,646,178 4646152374
20.2	25.0%	2 819,065,792	402,552 ********	1,187,409 60,245,066	1,589,963 4647742336
20.4	25.0%	1 819,065,793	372,257 ********		1,536,667 4649279003
			344,241 *******	1,164,409 61,409,475	
20.6	25.0%	1 819,065,794	344,241	1,141,854 62,551,329	1,486,097 4650765100
20.8	25.0%	1 819,065,795	318,334 ********	1,119,736 63,671,065	1,438,072 4652203172
21.0	25.0%	1 819,065,796	294,377 *********	1,098,047 64,769,113	1,392,425 4653595597
			272,223 *******		
21.2	25.0%	1 819,065,796	251,736 ********	1,076,778 65,845,890	1,349,001 4654944598
21.4	25.0%	1 819,065,797	201,/30 *********	1,055,921 66,901,811	1,307,657 4656252255
21.6	25.0%	0 819,065,797	232,791 *********	1,035,467 67,937,278	1,268,259 4657520514
21.8	25.0%	0 819,065,798	215,272 *********	1,015,410 68,952,689	1,230,682 4658751196
			199,071 ********	005 7/3 40 0/9 /30	1 10/ 017 //500/ 4000
22.0	25.0%	0 819,065,798	ו יועי וויייייייייייייייייייייייייייייי	995,742 69,948,430	1,194,813 4659946009
22.2	25.0%	0 819,065,798	184,089 ********	976,454 70,924,885	1,160,543 4661106552
22.4	25.0%	0 819,065,798	170,235 *********	957,540 71,882,425	1,127,775 4662234328
			157,423 ********		
22.6	25.0%	0 819,065,798	131,463	938,993 72,821,417	1,096,416 4663330744
22.8	25.0%	0 819,065,799	145,576 *********	920,804 73,742,222	1,066,380 4664397124
23.0	25.0%	0 819,065,799	134 620 ********	902,968 74,645,190	1,037,589 4665434713
			124,489 ********	885 478 75 530 447	1 000 067 /444///470
23.2	25.0%	0 819,065,799	145 400 444444444	885,478 75,530,667	1,009,967 4666444679
23.4	25.0%	0 819,065,799	115,120 ********	868,326 76,398,993	983,446 4667428125
23.6	25.0%	0 819,065,799	106.456 ********	851,506 77,250,500	957,963 4668386088
23.8	25.0%	0 819,065,799	98,445 *******	835,013 78,085,512	933,457 4669319546
		0 017,003,177	04 024 +++++++++		
24.0	25.0%	0 819,065,799	91,036 *********	818,838 78,904,351	909,874 4670229420
24.2	25.0%	0 819,065,799	84,185 *******	802,977 79,707,328	887,162 4671116583
24.4	25.0%	0 819,065,799	77 849 *********	787,424 80,494,752	865,273 4671981856
			71,990 *******	772,171 81,266,923	844,162 4672826018
24.6	25.0%	0 819,065,799	66,573 *******	712,111 01,200,723	977 707 11771100010
24.8	25.0%	0 819,065,799	00,3/3	757,214 82,024,138	823,787 4673649805
25.0	25.0%	0 819,065,799	61,563 *******	742,547 82,766,685	804,110 4674453914
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MAXIMUM PRODUCTION =
AVERAGE PRODUCTION =
MAX. YEARLY MOVING AVERAGE =

2,846,238 CF/DAY 1,215,647 CF/DAY IN 9 YEARS 2,867,334 CF/DAY

Time (yrs)	Readily (cf)	Moderate (cf)	Slowly (cf)	Total (cf) Annual Total
0.0		. 0	0	0
0.2		0	0	0 .
0.6		ŭ	0	5,096,978
0.8	10,730,896	ň	<b>0</b> <b>0</b>	7,396,946
1.0	15,561,708	8,402,652	ŏ	7,396,946 10,730,896 23,964,360 47,189,180 9,437,836
1.2	2 22,558,479	9,643,127	Ö	32,201,606 15,878,157
1.4	32,687,885	11,062,753	. 0	43,750,638 23,608,889
1.6		12,686,630	0	60.032.377 34.135.975
1.8 2.0	68,546,384 99,194,888	14,543,222	0	85,089,606 48,607,717
2.2	95,742,655	16,664,774 19,087,779	0 0	115,859,662 334,933,889 66,986,778
2.4	76,973,296	21,853,488	Ŏ	114,830,434 83,512,544
2.6	61,851,132	25,008,481	ŏ	98,826,784 94,527,773 86,859,613 99,893,220
2.8	3 49,672,661	28,605,282	· · · Ö	78,277,943 98,930,887
3.0	40,098,917	32,703,042	0	72.801.959 451.596.733 90.319.347
3.2		37,368,272	Ö	70,343,222 81,421,904 69,792,270 75,615,001
3.4 3.6		42,675,645 48,989,455	0	69,792,270 75,615,001
3.8	18,337,437	46,969,433 57,287,703	0 0	71,288,545 72,500,788 75,625,141 71,970,227
4.0		66,991,578	ŏ	75,625,141 71,970,227 82,071,190 369,120,368 73,824,074
4.2	2 12,400,570	78,339,178	Ŏ	82,071,190 369,120,368 73,824,074 90,739,748 77,903,379
4.4		91,608,930	Ö	101,806,417 84,306,208
4.6		107, 126, 425	64,151	115,576,378 93,163,775
4.8		125,272,404	65,469	132,233,855 104,485,517
5.0 5.2		146,492,102	66,790	152,229,735 592,586,133 118,517,227
5.4	2 4,663,362 3,834,870	171,306,172 200,323,459	68,112	176,037,646 135,576,806 204,227,763 156,061,076
5.6		234,255,940	69,434	204,227,763 156,061,076
5.8	2,593,305	273,936,190	70,752 72,065	237,480,259 180,441,852 276,601,561 209,315,393
6.0	2,132,579	142,323,587	73.371	144,529,537 1038876766 207,775,353
6.2	2 1,753,705	131,612,603	74,665	133,440,974 199,256,019
6.4		121,707,707	75.947 ·	123 225 796 183 055 625
6.6 6.8		112,548,233	77,212	113,811,376 158,321,849
7.0		104,078,082 96,245,377	78,456 79,678	105, 131, 777 124, 027, 892
7.2	659,499	89,002,146	77,070 81 337	97,127,033 572,736,957 114,547,391 89,742,983 105,807,793
7.4	542,333	82,304,026	81,337 84,582	89,742,983 105,807,793 82,930,941 97,748,822
7.6		76, 109, 993	87,957	76,643,931 90,315,333
7.8	366,749	70,382,110	91,466	70,840,324 83,457,042
8.0		65,085,295	95,115	65,482,002 385,640,181 77,128,036
8.2	248,011	60,187,108	98,909	60,534,029 71,286,246
8.4 8.6		55,657,549 51,468,875	102,856 106,959	55,964,355 65,892,928
8.8		47,595,433	111,226	51,743,550 60,912,852 47,844,579 56,313,703
9.0		44,013,497	115,664	47,844,579 56,313,703 44,242,578 260,329,091 52,065,818
9.2	93,267	40,701,131	120,278	40,914,676 48,141,948
9.4	76,697	37,638,047	125,077	37,839,821 44,517,041
9.6		34,805,484	130,067	34,998,622 41,168,055
9.8 10.0		32,186,094 20,747,877	135,256	32,373,216 38,073,783
10.0		29,763,834 27,523,869	140,652 146,263	29,947,138 176,073,473 35,214,695
10.4		25,452,478	152,098	27,705,206 32,572,801 25,633,620 30,131,530
10.6		23,536,977	158, 166	25,633,420 30,131,520 23,718,862 27,875,568
10.8	3 19,505	21,765,632	164,477	21.949.613 25.790.848
11.0	16,040	20,127,595	171,038	20,314,673 119,321,773 23,864,355

11.2	13, 190	19 412 977	177.0/2	40.007.007	
11.4	10,847	18,612,833 17,212,069	177,862 184,958	18,803,885 17,407,874 16,117,980	22,084,090
11.6	8,920	15,916,724	192,337	17,407,074 14,117,000	20,438,981
11.8	7,335	15,916,724 14,718,863	200 010	16,117,960	17 51/ 12/
12.0	6,032	17 411 152	207,990	13,825,174 81,081,121	18,918,805 17,514,124 16,216,224
12.2	4,960	12,586,804	216,288	12.808.052	15,017,058
12.4	4,079	12,586,804 11,639,547 10,763,578 9,953,533	224,917	14,926,209 13,825,174 81,081,121 12,808,052 11,868,543 11,000,823 10,199,513	13,909,192
12.6	3,354	10,763,578	233 800	11,000,823	12,885,760
12.8	2,758	9,953,533	243,221 252,924 263,015 273,508	10, 199, 513	13,909,192 12,885,760 11,940,421
13.0 13.2	2,268 1,865	9,204,451	252,924	9,409,044 00,000,074	11,067,315 10,261,029
13.4	1,534	8,511,743 7,871,166	263,015	8,776,623	10,261,029
13.6	1,261	7,278,798	273,308	8,146,208 7,564,479	9,516,562
13.8	1,037	6,731,011	284,420 295,767 307,567 319,837 332,597	7,027,815	8,829,293 8,194,954
14.0	853	6.224.448	307.567	6,532,868 38,047,994	0,194,934 7,600,500
14.2	701	5,756,009	319.837	6,532,868 38,047,994 6,076,548	7,609,599 7,069,584
14.4	577	6,224,448 5,756,009 5,322,824	332,597	5,655,998	6,571,542
14.6	474	4,922,239	343.866	5,268,580	6,112,362
14.8	390	4,551,801	359,665 374,014	4,911,856	5,689,170
15.0 15.2	321 367	4,209,242	374,014	4,583,577 26,496,558	6,112,362 5,689,170 5,299,312
15.4	264 217	3,892,463	388,935	4,281,662	4.940.334
15.6	178	3,599,524 3,328,631	404,452 420,588	4,004,193	4,609,973
15.8	147	3,078,125	437,368	3,749,398	4,306,137
16.0	121	2,846,472	454,817	3,515,639 3,301,409 18,852,301	4,020,094 3,770,740
16.2	99	2.632.252	472,962	3,105,313	3,770,400
16.4	82	2,434,154 2,250,965	491,831	2,926,066	3,319,565
16.6	67	2,250,965	491,831 511,453	2,762,484	3,122,182
16.8	55	2,081,562	531.857	2,762,484 2,613,474	2,941,749
17.0	45 37	1,924,908	553,076 575,141	2,478,029	4,026,894 3,770,460 3,535,190 3,319,565 3,122,182 2,941,749 2,777,073
17.2 17.4	37 31	1,780,043	575,141	2,355,221	2,627,055 2,490,681
17.6	25	1,646,081 1,522,200	598,087 621,948	2,244,198	2,490,681
17.8	21	1,407,642	646,761	2,144,173 2,054,424	2, <b>3</b> 67,019 2,255,209
18.0	21 17	1,301,706	672,564	1,974,286	2,154,460
18.2	14	1,203,742	699,396	1,903,152	2,064,047
18.4	12	1,113,151	699,396 727,299	1.840.461	1,983,299
18.6	9	1,029,378	756,314	1,840,461 1,785,701	1,911,605
18.8	8	951,909	786,488	1,738,404	1.848.401
19.0	6	880,270	817,865	1,698,142	1,793,172
19.2 19.4	<b>)</b>	814,023 752,761	850,494	1,664,522	1,745,446
19.6		696,110	884,425 919,710	1,637,191	1,704,792
19.8	3	643,722	956,402	1,615,823 1,600,127	1,670,816
20.0	. 2	595,277	994,558	1,589,838	1,643,161 1,621,500
20.2	2	550,477	1,034,237	1,584,716	1,605,539
20.4	2	509,050	1,075,498	1,584,549	1,605,539 1,595,011
20.6	1	470,740	1,118,406	1,589,147	1,589,675
20.8	1	435,313	1,163,025	1,598,339	1,589,318
21.0	1	402,552	1,209,425	1,611,977	1,593,746
21.2 21.4	<b>.</b>	372,257 7/4, 2/1	1,257,675	1,629,933	1,602,789
21.6	i	344,241 318,334	1,307,851	1,652,093	1,616,298
21.8	Ò	294,377	1,360,028 1,414,287	1,678,363 1,708,445	1,634,141 1,656,206
22.0	Ŏ	272,223	1,470,711	1 7/2 93/4	1,020,200
22.0 22.2	. 0	294,377 272,223 251,736	1,470,711 1,529,386	1,708,665 1,742,934 1,781,122 1,823,192 1,869,123 1,918,903	1,682,398 1,712,635
22.4	<u> </u>	232,791 215,272	1,590,401 1,653,851	1,823,192	1,746.855
22.6	0	215,272	1,653,851	1,869,123	1,746,855 1,785,007 1,827,055 1,872,975
22.8	0	199,071	1,719,832	1,918,903	1,827,055
23.0 23.2	0	184,089 170,235	1,788,446 1,859,797	1,972,535 2,030,032 2,091,418	1,872,975
23.4	0	170,235	1,009,797	2,050,032	1,922,757 1,976,402
23.6	ŏ	145,576	1,933,994 2,011,152	2,091,418 2,156,728	1,9/6,402
23.6 23.8	, ŏ	134,620	2,091,388	2,136,726	2,033,923
24.0	Ŏ	124,489	2,174,825	2,299,314	2,095,344 2,160,700
24.2	0	115,120	2,261,591	2,376,711	2,230,036
			•		

24.4	· n	106,456	1,210,864	1,317,320	2,075,216
24.4	0	98,445	1,187,409	1,285,854	1,901,041
24.6	, <b>u</b>		1,164,409	1,255,445	1,706,929
24.8	0	91,036		1,226,039	1,492,274
25.0	0	84,185	1,141,854	1,220,037	1,472,214

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Table 2-1

TYPICAL LANDFILL GAS COMPOSITION AT VARIOUS SITES (Component Percentage, Dry Volume Basis)

Compounds	Blanchet 1977	Ham et al 1977	Bray 1981	Cagliostro 1981	Elzy 1 <b>9</b> 83
Methane	44.0	47.5	50.0	53.4	50.0
Carbon Dioxide	34.2	47.0	35.0	34.3	42.5
Nitrogen _	20.8	3.7	13.0	6.2	5.4
Oxygen	1.0	8.0	1.7	0.05	0.2
Paraffin Hydrocarbons	· •	0.1	-	0.17	-
Aromatic and Cyclic Hydrocarbons	-	0.2	-	-	-
Hydrogen	•	0.1	-	0.005	1.9
Hydrogen Sulfide	0.7	0.01	0.3	0.005	-
Carbon Monoxide	-	0.1	-	0.005	<b>.</b> -
Trace Compounds	-	0.5	-	<b>-</b>	-

<sup>\*</sup>Trace compounds include: sulfur dioxide, benzene, toluene, methylene chloride, perchlorethylene, carbonyl sulfide, and vinyl chloride.

SOURCE: Final Report (August-July 1985); Landfill Gas: Resource Evaluation and Development - Gas Research Institute.

Response to FDER Comments
Dated October 2, 1990
Regarding the City of Jacksonville
East Duval Sanitary Landfill
Application to Construct Air
Pollution Source
(Landfill Gas Flare)
Application No. AC 16-186047





December 21, 1990

Mr. C.H. Fancy, P.E. Chief, Bureau of Air Regulation Florida Department of Environmental Regulation 2600 Blair Stone Road Tallahassee, Florida 32399

Re: Response to Request for Additional Information
East Duval Sanitary Landfill Flare
Construction Permit Application No. AC 16-186047

Dear Mr. Fancy:

Enclosed are responses to your letter of October 2, 1990 regarding the above referenced permit application.

For ease of review we have included your statement (in bold type) followed by our response. If you have any questions or need additional information, please contact me.

Very truly yours,

PBS&J ENVIRONMENTAL LABORATORIES

Jerome J. Guidry, P.E. Vice President

JJG/jdm/MISC II 044

Encs.

cc: G. Knecht, City of Jacksonville G. Threlkeld, PBS&J

22-087.00

## EAST DUVAL SANITARY LANDFILL FLARE RESPONSE TO REQUEST FOR ADDITIONAL INFORMATION

The following are responses to Mr. C. H. Fancy's request for additional information dated October 2, 1990 (included in Attachment 1) regarding the East Duval Sanitary Landfill Application to construct Air Pollution source (Landfill Gas Flare), Application No. AC 16-186047.

1. Complete Item B(1), Section III of the permit application (tons/day of Class I & III wastes this facility is designed to handle).

The East Duval Sanitary Landfill is currently accepting approximately 1,200 tons per day of municipal solid waste. There will not be any material accepted once the facility is closed, in which time the flare will be constructed. The landfill is expected to reach its capacity within 1 to 2 years. Upon closure, the landfill will contain approximately 6,207,000 cubic yards of municipal solid waste.

2. Submit a calculation sheet for Item C, Section III, for all contaminants which must include H<sub>2</sub>S emissions, along with Item H, Section III calculations.

Section III, Item C has been revised, and is included in Attachment 2. The estimated component qualities and stack information were provided by IT-McGill, a flare manufacturer. Any background data can be obtained by contacting Mr. Kyle Schotts at (918) 748-0700.

3. The control device, according to Item D, Section III of the application is McGill Environmental Systems, Inc., Model EGF-60 Flare (or equivalent). When do you expect to finalize the type and model of flare that will be installed. Please submit a manufacturer's brochure including the design specification sheet.

The type and model of flare will be finalized during the award of bid to perform the landfill closure construction. This will enable the City of Jacksonville to obtain the most cost effective flare unit. A copy of the manufacturers brochure including the design specification sheet is included in Attachment 3.

4. Is this flare steam-assisted or air-assisted? What is the net heating value of the gas being combusted?

The flare is neither steam nor air-assisted; it is a totally natural draft system. The net heating value of the gas being combusted ranges from 300 BTU/SCF to 520 BTU/SCF.

5. How is the presence of the flare pilot flame, exit gas temperature and gas flow rate monitored?

The flare pilot flame is sensed with a UV flame detector. The exit gas temperature is monitored with a thermocouple. The exit gas flow rate is not measured.

6. According to Section II "A" Attachment, the East Landfill is expected to achieve a final height of 132 feet while the flare stack height is only 40 feet. Do you plan to install the flare stack at the highest elevation at the landfill?

The top of the stack will not be installed at the highest elevation at the landfill. The flare will be installed on the east side of the landfill. The final elevation of the landfill is expected to be 132 feet National Geodetic Vertical Datum (NGVD), and the top of the stack is anticipated to be at elevation 51 NGVD. 7. Submit a process flow diagram showing the location of all extraction wells in the collection system along with gas flow rates (ACFM) for each well that will be routed to the flare.

A process flow diagram and a collection system layout with the location of all extraction wells in the collection system is shown in Attachment 4. The gas flow was estimated to be 150 CFM for each well.

# ATTACHMENT 1 FDER REQUEST FOR ADDITIONAL INFORMATION

#### **BEST AVAILABLE COPY**



## Florida Department of Environmental Regulation

Twin Towers Office Bldg. ● 2600 Blair Stone Road ● Tallahassee, Florida 32399-2400

Bob Martinez, Governor

Dale Twachtmann, Secretary

John Shearer, Assistant Secretary

October 2, 1990

#### CERTIFIED MAIL - RETURN RECEIPT REQUESTED

Mr. George R. Knecht, P.E. Manager of Disposal City of Jacksonville Solid Waste Disposal Division 1931 East Beaver Street Jacksonville, Florida 32202

Re: Duval County - A.P.

City of Jacksonville, East Duval

Sanitary Landfill-Flare

AC 16-186047

Dear Mr. Knecht:

The Department has received a permit application to construct a flare at the above referenced facility on September 4, 1990 and deemed it incomplete. Please provide the following information:

- Complete Item B(1), Section III of the permit application (tons/day of Class I & III wastes this facility is designed to handle).
- 2. Submit a calculation sheet for Item C, Section III, for all contaminants which must include  $\rm H_2S$  emissions, along with item H, Section III calculations.
- 3. The control device, according to Item D, Section III of the application is McGill Environmental Systems, Inc. Model EGF-60 Flare (or equivalent). When do you expect to finalize the type and model of flare that will be installed. Please submit a manufacturer's brochure including the design specification sheet.
- 4. Is this flare steam-assisted or air-assisted? What is the net heating value of the gas being combusted?
- 5. How is the presence of the flare pilot flame, exit gas temperature and gas flow rate monitored?

Mr. George R. Knecht October 2, 1990 Page 2

- 6. According to Section II "A" Attachment, the East Landfill is expected to achieve a final height of 132 feet while the flare stack height is only 40 feet. Do you plan to install the flare stack at the highest elevation at the landfill?
- 7. Submit a process flow diagram showing the location of all extraction wells in the collection system along with gas flow rates (ACFM) for each well that will be routed to the flare.

Processing of this application will continue as soon as the above referenced information has been received.

If you have any questions, please contact Mr. Mirza P. Baig at (904) 488-1344.

Sincerely,

C. H. Fancy, P.E.

Bours D. Klin

Chief

Bureau of Air Regulation

CHF/MB/plm

c: J. J. Guidry, P.E.

R. Roberson, BESD

A. Kutyna, Northeast District

### ATTACHMENT 2

PAGE 4 OF 12 OF AIR POLLUTION SOURCE PERMIT Revised December, 1990

#### SECTION III: AIR POLLUTION SOURCES & CONTROL DEVICES (Other than Incinerators)

Raw Materials and Chemicals Used in your Process, if applicable:

	Contaminants Utilization			
Description	Type	% Wt	Rate - lbs/hr	Relate to Flow Diagram
	· .			

8.	Process	Rate.	i f	applicable:	(See	Section V	_	Item	1)	
••		nate,	1,	abbtrcante:	(366	38CCTON A	•	Trem .	. ,	

Product Weight (lbs/hr):

1.	Total Process Input Rate (lbs/hr):	N/A	
2.	Product Weight (lbs/hr):	N/A	

Airborne Contaminants Emitted: (Information in this table must be submitted for each emission point, use additional sheets as necessary)

Name of	Emission		Emission <sup>1</sup>		Allowed <sup>2</sup> Emission Rate per	Allowable <sup>3</sup> Emission	Potential <sup>4</sup> Emission	Relate to Flow
Contaminant	Maximum lbs/hr	Actual T/yr	Rule 17-2	lbs/hr	lbs/yr T/yr	Diagram		
N2	88,168	386,176			See Section			
O2	15,632,	68.468			III C Attachment			
CO2	14,621	64,040				<u> </u>		
H20 CH4	7,188 55.4	31,483 242.7		•				
CO NOX	23.84 5.36	104.42	.					

 $^{\mathrm{H2S}}$  1See Section V, Item 2.

<sup>2</sup>Reference applicable emission standards and units (e.g. Rule 17-2.600(5)(b)2. Table II, E. (1) - 0.1 pounds per million BTU heat input)

Calculated from operating rate and applicable standard.

0.057

 $^4$ Emission, if source operated without control (See Section V, Item 3).

DER Form 17-1.202(1) Effective November 30, 1982

# ATTACHMENT 3. MANUFACTURER'S DESIGN SPECIFICATIONS

#### SECTION ONE - PROCESS SUMMARY

#### DESIGN BASIS

Gas Composition (Vol. %)

CH4 52% max. CO2, Air, Inerts 48%

100%

LHV 473 Btu/SCF

Temperature 100°F (45 - 120°F)

Mole Weight 29.46

Flare Gas

Type: Landfill Gas Max. Flow Rate: 2100 scfm

Waste Heat Release: 59.6 MMBtu/hr (Design Basis)

Min. Flow Rate: 10% of max. flow

Smokeless Flow: 100% Pressure Drop: 12" WG

Unit Design

Operating Temp: 1600 - 2000°F (2100°F shutdown)

Retention Time: 1600°F .66 Seconds 1800°F .69 Seconds

1800°F .69 Seconds 2000°F .72 Seconds

2000 1 172 0000100

Overall Unit Turndown: 6:1 (to hold 2000°F)

Flame Stability Turndown: 20:1 minimum

Fired Fuel Req'd: None (pilot only)

UTILITIES

Pilot Gas 22 SCFH propane (intermittent)

Compressed Air Not required

Electricity 460V/3Ph/60 Hz (McGill will step down to 110V

for control usage.)

#### MECHANICAL DESIGN

Design Wind Speed Ambient Temp Electrical Area 90 mph -20 to 120°F Non-hazardous

#### FLAME STABILITY

Low methane concentrations may require auxiliary fuel to initiate combustion and maintain temperature.

Flashback will not occur if the landfill gas 02 level is 6% or less.

#### SECTION TWO - EQUIPMENT DESCRIPTION

#### ITEM I - ENCLOSED FLARE SYSTEM

#### A. Enclosed Flare Stack

One McGill Landfill Gas Flare System, with:

- .. 2" layer A.P. Green (or equal) ceramic fiber refractory on Incomel pins and keepers. (2600°F hot face refractory).
- .. A-36 carbon steel shell (1/4" nom.).
- .. Stainless steel gas burner(s) with flame stabilizers for high temperature corrosion resistance.
- .. 12" flanged flare gas inlet.
- .. One (1) pilot assembly designed for 60,000 Btu/hr propane with electric spark ignitor. The pilot only operates during start-up.
- .. Heavy duty, galvanized, opposed blade combustion air dampers. Opposed blade design provides a 6:1 air turndown control. Galvanized finish and stainless steel press-fit bearings ensure smooth, long term operation.
- .. Four 3" NPT sample ports at 90° located 1/2 diameter from the top for accurate emission testing.
- .. Inorganic zinc primer coat for superior corrosion protection and 600°F temperature resistance.
- .. Continuous base plate for high wind stability.
- .. Lift lugs to assist in erection.

#### B. Control System Operation

The following is a brief outline of the control system start-up and operating sequence:

System start-up would begin with a timed air purge cycle to evacuate any fugitive hydrocarbons from the flare enclosure. After purge is completed, the pilot will be lit. Upon proving the pilot flame by the flame scanner, the landfill gas valve will be opened and the landfill gas blower (by others) will be started allowing landfill gas to flow to the flare enclosure. This allows use of the landfill gas for system warm-up.

Upon proving a flame on the pilot, the system will continue its warm-up sequence. The landfill gas valve will be opened allowing normal operation of the unit.

After the landfill gas valve has been opened, the pilot gas will then shut off to limit propane gas usage. If a flame is still sensed on the main burner the system will continue operation, if not it will shutdown on flame failure.

The unit temperature is set by adjusting the air dampers (manually or optional automatic). Opening the dampers will reduce the flue gas temperature by adding quench air. In the manual system, the operating temperature is set at 1800-2000°F at the maximum design flow and will fluctuate between 600-2100°F at variable gas flows.

Due to the presence of an open flame, the ground flare should be located in a "non-hazardous" electrical area.

#### C. Base Case Control Features - Manual Operation

- Manually operated combustion air dampers to control the operating temperature.
- High temperature shutdown switch with panel mounted temperature indicator.
- Pilot gas control system including pressure regulator, fail-closed shutdown valves, manual block valve and pressure indicator.
- Ignition system including ignition transformer, pilot spark electrode and ignition timer.
- Flame safeguard controls including self-checking flame scanner and panel mounted flame relay.
- Purge air blower with pressure proved switch and motor starter.
- All high voltage (440/220V) items are enclosed in a separate panel for electrical safety including:

Main power supply disconnect.

Power transformer. Client will supply 220-460V/3Ph/60 Hz electricity. McGill will stepdown to 110V/1 Ph for use as required.

Motor starter for client's landfill gas blower motor. (Client to specify horsepower).

Amp meter for waste gas blower motor (200% scale).

- "Manual-Off-Auto" blower selector switch.
- The following indicating lights:
  - a. Panel Power ON

  - b. Purging
  - c. Purge Complete
  - d. Pilot Gas ON

- e. Flame Proved
- f. High Stack Temperature (SD)
- Flame Failure (SD) g

- .. Contacts for control room monitoring of the system.
- .. 15A convenience outlet (duplex) with weatherproof cover.
- .. 100W high pressure sodium security light with manual switch and photocell (shipped loose).
- .. Additional relays, timers, controllers, etc. required for system operation.
- .. The appropriate items will be enclosed in a weatherproof (NEMA 4) panel.
- .. Controls and valving are prepiped and wired onto a support rack.

The control system will be given a functional test simulating actual operation in our shop to ensure that it is properly wired and will perform as designed.

Units can be operated in the manual mode which requires an operator at the flare to start and restart the system using a pushbutton sequence. If the units shutdown for any reason, operator assisted restart is required.

The flare operating temperature is set by manually adjusting the air dampers.

The base case is recommended for sites with stable gas flow and constant electrical supply.

#### OPTION I: AUTOMATIC START/RESTART

In the automatic mode, the unit will automatically start when power is applied. If the unit shuts down for any reason except high stack temperature, the automode will allow the unit to attempt to purge and restart for a specified time period. A remote signal is sent if the unit fails to restart.

#### OPTION II: INLET FLAME ARRESTOR

Varec 12" flame arrestor (or equal). Aluminum housing and aluminum internals. Internal elements can be cleaned without removing the flame arrestor body from the pipe.

#### OPTION III: INLET BLOCK VALVE WITH PNEUMATIC ACTUATOR

12" Pliaxseal high performance butterfly valve, ANSI 150# with carbon steel body, 316 stainless steel disk, PTFE seal with Bettis pneumatic, fail-closed actuator, 3-way solenoid valve, speed control valves and Bettis Auxiliary switches. (Nitrogen bottles supplied by others).

Although nitrogen cylinders are required to be installed, the advantage of this option is that the actuator is a highly reliable standard industrial actuator that will have less maintenance than an electric fail—closed actuator.

#### OPTION V: AUTOMATIC TEMPERATURE CONTROL (AIR)

Flue gas temperature would be automatically controlled by adjusting the air flow into the unit. Lower waste gas flows or lower methane concentrations would automatically close the inlet air louvers. The control loop consists of a thermocouple and temperature indicator/controller and two electric operated actuators on the air louvers.

#### OTHER ENCLOSED FLARE OPTIONS

McGill will design the Enclosed Flare system to meet most requirements or restrictions that our client's may have. Following are a number of optional features provided on previous projects:

- .. Temperature recorder for the flue gas. May be required for some local authorities.
- .. Landfill gas blower with explosion-proof motor (Arrq. 8).
- .. Caged access ladder to 30' elevation for access to thermocouples and flame scanner.
- .. 360° platform for access to sample connections. McGill does not recommend this option due to the proximity to the hot exit flue gas.
- .. Hinged manway (18") for access into the flare base. Normal access is through the air dampers, however, this option should be considered if automatic louvers are used.
- .. Incomel mesh cover for the ceramic fiber refractory. The mesh provides additional mechanical strength. If the unit is not used for extended periods, the mesh will extend the refractory life.
- .. Visual alarm beacon or audible alarm horn.
- .. Automatic telephone dialing system (requires phone line at flare).
- .. Finish coat of high temperature paint (aluminum color).
- .. Service agreement for a McGill technician to periodically check the operating characteristics and safety shutdown points.

#### Safety Controls and Other Features

We are providing "self-checking" type flame scanners and relay system, which affords a fail-safe shutdown. Without this feature an unsafe failure mode may occur. A normal scanner may be substituted at a substantial cost deduct, but all liability resulting from such a change must be borne by the purchaser.

#### Heat Tracing

It is not necessary to heat trace the piping between the blower and the flare.

#### McGILL FLARE MANUFACTURING STANDARDS

Following is a summary of our fabrication standards as they apply to the supply of this equipment.

The McGill shop is qualified to meet ASME boiler and pressure vessel codes and maintains quality control documentation and welder's qualifications which are available for our client's review. Inspectors have access to our company and subcontractors upon short notice.

McGill regularly uses local subcontract shops to assist in fabrication and assembly of our products. These shops work under McGill direction and project management and will meet our fabrication quality control standards.

#### 1. General Industry Standards

Welding - Gas Piping: ASME IX Electrical Wiring: NEC

> Burners: AWS 150 lb. ANSI Pipe Flanges:

Structural: AWS Pipe Threads: NPT

Weld Inspection: ASME V AISC A58.1 Structural Design:

Drawing Dimensions: English

#### 2. Nondestructive Testing

Dimensional Check: All exterior and mounting dimensions

X All Welds: 100% Visual Inspection

X Ignition Transformers: Functional Check

Control System: Function Check

#### 3. Quality Control Documentation

Welder Qualifications (on request)

X Welding Procedures (on request)

 $\overline{\mathbf{x}}$ Instrument Data Sheet/Catalog Sheet

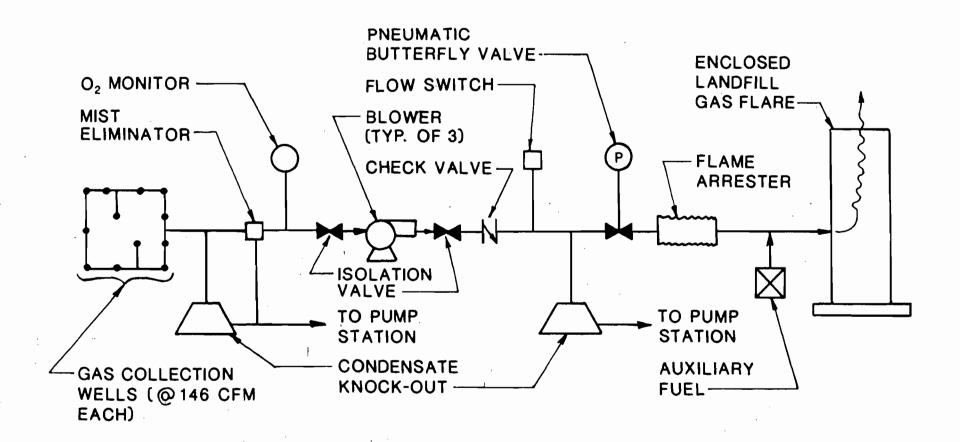
Other Standard McGill Inspection Reports

 $\overline{\mathbf{X}}$ Review Drawings (1R/3P)

 $\overline{\mathbf{x}}$ As Built Drawings (1R/3P)

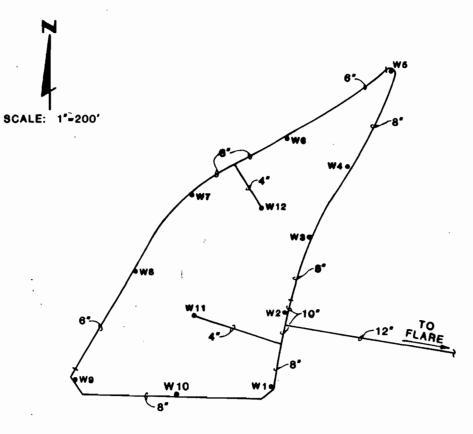
Operating & Maintenance Manual (3)

# ATTACHMENT 4 GAS MANAGEMENT SYSTEM PLANS





EAST DUVAL LANDFILL GAS FLARE PROCESS FLOW DIAGRAM



EAST LANDFILL
GAS COLLECTION PIPE LAYOUT

**ASSUMPTIONS** 

Maximum Allowable Velocity (V): 40
Maximum Gas Generation Rate per Well: 150
Perimeter Header Pipe Length: 3,300

40 FT/SEC 150 CFM 3,300 LF

50/50 Split in Flow Rate Half-Way Around Perimeter Header System

CALCULATIONS

Cross Sectional Area (A) of 12" Pipe: 0.785 SF
Cross Sectional Area (A) of 10" Pipe: 0.545 SF
Cross Sectional Area (A) of 8" Pipe: 0.349 SF
Cross Sectional Area (A) of 6" Pipe: 0.196 SF
Cross Sectional Area (A) of 4" Pipe: 0.087 SF

Pipe Section		Diameter	Flow (Q=VA)
From	To	(Inches)	(CFM)
W12	W12's Node	4	150
W12's Node	<b>W</b> 6	6	150
<b>W</b> 6	₩5	. 6	300
<b>W</b> 6	₩5	8	300
<b>W</b> 5	W4	8	450
W4	W3	8	600
<b>W</b> 3	i W2	8	750
W3	W2	10	750
W2	Exit Pipe	10	900
			•
<b>W</b> 7	w8	6	150
W8	₩9	6	300
W8	. <b>W</b> 9	8	300
. <b>W</b> 9	W10 .	. 8	450
W10	W1	8	600
W1	W11's Node	8	750
W11	W11's Node	4	150
W11's Node	Exit Pipe	10	900

Total Flow to Gas Flare (12" Exit Pipe) = 900 + 900 = 1,800 CFM Check: 12 x 150 = 1,800 CFM



EAST DUVAL SANITARY LANDFILL EXTRACTION WELL LOCATIONS AND GAS FLOW RATES

## CITY OF JACKSONVILLE EAST DUVAL LANDFILL LFG AND FLARE SYSTEM DESIGN MEMORANDUM

Post, Buckley, Schuh & Jernigan, Inc.
Prepared by Omar E. Smith

August 23, 1988
Revised: August 29, 1990
Revised for Final Design: September 27, 1990

#### 1. Design Considerations

- O Assume: Horizontal radius of influence (R.O.I.)/landfill depth ratio =
  - For Top of Landfill: 1.75/1For Sideslopes : 2/1
- O Assume: Bottom 10' ft. of LF assumed minimal LFG production
  Bottom EL of LF = 10' MSL

LFG production from top of fill to EL 20' MSL

Landfill Depth (for gas collection)

Side slopes @ EL 70': 70' - 20' = 50' Top @ EL 120': 120' - 20' = 100' For Top of Landfill:

Assume perforations = Side slope = 1/2 D = 1/2 ( 50) = 25' from bottom

Top = 2/3 D = 2/3 (100) = 67' from bottom

Radius of Influence (R.O.I)

R.O.I.: Side slopes @ 2:1 D = 50; R.O.I. = 100 (conservative)

Top @ 1.75:1 D= 100; R.O.I. = 175 (conservative)

Palm Beach County R.O.I has demonstrated 5:1.

Well Spacing

For side slopes - For R.O.I. = 100; spacing = 200

For top - For R.O.I. = 175;

Spacing = R.O.I.  $\times$  COS (30)  $\times$  2 = 300 feet

#### 2. LFG Generation/Recovery Rate

From LFG Model (see attached sheets) = 275 cf - LFG/cy - yr (Ave. Peak) Volume of Influence =  $2/3 \mu \text{ R}^2\text{H}$ For depth @ 50'; R.O.I. = 100; V = 38,800 cy @ 100'; R.O.I. = 175; V = 237,700 cy

Assume Recovery Rate Factor = 0.70 or 0.7 (Generation rate) V

From LFG Model (See attached Sheets)
:Top of LF = Each well will deliver: 87 cfm
:Side Slopes = Each well will deliver: 14 cfm

Preliminary Design of layout demonstrated:

Side slopes: 27 wells required Top: 12 wells required

#### Average Design

27 wells @ 14 cfm = 384 cfm 12 wells @ 87 cfm = 1045 cfm 1429 cfm or approximately 2.06 mmcfd

#### Peak Design

27 wells @ 24 cfm = 642 cfm 12 wells @ 146 cfm = 1748 cfm 2,390 cfm or approximately 3.44 mmcfd

#### 3. Recommendations

- System design for odor and LFG migration control.
- Use PVC pipe and fittings. (Schedule 80) for well head and well collection piping.
- Use HDPE piping for collection and header lines.
- Minimum header size = 4 inches Ø
- Locate all piping underground, atop landfill.
- Pipe slopes
   3% minimum in direction of LFG flow
   4% minimum in direction opposite of LFG flow
- Condensate traps at all low points
- Flexible connectors at all high and low points.
- Maximum velocity in header = 40 ft/s.

- Minimum pipeline cover:
  - Pipelines to be installed prior to installation of liners.
  - o 12 inches intermediate cover (under future liner).
  - o Plus 24 inches of final cover.
  - <sup>o</sup> Mark pipeline to prevent damage during placement of lines and final cover.
  - Maximum desired pipeline depth (below future liner) = 6 feet.
- Minimum well head pressure = 10 inches of H<sub>2</sub>O.
- Manhole and condensate trap covers if used to be rated for H-15 loading.
- Since 12 wells on top of fill collect > 70% (1045 cfm/1429 cfm) of LFG and well installation cost increases doubles with installation of 27 additional wells on side slopes then do not install side slopes wells at this time. Top of landfill vents should collect gas and cause a negative pressure inside the landfill since landfill has liner on sides and top.

#### Additional reasons include:

- O Difficulty in installing the pipe and wells on a side slopes (approximately 3:1).
- Possible additional differential settlement compared to the flat surface of the LF.
- Possible flooding of manholes and condensate traps if installed on side slopes.
- Significantly more piping and wells required (3 times more piping for < 30% additional LFG recovery).</li>
- o Higher unit cost for installation.
- If odor problems or migration of LFG persists then installation of collection field, and additional wells can be instituted in a Phase II construction scenario.
- Design collection piping and flare system for additional flow.
- Blower system

= 1,200 cfm = Required 2 units @ 600 cfm plus 1 standby plus 1 future for Phase II

Assume vacuum of 40 inches water column

for a total of 3 units.

- Flare system design for min. peak 2 @ 2,400 cfm (future with Phase II)

peak 1 @ 1,000 cfm (Phase I)

ave @ 1,200 cfm low @ 600 cfm

- To fully optimize the system; an actual extraction testing system should be used to verify the assumptions made in this analysis.

East Landfill City of Jacksonville Jacksonville, Florida \* SIDESLOPE OF LANDFILL \*

15.2 METERS

711.7 KG/CH

LANDFILL GAS PRODUCTION MODEL BASED ON THE PALOS VERDES KINETIC MODEL VERSION 3.2 - MARCH 7, 1989

#### REFUSE QUANTITY & CHARACTERISTICS

ASSUMPTIONS:	
TOTAL TONS OF REFUSE IN-	PLACE=
REFUSE TEMPERATURE =	
INITIAL MOISTURE CONTENT	=
METHANE CONTENT =	
AVERAGE REFUSE THICKNESS	=
AVERAGE IN-PLACE DENSITY	=

3,720,500 TONS 85 DEGREES F 35% 52%

50 FEET OR

1200 LB/CY OR

FINAL MOISTURE CONTENT=
YEARS LANDFILL WAS OPEN BEFORE CLOSURE =
PERCENTAGE REDUCTION OF MOISTURE PER YEAR
AFTER CLOSURE =

25%

13%

REFUSE COM	POSITION	% WET		% DRY	X VOLATILE SOLIDS	% VOLATILE SOLIDS BIODEGRAD.	METHANE GAS PER LB OF (cf-ch4	REFUSE	AD HISTED FACTORS
DECOMPOSIBILITY CLASS	COMPONENT	WEIGHT	% WATER	WEIGHT	(dry wt.)	(dry wt.)	wet	by class	ADJUSTED FACTORS (cf-CH4/lb)
Readily	Food Waste	14%	63%	5%	60%	50%	0.131	0.131	0.146
Moderate	Garden Waste Paper Waste	12% 42%	48% 20%	6% 34%	70% 85%	35% 20%	0.129 0.481	0.610	0.679
Slowly	Plastic/Rubber Textiles Wood	5% 2% 2%	13% 16% 14%	4% 2% 2%	95% 94% 85%	2% 5% 5%	0.007 0.007 0.006	0.020	0.022
inert	Metal Glass/Ceramics Ash/Dirt/Rock	9% 11% 3%	3% 2% 8%	9% 11% 3%	:	:			
	TOTAL	100%		75%		Total	0.761	0.761	0.847

#### GAS GENERATION FACTORS

DECOMPATIBILITY CLASS	READILY MO	DERATELY	SLOWLY
Total % Dry Weight	5%	40%	8%
Methane Yield Factor (cf/dry ton) Half-Life (yrs)	5,627 2	3,409 5	<b>568</b> 20
UltLife (yrs) Lag-Time (yrs)	0.2	15 0.8	60 4.4

#### KINETIC FACTORS GENERATION

DECOMPOSIBILITY CLASS	Assumed Half-Life (yrs)	Assumed UltLife (yrs)	k1 (yrs-1)	k2 (yrs-1)
Readily	2	6	1.956	0.978
Moderate	5	15	0.782	0.391
Slowly	20	60	0.196	0.098

#### RADIUS OF INFLUENCE

METHANE PRODUCTION RATE (r) =		cf/lb/day or	20.4 ml/kg/day or
(Note: r designed at a peak = 2 x	average)		143 cf-CH4/cy-yr
RADIUS OF INFLUENCE (ROI) ASSUMED=	100	FEET	
ROI: HORZ. RADIUS/LF DEPTH RATIO =	2		
RADIUS OF INFLUENCE THEORETICAL=	68	FEET	
VOLUME OF INFLUENCE =	38,804		
DESIGN FACTORS			
DESIGN PACTORS			
NO. OF WELLS IN RECOVERY FIELD=	27		

DESIGN FACTORS		
NO. OF WELLS IN RECOVERY FIELD=	27	
AVE. RECOVERY RATE =	70.0%	
WELL FLOW RATE (LFG) =	14 CFM OR	6.7 L/SEC
MAX. WITHDRAWAL RATE =	24 CFM/WELL	
AVE. WITHDRAWAL RATE =	10 CFM/WELL	
MIN. WELL SIZE FOR PASSIVE VENTS =	5 INCHES	
MIN. WELL SIZE FOR ACTIVE VENTS =	3 INCHES	
WELL SPACING=	200 FEET WELL TO WELL	
LFG SYSTEM DESIGN RECOVERY RATE =	384 CFM	0.55 MMcfd Recovered
LFG SYSTEM MAXIMUM RECOVERY RATE =	642 CFM	
MAXIMUM PRODUCTION =	2,846,238 CF-CH4/DAY	
AVERAGE PRODUCTION =	1,215,647 CF-CH4/DAY OVER 9	YEARS
	• •	

#### **BEST AVAILABLE COPY**

East Landfill Dity of Jacksonville Dacksonville, Florida

TOP OF LANDFILL

TOP OF LANDFILL

LANDFILL GAS PRODUCTION MODEL BASED ON THE PALOS VERDES KINETIC MODEL VERSION 3.2 - MARCH 7, 1989

#### REFUSE QUANTITY & CHARACTERISTICS

ASSUMPTIONS:			
TOTAL TONS OF REFUSE IN-PLACE=	3,720,500 TONS		
REFUSE TEMPERATURE =	85 DEGREES F		FINAL MOISTURE CONTENT=
INITIAL MOISTURE CONTENT =	35%		YEARS LANDFILL WAS OPEN BEFORE CLOSURE =
METHANE CONTENT =	52%		PERCENTAGE REDUCTION OF MOISTURE PER YEAR
AVERAGE REFUSE THICKNESS =	100 FEET OR	30.5 METERS	AFTER CLOSURE =
AVERAGE IN-PLACE DENSITY =	1200 LB/CY OR	711.7 KG/CM	

REFUSE COMPOSITION					% VOLATILE	X VOLATILE SOLIDS	METHANE GAS F PER LB OF (cf-ch4)	REFUSE	
DECOMPOSIBILITY CLASS	COMPONENT	% WET WEIGHT	% WATER	% DRY WEIGHT	SOLIDS (dry wt.)	BIODEGRAD. (dry wt.)	wet	by class	ADJUSTED FACTORS (cf-CH4/lb)
Readily	Food Waste	14%	63%	5%	60%	50%	0.131	0.131	0.146
Moderate	Garden Waste Paper Waste	12% 42%	48% 20%	6% 34%	70% 85%	35% 20%	0.129 0.481	0.610	0.679
Slowly	Plastic/Rubber Textiles Wood	5% 2% 2%	13X 16X 14X	4% 2% 2%	95% 94% 85%	2% 5% 5%	0.007 0.007 0.006	0.020	0.022
Inert	Metal Glass/Ceramics Ash/Dirt/Rock	9% 11% 3%	3% 2% 8%	9% 11% 3%	: :	:			
	TOTAL	100%		75%		Total	0.761	0.761	0.847

#### GAS GENERATION FACTORS

DECOMPATIBILITY CLASS	READILY MO	DERATELY	SLOWLY
Total % Dry Weight	5%	40%	8%
Methane Yield Factor (cf/dry ton) Half-Life (yrs)	5,627 2	3,409 5	- <b>568</b> 20
UltLife (yrs) Lag-Time (yrs)	6 0.2	15 0.8	60 + 4.4

#### KINETIC FACTORS GENERATION

DECOMPOSIBILITY CLASS	Assumed Half-Life (yrs)	Assumed UltLife (yrs)	k1 (yrs-1)	k2 (yrs-1)	
Readily	2	6	1.956	0.978	
Moderate	5	15	0.782	0.391	
Slowly	20	60	0.196	0.098	

#### RADIUS OF INFLUENCE

METHANE PRODUCTION RATE (r) =	0.0003 cf/lb/day o	20 / ml /kg/dm/ as
(Note: r designed at a peak = 2 x		r 20.4 ml/kg/day or 143 cf-CH4/cy-yr
(Note: r designed at a peak = 2 x		143 CT-UNA/CY-YT
RADIUS OF INFLUENCE (ROI) ASSUMED=	175 FEET	
ROI: HORZ. RADIUS/LF DEPTH RATIO =	1.75	
RADIUS OF INFLUENCE THEORETICAL=	119 FEET	
VOLUME OF INFLUENCE =	237,677 CY	
DESIGN FACTORS		

25% 0

13%

	NO. OF WELLS IN RECOVERY FIELD=	12	
	AVE. RECOVERY RATE =	70.0%	
	WELL FLOW RATE (LFG) =	87 CFM OR	41.1 L/SEC
	MAX. WITHDRAWAL RATE =	146 CFM/WELL	7111 2,020
	AVE. WITHDRAWAL RATE =	62 CFM/WELL	
	MIN. WELL SIZE FOR PASSIVE VENTS =	12 INCHES	
	MIN. WELL SIZE FOR ACTIVE VENTS =	7 INCHES	
	WELL SPACING=	303 FEET WELL TO WELL	
	LFG SYSTEM DESIGN RECOVERY RATE =	1,045 CFM	1.51 MMcfd Recovered
	LFG SYSTEM MAXIMUM RECOVERY RATE =	1,748 CFM	
	MAXIMUM PRODUCTION =	2,846,238 CF-CH4/DAY	
•	AVERAGE PRODUCTION =	1,215,647 CF-CH4/DAY OVER 9	YEARS
		* *	

27-Sep-90

### ENCLOSED FLARE SYSTEM CLIENT LIST

	Job No.	Client	Landfill	Location	Dia./Ht.	Inlet
٠						
	120343	Environ. Tech.	Shoosmith Bros.	Chester, VA	2 x 7	
	120348	WMI	Central Disposal	Pompano Bch, FL	$11 \times 40$	12
	120369	WMI	Oakland Scavenger	Livermore, CA	9 x 35	12
	120370	WMI	Oakland Scavenger	Fremont, CA	7 x 35	12
	120372	Emcon	De Paoli Equip.	Livermore, CA	7 × 35	10
	120373	Emcon	Ox Mountain	San Mateo, CA	6 x 35	8
	120374	Emcon	Hillside	Colma, CA	5 x 35	8
	120376	WMI	ELDA	Cincinnati, OH	$9 \times 40$	12
	120379	Emcon	Marsh Road	Menlo Park, CA	4 x 35	8
	120385	WMI	Oakland Scavenger	Livermore, CA	9 x 40	12
	120394	CID	Settlers Hill	Illinois	$8 \times 40$	10
	120396	Emcon	Leichner Bros.	Vancouver, WA	$5 \times 35$	8
	120402	Emcon	Junipero Serra	Colma, CA	5 x 40	8
	120413	Emcon	Turk Island	Turk Island, CA	5 x 35	8
	120420	WMI	Chesnut Ridge	Tennessee	8 x 35	
	120423	Emcon	Hidden Valley	Puyallup, WA	9 x 40	10
	120426	BFI	Sunshine Canyon	California	$13 \times 50$	12
	120435	Grunau	Pheasant Run	Wisconsin	5 x 35	4
	120443	City/Berkeley	City/Berkeley	Berkeley, CA	6 x 35	8
	120445	Donahue	42-2, 22-11-12	Fond Du Lac, WI	$5 \times 35$	
	120454	Environ. Res.	Singleton	San Jose, CA	5 x 35	6
	120456	WMI	Gulf Coast	Ft. Myers, FL	$11 \times 40$	
	120457	BFI		Chicopee, MA	8 x 40	
	120469	BFI	E & E Hauling	· · · · · · · · · · · · · · · · · · ·	•	
	120479	BFI	N/A	Fairfax, VA	$6.5 \times 40$	8 .
	120482	BFI	Disposal Spec.	Bellows Falls, VT	8 x 35	8
	120483	S.D. Warren	S.D. Warren	Skowhegan, ME	5 x 35	6
	120484	WMI	Valley Reclamation		8 x 40	10
	120489	WMI	Valley Trail	Berlin, WI	$6.5 \times 35$	8
	120498	BFI	Holmes Road	Memphis, TN	9 x 40	12
	120499	BFI	Newco Waste	Linwood, NJ	9 x 35	10
	120500	Emcon	Emcon	Puyallup, WA	5 x 24	6
	120508	General Elec.	General Electric	Pennsylvania	5 x 35	6
	120510	BFI	Little Dixie	Jackson, MS	9 x 40	12
	120511	Laidlaw		Plaineville, MA	9 x 40	12
	120512	Homer J. Olsen	City of San Fran.	San Francisco, C	A 5 x 65	4
	120513	Shell Pipeline	Shell Pipeline	Kilgore, TX	5 x 35	6
	120522	Laidlaw	Adrian Landfill	Adrian, MI	8 x 35	10
	120524	BFI	N/A	Hong Kong	8 x 40	12
	120525	WMI	Omega Hills	Menominee Falls	5 × 40	8
	120526	BFI	Laubscher Mdws.	Evansville, IN	11 x 40	16
	120532	Waste Energy	Valley Landfill	Irwin, PA	$10 \times 40$	12
	120533	BFI	Boulder Landfill	Boulder, CO	8 x 35	8
	120535	WMI	Lakeview Landfill	Erie, PA	10 × 40	16
	120538	WMI	York Landfill	Canada	8 x 35	10
	120539	BFI	Chateau Fresno	Fresno, CA	9 x 40	12
	120543	Laidlaw	Southeast	Kansas City, MO	8 x 40	12

#### **BEST AVAILABLE COPY**

Job No.	Client	<u>Landfill</u>	Location	Dia./Ht.	Inlet (In.)
120548	Accurate Mech.	East Landfill West Landfill	DePere, WI Hobart, WI	10 x 40 8 x 40	14 12
120549 120552	BFI BFI	Aubrey Hills Redbird	Northville, MI St. Louis, MO	12 x 50 9 x 40	20 12
120553 120554	WMI WMI	Woodlands Pheasant Run	South Elgin, IL Bristol, WI	9 x 40 8 x 40	12 12
120556 120557	Lakeland J.W. Operating	Oneida County	Rhinelander, WI Babylon, NY	5 x 35 8 x 40	6
120559 120563*	J.W. Operating WMI	Al Turi Landfill Pottstown	Goshen, NY Pottstown, PA	9 x 40 11 x 40	12
130364	BFI	Norris Landfill	Baltimore, MD	10 x 40	14

BKD/SPJ/410 - 10/18/90

<sup>\*</sup> Refurbish 11'  $\times$  40' Flare (originally located at Pompano Beach) and ship to Pottstown, PA. Flare originally sold on Job 120348.

PBS POST, BUCKLEY, SCHUH & JERNIGAN, INC.

SUBJECT: EAST DUVAL SANITARY LANDFILL

CLOSURE - LANDFELL GAS FLARE

COMP. BY: K WHETEHEA CHK. BY: 2 6/21/90 DATE: 6-21-90 SHEET NO .. \_\_ JOB NO .: 22-092.00

MAXIMUM EMISSIONS (IN LBS/HR) PROVIDED BY KYLE SCHOTTS OF MEGELL ENVERONMENTAL SYSTEMS, INC (918) 445-2431 ON 6-19-90 BASED ON 2100 CFM AND 52% METHANE ASSUMPTEONS.

	MAXEMUM EM	ESS TON ACTUAL
CHY	185/HR 55.4	7/4R 242,7
NOX	5.36	23.48
602	14,621	64,040
CO	23. 8Y	104.42
NZ	88,168	386,176
02	15,632	68,468
H26	7,188	31,483

F6. CALCULATION: CH, = 55.4 L95/HR X 24 HAS 10AY x 365 DAYS/YR 485, 304 LBS/1 = 2000LBS

= 242.7 TONS/YR

```
SAMPLE
                                                   PROGRAM
 MIRZA
ASSUMPTIONS:
    Operating Temperature
                                       1,800°F
    Destruction Efficiency
                                           98 %
    Waste Gas Rate (SCFM)
                                       2,100 cf/min
    Methane (CH<sub>4</sub>) Content
                                           52 %
    Carbon Dioxide (CO<sub>2</sub>) Content
                                          48 %
    Latent Heat Value (CH<sub>4</sub>)
                                         910 BTU/SCF
MAXIMUM HEAT RELEASE:
```

2,100 cf/min \* 60 min/hr \* 0.52 CH<sub>4</sub> \* 910 BTU/SCF = 59.6 mmBTU/hr

#### MAJOR COMPONENTS:

@ 14,621 lbs/hr  $CO_2$ @ 7,188 lbs/hr  $H_2O$ @ 88,168 lbs/hr @ 15,632 lbs/hr  $o_2$ 

#### MINOR COMPONENTS:

CO 0.4 lbs/mmBTU = 0.4 \* 59.6 mmBTU/hr = 23.84 lbs/hr0.09 lbs/mmBTU = 0.09 \* 59.6 mmBTU/hr = 5.36 lbs/hrHydrocarbons =

(2,100 cf/min \* 0.52 \* (1-0.98) \* 60 min/hr) = 1,310 cf/hr(1,310 cf/hr / 379.5 SCF/mol) \* 16.04 lbs/mol = 55.4 lbs/hr

DATE

THIS IS PROGRAM
WHICH MIRZA BAIG
HAS A FAY OF

PAGE 1 OF 2

:NOV 13, 1990

\*\*\*\*\*\*\*\*\*\*\*

LANDFILL FLARE MATERIAL AND ENERGY BALANCE WORKSHEET

\*\*\*\*\*\*\*\*\*\*\*\*

CUSTOMER: PBS&J

JOB NO. :FC-900264 DESIGNER:KDS

DESIGNER, RDC

OPERATING TEMP (F) 1800 ATMOS TEMP (F) 100
EXCESS AIR (%) 25 ATMOS PRESS (PSIA) 14.7
HEAT LOSS (BTU/HR) 600000 RELATIVE HUMID (%) 50

WASTE GAS FLOW RATE (SCFM) 2100

CH4 CONTENT OF WASTE STREAM (%) 52 REMAINDER ASSUMED CO2!

INLET WASTE STREAM TEMP. (F) 100

						PRO	DUCTS
,	MOL/HR	LB/HR R	ELEASE	DUTY	SENS. HT	MOL/HR	LB/HR
_******	******	*******	******	******	*******	******	*******
WASTE I	NLET TEM	P (F) =	100		AVG MW =	29.47	
CH4	172.65	2769.73	59.66	26.05	0.05	1820.84	50317.32
CO2	159.37	7013.93	0.00	3.30	0.05	159.37	7013.93
******	******	********	******	******	*******	******	*****
	332.02	9783.65	59.66	29.34	0.09	1980.21	57331.25
AIR FOR WA	STE	INLET TEMP	(F) =	100	AVG MW =	28.70	
		17945.23	0.00	0.00	0.37	22.10	398.16
		11986.31			0.09		
		********			******	******	******
:	2087.87	59931.5	0.00	5.43	0.46	439.67	12384.46
FUEL I	NLET TEM	P (F) = 3.04	100		AVG MW =	0.00	N/A
0	0.07	3.04	0.00	0.03	0.00	1.78	50.45
AIR FOR FU	EL	INLET TEMP	(F) =	100	AVG MW =	28.70	
STOCH AIR	1.67	47.81	0.00	0.00	0.00	0.02	0.40
EXCSS AIR	0.42	11.95	0.00	0.01	0.00	0.42	11.95
*******		*******					
	2.08	59.77	0.00	0.01	0.00	0.44	12.35
QUENCH AIR QUENCH		INLET TEMP	(F) =	100	AVG MW =	28.70	
QUENCH 1	1944.95 5	55829.16	0.00	25.30	0.43	1944.95	55829.16
		******					
		25607.2					125607.7
*******	*******	********	******	******	*******	******	******

***************	*******
SYSTEM ENERGY BALANCE	
****************	******
CENCIDIÉ HEATT INTO CVOTEM (MADELL/HD)	0 00
SENSIBLE HEAT INTO SYSTEM (MMBTU/HR) RELEASE FROM FUEL AND WASTE (MMBTU/HR)	1 50 66
RELEASE FROM FUEL AND WASTE (MMBIU/HR)	*****
	60.65
TOTAL HEAT INTO SYSTEM (MMBTU/HR)	00.00
DUTY FOR WASTE PRODUCTS (MMBTU/HR)	60.11
HEAT LOSS THROUGH VESSEL WALLS (MMBTU/HR)	
MEAT LOSS THROUGH VESSEL WALLS (MMBTO/HR)	****
TOTAL HEAT USED UP IN SYSTEM (MMBTU/HR)	60.71
**************	*******
SYSTEM MATERIAL BALANCE	
**************	******
TOTAL MASS INTO SYSTEM (LB/HR) TOTAL MASS OUT OF SYSTEM (LB/HR)	125607.1
TOTAL MASS OUT OF SYSTEM (LB/HR)	125607.6
***************	*******
COMBUSTION PRODUCTS	<del>.</del>
**************	*******
MOL/HR LB/HR MOLE	
***************	
CO2 332.2 14621.4 7	.6 11.6
H2O 399.0 7187.6 9	.1 5.7
	.1 70.2
02 488.5 15631.5 11	.2 12.4
****************	*****
4367.1 125608.3	
AVG. MW = 28.763	
TOTAL AIR REQD (SCFM) 25520.7 FURNACTOTAL AIR REQD (LB/HR) 115820.5	E ACFS 2001.14
MOLAL HUMIDITY OF ATM AIR (MOL H2O/MOL B.D.A.)	= 0.0134
·	

*********	**************************************		*******
*********			*******
	TOTAL INLET WASTE		332.0158
<b></b> 1	CH4 IN WASTE MOL	/HR	172.6482
	CH4 IN WASTE LB/		2769.726
<b>S</b>	CO2 IN WASTE MOL		159.3675
		•	7013.926
	CO2 IN WASTE LB/	nk .	7013.920
	TOTAL INLET WASTE	RATE LB/HR	9783.653
RELATIVE HUMIDITY	ASSUME 1 MOL WET	AIR BASIS	
	PARTIAL PRESSURE	OF WATER IN WET AI	R PSIA 0.1945
	MOLE FRACTION OF		0.013231
	BONE DRY AIR MOLE		0.986768
	MOLAL HUMIDITY	· ·	
	AVERAGE MW OF AIR		28.70467
	MOLE FRACTION OF 1		0.780040
	MOLE FRACTION OF (	D2 IN AIR	0.206728
2	OMOGU AID DEGUIDE	D DOD WAGED WOLL	up 1670 202
2	<del>-</del>	D FOR WASTE MOL/	
	STOCH AIR REQUIRE	D FOR WASTE LB/HR	47945.22
3	FYCESS AID DECITED	ED FOR WASTE MOL	/HR 417.5732
		ED FOR WASTE LB/H	•
	EXCESS AIR REQUIRE	D FOR WASIE LEYN	r 11900.30
4	FUEL FLOW RATE I	LB/HR	3.036437
MIN FUEL		MOL/HR	- 0.068869
CALCS	TODD TOOM WITH		
5	STOCH AIR REQUIRES	FOR FUEL MOL/H	R 1.665691
		FOR FUEL LB/HR	
6	EXCESS AIR REQUIRE	ED FOR FUEL MOL/	HR 0.416422
	EXCESS AIR REQUIRE	ED FOR FUEL LB/H	R 11.95328
	•		
7	QUENCH AIR	MOL/HR	1944.949
·	402.00.	LB/HR	55829.16
		22,	00020120
8	THEORETICAL PRODUC		
	•	MOL/HR	LB/HR
		172.6482	7598.420
		345.2964	6220.860
	N2 WSTN2PD	1302.896	36498.04
	******	*******	*****

		TOTAL		1820.84 METHPRO		50317.32 METHPRLB	
		THEORETICA					*
		CO2 ******	******		5	LB/HR 7013.926 ******	
		TOTAL THEO					
10		EXCESS AIR EXCESS AIR					417.5732 11986.30
13		EXCESS AIR EXCESS AIR					0.416422 11.95328
9		WATER IN ST					
12		WATER IN ST					
11		H2O FU N2 FU *******	******** JCO2PD JH2OPD JN2PD ******	******** MOL/HR 0.206607 0.275476 1.299307 *****	******	**************************************	·
		TOTAL		1.781390 MFPRDMOL		50.45346 MFPRDLB	
14		QUENCH AIR			MOL/HR LB/HR		1944.949 55829.16
	CHECK FOR ************************************	**************************************	N MATER ****** LANCE E	IAL BALA ******* QUATION	NCE ******** LB'S MAS	******** S BASIS	******
	SYSTE	M INPUTS ******	= ****	*****	SYSTEM O	UTPUTS	<b>. 't</b>

2089.948

0.463370

SUMMARY OF TOTAL AIR REQUIREMENTS EXCLUDING ONLY QUENCH AIR

******	******				******	*******
	*****		RGY BALA	· · <del>-</del> —		
****	****	****	****	• • • • • • • • • • • • •		****
				RANGES FOR		_
	*******	*******	******	******	******	*****
	COMPONENT				SPEC HT	• •
•				********	*****	
	CH4	100	TO	100		8.55232
	CO2	100	TO	100		9.169516
	CO2 (AVG)	100	TO	1800		12.16430
	02	100	TO	100		7.009529
	O2 (AVG) N2	100	TO	1800		8.013736 6.89016
	N2 N2 (AVG)	100 100	TO TO	100 1800		7.528297
	H2O	100	TO	100		7.92664
	H2O (AVG)	100	TO	1800		9.28919
	AIR	100	TO	100		6.928551
	AIR (AVG)	100	TO	1800		7.651950
	0	100	TO	100		17.6
	-			*********	*******	
						<b>=</b>
				<del>_</del>		
1	HEAT CONTAIN					0.047249
	HEAT CONTAIN	ED IN ENTE	ERING CO2	2 IN WASTE (M	(MBTU/HR)	0.046762
		·				
	TOTAL HEAT C	ONTAINED I	IN WASTE	STREAM (MMBT	'U/HR)	0.094011
9	HEAT RELEASE	D BY COMBI	ISTION OF	CUA (MMPTIIA	'מם /	59.65708
2	HEAT RELEASE	D BI COMBO	SIION OF	Ch4 (MMBIU)	nk)	33.03100
		•				
3	HEAT CONTAIN	ED IN ENTE	RING FUE	EL (MMBTU/HR)	ı	0.000036
				,		
		• •				
4	HEAT RELEASE	D BY COMBU	STION OF	F FUEL (MMBTU	/HR)	0.06
_	momat *******			MOT (115)		
5	TOTAL INCOMI	NG AIR FLO	WKATE (	MOL/HR)		

FROM MATERIAL BALANCE ADD 2 + 3 + 5 + 6

TOTAL HEAT CONTAINED IN ENTERING AIR (MMBTU/HR)

## 6 HEAT IN ENTERING QUENCH AIR WILL BE DETERMINED LATER TOTAL OF HEAT INPUTS INTO SYSTEM 1 +2 +3 + 4 + 5 AA 60.27449 7 HEAT LOSS THROUGH VESSEL WALLS (MMBTU/HR) 0.6 8 HT TO RAISE CO2 PRDCD FRM CMB CH4 TO OPTG T (MMBTU/HR)3.570246 HT TO RAISE H20 PRDCD FRM CMB CH4 TO OPTG T (MMBTU/HR)5.452791 HT TO RAISE N2 PRDCD FRM CMB CH4 TO OPTG T (MMBTU/HR) 16.67460 HT TO RAISE H20 IN S.A.FOR WST TO OPTG T (MMBTU/HR) 0.348997 HT TO RAISE CH4 PROD TO OPTINGT 26.04664 HT TO RAISE CO2 IN WASTE TO OPTING T (MMBTU/HR) 3.295612 TOTAL HEAT TO RAISE WASTE PROD UP TO OP T (MMBTU/HR) 29.34225 9 HT TO RAISE XCSS AIR FOR CH4 TO OPTINGT (MMBTU/HR) 5.431925 10 HT TO RAISE CO2 PRDCD FRM FUEL TO OP T (MMBTU/HR) 0.004272 HT TO RAISE H2O PRDCD FRM FUEL TO OP T (MMBTU/HR) 0.004350 HT TO RAISE N2 PRDCD FRM FUEL TO OP T (MMBTU/HR) 0.016628 HT TO RAISE H2O IN S.A. FOR FUEL TO OPTG T (MMBTU/HR) 0.000348 TOTAL HT TO RAISE FUEL PRODUCT TO OP T (MMBTU/HR) 0.025599 11 HT TO RAISE XCSS AIR FOR FUEL TO OP T (MMBTU/HR) 0.005416 TOTAL HEAT IN EXITING PRODUCTS (MMBTU/HR) 35.40519 BB7 + 8 + 9 + 10 + 11DUTY OF QUENCH AIR = BB - AA (MMBTU/HR) -24.8693QUENCH AIR REQUIRED (MOL/HR) 1944.949 QUENCH AIR REQUIRED (LB/HR) 55829.16 6 HEAT IN ENTERING QUENCH AIR (MMBTU/HR) 0.431221

12 HEAT ABSORBED BY Q.A. IN GOING UP TO OP T (MMBTU/HR) 25.30052

### COMPOSITION OF QUENCH AIR

	MOL/HR	LB/HR
O2	402.0757	12866.42
N 2	1517.140	42499.64
H20	25.73420	463.6273
******	*****	*****
TOTAI.	1944.949	55829.69



Pollution Control Systems

5800 West 68th Street Post Office Box 9667 Tulsa, Okiahoma 74157-0667 Telephone: 918-445-2431 FAX: 918-446-3892

Date 3/5/4/ By\_KOS Sheet\_

Emission Calculations for Minor Components See attached trasil & 1800 F Operating Tomp. Energy Balance for (Asot) Rasis : Major Component emissions 8X40 Vessel

2100 SCFM Londill Gas 51% Methone

59.6 MIRTU/HR Heat Release (See attached Mat 1 & Engy Bal)

Min Hydrocarbon Destruction Efficiency = 98% Fest Oata: CO emission rate 0.4 #/1717 BTU Refersed
NO. " 0.9 4/1717 BT - Reposed Based on Tests on Actual Units

Methone Methone in = (2100 SCFIT X TOO Methone) = 379.5 Mol Calculations: x60 = 172,65 mo/hr

98% of Methone will be destroyed : 2% will be emitted

CH4 in Flor Gos = .02 x 172.65 = 3.453 = x16.04 = 55.39 #/

: CH4 Emitted = 55.39 6/21

CO Calculations: CO emission rate = 0.4 #100

Heat Release = 59.6 MTIBN

: CO Emitted = . 4 FABO- X 59.6 MABN = 23.84 1/2

Nox Colsulations: NOx emission rate = 0.9 ATIBI-Rikessel

00 NO, Em. Hol= .9 FROX X 59.6 mm = 53.64 % -

PAGE 1 OF 2

TO

# LANDFILL FLARE MATERIAL AND ENERY BANLANCE WORKSHEET

CUSTOMER: PBS&J JOB NO. : DATE :MARCH 6, 1991 DESIGNER: K. SHOTTS

OPERATING TEMP (F) 1800 EXCESS AIR (%) 25 HEAT LOSS (BTU/HR) 600000 ATMOS TEMP (F) 100 ATMOS PRESS (PSIA) 14.7 RELATIVE HUMID (%) 50

WASTE GAS FLOW RATE (SCFM)
CH4 CONTENT OF WASTE STREAM (%)
INLET WASTE STREAM TEMP. (F)

2100 52 REMAINDER ASSUMED CO2! 100

Landfill Gos Heat Release **PRODUCTS** MOL/HR LB/HR RELEASE > DUTY SENS. HT MOL/HR LB/HR \*\*\*\*\*\*\*\*\*\*\*\*\*\*\*\* WASTE INLET TEMP (F) =100 AVG MW = 29.47 INLET TEMP (F) = AIR FOR WASTE 100 AVG MW = 28.70 STOCH AIR 1670.29 47945.23 0.00 0.00 0.37 22.10 398.16 EXCSS AIR 417.57 11986.31 0.09 417.57 11986.31 0.00 5.43 \*\*\*\*\*\*\*\*\*\*\*\*\*\*\* 2087.87 59931.5 0.00 5.43 0.46 439.67 12384.46 INLET TEMP (F) = FUEL 100 AVG MW = 0.00 0.00 0.07 3.04 0.03 0.00 1.78 50.45 AIR FOR FUEL INLET TEMP (F) =100 AVG MW = 28.70 1.67 STOCH AIR 0.00 47.81 0.00 0.00 0.02 0.40 0.42 EXCSS AIR 11.95 0.00 0.01 0.00 0.42 11.95 \* 2.08 59.77 0.00 0.01 0.00 0.44 12.35 QUENCH AIR INLET TEMP (F) = 100 AVG MW = 28.70 QUENCH 1944.95 55829.16 0.00 25.30 0.43 1944.95 55829.16 \* TOTAL 4366.98 125607.2 59.66 60.11 0.99 4367.05 125607.7

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#### PAGE 2 OF 2

**************************************	
SENSIBLE HEAT INTO SYSTEM (MMBTU/HR) RELEASE FROM FUEL AND WASTE (MMBTU/HR)	****
TOTAL HEAT INTO SYSTEM (MMBTU/HR)  DUTY FOR WASTE PRODUCTS (MMBTU/HR)  HEAT LOSS THROUGH VESSEL WALLS (MMBTU/HR)	60.65
TOTAL HEAT USED UP IN SYSTEM (MMBTU/HR)	******* 60.71
SYSTEM MATERIAL BALANCE  ***********************************	**************************************

		MOL/HR	LB/HR	MOLE &	WT %	
,	*****	******	*****	****	****	~~~
components -Emissions	co2 کے		14621.4	7.6	11.6	<
1 am Por	7 H2O	399.0	7187.6	9.1	5.7	_/
55.64 S	Z N2		88167.7		70.2	
Emily	<u> </u>	488.5	15631.5	11.2	12.4	<b>_</b>
	*****	******	******	*****	*****	)
			125608.3			

AVG. MW = 28.763

TOTAL AIR REQD (SCFM) 25520.7 FURNACE ACFS 2001.14
TOTAL AIR REQD (LB/HR) 115820.5
MOLAL HUMIDITY OF ATM AIR (MOL H2O/MOL B.D.A.) = 0.0134

### **BEST AVAILABLE COPY**



ENGINEERING PLANNING

November 12, 1992

Mr. Steve Smallwood, P.L.
Director - Bureau of Air Regulation
Florida Department of Environmental Regulation
Twin Towers Office Building
2600 Blair Stone Road
Tallahassee, Florida 32399-2400

RE: EAST DUVAL SANITARY LANDFILL

FDER File No. AC 16-186047 Equivalent Flare Notification

Dear Mr Smallwood:

On behalf of the City of Jacksonville, Post, Buckley, Schuh & Jernigan, Inc. (PBS&J) submits the following information for the East Duval Sanitary Landfill's enclosed flare system.

In accordance with Specific Condition No. 1 of the Construct/Operate Air Pollution Source Permit No. AC-186047, PBS&J requests written approval on an equivalent flare.

The Engineer has reviewed LFG Specialties, Inc. Model No. EF840S4 and has found it to be an equal to IT-McGill Model No. EGF-60.

Please contact our office if you should have comments or questions. I will look forward to your response.

Sincerely,

Karl Schmit, E.I.

Project Engineer Solid Waste Division

Kare A Schnise

cer. Hamaker/City of Jacksonville E. Hilton/PBS&J

KS/cla/FLARESC

07-421.05